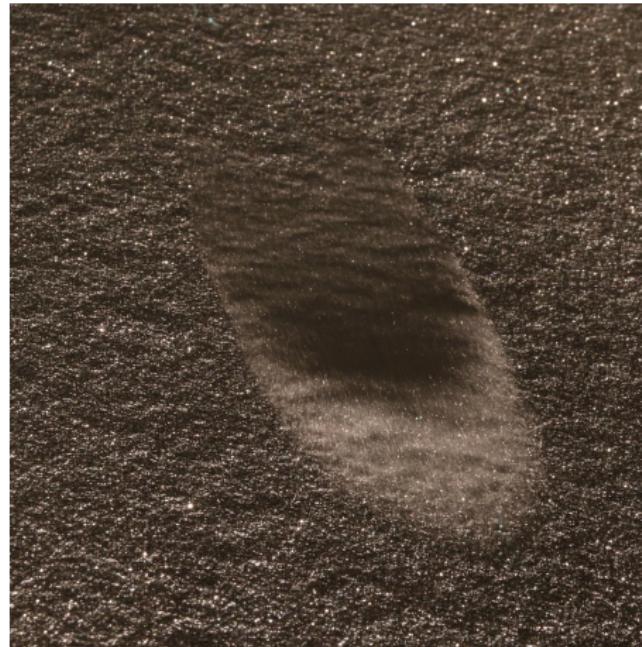


GRANULAR AVALANCHES: RELEASE OF A FINITE MASS ON A ROUGH INCLINED PLANE

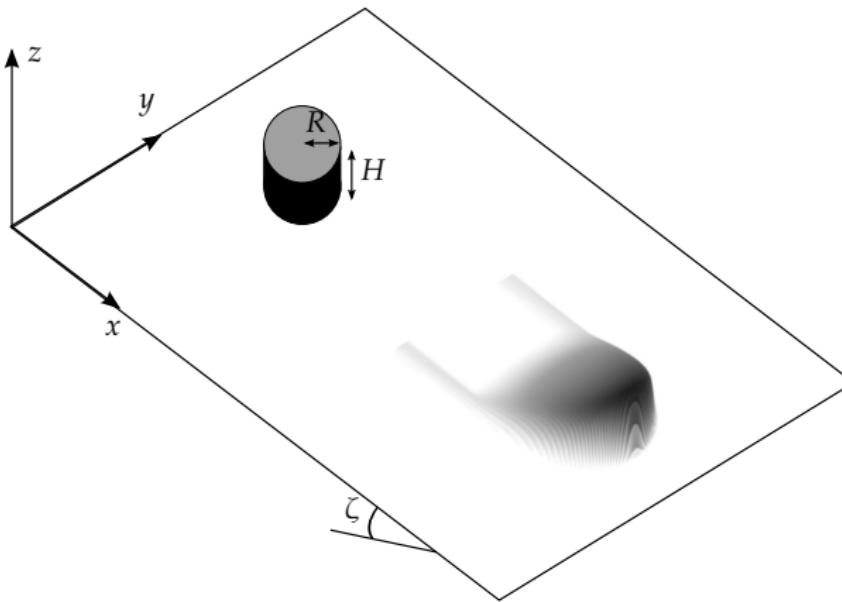


Andrew Edwards (DAMTP)

Experiments: Dr. Sylvain Viroulet, PI: Prof. Nico Gray (University of Manchester)

