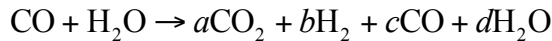


**14-4-1 [BSP]** An equimolar mixture of carbon monoxide and water vapor at 1 atm and 298 K enters a reactor operating at steady state. The equilibrium mixture, composed of  $\text{CO}_2$ ,  $\text{CO}$ ,  $\text{H}_2\text{O}(\text{g})$  and  $\text{H}_2$ , leaves at 2000 K. Determine (a) equilibrium composition of  $\text{CO}_2$  in the mixture, (b) the heat transfer ( $Q$ ) between the reactor and surroundings in kJ per kmol of  $\text{CO}$  entering the reactor.

### SOLUTION

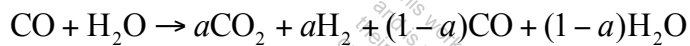
First, we start with balancing the equation:



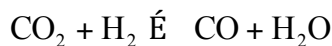
$$\text{C} : 1 = a + c \Rightarrow c = 1 - a$$

$$\text{O} : 2 = 2a + c + d \Rightarrow 2 = 2a + (1 - a) + d \Rightarrow d = 1 - a$$

$$\text{H}_2 : 1 = b + d \Rightarrow a = b$$



Now we need one more equation. The equilibrium constant equation of the stoichiometric reaction of the products will be used to get this equation.



The equilibrium constant equation;

$$K = \left( \frac{y_{\text{CO}} y_{\text{H}_2\text{O}}}{y_{\text{CO}_2} y_{\text{H}_2}} \right) \left( \frac{1}{1} \right)^{2-2} = \frac{(1-a)(1-a)}{(a)(a)} = \frac{1-2a+a^2}{a^2}$$

From the equilibrium constant table we get

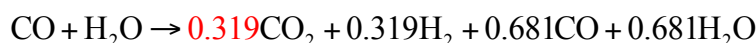
$$K = e^{1.51} = 4.53$$

Now we find  $a$  solving the following equation

$$4.53 = \frac{1-2a+a^2}{a^2};$$

$$\Rightarrow a = 0.319$$

So the balanced overall reaction will be



Now we can find the heat transfer using the energy balance equation;

$$\frac{\dot{Q}}{\dot{m}_F} = \bar{h}_P - \bar{h}_R$$

where,  $\bar{h}_p$  and  $\bar{h}_R$  can be evaluated using the procedure described in chapter 13.

$$\bar{h}_p = -230890.15 \frac{\text{kJ}}{\text{kmol}}$$

$$\bar{h}_R = -352154.57 \frac{\text{kJ}}{\text{kmol}}$$

Therefore,

$$\frac{Q}{R_F} = \bar{h}_p - \bar{h}_R = -230890.15 - (-352154.57) = 121264.42 \frac{\text{kJ}}{\text{kmol CO}}$$

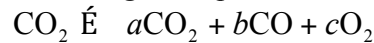
**TEST Solution:** Use TESTcalc Combustion and Chemical Equilibrium, Chemical Equilibrium Analysis to verify the solution.

This work is protected by United States copyright laws and is provided solely for the use of instructors in teaching their courses and assessing student learning. Dissemination or sale of any part of this work (including on the World Wide Web) will destroy the integrity of the work and is not permitted.

**14-4-2 [BSX]** Carbon dioxide gas at 1 atm, 298 K enters a reactor operating at steady state. If an equilibrium mixture of CO<sub>2</sub>, CO and O<sub>2</sub> exits at 2800 K, 1 atm, determine (a) the composition of the CO<sub>2</sub> in the products and (b) the heat transfer to the surroundings per unit mass of carbon dioxide.

**SOLUTION**

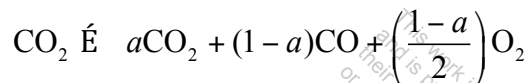
Balancing the equation;



$$a + b = 1 \Rightarrow b = 1 - a$$

$$a + 2c = 1 \Rightarrow c = \frac{1 - a}{2}$$

Balanced equation is



The exit mixture is assumed to be an equilibrium mixture, thus;



$$y_{\text{CO}_2} = \frac{2a}{3 - a}; y_{\text{CO}} = \frac{2(1 - a)}{3 - a}; y_{\text{O}_2} = \frac{1 - a}{3 - a}$$

The equilibrium constant equation

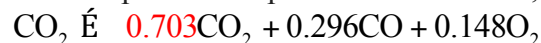
$$K = \left( \frac{y_{\text{CO}} y_{\text{O}_2}^{0.5}}{y_{\text{CO}_2}} \right) \left( \frac{p}{p_0} \right)^{1+0.5-1} = \left( \frac{2(1 - a)}{3 - a} \right) \left( \frac{1 - a}{3 - a} \right)^{0.5} \left( \frac{3 - a}{2a} \right) \Rightarrow K = \frac{(1 - a)}{a} \sqrt{\frac{1 - a}{3 - a}}$$

Using Table G-3 at 2800 K;

$$\Rightarrow e^{-1.894} = \frac{(1 - a)}{a} \sqrt{\frac{1 - a}{3 - a}}$$

Solving,  $a = 0.703$

The composition of products is therefore,



(b) The heat transfer to the surroundings per unit mass of CO<sub>2</sub>

$$\frac{\dot{Q}}{\dot{m}_F} = \bar{h}_P - \bar{h}_R$$

$$\bar{h}_p = -171886.61 \frac{\text{kJ}}{\text{kmol}}$$

$$\bar{h}_R = -393404.38 \frac{\text{kJ}}{\text{kmol}}$$

Therefore,

$$\frac{\mathcal{Q}}{\mathcal{R}_F} = \bar{h}_p - \bar{h}_R = -171886.61 - (-393404.38) = 221517.7 \frac{\text{kJ}}{\text{kmol CO}_2} = 5034.49 \frac{\text{kJ}}{\text{kg CO}_2}$$

**TEST Solution:** Use TESTcalc Combustion and Chemical Equilibrium, Chemical Equilibrium Analysis to verify the solution.

This work is protected by United States copyright laws and is provided solely for the use of instructors in teaching their courses and assessing student learning. Dissemination or sale of any part of this work (including on the World Wide Web) will destroy the integrity of the work and is not permitted.

**14-4-3 [BSC]** Hydrogen is heated in an open-steady device at 100 kPa from 300 K to 3000 K at a rate of 0.5 kg/min. Determine the rate of heat transfer in kW, assuming (a) no dissociation takes place, (b) dissociation takes place.

**SOLUTION**

The mass flow rate is given

$$\dot{m} = 0.5 \frac{\text{kg}}{\text{min}} = 0.008333 \frac{\text{kg}}{\text{s}}$$

(a) No dissociation takes place,



The heat transfer is

$$\dot{Q} = \dot{m} (\bar{h}_P - \bar{h}_R) = \dot{m} (h_P - h_R)$$

From the n-IGE Model Chemical Equilibrium TESTcalc

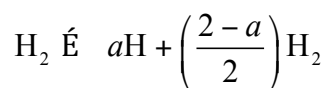
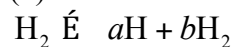
$$h_P = 44019.21 \frac{\text{kJ}}{\text{kg}}$$

$$\bar{h}_R = 26.57 \frac{\text{kJ}}{\text{kg}}$$

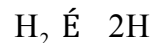
Therefore,

$$\dot{Q} = \dot{m} (h_P - h_R) = (0.008333)(44019.21 - 26.57) = 366.6 \text{ kW}$$

(b) Dissociation takes place,



The exit mixture is assumed to be an equilibrium mixture, thus;



$$y_{\text{H}} = \frac{2a}{a+2}; y_{\text{H}_2} = \frac{2-a}{a+2}$$

The equilibrium constant equation;

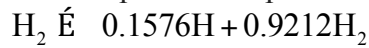
$$K = \frac{y_{\text{H}}^2}{y_{\text{H}_2}} = \frac{4a^2}{(a+2)^2} \frac{a+2}{2-a} \Rightarrow K = \frac{4a^2}{4-a^2}$$

Using Table G-3 at 3000 K

$$\Rightarrow e^{-3.685} = \frac{4a^2}{4-a^2}$$

Solving,  $a = 0.1576$

The composition of products is therefore,



The heat transfer is

$$\dot{Q} = \dot{m}_f (\bar{h}_P - \bar{h}_R) = \dot{m} (h_P - h_R)$$

From the n-IGE Model Chemical Equilibrium TESTcalc

$$h_P = 61976.74 \frac{\text{kJ}}{\text{kg}}$$

$$\bar{h}_R = 26.57 \frac{\text{kJ}}{\text{kg}}$$

Therefore,

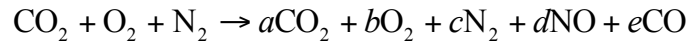
$$\dot{Q} = \dot{m} (h_P - h_R) = (0.008333)(61976.74 - 26.57) = 516.23 \text{ kW}$$

**TEST Solution:** Use TESTcalc Combustion and Chemical Equilibrium, Chemical Equilibrium Analysis, IGE mixture model to verify the solution.

