Lab Power Supply Manual Rev. B

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July 8, 2019

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5	4.8 Calibrating the output error indicator	3 4	The creation of this lab power supply was generously funded by the Reed College Physics Department. I would like to thank Edgar Perez for his
	5.1 The LT3081 linear regulator 5.2 The internal load 5.3 The Hot indicator circuit 5.4 The $V_{\rm out}$ error indicator circuit	4 4 4 5	kind advice, as well as Lucas Illing for supporting this project.
6	Schematic Diagram	8	2 Motivation
7	Printed Circuit Board Layers	9	Often when working in electronics, several voltage sources are needed. In addition to a main
	 7.1 Front Copper 7.2 Back Copper 7.3 Front Solder Mask 7.4 Back Solder Mask 7.5 Front Silk Screen 7.6 Front Fabrication 7.7 Plated Through-Hole Drill Map 7.8 Non-Plated Through-Hole Drill Map 		power rail, one may need a complementary negative power rail for analog circuitry, or a different logic power supply at 3.3 V instead of 5 V. Low-impedance bias voltages are also a frequent requirement, needed for biasing BJTs, comparator inputs, and more. For most applications, a power supply fulfilling the requirements of these applications need not be
	7.9 User Comments	17 18	capable of supplying much more than 1 A of current, must have a stable voltage output (requiring

a linear regulator), and must have a current limiting function. Additionally, it would be nice if the power supply was much smaller than a conventional 30 V, 3 A output bench power supply with a large transformer, being conveniently powered from a common wall plug, batteries, or any other DC power source at hand. I have attempted to construct such a power supply.

3 Safety Notice (Grounding)

Please note that the negative voltage output of the supply is directly connected to the negative voltage input to the supply. That is, the output voltage of the supply floating relative to earth ground if and only if the input voltage is floating.

If you are uncertain if the supply (or any other piece of equipment) is floating, it is quick and simple to check if this is the case. Set a digital multimeter to its resistance measurement or continuity check mode. Connect one probe to the negative output of the PSU (the black five-way binding post) or to the other terminal in question, and then connect the other probe to earth ground. This can be done either by insertion in to the *earth* socket of a wall outlet, or by touching the outside of a BNC connector on any nearby oscilloscopes, as these are almost always earth grounded. If inserting into a wall outlet, be certain that you know which hole is which, and that you are using a multimeter approved for wall testing (most are).

If the output is not floating (earth-referenced), then one must be careful to only connect oscilloscope ground leads to the negative output of the supply. Whatever the ground lead is connected to will be shorted to earth ground. If an incorrect connection is made, then connected circuit components, oscilloscopes, or computers (e.g. through USB) may be damaged. If you are uncertain, connect probes as if the circuit is not floating.

If the output is floating (or if you know which terminals are earthed and which are not), then the supply may be safely connected to other voltage sources in whatever configurations are convenient, such as in a dual-rail setup.

4 Usage Instructions

4.1 Setting the output voltage

Connect a voltmeter to the output of the supply. You may use either the binding posts or the test points labeled on the board to achieve this. Turn the PSU on and adjust the voltage using the coarse and fine adjustment knobs as needed. Note that the maximum output voltage is about 1.5 V below the input voltage.

4.2 Setting the current limit

To set the current limit to its minimum value, short the minimum limit jumper (labeled *Min Lim*, JP1). To set the current limit to higher than this value, the jumper must be *open*.

The current limit is set to fixed values by moving the switches on the board. The default values are 1, 2.5, 5, 10, 25, 50, and 100 mA. To set the limit to any of the upper four values, the switch for the lower values must be in its rightmost position, as indicated on the board.

Alternatively, the switch section on the board may not be populated, and a $10\,\mathrm{k}\Omega$ (preferably 10-turn) potentiometer (RV4) may be soldered in to provide a continuously variable current limit.

To set the current limit to its maximum value, open the no limit jumper (labeled No Limit, JP2). To set the current limit to lower than this value, the jumper must be shorted. The maximum value is about 2.0 A in normal operation, and less when the device shuts down to prevent overheating.