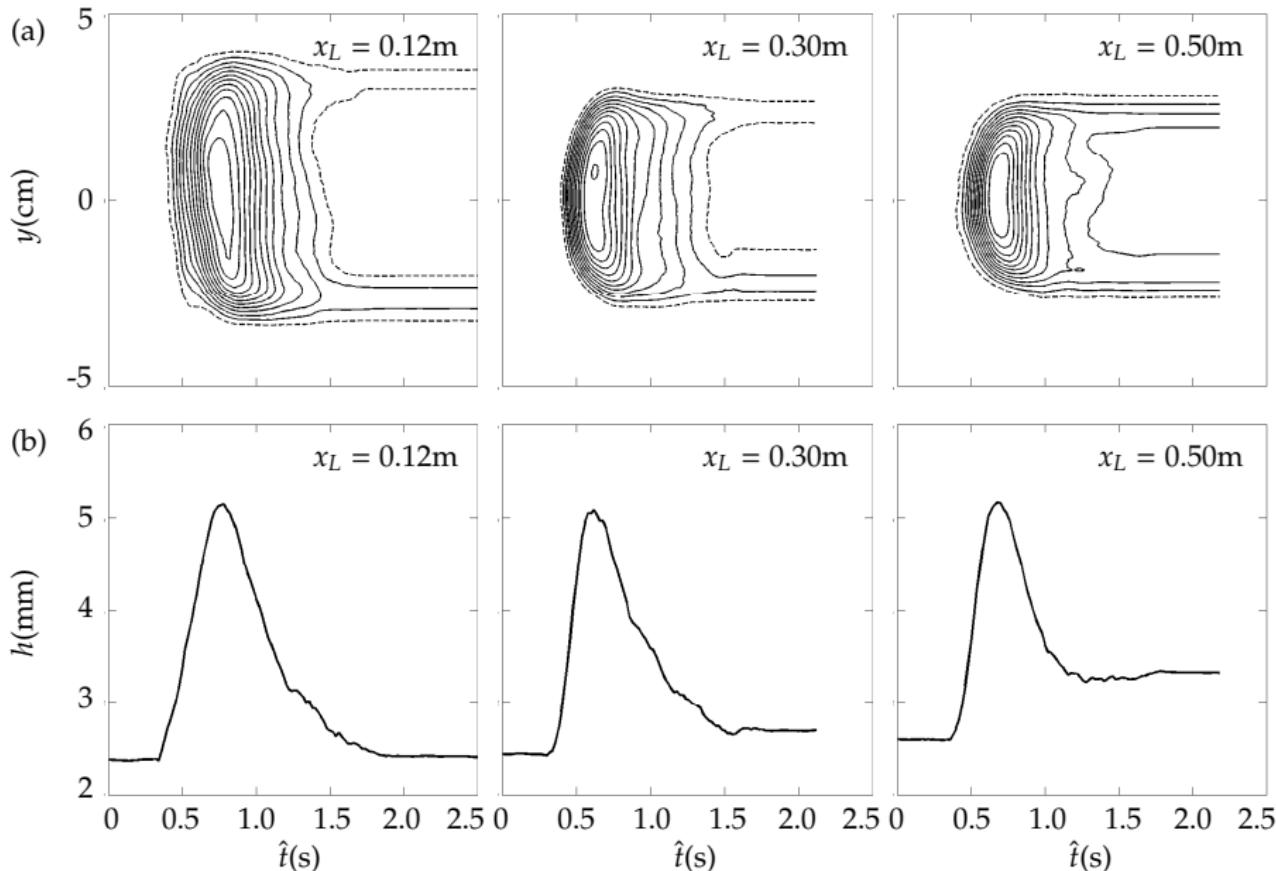
8th May 2015

EXPERIMENTAL SETUP

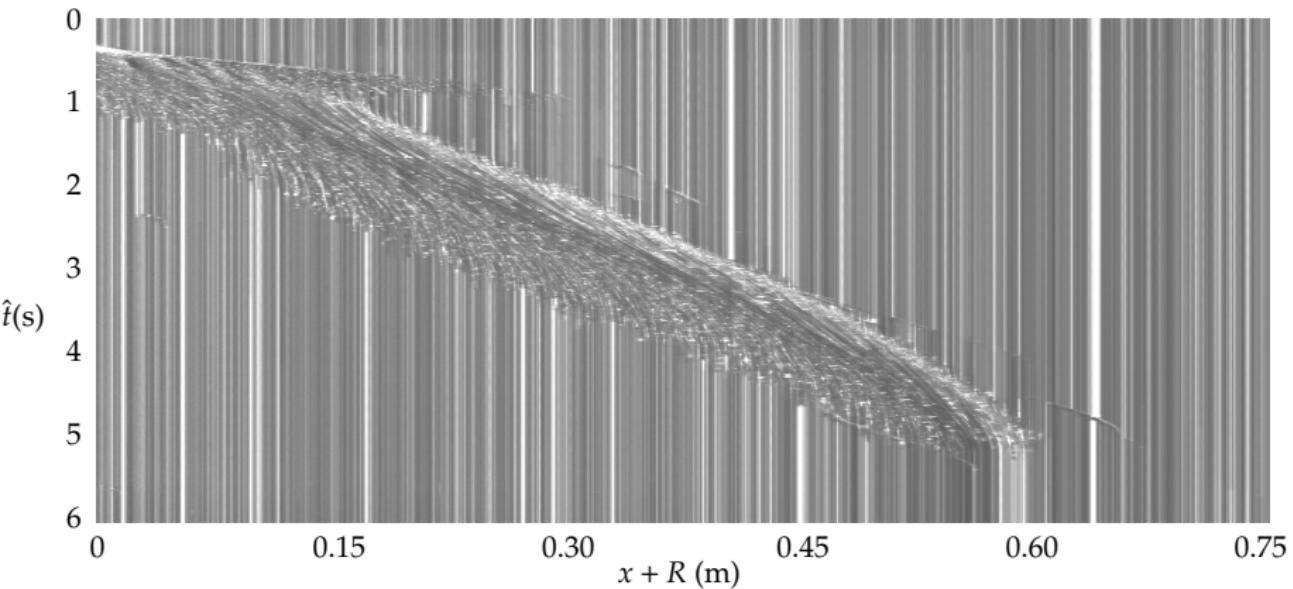


- Release of cylindricial mass ($R = 1.4\text{cm}$, $H = 1.8\text{cm}$) of $280 - 350\mu\text{m}$ diameter carborundum particles on a static erodible layer of the same material
- Rough bed of attached $750 - 1000\mu\text{m}$ diameter spherical glass beads