**14-4-4 [BSV]** An equimolar mixture of CO<sub>2</sub>, O<sub>2</sub>, and N<sub>2</sub> enter a reactor operating at steady state. An equilibrium mixture of CO<sub>2</sub>, O<sub>2</sub>, N<sub>2</sub>, NO, and CO exits at 3500 K and 600 kPa. Determine the (a) molar amount of CO<sub>2</sub> (in kmols) in the mixture and (b) heat transfer ( $q$ ) to the surroundings per unit mass of CO<sub>2</sub>. Assume the surroundings to be 300 K and 100 kPa.

### SOLUTION

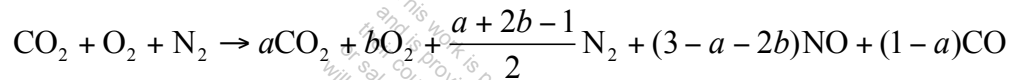
First, we start with balancing the equation:



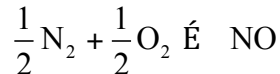
$$a + e = 1 \Rightarrow e = 1 - a$$

$$2c + d = 2 \Rightarrow d = 2 - 2c$$

$$2a + 2b + d + e = 4 \Rightarrow a + 2b - 2c = 1$$



At equilibrium two independent reactions relate the components of the mixture;



For the first reaction

$$K_1 = \left( \frac{y_{\text{CO}} y_{\text{O}_2}^{0.5}}{y_{\text{CO}_2}} \right) \left( \frac{p}{p_0} \right)^{1+0.5-1} \Rightarrow \left( \frac{2(1-a)}{7-a} \right) \sqrt{\frac{2b}{7-a}} \left( \frac{7-a}{a} \right) \left( \frac{600}{100} \right)^{0.5} = e^{0.435}$$

For the second reaction;

$$K_2 = \left( \frac{y_{\text{NO}}}{y_{\text{N}_2}^{0.5} y_{\text{O}_2}^{0.5}} \right) \left( \frac{p}{p_0} \right)^{1-0.5-0.5} \Rightarrow \left( \frac{2(3-a-2b)}{7-a} \right) \sqrt{\frac{7-a}{a+2b-1}} \sqrt{\frac{2b}{7-a}} = e^{-1.601}$$

Solving two equations above

$$a = 0.481; b = 1.155$$

The heat transfer is;

$$\dot{Q} = \dot{h}_P - \dot{h}_R$$

$$\bar{h}_P = 178722.9 \frac{\text{kJ}}{\text{kmol}}$$

$$\bar{h}_R = -393415.8 \frac{\text{kJ}}{\text{kmol}}$$

$$\bar{q} = \frac{\bar{Q}}{\bar{N}_F} = \bar{h}_P - \bar{h}_R = 178722.9 - (-393415.8) = 572138.7 \frac{\text{kJ}}{\text{kmol CO}_2}$$

Therefore,

$$q = \frac{\bar{q}}{\bar{M}_{\text{CO}_2}} = \frac{572138.7}{44} = 13003.15 \frac{\text{kJ}}{\text{kg CO}_2}$$

**TEST Solution:** Use TESTcalc Combustion and Chemical Equilibrium, Chemical Equilibrium Analysis to verify the solution.

This work is protected by United States copyright laws and is provided solely for the use of instructors in teaching their courses and assessing student learning. Dissemination or sale of any part of this work (including on the World Wide Web) will destroy the integrity of the work and is not permitted.



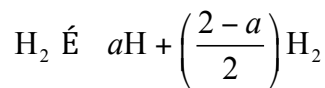
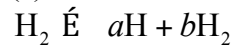
**14-4-5 [BSQ]** Hydrogen ( $H_2$ ) is heated during a steady-flow process at 1 atm from 298 K to 3000 K at a rate of 0.6 kg/min. Determine the rate of heat transfer needed during this process, assuming (a) some  $H_2$  dissociates into H and (b) no dissociation takes place.

**SOLUTION**

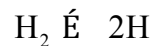
The mass flow rate is given

$$\dot{m} = 0.6 \frac{\text{kg}}{\text{min}} = 0.01 \frac{\text{kg}}{\text{s}}$$

(a) Dissociation takes place,



The exit mixture is assumed to be an equilibrium mixture, thus;



$$y_H = \frac{2a}{a+2}; y_{H_2} = \frac{2-a}{a+2}$$

The equilibrium constant equation

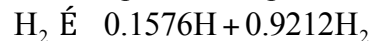
$$K = \frac{y_H^2}{y_{H_2}} = \left(\frac{4a^2}{(a+2)^2}\right) \left(\frac{a+2}{2-a}\right) = \frac{4a^2}{4-a^2}$$

Using Table G-3 at 3000 K

$$\Rightarrow e^{-3.685} = \frac{4a^2}{4-a^2}$$

Solving,  $a = 0.1576$

The composition of products is therefore,



The heat transfer is

$$\dot{Q} = \dot{m} (\bar{h}_P - \bar{h}_R) = \dot{m} (h_P - h_R)$$

From the n-IGE Model Chemical Equilibrium TESTcalc

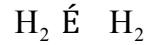
$$h_P = 61859.70 \frac{\text{kJ}}{\text{kg}}$$

$$\bar{h}_R = -2.05 \frac{\text{kJ}}{\text{kg}}$$

Therefore,

$$\dot{Q} = \dot{m}(h_p - h_R) = (0.01)(61859.70 + 2.05) = 618.62 \text{ kW}$$

(b) No dissociation takes place,



The heat transfer is

$$\dot{Q} = \dot{m}(\bar{h}_p - \bar{h}_R) = \dot{m}(h_p - h_R)$$

From the n-IGE Model Chemical Equilibrium TESTcalc

$$h_p = 44019.21 \frac{\text{kJ}}{\text{kg}}$$

$$\bar{h}_R = -2.05 \frac{\text{kJ}}{\text{kg}}$$

Therefore,

$$\dot{Q} = \dot{m}(h_p - h_R) = (0.01)(44019.21 + 2.05) = 440.2 \text{ kW}$$

**TEST Solution:** Use TESTcalc Combustion and Chemical Equilibrium, Chemical Equilibrium Analysis, IGE mixture model to verify the solution.

**14-4-6 [BST]** Carbon at 300 K, 100 kPa enters a chamber and reacts with oxygen entering at the same molar flow rate at 400 K, 100 kPa. An equilibrium mixture consists of CO<sub>2</sub>, CO, and O<sub>2</sub> exits at 3000 K, 100 kPa. Determine the heat transfer to the surroundings in kJ/kmol of carbon.

