

STATS 604

Lecture 9

Quantifying uncertainty

Jonathan Terhorst

The Challenger Disaster



The Rogers Commission

- After the disaster, President Reagan formed a commission to investigate the causes.
- Notable members: Neil Armstrong, Sally Ride, Chuck Yeager, Richard Feynman.

S. HRG. 99-967
SPACE SHUTTLE ACCIDENT

HEARINGS

BEFORE THE
SUBCOMMITTEE ON
SCIENCE, TECHNOLOGY, AND SPACE
OF THE

COMMITTEE ON COMMERCE,
SCIENCE, AND TRANSPORTATION
UNITED STATES SENATE

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ON

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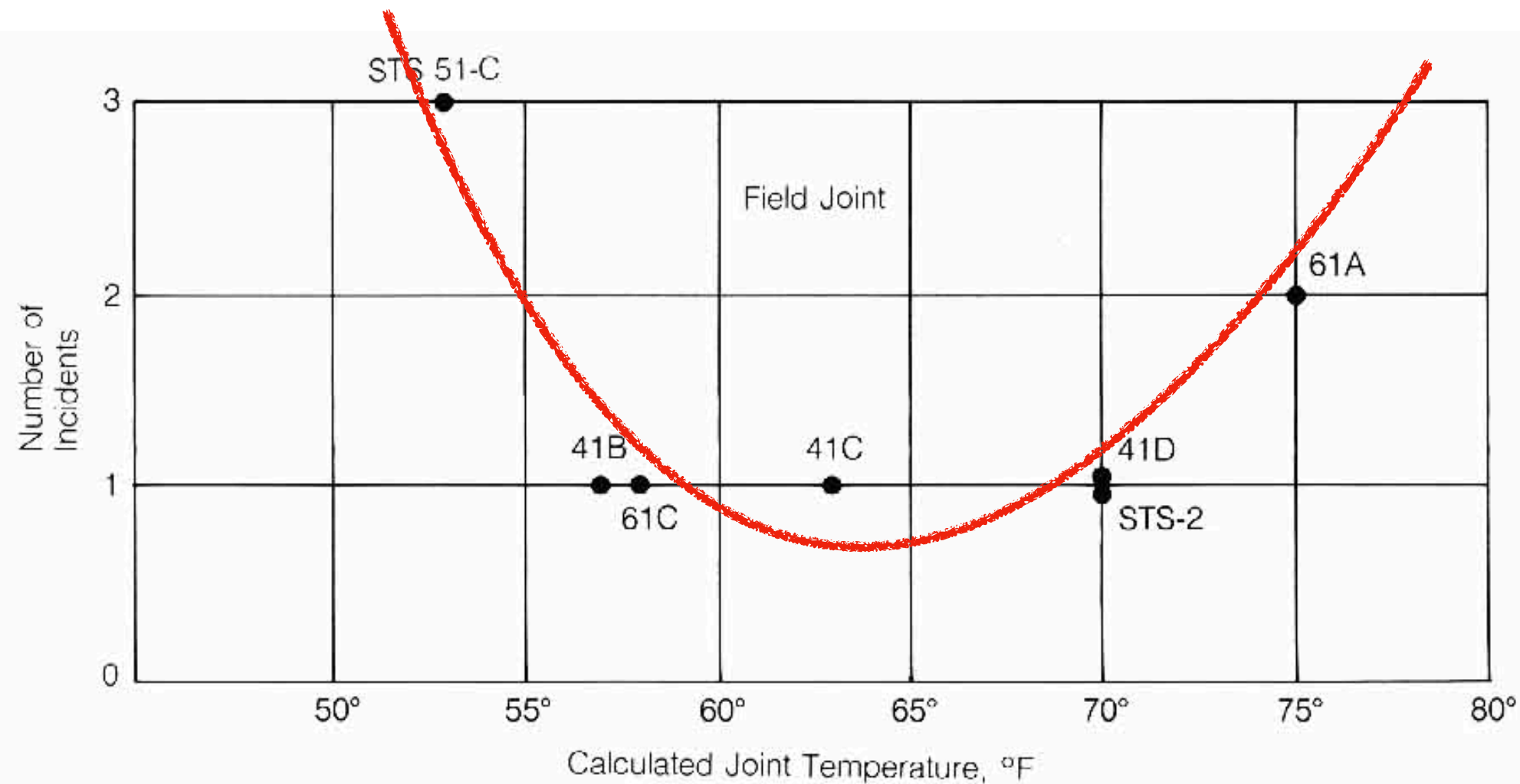


Figure 6
Plot of flights with incidents of O-ring thermal distress as function of temperature

“Based on the U configuration of points (identified by the flight number), it was concluded that there was no evidence from the historical data about a temperature effect.”

