EE3015 (Power Systems & Protection)

Tutorial 1/Week 2 (PU System I)

1.1 A 3-phase generator rated 100 MVA, 13.2 kV, X = 20% is connected through a Δ/Y transformer to a transmission line whose series reactance is 40 ohms per phase. Assume that the base values in the line circuit are 200 MVA and 115 kV.

(a) Find the pu reactance of the transmission line.

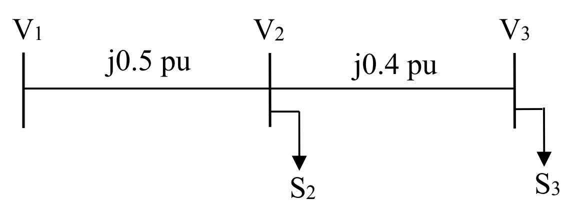
(b) Find the generator and transformer reactances in pu for the following cases:

(i) The transformer is a 3-phase unit rated 100MVA, 13.8Δ/120Y kV, X = 8%.

(ii) The transformer is composed of three single-phase units, each rated 35 MVA, 13.8/69 kV, X = 8%.

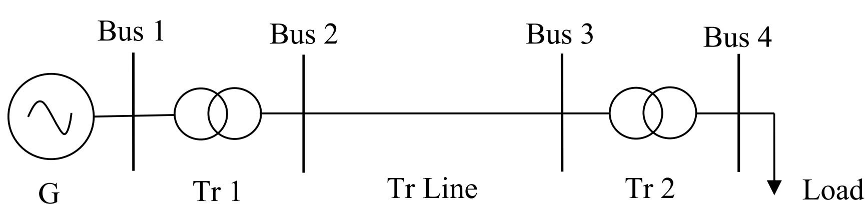
Ans.: (a) 0.6049 pu; (b) (i) 0.3985 pu, 0.1742 pu; (ii) 0.3952 pu, 0.1646 pu

1.2 The one-line diagram of a three-phase power system is shown below; impedances marked are in per unit on a 100-MVA, 400-kV base. Given that loads $S_2 = (15.93 - j33.4)$ MVA, and $S_3 = (77 + j14)$ MVA, and that the voltage at bus 3 is maintained at 400 kV, determine the magnitude of the voltage at bus 1.



Ans.: 480 kV

1.3 Obtain the impedance diagram in per unit for the system shown below. Assume a base of 200 MVA, 11 kV in the generator circuit. Without modeling the generator, and given that the transmission line X = 50 ohms and R = 2.5 ohms; transformer ratings for Tr 1 are 50 MVA, 11/132 kV, X = 12%, R = 2%, and the corresponding Tr 2 values are 40 MVA, 132/33 kV, X = 10%, R = 1%. The load connected at bus 4 is 40 MW at 0.8 pf lag, at a voltage of 30 kV.



Ans.: $Z_{Tr\,1} = 0.08 + j0.48$ pu, $Z_{Line} = 0.029 + j0.574$ pu, $Z_{Tr\,2} = 0.05 + j0.50$ pu, $Z_{load} = 3.305\angle 36.8°$ pu

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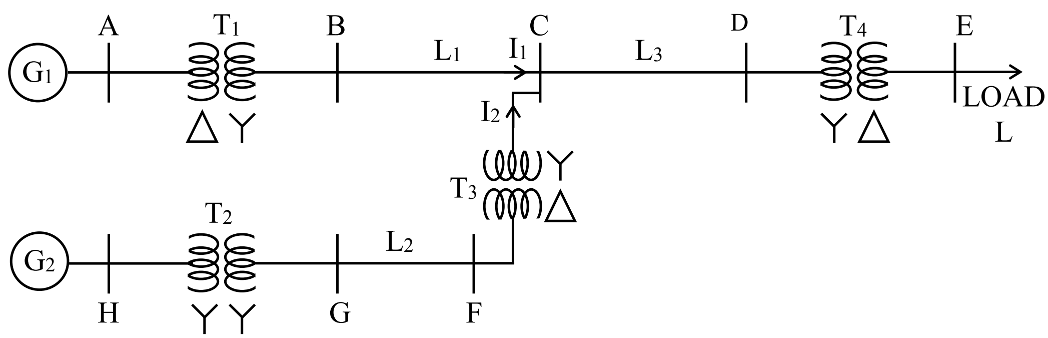
Tutorial 2/Week 3 (PU System II)

