

PSSE Year 0 Topology 0 Analysis

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Contents

1	Introduction	4
1.1	Study Description	4
1.2	Contingency Analysis	5
2	Contingency Limit Violations	7
2.1	Introduction	7
2.2	Branch Overload Violation	7
2.3	Upper Emergency Bus Voltage Violation	7
2.4	Lower Emergency Bus Voltage Violation	7
3	Dynamic Stability Analysis	8
3.1	Introduction	8
3.2	BUS 151	8
3.3	BUS 205	9
3.4	SING OPN LIN 11 202-203(1)	10
4	Conculsion	11
	Appendix	12
4.1	Python program to check dynamic stability of the system for contingencies reporting violations . . .	12

List of Figures

1.1	Single Line Diagram Year 0, Topology 0	4
1.2	System Totals for Year - 0, Topology - 0	5
1.3	The subsystem file corresponding to Year 1 Topology 1	5
1.4	The monitored file corresponding to Year 1 Topology 1	5
1.5	The contingency file corresponding to Year 1 Topology 1	6
3.1	Progress bar output for Bus fault at BUS 151	8
3.2	Progress bar output for Bus fault at BUS 151 - continued	8
3.3	Progress bar output for Bus fault at BUS 151 - continued	9
3.4	Progress bar output for Bus fault at BUS 205 - continued	9
3.5	System Totals for Year - 0, Topology - 0	10

List of Tables

2.1	Branch Loaded greater than 100% for Topology 0	7
2.2	Upper emergency range violation for Topology 0	7

Chapter 1

Introduction

1.1 Study Description

The Year 0 Topology 0 contingency analysis of the hypothetical SAVNW system is carried out to report the branches reporting loading greater than 100% and buses reporting upper and lower voltage limit violations.

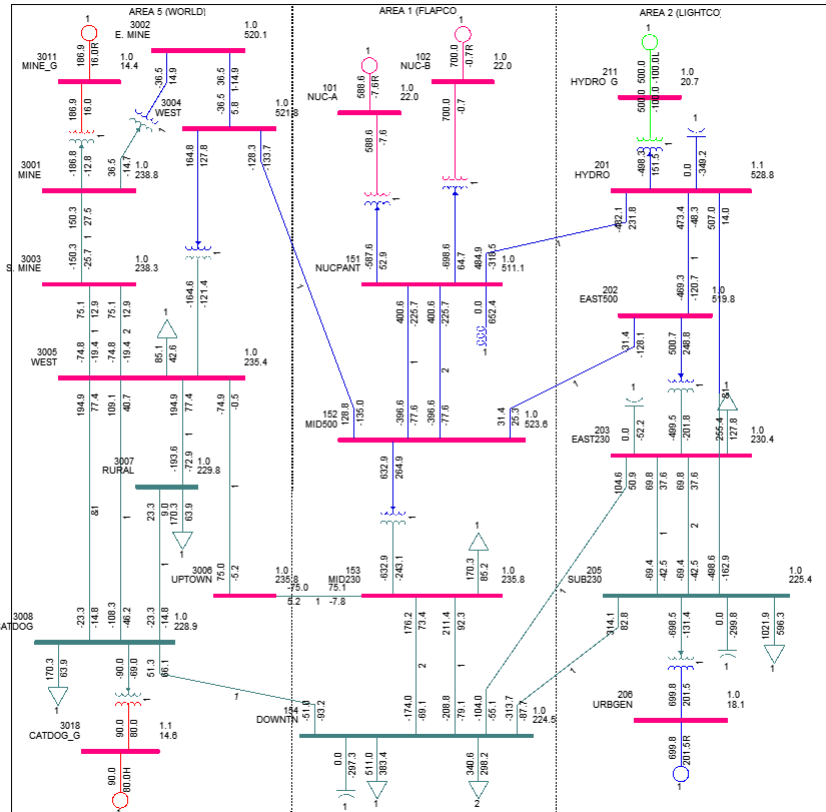


Figure 1.1: Single Line Diagram Year 0, Topology 0

For the hypothetical SAVNW system, the Year 0 Topology 0 of the system represents the present year system as shown in Figure 1.1. There are 6 generators in 3 areas. Total installed capacity of the system is the sum of firm capacity provided by 6 generating units and equals 4153.25 MW.