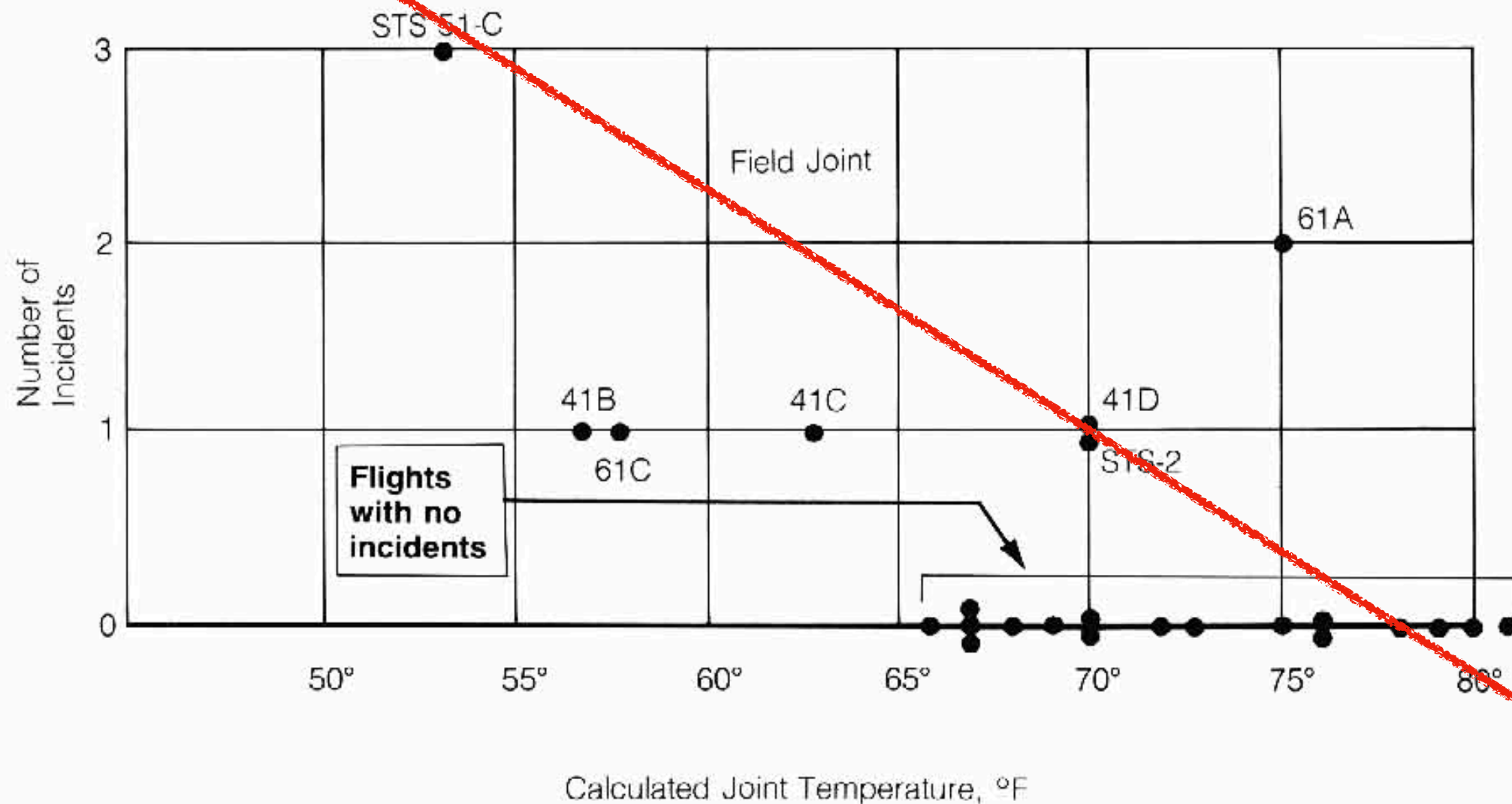


Figure 7
Plot of flights with and without incidents of O-ring thermal distress

“The Rogers Commission noted a mistake ... the flights with zero incidents were left off the plot because it was felt that these flights did not contribute any information about the temperature effect.”