4.3 Indicator LEDs

The power supply includes two indicator LEDs for when output voltage regulation is not guaranteed.

The Hot indicator LED (D2) lights when the main regulation IC (see Section 5.1) starts to get hot (when the junction temperature is about 100 °C or above). This light is a warning, and the output should continue to be regulated as normal. If the IC continues to heat up (to a junction temperature of 125 °C), then internal protection circuitry will prevent damage and reduce the output voltage.

The V_{out} Error (I lim) indicator LED (D1) lights when the actual output voltage is not sufficiently close to the set output voltage. The most common cause for this is if the current limiting function is active, but internal protection circuitry or a set voltage that is too high may also cause an output error.

4.4 Monitoring the output current

If it is not preferred to use an ammeter to measure the output current, the I_{out} test point is provided for convenient measurement or external control of the load current. The signal at I_{out} is one volt for every ampere of output current, including the internal load (see Table 1 and Section 5.2). For example, if the supply is outputting 25 mA total, then I_{out} should read 25 mV.

4.5 Monitoring the internal temperature

For more quantitative information about the temperature of the main regulation IC (see Section 5.1) than is provided by the Hot indicator LED, the Temp test point is provided. The signal at Temp is one millivolt for every degree Celsius of junction temperature. For example, if the junction temperature of the IC is about $73\,^{\circ}$ C (subject to variation inside the IC), then Temp should read $73\,\mathrm{mV}$.

4.6 Disabling the internal load

The internal load may be disabled by opening the *Internal Load* jumper. Note that this will increase the current limit by at most 4 mA above the current limit displayed on the switches or that previously set by RV4, if installed. For most purposes, the *Internal Load* jumper should be in its normal, shorted position (see Section 5.2).

4.7 Calibrating the current limit

The power supply requires a minimum load in order to regulate the output voltage properly. An internal load usually supplies this minimum load (see Section 5.2), but this offsets the effective

current limit on the output. A trimmer potentiometer is provided to compensate for this offset.

First, choose which current limit range you most value precision on, say the 10 mA range. Set the supply to a relatively low voltage, like 1 V, and place the appropriate load on the output of the supply with a potentiometer. In this case, we would adjust a potentiometer until it drew 10 mA through itself. The V_{out} Error (I lim) indicator LED should be off. Measuring I_{out} should show about 13 mV, corresponding the 10 mA external load and the (fixed) 3 mA internal load. Using a screwdriver, adjust the potentiometer (labeled Load Offset, RV1) until the output voltage is stable (no current limiting), and then carefully reverse direction and adjust until the current limit just starts to activate. This may be judged by checking the output voltage with a voltmeter, or by using the built-in indicator if it is calibrated as described in Section 4.8. If using a voltmeter (the more precise method), aim for a limit situation where the output is about 10 mV below the set (stable) voltage.

4.8 Calibrating the output error indicator

The issues associated with creating a reliable output error indicator are discussed in Section 5.4. If necessary, a trimmer potentiometer (RV5) may be populated to correct the default setting by the resistor R21.

Attach a voltmeter to the PSU and set the output voltage to 1 V. Attach an external potentiometer to the output of the supply, valued to draw a typical current for your application. Set the PSU current limit so that increasing the load current will trigger the limit function. If the 1 V output does not demand enough current, it may be increased, but try to keep it as low as possible (see 5.4 for why). Wait until the temperature of the circuit has stabilized. Error on the side of drawing a slightly lower current than needed, depending on the sensitivity required (see below). Increase the load gradually, and watch the error indicator LED (D1).

If the default indication threshold set by R21 is not sensitive enough for your needs, solder in

the $500\,\mathrm{k}\Omega$ RV5 and try the adjustment procedure below.

If this does not work, or if the default indication did not work at all, solder in RV5 and *remove* R21. This provides a wider range of variation for the indication threshold, at the cost of a coarser adjustment rate.

