# Week8 – Relaxation Time Approximation

ECE 695-O Semiconductor Transport Theory Fall 2018

Instructor: Byoung-Don Kong



#### Contents

• Relaxation Time Approximation- continues.



### Electrical Conductivity in the Relaxation Time Approximation-E-field only

 We considered relaxation time approximation of BTE when there is only efiled and arrived at

$$J_{x} = \frac{e^{2}n}{m^{*}} \langle \tau \rangle E_{x} .$$

We can generalize this expression such as

$$\mathbf{J} = \frac{e^2 n}{m^*} \langle \tau \rangle \mathbf{E}$$

where

$$\langle \tau \rangle = \frac{\int_0^{\mathcal{E}_m} \tau \, \mathcal{E}^{\frac{3}{2}} \, f_0(1 - f_0) d\mathcal{E}}{\int_0^{\mathcal{E}_m} \, \mathcal{E}^{\frac{3}{2}} \, f_0(1 - f_0) d\mathcal{E}}$$

• Mobility 
$$\mu = \frac{q}{m^*} \langle \tau \rangle$$

## Electrical Conductivity in the Relaxation Time Approximation-E-field only(2)

For non-degenerate semiconductors,

$$f_0(1-f_0) \cong f_0 \cong e^{-(\mathcal{E}-\mathcal{E}_F)/k_BT}$$

This gives

$$J_{x} \cong \frac{e^{2}nE_{x}}{m^{*}} \frac{\int_{0}^{\varepsilon_{m}} \tau \ \varepsilon^{\frac{3}{2}} e^{-(\varepsilon-\varepsilon_{F})/k_{B}T} \ d\varepsilon}{\int_{0}^{\varepsilon_{m}} \varepsilon^{\frac{3}{2}} e^{-(\varepsilon-\varepsilon_{F})/k_{B}T} \ d\varepsilon}$$
$$= \frac{e^{2}nE_{x}}{m^{*}} \frac{\int_{0}^{\varepsilon_{m}} \tau \ \varepsilon^{\frac{3}{2}} e^{-\varepsilon/k_{B}T} \ d\varepsilon}{\int_{0}^{\varepsilon_{m}} \varepsilon^{\frac{3}{2}} e^{-\varepsilon/k_{B}T} \ d\varepsilon}.$$

- Let's assume  $\tau = A \mathcal{E}^{-s}$  where  $s = \frac{1}{2}$  for acoustic phonon scattering and  $s = -\frac{3}{2}$  for charge impurity scattering.
- This will be discussed in the scattering section later but we just use the results here.



### Electrical Conductivity in the Relaxation Time Approximation-E-field only(3)

- Let's assume  $\tau = A\mathcal{E}^{-s}$  where  $s = \frac{1}{2}$  for acoustic phonon scattering and  $s = -\frac{3}{2}$  for charge impurity scattering.
- This will be discussed in the scattering section later but we just use the results here.
- However, you can understand this intuitively like followings.
- At high temperature,  $\tau_{ac\ ph} = A \mathcal{E}^{-\frac{1}{2}}$  is dominant term, and as  $\mathcal{E}$  increases, the scattering rate increases.
- At lower temperature,  $\tau_{ii} = A \mathcal{E}^{\frac{3}{2}}$  is dominant term, and as  $\mathcal{E}$  increases, the scattering rate decreases.
- $au_{ii}$  has Columbic origin. If incoming speed is fast, only electron trajectory is slightly affected.