The role of statistics

- Could statistical modeling have saved the Challenger?
- What are we trying to model?
- What are the data?

Risk Analysis of the Space Shuttle: Pre-*Challenger* Prediction of Failure

SIDDHARTHA R. DALAL, EDWARD B. FOWLKES, and BRUCE HOADLEY*

The Rogers Commission report on the space shuttle *Challenger* accident concluded that the accident was caused by a combustion gas leak through a joint in one of the booster rockets, which was sealed by a device called an O-ring. The commission further concluded that O-rings do not seal properly at low temperatures. In this article, data from the 23 preaccident launches of the space shuttle is used to predict O-ring performance under the *Challenger* launch conditions and relate it to the catastrophic failure of the shuttle. Analyses via binomial and binary logistic regression show that there is strong statistical evidence of a temperature effect on incidents of O-ring thermal distress. In addition, a probabilistic risk assessment at 31°F, the temperature at which *Challenger* was launched, yields at least a 13% probability of catastrophic field-joint O-ring failure. Postponement to 60°F would have reduced the probability to at least 2%. To assess uncertainty in estimates and for any future prediction under the *Challenger* scenario, a postanalysis prior distribution of the probability of a catastrophic failure is derived. The mean and median for this distribution for 31°F are at least .16 and .13, and for 60°F they are at least .004 and .02, respectively. The analysis of this article demonstrates that statistical science can play an important role in the space-shuttle risk-management process.

KEY WORDS: Catastrophic failure; Data analysis; O-rings; Probability risk assessment; Statistical science.

1. INTRODUCTION AND SUMMARY

On the night of January 27, 1986, the night before the space shuttle *Challenger* accident, there was a three-hour teleconference among people at Morton Thiokol (manufacturer of the solid rocket motor), Marshall Space Flight Center [NASA (National Aeronautics and Space Administration) center for motor design control], and Kennedy Space Center. The discussion focused on the forecast of a 31°F temperature for launch time the next morning, and the effect of low temperature on O-ring performance. A data set, Figure 1a, played an important role in the discussion. Each plotted point represents a shuttle flight that experienced thermal distress on the field-joint O-rings; the X axis shows the joint temperature at launch and the Y axis shows the number of O-rings that experienced some thermal distress. The O-rings seal the field joints of the solid rocket motors, which boost the shuttle into orbit. Based on the U configuration of points (identified by the flight number), it was concluded that there was no evidence from the historical data about a temperature effect.

Nevertheless, there was a debate on this issue, and some participants recommended that the launch be postponed until the temperature rose above 53°F—the lowest temperature experienced in previous launches—because the corresponding flight had the highest number of distressed O-rings. Some participants believed, based on the physical evidence, that there was a temperature effect on O-ring performance; for example, one of the participants, Roger Boisjoly, stated: “temperature was indeed a discriminator.” In spite of this, the final recommendation of Morton

Thiokol was to launch the *Challenger* on schedule. The recommendation transmitted to NASA stated that “Temperature data [are] not conclusive on predicting primary O-ring blowby.” The same telefax stated that “Colder O-rings will have increased effective durometer (‘harder’), and ‘Harder’ O-rings will take longer to ‘seat’” [Presidential Commission Report, Vol. 1 (PC1), p. 97 (Presidential Commission on the Space Shuttle *Challenger* Accident 1986)].

After the accident a commission was appointed by President R. Reagan to find the cause. The commission was headed by former Secretary of State William Rogers and included some of the most respected names in the scientific and space communities. The commission determined the cause of the accident to be the following: “A combustion gas leak through the right Solid Rocket Motor aft field joint initiated at or shortly after ignition eventually weakened and/or penetrated the External Tank initiating vehicle structural breakup and loss of the Space Shuttle *Challenger* during mission 51-L” (PC1, p. 70). This is the type of failure that was debated the night before the *Challenger* accident.