With the potentiometer RV5 and the default resistor R21 soldered on the board or not depending on your needs, adjust the external load potentiometer until the output is $2-10\,\mathrm{mV}$ below the set voltage. If you intend to use the supply only above about 5 V, the lower the better (you may even be able to remove RV5 and wire a short across R21 for a bit more sensitivity). To complete the calibration, adjust RV5 to the barrier where D1 just barely lights, or perhaps flickers.

5 Principles of Operation

5.1 The LT3081 linear regulator

All of the regulation that the power supply provides is done by the LT3081, a rugged linear regulator IC. The regulation circuitry is depicted in Figure 1. An internal current source of $50\,\mu\text{A}$ allows the set voltage to be configured with a single resistor R_{set} . In the power supply, R_{set} is determined by the two potentiometers RV2 and RV3.

If $V_{\text{out}} < V_{\text{set}}$, then the error amplifier will increase the base voltage of the NPN transistor until the entire Sziklai pair has V_{set} at its emitter. Similarly, the base voltage will be suitably reduced if $V_{\text{out}} > V_{\text{set}}$. In this way, the output voltage is regulated by a negative feedback loop.

In practice, it may be difficult to stabilize such a circuit constructed of discrete components against oscillation. Using an integrated circuit solution such as the LT3081 allows us to have matched transistors at close to the same temperature, as well as to take advantage of the work done by previous engineers to make the output voltage stable. We simply add on some additional capacitances (C1 to C4 and C8) to improve noise characteristics, transcient performance, and stability a bit more.

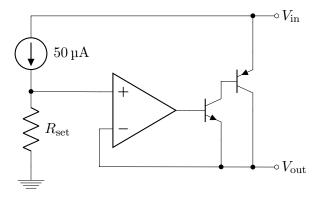


Figure 1: The equivalent voltage regulation circuitry inside the LT3081. The equivalent current regulation circuitry is not depicted here or in the LT3081 datasheet.

5.2 The internal load

Given the requirement that any circuitry used in the power supply must function consistently over the entire range of $V_{\rm in}$, a simple resistor (as in the LT3081 datasheet) cannot be used as a means of meeting the minimum load requirement of the LT3081. Instead, the LM334 current source (U4) was used. With R23 set to 22Ω , we expect about 3.1 mA to be sunk from the output of the power supply, which is well above the minimum load requirement of the LM3081, over temperature. Since we are manually nulling the offset due to this current, it is allowable to use a common through-hole 5% tolerance resistor for R23, but if your application requires precise current limiting over a wide and changing range of temperatures, a 1% or better tolerance resistor should be used for added thermal stability.

5.3 The *Hot* indicator circuit

To establish a precise voltage of $100 \,\mathrm{mV}$ over the entire range of V_{in} , corresponding to a junction temperature of $100 \,^{\circ}\mathrm{C}$, a $2.5 \,\mathrm{V}$ LM4040 voltage reference (U1) and a voltage divider were used. The LM393 comparator (U3B) compares the Temp output to this reference temperature, and is configured to pull the open collector output of the comparator low if the Temp output goes above the reference. This connects the indicator LED to ground. A LM317 (U6) configured as a cur-

Table 1: Electrical characteristics. The ♦ mark indicates specifications which apply over the full operating temperature range. Otherwise, specifications are at (junction) temperatures of 25 °C. Note that application of negative input voltages may damage the supply. Specifically, such damage tends to disable any current limiting functionality, while maintaining the capability for voltage regulation.