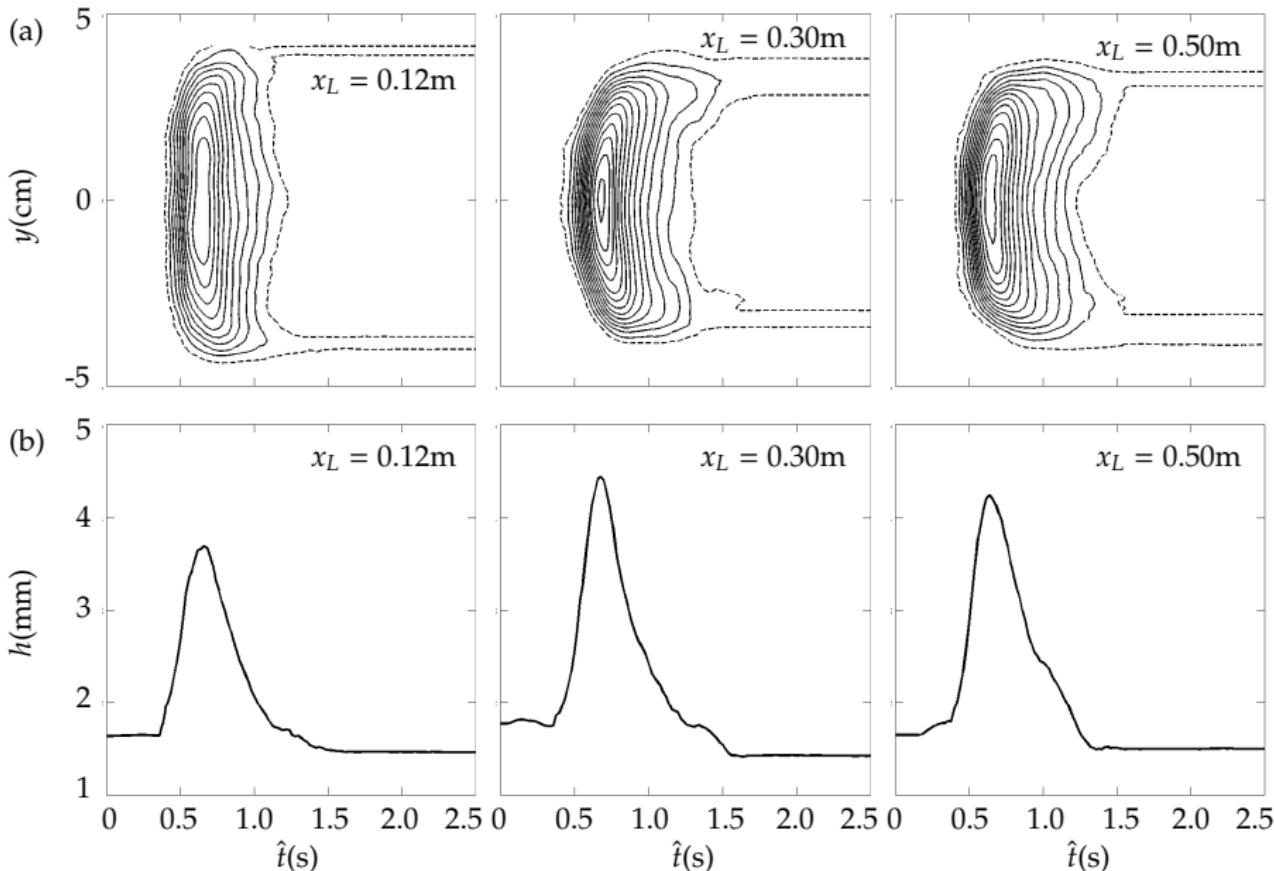
EXPERIMENTAL OBSERVATIONS FOR $\zeta = 34.0^\circ$



