



광전자공학 Ch. 4

Multiple beam interference

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Multiple wave interference

$$U = U_1 + U_2 + \cdots + U_M$$

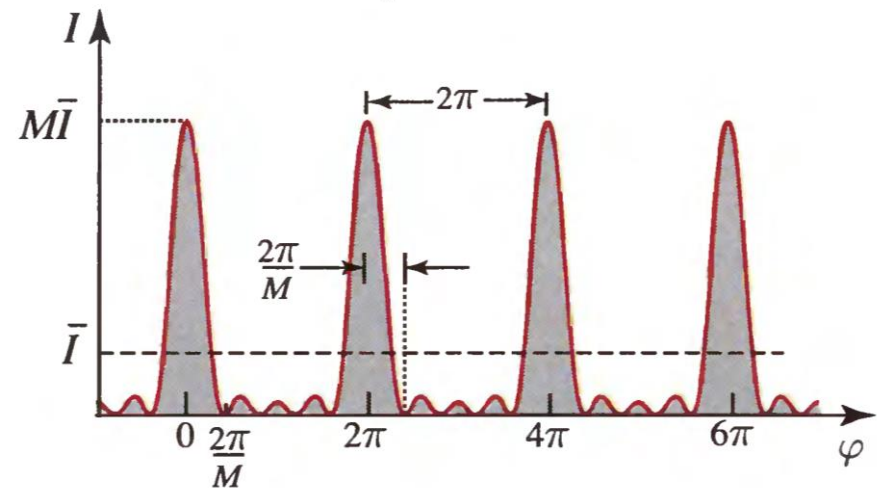
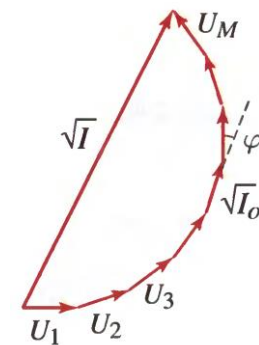
Interference of M Waves with Equal Amplitudes and Equal Phase Differences

$$U_m = \sqrt{I_0} \exp[j(m-1)\varphi], \quad m = 1, 2, \dots, M.$$

$$U = \sqrt{I_0} \frac{1 - \exp(jM\varphi)}{1 - \exp(j\varphi)}$$

$$I = |U|^2 = I_0 \left| \frac{\exp(-jM\varphi/2) - \exp(jM\varphi/2)}{\exp(-j\varphi/2) - \exp(j\varphi/2)} \right|^2$$

$$I = I_0 \frac{\sin^2(M\varphi/2)}{\sin^2(\varphi/2)}.$$



Multiple wave interference

Interference of an Infinite Number of Waves of Progressively Smaller Amplitudes and Equal Phase Differences

$$U = \frac{\sqrt{I_0}}{1 - h} = \frac{\sqrt{I_0}}{1 - |h|e^{j\varphi}}$$

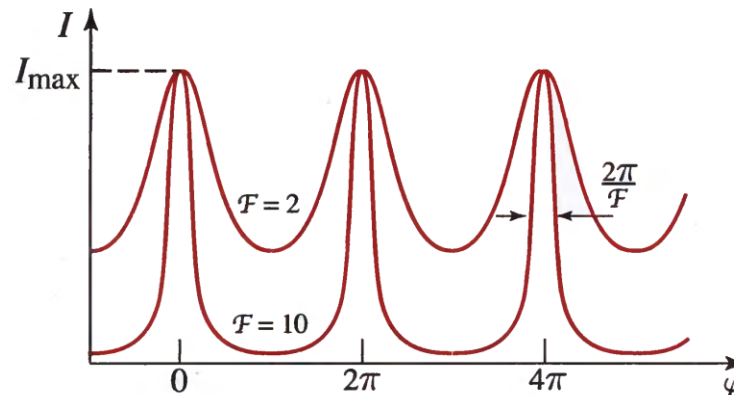
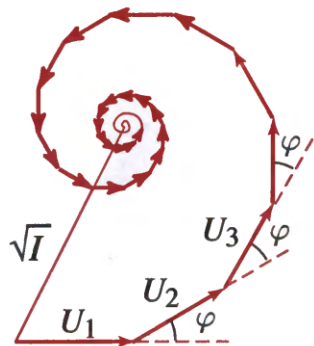
$$I = \frac{I_0}{(1 - |h|)^2 + 4|h| \sin^2(\varphi/2)}$$