Parameter		Conditions		Min	Тур	Max	Units
Input Voltage	$V_{ m in}$)	5.0		32.0	V
Output Voltage	$V_{ m out}$	$I_{\rm load} < I_{\rm lim}, V_{\rm in} < 16 \mathrm{V}$	•	0.7		$V_{\rm in} - V_{\rm do}$	V
		$I_{\rm load} < I_{\rm lim}, V_{\rm in} \ge 16 \mathrm{V}$	•	0.7		16	V
		No internal load	•	0.0			V
Dropout Voltage	$V_{ m do}$	$I_{\text{load}} = 100 \text{mA}$			1.21		V
		$I_{\text{load}} = 1.5 \text{A}$	•		1.23	1.5	V
Internal Current Limit	$I_{ m max}$	$V_{\rm in} = 5 \text{V}, V_{\rm set} = 0 \text{V}, V_{\rm out} = -0.1 \text{V}$	•	1.5	2.0		A
$I_{ m out}$ Relative Error		$I_{\text{load}} = 1.5 \text{A}$		0	6	11	%
I_{out} Operating Range		()	$V_{ m out}-40{ m V}$		$V_{ m out} + 0.4{ m V}$	V
Temp Absolute Error		$0 ^{\circ}\text{C} \le T_J \le 125 ^{\circ}\text{C}$		-10		10	μA
		$125 ^{\circ}\text{C} < T_J \le 150 ^{\circ}\text{C}$		-15		15	μA
Ripple Rejection	PSRR	$f = 120 \mathrm{Hz}$		75	90		dB
$V_{\text{ripple}} = 0.5 \text{V}_{\text{pp}}, I_{\text{load}} = 0.1 \text{A},$		f = 10 kHz			75		dB
$V_{\rm in} = V_{\rm out(nom)} + 3 \mathrm{V}$		$f = 1 \mathrm{MHz}$			20		dB
Internal Load	$I_{ m int}$	│	•	2	3	4	mA

rent source supplies a stable current to the LED over the full range of $V_{\rm in}$. Inspection of the circuit shows that errors introduced by resistor tolerances and comparator input offset currents and voltages will result in an absolute error of at most 5 °C. Furthermore, the comparator operates without hysteresis, so the LED may flicker when the actual and reference temperatures coincide. For the purpose of a coarse temperature indication, these undesirable characteristics are inconsequential.

5.4 The V_{out} error indicator circuit

The general configuration of the $V_{\rm out}$ error indicator circuit is similar to that of the Hot indicator circuit, described in Section 5.3. However, the error introduced by that circuit is unacceptable for the purpose of displaying the current status of regulation. Additionally, we expect the output voltage to coincide precisely (to within a few millivolts) with the set voltage. Without any correction, the LED may reasonably indicate an error indefinitely, or at least flicker, when the output voltage is actually well-regulated.

The standard solution that one may propose is to add hysteresis (in the form of a Schmitt trigger) to the comparator. This will not work. A Schmitt trigger must have an upper trigger threshold that lies *above* the set voltage, but in

the course of recovering from current limiting, the output voltage may never overshoot the set voltage. Thus the threshold will never be crossed, and the error indicator may remain on indefinitely. What is needed instead, is a small offset.

If the comparator recieved a set voltage that was, say, $10\,\mathrm{mV}$ below V_{set} , then the problem is solved. Hysteresis is not even needed, since most all causes for a failure in regulation will not manifest as a steady offset of $10\,\mathrm{mV}$. But how can we create such a small offset over the entire range of V_{out} , especially when the offset is comparable in size to all of the sources of error involved? The main barriers to control that must be addressed include

- Resistor tolerances,
- Loading of input sources,
- Comparator input offset voltage,
- Comparator input bias current,
- Comparator input offset current, and
- Noise.

Since the entire point of adding the offset is to allow for errors, we can deal with the comparator input offset voltage and current by lumping in the

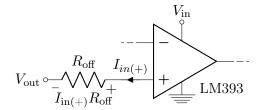


Figure 2: Introducing a small voltage offset by exploiting the input bias current of the LM393 comparator.

effect of their worst-case absolute errors with the error in regulation. This increases the minimum offset needed from that due to regulation, but only to about the 10 mV stated before. However, we cannot increase the offset too much: at an output voltage of 1.00 V, an offset of 10 mV already represents a 1% error in indication. The aim is to keep this level of precision for set voltages from 1.00 V to 30.0 V. If better precision than about 10% is needed below about 100 mV, the calibration procedure detailed in Section 4.8 may be done at the necessary low voltage, at the cost of less realiable indication at higher voltages of 10 V to 30 V, depending on the configuration.