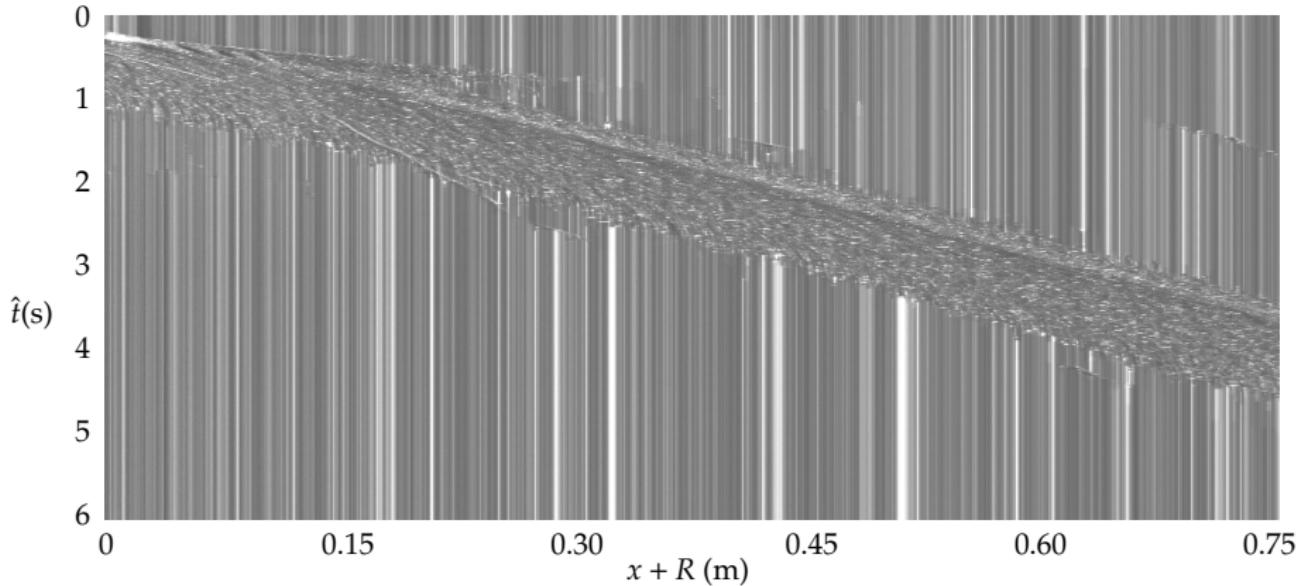
EXPERIMENTAL OBSERVATIONS FOR $\zeta = 34.0^\circ$



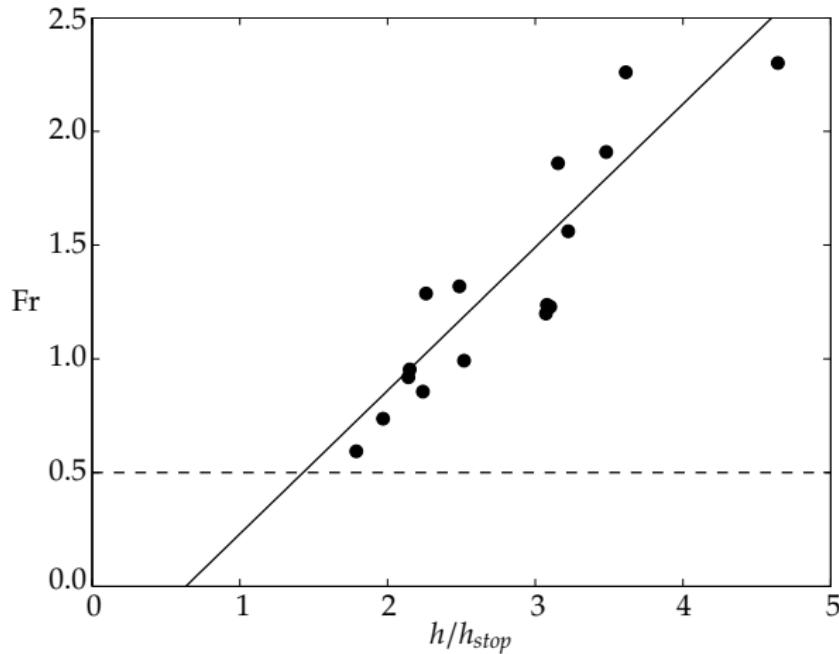
EXPERIMENTAL OBSERVATIONS FOR $\zeta = 35.2^\circ$



EXPERIMENTAL OBSERVATIONS FOR $\zeta = 35.2^\circ$

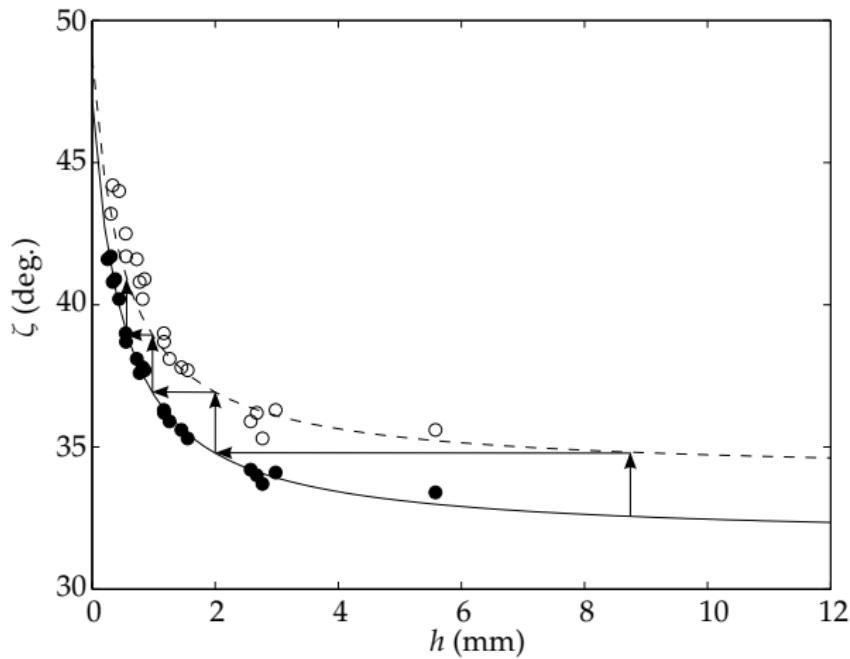


BASAL FRICTION LAW



- Steady uniform flow rule: $Fr = \frac{\bar{u}}{\sqrt{hg \cos \zeta}} = \beta \frac{h}{h_{stop}(\zeta)} - \Gamma$
- Here $\beta = 0.63$, $\Gamma = 0.40$ and $\alpha = 0.5$ (unsteady cut-off)
- Spherical glass beads: $\beta = 0.136$, $\Gamma = 0$
Sand: $\beta = 0.65$, $\Gamma = 0.77$ (Pouliquen & Forterre 2002)

