

# PSSE Year 0 Topology 0 Analysis

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# Chapter 1

# Introduction

## 1.1 Study Description

The Year 0 Topology 0 contingency analysis of the hypothetical SAVNW system is carried out to report the branches reporting loading greater than 100% and buses reporting upper and lower voltage limit violations.

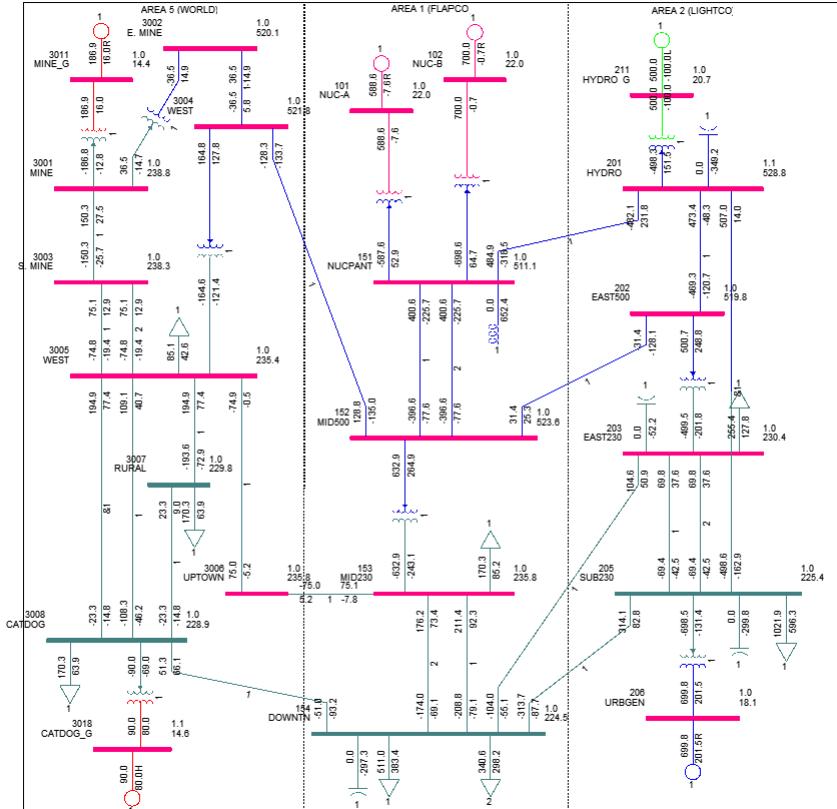


Figure 1.1: Single Line Diagram Year 0, Topology 0

For the hypothetical SAVNW system, the Year 0 Topology 0 of the system represents the present year system as shown in Figure 1.1. There are 6 generators in 3 areas. Total installed capacity of the system is the sum of firm capacity provided by 6 generating units and equals 4153.25 MW.

Detailed analysis of Year 0 Topology 0 Base Case was carried out and can be found here. The combined total generation in all areas of 2765 MW is serving a total load of 2723 MW with the generators 102\_NUC-B, 211-HYDRO\_G, 3018-CATDOG\_G operating at their nominal power output of 700 MW, 500 MW and 90 MW respectively. The swing generator in each area operates to meet the load, loss and interchange criteria. The desired

interchange for all the scenarios studied is highlighted in Figure 1.2. For all the scenarios studied the desired interchange from FLAPCO to LIGHTCO is 100 MW, and from FLAPCO to WORLD is 150 MW.