The Rogers Commission (PC1, p. 145) noted that a mistake in the analysis of the thermal-distress data (Fig. 1a) was that the flights with zero incidents were left off the plot because it was felt that these flights did not contribute any information about the temperature effect (see Fig. 1b). The Rogers Commission concluded that “A careful analysis of the flight history of O-ring performance would have revealed the correlation of O-ring damage in low temperature” (PC1, p. 148).

This article aims to give more substance to this quote and show how statistical science could have provided valuable input to the launch decision process. Clearly, the key question was What would have constituted proof that it was unsafe to launch? Since the phenomenon is sto-

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Modeling O-ring failure

- There are six O-rings per booster.
- Let t denote temperature and s denote pressure.
 - Let $p(s, t)$ denote the probability of an O-ring experiencing thermal distress.
- The number of failures per launch $X \mid s, t \sim \text{Binomial}(6, p(s, t))$

Logistic regression model

$$\log \left(\frac{p(s, t)}{1 - p(s, t)} \right) = \alpha + \beta t + \gamma s.$$

Call:

```
glm(formula = damaged/6 ~ temp + pressure, family = "binomial",  
    data = orings, weights = rep(6, nrow(orings)))
```

Deviance Residuals:

Min	1Q	Median	3Q	Max
-1.0361	-0.6434	-0.5308	-0.1625	2.3418

Coefficients:

	Estimate	Std. Error	z value	Pr(> z)
(Intercept)	2.520195	3.486784	0.723	0.4698
temp	-0.098297	0.044890	-2.190	0.0285 *
pressure	0.008484	0.007677	1.105	0.2691

Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

(Dispersion parameter **for** binomial family taken to be 1)

Null deviance: 24.230 on 22 degrees of freedom
Residual deviance: 16.546 on 20 degrees of freedom
AIC: 36.106

Residual deviance

- From the last slide:

Null deviance: 24.230 on 22 degrees of freedom

Residual deviance: 16.546 on 20 degrees of freedom

AIC: 36.106

- Recall that
 - Null deviance: $2 \times [\text{LL}(\text{Saturated model}) - \text{LL}(\text{null model})]$
 - Residual deviance: $2 \times [\text{LL}(\text{Saturated model}) - \text{LL}(\text{the model})]$
- If the model is good, residual deviance is low.

Does pressure matter?

- “90% bootstrap confidence intervals for the expected numbers of incidents were calculated for each temperature, first holding pressure constant at 50 psi and next setting the pressure at 200 psi.”
- **Exercise:** what are the 90% bootstrap CI's for the expected number of incidents at $s = 50$ and $s = 200$?

Pressure-only model

Call:

```
glm(formula = damaged/6 ~ temp, family = "binomial", data = orings,  
     weights = rep(6, nrow(orings)))
```

Deviance Residuals:

Min	1Q	Median	3Q	Max
-0.95227	-0.78299	-0.54117	-0.04379	2.65152

Coefficients:

	Estimate	Std. Error	z value	Pr(> z)
(Intercept)	5.08498	3.05247	1.666	0.0957 .
temp	-0.11560	0.04702	-2.458	0.0140 *

