



광전자공학 Ch. 2 Part 2

Reflection and Refraction

Seung-Yeol Lee

Impedance of plane wave

From $\mathbf{k} \times \mathbf{H} = -\varepsilon\omega\mathbf{E}$ or $\mathbf{k} \times \mathbf{E} = \mu\omega\mathbf{H}$

$$\eta = \frac{|\mathbf{E}|}{|\mathbf{H}|} = \frac{k}{\varepsilon\omega} = \frac{\mu\omega}{k} = \sqrt{\frac{\mu}{\varepsilon}}$$

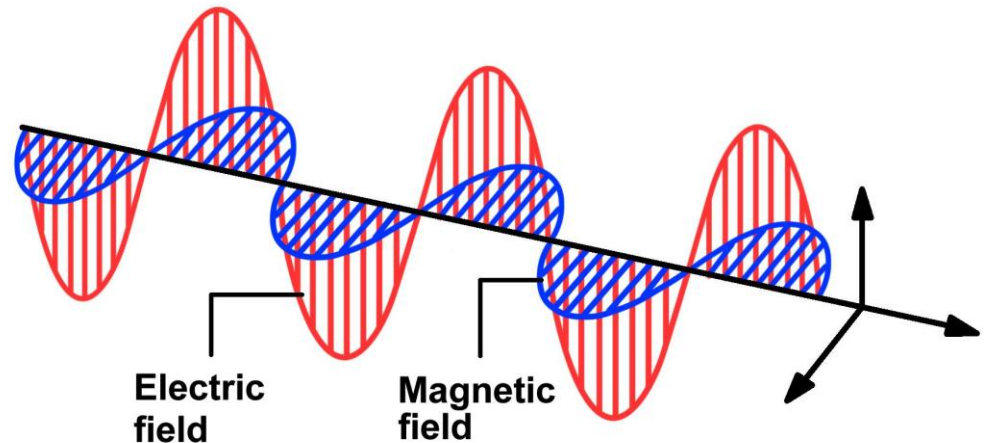
Impedance of plane wave
(Magnitude ratio of E and H)

In free space,

$$\eta_0 = \frac{|\mathbf{E}|}{|\mathbf{H}|} = \sqrt{\frac{\mu_0}{\varepsilon_0}} = 377 \, \Omega$$

In nonmagnetic material,

$$\eta = \frac{|\mathbf{E}|}{|\mathbf{H}|} = \sqrt{\frac{\mu_0}{\varepsilon}} = \frac{\eta_0}{n}$$



Energy carried by EM wave

Using Maxwell curl equations,

$$\mathbf{H} \cdot \nabla \times \mathbf{E} = -\mathbf{H} \cdot \frac{\partial \mathbf{B}}{\partial t} \qquad \mathbf{E} \cdot \nabla \times \mathbf{H} = \mathbf{J} \cdot \mathbf{E} + \mathbf{E} \cdot \frac{\partial \mathbf{D}}{\partial t}$$

Subtracting above equations,

$$\nabla \cdot (\mathbf{E} \times \mathbf{H}) = \mathbf{H} \cdot \nabla \times \mathbf{E} - \mathbf{E} \cdot \nabla \times \mathbf{H} = -\mathbf{H} \cdot \frac{\partial \mathbf{B}}{\partial t} - \mathbf{E} \cdot \frac{\partial \mathbf{D}}{\partial t} - \mathbf{J} \cdot \mathbf{E}$$

We define Poynting vector as $\mathbf{S} = \mathbf{E} \times \mathbf{H}$

$$\nabla \cdot \mathbf{S} = -\frac{\partial}{\partial t} \left(\frac{1}{2} \mu_0 \mathbf{H}^2 + \frac{1}{2} \mu_0 \mathbf{E}^2 \right) - \mathbf{J} \cdot \mathbf{E}$$


Energy Conservation

$$\boxed{\nabla \cdot \mathbf{S} + \mathbf{J} \cdot \mathbf{E}} = -\frac{\partial}{\partial t} \left(\frac{1}{2} \mu_0 \mathbf{H}^2 + \frac{1}{2} \mu_0 \mathbf{E}^2 \right)$$

EM wave radiation flux

Heat dissipation

Decrease of stored energy



Poynting vector

Poynting vector indicates the energy flow direction of light

$$\mathbf{S} = \mathbf{E} \times \mathbf{H}$$

For a plane wave $\mathbf{E} = \mathbf{E}_0 \cos(\mathbf{k} \cdot \mathbf{r} - \omega t)$ $\mathbf{H} = \mathbf{H}_0 \cos(\mathbf{k} \cdot \mathbf{r} - \omega t)$

$$\mathbf{S} = \mathbf{E}_0 \times \mathbf{H}_0 \cos^2(\mathbf{k} \cdot \mathbf{r} - \omega t)$$