X-- AREA --X	FROM -----AT AREA BUSES-----				TO XFRMR				-NET INTERCHANGE-			DESIRED NET INT	
	GENE- RATION	FROM IND GENERATN	TO IND MOTORS	TO LOAD	TO BUS SHUNT	GNE BUS DEVICES	TO LINE SHUNT	MAGNE- TIZING	FROM CHARGING	TO LOSSES	TO TIE LINES	TO TIES + LOADS	
1 FLAPCO	1288.6 -8.2	0.0 0.0	0.0 0.0	1021.9 766.7	0.0 355.0	0.0 0.0	0.0 -0.0	0.0 -0.0	0.0 878.1	15.3 317.3	251.5 -569.2	1103.0 112.3	250.0
2 LIGHTCO	1199.8 101.5	0.0 0.0	0.0 0.0	1277.3 724.1	0.0 -701.1	0.0 0.0	0.0 -0.0	0.0 -0.0	0.0 651.0	21.1 396.2	-98.6 333.3	-950.2 -348.2	-100.0
5 WORLD	276.9 96.0	0.0 0.0	0.0 0.0	425.7 170.4	0.0 -0.0	0.0 0.0	0.0 -0.0	0.0 -0.0	0.0 366.0	4.1 55.8	-152.9 235.9	-152.9 235.9	-150.0
COLUMN TOTALS	2765.3 189.3	0.0 0.0	0.0 0.0	2724.8 1661.2	0.0 -346.1	0.0 0.0	0.0 0.0	0.0 0.0	0.0 1895.2	40.5 769.3	0.0 0.0	0.0 0.0	0.0

Figure 1.2: System Totals for Year - 0, Topology - 0

## 1.2 Contingency Analysis

AC contingency calculation was conducted on the hypothetical SAVNW system for Year 0 Topology 0. The configuration files used are:

- Subsystem file savnw.sub - Studied subsystems of the studied case defined via the Subsystem Definition data file (Figure 1.3)
- Monitor file savnw.mon - Monitored Element Data File identifies the branches that are to be monitored for flow violations and the buses that are to be monitored for voltage violations (Figure 1.4)
- Contingency file savnw.con - Contingency cases that are to be tested are defined in the Contingency Definition data file (Figure 1.5)

```

SUBSYSTEM CON
AREA 1
AREA 2
AREA 5
END

SUBSYSTEM MON
AREA 1
AREA 2
AREA 5
END

END

```

Figure 1.3: The subsystem file corresponding to Year 1 Topology 1

```

MONITOR VOLTAGE RANGE ALL BUSES 0.9 1.1
MONITOR ALL BRANCHES
MONITOR TIES FROM AREA 1 TO AREAS 2 5
MONITOR TIES FROM AREA 2 TO AREA 5
END
END

```

Figure 1.4: The monitored file corresponding to Year 1 Topology 1

```

SINGLE BRANCH IN AREA 1
SINGLE BRANCH IN AREA 2
SINGLE BRANCH IN AREA 5
SINGLE BUS IN AREA 1
SINGLE BUS IN AREA 2
SINGLE BUS IN AREA 5
SINGLE MACHINE IN AREA 1
SINGLE MACHINE IN AREA 2
SINGLE MACHINE IN AREA 5
END

```

Figure 1.5: The contingency file corresponding to Year 1 Topology 1

The API DFAX\_2 is used to construct distribution factor data files corresponding to the case .sav file, and the defined .sub, .mon, .con configuration files. By running the AC contingency calculation function ACCC\_WITH\_DSP\_3, the contingency solution output .acc files is obtained.

Python code to conduct AC contingency calculation is:

```

import psspy
psspy.case(r"""savnw.sav""")
psspy.fdns([0,1,0,0,0,0,99,0])
psspy.dfax_2([1,1,0],r"""savnw.sub""",r"""savnw.mon""",r"""savnw.con""",r"""savnw.dfx""")
psspy.accc_with_dsp_3(0.1,[0,0,0,0,1,2,0,0,0,2,0],r"""CON""",r"""savnw.dfx""",r"""savnw.acc""",",
",",")

```

Using the contingency solution output file savnw.acc, the results is exported as an excel file for further analysis. The results exported are ACCC Analysis Summary, Monitored Branch Flow (MVA), Monitored Bus Voltage. jbr;

Python code to export AC contingency solution output file as excel is:

```

import psspy
import pssexcel
pssexcel.accc('savnw.acc', ['s','b'], colabel='', stype='contingency', busmsm=0.5, sysmsm=5.0,
               rating='a', namesplit=False, xlsfile='out.xlsx', sheet='', overwritesheet=True,
               show=False, ratecon='b',
               baseflowvio=False, basevoltvio=False, flowlimit=100.0, flowchange=0.0, voltchange=0
               .0, swdrating='a',
               swdratecon='b', baseswdflowvio=False, basenodevoltvio=False, overloadreport=False)

```

Contingency analysis was carried out in PSSE for the studied case for Year 0 Topology 0. It was seen that the power flow solution did not converge for some of the tested contingencies. For the studied case, 42 contingencies were converged out of the 47 contingencies tested, the contingencies not converged are UNIT 206(1), SING OPN LIN 14 205-206(1), BUS 152, BUS 154, BUS 201.

