9.1 Flux Linkage.

& B Re = pro I end = D I end = Ke.

Jobke + Sode + Sobe + Sobe + Sobe = noke

JEBRE + JABBE = MIKE.

= 0 B = Nok top sheet and B = hok bottom sheet

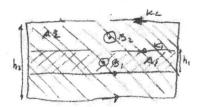
2.

h. I I A = h, w, I = ke, B = hok Mok

In=IL, DL = I In=I Bds = Le how (h. w)

4, = Mo h. w

 $e_i = -\frac{\text{No } h_i w}{\text{A}e} \frac{\partial J_i}{\partial t}$ 



B2 will be smaller than B1. Field due to inner duct is zero out side of it

$$A_{1} \Rightarrow \overline{I}_{m_{1}} \Rightarrow L_{1} = \frac{1}{I_{1}} \int_{S} B_{1} ds_{1} + \frac{1}{I_{2}} \int_{S} B_{2} ds_{1} = B_{1} = \frac{2 \mu_{0} K_{1}}{B_{2}}$$

$$= \frac{1}{\mu_{0}} \frac{\mu_{0} K_{1}}{E} (h_{1} w) + \frac{1}{\mu_{2}^{2}} \frac{\mu_{0} K_{2}}{E} (h_{1} w) = \frac{\mu_{0} h_{1} w}{E}$$

$$A_2 \Rightarrow \overline{\Phi}_2 \Rightarrow b_2 \Rightarrow b_2 \Rightarrow \frac{1}{I_2} \int_S B_2 ds_2 + \int_S B_3 ds_3 = \frac{1}{160} \frac{h_0 M_2}{2} (h_2 \omega) + \frac{1}{160} \frac{h_0 M_3}{2} (h_3 \omega) = \frac{1}{160} \frac{h_0 M_2}{2} (h_3 \omega) + \frac{1}{160} \frac{h_0 M_3}{2} (h_3 \omega) = \frac{1}{160} \frac{h_0 M_3}{2} (h_0 M_3) = \frac{1$$

4. 
$$h_1$$
 $h_2$ 
 $h_1$ 
 $h_2$ 
 $h_3$ 
 $h_4$ 
 $h_4$ 
 $h_5$ 
 $h_6$ 
 $h$ 

For 
$$\overline{D}_{m_{2}} \Rightarrow L_{2} = \frac{1}{I_{2}} \int_{S} B_{2} ds_{2} + \frac{1}{I_{1}} \int_{S} B_{1} ds_{1} - \frac{1}{I_{1}} \int_{S} B_{1} (ds_{3} - ds_{1}) = \frac{1}{I_{2}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) - \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) = \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) - \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) - \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) - \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) - \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) - \frac{1}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) - \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{10}} \left( h_{10} \, W \right) + \frac{I_{10}}{I_{10}} \int_{S} \frac{I_{10} \, W_{1}}{I_{1$$

$$\mathcal{E}_{2} = -\left[\frac{\mu_{0} \, \omega}{e} \left(h_{2} + h_{1}\right) \left(\frac{\partial I_{2}}{\partial t} + \frac{\partial I_{1}}{\partial t}\right) - \frac{1}{2} \frac{\mu_{0} \, \omega}{e} \left(h_{2} - h_{1}\right) \frac{\partial I_{1}}{\partial t}\right]$$

$$\mathcal{E}_{1} = -\frac{\mu_{0} \omega_{0}(h_{2} + h_{1})}{e} \frac{\partial I}{\partial t} + \frac{1}{2} \frac{\mu_{0} \omega_{0}(h_{2} - h_{1})}{e} \frac{\partial I}{\partial t}$$

$$E = -\left[\frac{\mu_0 \omega_1}{e} + \frac{\mu_0 \omega_2}{e} \left(h_2 + h_1\right)\right] \frac{\partial I}{\partial t} + \frac{1}{2} \frac{\mu_0 \omega_2}{e} \left(h_1 - h_1\right) \frac{\partial I}{\partial t} = -\left[\frac{\mu_0 \omega_2}{e} \left(2h_1 + h_2\right) \frac{\partial I}{\partial t} - \frac{1}{2} \frac{\mu_0 \omega_2}{e} \left(h_2 - h_1\right) \frac{\partial I}{\partial t}\right]$$

5. Fleet Curkage:

When arrent flows though a conclusion, it induces a singuetic faced wormed to the acreest direction, pollowing the might havel rule. This preasure the field can affect other conclusions a vicuity ward; creating a link, this link created by the majurate field of the original creatificanductor affects the second arount, changing the voltage, Implicatione, suggester fixed, and other permueters of the second arount/conductor (and one very). This flux linkage creates a mental pendictures coupling, that can be calculated using tarellay's taw, by integrating the suggester flux andred by the first conductor/ arount, due to the amend in that and what and with a mental for the area of the second conductor or arount.