A time-average Poynting vector can be expressed as

$$\langle \mathbf{S} \rangle = \bar{\mathbf{S}} = \frac{1}{2} \mathbf{E}_0 \times \mathbf{H}_0 = \frac{1}{2} \bar{\mathbf{E}} \times \bar{\mathbf{H}}^*$$

Upper-bar indicates a complex phasor notation

For isotropic media, \mathbf{S} has the same direction as \mathbf{k}

Snell's law

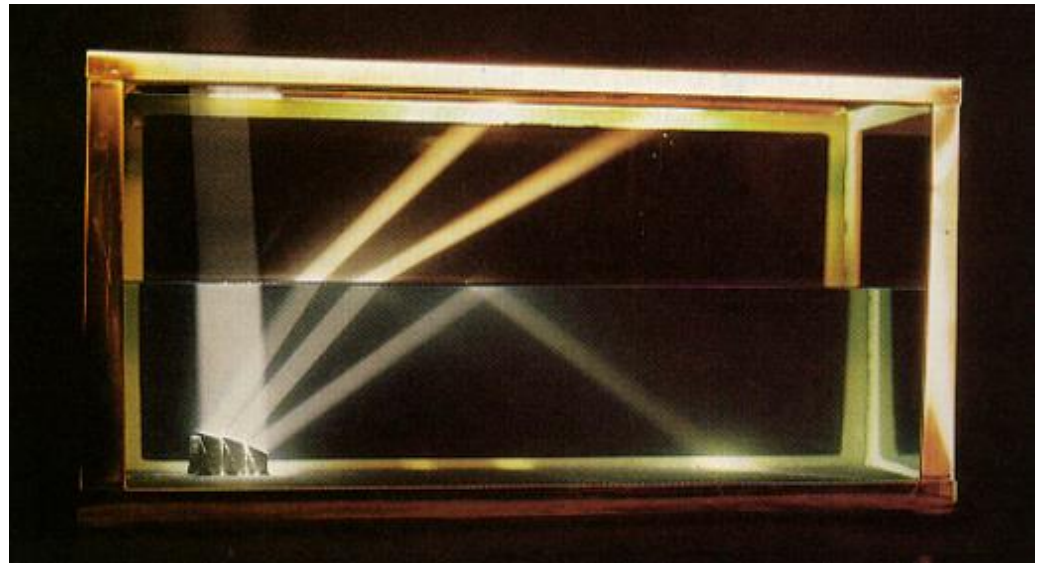
스넬의 법칙

$$n_i \sin \theta_i = n_r \sin \theta_r$$

1. 빛을 광선의 관점으로 해석하면:
페르마의 원리로 증명 가능
2. 빛을 파동의 관점으로 해석하면:
Phase matching condition 으로 해석 가능



빌레브로르트 스넬



physlab.snu.ac.kr



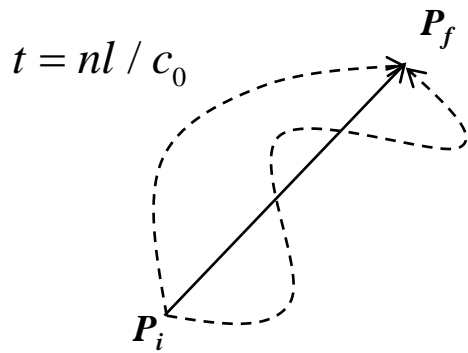
Fermat's Principle



헤론 (c. 10~c. 70)

빛은 두 지점 간의 최단거리의 경로를 통과하여 지나간다.

- 반사의 원리를 설명하였으나, 굴절의 원리를 정확히 설명할 수 없었다.



광경로란, 굴절률과 거리의 곱의 개념으로, 매질에 관계없이 단위 시간동안 빛은 같은 거리의 광경로를 지나간다.