$$I = \frac{I_{\max}}{1 + (2\mathcal{F}/\pi)^2 \sin^2(\varphi/2)}$$

$$I_{\max} = \frac{I_0}{(1 - |h|)^2}$$

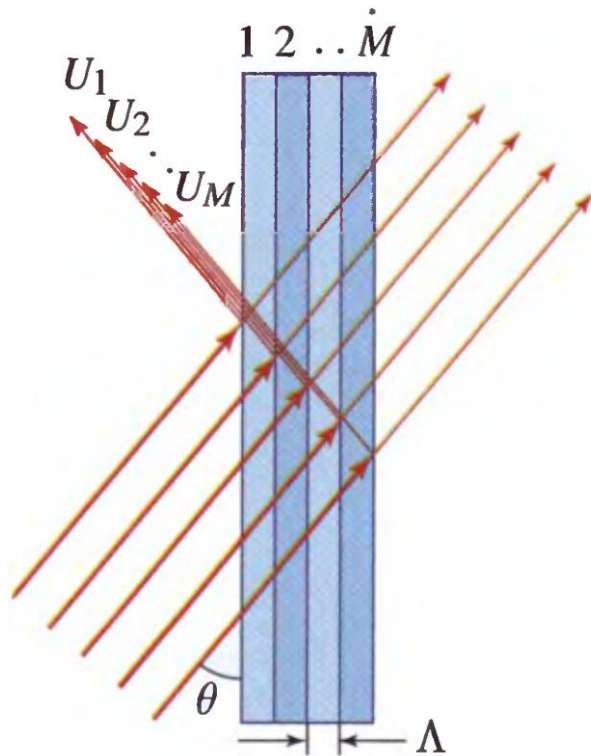
Finesse

$$\mathcal{F} = \frac{\pi \sqrt{|h|}}{1 - |h|}$$



Bragg reflection

Multiple reflections in periodic dielectric slab



$$\varphi = k(2\Lambda \sin \theta)$$

$$\sin \theta = \frac{\lambda}{2\Lambda} \quad \text{Bragg Angle}$$

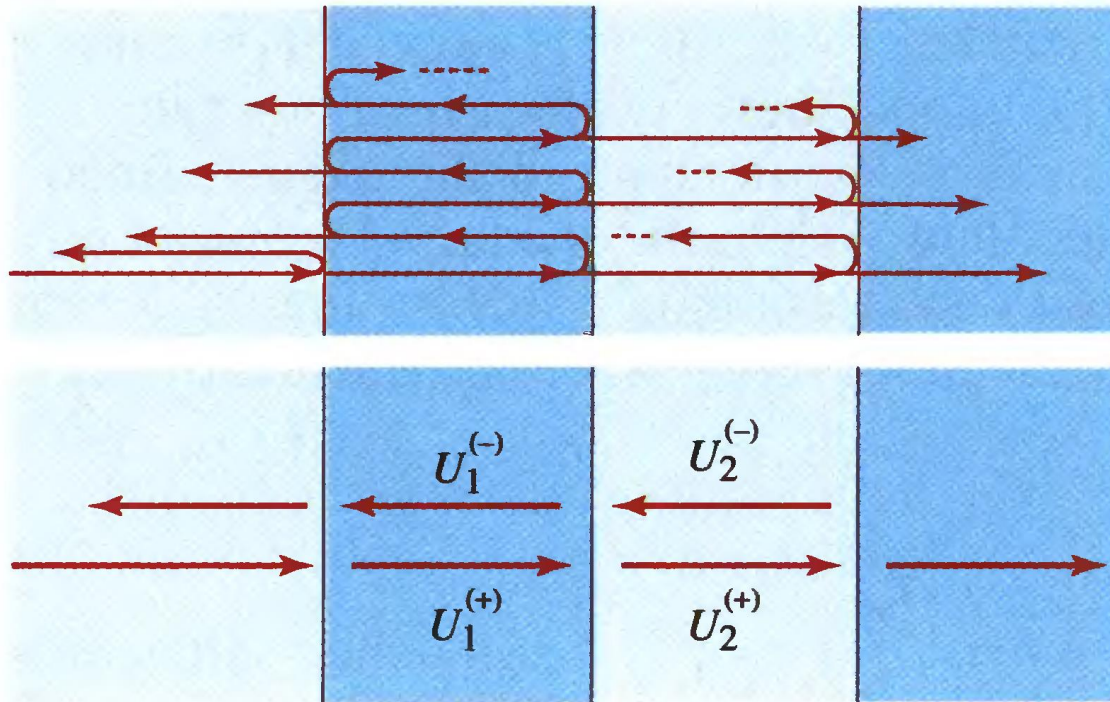
Specific angle of incident light
will totally reflected