For the converged contingencies for the studied case, the result of the contingency analysis is analysed to check for branch overload ( $> 100\%$ ) and out of range bus voltage violations (lower emergency limit  $< 0.9PU$  and upper emergency limit  $> 1.1PU$ ). It was seen that for some of the contingencies there were no branch overload or bus voltage violations reported. Rest of the contingencies violating branch overload and bus voltage emergency range violation are reported. Chapter 2 gives the observed branch flow violations, upper and lower emergency voltage violations for the studied case. As load flow analysis checks the power balance of the network at the instant the fault occurred on the system, it will not give the information regarding the dynamic behaviour of the system. Chapter 3 gives the result of the dynamic stability analysis carried out to see if the system is stable after the occurrence of the fault. To conclude, Chapter 4 summarises the results of all the analysis carried out on Year 0, Topology 0 of the hypothetical SAVNW system.

# Chapter 2

# Contingency Limit Violations

## 2.1 Introduction

In this chapter, for Year 0, Topology 0, the branches that are loaded more than 100% of their rating, and buses violating the upper and lower emergency ratings are reported.

## 2.2 Branch Overload Violation

For Year 0, Topology 0, loading violations were reported for 3 branches 153-154(1), 3001-3003(1), and 154-203(1). For the branch 153-154(1), loading of 102.62% was reported for the contingency SING OPN LIN 11 202-203(1). The branch 3001-3003(1), reporting a loading of 199.87% for the contingency BUS 151 is considered as severe/ critical loading. For the branch 154-203(1), loading of 117.68 was reported for the contingency BUS 205. The Table gives the loading violations in tabular form.

BRANCH	CONTINGENCY	MVAFLOW	AMPFLOW	RATE RATE1/RATE2	Loading
153-154(1)	SING OPN LIN 11 202-203(1)	-349.97	359.16	350.00	102.62
3001-3003(1)	BUS 151	616.28	599.62	300.00	199.87
154-203(1)	BUS 205	266.19	294.19	250.00	117.68

Table 2.1: Branch Loaded greater than 100% for Topology 0

## 2.3 Upper Emergency Bus Voltage Violation

The only upper voltage violation was reported by the bus 201 for the bus fault at bus 151 labelled BUS 151. The reported violation is tabulated in Table 2.2.

BUS	CONTINGENCY	BASE VOLTS	CONT VOLTS	RANGE VIO
201	BUS 151	1.058	1.101	0.001

Table 2.2: Upper emergency range violation for Topology 0

## 2.4 Lower Emergency Bus Voltage Violation

There was no lower emergency voltage limit violation reported for the studied case for the Year 0 Topology 0.

# Chapter 3

# Dynamic Stability Analysis

## 3.1 Introduction

As load flow analysis checks the power balance of the network at the instant the fault occurred on the system, it will not give the information regarding the dynamic behaviour of the system. Dynamic stability analysis is carried out to see if the system is stable after the occurrence of the fault. From chapter 2, the faults causing overloading and/ or voltage limit violations are 'BUS 205 , 'SING OPN LIN 11 202-203(1)', 'BUS 151'. Dynamic simulation is carried out on the studied case by applying each individual fault at TIME = 2 Seconds to check the dynamic stability of the faulted system. The python script used to carry out this simulation is given in the Appendix 4 of the document.