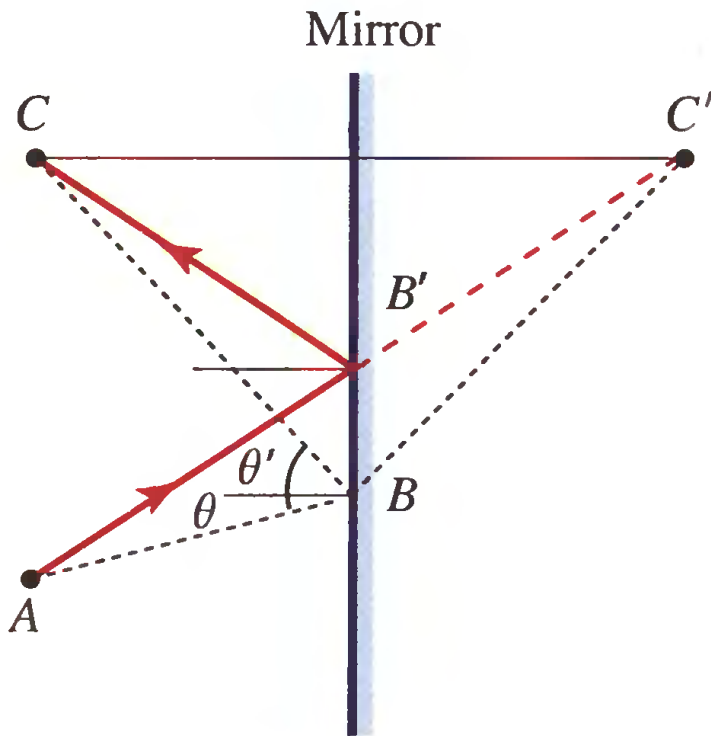
빛은 두 지점 간의 가장 짧은 광경로, 즉 최단시간의 경로를 통과하여 지나간다.



피에르 드 페르마 (1601~1665)

Fermat's Principle

Fermat's principle in Mirror reflection

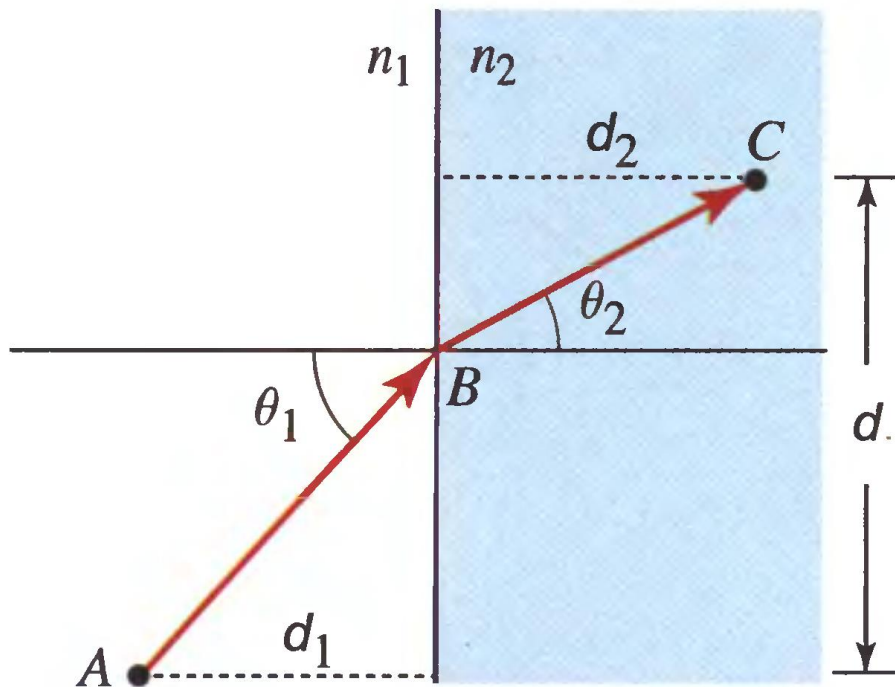


$$\overline{AB'C} = \overline{AB'C'} < \overline{ABC'}$$

Light choose the way having the shortest optical pathlength!