#### Electrical Conductivity in the Relaxation Time Approximation-E-field only(4)

• Thus, with  $\tau = A \mathcal{E}^{-S}$  ,

$$\langle \tau \rangle = \frac{\int_0^{\mathcal{E}_m} A \mathcal{E}^{-s} \ \mathcal{E}^{\frac{3}{2}} e^{-\mathcal{E}/k_B T} \ d\mathcal{E}}{\int_0^{\mathcal{E}_m} \mathcal{E}^{\frac{3}{2}} e^{-\mathcal{E}/k_B T} \ d\mathcal{E}} \longrightarrow \text{become zero before } \mathcal{E}_m.$$

$$= A \frac{\int_0^{\infty} \mathcal{E}^{\frac{3}{2} - s} e^{-\mathcal{E}/k_B T} \ d\mathcal{E}}{\int_0^{\infty} \mathcal{E}^{\frac{3}{2}} e^{-\mathcal{E}/k_B T} \ d\mathcal{E}} \longrightarrow \text{You can recognize gamma function } \mathcal{E}_m$$
in the numerator and the denomination of the numerator and numerat

You can recognize gamma function forms in the numerator and the denominator.

• Let's put  $\frac{\varepsilon}{k_B T} = x$ ,

$$\Rightarrow \langle \tau \rangle = \frac{A}{(k_B T)^s} \frac{\int_0^\infty x^{\frac{3}{2} - s} e^{-x} dx}{\left(\int_0^\infty x^{\frac{3}{2}} e^{-x} dx\right)} = \Gamma\left(\frac{5}{2}\right)$$
$$\Rightarrow \langle \tau \rangle = \frac{A}{(k_B T)^s} \frac{\Gamma\left(\frac{5}{2} - s\right)}{\Gamma\left(\frac{5}{2}\right)}$$

$$\Gamma(z) = \int_0^\infty x^{z-1} e^{-x} dx$$

$$\Gamma(z+1) = z\Gamma(z)$$

$$\Gamma(1) = 1$$

$$\Gamma\left(\frac{1}{2}\right) = \sqrt{\pi}$$

## Electrical Conductivity in the Relaxation Time Approximation-E-field only(5)

• For acoustic phonon scattering,  $\tau = A \mathcal{E}^{-\frac{1}{2}}$  and  $s = \frac{1}{2}$ ,

$$\Rightarrow \langle \tau \rangle_{ac\ ph} = \frac{A}{(k_B T)^s} \frac{\Gamma\left(\frac{5}{2} - s\right)}{\Gamma\left(\frac{5}{2}\right)}$$

$$= \frac{A}{(k_B T)^{\frac{1}{2}}} \frac{\Gamma\left(\frac{5}{2} - \frac{1}{2}\right)}{\Gamma\left(\frac{5}{2}\right)}$$

$$= \frac{A}{(k_B T)^{\frac{1}{2}}} \frac{\Gamma\left(\frac{5}{2} - \frac{1}{2}\right)}{\Gamma\left(\frac{5}{2}\right)}$$

$$= \frac{A}{(k_B T)^{\frac{1}{2}}} \frac{\Gamma\left(\frac{4}{2}\right)}{\Gamma\left(\frac{5}{2}\right)} = \frac{A}{(k_B T)^{\frac{1}{2}}} \frac{\Gamma(2)}{\Gamma\left(\frac{5}{2}\right)}$$

$$= \frac{A}{(k_B T)^{\frac{1}{2}}} \frac{1 \times \Gamma(1)}{\frac{3}{2} \times \Gamma\left(\frac{3}{2}\right)} = \frac{A}{(k_B T)^{\frac{1}{2}}} \frac{1}{\frac{3}{2} \times \frac{1}{2} \times \Gamma\left(\frac{1}{2}\right)}$$

$$= \frac{4}{3} \frac{A}{(\pi k_B T)^{\frac{1}{2}}}$$

## Electrical Conductivity in the Relaxation Time Approximation-E-field only(6)

$$\Rightarrow \langle \tau \rangle_{ac\ ph} = \frac{4}{3} \frac{A}{(\pi k_B T)^{\frac{1}{2}}} \propto T^{-\frac{1}{2}}$$

- Thus, as T goes up,  $\langle \tau \rangle_{ac\ ph}$  goes down. Shorter relaxation time means more scattering; scattering or relaxation rate goes up.
- For ionized impurity scattering,  $\tau = A \mathcal{E}^{\frac{3}{2}}$  and  $s = -\frac{3}{2}$  ,
- We repeat the same stuff here;

$$\Rightarrow \langle \tau \rangle_{ii} = \frac{A'}{(k_B T)^s} \frac{\Gamma\left(\frac{5}{2} - s\right)}{\Gamma\left(\frac{5}{2}\right)} = \frac{8A'}{\sqrt{\pi}} (k_B T)^{3/2} \propto T^{\frac{3}{2}}$$

• And, as temperature goes up, scattering rate goes down.