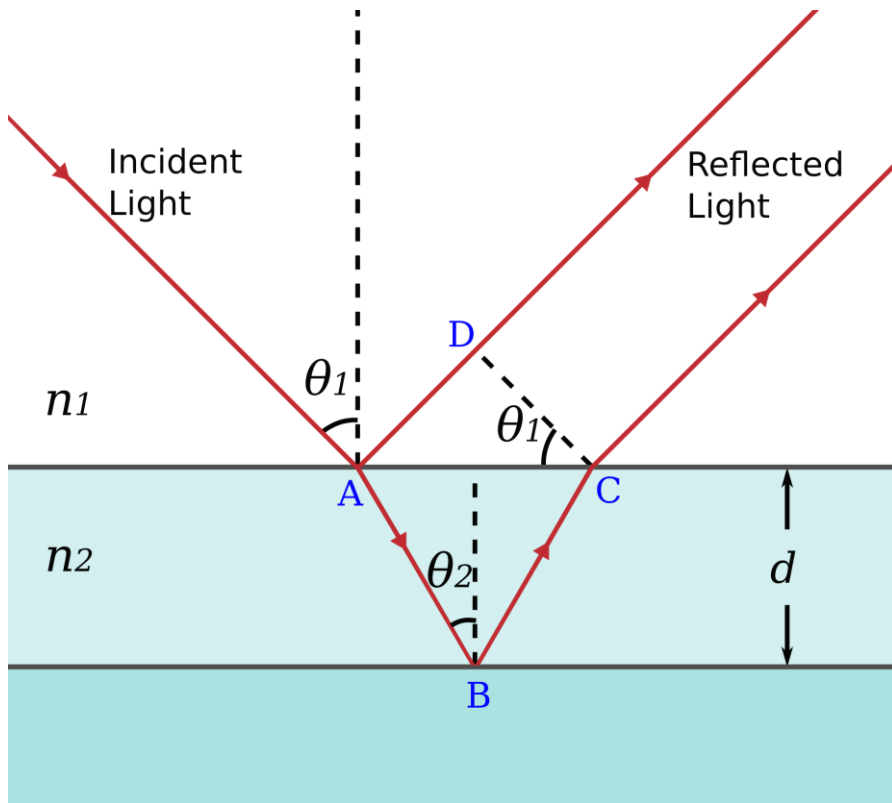
Bragg mirrors

Multiple-reflections at interfaces

When light illuminates the **thin-film layer**, there may be multiple reflections, and we have to consider the superposed value.



Thin-film interference



$$OPD = n_2(\overline{AB} + \overline{BC}) - n_1(\overline{AD})$$

Where,

$$\overline{AB} = \overline{BC} = \frac{d}{\cos(\theta_2)}$$

$$\overline{AD} = 2d \tan(\theta_2) \sin(\theta_1)$$

Using [Snell's Law](#), $n_1 \sin(\theta_1) = n_2 \sin(\theta_2)$

$$OPD = n_2 \left(\frac{2d}{\cos(\theta_2)} \right) - 2d \tan(\theta_2) n_2 \sin(\theta_2)$$

$$OPD = 2n_2 d \left(\frac{1 - \sin^2(\theta_2)}{\cos(\theta_2)} \right)$$

$$OPD = 2n_2 d \cos(\theta_2)$$

$$2n_2 d \cos(\theta_2) = m\lambda$$

Simply,

$$2k_z d = 2\pi m \Rightarrow 2n_2 k_0 \cos(\theta_2) d = 2\pi m$$

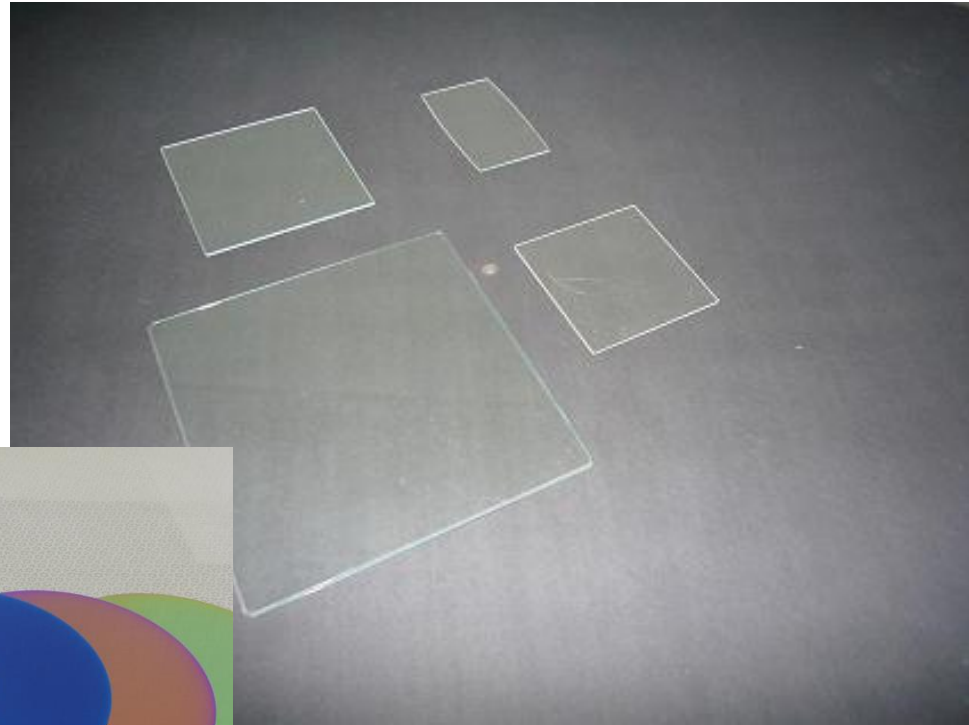
Thin-film interference

Why only thin-film interference? No thick-film interference??

