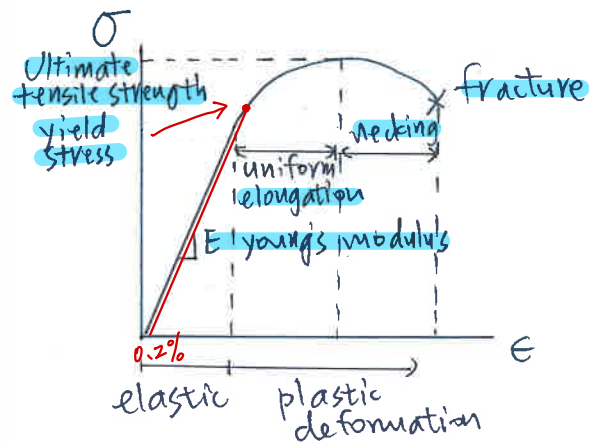


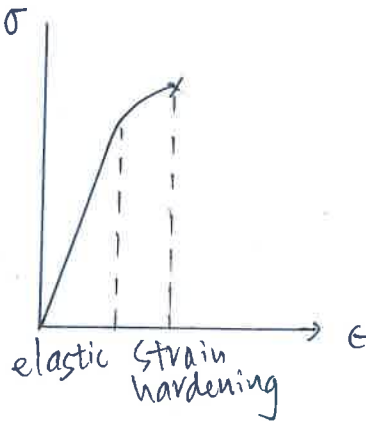
a)

- ① Football helmet : polycarbonate, Injection compression molding
- ② Coffee mug : ceramic, casting (investment casting)
- ③ Lego : ABS, IM
- ④ Bottle : PET, blow molding
- ⑤ Dreamliner fuselage : Carbon fiber reinforced polymer (composite) extrusion
- ⑥ Turbine blade : Ni-alloy, casting (engine blade - die casting)
- ⑦ Toothbrush grip : rubber, IM (CO)
- ⑧ Bumper of car : polycarbonate, reaction-IM
- ⑨ Apple notebook case : Al, CNC

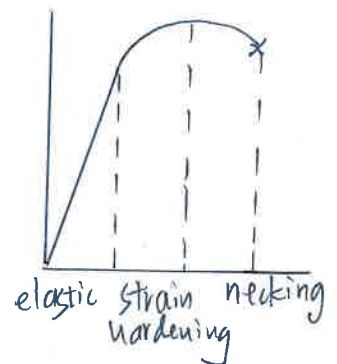
stress-strain curve



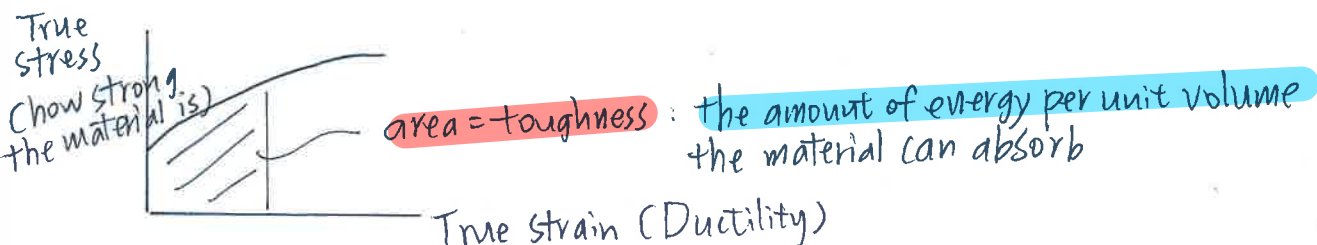
Brittle material



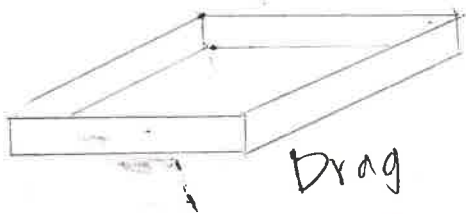
Ductile material



True stress - True strain curve



Sand Casting

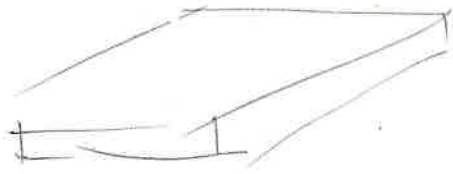


(Drag)

Put pattern into the box.
then sand.