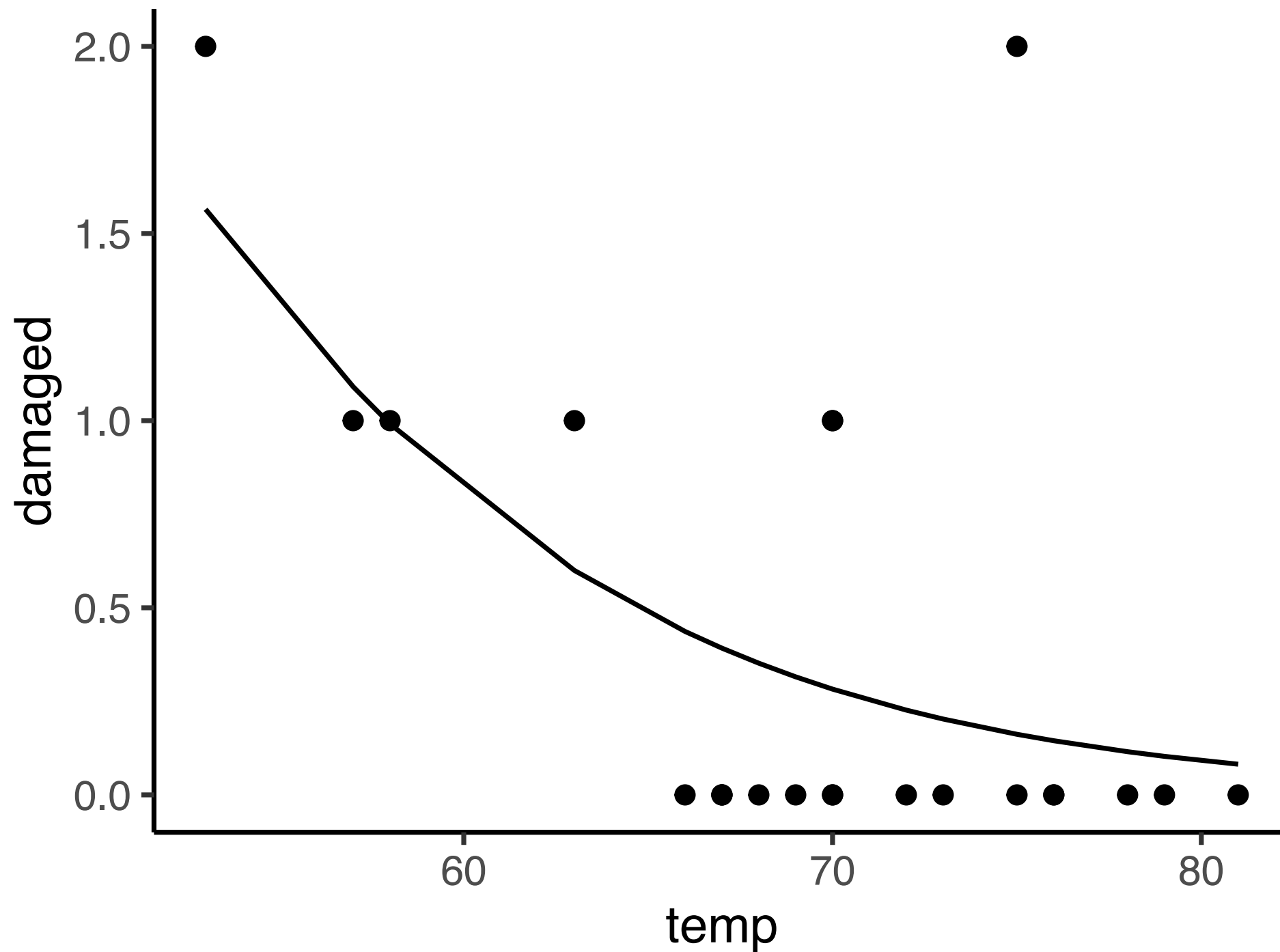
Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

(Dispersion parameter **for** binomial family taken to be 1)

Null deviance: 24.230 on 22 degrees of freedom
Residual deviance: 18.086 on 21 degrees of freedom
AIC: 35.647

Number of Fisher Scoring iterations: 5

Predicted vs. observed



Alternative model

- The prediction of interest is really whether *any* O-rings will fail.

Call:

```
glm(formula = pmin(damaged, 1) ~ temp, family = "binomial", data = orings)
```

Deviance Residuals:

Min	1Q	Median	3Q	Max
-1.0611	-0.7613	-0.3783	0.4524	2.2175

Coefficients:

	Estimate	Std. Error	z value	Pr(> z)
(Intercept)	15.0429	7.3786	2.039	0.0415 *
temp	-0.2322	0.1082	-2.145	0.0320 *