Thin-film



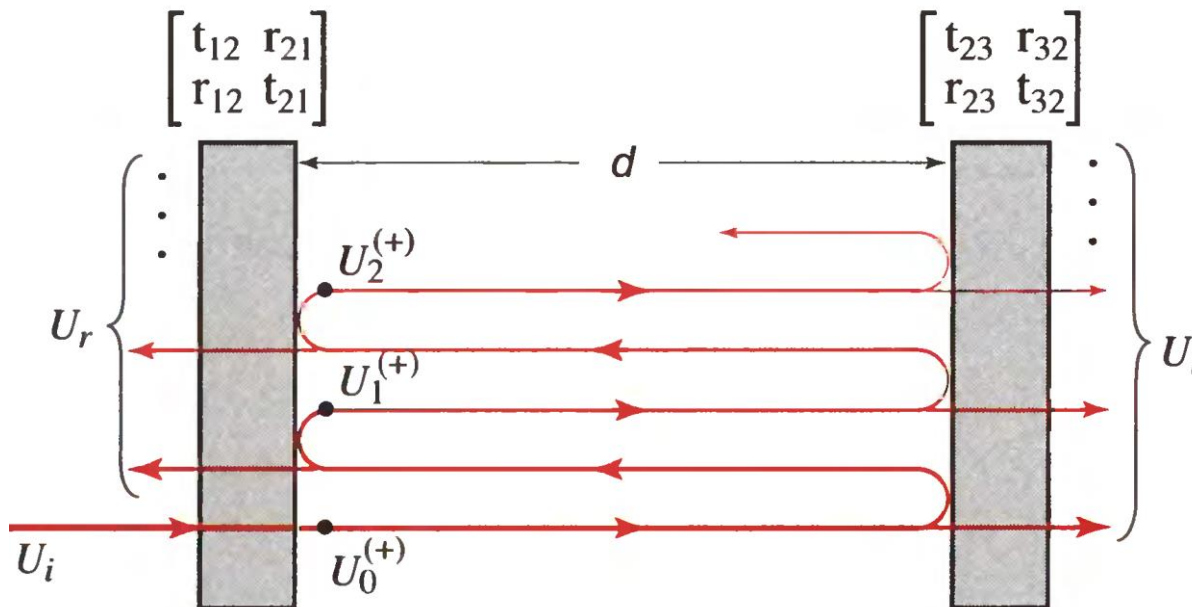
Thick-film



Thin-film

Airy's formula

Two cascade systems distanced with homogeneous media.
 –Multiple reflections are analytically calculated.



$$t_{13} = \frac{t_{12}t_{23} \exp(-j\varphi)}{1 - r_{21}r_{23} \exp(-j2\varphi)},$$

$$r_{13} = r_{12} + \frac{t_{12}t_{21}r_{23} \exp(-j2\varphi)}{1 - r_{21}r_{23} \exp(-j2\varphi)}$$

$$\varphi = nk_o d$$

Thin-film resonance condition

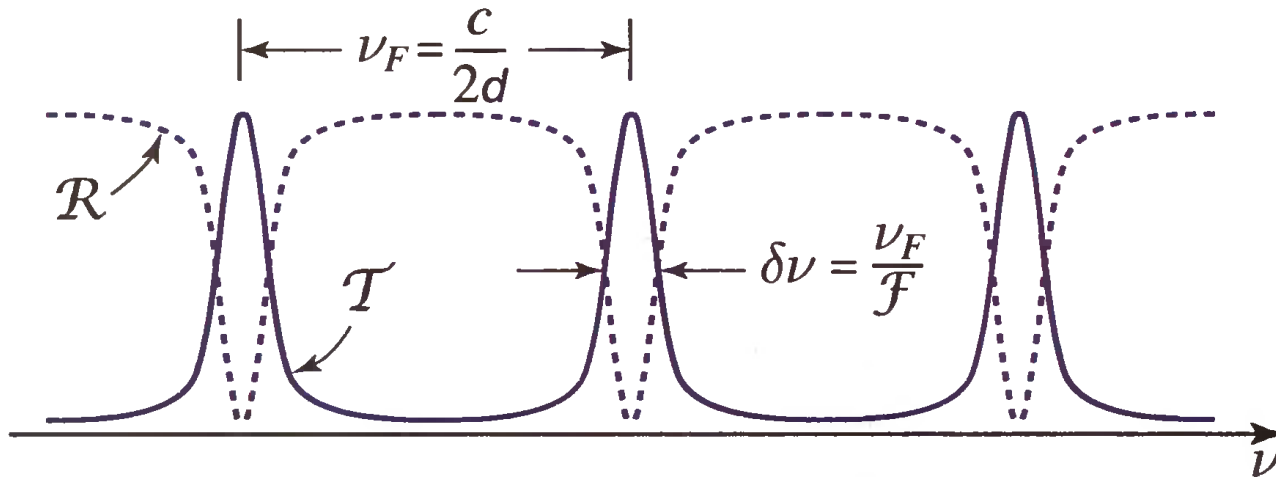
$$2\varphi = 2\pi m$$

Fabry-Perot Etalon

Two mirror system can act as a resonator.