Detailed analysis of Year 0 Topology 0 Base Case was carried out and can be found here. The combined total generation in all areas of 2765 MW is serving a total load of 2723 MW with the generators 102 NUC-B, 211-HYDRO_G, 3018-CATDOG_G operating at their nominal power output of 700 MW, 500 MW and 90 MW respectively. The swing generator in each area operates to meet the load, loss and interchange criteria. The desired

interchange for all the scenarios studied is highlighted in Figure 1.2. For all the scenarios studied the desired interchange from FLAPCO to LIGHTCO is 100 MW, and from FLAPCO to WORLD is 150 MW.

X-- AREA --X	FROM GENE- RATION	-----AT FROM IND GENERATN	AREA BUSES----- TO IND MOTORS	TO LOAD	TO BUS SHUNT	TO GNE BUS DEVICES	TO LINE SHUNT	TO XFRMR MAGNE- TIZING	FROM CHARGING	TO LOSSES	-NET TO TIE LINES	INTERCHANGE- TO TIES + LOADS	DESIRED NET INT
1 FLAPCO	1288.6 -8.2	0.0 0.0	0.0 0.0	1021.9 766.7	0.0 355.0	0.0 0.0	0.0 -0.0	0.0 -0.0	0.0 878.1	15.3 317.3	251.5 -569.2	1103.0 112.3	250.0
2 LIGHTCO	1199.8 101.5	0.0 0.0	0.0 0.0	1277.3 724.1	0.0 -701.1	0.0 0.0	0.0 -0.0	0.0 -0.0	0.0 651.0	21.1 396.2	-98.6 333.3	-950.2 -348.2	-100.0
5 WORLD	276.9 96.0	0.0 0.0	0.0 0.0	425.7 170.4	0.0 -0.0	0.0 0.0	0.0 -0.0	0.0 -0.0	0.0 366.0	4.1 55.8	-152.9 235.9	-152.9 235.9	-150.0
COLUMN TOTALS	2765.3 189.3	0.0 0.0	0.0 0.0	2724.8 1661.2	0.0 -346.1	0.0 0.0	0.0 0.0	0.0 0.0	0.0 1895.2	40.5 769.3	0.0 0.0	0.0 0.0	0.0

Figure 1.2: System Totals for Year - 0, Topology - 0

1.2 Contingency Analysis

AC contingency calculation was conducted on the hypothetical SAVNW system for Year 0 Topology 0. The configuration files used are:

- Subsystem file savnw.sub - Studied subsystems of the studied case defined via the Subsystem Definition data file (Figure 1.3)
- Monitor file savnw.mon - Monitored Element Data File identifies the branches that are to be monitored for flow violations and the buses that are to be monitored for voltage violations (Figure 1.4)
- Contingency file savnw.con - Contingency cases that are to be tested are defined in the Contingency Definition data file (Figure 1.5)

```
SUBSYSTEM CON
AREA 1
AREA 2
AREA 5
END

SUBSYSTEM MON
AREA 1
AREA 2
AREA 5
END

END
```

Figure 1.3: The subsystem file corresponding to Year 1 Topology 1

```
MONITOR VOLTAGE RANGE ALL BUSES 0.9 1.1
MONITOR ALL BRANCHES
MONITOR TIES FROM AREA 1 TO AREAS 2 5
MONITOR TIES FROM AREA 2 TO AREA 5
END
END
```

Figure 1.4: The monitored file corresponding to Year 1 Topology 1

```

SINGLE BRANCH IN AREA 1
SINGLE BRANCH IN AREA 2
SINGLE BRANCH IN AREA 5
SINGLE BUS IN AREA 1
SINGLE BUS IN AREA 2
SINGLE BUS IN AREA 5
SINGLE MACHINE IN AREA 1
SINGLE MACHINE IN AREA 2
SINGLE MACHINE IN AREA 5
END

```

Figure 1.5: The contingency file corresponding to Year 1 Topology 1

The API DFAX_2 is used to construct distribution factor data files corresponding to the case .sav file, and the defined .sub, .mon, .con configuration files. By running the AC contingency calculation function ACCC_WITH_DSP_3, the contingency solution output .acc files is obtained.

Python code to conduct AC contingency calculation is:

```

import psspy
psspy.case(r""savnw.sav"")
psspy.fdns([0,1,0,0,0,0,99,0])
psspy.dfax_2([1,1,0],r""savnw.sub"",r""savnw.mon"",r""savnw.con"",r""savnw.dfx"")
psspy.accc_with_dsp_3(0.1,[0,0,0,0,1,2,0,0,0,2,0],r""CON"",r""savnw.dfx"",r""savnw.acc"",",
    "", "")

```

Using the contingency solution output file savnw.acc, the results is exported as an excel file for further analysis. The results exported are ACCC Analysis Summary, Monitored Branch Flow (MVA), Monitored Bus Voltage.