So how are we to obtain the offset? Since the input bias current of the comparator may introduce errors comparable to the offset, we can change perspective. The "error" that it introduces can in fact be used as the offset. The LM393 and many other common differential-input analog devices such as the LM358 have PNP darlington pair input stages. This means that any input bias current will flow out of the input terminals, conveniently allowing us to place a resistor on the noninverting input of the comparator to achieve an offset in the correct direction. Since the noninverting input is connected to the low-impedance V_{out} , the offset voltage introduced may be reliably predicted as $I_{\text{in}(+)}R_{\text{off}}$ (see Figure 2). For the typical $I_{\text{in}(+)} = 25 \,\text{nA}$ and $R_{\text{off}} = 150 \,\text{k}\Omega$ (R21), we obtain an offset of 3.8 mV. This should handle possible offsets due to comparator input offset voltage and regulation of up to 3 mV, and more offset may be provided with a potentiometer as described in Section 4.8.

But there is a problem with this circuit. Let's

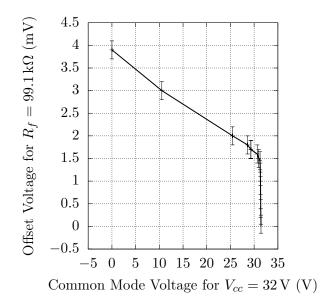


Figure 3: In the configuration of Figure 2, the offset voltage due to the input bias current of the LM358 decreases with increasing common mode voltage.