### SOLUTION

Molar analysis:



$$\text{C}: 1 = a + b; \quad \Rightarrow b = 1 - a$$

$$\text{O}: 2 = 2a + b + 2c; \quad \Rightarrow c = \frac{1-a}{2}$$

Using the n-IGE Model TESTcalc, the coefficients are found to be

$$\text{CO}_2: a = 0.5615$$

$$\text{CO}: b = 0.4385$$

$$\text{O}_2: c = 0.2193$$

Using the molar masses of carbon and oxygen and assuming one kmol of each reactant, the mass of each reactant can be found. The conservation of mass can also be applied to find the total mass of products.

$$\bar{M}_\text{C} = 12 \frac{\text{kg}}{\text{kmol}}$$

$$\bar{M}_{\text{O}_2} = 32 \frac{\text{kg}}{\text{kmol}}$$

$$m_\text{C} = n_\text{C} \bar{M}_\text{C} = 12 \text{ kg}$$

$$m_{\text{O}_2} = n_{\text{O}_2} \bar{M}_{\text{O}_2} = 32 \text{ kg}$$

$$m_\text{p} = m_\text{C} + m_{\text{O}_2} = 12 + 32 = 44 \text{ kg}$$

Now using the n-IGE Model TESTcalc, the specific enthalpies of the reactants and products can be found

$$h_\text{C} = 59676.16 \frac{\text{kJ}}{\text{kg}}$$

$$h_{\text{O}_2} = 94.57 \frac{\text{kJ}}{\text{kg}}$$

$$h_\text{p} = -2571.29 \frac{\text{kJ}}{\text{kg}}$$

The energy equation can be used to find the heat transfer to the surroundings. Since there is no work done,

$$Q = m_p h_p - \sum (m_r h_r) = m_p h_p - (m_C h_C + m_{O_2} h_{O_2});$$

$$Q = (44)(-2571.29) - [(12)(59676.16) + (32)(94.57)] = -832276.92 \text{ kJ} = -832.23 \text{ MJ}$$

$$Q_{\text{out}} = 832.23 \text{ MJ}$$

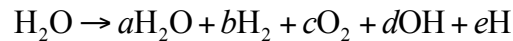
**TEST Solution:** Use TESTcalc Combustion and Chemical Equilibrium, Chemical Equilibrium Analysis to verify the solution.

This work is protected by United States copyright laws and is provided solely for the use of instructors in teaching their courses and assessing student learning. Dissemination or sale of any part of this work (including on the World Wide Web) will destroy the integrity of the work and is not permitted.

**14-4-7 [BSY]** Steam enters a heat exchanger operating at steady state. An equilibrium mixture of  $\text{H}_2\text{O}$ ,  $\text{H}_2$ ,  $\text{O}_2$ ,  $\text{H}$ , and  $\text{OH}$  exits at 2500 K and 100 kPa. Determine the (a) equilibrium composition of  $\text{H}_2\text{O}$  (in kmols) and (b) heat transfer ( $q$ ) to the surroundings per unit mass of steam. Assume the surroundings to be 300 K and 100 kPa.

**SOLUTION**

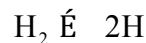
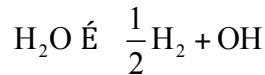
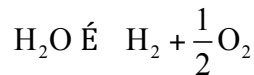
Molar analysis:



$$\text{H}: 2 = 2a + 2b + d + e$$

$$\text{O}: 1 = a + 2c + d$$

There are three reactions occurring simultaneously



Using Table G-3, you get for the first, second, and third reactions, respectively

$$\ln K_{p,1} = -4.919$$

$$\ln K_{p,2} = -4.954$$

$$\ln K_{p,3} = -7.364$$

Using a different form of the relation for the equilibrium constant

$$\ln K_{p,1} = \ln \left[ \left( \frac{N_{\text{H}_2}^{v_{\text{H}_2}} N_{\text{O}_2}^{v_{\text{O}_2}}}{N_{\text{H}_2\text{O}}^{v_{\text{H}_2\text{O}}}} \right) \left( \frac{p}{N_{\text{total}}} \right)^{v_{\text{H}_2} + v_{\text{O}_2} - v_{\text{H}_2\text{O}}} \right];$$

$$\Rightarrow -4.919 = \ln \left[ \left( \frac{(b)(c)^{0.5}}{a} \right) \left( \frac{1}{a+b+c+d+e} \right)^{0.5} \right]$$

$$\ln K_{p,2} = \ln \left[ \left( \frac{N_{\text{H}_2}^{v_{\text{H}_2}} N_{\text{OH}}^{v_{\text{OH}}}}{N_{\text{H}_2\text{O}}^{v_{\text{H}_2\text{O}}}} \right) \left( \frac{p}{N_{\text{total}}} \right)^{v_{\text{H}_2} + v_{\text{OH}} - v_{\text{H}_2\text{O}}} \right];$$

$$\Rightarrow -4.954 = \ln \left[ \left( \frac{(b)^{0.5}(d)}{a} \right) \left( \frac{1}{a+b+c+d+e} \right)^{0.5} \right]$$

$$\ln K_{p,3} = \ln \left[ \left( \frac{N_{\text{H}}^{v_{\text{H}}}}{N_{\text{H}_2}^{v_{\text{H}_2}}} \right) \left( \frac{p}{N_{\text{total}}} \right)^{v_{\text{H}} - v_{\text{H}_2}} \right];$$

$$\Rightarrow -7.364 = \ln \left[ \left( \frac{(e)^2}{b} \right) \left( \frac{1}{a+b+c+d+e} \right)^1 \right]$$

Now with five equations and five unknowns, the coefficients can be found. Using the n-IGE Model Chemical Equilibrium TESTcalc, the coefficients are

$$\text{H}_2\text{O}: a = 0.9403$$

$$\text{H}_2: b = 0.0438$$

$$\text{O}_2: c = 0.0167$$

$$\text{OH}: d = 0.0262$$

$$\text{H}: e = 0.0053$$

Using the n-IGE Model Chemical Equilibrium TESTcalc, the following enthalpies are obtained

$$h_p = -6935.37 \frac{\text{kJ}}{\text{kg}}$$

$$h_R = -13419.10 \frac{\text{kJ}}{\text{kg}}$$

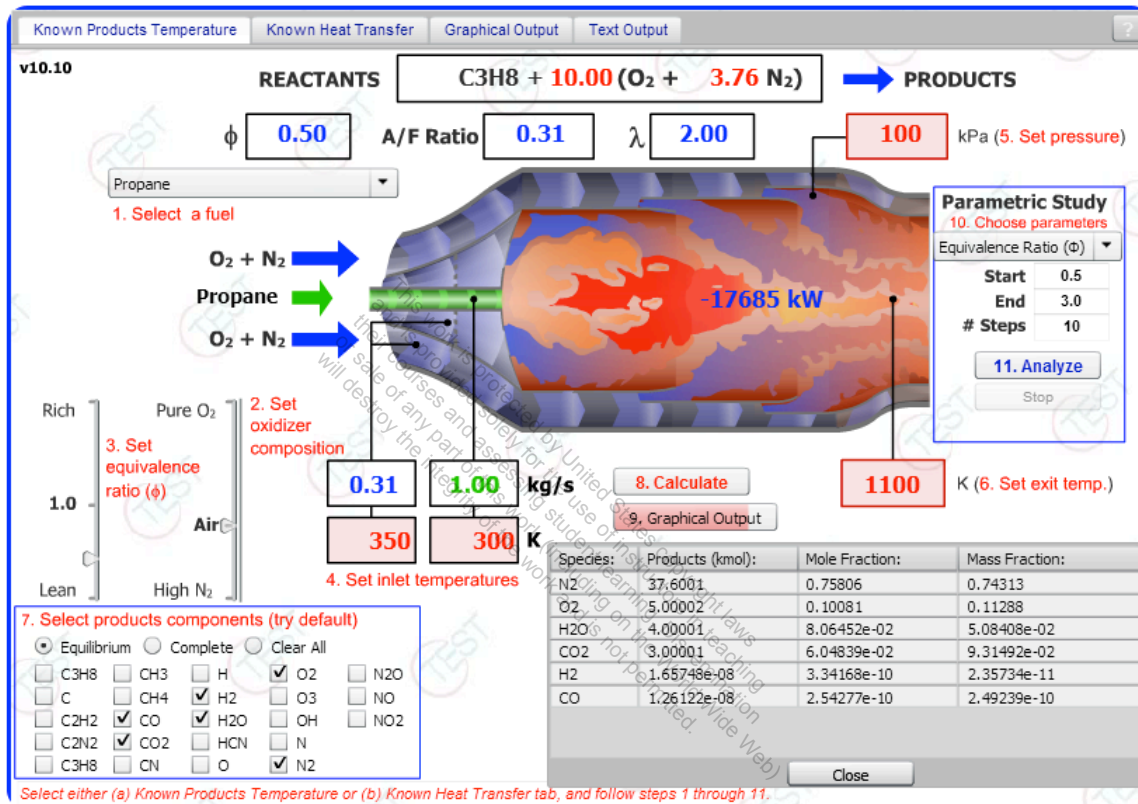
Since there is no work, the energy equation will be

$$Q = m(h_p - h_R) = 1(-6935.37 + 13419.10) = 6483.73 \frac{\text{kJ}}{\text{kg H}_2\text{O}}$$

**TEST Solution:** Use TESTcalc Combustion and Chemical Equilibrium, Chemical Equilibrium Analysis to verify the solution.