Fermat's Principle

Fermat's principle in Snell's law



Find the minimum value of

$$OPL = n_1 \overline{AB} + n_2 \overline{BC}$$

$$OPL = n_1 d_1 \sec \theta_1 + n_2 d_2 \sec \theta_2$$

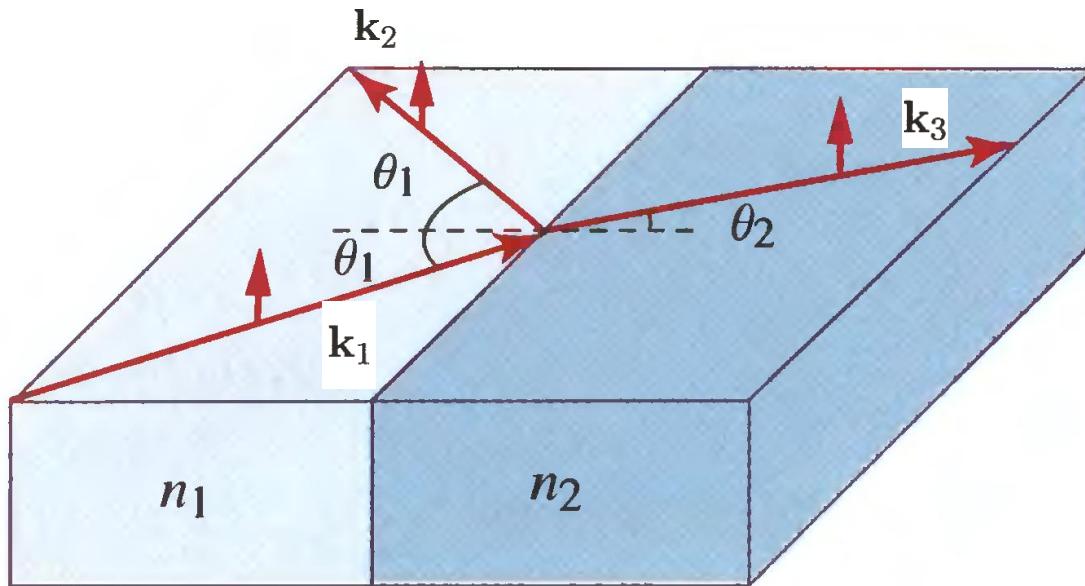
$$d = d_1 \tan \theta_1 + d_2 \tan \theta_2 \text{ (Constant)}$$

$$\text{Use } \frac{d\theta_2}{d\theta_1} = -\frac{d_1 \sec^2 \theta_1}{d_2 \sec^2 \theta_2}$$

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

Phase matching condition

At any point of boundary, wavefront must be continuous, in order to satisfy the EM boundary condition.



$$k_{1x} = k_{2x}$$

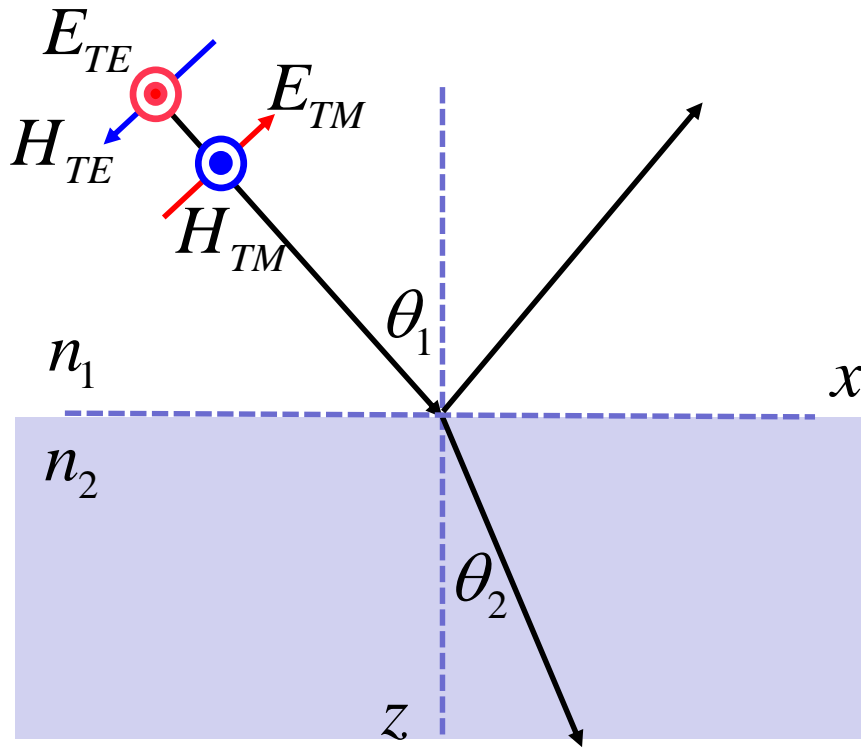


$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

$$\mathbf{k}_1 \cdot \mathbf{r} = \mathbf{k}_2 \cdot \mathbf{r} = \mathbf{k}_3 \cdot \mathbf{r} \quad \text{for all } \mathbf{r} = (x, y, 0)$$