(Cope)



(cope → pattern → sand
(box)

insert gate, sprues → pour metal into mold

- Pros:**
- no limit in size
 - almost all metals (variety of metals)
 - low cost, reuse sand
 - expendable mold, reusable pattern

Cons: not precise

Die casting - Permanent mold (no pattern) usually metal mold

- mold cost high, but can be reuse
- rapid high production for simple or complex, thin wall, precision parts
- usually small to moderate in size
- non-ferrous metals (Fe)
x
- can produce multiple parts
- < Hot chamber - low melting temp. materials - plunger
Cold chamber - higher melting materials - feed system

Cons: x large part
high die cost

x for very high melting metals and alloy

Investment Casting - expendable mold, expendable pattern

- mold: ceramic
- pattern: wax (made by IM)
- takes time. expensive process

Part molded in wax → attach runner → dip in wet ceramic slurry
→ drying → heat → molten metal → break ceramic mold

Pros: complex shape, close tolerance, thin wall.
Smooth finishes

CNC

precise, speed, repeatable

(Pros)

1. continuous use (no need to shut down)
2. consistency
3. less staff
4. update software can improve machine performance
5. Training, no degrees needed

(Cons)

1. cost more
2. expensive
3. maintenance

IM

pros: fast production
low labor cost
multiple materials
low production cost.

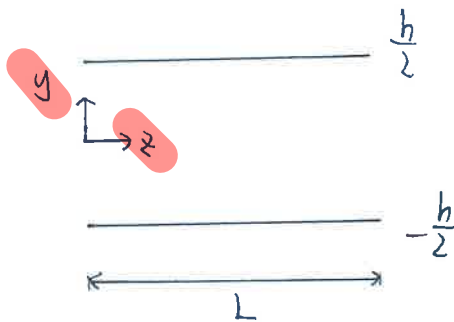
cons: expensive mold
some design restriction

AM

pros: - not only rapid prototyping, but have good mechanical properties
- can be post processed
- moving assemblies

cons: resolution
support structure
small voids

Slit



$$\mu \frac{d^2 u_z}{dy^2}$$

$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} = 0 \rightarrow u_z(z) = 0$$

$$0 = -\frac{\partial P}{\partial z} + \mu \left(\frac{d^2 u_z}{dy^2} \right) \rightarrow \frac{\partial P}{\partial z} = \mu \left(\frac{d^2 u_z}{dy^2} \right)$$

$$\frac{d^2 u_z}{dy^2} = \frac{1}{\mu} \cdot \frac{\partial P}{\partial z}$$

$$\frac{\partial u_z}{\partial y} = \frac{1}{\mu} \cdot \frac{\partial P}{\partial z} \cdot y + C_1$$

$$u_z(y) = \frac{1}{\mu} \cdot \frac{\partial P}{\partial z} \cdot \frac{y^2}{2} + C_1 y + C_2$$

BCs: ① $y = +\frac{h}{2}$, $u_z = 0 \rightarrow 0 = \frac{1}{\mu} \cdot \frac{\partial P}{\partial z} \cdot \frac{h^2}{8} + C_2 \rightarrow C_2 = -\frac{1}{\mu} \cdot \frac{\partial P}{\partial z} \cdot \frac{h^2}{8}$

② $y = 0$, $\frac{\partial u_z}{\partial y} = 0 \rightarrow C_1 = 0$

$$u_z(y) = \frac{1}{\mu} \cdot \frac{\partial P}{\partial z} \cdot \left(\frac{y^2}{2} - \frac{h^2}{8} \right)$$

$$\frac{1}{h/2} \int_0^{h/2} u_z(y) dy$$

$$\bar{u}_z = \frac{1}{h/2} \int_0^{h/2} u_z(y) dy$$

$$= \frac{2}{h} \left(\frac{1}{6\mu} \cdot \frac{\partial P}{\partial z} \cdot y^3 - \frac{\partial P}{8\mu L} \cdot y h^2 \right) \Big|_{y=0}^{h/2}$$

$$= \frac{2}{h} \left(\frac{\partial P}{6\mu L} \cdot \frac{h^3}{8} - \frac{\partial P}{8\mu L} \cdot \frac{h^3}{2} \right) = \frac{h^2 \partial P}{12\mu L \partial z}$$

$$Q = L \cdot h \cdot \bar{u}_z = L \cdot h \cdot \frac{h^2 \partial P}{12\mu L} = \frac{h^3 \partial P}{12\mu}$$

Pressure Driven Flow Through a Slit - Cont'd

Continuity equation: $u_x = 0$ $u_y = 0$

$$\frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} = \frac{du_z}{dz} = 0$$

Momentum equations:

Table 2.4: Navier-Stokes Equations

Cartesian Coordinates (x, y, z) :

$$\rho \left(\frac{\partial u_x}{\partial t} + u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} + u_z \frac{\partial u_x}{\partial z} \right) = -\frac{\partial p}{\partial x} + \mu \left[\frac{\partial^2 u_x}{\partial x^2} + \frac{\partial^2 u_x}{\partial y^2} + \frac{\partial^2 u_x}{\partial z^2} \right] + \rho g_x \rightarrow \frac{\partial p}{\partial x} = 0$$

$$\rho \left(\frac{\partial u_y}{\partial t} + u_x \frac{\partial u_y}{\partial x} + u_y \frac{\partial u_y}{\partial y} + u_z \frac{\partial u_y}{\partial z} \right) = -\frac{\partial p}{\partial y} + \mu \left[\frac{\partial^2 u_y}{\partial x^2} + \frac{\partial^2 u_y}{\partial y^2} + \frac{\partial^2 u_y}{\partial z^2} \right] + \rho g_y \rightarrow \frac{\partial p}{\partial y} = 0$$

$$\rho \left(\frac{\partial u_z}{\partial t} + u_x \frac{\partial u_z}{\partial x} + u_y \frac{\partial u_z}{\partial y} + u_z \frac{\partial u_z}{\partial z} \right) = -\frac{\partial p}{\partial z} + \mu \left[\frac{\partial^2 u_z}{\partial x^2} + \frac{\partial^2 u_z}{\partial y^2} + \frac{\partial^2 u_z}{\partial z^2} \right] + \rho g_z$$

Steady state: u_x independent of x

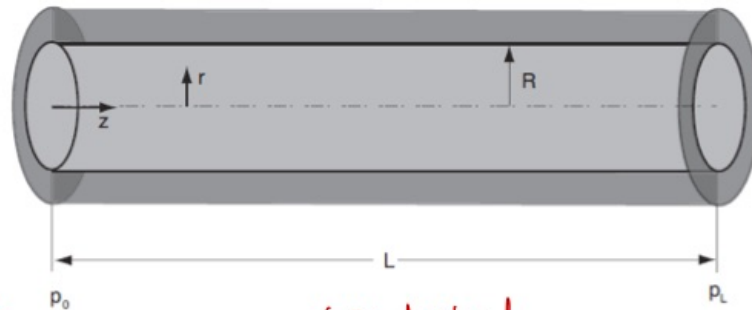
Fully developed flow: u_z independent of z

Fully developed flow: u_z independent of z

Body force negligible

Tube

4. Tube flow is encountered in several material manufacturing processes. Let's assume that the flow inside the tube is steady, fully developed, and is axis-symmetric. Furthermore, it has no entrance effects, the gravitational force is negligible, and the fluid is a Newtonian fluid. Based on the momentum equation in the z direction, simplify it and then solve for the velocity profile, $u_z(r)$ and the volumetric flow rate, Q .



$$u_r = u_\theta = 0$$

Steady State fully developed

$$\rho \left(\cancel{\frac{\partial u_z}{\partial t}} + u_r \cancel{\frac{\partial u_z}{\partial r}} + \frac{u_\theta}{r} \cancel{\frac{\partial u_z}{\partial \theta}} + u_z \cancel{\frac{\partial u_z}{\partial z}} \right) = \text{axis-symmetry } g \text{ force negligible}$$

$$-\frac{\partial p}{\partial z} + \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_z}{\partial r} \right) + \frac{1}{r^2} \cancel{\frac{\partial^2 u_z}{\partial \theta^2}} + \cancel{\frac{\partial^2 u_z}{\partial z^2}} \right] + \cancel{\rho g_z}$$

fully developed

$$\frac{\partial p}{\partial z} = \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_z}{\partial r} \right) \right]$$

$$u_z = \frac{\partial p}{\partial z} \frac{1}{4\mu} (R^2 - r^2)$$

$$\frac{\partial}{\partial r} \left(r \frac{\partial u_z}{\partial r} \right) = \frac{r}{\mu} \frac{\partial p}{\partial z}$$

$$Q = \int_0^R 2\pi r \left(\frac{\partial p}{\partial z} \cdot \frac{1}{4\mu} (R^2 - r^2) \right) dr$$

$$r \frac{\partial u_z}{\partial r} = \frac{1}{2} \frac{r^2}{\mu} \frac{\partial p}{\partial z} + C_1 \quad (1)$$

$$= \frac{\partial p}{\partial z} \frac{\pi R^4}{8\mu}$$

$$\frac{\partial u_z}{\partial r} = \frac{1}{2} \frac{r}{\mu} \frac{\partial p}{\partial z} + \frac{C_1}{r}$$

$$= \frac{\pi R^4}{8\mu} \frac{\Delta p}{L}$$

$$u_z = \frac{1}{4} \frac{r^2}{\mu} \frac{\partial p}{\partial z} + C_1 \ln r + C_2 \quad (2)$$

$$(1) \quad r = R, \quad u_z = 0 \quad C_2 = \frac{R^2}{4\mu} \frac{\partial p}{\partial z}$$

$$(2) \quad r = 0, \quad u_z = 0 \quad C_1 = 0$$