BASAL FRICTION LAW



- Critical slope angle functions:

$$\tan \zeta_{stop,start} = \tan \zeta_{1,3} + \frac{\tan \zeta_2 - \tan \zeta_1}{1 + h/\mathcal{L}}$$

- $\zeta_1 = 31.7^\circ$, $\zeta_2 = 47.2^\circ$, $\zeta_3 = 34.0^\circ$, $\mathcal{L} = 0.39\text{mm}$

BASAL FRICTION LAW

- $\mu(h, \text{Fr}) =$

$$\begin{cases} \mu_1 + \frac{\mu_2 - \mu_1}{1 + h\beta/\mathcal{L}(\text{Fr} + \Gamma)} & \text{Fr} \geq \alpha \\ \left(\frac{\text{Fr}}{\alpha}\right)^k \left(\mu_1 + \frac{\mu_2 - \mu_1}{1 + h\beta/\mathcal{L}(\alpha + \Gamma)} - \mu_3 - \frac{\mu_2 - \mu_1}{1 + h/\mathcal{L}} \right) + \mu_3 + \frac{\mu_2 - \mu_1}{1 + h/\mathcal{L}} & 0 < \text{Fr} \leq \alpha \\ \mu_3 + \frac{\mu_2 - \mu_1}{1 + h/\mathcal{L}} & \text{Fr} = 0 \end{cases}$$

where $\mu_i = \tan \zeta_i$ ($i = 1 \dots 3$)

- Deposit layer thickness $h = h_{stop}$ when $\text{Fr} = \beta - \Gamma \geq \alpha \Rightarrow$

$$h_{stop}(\zeta) = \mathcal{L} \left(\frac{\tan \zeta_2 - \tan \zeta_1}{\tan \zeta - \tan \zeta_1} - 1 \right)$$

- $h_{stop}(34.0^\circ) = 2.778\text{mm}$, $h_{stop}(35.2^\circ) = 1.663\text{mm}$

2D GOVERNING EQUATIONS

- Mass and momentum balance:

$$\frac{\partial h}{\partial t} + \frac{\partial}{\partial x} (h\bar{u}) + \frac{\partial}{\partial y} (h\bar{v}) = 0,$$

$$\frac{\partial}{\partial t} (h\bar{u}) + \frac{\partial}{\partial x} (h\bar{u}^2) + \frac{\partial}{\partial y} (h\bar{u}\bar{v}) + \frac{\partial}{\partial x} \left(\frac{1}{2} h^2 g \cos \zeta \right) = hgS_x + \frac{\partial}{\partial x} \left(\nu h^{3/2} D_x \right),$$

$$\frac{\partial}{\partial t} (h\bar{v}) + \frac{\partial}{\partial x} (h\bar{u}\bar{v}) + \frac{\partial}{\partial y} (h\bar{v}^2) + \frac{\partial}{\partial y} \left(\frac{1}{2} h^2 g \cos \zeta \right) = hgS_y + \frac{\partial}{\partial y} \left(\nu h^{3/2} D_y \right),$$

- Source terms:

$$S^x = \sin \zeta - \mu \frac{\bar{u}}{|\bar{u}|} \cos \zeta,$$

$$S^y = - \mu \frac{\bar{v}}{|\bar{u}|} \cos \zeta,$$

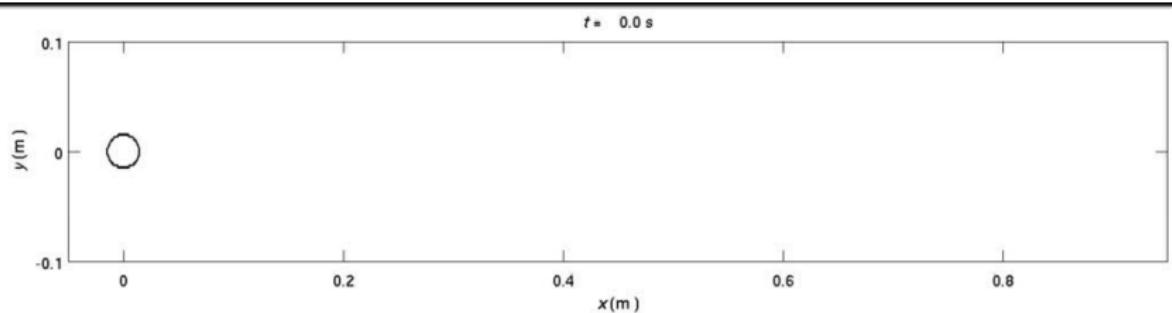
- Diffusive terms (see Gray & Edwards 2014)

$$D_x = \frac{\partial \bar{u}}{\partial x} + \frac{1}{2} \left(\frac{\partial \bar{v}}{\partial x} + \frac{\partial \bar{u}}{\partial y} \right),$$