Reflection and Refraction

Definition TE-pol and TM-pol



Plane of incidence : x-z plane

TE-pol (s-pol)

$$\begin{aligned}\mathbf{E} &= E_0 \exp(jk_1 \sin \theta_1 x + jk_1 \cos \theta_1 z) \hat{y} \\ &= E_0 \hat{y} \exp(j(k_x x + k_z z)) \\ \mathbf{H} &= -\frac{j}{\omega \mu_0} \nabla \times \mathbf{E} = -\frac{j}{\omega \mu_0} \left(-\frac{\partial E_y}{\partial z} \hat{x} + \frac{\partial E_y}{\partial x} \hat{z} \right) \\ &= -\frac{E_0 n_1}{\eta_0} (\cos \theta_1 \hat{x} - \sin \theta_1 \hat{z}) \exp(j(k_x x + k_z z))\end{aligned}$$

TM-pol (p-pol)

$$\begin{aligned}\mathbf{H} &= H_0 \hat{y} \exp(j(k_x x + k_z z)) \\ \mathbf{E} &= \frac{j}{\omega \epsilon} \nabla \times \mathbf{H} = \frac{j}{\omega \epsilon} \left(-\frac{\partial H_y}{\partial z} \hat{x} + \frac{\partial H_y}{\partial x} \hat{z} \right) \\ &= \frac{\eta_0 H_0}{n_1} (\cos \theta_1 \hat{x} - \sin \theta_1 \hat{z}) \exp(j(k_x x + k_z z))\end{aligned}$$

Reflection and Refraction

Reflection & Refraction at interface

TE-pol (s-pol)

E_y

$$E_i = \hat{y}E_0 \exp(j(k_x x + k_{z1} z))$$

$$E_r = \hat{y}r_s E_0 \exp(j(k_x x - k_{z1} z))$$

$$E_t = \hat{y}t_s E_0 \exp(j(k_x x + k_{z2} z))$$



$$1 + r_s = t_s \quad 1 - r_s = t_s \frac{n_2 \cos \theta_2}{n_1 \cos \theta_1}$$



H_x

$$H_i = -\frac{n_1 E_0}{\eta_0} \cos \theta_1 \hat{x} \exp(j(k_x x + k_z z))$$

$$H_r = -\frac{-n_1 r_s E_0}{\eta_0} \cos \theta_1 \hat{x} \exp(j(k_x x - k_z z))$$

$$H_t = -\frac{n_2 t_s E_0}{\eta_0} \cos \theta_2 \hat{x} \exp(j(k_x x + k_{z2} z))$$

$$r_s = \frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2}$$

$$t_s = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + n_2 \cos \theta_2}$$

Reflection and Refraction

Reflection & Refraction at interface

TM-pol (p-pol)

Ex

$$E_i = \hat{x}E_0 \exp(j(k_x x + k_{z1} z))$$

$$E_r = \hat{x}E_0 r_p \exp(j(k_x x - k_{z1} z))$$

$$E_t = \hat{x}E_0 t_p \exp(j(k_x x + k_{z2} z))$$



$$1 + r_p = t_p \quad 1 - r_p = t_p \frac{n_2 \sec \theta_2}{n_1 \sec \theta_1}$$



Hy

$$H_i = \frac{n_1 E_0}{\eta_0} \sec \theta_1 \hat{y} \exp(j(k_x x + k_z z))$$

$$H_r = \frac{n_1 E_0}{\eta_0} r_p \sec \theta_1 \hat{y} \exp(j(k_x x - k_z z))$$

$$H_t = \frac{n_2 E_0}{\eta_0} t_p \sec \theta_2 \hat{y} \exp(j(k_x x + k_{z2} z))$$

$$r_s = \frac{n_1 \sec \theta_1 - n_2 \sec \theta_2}{n_1 \sec \theta_1 + n_2 \sec \theta_2}$$

$$t_s = \frac{2n_1 \sec \theta_1}{n_1 \sec \theta_1 + n_2 \sec \theta_2}$$



Fresnel Equations

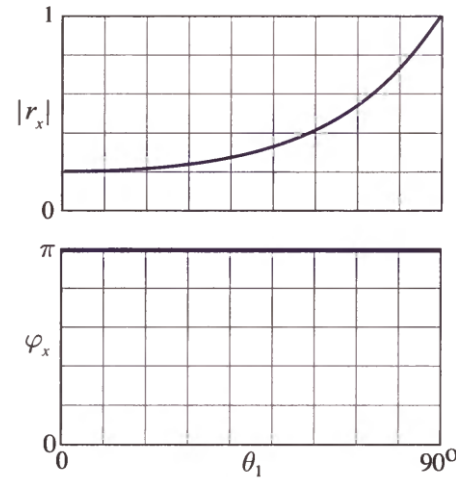
Reflection & Refraction at interface

TE-pol (s-pol)