### Electrical Conductivity in the Relaxation Time Approximation-E-field only(7)

- Usually there are multiple scattering mechanisms.
- If we recall the way we calculated relaxation time,

$$\frac{1}{\tau} \propto \int P_{\mathbf{k}\mathbf{k}'}\{\cdots\} d^3k'$$

and  $P_{\mathbf{k}\mathbf{k}'}$  is transition probability from  $\mathbf{k}$  to  $\mathbf{k}'$ .

• If there are many scattering mechanism, let's say  $P_{\mathbf{k}\mathbf{k}'}^1$ ,  $P_{\mathbf{k}\mathbf{k}'}^2$ ,  $P_{\mathbf{k}\mathbf{k}'}^3$ , etc., these can be added. Thus, the total scattering rate can be

$$\begin{split} \frac{1}{\tau_{total}} & \propto \int \left( P_{\mathbf{k}\mathbf{k}'}^{1} + P_{\mathbf{k}\mathbf{k}'}^{2} + P_{\mathbf{k}\mathbf{k}'}^{3} + \cdots \right) \{ \cdots \} d^{3}k' \\ & = \int P_{\mathbf{k}\mathbf{k}'}^{1} \{ \cdots \} d^{3}k' + \int P_{\mathbf{k}\mathbf{k}'}^{1} \{ \cdots \} d^{3}k' + \int P_{\mathbf{k}\mathbf{k}'}^{1} \{ \cdots \} d^{3}k' + \cdots \\ & = \frac{1}{\tau_{1}} + \frac{1}{\tau_{2}} + \frac{1}{\tau_{3}} + \cdots \end{split}$$



## Electrical Conductivity in the Relaxation Time Approximation-E-field only(8)

• Ideally, we can plug this,

$$\frac{1}{\tau_{total}} = \frac{1}{\tau_1} + \frac{1}{\tau_2} + \frac{1}{\tau_3} + \cdots$$

into

$$\langle \tau \rangle = \frac{\int_0^{\mathcal{E}_m} \tau \, \mathcal{E}^{\frac{3}{2}} \, f_0(1 - f_0) d\mathcal{E}}{\int_0^{\mathcal{E}_m} \, \mathcal{E}^{\frac{3}{2}} \, f_0(1 - f_0) d\mathcal{E}}$$

and calculate  $\langle \tau \rangle$ , but that is not easy.

As an approximation, we will use

$$\frac{1}{\langle \tau \rangle_{total}} \cong \frac{1}{\langle \tau \rangle_{1}} + \frac{1}{\langle \tau \rangle_{2}} + \frac{1}{\langle \tau \rangle_{3}} + \cdots$$

and this is so-called 'Matthiessen's rule'.



## Electrical Conductivity in the Relaxation Time Approximation-E-field only(9)

• Thus,

$$\frac{1}{\langle \tau \rangle} = \frac{1}{\langle \tau \rangle_{ac\ ph}} + \frac{1}{\langle \tau \rangle_{ii}}$$

and

$$\frac{1}{\mu} = \frac{m^*}{q} \left( \frac{1}{\langle \tau \rangle_{ac\ ph}} + \frac{1}{\langle \tau \rangle_{ii}} \right) .$$

If there are more scattering mechanism, you can keep adding here.

