

The University of Texas at Austin
Mechanical Engineering Department
MODELING OF PHYSICAL SYSTEMS

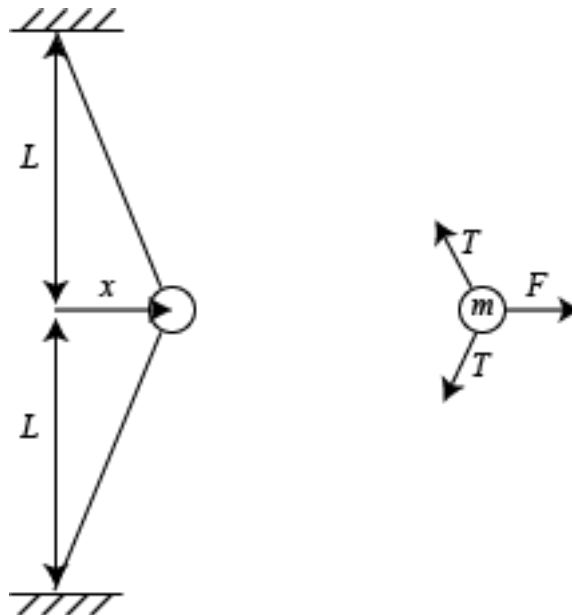
J.J. Beaman
Assigned 3/12/2022

ME 383Q.4
Assignment 4

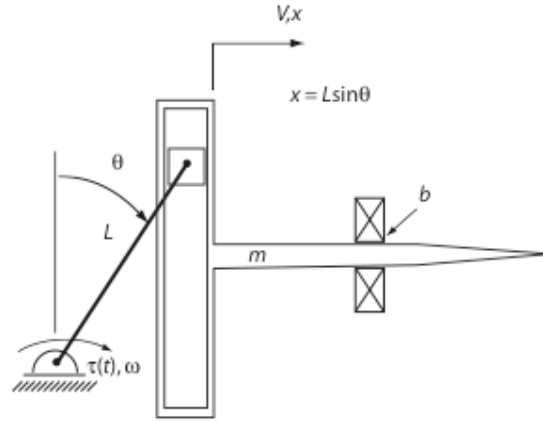
Spring 2022
Due 3/24/2022

Read Chapter 4.6, 4.7, 4.8, 6

1. Shown below is a mass m constrained by two equal extensible strings. The strings are put into a relatively constant tension by a vertical force T . There is a mass m between the two strings which can be pulled a distance x by a horizontal force F . The tension force T remains constant during this pull. The mass is pulled out a distance x_0 and released from rest.



- Derive nonlinear state equations for this mass string system in terms of distance x and mass momentum p .
 - Linearize the nonlinear state equations for a small value of $x = \delta x$.
 - For $L = 1$ m, $m = 0.1$ kg, and $T = 100$ N, simulate your nonlinear and linear state equations with $x_0 = .05, .1, .5$, and $x_0 = 1$ meters for time span of 1 sec. Comment on the accuracy of the linearized model with respect to initial distance pulled x_0 .
2. In a certain type of sewing machine, a scotch yoke mechanism is used to drive a reciprocating needle.
- Develop a bond graph model for this system (Use just the elements indicated by the parameters and the relations in the figure with torque input).
 - Obtain state equations for your system.



3. Read the material on the energy-saving hydraulic power supply in Doeblin.pdf.

(a) Develop a bond graph model of this system using the article's description.

Use the following variables in your model.

F_K = spring force A = piston area and transformer modulus

x = spring deflection Q_{piston} = piston volume flow τ_{Be} = motor friction torque

P = supply pressure Q_p = pump volume flow $T_l(t)$ = motor load torque

F_L = lever force Q_{pl} = pump leakage L = lever length

V_L = lever tip velocity $\omega_p(t)$ = pump angular velocity

F_p = piston force $d_p\phi = Q_p/\omega_p$ pump modulated transformer modulus

τ_L = lever torque τ_m = motor torque

h_ϕ = lever angular momentum Q_{ml} = motor leakage

ϕ = lever angle $d_m = \tau_m/P = Q_m/\omega_m$ motor transformer modulus

τ_B = lever friction torque ω_m = motor angular velocity

ω_L = lever angular velocity h_m = motor angular momentum

(b) Simulate your model with the following parameters

$J_i = .1$ in-lb-sec² pump angular inertia

$B_i =$ in-lb-sec pump angular damping

$K = 100$ lb/in spring constant

$L = 1$ in lever length

$K_{si} = KL^2$

$J_m = .043$ in-lb-sec² motor angular inertia

$B_m = 20$ in-lb-sec motor angular damping

$C_f = .0001$ lb/in⁵ or .001 lb/in⁵ pipe fluid compliance

$d_m = .486$ in³ transformer modulus

$d_p = 1.0$ in³/radian modulated transformer modulus

$A = .5$ in² piston area and transformer modulus

$K_{pl} = .0006$ in⁵/sec pump leakage loss coefficient

$\omega_p(t) = 180$ radian/sec pump angular velocity step input

$T_l(t) = 0$ in-lb motor load torque

$K_{ml} = .0004$ in⁵/sec motor leakage loss coefficient

(c) Develop a set of state equations from your bond graph.

(d) What is wrong with the state equations as given in this article?

(e) With $J_i = .1$, $L = 1$, $K = 100.$, $J_m = .043$, $B_m = 20$, $d_m = .486$, $d_p = 1$, $A = .5$, $K_{pl} = .0006$, $\omega_p = 180$, $T_l = 0$, and $K_{ml} = .0004$, perform a digital simulation with $B_i = 50$ and $C_f = .0001$.

Compare with the results from the article. Repeat for $B_i = 20$ and $C_f = .001$. Compare with the results from the article.