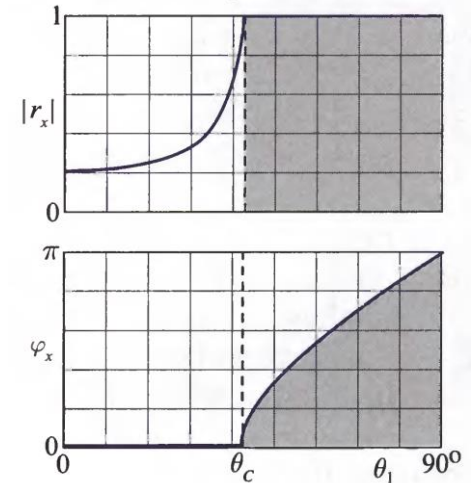
$$r_s = \frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2}$$

$$t_s = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + n_2 \cos \theta_2}$$

$n_1 < n_2$



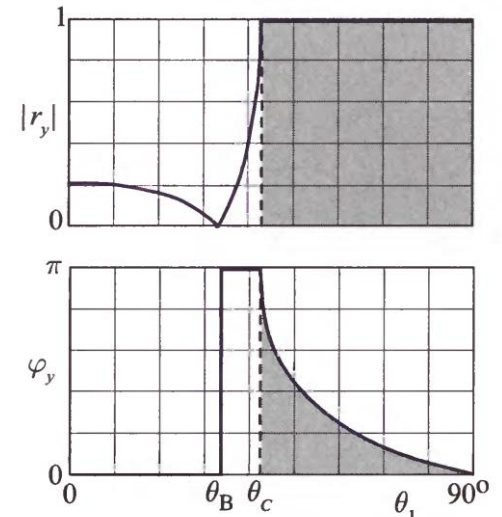
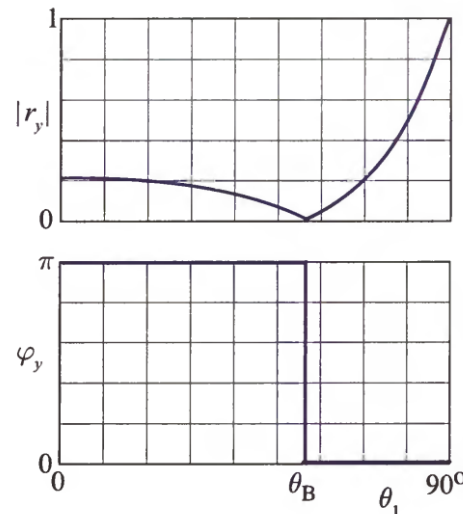
$n_1 > n_2$



TM-pol (p-pol)

$$r_p = \frac{n_1 \sec \theta_1 - n_2 \sec \theta_2}{n_1 \sec \theta_1 + n_2 \sec \theta_2}$$

$$t_p = \frac{2n_1 \sec \theta_2}{n_1 \sec \theta_1 + n_2 \sec \theta_2}$$



Critical angle

Only shown for internal reflection ($n_1 > n_2$)

$$\text{If } k_x = n_1 k_0 \sin \theta_1 \geq n_2 k_0$$

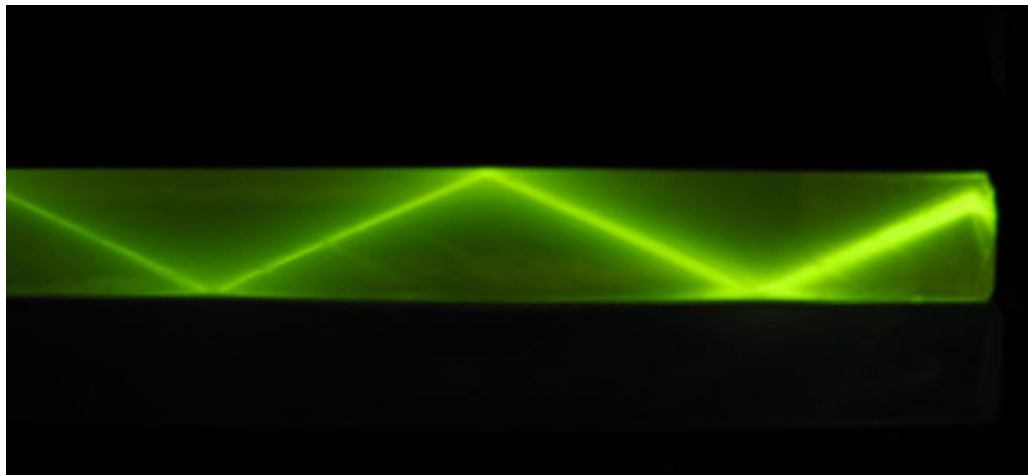
$$k_{z2} = k_0 \sqrt{n_2^2 - (n_1 \sin \theta_1)^2} = -jn_2 k_0 \sqrt{\left(\frac{n_1}{n_2} \sin \theta_1\right)^2 - 1} = -j\kappa$$