**14-4-8 [BSJ]** Propane gas ( $C_3H_8$ ) at 300 K and 100 kPa enters combustion chamber operating at steady state and reacts with 100% of excess air entering at 350 K and 100 kPa. An equilibrium mixture consists of  $CO_2$ ,  $CO$ ,  $H_2O(g)$ ,  $H_2$ ,  $O_2$ , and  $N_2$  exits at 1100 K and 100 kPa. Determine (a) the heat transfer ( $Q$ ) to the surroundings in kJ/kmol of propane. (b) What-if Scenario: What would the heat transfer be if 200% excess air enters the chamber instead?

## SOLUTION



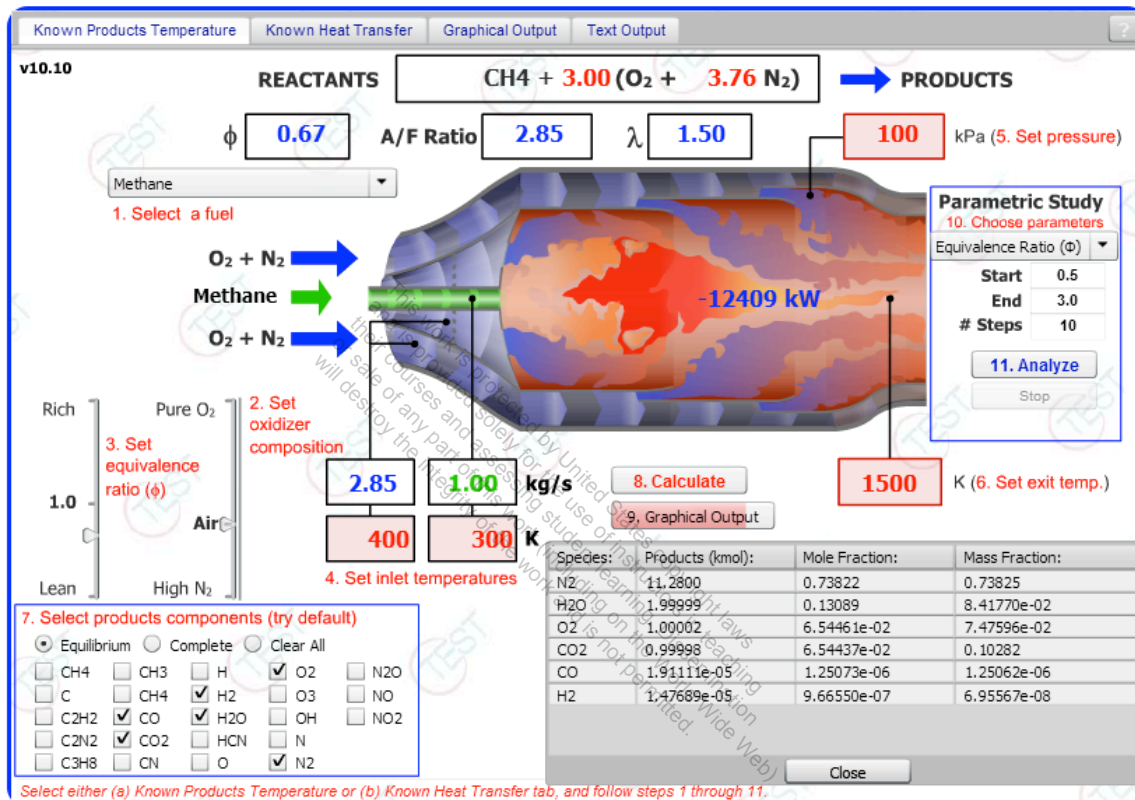
The heat transfer per kmol of propane

$$\bar{q} = q\bar{M}_{C_3H_8} = (-17685)(44.1) = -779908.5 \frac{\text{kJ}}{\text{kmol } C_3H_8}$$

$$\bar{q}_{\text{out}} = 779908.5 \frac{\text{kJ}}{\text{kmol } C_3H_8}$$

**14-4-9 [BSF]** Methane gas ( $\text{CH}_4$ ) at 300 K and 100 kPa enters combustion chamber operating at steady state and reacts with 50% of excess air entering at 400 K and 100 kPa. An equilibrium mixture of  $\text{CO}_2$ ,  $\text{CO}$ ,  $\text{H}_2\text{O(g)}$ ,  $\text{H}_2$ , and  $\text{N}_2$  exits at 2000 K and 100 kPa. Determine (a) the heat transfer ( $Q$ ) to the surroundings in kJ/kmol of methane. (b) What-if Scenario: What would the heat transfer be if 100% excess air enters the chamber instead?

## SOLUTION



The heat transfer per kmol of methane

$$\bar{q} = q \bar{M}_{\text{CH}_4} = (-12409)(16) = -198544 \frac{\text{kJ}}{\text{kmol CH}_4}$$

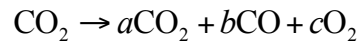
$$\bar{q}_{\text{out}} = 198544 \frac{\text{kJ}}{\text{kmol CH}_4}$$



**14-4-10 [BSD]** CO<sub>2</sub> gas at 300 K and 400 kPa enters a steady state heat exchanger. An equilibrium mixture consists of CO<sub>2</sub>, O<sub>2</sub>, and CO exits at 2700 K and 350 kPa. Determine the (a) composition of CO<sub>2</sub> in the exiting mixture and (b) heat transfer ( $Q$ ) to the gas in kJ/kmol of CO<sub>2</sub>.

**SOLUTION**

Molar analysis:



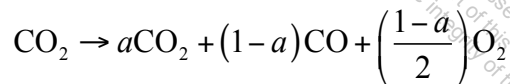
$$\text{C}: 1 = a + b; \quad \Rightarrow b = 1 - a$$

$$\text{O}: 2 = 2a + b + 2c; \quad \Rightarrow c = \frac{1-a}{2}$$

$$a + b + c = \frac{3-a}{2}$$

$$y_{\text{CO}_2} = \frac{2a}{3-a}; \quad y_{\text{CO}} = \frac{2-2a}{3-a}; \quad y_{\text{O}_2} = \frac{1-a}{3-a}$$

Plugging the relations for the stoichiometric coefficients into the equation above we get,



For CO<sub>2</sub>  $\rightleftharpoons$  CO +  $\frac{1}{2}$  O<sub>2</sub> use of the n-IGE Chemical Equilibrium TESTcalc finds at 2700 K and 350 kPa,  $\ln K_p = -2.323$ .

$$\begin{aligned} \ln K_p &= \ln \left[ \left( \frac{y_{\text{CO}}^{\nu_{\text{CO}}} y_{\text{O}_2}^{\nu_{\text{O}_2}}}{y_{\text{CO}_2}^{\nu_{\text{CO}_2}}} \right) \left( \frac{p}{p_{\text{atm}}} \right)^{\nu_{\text{CO}} + \nu_{\text{O}_2} - \nu_{\text{CO}_2}} \right] = \ln \left[ \left( \frac{y_{\text{CO}}^1 y_{\text{O}_2}^{0.5}}{y_{\text{CO}_2}^1} \right) (3.5)^{1.5-1} \right] = \ln \left[ \frac{\left( \frac{2-2a}{3-a} \right)^1 \left( \frac{1-a}{3-a} \right)^{0.5}}{\left( \frac{2a}{3-a} \right)^1} (3.5)^{0.5} \right]; \\ \ln K_p &= \ln \left[ \left( \frac{2-2a}{2a} \right) \left( \frac{1-a}{3-a} \right)^{0.5} (3.5)^{0.5} \right]; \quad \Rightarrow -2.323 = \ln \left[ \left( \frac{1-a}{a} \right) \left( \frac{1-a}{3-a} \right)^{0.5} \left( \frac{2a}{3.5} \right)^{0.5} \right]; \\ \Rightarrow e^{-2.323} &= \left[ \left( \frac{1-a}{a} \right) \left( \frac{1-a}{3-a} \right)^{0.5} (3.5)^{0.5} \right]; \quad \Rightarrow 0.09797921 = \left[ \left( \frac{1-a}{a} \right) \left( \frac{1-a}{3-a} \right)^{0.5} (3.5)^{0.5} \right]; \\ \Rightarrow 0.00959993 &= \left[ \left( \frac{1-a}{a} \right)^2 \left( \frac{1-a}{3-a} \right) (3.5) \right]; \quad \Rightarrow 0.00274284 = \left[ \frac{1-3a+3a^2-a^3}{3a^2-a^3} \right] \end{aligned}$$