2.1 The single line diagram of a three-phase power system shown below has the following component ratings:

Generator G_1: 12 kV, 50 MVA, X = 8%
Generator G_2: 12 kV, 40 MVA, X = 8%
Transformer T_1: three single-phase units, each rated 13/80 kV, 15 MVA, X = 9%
Transformer T_2: three single-phase units, each rated 6.9/39.8 kV, 25 MVA, X = 8%
Transformer T_3: three single-phase units, each rated 70/80 kV, 25 MVA, X = 13%
Transformer T_4: 12/138 kV, 80 MVA, X = 12%
Line L_1: X = 30 Ω/phase; Line L_2: X = 30 Ω/phase; Line L_3: X = 50 Ω/phase
Load L: 60 MW, 0.9 pf lag at 11 kV (resistance and reactance in series)



(a) Selecting bases of 100 MVA and 140 kV in line L_3, draw the per unit impedance diagram. Clearly mark the values of all impedances on this diagram.

(b) Assume that current phasors I_1 and I_2 are equal when load L is drawing 60 MW at 0.9 pf lag and 11 kV. Calculate the magnitude of the voltage at the terminals of each generator of the system.

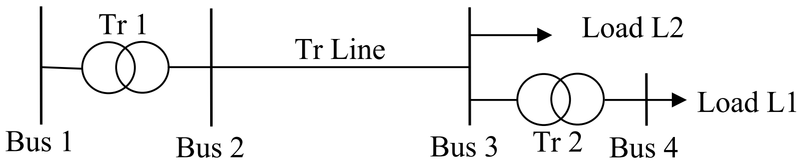
Ans: (a) G_1: j0.1335, G_2: j0.1916, L_1: j0.1531, L_2: j0.5998, L_3: j0.2551, T_1: j0.1959, T_2: j0.1013, T_3: j0.1698, T_4: j0.1457, Z_L = 1.1022 + j0.5338; (b) V_1: 15.1527 kV, V_2: 15.9066 kV

2.2 The single line diagram of a 3-phase power system shown below has the following component ratings:

T. Line X = 7.2 Ω/phase; R = 1.5 Ω/phase
Load L1: Y-connected R = 32 Ω/phase
Load L2: 4 MW, 0.8 pf lag, 22 kV
Tr 1: 10 MVA, 230/22 kV, Z = (2 + j8)%
Tr 2: 5 MVA, 22/12 kV, Z = (1.2 + j6)%

(a) Sketch the impedance diagram of the power system showing all quantities in pu. Assume 10 MVA and 22 kV as base values in the transmission line circuit.

(b) If the voltage at Bus 3 is maintained at 22 kV, calculate the voltages at Buses 2 and 1.



Ans.: (a) Tr 1: 0.02 + j0.08, Tr Line: 0.0309 + j0.1488, Tr 2: 0.024 + j0.12, Z_{L1} = 2.222, $Z_{L2} = 2\angle 36.87°$; (b) V(Bus2) = 23.77 kV, V(Bus1) = 260.12 kV

2.3 The single-line diagram of a 3-phase power system is shown below. The component ratings are as follows:

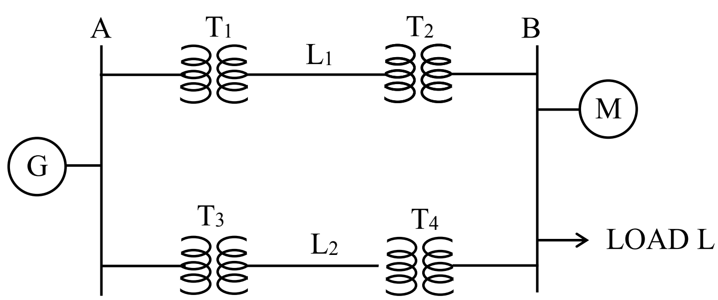
Generator G: 90 MVA, 22 kV, X = 18%
Transformer T1: 50 MVA, 220/22 kV, X = 10%
Transformer T2: 40 MVA, 11/220 kV, X = 6%
Transformer T3: 40 MVA, 110/22 kV, X = 6.4%
Transformer T4: 40 MVA, 11/110 kV, X = 8%
Synchronous motor M: 66.5 MVA, 10.45 kV, X = 18.5%
Load L: 57 MVA, 0.6 pf lag, 10.45 kV (R & X in series)
Line L1: X = 48.4 ohms per phase
Line L2: X = 65.43 ohms per phase

(a) Selecting a base of 100 MVA and 22 kV in the generator circuit, sketch the per unit impedance diagram of the system (with all values in per unit).