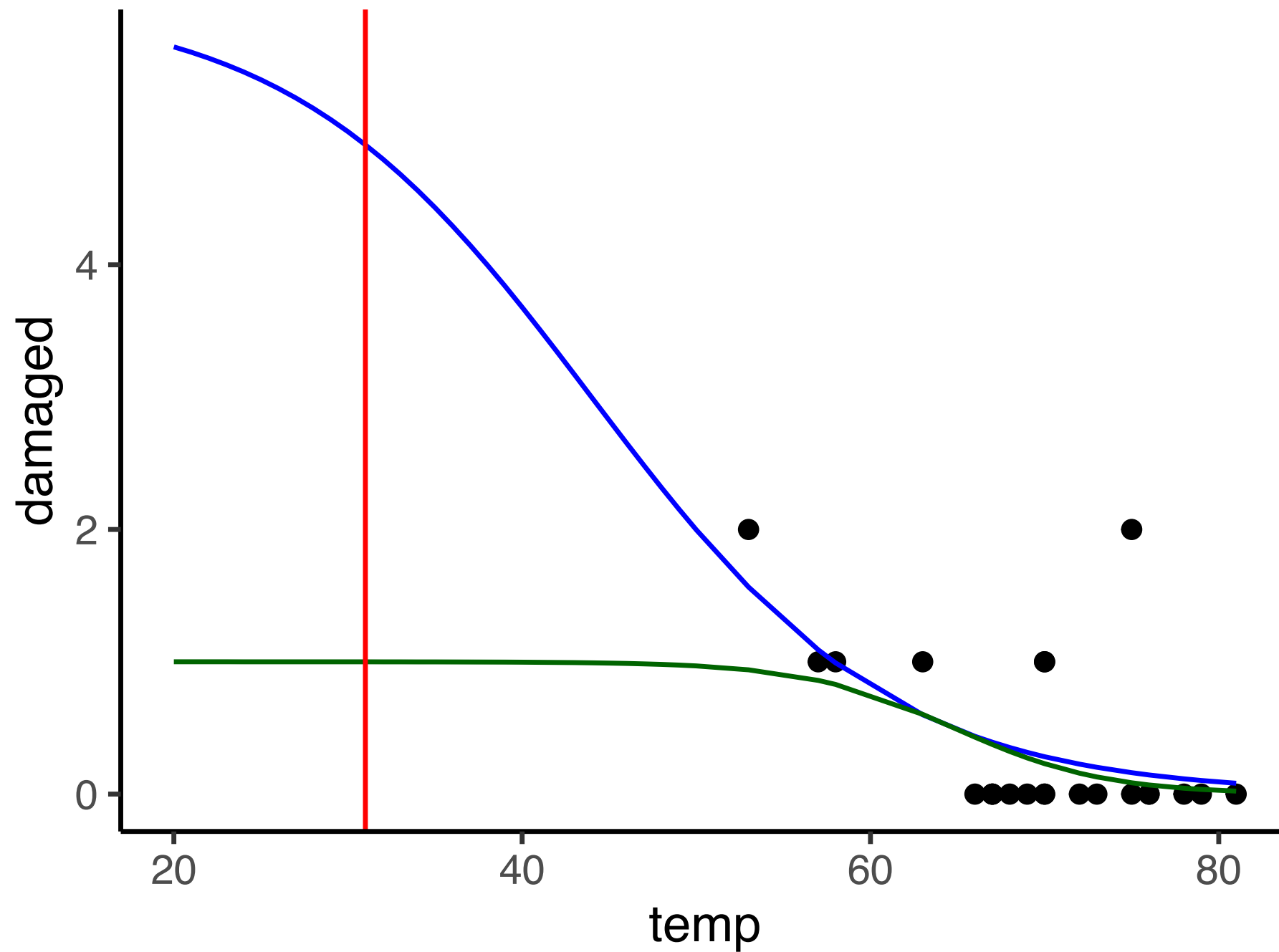
Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

(Dispersion parameter **for** binomial family taken to be 1)

Null deviance: 28.267 on 22 degrees of freedom
Residual deviance: 20.315 on 21 degrees of freedom
AIC: 24.315