## 3.2 BUS 151

Dynamic simulation was conducted on the system for a bus fault at bus 151. When the bus fault at bus 151 was applied on the system at 2.0 seconds, Network not converged was first reported at TIME = 2.1167 seconds (Figure 3.1). At TIME = 3.175 seconds, 3 bus(es) in island(s) were reported (Figure 3.2). At TIME = 4.9667 seconds, 19 bus(es) in island(s) with no in-service machines was reported(Figure 3.3). Hence, the system is not dynamically stable for a bus fault at BUS 151.

```
Network not converged at TIME = 2.1167  
Network not converged at TIME = 2.125
```

Figure 3.1: Progress bar output for Bus fault at BUS 151

```
AT TIME = 3.175 VOLTAGES OUTSIDE OF BAND 0.50000 TO 1.50000:  
X----- B U S -----X VOLTAGE X----- B U S -----X VOLTAGE  
 101 [NUC-A      21.600] 0.20868LO    102 [NUC-B      21.600] 0.00000LO  
 151 [NUCPANT    500.00] 0.00000LO  
  
3.1750  0.0000    0.0000    0.0000    0.0000    237.21    617.52  
 7     552.14    0.0000    226.79    0.0000    887.23    887.30  
 13    1.3039    0.88552   1.2939    1.3291    0.83704   1.2811  
 19    1.2812    6.43503E-02 0.0000    9.1740    5.3491    13.489  
 25    0.0000    3.0499    0.0000    3.6616    1.7310    0.89153  
 31    0.0000    0.20829   0.0000    0.95247   1.3220    1.2858  
 37    0.0000    0.20868   7.67088E-07 0.95247   1.3220    1.2858  
 43    0.0000  
  
3 bus(es) in island(s) with no in-service machines  
The following buses are disconnected:  
  BUS#-SCT X-- NAME --X BASKV  BUS#-SCT X-- NAME --X BASKV  BUS#-SCT X-- NAME --X BASKV  
 101      NUC-A        21.600    102      NUC-B        21.600    151      NUCPANT    500.00
```

Figure 3.2: Progress bar output for Bus fault at BUS 151 - continued

```

Power unbalance=*****; Threshold= 1.10000
MACHINE 1 AT BUS 3011 [MINE_G 13.800] TRIPPED AT TIME = 4.9667

```

Network not converged at TIME = 4.9667

AT TIME = 4.967 VOLTAGES OUTSIDE OF BAND 0.50000 TO 1.50000:

	B U S	X VOLTAGE		B U S	X VOLTAGE	
152	[MID500	500.00]	*****HI	153	[MID230	230.00]
154	[DOWNTN	230.00]	*****HI	201	[HYDRO	500.00]
202	[EAST500	500.00]	*****HI	203	[EAST230	230.00]
204	[SUB500	500.00]	*****HI	205	[SUB230	230.00]
206	[URBGEN	18.000]	*****HI	211	[HYDRO_G	20.000]
3001	[MINE	230.00]	*****HI	3002	[E. MINE	500.00]
3003	[S. MINE	230.00]	*****HI	3004	[WEST	500.00]
3005	[WEST	230.00]	*****HI	3006	[UPTOWN	230.00]
3007	[RURAL	230.00]	*****HI	3008	[CATDOG	230.00]
3011	[MINE_G	13.800]	*****HI			

	4.9667	0.0000	0.0000	0.0000	1.09211E+19	1.30051E+20
7	1.26495E+20	0.0000	1.03619E+19	0.0000	5.03233E+19	5.59668E+19
13	2.94688E+08	4.35145E+08	3.94863E+08	3.33065E+08	4.37460E+08	1.60471E+08
19	1.78467E+08	0.0000	0.0000	0.0000	0.0000	-2.16108E+11
25	0.0000	0.0000	0.0000	0.0000	0.0000	-5.13488E+12
31	0.0000	0.0000	0.0000	0.0000	0.0000	3.49685E+05
37	0.0000	0.0000	0.0000	4.34224E+08	3.94863E+08	1.24794E+08
43	0.0000					

19 bus(es) in island(s) with no in-service machines

The following buses are disconnected:

BUS#-SCT X-- NAME --X BASKV	BUS#-SCT X-- NAME --X BASKV	BUS#-SCT X-- NAME --X BASKV
152 MID500 500.00	153 MID230 230.00	154 DOWNTN 230.00
201 HYDRO 500.00	202 EAST500 500.00	203 EAST230 230.00
204 SUB500 500.00	205 SUB230 230.00	206 URBGEN 18.000
211 HYDRO_G 20.000	3001 MINE 230.00	3002 E. MINE 500.00
3003 S. MINE 230.00	3004 WEST 500.00	3005 WEST 230.00
3006 UPTOWN 230.00	3007 RURAL 230.00	3008 CATDOG 230.00
3011 MINE_G 13.800		