Solving yields

$$a = 0.8390$$

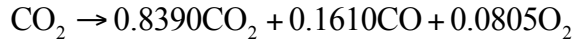
Therefore

$$\text{CO}_2 : a = 0.8390$$

$$\text{CO} : b = 1 - a = 1 - 0.8390 = 0.1610$$

$$\text{O}_2 : c = \frac{1 - a}{2} = \frac{1 - 0.8390}{2} = 0.0805$$

Substituting in the known values



Using the n-IGE Model Chemical Equilibrium TESTcalc, the following enthalpies are obtained

$$h_p = -215084.80 \frac{\text{kJ}}{\text{kg}}$$

$$h_R = -393330.44 \frac{\text{kJ}}{\text{kg}}$$

Using the molar mass of carbon dioxide and knowing that mass is conserved,

$$\bar{M}_{\text{CO}_2} = 44 \frac{\text{kg}}{\text{kmol}}$$

$$m_1 = m_2 = n\bar{M}_{\text{CO}_2} = (1)(44) = 44 \frac{\text{kg}}{\text{kmol CO}_2}$$

Since there is no work, the equation will be

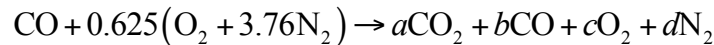
$$Q = m_2 h_p - m_1 h_R = -215084.80 + 393330.44 = 178245.64 \frac{\text{kJ}}{\text{kmol CO}_2} = 178.25 \frac{\text{MJ}}{\text{kmol CO}_2}$$

**TEST Solution:** Use TESTcalc Combustion and Chemical Equilibrium, Chemical Equilibrium Analysis to verify the solution.

**14-4-11 [BSM]** Carbon monoxide at 20°C and 100 kPa enters a combustion chamber and burns with 25% excess air entering at the same temperature and pressure. An equilibrium mixture consists of CO<sub>2</sub>, CO, O<sub>2</sub>, and N<sub>2</sub> exits at 1200°C and 100 kPa. Determine (a) the heat transfer ( $Q$ ) to the surroundings in kJ/kmol of CO. (b) What-if Scenario: What would the heat transfer to the surroundings be if 85% excess air enters the chamber instead?

### SOLUTION

Molar analysis:



$$\text{C: } 1 = a + b; \quad \Rightarrow b = 1 - a$$

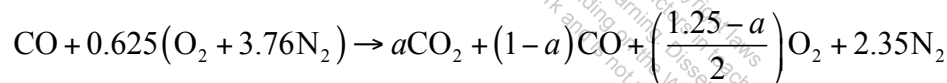
$$\text{O: } 2.25 = 2a + b + 2c; \quad \Rightarrow c = \frac{1.25 - a}{2}$$

$$\text{N: } 2.35 = d$$

$$a + b + c + d = \frac{7.95 - a}{2}$$

$$y_{\text{CO}_2} = \frac{2a}{7.95 - a}; \quad y_{\text{CO}} = \frac{2 - 2a}{7.95 - a}; \quad y_{\text{O}_2} = \frac{1.25 - a}{7.95 - a}; \quad y_{\text{N}_2} = \frac{4.70}{7.95 - a}$$

Plugging the relations for the stoichiometric coefficients into the equation above we get,



For CO<sub>2</sub> É CO +  $\frac{1}{2}$ O<sub>2</sub> use of the n-IGE Chemical Equilibrium TESTcalc finds at 1200°C,  $\ln K_p = -12.635$ . At 100 kPa,

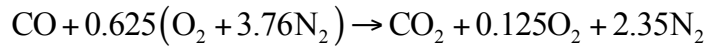
$$\begin{aligned} \ln K_p &= \ln \left[ \left( \frac{y_{\text{CO}}^{v_{\text{CO}}} y_{\text{O}_2}^{v_{\text{O}_2}}}{y_{\text{CO}_2}^{v_{\text{CO}_2}}} \right) \left( \frac{p}{1.01325} \right)^{v_{\text{CO}} + v_{\text{O}_2} - v_{\text{CO}_2}} \right] = \ln \left[ \left( \frac{y_{\text{CO}}^1 y_{\text{O}_2}^{0.5}}{y_{\text{CO}_2}^1} \right) (1)^{1.5-1} \right] = \ln \left[ \left( \frac{\left( \frac{2 - 2a}{7.95 - a} \right)^1 \left( \frac{1.25 - a}{7.95 - a} \right)^{0.5}}{\left( \frac{2a}{7.95 - a} \right)^1} \right) \right]; \\ \ln K_p &= \ln \left[ \left( \frac{2 - 2a}{2a} \right) \left( \frac{1.25 - a}{7.95 - a} \right)^{0.5} \right]; \quad \Rightarrow -12.635 = \ln \left[ \left( \frac{1 - a}{a} \right) \left( \frac{1.25 - a}{7.95 - a} \right)^{0.5} \right]; \\ \Rightarrow e^{-12.635} &= \left[ \left( \frac{1 - a}{a} \right) \left( \frac{1.25 - a}{7.95 - a} \right)^{0.5} \right]; \quad \Rightarrow 3.256 \times 10^{-6} = \left[ \left( \frac{1 - a}{a} \right) \left( \frac{1.25 - a}{7.95 - a} \right)^{0.5} \right]; \\ \Rightarrow 1.060 \times 10^{-11} &= \left[ \left( \frac{1 - a}{a} \right)^2 \left( \frac{1.25 - a}{7.95 - a} \right) \right]; \quad \Rightarrow 1.060 \times 10^{-11} = \left[ \frac{1.25 - 3.5a + 3.25a^2 - a^3}{7.95a^2 - a^3} \right]; \end{aligned}$$

$$\Rightarrow (1.060 \times 10^{-11})(7.95a^2 - a^3) \cong 0 = 1.25 - 3.5a + 3.25a^2 - a^3;$$

$$\Rightarrow a = 1, 1.25$$

The value of  $a$  cannot be above 1, otherwise the balance for carbon would demand a negative value for  $b$ .

Substituting in the known value for  $a$  yields



Now we can find the heat transfer using the energy balance equation;

$$Q - W_{\text{ext}} = \bar{h}_p - \bar{h}_R = \sum \nu_p \bar{h}_p - \sum \nu_r \bar{h}_r$$

Since there is no work, the equation will be;

$$Q = \sum \nu_p \bar{h}_p - \sum \nu_r \bar{h}_r = -231889 + 111119 = -120770 \frac{\text{kJ}}{\text{kmol CO}}$$

$$Q_{\text{out}} = 120770 \frac{\text{kJ}}{\text{kmol CO}}$$

	$\nu_k$	$\bar{h}_f$	$\Delta \bar{h}_k$	$\bar{h}_k = \bar{h}_f + \Delta \bar{h}_k$	$\nu_k \bar{h}_k$
CO	1	-110530	-148	-110678	-110678
O <sub>2</sub>	0.625	0	-148	-148	-93
N <sub>2</sub>	2.35	0	-148	-148	-348
				$\sum \nu_r \bar{h}_r$	-111119
CO <sub>2</sub>	1	-393520	67554	-325966	-325966
CO	0	-	-	-	0
O <sub>2</sub>	0.125	0	48306	48306	6038
N <sub>2</sub>	2.35	0	37465	37465	88042
				$\sum \nu_p \bar{h}_p$	-231886

Checking with the more accurate n-IGE Model TESTcalc,

$$Q_{\text{out}} = 129100 \frac{\text{kJ}}{\text{kmol CO}}$$

**TEST Solution:** Use TESTcalc Combustion and Chemical Equilibrium, Chemical Equilibrium Analysis to verify the solution.

**14-4-12 [BSW]** Methane ( $\text{CH}_4$ ) at  $25^\circ\text{C}$  and 1 atm enters a well-insulated reactor and reacts with air entering at the same conditions. For steady-state operation, negligible effects of  $k_e$  and  $p_e$ , and negligible pressure loss, plot the temperature of the combustion products against equivalent ratio ranging from 0.5 through 3.0. (a) Assume complete combustion with PG mixture model, (b) assume complete combustion with IG mixture model, (c) assume equilibrium combustion with IG mixture model and having  $\text{CO}_2$ ,  $\text{H}_2\text{O}$ ,  $\text{N}_2$ ,  $\text{O}_2$ ,  $\text{NO}$ ,  $\text{OH}$ ,  $\text{CO}$ ,  $\text{O}$ ,  $\text{H}_2$  and  $\text{H}$  in the products mixture. For part (c), also plot the mole fraction of  $\text{CO}$  and  $\text{NO}$  in the products against the equivalent ratio.