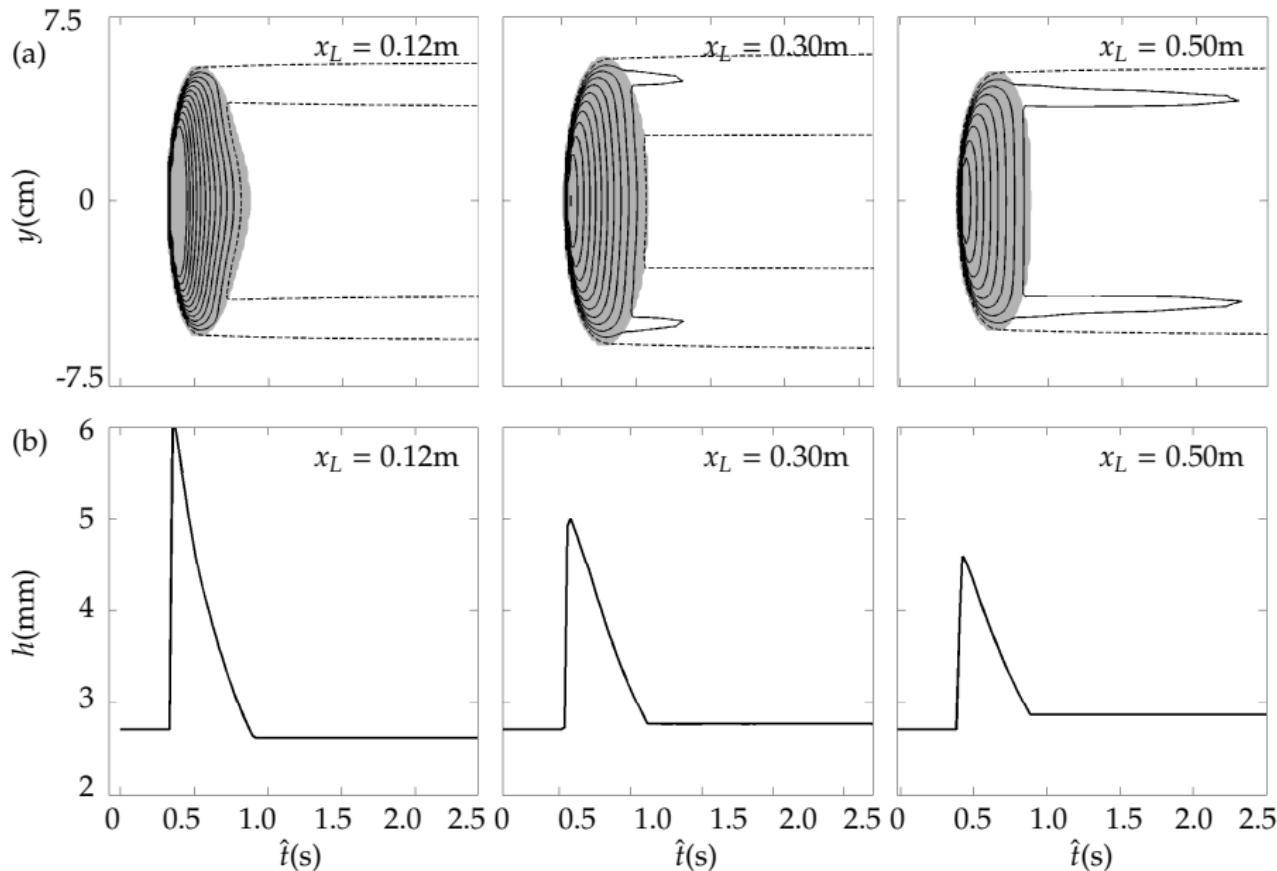
$$D_y = \frac{1}{2} \left(\frac{\partial \bar{u}}{\partial y} + \frac{\partial \bar{v}}{\partial x} \right) + \frac{\partial \bar{v}}{\partial y}.$$

NUMERICAL SIMULATIONS FOR $\zeta = 34.0^\circ$

- ICs: cylindrical cap $R = 1.4\text{cm}$, $H = 1.8\text{cm}$ on a stationary layer $h_0 = 2.7\text{mm} < h_{stop}$
- BCs: stationary layer $h_0 = 2.7\text{mm}$, $\bar{u} = \bar{v} = 0$ inflow on LHS, free outflow on RHS

