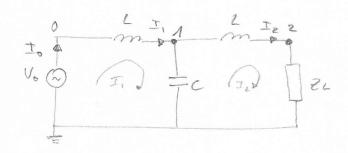


11.1 Part I



11.1.1. Apply Kirchhoff aurant and vollage law:

Voltage around each loop:

Ist loop:
$$\tilde{V}_0 - 2\frac{d\tilde{I}_1}{dt} - \frac{1}{c} \int (\tilde{I}_1 - \tilde{I}_2) dt = 0$$
 = D for $\frac{1}{c} \int c\tilde{I}_1 - \tilde{I}_2 dt = \tilde{V}_1$

$$\tilde{V}_0 - 2\frac{d\tilde{I}_1}{dt} - \tilde{V}_1 = 0$$
 replacing $\frac{d}{dt}$ with $j\omega = D$

$$\tilde{V}_0 - j\omega L\tilde{I}_1 - \tilde{V}_1 = 0 = D$$

$$\tilde{V}_0 - j\omega L\tilde{I}_1 - \tilde{V}_1 = 0 = D$$

$$\tilde{V}_1 = \tilde{V}_0 - j\omega L\tilde{I}_1, \quad V$$

2nd loop:
$$-\frac{1}{C}\int (\widetilde{J}_{2}-\widetilde{J}_{1})dt - L \frac{d\widetilde{J}_{2}}{dt} - \widetilde{J}_{2}ZL = 0$$

$$\operatorname{Rer} \frac{1}{C}\int (\widetilde{J}_{2}-\widetilde{J}_{1}) dt = -V, \text{ and } \widetilde{J}_{2}ZL = \widetilde{V}_{2}$$

$$\widetilde{V}_{1} - L \frac{d\widetilde{J}_{2}}{dt} - \widetilde{V}^{2} = 0 \text{ replacing } \frac{d}{dt} \text{ with } j\omega$$

$$\widetilde{V}_{2} = \widetilde{V}_{1} - j\omega L\widetilde{J}_{2}V$$

current at each Noce: O is not a mode.

Mode 1?
$$\frac{1}{L}\int (\widetilde{V}_1-\widetilde{V}_0) dt + \frac{1}{L}\int (\widetilde{V}_1-\widetilde{V}_2) dt + C\frac{d\widetilde{V}_1}{ct} = 0 = D-\widetilde{J}_1 + \widetilde{J}_2 + C\frac{d\widetilde{V}_1}{ct} = 0$$

= D replacing d with jw = D Iz = I, - jweV, V

Node 2:
$$\frac{1}{2} \left(\widetilde{J}_2 - \widetilde{J}_1 \right) dt + \frac{\widetilde{V}_2}{2L} = 0 = D - \widetilde{I}_2 + \frac{\widetilde{V}_2}{2L} = 0$$

$$-\widetilde{I}_2$$

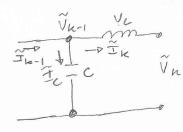
$$\widetilde{I}_2 = \frac{\widetilde{V}_2}{2L}$$

11.1.2 = D
$$V_0 = V_0$$
 and $T_1 = \frac{V_0}{20}$ with $T_1 = T_0$

$$V_0 = V_0$$

11.1.3

$$\begin{split} \widetilde{J}_{k} &= J_{k-1} - j\omega C \widetilde{V}_{k-1} \quad \text{and} \quad \widetilde{J}_{k} &= \widetilde{V}_{k-1} - j\omega L \widetilde{J}_{k} \\ \widetilde{J}_{2} &= \widetilde{J}_{1} - j\omega C \widetilde{V}_{1} \quad \text{and} \quad \widetilde{V}_{2} &= \widetilde{V}_{1} - j\omega L \widetilde{J}_{2} \\ \widetilde{J}_{1} &= \widetilde{J}_{0} - j\omega d \widetilde{V}_{0} \quad \text{and} \quad \widetilde{V}_{1} &= \widetilde{J}_{0} - j\omega L \widetilde{J}_{1} \\ \widetilde{J}_{1} &= \widetilde{J}_{0} \quad 0 \end{split}$$



VK = VK-, - jwl Ik is obvious, as VK will be equal to Vk-, mims the voltage drop in the inductor L denoted by Vi = jwl Ik Likewise, \vec{J}_k is the total current ambing at the mode \vec{J}_{k-1} mins the current drawn by the capacitor $\vec{J}_c = \vec{J}_w \in \vec{V}_{k-1}$

Therefore the general Fritation is corret:

Ik = Ik-1 - jwc Tk-1 and Tk = Jk-1 - jw LIK V

In tune domain with a 21 matched impedance, and no reflecting ware:

$$\tilde{V}_{o}(t) = V_{o} \cos \omega t = V_{o} e^{j\omega t}$$
 and $\tilde{J}_{o}(t) = \frac{\tilde{V}_{o}(t)}{z_{o}}$

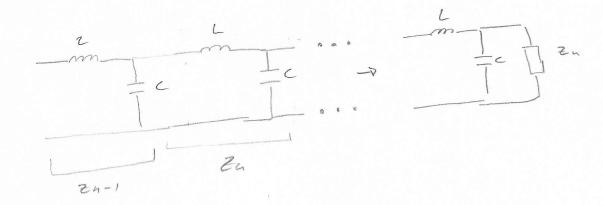
$$\widetilde{V}_{i}(t) = \widetilde{V}_{o}(t) - L \frac{d\widetilde{I}_{i}(t)}{dt}$$
 and $\widetilde{I}_{i}(t) = \widetilde{I}_{o}(t) - e \frac{dV_{i}(t)}{dt}$

$$V_2(t) = \widetilde{V}_1(t) - L \frac{dI_2(t)}{dt}$$
 and $I_2(t) = \overline{I}_1(t) - c \frac{dV_2(t)}{dt}$

$$\stackrel{\sim}{V_{k}(t)} = \stackrel{\sim}{V_{k-1}(t)} - L \stackrel{\sim}{ceI_{k}(t)}$$

$$\widetilde{I}_{k}(t) = \widetilde{I}_{k-1}(t) - c \frac{dV_{k}(t)}{dt}$$

11.1,4



$$\frac{2n-1}{2n+1} = \frac{2n}{j\omega c} + j\omega L \quad \text{for } Z_N = Z_L, \quad Z_N = Z_N + j\omega L$$

$$\frac{N-1}{2m} = \frac{N}{2m} = \frac{N}{2m+j\omega L} = \frac{N}{j\omega L} = \frac{$$

$$= \frac{z_n + j\omega L}{z_n j\omega C + j\omega C j\omega L + 1} = h$$

$$\frac{2n+j\omega L}{2nj\omega C-\omega^2 C L+1}$$

and to = jw2+ Z1

2.
$$\widetilde{J}_{k} = \widetilde{J}_{k-1} - j \omega C \widetilde{V}_{k-1}$$
 for $k = 0,1,...,N$ and $\widetilde{I}_{1} = \frac{\widetilde{V}_{0}}{20}$