$$\mathcal{T} = |t|^2 = \frac{|t_1 t_2|^2}{|1 - r_1 r_2 \exp(-j2\varphi)|^2}$$

$$\mathcal{T} = \frac{\mathcal{T}_{\max}}{1 + (2\mathcal{F}/\pi)^2 \sin^2 \varphi}$$



Maximum transmission

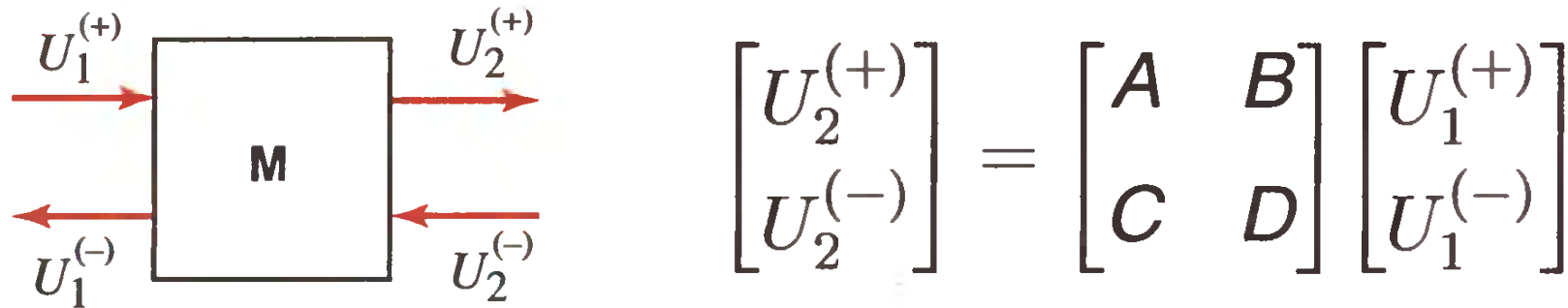
$$\mathcal{T}_{\max} = \frac{|t_1 t_2|^2}{(1 - |r_1 r_2|)^2}$$

Finesse

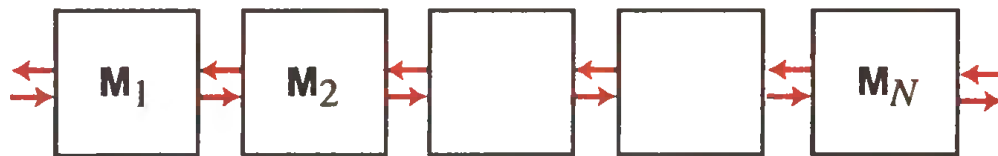
$$\mathcal{F} = \frac{\pi \sqrt{|r_1 r_2|}}{1 - |r_1 r_2|}$$

Transfer & scattering matrix

Transfer matrix : input-to-output layer relation



Benefit: Cascaded system can be simply calculated



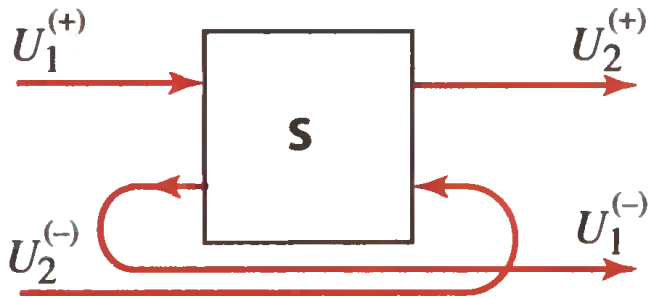
$$\mathbf{M} = \mathbf{M}_N \dots \mathbf{M}_2 \mathbf{M}_1$$

Drawback: parameter A B C D, do not contain physical insights.

Applications : ray transfer, thin-film system etc.

Transfer & scattering matrix

Scattering matrix : matrix given by reflection, transmission coefficients



$$\begin{bmatrix} U_2^{(+)} \\ U_1^{(-)} \end{bmatrix} = \begin{bmatrix} t_{12} & r_{21} \\ r_{12} & t_{21} \end{bmatrix} \begin{bmatrix} U_1^{(+)} \\ U_2^{(-)} \end{bmatrix}$$

Benefit: Each elements have direct physical meaning.

Drawback: cascading calculation is more difficult compared to transfer matrix.

Applications : transmission line, microwave circuits, scattering system.