#### Single ellipsoidal energy minima – an example

In this case, the energy is given as

$$\mathcal{E} = \frac{\hbar^2 k_x^2}{2m_x^*} + \frac{\hbar^2 k_y^2}{2m_y^*} + \frac{\hbar^2 k_z^2}{2m_z^*}$$

and we assume electric field along x direction such as

$$\mathbf{E} = E_{x}\hat{\mathbf{x}}$$

$$J_{x} = \frac{e^{2}n}{m^{*}} \langle \tau \rangle E_{x}$$

Generally, this should be

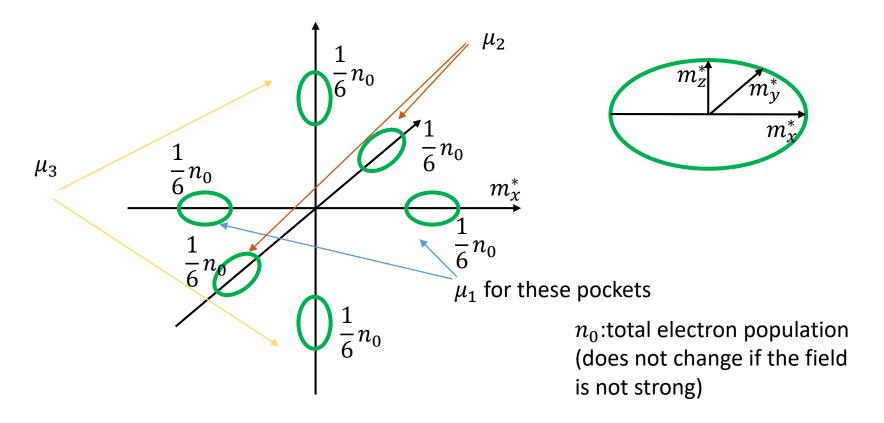
where 
$$\mathbf{\sigma}=egin{pmatrix} \mathbf{J}=\mathbf{\sigma}\mathbf{E} \\ \mathbf{\sigma}=egin{pmatrix} en\mu_1 & 0 & 0 \\ 0 & en\mu_2 & 0 \\ 0 & 0 & en\mu_3 \end{pmatrix} \quad \text{and} \quad \mu_i=rac{q\langle \tau \rangle}{m_i^*} \;.$$

• If E-field direction is parallel to the principal axis (x, y, z) then the current is parallel to the E-field. However, if the E-field is applied along other directions, current is not parallel to E-field.



#### Multiple ellipsoidal energy minima

- However, normally there are multiple minima exist so they will compensate the effect.
- In the case of Si, there are 6 minima near X.



### Multiple ellipsoidal energy minima(2)

• When  $\mathbf{E} = E_{x}\hat{\mathbf{x}}$ ,

$$J_{x} = \frac{1}{6} (n_{0}e\mu_{1}E_{x} + n_{0}e\mu_{1}E_{x} + n_{0}e\mu_{2}E_{x} + n_{0}e\mu_{2}E_{x} + n_{0}e\mu_{3}E_{x} + n_{0}e\mu_{3}E_{x})$$

$$= \frac{n_{0}e}{3} (\mu_{1} + \mu_{2} + \mu_{3})E_{x}$$

- If we change the field direction to along y-axis, we will get the same results since we will have the same  $\mu_1$ ,  $\mu_2$ , and  $\mu_3$ .
- Thus,

$$\mathbf{J}=\sigma\mathbf{E}$$
 where  $\sigma=\frac{ne}{3}(\mu_1+\mu_2+\mu_3)\equiv ne\mu$  .

• Since 
$$\mu \equiv \frac{1}{3}(\mu_1 + \mu_2 + \mu_3)$$
, 
$$\frac{q\langle \tau \rangle}{m^*} = q\langle \tau \rangle \frac{1}{3} \left( \frac{1}{m_x^*} + \frac{1}{m_y^*} + \frac{1}{m_z^*} \right)$$
 =  $\frac{1}{m_{cond}^*}$ : conductivity effective mass