take a closer look at the input bias current. While datasheets like that for the LM393 give the input bias current at $0\,\mathrm{V}$ common mode voltage, we must know it for all common mode voltages up to V_{in} . The LM358 has a simpler input stage than the LM393, so let's look at it instead to understand what is going on. Some quick measurements reveal that the offset voltage we are after decreases with increasing common mode voltage (Figure 3). For simplicity, we may treat this decrease as linear, as we will only be operating in the approximately linear region.

Thus our solution does not work well at high common mode voltages. We fix this by adding a high-ratio voltage divider on the other input to the comparator. Note that for a voltage divider with gain close to unity $(R_1 \ll R_2)$,

$$A_V = \frac{R_b}{R_a + R_b} = \frac{1}{1 + R_a/R_b} \approx 1 - R_a/R_b \ .$$

Thus with 1% resistors, we expect a relative error of about 1.4% in R_a/R_b . For the values actually used (R17 and R18), we then obtain an absolute error of 21 μ V per volt in, giving a worst case 0.6 mV error for a 30 V input. Not bad.

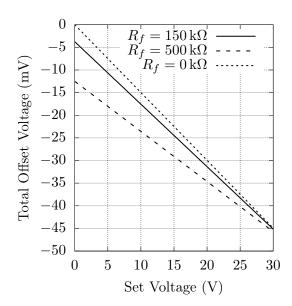
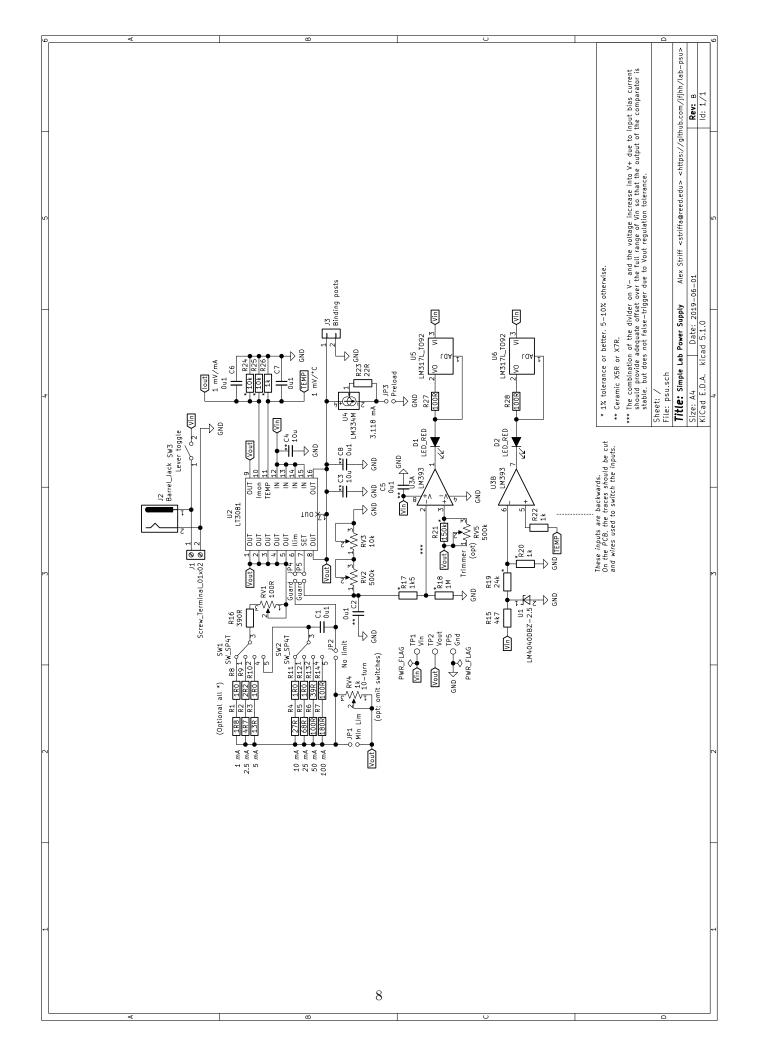
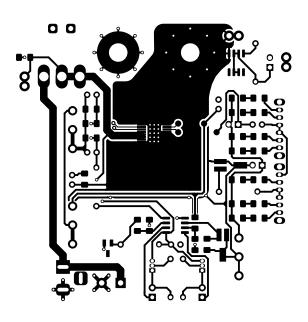