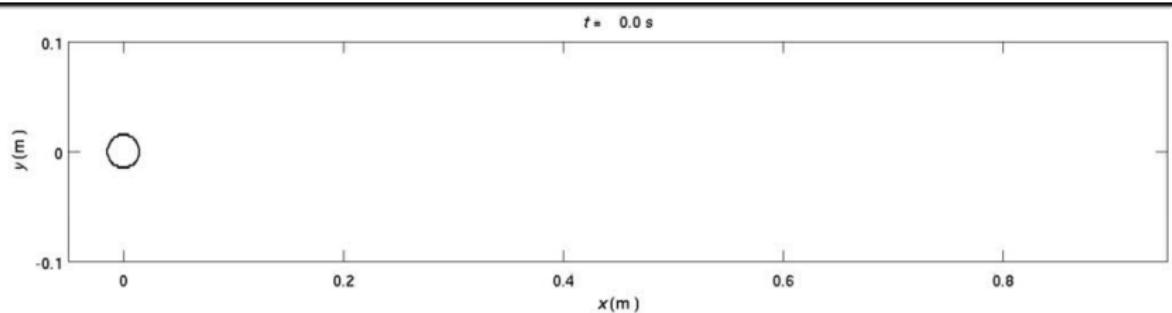


NUMERICAL SIMULATION FOR $\zeta = 34.0^\circ$

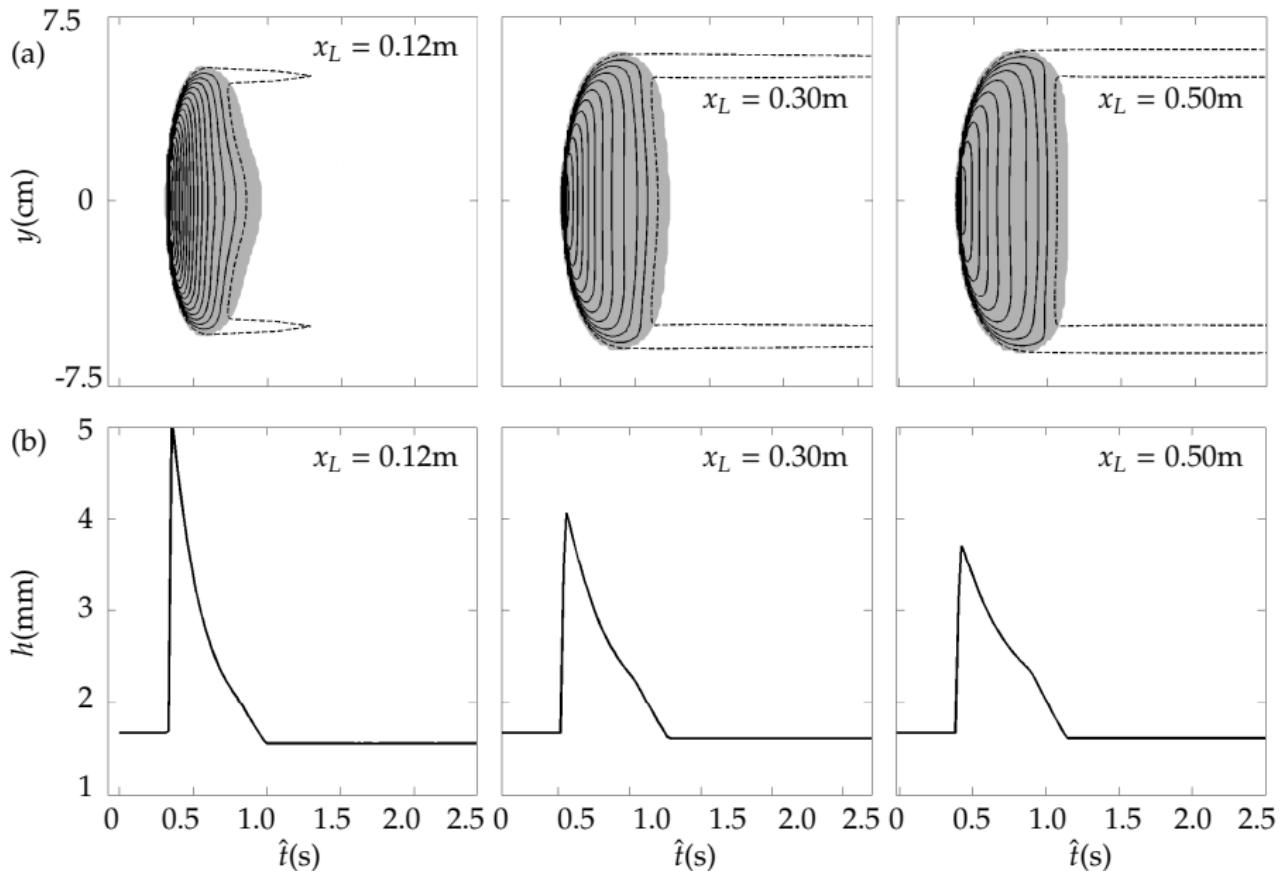


NUMERICAL SIMULATIONS FOR $\zeta = 35.2^\circ$

- ICs: cylindrical cap $R = 1.4\text{cm}$, $H = 1.8\text{cm}$ on a stationary layer $h_0 = 1.66\text{mm} < h_{stop}$
- BCs: stationary layer $h_0 = 1.66\text{mm}$, $\bar{u} = \bar{v} = 0$ inflow on LHS, free outflow on RHS