Transfer & scattering matrix

Conversion of transfer matrix to scattering matrix and vice versa,

$$\mathbf{M} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} = \frac{1}{t_{21}} \begin{bmatrix} t_{12}t_{21} - r_{12}r_{21} & r_{21} \\ -r_{12} & 1 \end{bmatrix},$$

$$\mathbf{S} = \begin{bmatrix} t_{12} & r_{21} \\ r_{12} & t_{21} \end{bmatrix} = \frac{1}{D} \begin{bmatrix} AD - BC & B \\ -C & 1 \end{bmatrix}.$$

For lossless, reciprocal system,

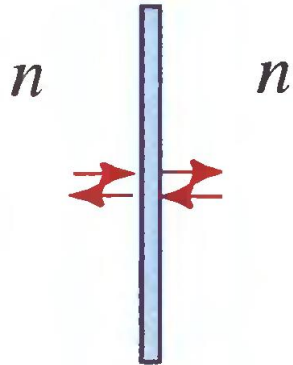
$$|t|^2 + |r|^2 = 1 \quad t/r = -(t/r)^* \quad r_{21} = r_{12} \equiv r \quad t_{21} = t_{12} \equiv t$$

$$\arg\{t\} - \arg\{r\} = \pm\pi/2.$$

$$\mathbf{S} = \begin{bmatrix} t & r \\ r & t \end{bmatrix}, \quad \mathbf{M} = \begin{bmatrix} 1/t^* & r/t \\ r^*/t^* & 1/t \end{bmatrix}$$

Transfer & scattering matrix

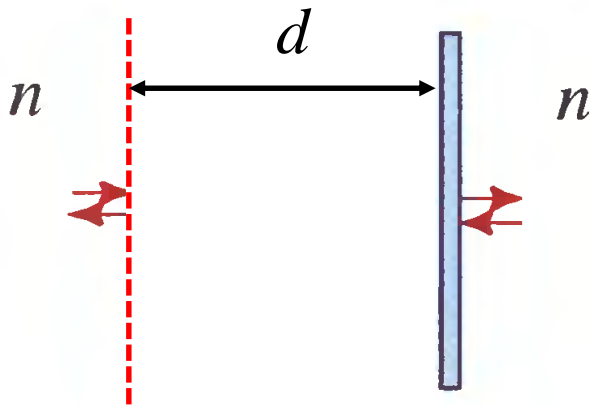
For example, at partially-reflective mirror



$$\mathbf{S} = \begin{bmatrix} |t| & j|r| \\ j|r| & |t| \end{bmatrix}, \quad |t|^2 + |r|^2 = 1$$

$$\mathbf{M} = \frac{1}{|t|} \begin{bmatrix} 1 & j|r| \\ -j|r| & 1 \end{bmatrix}$$

Partially-reflective mirror distance with d



$$\mathbf{S}_1 = \begin{bmatrix} e^{j\varphi} & 0 \\ 0 & e^{j\varphi} \end{bmatrix} \quad \mathbf{S}_2 = \begin{bmatrix} |t| & j|r| \\ -j|r| & |t| \end{bmatrix}$$

$$\mathbf{M} = \frac{1}{|t|} \begin{bmatrix} 1 & j|r| \\ -j|r| & 1 \end{bmatrix} \begin{bmatrix} e^{-j\varphi} & 0 \\ 0 & e^{j\varphi} \end{bmatrix} = \frac{1}{|t|} \begin{bmatrix} e^{-j\varphi} & j|r|e^{j\varphi} \\ -j|r|e^{-j\varphi} & e^{j\varphi} \end{bmatrix}$$

Transfer & scattering matrix

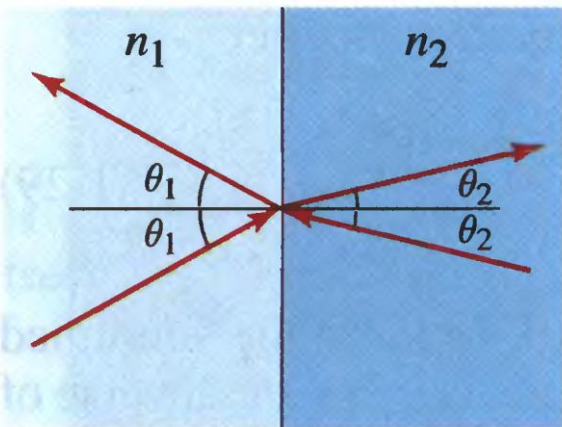
For example, at a single dielectric boundary

Using Fresnel equations,

$$\mathbf{S} = \begin{bmatrix} t_{12} & r_{21} \\ r_{12} & t_{21} \end{bmatrix} = \frac{1}{n_1 + n_2} \begin{bmatrix} 2n_1 & n_2 - n_1 \\ n_1 - n_2 & 2n_2 \end{bmatrix}$$

$$\mathbf{M} = \frac{1}{2n_2} \begin{bmatrix} n_2 + n_1 & n_2 - n_1 \\ n_2 - n_1 & n_2 + n_1 \end{bmatrix}$$

