The basis of the pulse input experiment lies in the Dirac delta. A variety of definitions for the Dirac delta exist. The definition to be used herein is that it is the limit of a Gaussian distribution as the standard deviation becomes very small [??]:

$$\delta(t) = \lim_{\sigma \to 0} \frac{1}{\sigma \sqrt{2\pi}} e^{-\frac{t^2}{2\sigma^2}} \tag{1}$$

Given that the Dirac delta takes on the same form as a probability distribution, the following must be true:

$$\int_{-\infty}^{+\infty} \delta(t)dt = 1 \tag{2}$$

This very easily extends to the following (for  $t_0 \in \mathbb{R}$ ):

$$\int_{-\infty}^{+\infty} \delta(t - t_0) dt$$

$$= \int_{-\infty}^{+\infty} \delta(t') dt' \left( let \ t' = t - t_0 \right)$$

$$= 1 \left( by \ equation \ (??) \right)$$
(3)

The proof is omitted for the sake of brevity, but the following results from equation (??):

$$\int \delta(t - t_0)dt = \mathcal{U}(t - t_0) \tag{4}$$

Here,  $\mathcal{U}(t)$  is the unit step function, which is 1 for  $t \geq 0$  and 0 for t < 0. Given this information, an important result, known as the sifting property, can be ascertained [??]. Let f(t) be a continuous function such that  $\lim_{t \to +\infty} f(t) = \lim_{t \to -\infty} f(t) = 0$  and  $t_0 \in \mathbb{R}$ :

$$\int_{-\infty}^{+\infty} \delta(t - t_0) f(t) dt = [f(t) \int \delta(t - t_0) dt]|_{-\infty}^{+\infty} - \int_{-\infty}^{+\infty} f'(t) [\int \delta(t - t_0) dt] dt$$

$$= [f(t) \mathcal{U}(t - t_0)]|_{-\infty}^{+\infty} - \int_{-\infty}^{+\infty} f'(t) \mathcal{U}(t - t_0) dt \ (by \ equation \ (\ref{eq:total_$$

These properties of the Dirac delta prove to be useful when discussing linear time-invariant, or LTI, systems. For an input signal x(t) to a causal LTI system  $\mathcal{T}$ , the output signal y(t) is given by:

$$y(t) = x(t) * h(t) = \int_0^{+\infty} h(\tau)x(t-\tau)d\tau$$
 (6)

The function h(t) is known as the system's impulse response. The purpose of this portion of the experiment is to determine the impulse response h(t) since all information about the high-pass and low-pass filtering systems can be acquired from this function alone. h(t) can be acquired by applying a Dirac delta as the input and observing the system's response. To acquire the theoretical impulse response, the Laplace transform of f(t) must first be defined:

$$\mathcal{L}\{f(t)\} = \int_{0^{-}}^{+\infty} e^{-st} f(t) dt \ (s \in \mathbb{C})$$
 (7)

This leads to a necessary result in the theory of LTI systems known as the convolution theorem [??]:

$$\mathcal{L}\{x(t) * h(t)\} = X(s)H(s) \tag{8}$$

X(s) and H(s) are the Laplace transforms of x(t) and h(t), respectively. Specifically, H(s) is known as the transfer function.

The Dirac delta is used as the input to the filters because its output is simply the impulse response. Without performing a formal proof, it is clear by equation (??) that  $\delta(t)$  is 0 except at t=0, where its value becomes very large. With this knowledge, the Laplace transform of the Dirac delta is proven to be 1:

$$\mathcal{L}\{\delta(t)\} = \int_{0^{-}}^{+\infty} e^{-st} \delta(t) dt \ (by \ equation \ (\ref{eq:constraints}))$$

$$= 0 + \int_{0^{-}}^{+\infty} e^{-st} \delta(t) dt$$

$$= \int_{-\infty}^{0^{-}} e^{-st} \delta(t) dt + \int_{0^{-}}^{+\infty} e^{-st} \delta(t) dt$$

$$= \int_{-\infty}^{+\infty} e^{-st} \delta(t) dt$$

$$= e^{-s \cdot 0} \ (by \ equation \ (\ref{eq:constraints}))$$

$$= 1$$

Assume the existence of an inverse Laplace transform  $\mathcal{L}^{-1}$ . The statement above can then be proven, justifying the use of the Dirac delta as the input to the system:

$$y(t) = \delta(t) * h(t)$$

$$\mathcal{L}\{y(t)\} = \mathcal{L}\{\delta(t) * h(t)\}$$

$$\mathcal{L}\{y(t)\} = \mathcal{L}\{\delta(t)\} \cdot \mathcal{L}\{h(t)\} \ (by \ equation \ (\ref{eq:constraints}))$$

$$\mathcal{L}\{y(t)\} = 1 \cdot H(s) = H(s) \ (by \ equation \ (\ref{eq:constraints}))$$

$$y(t) = \mathcal{L}^{-1}\{H(s)\} = \mathcal{L}^{-1}\{\mathcal{L}\{h(t)\}\} = h(t)$$

$$(10)$$

## 0.0.1 Low-Pass Filter

The transfer function for the low-pass filter can be acquired using voltage division in the Laplace domain with the output voltage taken over the capacitor:

$$H(s) = \frac{\frac{1}{sC}}{\frac{1}{sC} + R} = \frac{\frac{1}{RC}}{\frac{1}{RC} + s} \xrightarrow{\mathcal{L}^{-1}} h(t) = \frac{e^{-\frac{t}{\tau}}}{\tau} \left( \text{ by equation (??)} \right)$$
 (11)