I I using method of part 4. neglects the coupling between the two ducts.

9.2 Multiple Impeclances

In steady state, all replex hows

 $E_{0}^{+} \bigcirc P_{0} \qquad E_{1} \qquad E_{2} \qquad V_{0}^{+}$   $E_{0}^{+} \bigcirc P_{0} \qquad E_{1} \not \downarrow_{1} \qquad E_{2} \not \downarrow_{2}$   $E_{0} \not\downarrow_{1} \qquad E_{2} \not\downarrow_{2} \qquad E_{3} \not\downarrow_{2} \qquad E_{4} \not\downarrow_{2} \qquad E_{4} \not\downarrow_{3} \qquad E_{5} \not\downarrow_{4}$   $E_{0} \not\downarrow_{1} \qquad E_{1} \not\downarrow_{1} \qquad E_{2} \not\downarrow_{2} \qquad E_{3} \not\downarrow_{2} \qquad E_{4} \not\downarrow_{3} \qquad E_{5} \not\downarrow_{4} \qquad E_{5} \not\downarrow_{5} \qquad E_{5} \not\downarrow_$ 

Va(2) = V+ e-1 and + Vn e-1 pn = = = = = = = = = = = = = = = [Vn(2) = jut]

 $V_0^{\pm}$  is known and  $V_2^{\pm} = 0$ ; Find  $V_0(z)$ ,  $V_1^{\pm}(z)$ ,  $V_1^{\pm}(z)$  and  $V_2^{\pm}(z)$  $\beta_0 = \frac{\omega}{V_0} = \omega \sqrt{\epsilon_0 \mu_0}$ ;  $\beta_1 = \omega \sqrt{\epsilon_0 \mu_0}$ ,  $\beta_2 = \omega \sqrt{\epsilon_0 \mu_0}$ 

Vo(2) = V+ e-ipo = + Vo e i sot and p = 2, + 20 from 5.7(8)

=> Vo = Vo peise at == => Vo[2) = Vo p = V. ( ti - 20 ) eise =

V; = Vo 7. ev Biz =0 for 7 = 22, from 5.7 (9)

at == 1 Via)= Vo 7, e-1 A.Z

For  $V_1 = V_1^+(A) = V_0^+ T_0 \in \mathcal{B}_1 \Delta$  and  $P_0 = \frac{21-21}{21+20} \in \mathcal{B}_1 \in \mathcal{B}_2$ 

 $= \bigvee_{i=1}^{\infty} \widehat{V_{i}(z)} = \widehat{V_{o}}^{+} \left( \frac{2+i}{3+2i} \right) \left( \frac{32-3i}{32+2i} \right) e^{i\beta_{i}z}$ 

at == 0 =>  $\gamma = \frac{22a}{22+21}$  and at 2=0+1=0

 $= \int_{1}^{\sqrt{2}} (z) = \tilde{V}_{1}^{+} \gamma e^{i\beta_{2}(\Delta+1)} = \tilde{V}_{0}^{+} \left(\frac{2^{\frac{2}{2}i}}{2_{1}+2i}\right) \left(\frac{2^{\frac{2}{2}2}}{2_{2}+2i}\right) e^{i\beta_{2}z}$   $= \int_{1}^{\sqrt{2}} = 0$   $\tilde{V}_{1}^{+} = 0$ 

Recalculate Vo = Vo(0) + V, (0) 76 = Vo (21-20) e 100 + Vo (21-20) (22-21) (22-21) (21-20) e joit

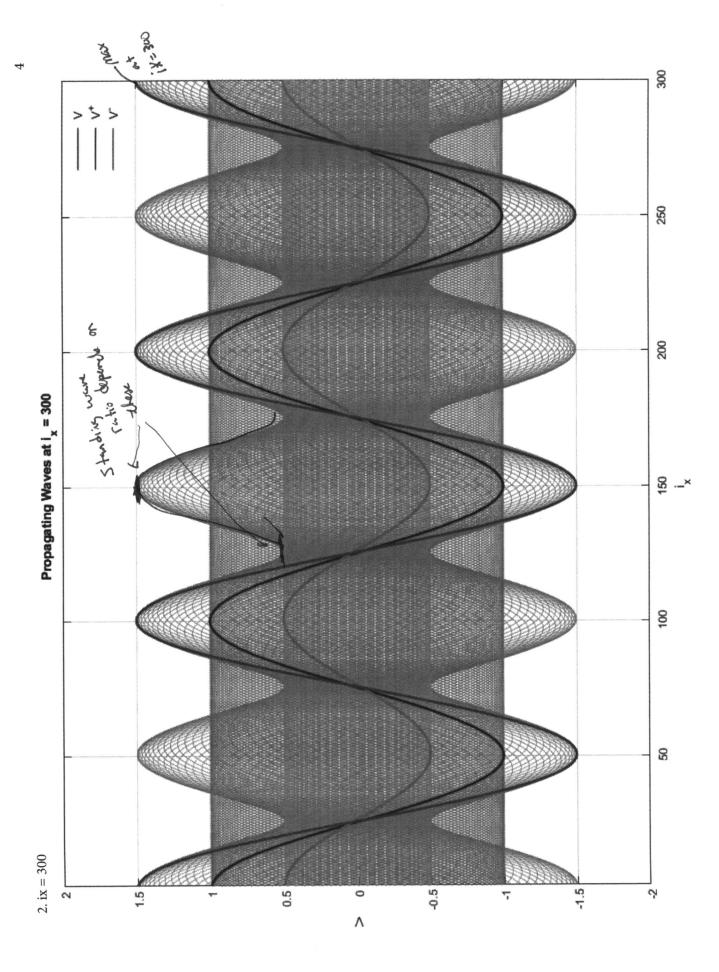
See solve for general procedure for steady state.