Number of Fisher Scoring iterations: 5

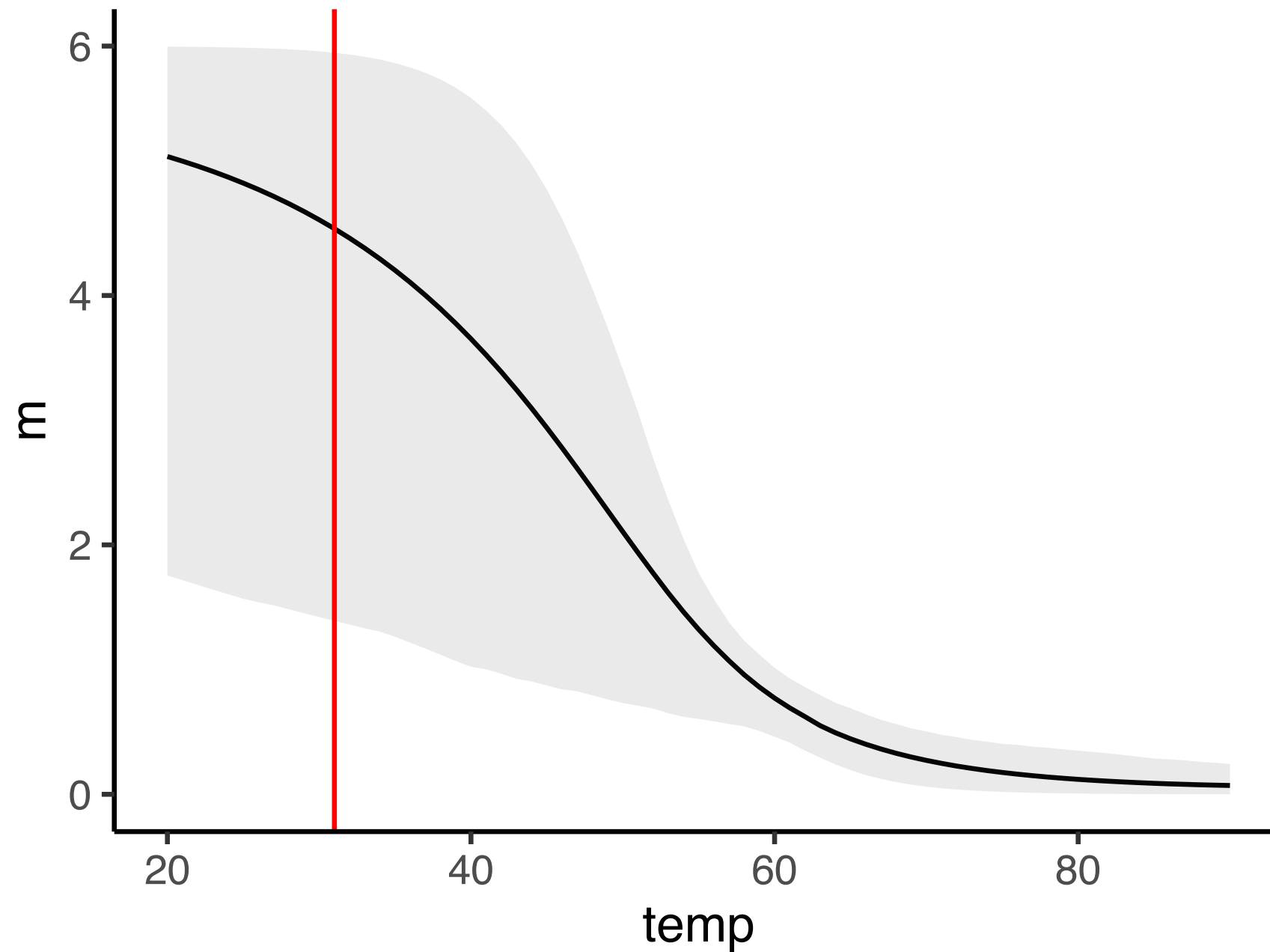
Binomial vs. logit model



Confidence bands

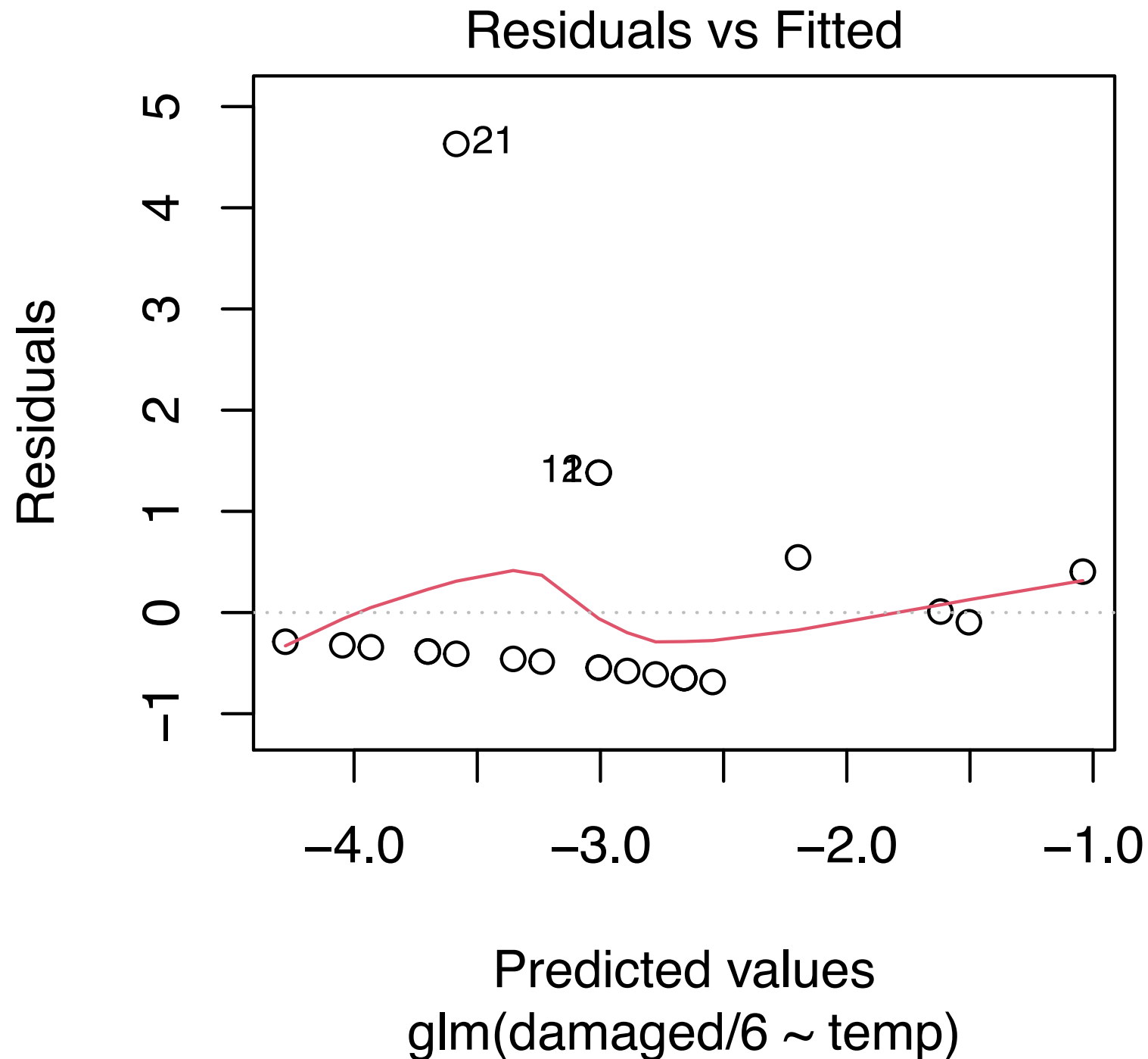
- Both models predict that at 31F, about 4-5 O-rings would fail.
- How confident can we be in this prediction?
- We will generate (pointwise) confidence bands using the parametric bootstrap.

Bootstrap confidence bands



Stability checking

- Are there any outliers? Are our findings robust to them?



Removing outlying observation 21

```
glm(formula = damaged/6 ~ temp, family = "binomial", data = orings,  
     weights = rep(6, nrow(orings)), subset = order != 21)
```

Deviance Residuals:

Min	1Q	Median	3Q	Max
-0.7608	-0.5742	-0.3321	-0.1861	1.5204

Coefficients:

	Estimate	Std. Error	z value	Pr(> z)	
(Intercept)	8.66157	3.63441	2.383	0.01716	*
temp	-0.17680	0.05869	-3.013	0.00259	**

Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

(Dispersion parameter **for** binomial family taken to be 1)

Null deviance: 20.0667 on 21 degrees of freedom
Residual deviance: 9.4096 on 20 degrees of freedom
AIC: 24.748

Number of Fisher Scoring iterations: 6

(Obs. 21 removed)