Here,  $\tau = RC$  is the time constant. It can be experimentally measured by observing where h(t) acquires a value of  $e^{-1} \approx 0.37$  times the maximum value of h(t) at the start (t=0). See the "Appendix" section at the end for the script that generates the tables and data.

□ ./images/LPF response .JPG

Figure 1: Low-Pass Filter Impulse Response

Resistor R is  $10k\Omega$ . Capacitor C is 1nF. Frequency is set to 20kHz. Pulse height is 20V. Pulse width is  $1\mu s$ . Each value represents a different measurement. The first reported value is a 1  $\tau$  measurement. The next is a 2  $\tau$  measurement, and so on.

The results for the low-pass filter are fairly close to theory. At the very beginning, the quick surge of the power supply's voltage charges the capacitor. When the pulse turns off, the capacitor simply discharges, and its voltage decays exponentially. Each measurement corresponds to a particular number of time constants. The first is  $\tau$  calculated by observing the point at which the voltage is  $e^{-1}$  times its peak value. The second is  $\tau$  calculated by finding the point that is  $e^{-2}$  of the peak, which would be  $t=2\tau$ , and then dividing the time by 2. As the measurements are taken at later values of t, the approximation for  $\tau$  has a lower and lower percentage error from theory. Thus, much of the error is a result of the difficulty of acquiring accurate measurements from  $\tau$  rather than deviations from theory. For minimal error, a very low pulse frequency should be used, and measurements should be taken at a later time, like  $t=5\tau$ , dividing by 5 to acquire  $\tau$ . Another potential source of error is the nonideality of the Dirac delta input. Because the input voltage pulse has a finite height of 20V and a finite width of  $1\mu s$ , the results deviate from when the input signal is perfectly  $\delta(t)$ .

## 0.0.2 High-Pass Filter

The high-pass filter's impulse response can also be acquired using voltage division:

$$h(t) = \mathcal{L}^{-1}\left\{\frac{sRC}{1 + sRC}\right\} = \delta(t) - \frac{e^{-\frac{t}{RC}}}{RC}$$
(12)

☐./images/HPF closeup".JPG

Figure 2: Attempt 1 - High-Pass Filter Impulse Response

The same settings are used in this test as are used in the low-pass filter test. Please see the footnote of table ?? for details on the test settings.

☐./images/HPF response".JPG

Figure 3: Attempt 2 - High-Pass Filter Impulse Response (Closeup)

See the footnote of table ?? for details on the test settings, such as pulse width and voltage.

\_"./images/HPF zoomout".JPG

Figure 4: Attempt 2 - High-Pass Filter Impulse Response (Zoomout)

See the footnote of table ?? for details on the test settings, such as pulse width and voltage.

Resistor R is  $10k\Omega$ . Capacitor C is 1nF. Frequency is set to 10kHz. Pulse height is 20V. Pulse width is  $2\mu s$ . Measurements follow the same convention as table ??, namely whether they are  $1\tau$  or higher measurements.

Acquiring measurements for the high-pass filter is difficult. The frequency should be decreased by a factor of 2. This allows the capacitor to take more time to discharge through the resistor so that  $\tau$  measurements can be taken more easily. However, the peak value of the resistor's voltage drop must also increase in magnitude in order for the decay to observable. So, the pulse width should be increased by a factor of 2 to give the capacitor more time to charge, the resistor more current, and therefore more voltage, when the capacitor discharges. The impulse response is essentially as expected once the tweaks to the power supply settings are made. The sudden charging of the capacitor at the start demands a large current flowing through the resistor. This gives rise to a high voltage drop, explaining the Dirac delta term in equation (??). When the supply's pulse ends, the capacitor discharges through the resistor. Thus, the current, and therefore the voltage drop over the resistor, flips polarity, which is why the resistor's voltage drop becomes negative. As the capacitor discharges, less and less current (in terms of magnitude) flows. Thus, the magnitude of the voltage drop decreases, which explains the exponential curve. The same trend in percentage errors is observed in the high-pass filter. Like with the low-pass filter, the decreasing trend in percentage errors indicates that the accuracy of the experiment is limited by the accuracy of  $\tau$  measurements. For an accurate measurement of the high-pass filter, a higher voltage, lower pulse frequency, and wider pulse width are likely necessary, so a  $5\tau$  measurement or so can be taken.