## SOLUTION

The solution was done using TEST. But first, the equivalent ratio needed to be converted to the theoretical air percentage used, then to excess/deficit air percentage. The latter is a useful input in TEST.

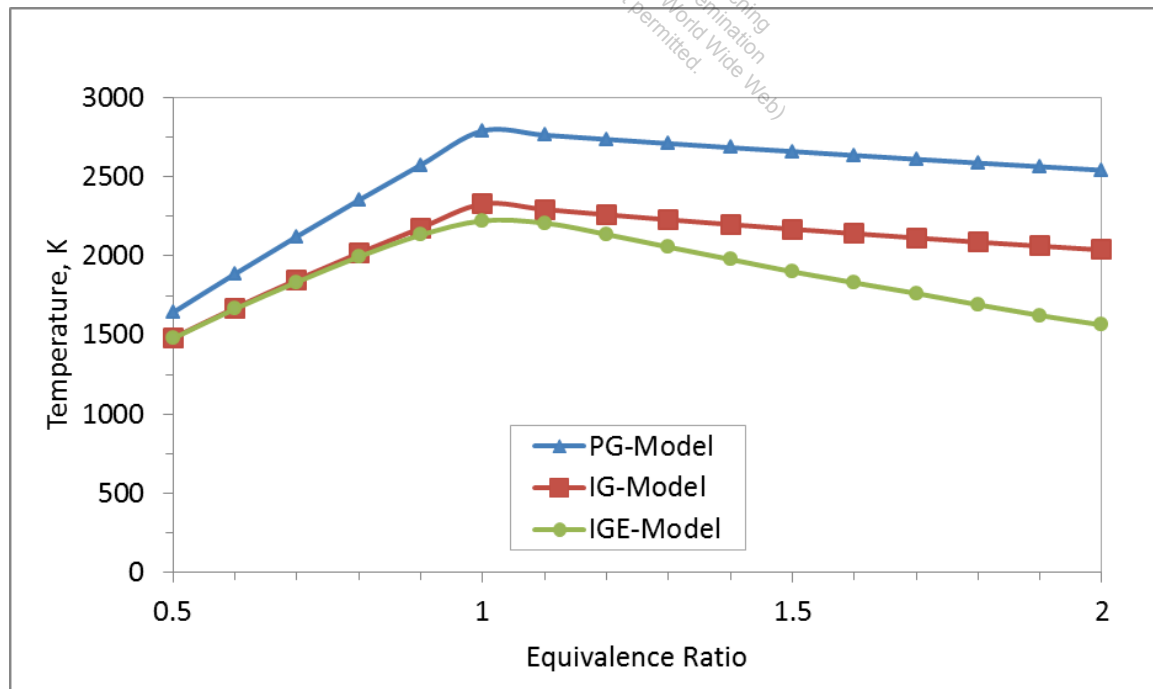
$$\varphi = \frac{\text{FA}}{(\text{FA})_{th}} = \frac{(\text{AF})_{th}}{\text{AF}} = \frac{1}{x}, \text{ where } x \text{ is the theoretical air percentage}$$

Then we get the excess/deficit percentage  $= (x - 1) \cdot 100$

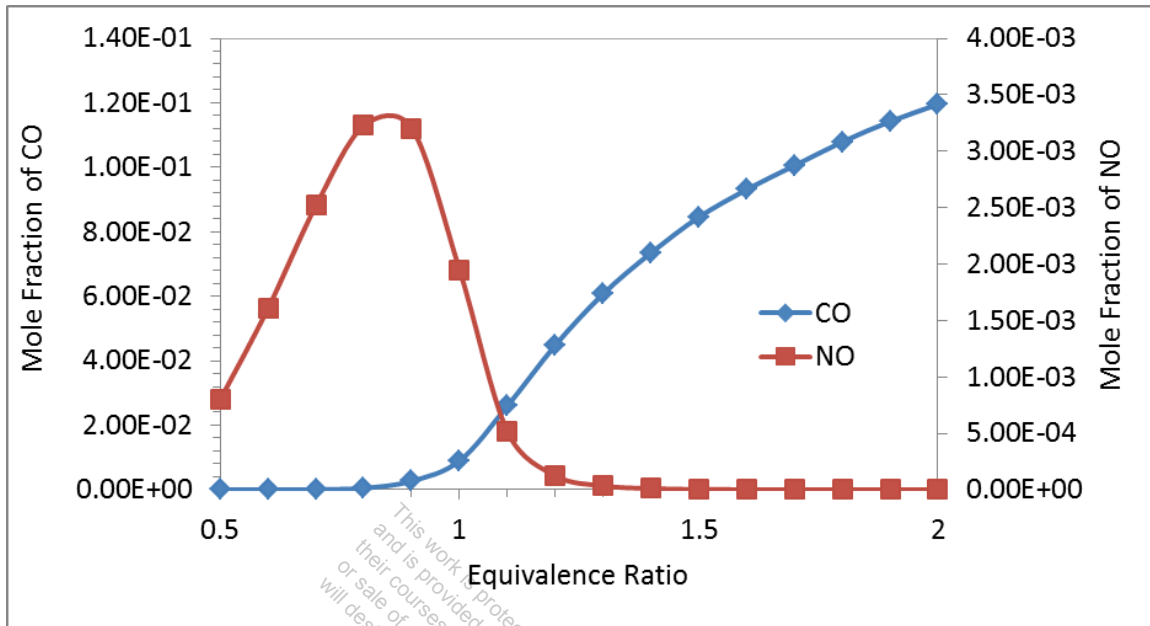
The sign will tell whether it is excess (+) or deficit (-), the value can be plugged in TEST.

$$\text{For example, } \varphi = 0.9; x = \frac{1}{\varphi} = \frac{1}{0.9} = 1.11$$

$$\text{The excess/deficit percentage} = (x - 1) \cdot 100 = (1.11 - 1) \cdot 100 = 11\% \text{ excess}$$