Python code to export AC contingency solution output file as excel is:

```

import psspy
import pssexcel
pssexcel.accc('savnw.acc', ['s','b'], colabel='', type='contingency', busmsm=0.5, sysmsm=5.0,
    rating='a', namesplit=False, xlsfile='out.xlsx', sheet='', overwritesheet=True,
    show=False, ratecon='b',
    baseflowvio=False, basevoltvio=False, flowlimit=100.0, flowchange=0.0, voltchange=0
    .0, swdrating='a',
    swdratecon='b', baseswdfio=False, basenodevoltvio=False, overloadreport=False)

```

Contingency analysis was carried out in PSSE for the studied case for Year 0 Topology 0. It was seen that the power flow solution did not converge for some of the tested contingencies. For the studied case, 42 contingencies were converged out of the 47 contingencies tested, the contingencies not converged are UNIT 206(1), SING OPN LIN 14 205-206(1), BUS 152, BUS 154, BUS 201.

For the converged contingencies for the studied case, the result of the contingency analysis is analysed to check for branch overload ($> 100\%$) and out of range bus voltage violations (lower emergency limit $< 0.9PU$ and upper emergency limit $> 1.1PU$). It was seen that for some of the contingencies there were no branch overload or bus voltage violations reported. Rest of the contingencies violating branch overload and bus voltage emergency range violation are reported. Chapter 2 gives the observed branch flow violations, upper and lower emergency voltage violations for the studied case. As load flow analysis checks the power balance of the network at the instant the fault occurred on the system, it will not give the information regarding the dynamic behaviour of the system. Chapter 3 gives the result of the dynamic stability analysis carried out to see if the system is stable after the occurrence of the fault. To conclude, Chapter 4 summarises the results of all the analysis carried out on Year 0, Topology 0 of the hypothetical SAVNW system.

Chapter 2

Contingency Limit Violations

2.1 Introduction

In this chapter, for Year 0, Topology 0, the branches that are loaded more than 100% of their rating, and buses violating the upper and lower emergency ratings are reported.

2.2 Branch Overload Violation

For Year 0, Topology 0, loading violations were reported for 3 branches 153-154(1), 3001-3003(1), and 154-203(1). For the branch 153-154(1), loading of 102.62% was reported for the contingency SING OPN LIN 11 202-203(1). The branch 3001-3003(1), reporting a loading of 199.87% for the contingency BUS 151 is considered as severe/ critical loading. For the branch 154-203(1), loading of 117.68 was reported for the contingency BUS 205. The Table gives the loading violations in tabular form.

BRANCH	CONTINGENCY	MVAFLOW	AMPFLOW	RATE	RATE1/RATE2	Loading
153-154(1)	SING OPN LIN 11 202-203(1)	-349.97	359.16		350.00	102.62
3001-3003(1)	BUS 151	616.28	599.62		300.00	199.87
154-203(1)	BUS 205	266.19	294.19		250.00	117.68

Table 2.1: Branch Loaded greater than 100% for Topology 0

2.3 Upper Emergency Bus Voltage Violation

The only upper voltage violation was reported by the bus 201 for the bus fault at bus 151 labelled BUS 151. The reported violation is tabulated in Table 2.2.

BUS	CONTINGENCY	BASE VOLTS	CONT VOLTS	RANGE VIO
201	BUS 151	1.058	1.101	0.001

Table 2.2: Upper emergency range violation for Topology 0

2.4 Lower Emergency Bus Voltage Violation

There was no lower emergency voltage limit violation reported for the studied case for the Year 0 Topology 0.

Chapter 3

Dynamic Stability Analysis

3.1 Introduction

As load flow analysis checks the power balance of the network at the instant the fault occurred on the system, it will not give the information regarding the dynamic behaviour of the system. Dynamic stability analysis is carried out to see if the system is stable after the occurrence of the fault. From chapter 2, the faults causing overloading and/ or voltage limit violations are 'BUS 205', 'SING OPN LIN 11 202-203(1)', 'BUS 151'. Dynamic simulation is carried out on the studied case by applying each individual fault at TIME = 2 Seconds to check the dynamic stability of the faulted system. The python script used to carry out this simulation is given in the Appendix 4 of the document.