(b) Assuming that the motor M operates at full-load 0.8 pf leading at a terminal voltage of 10.45 kV, find

(i) the voltage at the generator bus

(ii) the generator and motor internal emfs.



Ans.: (a) G: j0.2, T_1: j0.2, L_1: j0.1, T_2: j0.15, T_3: j0.16, L_2: j0.5407, T_4: j0.2, M: j0.2511, Z_L = 0.95 + j1.267; (b) (i) 22.145 kV; (ii) 23.817 kV, 11.713 kV

EE3015 (Power Systems & Protection)

Tutorial 3/Week 4 (Synchronous Generators I)

3.1 A three-phase, 125-MVA, 0.8 pf (lag), 13.2-kV, 1800-rpm synchronous generator has a synchronous reactance of 1.7 Ω per phase and negligible stator resistance.

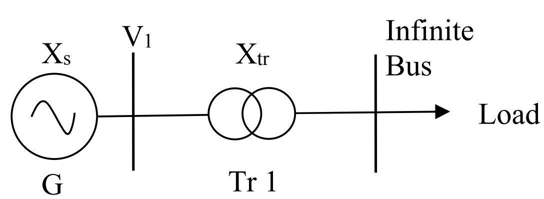
(a) If the machine is connected to an infinite bus operating at 13.2 kV, and it delivers 100 MW at unity power factor, find the magnitude of the generated voltage, the power angle, and the reactive power.
(b) Assume that the prime mover input to the generator of part (a) is reduced by 50% without changing the excitation. Find the new operating conditions.
(c) Starting at the condition of part (a), assume that the excitation is adjusted to provide 100 MW at 0.8 pf leading. Evaluate the new operating conditions.
(d) Sketch a single phasor diagram to depict the three operating conditions in parts (a) – (c).

Ans.: (a) 18.442 kV, 44.295°, 0; (b) 20.437°, 31.687 Mvar produced by the generator; (c) 13.357 kV, 74.63°, 75 Mvar absorbed by the generator

3.2 A three-phase Y-connected synchronous generator has a synchronous reactance of 10 ohms and negligible armature resistance. At unity power factor the generator supplies 188 A to a 13.2-kV infinite bus. When the generator excitation is increased by 25%, without changing the mechanical power input, determine the generator line current and power factor. Use the per unit system for your calculations. Sketch a phasor diagram to show the two operating conditions.

Ans.: 275.15 A, 0.683 lag

3.3 A 120-MVA, 22-kV synchronous generator has X_s = 1.16pu. The generator supplies power to a large power system (Infinite bus) through a 150 MVA, 22/345 kV, X_{tr} = 0.06 pu transformer, as shown below.



(a) Determine the induced emf and the terminal voltage of the generator when the load supplied to the infinite bus is 80 MW at 0.8 pf leading, at the rated voltage of 345 kV.

(b) If the generator excitation is increased by 20% while supplying the constant load of 80 MW, calculate:

(i) the generator terminal voltage

(ii) the reactive power output of the generator at its terminals, and
(iii) the reactive power delivered to the infinite bus.

(c) Determine the maximum real powers the generator can supply to the infinite bus at the excitation levels in (a) and (b) respectively. In addition, find the power factors of the load at the infinite bus while delivering these maximum powers.

Ans.: (a) 19.743 kV, 21.4835 kV; (b) 21.762 kV, 25.43 Mvar absorbed by the generator, 28.31 Mvar flowing towards the transformer; (c) 89.146 MW, 0.6678 lead, 106.975 MW, 0.7328 lead

EE3015 (Power Systems & Protection)

Tutorial 4/Week 5 (Synchronous Generators II)

4.1 A 24-MVA, 17.32-kV, 60-Hz, Y-connected, 3-phase synchronous generator has a synchronous reactance of 5 ohms per phase, and negligible armature resistance.

(i) At a certain excitation, the generator delivers rated MVA at 0.8 power factor lagging, to an infinite bus operating at 17.32 kV. Determine the magnitude of the internal emf per phase and the power angle of the generator.
(ii) The internal emf and terminal voltage are maintained constant at 13.4 kV/phase and 10 kV/phase respectively. What is the maximum three-phase real power this generator can develop before it pulls out of synchronism? What are the armature current and reactive power under this condition?