Figure 3.3: Progress bar output for Bus fault at BUS 151 - continued

### 3.3 BUS 205

Dynamic simulation conducted on the system with fault applied at Bus 205 at TIME = 2.0 seconds. At TIME = 6.558 seconds, 21 bus(es) in island(s) with no in-service machines was reported and the bus disconnected from the system were reported. Hence, the system is not dynamically stable for a bus fault at BUS 205.

AT TIME = 6.558 VOLTAGES OUTSIDE OF BAND 0.50000 TO 1.50000:

	B U S	X VOLTAGE		B U S	X VOLTAGE	
102	[NUC-B	21.600]	0.44607L0	151	[NUCPANT	500.00]
152	[MID500	500.00]	0.21566L0	153	[MID230	230.00]
154	[DOWNTN	230.00]	0.02762L0	201	[HYDRO	500.00]
202	[EAST500	500.00]	0.19825L0	203	[EAST230	230.00]
204	[SUB500	500.00]	0.10468L0	205	[SUB230	230.00]
211	[HYDRO_G	20.000]	0.30992L0	3001	[MINE	230.00]
3002	[E. MINE	500.00]	0.14619L0	3003	[S. MINE	230.00]
3004	[WEST	500.00]	0.16050L0	3005	[WEST	230.00]
3006	[UPTOWN	230.00]	0.16338L0	3007	[RURAL	230.00]
3008	[CATDOG	230.00]	0.07039L0	3011	[MINE_G	13.800]

	6.5583	52.316	43.485	8.2551	6.8819	4.1568	116.51
7	85.348	117.77	14.051	55.697	3.7696	3.7157	
13	0.17566	2.76161E-02	0.30992	0.19825	9.37593E-02	0.14231	
19	0.14027	1.1741	0.0000	0.0000	0.0000	0.0000	
25	0.0000	13.216	0.0000	0.0000	0.0000	0.0000	
31	0.0000	0.72615	0.0000	0.0000	0.0000	0.0000	
37	0.0000	0.71372	0.44607	0.0000	0.30992	0.14231	
43	0.0000						

21 bus(es) in island(s) with no in-service machines

The following buses are disconnected:

BUS#-SCT X-- NAME --X BASKV	BUS#-SCT X-- NAME --X BASKV	BUS#-SCT X-- NAME --X BASKV
101 NUC-A 21.600	102 NUC-B 21.600	151 NUCPANT 500.00
152 MID500 500.00	153 MID230 230.00	154 DOWNTN 230.00
201 HYDRO 500.00	202 EAST500 500.00	203 EAST230 230.00
204 SUB500 500.00	205 SUB230 230.00	211 HYDRO_G 20.000
3001 MINE 230.00	3002 E. MINE 500.00	3003 S. MINE 230.00
3004 WEST 500.00	3005 WEST 230.00	3006 UPTOWN 230.00
3007 RURAL 230.00	3008 CATDOG 230.00	3011 MINE_G 13.800

Figure 3.4: Progress bar output for Bus fault at BUS 205 - continued

### 3.4 SING OPN LIN 11 202-203(1)

Dynamic simulation was conducted with bus fault applied at 2.0 seconds. It was seen that the system was dynamically stable. Slight overloading was reported (Figure 3.5) for the branch 153-154(1) similar to the overload reported in Table 2.1 from the contingency analysis.