3.2 BUS 151

Dynamic simulation was conducted on the system for a bus fault at bus 151. When the bus fault at bus 151 was applied on the system at 2.0 seconds, Network not converged was first reported at TIME = 2.1167 seconds (Figure 3.1). At TIME = 3.175 seconds, 3 bus(es) in island(s) were reported (Figure 3.2). At TIME = 4.9667 seconds, 19 bus(es) in island(s) with no in-service machines was reported (Figure 3.3). Hence, the system is not dynamically stable for a bus fault at BUS 151.

```
Network not converged at TIME = 2.1167
Network not converged at TIME = 2.125
```

Figure 3.1: Progress bar output for Bus fault at BUS 151

```
AT TIME = 3.175 VOLTAGES OUTSIDE OF BAND 0.50000 TO 1.50000:

X----- B U S -----X VOLTAGE      X----- B U S -----X VOLTAGE
101      [NUC-A      21.600] 0.20868LO    102      [NUC-B      21.600] 0.00000LO
151      [NUCPANT    500.00] 0.00000LO

3.1750  0.0000      0.0000      0.0000      0.0000      237.21      617.52
7       552.14      0.0000      226.79      0.0000      887.23      887.30
13      1.3039      0.88552      1.2939      1.3291      0.83704      1.2811
19      1.2812      6.43503E-02      0.0000      9.1740      5.3491      13.489
25      0.0000      3.0499      0.0000      3.6616      1.7310      0.89153
31      0.0000      0.20829      0.0000      0.95247      1.3220      1.2858
37      0.0000      0.20868      7.67088E-07      0.95247      1.3220      1.2858
43      0.0000

3 bus(es) in island(s) with no in-service machines
The following buses are disconnected:
BUS#-SCT X-- NAME --X BASKV      BUS#-SCT X-- NAME --X BASKV      BUS#-SCT X-- NAME --X BASKV
101      NUC-A      21.600      102      NUC-B      21.600      151      NUCPANT      500.00
```

Figure 3.2: Progress bar output for Bus fault at BUS 151 - continued

```
Power unbalance=*****; Threshold= 1.10000
MACHINE 1 AT BUS 3011 [MINE_G 13.800] TRIPPED AT TIME = 4.9667
```

Network not converged at TIME = 4.9667

AT TIME = 4.967 VOLTAGES OUTSIDE OF BAND 0.50000 TO 1.50000:

```
X----- B U S -----X VOLTAGE      X----- B U S -----X VOLTAGE
152 [MID500 500.00]*****HI 153 [MID230 230.00]*****HI
154 [DOWNTN 230.00]*****HI 201 [HYDRO 500.00]*****HI
202 [EAST500 500.00]*****HI 203 [EAST230 230.00]*****HI
204 [SUB500 500.00]*****HI 205 [SUB230 230.00]*****HI
206 [URBGEN 18.000]*****HI 211 [HYDRO_G 20.000]*****HI
3001 [MINE 230.00]*****HI 3002 [E. MINE 500.00]*****HI
3003 [S. MINE 230.00]*****HI 3004 [WEST 500.00]*****HI
3005 [WEST 230.00]*****HI 3006 [UPTOWN 230.00]*****HI
3007 [RURAL 230.00]*****HI 3008 [CATDOG 230.00]*****HI
3011 [MINE_G 13.800]*****HI

4.9667 0.0000 0.0000 0.0000 0.0000 1.09211E+19 1.30051E+20
7 1.26405E+20 0.0000 1.03619E+19 0.0000 5.03233E+19 5.59668E+19
13 2.94688E+08 4.35145E+08 3.94863E+08 3.33065E+08 4.37460E+08 1.60471E+08
19 1.78467E+08 0.0000 0.0000 0.0000 0.0000 -2.16108E+11
25 0.0000 0.0000 0.0000 0.0000 0.0000 -5.13488E+12
31 0.0000 0.0000 0.0000 0.0000 0.0000 3.49605E+05
37 0.0000 0.0000 0.0000 4.34224E+08 3.94863E+08 1.24794E+08
43 0.0000
```

19 bus(es) in island(s) with no in-service machines

The following buses are disconnected:

BUS#-SCT	X--	NAME	--X	BASKV	BUS#-SCT	X--	NAME	--X	BASKV	BUS#-SCT	X--	NAME	--X	BASKV
152		MID500		500.00	153		MID230		230.00	154		DOWNTN		230.00
201		HYDRO		500.00	202		EAST500		500.00	203		EAST230		230.00
204		SUB500		500.00	205		SUB230		230.00	206		URBGEN		18.000
211		HYDRO_G		20.000	3001		MINE		230.00	3002		E. MINE		500.00
3003		S. MINE		230.00	3004		WEST		500.00	3005		WEST		230.00
3006		UPTOWN		230.00	3007		RURAL		230.00	3008		CATDOG		230.00
3011		MINE_G		13.800										

Figure 3.3: Progress bar output for Bus fault at BUS 151 - continued

3.3 BUS 205

Dynamic simulation conducted on the system with fault applied at Bus 205 at TIME = 2.0 seconds. At TIME = 6.558 seconds, 21 bus(es) in island(s) with no in-service machines was reported and the bus disconnected from the system were reported. Hence, the system is not dynamically stable for a bus fault at BUS 205.

AT TIME = 6.558 VOLTAGES OUTSIDE OF BAND 0.50000 TO 1.50000:

```
X----- B U S -----X VOLTAGE      X----- B U S -----X VOLTAGE
102 [NUC-B 21.600] 0.44607LO 151 [NUCPANT 500.00] 0.44607LO
152 [MID500 500.00] 0.21566LO 153 [MID230 230.00] 0.17566LO
154 [DOWNTN 230.00] 0.02762LO 201 [HYDRO 500.00] 0.30992LO
202 [EAST500 500.00] 0.19825LO 203 [EAST230 230.00] 0.09376LO
204 [SUB500 500.00] 0.10468LO 205 [SUB230 230.00] 0.00000LO
211 [HYDRO_G 20.000] 0.30992LO 3001 [MINE 230.00] 0.14231LO
3002 [E. MINE 500.00] 0.14619LO 3003 [S. MINE 230.00] 0.14027LO
3004 [WEST 500.00] 0.16050LO 3005 [WEST 230.00] 0.13265LO
3006 [UPTOWN 230.00] 0.16338LO 3007 [RURAL 230.00] 0.09603LO
3008 [CATDOG 230.00] 0.07039LO 3011 [MINE_G 13.800] 0.14231LO

6.5583 52.316 43.485 8.2551 6.8819 4.1568 116.51
7 85.348 117.77 14.051 55.697 3.7696 3.7157
13 0.17566 2.76161E-02 0.30992 0.19825 9.37593E-02 0.14231
19 0.14027 1.1741 0.0000 0.0000 0.0000 0.0000
25 0.0000 13.216 0.0000 0.0000 0.0000 0.0000
31 0.0000 0.72615 0.0000 0.0000 0.0000 0.0000
37 0.0000 0.71372 0.44607 0.0000 0.30992 0.14231
43 0.0000
```

21 bus(es) in island(s) with no in-service machines

The following buses are disconnected:

BUS#-SCT	X--	NAME	--X	BASKV	BUS#-SCT	X--	NAME	--X	BASKV	BUS#-SCT	X--	NAME	--X	BASKV
101		NUC-A		21.600	102		NUC-B		21.600	151		NUCPANT		500.00
152		MID500		500.00	153		MID230		230.00	154		DOWNTN		230.00
201		HYDRO		500.00	202		EAST500		500.00	203		EAST230		230.00
204		SUB500		500.00	205		SUB230		230.00	211		HYDRO_G		20.000
3001		MINE		230.00	3002		E. MINE		500.00	3003		S. MINE		230.00
3004		WEST		500.00	3005		WEST		230.00	3006		UPTOWN		230.00
3007		RURAL		230.00	3008		CATDOG		230.00	3011		MINE_G		13.800

Figure 3.4: Progress bar output for Bus fault at BUS 205 - continued

3.4 SING OPN LIN 11 202-203(1)

Dynamic simulation was conducted with bus fault applied at 2.0 seconds. It was seen that the system was dynamically stable. Slight overloading was reported (Figure 3.5) for the branch 153-154(1) similar to the overload reported in Table 2.1 from the contingency analysis.

```
SUBSYSTEM LOADING CHECK (INCLUDED: LINES; BREAKERS AND SWITCHES; TRANSFORMERS) (EXCLUDED: NONE)
LOADINGS ABOVE 100.0 % OF RATING SET 2 (MVA FOR TRANSFORMERS, CURRENT FOR NON-TRANSFORMER BRANCHES):

X----- FROM BUS -----X X----- TO BUS -----X
BUS#-SCT X-- NAME --X BASKV AREA BUS#-SCT X-- NAME --X BASKV AREA CKT LOADING RATE2 PERCENT
153 MID230 230.00 1 154 DOWNTN 230.00* 1 1 360.9 350.0 103.1
```