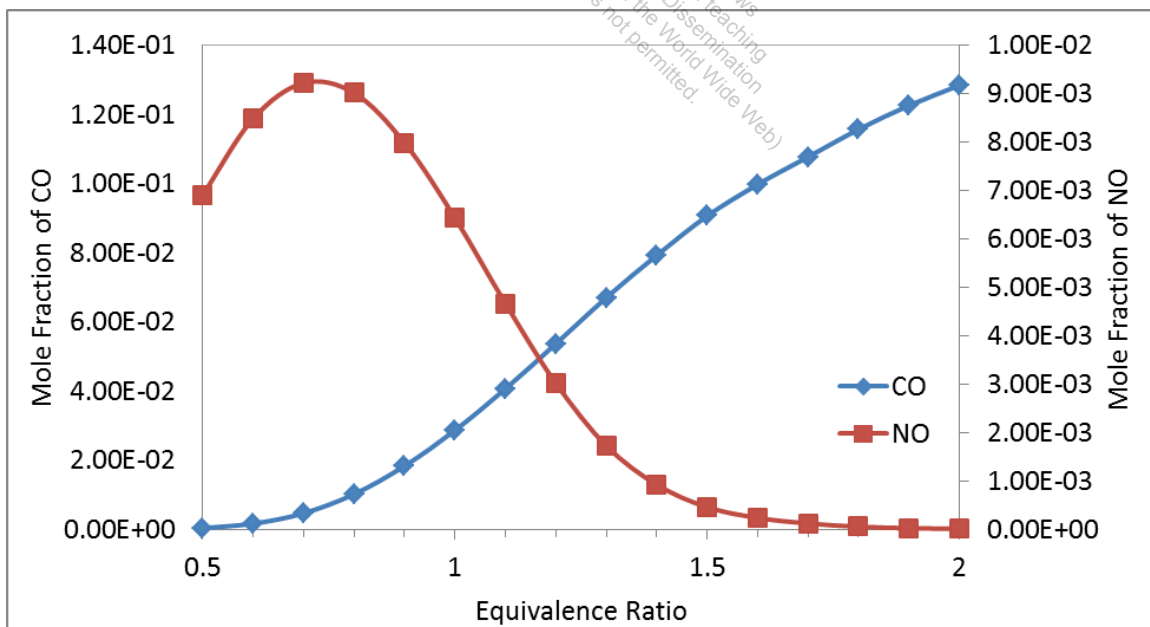
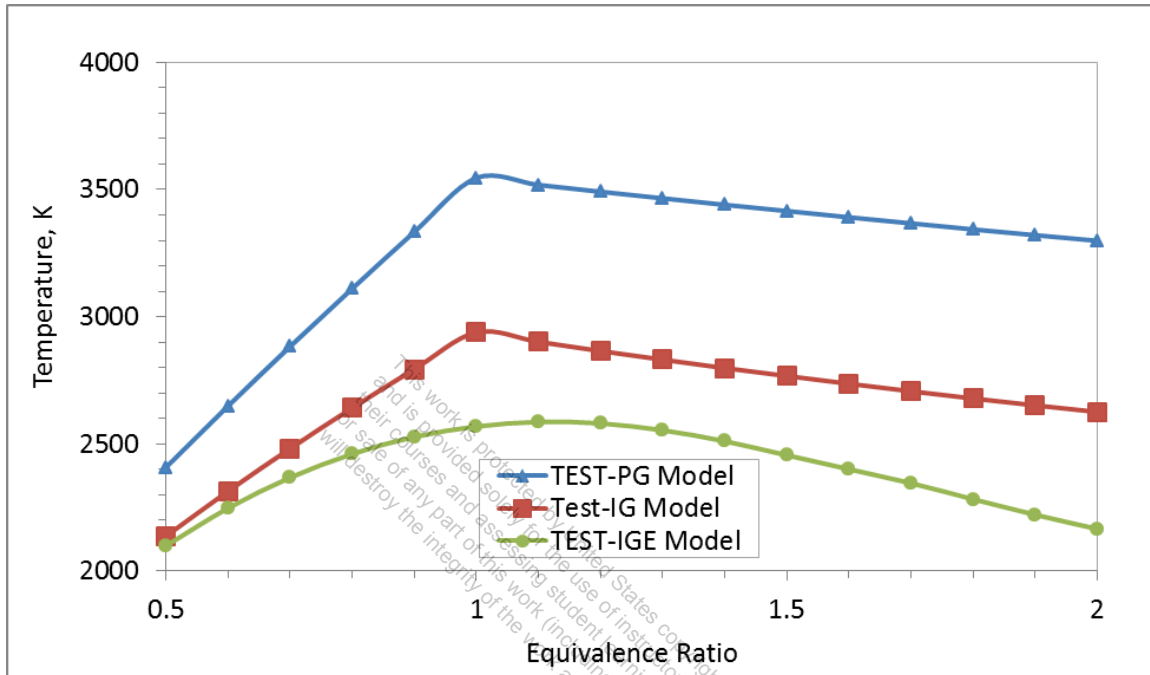
To compare the adiabatic flame temperature of the three different models used, they were plotted all in one graph.



**14-4-13 [BAR]** Repeat 14-4-12[BSW] if the reactants enter the chamber at 800°C and 1 atm.

### SOLUTION

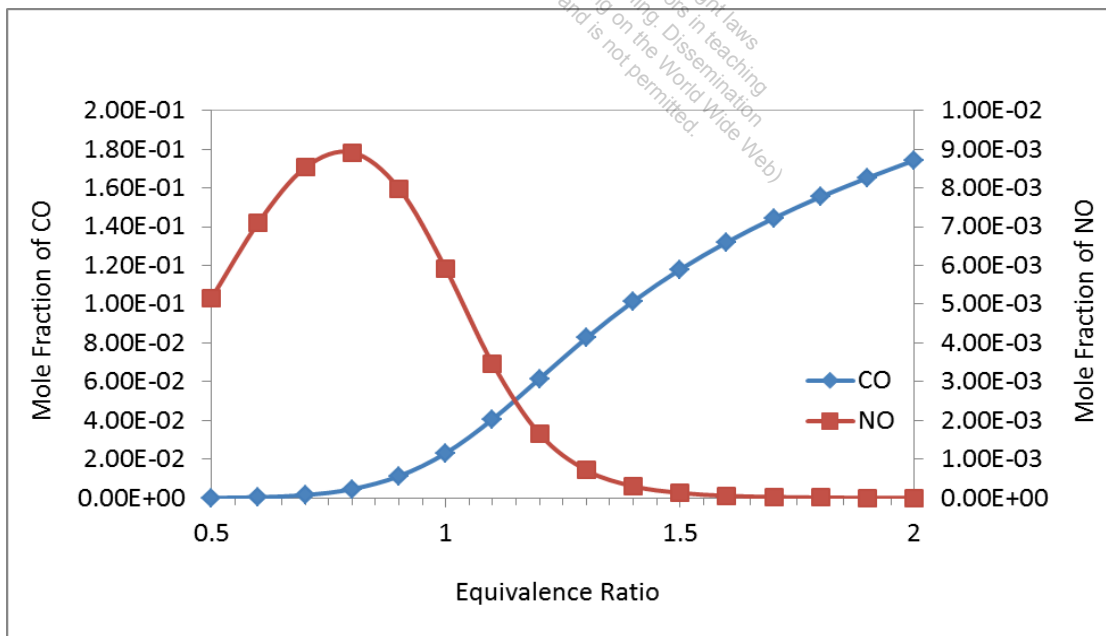
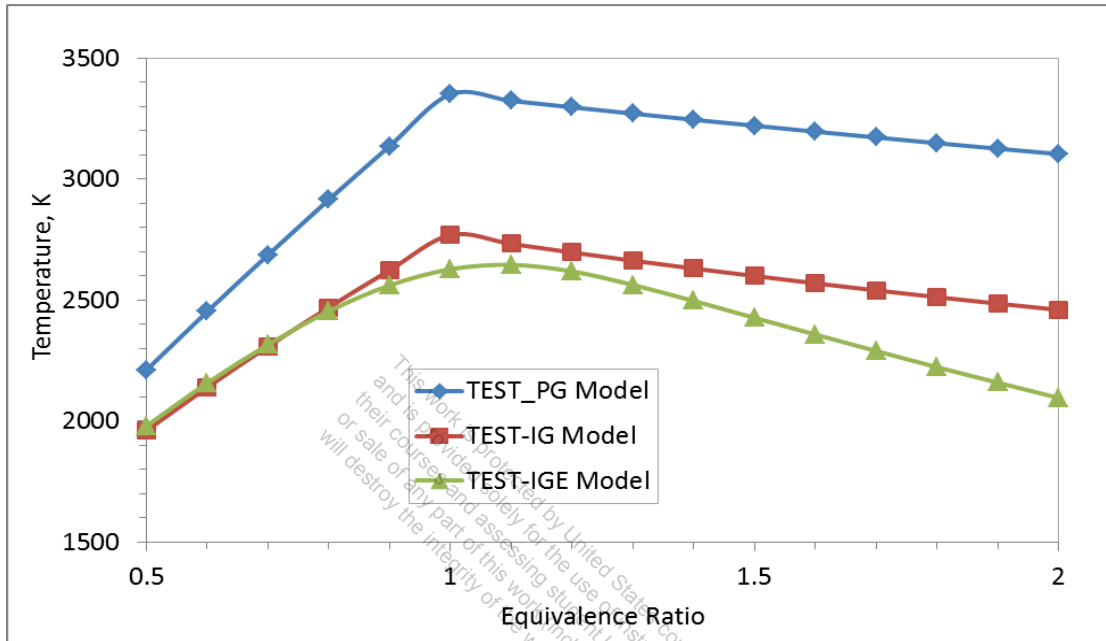
The data for the plots below is collected using TEST.



**14-4-14 [BAO]** Repeat 14-4-12[BSW] if the reactants enter the chamber at 600°C and 10 atm.

## SOLUTION

The data for the plots below is collected using TEST.





**14-4-15 [BAB]** Octane ( $C_8H_{18}$ ) at  $25^\circ C$ , 1 atm enters a combustion chamber and reacts with 111% theoretical air entering at the same conditions. If the products exiting at 1800 K contains CO,  $CO_2$ , CN, H,  $H_2$ ,  $H_2O$ , HCN, O,  $O_2$ ,  $O_3$ , OH, N,  $N_2$ ,  $N_2O$ , NO and  $NO_2$ , determine (a) the molar fraction of NO in the products, in ppm and (b) the heat transfer rate for a fuel mass flow rate of 1 kg/s. (c) What-if Scenario: What would the molar fraction of NO be if the chamber were adiabatic? (d) What is the equilibrium flame temperature?