$$\frac{\sqrt[4]{\sqrt{6}}}{\sqrt[4]{\sqrt{6}}} = \frac{\sqrt[4]{\sqrt[4]{2}}}{\sqrt[4]{\sqrt{6}}} = \frac{\sqrt[4]{2}}{\sqrt[4]{\sqrt{6}}} = \frac{\sqrt[4]{2}}{\sqrt{6}} = \frac{\sqrt[4]{2}}{\sqrt{6}}$$

$$= \frac{2_{1}-2_{0}}{2_{1}+2_{0}} = \frac{2_{1}B_{0}2}{+\left(\frac{22_{1}}{2_{1}+2_{0}}\right)\left(\frac{2_{2}-2_{1}}{2_{2}+2_{1}}\right)\left(\frac{22_{1}}{2_{1}-2_{0}}\right)} = \frac{12(B_{0}+B_{1})}{2_{1}-2_{0}} = \frac{12($$

$$\frac{\widehat{V}_{1}(2)}{\widehat{V}_{1}^{+}(2)} = \frac{\widehat{V}_{0}^{+}\left(\frac{2\cdot 2}{2i+2i}\right)\left(\frac{32-2i}{22+2i}\right)e^{-i\beta_{1}\cdot 2}}{\widehat{V}_{0}^{+}\left(\frac{2\cdot 2}{2i+2i}\right)e^{-i\beta_{1}\cdot 2}} = \left(\frac{22-2i}{22+2i}\right)e^{-2i\beta_{1}\cdot 2} = \rho_{1}e^{-2i\beta_{1}\cdot 2}$$

ž



9.2.2 •  $V(z,t) = V^{+}[co(\omega t - Bz) + p co(\omega t + Bz)]$ 1.  $V(z,t) = A co \omega t co Bz + B sm \omega t sm Bz = D find A and B$ 

V+ Cos(wt-Bz) = V+ Cos wt cos Bz + V+ sin wt supt V+ Cos (wt+Bz) = V+p cos wt cos Bz - V+ sun wt sup BE.

V(e,t) = V+ cos(wt- p2) + Vp as(wt + p2) =
= U+ cos wt cosp2 + V+ sum wt sumpt + V+p cos wt cosp2 - Vp sum wt sumpt = 0

=  $V^+(1+p)$  con ut con  $\beta = + V^+(1-p)$  sun ut sun  $\beta = -5$  $A = V^+(1+p)$  and  $B = V^+(1-p) = -5$ 

= 1 A wo wt con Be + B smut sur BE

.. this is origin of the term Standing wave ratio. 4. From The plot, and as defore in 3.

$$1P1 = \frac{s-1}{s+1} = 0.5$$

however, with ix=550, Op his changed, and Vinin is at ix=500 or . (0.51), tweefore

which seems about 180° difference.

Note also that at ix = 300 vswR envelope
is at a minimum. In previous plot, i't was at maximum.

is at a minimum. In previous plot, i't was at maximum.

is at a minimum. In previous plot, i't was at maximum.

Shifts VswR from max to min.

3. By ploting a V = 1/2 traveling to the left, we are replicating.

The reflected wave at ix = 300. When we add V+=1 and V=0.5

We can observe the V wax = 1.5 and V min = 0.5 conted in

that ware ( there is my plot ). From this V max and V min, we

can obtain the Voltge wave Shoulding Ratio ( V SWR ) by

L'hewite we could Obtain the against of the reflection confront p

$$1p1 = \frac{s-1}{s+1} = \frac{2}{4} = 0.5$$

However, just from the plat is different to calculate 8p. to obtain policies, but an attent looking at Vinin from ix=300 looks like at ix= 275, or (0.251) and

This confines the lack of phase difference in V+ and V- accross the plot, and:

$$p = |p| = \frac{1}{2}$$