Figure 3.5: System Totals for Year - 0, Topology - 0

Chapter 4

Conculsion

The contingency analysis was carried out on the hypothetical SAVNW study system for the Year 0, Topology 0 to study the (N-1) bus, single line open, unit contingencies. Out of all the studied (N-1) contingencies, the contingencies for which the system did not converge are the contingencies UNIT 206(1), SING OPN LIN 14 205-206(1), BUS 152, BUS 154, BUS 201.

For the converged contingency scenarios, Chapter 2 reported the branch overload, upper and lower limit voltage violations. From the branch overload table, Table 2.1 branches reporting loading greater than 130% was the branch 3001-3003(1), for a bus fault BUS 151. There was a slight violation from upper emergency voltage value for Bus 201 and no lower limit voltage violations were reported for any of the studied Buses.

In the Chapter 3 for the faults reporting the violations, dynamic simulations were carried out to determine the dynamic stability of the system. For the bus fault at buses 151 and 205, the system was not dynamically stable. For the single line open 202-203(1), the system was dynamically stable with the branch 153-154(1) still reporting overload violations.

Hence it can be concluded that in addition to the contingencies not converging reported by contingency analysis, the contingencies corresponding to the bus faults BUS 151 and BUS 205 also causes system to be unstable.

Appendix

4.1 Python program to check dynamic stability of the system for contingencies reporting violations

```
import psspy
psspy.case(r""savnw.sav"")
psspy.fdns([0,1,0,0,0,1,99,0])
psspy.cong(0)
psspy.conl(0,1,1,[0,0],[40.0,30.0,40.0,30.0])
psspy.conl(0,1,2,[0,0],[40.0,30.0,40.0,30.0])
psspy.conl(0,1,3,[0,0],[40.0,30.0,40.0,30.0])
psspy.ordr(1)
psspy.fact()
psspy.tysl(1)
psspy.dyre_new([1,1,1,1],r""savnw.dyr""",",",",")
psspy.set_ossca2(1,1,0)
psspy.set_relsca(1)
psspy.set_vltscn(1,1.5,0.5)
psspy.set_genpwr(1,1.1)
psspy.set_genang3(1,180.0,0.0,1)
psspy.set_genspdev(1,10.0,1)
psspy.set_volt_viol_subsys_flag(0)
psspy.set_voltage_dip_check(1,0.8,0.2)
psspy.set_voltage_rec_check(1,1,0.8,0.4,0.9,1.0)
psspy.set_netfrq(1)
psspy.set_relang(1,0,"")
psspy.bsys(1,0,[0.0,0.0],0,[],8,[153,154,202,203,3001,3003,203,201],0,[],0,[])
psspy.chsb(1,0,[1,9,1,1,17,0])
psspy.bsys(1,0,[0.0,0.0],0,[],7,[153,154,202,203,3001,3003,201],0,[],0,[])
psspy.chsb(1,0,[13,21,37,1,13,0])
psspy.strt2([0,0],r""slg_202_203.out"")
# For Bus fault at 205
psspy.run(0,2.0,2,2,0)
psspy.dist_3phase_bus_fault(205,0,1,0.0,[0.0,-0.2E+10])
psspy.run(0,10.0,2,2,0)
# For Bus fault at 151
psspy.run(0,2.0,2,2,0)
psspy.dist_3phase_bus_fault(151,0,1,0.0,[0.0,-0.2E+10])
psspy.run(0,10.0,2,2,0)
# for Single Line Open from 202 to 203
psspy.dist_branch_fault(202,203,r""1""",1,500.0,[0.0,-0.2E+10])
psspy.run(0,10.0,2,2,0)
# Power flow after dynamic simulation
psspy.ordr(1)
psspy.fact()
psspy.tysl(1)
# Overload check > 100%
psspy.rate2(0,1,1,1,1,2,100.0)
# range violation check V < 0.9 PU, V > 1.1 PU
psspy.vchk(0,1,0.9,1.1)
```