### Multiple ellipsoidal energy minima(3)

• When  $\mathbf{E} = E_{x}\hat{\mathbf{x}}$ ,

$$J_{x} = \frac{1}{6} (n_{0}e\mu_{1}E_{x} + n_{0}e\mu_{1}E_{x} + n_{0}e\mu_{2}E_{x} + n_{0}e\mu_{2}E_{x} + n_{0}e\mu_{3}E_{x} + n_{0}e\mu_{3}E_{x})$$

$$= \frac{n_{0}e}{3} (\mu_{1} + \mu_{2} + \mu_{3})E_{x}$$

- If we change the field direction to along y-axis, we will get the same results since we will have the same  $\mu_1$  ,  $\mu_2$  , and  $\mu_3$  .
- Thus,

$$\mathbf{J} = \sigma \mathbf{E}$$
 where  $\sigma = \frac{ne}{3} (\mu_1 + \mu_2 + \mu_3) \equiv ne\mu$ .

• Since 
$$\mu \equiv \frac{1}{3}(\mu_1 + \mu_2 + \mu_3)$$
, 
$$\frac{q\langle \tau \rangle}{m^*} = q\langle \tau \rangle \frac{1}{3} \left( \frac{1}{m_x^*} + \frac{1}{m_y^*} + \frac{1}{m_z^*} \right)$$
 =  $\frac{1}{m_{cond}^*}$ : conductivity effective mass

### Multiple ellipsoidal energy minima(4)

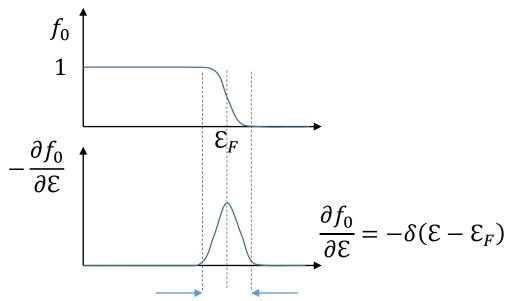
• Usually for silicon,

$$\frac{1}{m_{cond}^*} = \frac{1}{3} \left( \frac{1}{m_l^*} + \frac{2}{m_t^*} \right)$$

• FYI, 
$$m_{DOS}^* = \left(m_{\mathcal{X}}^* m_{\mathcal{Y}}^* m_{\mathcal{Z}}^*\right)^{1/3}$$

#### Conductivity in metals

- In metals, we cannot use the approximation,  $f_0(1-f_0) \approx$  Maxwell-Boltzmann distribution, since it is degenerate case.
- We will use  $f_0(1-f_0) = -k_B T \frac{\partial f_0}{\partial \varepsilon}$ .



Thermal broadening of order of  $k_BT$ 

$$\int_{-\infty}^{\infty} \frac{\partial f_0}{\partial \mathcal{E}} d\mathcal{E} = f_0 \Big|_{-\infty}^{\infty} = -1$$

So this is good

approximation

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### Conductivity in metals(2)

• Thus, for metals,

$$\langle \tau \rangle = \frac{\int \tau \ \mathcal{E}^{\frac{3}{2}} \frac{df_0}{d\mathcal{E}} d\mathcal{E}}{\int \mathcal{E}^{\frac{3}{2}} \frac{df_0}{d\mathcal{E}} d\mathcal{E}} = \frac{\int \tau \ \mathcal{E}^{\frac{3}{2}} \delta(\mathcal{E} - \mathcal{E}_F) d\mathcal{E}}{\int \mathcal{E}^{\frac{3}{2}} \delta(\mathcal{E} - \mathcal{E}_F) d\mathcal{E}}$$
$$\approx \frac{\tau(\mathcal{E}_F) \mathcal{E}_F^{\frac{3}{2}}}{\mathcal{E}_F^{\frac{3}{2}}} \approx \tau(\mathcal{E}_F)$$
.

- So, in metals,  $\langle \tau \rangle$  near  $\mathcal{E}_F$  is the dominant factor.
- In metal everything happens near Fermi level, and the states some energy under Fermi level do not have any empty spot to scatter in.

• So 
$$\mu = \frac{q}{m^*} \tau(\mathcal{E}_F)$$