## SOLUTION

Chemical Equilibrium Interactive: *Steady-State Reactor Simulator*

thermofluids.net · Interactives (Macromedia Flash Based Rich Interactive Animations) · **Steady-State Reactor**

Known Products Temperature | Known Heat Transfer | Graphical Output | Text Output

v10.10

**REACTANTS**  $C_8H_{18} + 11.36 (O_2 + 3.76 N_2)$  **PRODUCTS**

$\phi$  **1.10** A/F Ratio **13.66**  $\lambda$  **0.91** **100** kPa (5. Set pressure)

n-Octane (Liquid)  
1. Select a fuel

$O_2 + N_2$   
n-octane  
 $O_2 + N_2$

Rich Pure  $O_2$   
1.0  
Air  
Lean High  $N_2$   
3. Set equivalence ratio ( $\phi$ )

2. Set oxidizer composition

13.66 1.00 kg/s  
298.15 298.15 K  
4. Set inlet temperatures

8. Calculate  
9. Graphical Output

Parametric Study  
10. Choose parameters  
Equivalence Ratio ( $\phi$ )  
Start 0.5  
End 3.0  
# Steps 10  
11. Analyze  
Stop

1800 K (6. Set exit temp.)

7. Select products components (try default)  
☒ Equilibrium ☐ Complete ☐ Clear All  
☐ n-Octa ☐ CH<sub>3</sub> ☒ H ☒ O<sub>2</sub> ☒ N<sub>2</sub>O  
☐ C ☐ CH<sub>4</sub> ☒ H<sub>2</sub> ☒ O<sub>3</sub> ☒ NO  
☐ C<sub>2</sub>H<sub>2</sub> ☒ CO ☒ H<sub>2</sub>O ☒ OH ☒ NO<sub>2</sub>  
☐ C<sub>2</sub>N<sub>2</sub> ☒ CO<sub>2</sub> ☒ HCN ☒ N  
☐ C<sub>3</sub>H<sub>8</sub> ☒ CN ☒ O ☒ N<sub>2</sub>

Species	Products (kmol)	Mole Fraction	Mass Fraction
N <sub>2</sub>	42.7134	0.71527	0.71466
H <sub>2</sub> O	8.40781	0.14080	9.04677e-02
CO <sub>2</sub>	6.30940	0.10566	0.16585
CO	1.69060	2.83107e-02	2.82830e-02
H <sub>2</sub>	0.58998	9.87977e-03	7.10350e-04
OH	2.29441e-03	3.84220e-05	2.33065e-05
H	2.12801e-03	3.56354e-05	1.28370e-06
NO	4.22549e-04	7.07597e-06	7.57379e-06

Close

Select either (a) Known Products Temperature or (b) Known Heat Transfer tab, and follow steps 1 through 11.

**14-4-16 [BVL]** Octane ( $C_8H_{18}$ ) at  $25^\circ C$  and 100 kPa enters a combustion chamber and reacts with 100% theoretical air entering at the same conditions. Determine the equilibrium flame temperature assuming the products contains CO,  $CO_2$ , CN, H,  $H_2$ ,  $H_2O$ , HCN, O,  $O_2$ ,  $O_3$ , OH, N,  $N_2$ ,  $N_2O$ , NO and  $NO_2$ . Use the equilibrium Interactive linked from the left margin. (c) What-if Scenario: How would the temperature change if the chamber pressure were increased to 1 MPa?

## SOLUTION

Known Products Temperature Known Heat Transfer Graphical Output Text Output

v10.10

**REACTANTS**  $C_8H_{18}, n-o + 12.5 (O_2 + 3.76 N_2)$  **PRODUCTS**

$\phi$  **1.0** A/F Ratio **15.03**  $\lambda$  **1.0** **100** kPa (5. Set pressure)

n-Octane

1. Select a fuel

$O_2 + N_2$  n-Octane  $O_2 + N_2$

2. Set oxidizer composition

Rich Pure  $O_2$  1.0 Air Lean High  $N_2$

3. Set equivalence ratio ( $\phi$ )

4. Set inlet temperatures

**15.03** **1.00** kg/s **298.15** **298.15** K

8. Calculate 9. Graphical Output

**0** kW (6. Set heat transfer)

**Parametric Study**  
10. Choose parameters  
Equivalence Ratio ( $\phi$ )  
Start 0.5  
End 3.0  
# Steps 10  
11. Analyze  
Stop

7. Select products components (try default)  
☒ Equilibrium ☐ Complete ☐ Clear All  
☐  $C_8H_{18}$ , ☐  $CH_3$  ☒ H ☒  $O_2$  ☒  $N_2O$   
☐ C ☐  $CH_4$  ☒  $H_2$  ☒  $O_3$  ☒ NO  
☐  $C_2H_2$  ☒ CO ☒  $H_2O$  ☒ OH ☒  $NO_2$   
☐  $C_2N_2$  ☒  $CO_2$  ☒ HCN ☒ N  
☐  $C_3H_8$  ☒ CN ☒ O ☒  $N_2$

Species:	Products (kmol):	Mole Fraction:	Mass Fraction:
$N_2$	46.9169	0.72591	0.71787
$H_2O$	8.67459	0.13422	8.53569e-02
$CO_2$	7.11361	0.11006	0.17100
CO	0.88644	1.37153e-02	1.35617e-02
$O_2$	0.39775	6.15406e-03	6.95167e-03
OH	0.22896	3.54251e-03	2.12687e-03
$H_2$	0.19599	3.03242e-03	2.15798e-04
NO	0.16589	2.56670e-03	2.71917e-03

Close

Select a tab (a) Known Products Temperature or (b) Known Heat Transfer tab, and follow steps 1 through 11.

**14-4-17 [BVD]** In problem 13-2-10 [BVF], an equilibrium mixture consisting of  $\text{CO}_2$ ,  $\text{CO}$ ,  $\text{H}_2$ ,  $\text{H}_2\text{O}$  and  $\text{O}_2$  exits at 2500 K, 100 kPa. Determine (a) molar composition of  $\text{CO}_2$  at equilibrium and (b) the amount of heat transfer per kg of fuel. (c) What-if Scenario: What would be the heat transfer if there is no  $\text{CO}$  present in the products mixture?

## SOLUTION

**Reactants:**  $\text{C}_2\text{H}_6 + 14.00 (\text{O}_2 + 0.00 \text{N}_2)$

**Products:**

**Equivalence Ratio ( $\phi$ ):** 0.25

**A/F Ratio:** 0.08

**$\lambda$ :** 4.00

**Pressure:** 100 kPa (5. Set pressure)

**Inlet Temperatures:** 298.15 K

**Exit Temperature:** 2500 K (6. Set exit temp.)

**Heat Transfer:** -1120 kW

**Species Composition Table:**

Species:	Products (kmol):	Mole Fraction:	Mass Fraction:
$\text{O}_2$	10.5535	0.67853	0.70641
$\text{H}_2\text{O}$	2.97853	0.19150	0.11225
$\text{CO}_2$	1.91451	0.12309	0.17625
$\text{CO}$	8.54949e-02	5.49682e-03	5.00932e-03
$\text{H}_2$	2.14740e-02	1.38065e-03	9.05527e-05

**TEST Analysis** Launch the open-steady IGE equilibrium TESTcalc. In the composition panel, compose the reactants (fuel and oxygen). Select the products components. Evaluate the reactants state, State-1, with  $p_1 = 100$  kPa,  $T_1 = 298$  K, and the products state, State-2, with  $p_2 = p_1$  and  $T_2 = 3000$  K (select the Products radio-button). The mole fraction of  $\text{CO}_2$  can be found in the composition and the I/O panel. To determine the heat transfer, enter  $\dot{m}_{\text{dot}1} = 478$  kg/s,  $\dot{m}_{\text{dot}2} = \dot{m}_{\text{dot}1}$  (total amount of products for burning 1 kmol of fuel). In the device panel, load the inlet and exit states, and enter  $\dot{W}_{\text{dot\_ext}} = 0$  to obtain  $\dot{Q}_{\text{dot}}$ , which is positive, indicating heat must be added to obtain the given exit temperature. Repeat the solution with no  $\text{CO}$  in the products.