For off-axis case,



$$\mathbf{S} = \begin{bmatrix} t_{12} & r_{21} \\ r_{12} & t_{21} \end{bmatrix} = \frac{1}{\tilde{n}_1 + \tilde{n}_2} \begin{bmatrix} 2a_{12}\tilde{n}_1 & \tilde{n}_2 - \tilde{n}_1 \\ \tilde{n}_1 - \tilde{n}_2 & 2a_{21}\tilde{n}_2 \end{bmatrix}$$

$$\mathbf{M} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} = \frac{1}{2a_{21}\tilde{n}_2} \begin{bmatrix} \tilde{n}_1 + \tilde{n}_2 & \tilde{n}_2 - \tilde{n}_1 \\ \tilde{n}_2 - \tilde{n}_1 & \tilde{n}_1 + \tilde{n}_2 \end{bmatrix}.$$

$$\begin{array}{lll} \text{TE:} & \tilde{n}_1 = n_1 \cos \theta_1, & \tilde{n}_2 = n_2 \cos \theta_2, & a_{12} = a_{21} = 1, \\ \text{TM:} & \tilde{n}_1 = n_1 \sec \theta_1, & \tilde{n}_2 = n_2 \sec \theta_2, & a_{12} = \cos \theta_1 / \cos \theta_2 = 1/a_{21} \end{array}$$

Airy's formula using T-matrix

Two cascade systems distanced with homogeneous media.

$$\mathbf{M} = \begin{bmatrix} 1/t_1^* & r_1/t_1 \\ r_1^*/t_1^* & 1/t_1 \end{bmatrix} \begin{bmatrix} \exp(-j\varphi) & 0 \\ 0 & \exp(j\varphi) \end{bmatrix} \begin{bmatrix} 1/t_2^* & r_2/t_2 \\ r_2^*/t_2^* & 1/t_2 \end{bmatrix}$$

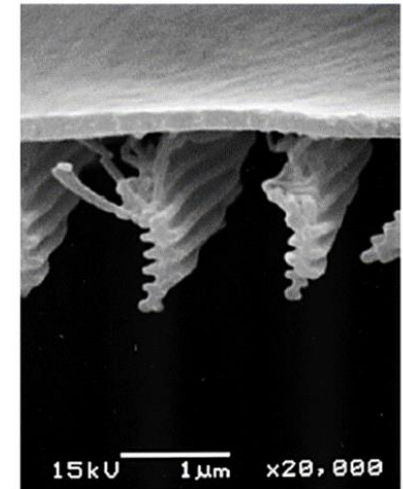
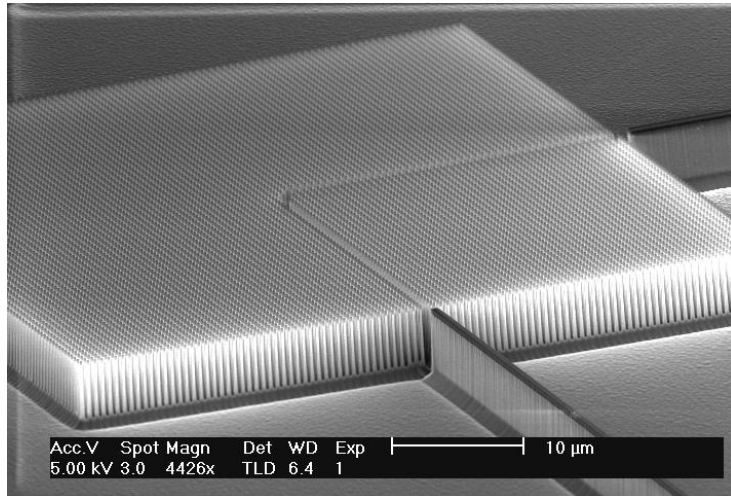
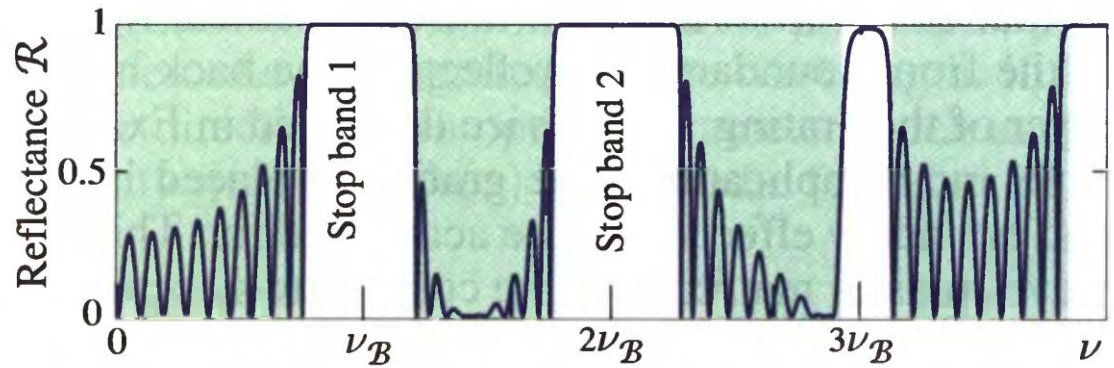
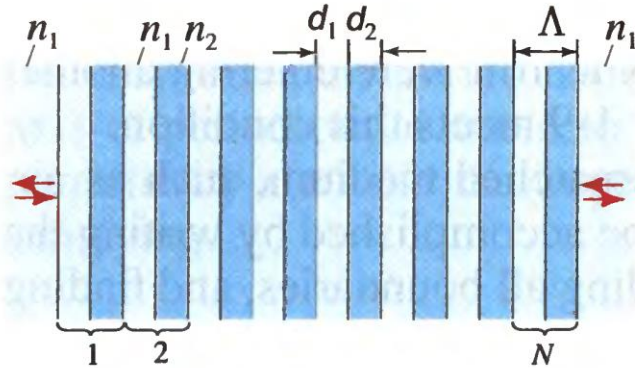
$$\mathbf{M} = \begin{bmatrix} 1/t_1^* & r_1/t_1 \\ r_1^*/t_1^* & 1/t_1 \end{bmatrix} \begin{bmatrix} 1/t_2^* \exp(-j\varphi) & r_2/t_2 \exp(-j\varphi) \\ r_2^*/t_2^* \exp(j\varphi) & 1/t_2 \exp(j\varphi) \end{bmatrix}$$