SUBSYSTEM LOADING CHECK (INCLUDED: LINES; BREAKERS AND SWITCHES; TRANSFORMERS) (EXCLUDED: NONE)  
LOADINGS ABOVE 100.0 % OF RATING SET 2 (MVA FOR TRANSFORMERS, CURRENT FOR NON-TRANSFORMER BRANCHES):

X----- FROM BUS -----X X-----		TO BUS -----X											
BUS#-SCT	X-- NAME	--X	BASKV	AREA	BUS#-SCT	X-- NAME	--X	BASKV	AREA	CKT	LOADING	RATE2	PERCENT
153	MID230		230.00	1	154	DOWNTN		230.00*	1	1	360.9	350.0	103.1

Figure 3.5: System Totals for Year - 0, Topology - 0

# Chapter 4

## Conclusion

The contingency analysis was carried out on the hypothetical SAVNW study system for the Year 0, Topology 0 to study the (N-1) bus, single line open, unit contingencies. Out of all the studied (N-1) contingencies, the contingencies for which the system did not converge are the contingencies UNIT 206(1), SING OPN LIN 14 205-206(1), BUS 152, BUS 154, BUS 201.

For the converged contingency scenarios, Chapter 2 reported the branch overload, upper and lower limit voltage violations. From the branch overload table, Table 2.1 branches reporting loading greater than 130% was the branch 3001-3003(1), for a bus fault BUS 151. There was a slight violation from upper emergency voltage value for Bus 201 and no lower limit voltage violations were reported for any of the studied Buses.

In the Chapter 3 for the faults reporting the violations, dynamic simulations were carried out to determine the dynamic stability of the system. For the bus fault at buses 151 and 205, the system was not dynamically stable. For the single line open 202-203(1), the system was dynamically stable with the branch 153-154(1) still reporting overload violations.

Hence it can be concluded that in addition to the contingencies not converging reported by contingency analysis, the contingencies corresponding to the bus faults BUS 151 and BUS 205 also causes system to be unstable.

# Appendix

## 4.1 Python program to check dynamic stability of the system for contingencies reporting violations

```
import psspy
psspy.case(r"""\savnw.sav""")
psspy.fdns([0,1,0,0,0,1,99,0])
psspy.cong(0)
psspy.conl(0,1,1,[0,0],[40.0,30.0,40.0,30.0])
psspy.conl(0,1,2,[0,0],[40.0,30.0,40.0,30.0])
psspy.conl(0,1,3,[0,0],[40.0,30.0,40.0,30.0])
psspy.ordr(1)
psspy.fact()
psspy.tysl(1)
psspy.dyre_new([1,1,1,1],r"""\savnw.dyr""", "", "", "")
psspy.set_osscan_2(1,1,0)
psspy.set_relscn(1)
psspy.set_vltscn(1,1.5,0.5)
psspy.set_genpwr(1,1.1)
psspy.set_genang_3(1,180.0,0.0,1)
psspy.set_genspdev(1,10.0,1)
psspy.set_volt_viol_subsys_flag(0)
psspy.set_voltage_dip_check(1,0.8,0.2)
psspy.set_voltage_rec_check(1,1,0.8,0.4,0.9,1.0)
psspy.set_netfrq(1)
psspy.set_relang(1,0, "")
psspy.bsys(1,0,[0.0,0.0],0,[],8,[153,154,202,203,3001,3003,203,201],0,[],0,[])
psspy.chsb(1,0,[1,9,1,1,17,0])
psspy.bsys(1,0,[0.0,0.0],0,[],7,[153,154,202,203,3001,3003,201],0,[],0,[])
psspy.chsb(1,0,[13,21,37,1,13,0])
psspy.strt_2([0,0],r"""\slg_202_203.out""")
# For Bus fault at 205
psspy.run(0,2.0,2,2,0)
psspy.dist_3phase_bus_fault(205,0,1,0.0,[0.0,-0.2E+10])
psspy.run(0,10.0,2,2,0)
# For Bus fault at 151
psspy.run(0,2.0,2,2,0)
psspy.dist_3phase_bus_fault(151,0,1,0.0,[0.0,-0.2E+10])
psspy.run(0,10.0,2,2,0)
# for Single Line Open from 202 to 203
psspy.dist_branch_fault(202,203,r"""1""",1,500.0,[0.0,-0.2E+10])
psspy.run(0,10.0,2,2,0)
# Power flow after dynamic simulation
psspy.ordr(1)
psspy.fact()
psspy.tysl(1)
# Overload check > 100%
psspy.rate_2(0,1,1,1,1,2,100.0)
# range violation check V < 0.9 PU, V > 1.1 PU
psspy.vchk(0,1,0.9,1.1)
```