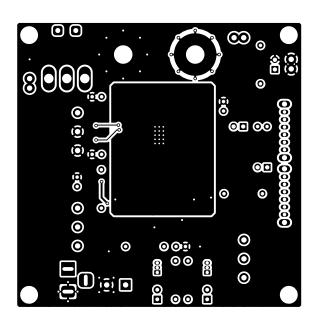
Figure 4: The expected offsets from the full offset circuit for varying values of R_f .

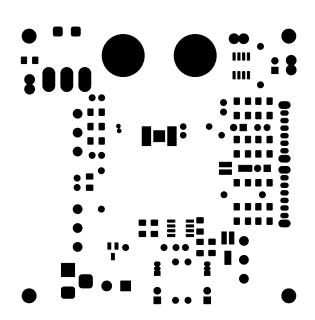
Now that we know why, a quick analysis of the actual offset circuit, where we have both offset methods acting together, gives the characteristic plot of Figure 4. Values were chosen to give an increasing offset with common mode, rather than the constant offset originally discussed, for additional margin and a more understandable relative-drop trigger, rather than an offset trigger. This way, the higher voltage ranges do not seem more sensitive to loading than the lower ranges.

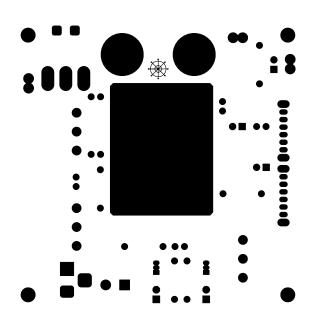


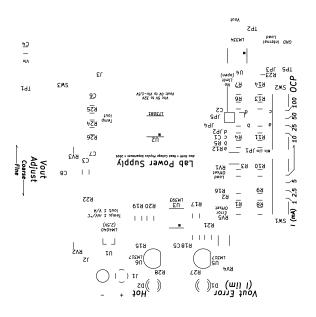
7 Printed Circuit Board Layers

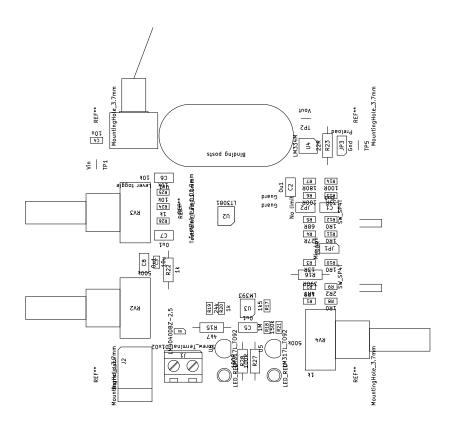


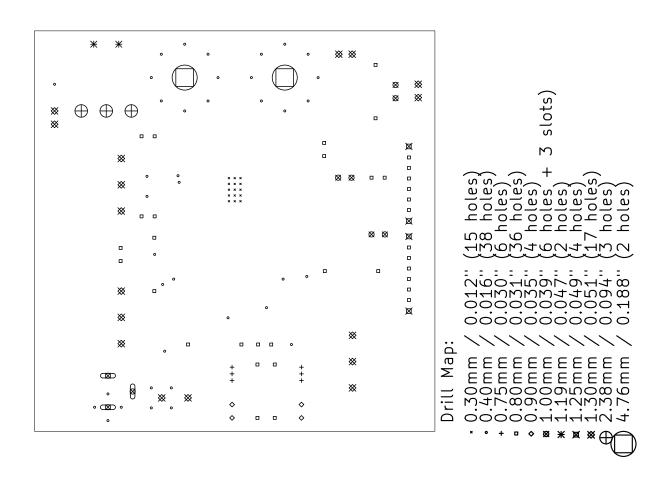


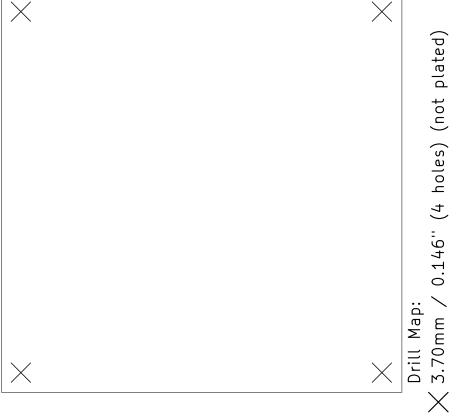












Material: 1.6 mm FR4 (standard); 1 oz copper; 2 layers. Board dimensions: 3 in x 3 in. Colors: White solder mask, black silk screen (front). Surface finish: HASL (with lead) (standard). NO gold fingers NO panelization NO castellated holes NO tented vias NO stencil

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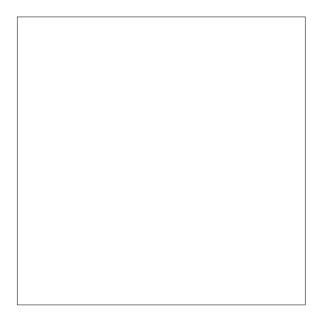


 Table 2: Bill of materials with collated items. There are 60 components total.