$$E_t = tE_0 \exp(-j(k_x x - j\kappa z)) = tE_0 \exp(-\kappa x) \exp(-jk_x x) \quad \text{Evanescent field}$$

Total internal reflection

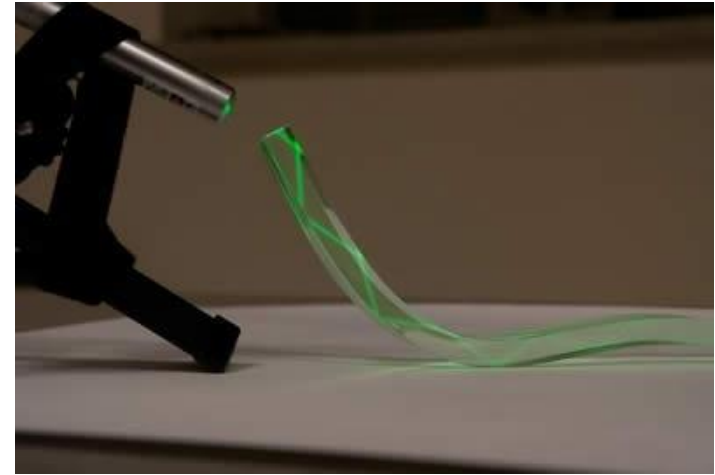
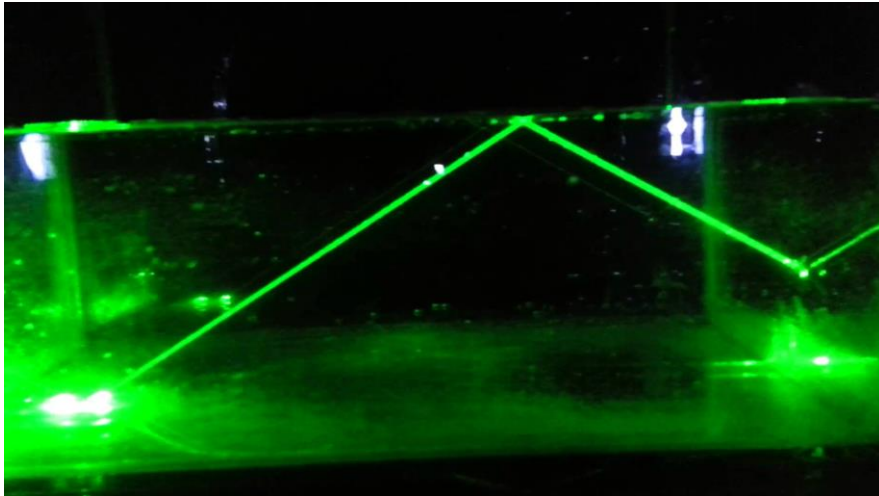
Critical angle

