

## 11.2. Final Part II

Used the function created in the last problem (11.1.4) to calculate and return the values of  $Z_k$ ,  $V_k$ , and  $I_k$ . As we know from HW 9.2.1, to obtain  $V_k(z, t)$  from  $\tilde{V}_k(z)$ , we use:

$$\tilde{V}_k(z, t) = \text{Re} [\tilde{V}_k(z) e^{j\omega t}], \text{ so apply this to our } \tilde{V}_k \text{ and } \tilde{I}_k$$

we obtain:

$$V_k(t) = \text{Re} [\tilde{V}_k e^{j\omega t}] \quad \text{and} \quad I_k(t) = \text{Re} [\tilde{I}_k e^{j\omega t}]$$

In the HW, you reference, the subscript was a segment of a transmission line with the same characteristic impedance. Here the subscript is a differential element on a transmission line. You need to relate  $z$  to the  $k$  in this problem.

Final\_Part-II\_code.m executes this code in part of the program.

1. Plotting  $V_k(t)$  at  $t=0$  in Final\_Part-II\_Figure-1.pdf, we see that at  $t=0$ ,  $V_k(t)$  and  $I_k(t)$  follow  $V_k$  and  $I_k$  exactly, as at  $t=0$ , the  $\cos(\omega t) = 1$ . In addition, in the third subplot of Figure-1, we compare  $Z_k$  with  $\frac{V_k(t)}{I_k(t)}$ , and see that both match very well.

Figure-1 presents the solution for  $Z_L = \sqrt{L/C}$  for a matched impedance, as  $Z_0 = \sqrt{L/C}$  as  $\Delta Z \neq 0$ . For the transmission line, and the amplitude of the waves do not see any reflection.

In Figure-2, the load impedance was changed to  $Z_L = 5 \times \sqrt{L/C}$  to represent a mismatch in impedance, where we see that the amplitude of  $V_k$  and  $V_k(t)$  has increase to account for the forward and reflected waves. In this case, we also see that  $V_k(t)$ ,  $I_k(t)$ , and  $Z_k(t)$  follow their counterparts  $V_k$ ,  $I_k$  and  $Z_k$

Could compute VSWR and compare with expected for continuous

2. For  $t = (2\pi/\omega)/4$ , the  $\cos(\omega t) = 0$  as the  $\omega$  cancel, and the cosine function is evaluated at  $\frac{2\pi}{4}$  or  $90^\circ$ . In this case, as we can see in Figure-3,  $V_k(t)$  is out of phase with  $V_k$  the corresponding  $90^\circ$ , and the wave starts propagating at  $N=0$  with a value of 0. The current plot follows similar pattern, and  $Z_k$  and  $Z_k(t)$  still matches. In Figure-4,  $Z_L$  was changed to create a mismatch ( $Z_L = 5 * \sqrt{L/C}$ ) with the transmission line. Same as in Figure-2, the amplitude of  $V_k(t)$  and  $I_k(t)$  has changed to incorporate the reflected wave. It is of interest to note (same as in Figure-2) that the impedance of the Transmission line drops to almost 0 for most of the Transmission line, except at values of  $\frac{1}{2}$  from  $Z_0$ , where the source sees  $Z_L$  at this point (as it should) with  $N = 372$  in our case.

Good observation.

### Discrete vs exact solution

1. for  $Z_L = \sqrt{L/C}$  and  $Z_0 = \sqrt{L/C}$ , as the characteristic impedance of the transmission line used for the exact solution.

Figures 5 and 6 show the discrete  $V_k(t)$ ,  $I_k(t)$  and  $Z_k$  vs

The exact  $V_z(t)$ ,  $I_z(t)$  and  $Z(t) = \frac{V_z(t)}{I_z(t)}$  for  $t=0$  and

$t = (\frac{2\pi}{\omega})/4$ . In these figures we can observe how well the discrete solution matches the exact solution when  $Z_L$  is matched to the transmission line impedance  $Z_0 = \sqrt{L/C}$ .



2. For  $Z_L \neq \sqrt{L/C}$  in our case  $Z_L = 5 + \sqrt{L/C}$  we can observe in Figure 7 for  $t=0$  that  $I_k(t)$  and  $I_z(t)$  matched quite well, but  $V_z(t)$  deviates from  $V_k(t)$  significantly. By contrast in Figure 8, when  $t = \left(\frac{2\pi}{\omega}\right)/4$ ,  $V_z(t)$  follows  $V_k(t)$ , while  $I_z(t)$  deviates from  $I_k(t)$ .

This may be due to the impedance of the exact transmission line fixed at  $Z_0 = \sqrt{L/C}$ , that we can see in both figures that it remains at  $1\Omega$ , instead of being close to 0 and only seen  $5\Omega$  at  $\frac{d}{2}$ .

The issue here is that  $V_k$  will never change.  $V_k(t) = \text{Re}(V^k e^{j\omega t})$  where  $V^k$  is the complex voltage amplitudes. If you animate this, you will see  $V_k(t)$  is the  $V^k$  wave moving to the right.

Both Figures, however, show an increase in voltage and current amplitude due to the reflected wave.

Of interest is to observe Figures 10, 11 and 12, where the exact calculation was done to allow the impedance of the transmission line to change for each LC combination. In figure 10, we can see that the exact calculation of  $V_z(t)$  and  $I_z(t)$  change "frequency" as it progresses through the transmission line, referring to the velocity propagation of the wave changing at each  $Z_k$  stage. As we discussed in the piazza discussion of problem 10.2 about the change in the propagation velocity changing the wavelength, and the wave seems to compress as it travels along the transmission line. Figures 11 and 12 show the result of this with an impedance mismatch, at  $t=0$  and  $t = \left(\frac{2\pi}{\omega}\right)/4$ .

In the cases shown in Figs 10, 11 and 12, The impedance of the exact solution  $z(t) = \frac{V_2(t)}{I_2(t)}$  matches the impedance of

$z_k$  and  $\frac{V_k(t)}{I_k(t)}$ , even though the currents and voltages

of both the exact and discrete approximation deviate from each other as  $N$  increases.

3. In the plots of Figure 9, we can observe how the error between  $V_k(t)$  and  $V_z(t)$  decreases when changing  $w$  from 0.1 to 0.01 and 0.001.

Good comparison