Item	Qty	Reference(s)	Value	LibPart	Footprint
-	9	2 2 2 2 2	01	Doming Compil	Consistent THT, C Rice DE Own Wo Euro Do Eftern
٦ ،	0 (CI, Cz, C3, C6, C1, C6	ınn	Device:	Capacitor Intic Disc Doum Weblin February
7	?	S, E	10u	Device: C_Small	Capacitor_SMD:C_1206_3216Metric_Pad1.42x1.75mm_HandSolder
က	2	D1, D2	LED_RED	Device:LED_ALT	LED_THT:LED_D3.0mm
4	П	J1	Screw_Terminal_01x02	Connector:Screw_Terminal_01x02	TerminalBlock MetzConnect:TerminalBlock MetzConnect Type094 RT03502HBLU 1x02 P5.00mm Horizontal
50	_	J2	Barrel Jack	Connector:Barrel Jack	Connector BarrelJack:BarrelJack Horizontal
9	П	J3	x	Connector Generic:Conn 01x02	psu-foot:Binding Posts
- 1-	-	IBI		Device:Immber NO Small	Connector PinHaader 2 54mm-PinHeader 1x()? P2 54mm Vertical
- oc		JP2		Device: Jumper NO Small	Connector Pin Header 2.54mm.Pin Header 1x02 P5.54mm Vertical
0 0	٠.	ID3		Designation Transfer	Commerced II Interest Section 1 - 100 DD E 4 - 1 - 1 - 100 DD E 4 - 1 - 1 - 100 DD E 4 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
, מ	- •	JF3		Device:Jumper_NO_Small	Connector Tin Header 2.54mm; Tin Header 1x02 F2.54mm Vertical
10	7	JP4, JP5	rd	Device:Jumper_NO_Small	psu-foot;GuardJumper
11	_	R1	1R8	Device:R	Resistor_SMD:R_1206_3216Metric_Pad1.42x1.75mm_HandSolder
12	_	R2	4R7	Device:R	Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
13	П	R3	13R	Device:R	Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
14	-	R4	27B.	Device:R.	Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
15	-	R5	68R		Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
16	2	R6. R14	100R		Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
17		B.7	180R		Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
×	4	B8 B10 B11 B12	180		Resistor SMD·R 1206 3216Metric Pad142×175mm HandSolder
9 5	۰.	E0, 1010, 1011, 1012	303	wiso. D	Accessor South 1200 Colonial Contract Thront Hendeldon
13		ng.			Nession 500 D. 1200 5210Metric Fatt. 2211. Juliu Handsouter
50	_	R13		Device:R	Resistor_SMD:R_1206_3216Metric_Pad1.42x1.75mm_HandSolder
21	_	R15			Resistor_THT:R_Axial_DIN0207_L6.3mm_D2.5mm_P10.16mm_Horizontal
22	_	R16	390R	Device:R	Resistor_THT:R_Axial_DIN0207_L6.3mm_D2.5mm_P10.16mm_Horizontal
23	_	R17	1k5	Device:R	Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
24	_	R18	^{1}M	Device:R	Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
25	П	R19	24k	Device:R	Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
56	2	R20, R26	1k	Device:R	Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
27	-	R21	150k	Device: B.	Resistor SMD:R 1206 3216Metric Pad1.42x1.75mm HandSolder
: 83	-	R22	14		Resistor THT: R Axial DIN0207 L6.3mm D2.5mm P10.16mm Horizontal
53	-	B23	22B	evice:B	Resistor THT: R Axial DIN0207 L6.3mm D2.5mm P10.16mm Horizontal
8	· c	B34 B35	101	Dornico:R	Raciety CMD. 1906 2916Matric Bad 1494 75mm Handsdam
3 25	10	R27 R28	100B	Device:B	Resistor THE Axia DINOQT 16.3mm D2.5mm P10.16mm.
33	ı -	BV1	100B	Darrico:R POT 11S	ren-foot-Trim not former TC-23X-9-10HF
33 83	٠.	EV.	5001	Derico: POT 118	postrocismus Downs I woode - I woode - I work to Defend on the Charles of the Control of the Con
76	٠.	IV 2 DV3		Device: IL C.	1 overlations of a 1111. Octavalent of the control
t t	٠.	DAZA		Device: n_roi_roi	To occur to the control of the contr
8	٦.	KV4		Device:R_FUI_US	Potentiometer THT: Fotentiometer Prier PC-16_Single_Horizontal
36		RV5		Device:R_POT_US	psu-foot:Trim_pot_Bourns_TC33X-2-101E
37	2	SW1, SW2	SW_SP4T		$psu-foot:SP4T_CK_SK-14D01-G-6$
38	1	SW3	Lever toggle		psu-foot;SW_SPST_Lever_Rubber
33	П	U1	LM4040DBZ-2.5	14040DBZ-2.5	Package TO SOT SMD:SOT-23
40	П	U2	LT3081		Package SO:HTSSOP-16-1EP 44x5mm P0.65mm EP3.4x5mm Mask3x3mm ThermalVias
41	П	U3	LM393	1393	Package SO:SOIC-8 3.9x4.9mm_P1.27mm
42	П	U4	LM334M	Reference_Current:LM334M	Package SO:SOIC-8 3.9x4.9mm_P1.27mm
43	2	U5, U6	$LM317L_TO92$	Regulator_Linear:LM317L_TO92	Package_TO_SOT_THT:TO-92_Inline