$$\mathbf{M}_{22} = \frac{1}{t_{total}} = -r_1 r_2 \exp(-j\varphi) / t_1 t_2 + \exp(j\varphi) / t_1 t_2 = \frac{1 - r_1 r_2 \exp(-j2\varphi)}{t_1 t_2 \exp(-j\varphi)}$$

$$t = \frac{t_1 t_2 \exp(-j\varphi)}{1 - r_1 r_2 \exp(-j2\varphi)}$$

Photonic crystals

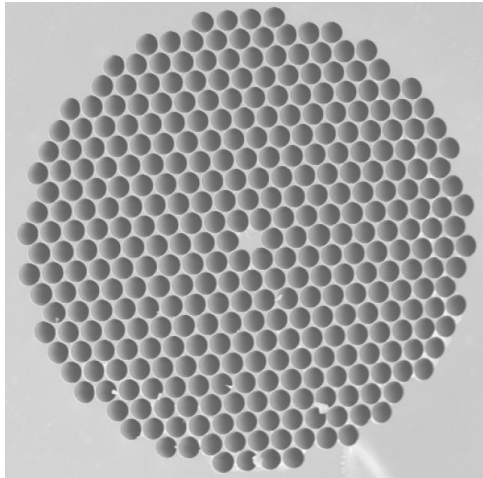
A photonic crystal is a periodic arrangement of a dielectric material that exhibits strong interaction with light



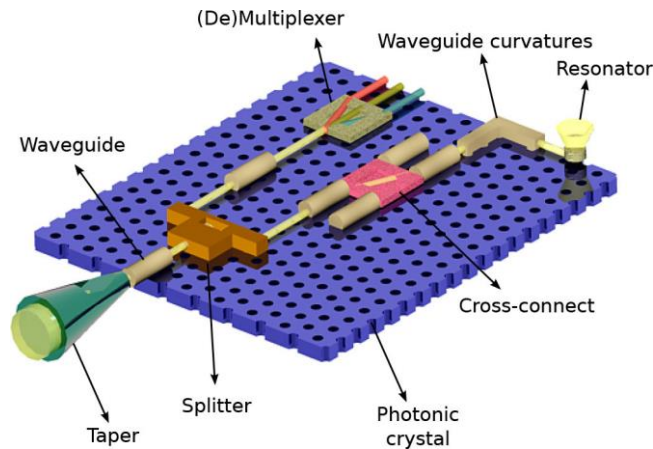
Zijlstra, van der Drift, De Dood, and Polman (DIMES, FOM)

Photonic crystals applications

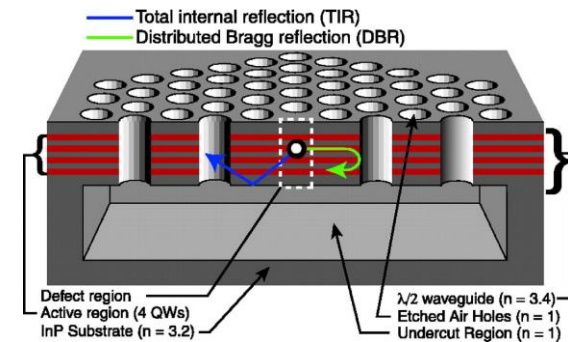
Photonic crystal fiber



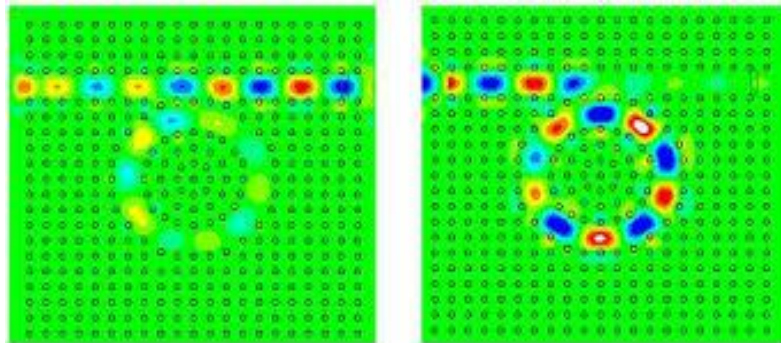
Integrated optics



Microcavity & laser



Photonic crystal ring resonator



Photonic crystal waveguides