$$\theta_c = \sin^{-1} \left(\frac{n_2}{n_1} \right)$$

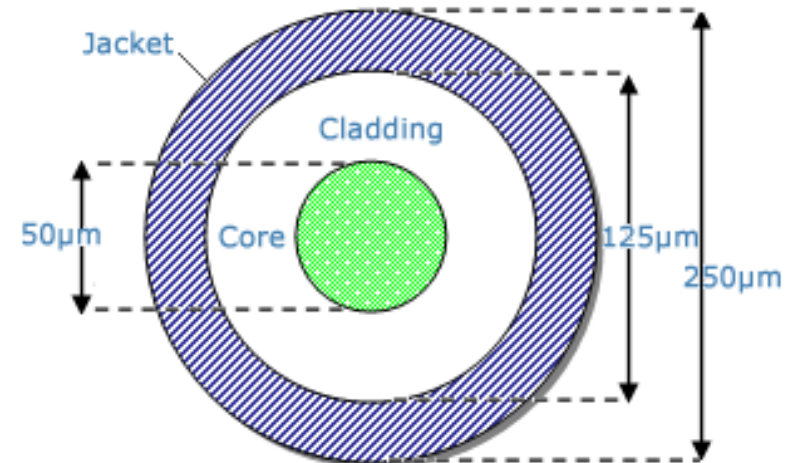


Total internal reflection

Total Internal Reflection



Key principle for designing optical fiber



Brewster angle

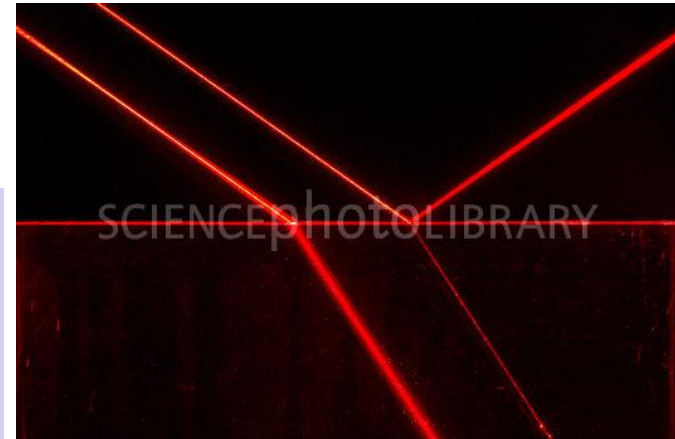
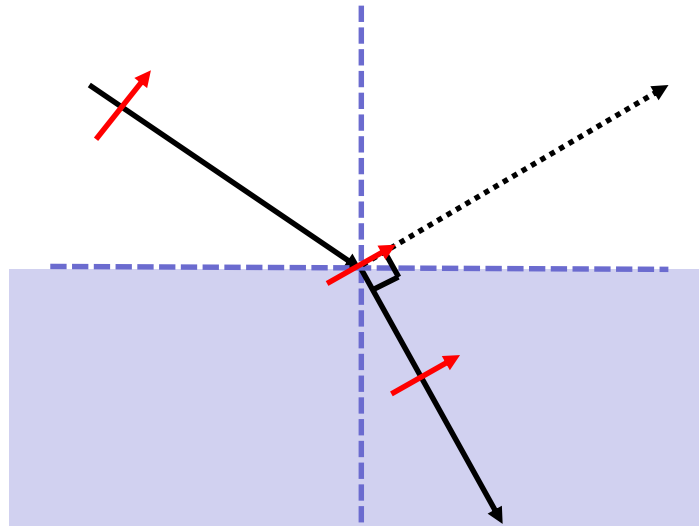
Only shown for TM polarization

$$r_p = \frac{n_1 \sec \theta_1 - n_2 \sec \theta_2}{n_1 \sec \theta_1 + n_2 \sec \theta_2} = 0, \text{ when } n_1 \sec \theta_1 - n_2 \sec \theta_2 = 0$$

$$\frac{\cos \theta_2}{\cos \theta_1} = \frac{n_2}{n_1} = \frac{\sin \theta_1}{\sin \theta_2}$$

$$\theta_1 + \theta_2 = 90^\circ$$

$$\tan \theta_1 = \frac{n_2}{n_1}$$



There is no reflection at Brewster angle for TM pol

Power reflectance & transmittance

Use complex Poynting vector and take z-component

$$\bar{\mathbf{S}} = \frac{1}{2} \bar{\mathbf{E}} \times \bar{\mathbf{H}}^* \quad S_z = \frac{1}{2} (E_x H_y^* - E_y H_x^*)$$

TE-pol (s-pol)

$$S_{zi} = \frac{k_0 |E_0|^2}{\omega \mu_0} n_1 \cos \theta_1 \quad S_{zr} = -\frac{k_0 |E_0|^2}{\omega \mu_0} |r|^2 n_1 \cos \theta_1 \quad S_{zt} = \frac{k_0 |E_0|^2}{\omega \mu_0} |t|^2 n_2 \cos \theta_2$$

Power reflectance & transmittance

$$\mathbf{R} = -\frac{S_{zr}}{S_{zi}} = |r|^2 \quad \mathbf{T} = \frac{S_{zt}}{S_{zi}} = \frac{n_2 \cos \theta_2}{n_1 \cos \theta_1} |t|^2$$