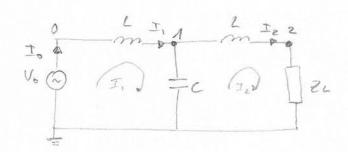


11.1 Part I



11.1.1. Apply Kirchhoff arrant and vollage law:

Voltage aroud each loop:

Istluop: 
$$\widetilde{V}_{0} - 2\frac{d\widetilde{I}_{1}}{dt} - \frac{1}{c}\int_{C\widetilde{I}_{1}}(\widetilde{I}_{1}-\widetilde{I}_{2})dt = 0 = 0$$
 for  $\frac{1}{c}\int_{C\widetilde{I}_{1}}(\widetilde{I}_{1}-\widetilde{I}_{2})dt = \widetilde{V}_{1}$ 

$$\widetilde{V}_{0} - 2\frac{d\widetilde{I}_{1}}{dt} - \widetilde{V}_{1} = 0 \quad \text{replacing} \quad \frac{d}{dt} \quad \text{with } j\omega = 0$$

$$\widetilde{V}_{0} - j\omega 2\widetilde{I}_{1} - \widetilde{V}_{1} = 0 = 0 \quad \widetilde{V}_{1} = \widetilde{V}_{0} - j\omega 2\widetilde{I}_{1}, \quad V$$

2nd loop: 
$$-\frac{1}{C}\int (\widetilde{I}_2 - \widetilde{I}_1)dt - L \frac{d\widetilde{I}_2}{dt} - \widetilde{I}_2 \tilde{E}_L = 0$$

$$\operatorname{Rer} \int \int (\widetilde{I}_2 - \widetilde{I}_1) dt = -V, \text{ and } \widetilde{I}_2 \tilde{E}_L = \widetilde{V}_2$$

$$\widetilde{V}_1 - L \frac{d\widetilde{J}_2}{dt} - \widetilde{V}^2 = 0 \text{ replacing } \frac{d}{dt} \text{ with } \widetilde{J}_0 \omega$$

$$\widetilde{V}_2 = \widetilde{V}_1 - \widetilde{J}_1 \omega L\widetilde{I}_2 \omega$$

current at each Nock: O is not a node.

Mode 1? 
$$\frac{1}{2}\int (\widetilde{V}_1-\widetilde{V}_0)\,dt + \frac{1}{2}\int (\widetilde{V}_1-\widetilde{V}_2)dt + C\frac{d\widetilde{V}_1}{ct\epsilon} = 0 = D-\widetilde{J}_1+\widetilde{J}_2+C\frac{d\widetilde{V}_1}{c\epsilon\epsilon} = 0$$

= D replacing d with jw = b Iz = I, - jweV, V

Node 2: 
$$\frac{1}{2} \left( \widetilde{J}_2 - \widetilde{J}_1 \right) dt + \frac{\widetilde{V}_2}{2L} = 0 = D - \widetilde{I}_2 + \frac{\widetilde{V}_2}{2L} = 0$$

$$-\widetilde{I}_2$$

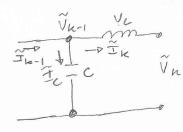
$$\widetilde{I}_2 = \frac{\widetilde{V}_2}{2L}$$

11.1.2 = D 
$$V_0 = V_0$$
 and  $T_1 = \frac{V_0}{20}$  with  $T_1 = T_0$ 

$$V_0 = V_0$$

11.1.3

$$\begin{split} \widetilde{J}_{k} &= J_{k-1} - j\omega C \widetilde{V}_{k-1} \quad \text{and} \quad \widetilde{J}_{k} &= \widetilde{V}_{k-1} - j\omega L \widetilde{J}_{k} \\ \widetilde{J}_{2} &= \widetilde{J}_{1} - j\omega C \widetilde{V}_{1} \quad \text{and} \quad \widetilde{V}_{2} &= \widetilde{V}_{1} - j\omega L \widetilde{J}_{2} \\ \widetilde{J}_{1} &= \widetilde{J}_{0} - j\omega d \widetilde{V}_{0} \quad \text{and} \quad \widetilde{V}_{1} &= \widetilde{J}_{0} - j\omega L \widetilde{J}_{1} \\ \widetilde{J}_{1} &= \widetilde{J}_{0} \quad 0 \end{split}$$



VK = VK-, - jwl Ik is obvious, as VK will be equal to Vk-, mims the voltage drop in the inductor L denoted by Vi = jwl Ik Likewise,  $\tilde{I}_{k}$  is the total current among at the mode  $\tilde{I}_{k-1}$  mins the current drawn by the capacitor  $\tilde{I}_{c} = \tilde{J}_{w} \subset \tilde{V}_{k-1}$ 

Therefore the generalititation is corret:

Ik = Ik-1 - jwc Tk-1 and Tk = Jk-1 - jw LIk V

In turne domain with a Ze matched impedance, and no reflecting ware:

 $\tilde{V}_{o}(t) = V_{o} \cos \omega t = V_{o} e^{j\omega t}$  and  $\tilde{J}_{o}(t) = \frac{\tilde{V}_{o}(t)}{z_{o}}$ 

 $\widetilde{V}_{i}(t) = \widetilde{V}_{o}(t) - L \frac{d\widetilde{I}_{i}(t)}{dt}$  and  $\widetilde{I}_{i}(t) = \widetilde{I}_{o}(t) - e \frac{dV_{i}(t)}{dt}$ 

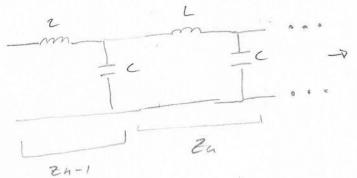
 $V_2(t) = \widehat{V}_1(t) - L \frac{dI_2(t)}{dt}$  and  $I_2(t) = \overline{I}_1(t) - c \frac{dV_2(t)}{dt}$ 

 $V_{k}(t) = V_{k-1}(t) - L \stackrel{\frown}{cl} I_{k}(t)$ 

 $\widetilde{I}_{k}(t) = \widetilde{I}_{k-1}(t) - c \frac{d V_{k}(t)}{dt}$ 

11.1.4





$$\frac{2n-1}{2n+\frac{1}{j\omega c}} + j\omega L \qquad For \ Z_N = Z_L, \ Z_n = Z_N + j\omega L$$

$$\frac{N-1}{\sqrt{2n}} = \frac{N}{\sqrt{2n}} = \frac{N}{\sqrt{2n}}$$

$$= \frac{z_n + j\omega L}{z_n j\omega C + j\omega C j\omega L + 1} = 0$$

and to = j w2 + 21

2. 
$$\widehat{J}_{k} = \widehat{J}_{k-1} - j \omega C \widehat{V}_{k-1}$$
 for  $k = 0, 1, ..., N$  and  $\widehat{I}_{i} = \frac{\widehat{J}_{o}}{20}$