NUMERICAL SIMULATION FOR $\zeta = 35.2^\circ$



TRAVELLING-FRAME EQUATIONS

- Transform to coordinates (ξ, y, t) moving at wavespeed u_w by $\xi = x - u_w t$
- Mass and momentum balance:

$$\frac{\partial h}{\partial t} + \frac{\partial}{\partial \xi} (h(\bar{u} - u_w)) + \frac{\partial}{\partial y} (h\bar{v}) = 0,$$

$$\frac{\partial}{\partial t} (h\bar{u}) + \frac{\partial}{\partial \xi} (h\bar{u}(\bar{u} - u_w)) + \frac{\partial}{\partial y} (h\bar{u}\bar{v}) + \frac{\partial}{\partial \xi} \left(\frac{1}{2} h^2 g \cos \zeta \right) = hgS^\xi + D^\xi(\xi, y),$$

$$\frac{\partial}{\partial t} (h\bar{v}) + \frac{\partial}{\partial \xi} (h\bar{v}(\bar{u} - u_w)) + \frac{\partial}{\partial y} (h\bar{v}^2) + \frac{\partial}{\partial y} \left(\frac{1}{2} h^2 g \cos \zeta \right) = hgS^y + D^y(\xi, y),$$

- Source terms:

$$S^\xi = \sin \zeta - \mu \frac{\bar{u}}{|\bar{u}|} \cos \zeta,$$

$$S^y = - \mu \frac{\bar{v}}{|\bar{u}|} \cos \zeta,$$

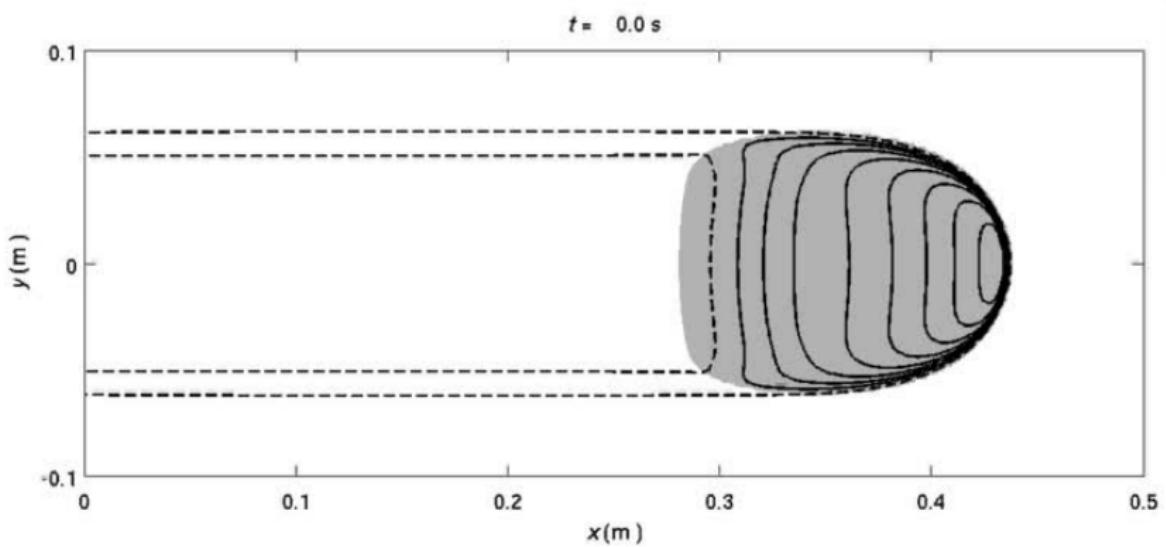
- Diffusive terms

$$D^\xi(\xi, y) = \frac{\partial}{\partial \xi} \left(\nu h^{3/2} \frac{\partial \bar{u}}{\partial \xi} \right) + \frac{\partial}{\partial y} \left(\frac{1}{2} \nu h^{3/2} \left(\frac{\partial \bar{v}}{\partial \xi} + \frac{\partial \bar{u}}{\partial y} \right) \right),$$

$$D^y(\xi, y) = \frac{\partial}{\partial \xi} \left(\frac{1}{2} \nu h^{3/2} \left(\frac{\partial \bar{u}}{\partial y} + \frac{\partial \bar{v}}{\partial \xi} \right) \right) + \frac{\partial}{\partial y} \left(\nu h^{3/2} \frac{\partial \bar{v}}{\partial y} \right).$$

TRAVELLING-FRAME SIMULATIONS

- $u_w = 0.21\text{ms}^{-1}$
- ICs: profile from $\zeta = 35.2^\circ$ simulation
- BCs: stationary layer $h_0 = 1.66\text{mm}$, $\bar{u} = \bar{v} = 0$ inflow on RHS, free outflow on LHS



THANK YOU FOR LISTENING