Ans.: (i) 12.806 kV, 14.47°; (ii) 80.4 MW, 3344.106 A, 60 MVar absorbed by the generator

4.2 Two generators, rated 3 MW each, are operating in parallel to supply a total load of 4 MW at 0.8 pf (lag). The generators have no-load frequencies of 52 Hz and 51 Hz respectively. The frequencies of both generators fall to 49 Hz at full load.

(a) What is the system frequency and how much power is supplied by each generator?

(b) Find the pf of the second generator if the first generator is operating at 0.85 (lag).

(c) Determine the no-load frequency setting of the second generator to bring the system back to 50 Hz at this load.

Ans.: (a) 49.8 Hz, 2.2 MW, 1.8 MW; (b) 0.74 lag; (c) 51.33 Hz

4.3 A 480-V, 200-kW, 2-pole, 3-phase, 50-Hz synchronous generator's prime mover has a no-load speed of 3040 rpm, and a full-load speed of 2975 rpm. It is operating in parallel with a 480-V, 150-kW, 4-pole, 3-phase, 50-Hz synchronous generator whose prime mover has a no-load speed of 1500 rpm, and a full-load speed of 1485 rpm. The total load supplied by the two generators is 200 kW at 0.85 pf lagging.

(a) Find the operating frequency of the power system.

(b) Find the power being supplied by each of the two generators.

Ans.: (a) 49.843 Hz; (b) 153 kW, 47 kW

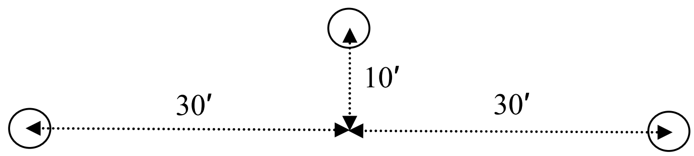
4.4 Two three-phase, 6.6-kV, Y-connected synchronous generators operating in parallel supply a load of 3 MW at 6.6 kV and 0.8 pf lagging. The synchronous impedances of the machines A and B are (0.5 + j10) Ω and (0.4 + j12) Ω respectively. The excitation of machine A is adjusted so that it delivers 150 A at a lagging pf, and the governors of the two machines are so set that the load (real power) is shared equally between the machines. Determine the armature current of the second machine, and also the power factor, internal voltage and power angle of each machine. Sketch a phasor diagram showing all currents and voltages.

Ans.: 180.63 A, 0.8747 lag, 8.274 kV, 15.49˚, 0.7264 lag, 9.640 kV, 15.90˚

EE3015 (Power Systems & Protection)

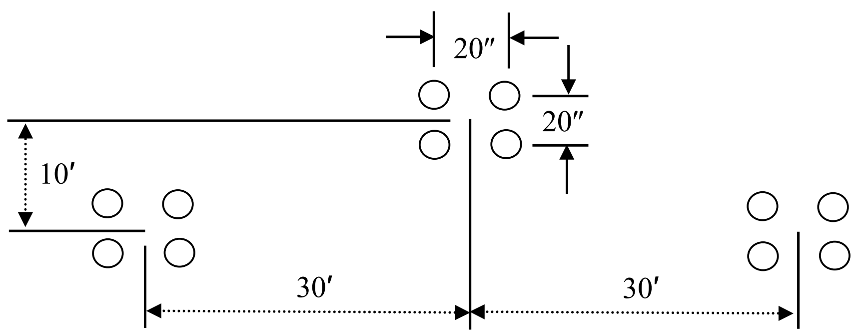
Tutorial 5/Week 6 (Transmission Lines)

5.1(a) A three-phase transmission line consisting of stranded ACSR conductors is shown below. Given that the system frequency is 50 Hz, R = 0.1204 ohms/mile, GMR = 0.0403 ft, conductor diameter = 1.196 inches, calculate the resistance, inductance, series reactance, capacitance, and shunt admittance per km of the line.



Ans.: 0.0748 Ω; 1.3758 mH; 0.432 Ω; 0.008341 μF to neutral; j2.62 μS

5.1(b) Each phase of the line in part (a) above consists of a bundle of 4 stranded conductors as shown below. Find the new R, L, X, C and Y for the line.



Ans.: 0.0187 Ω, 0.8002 mH, 0.2514 Ω, 0.01409 μF, j4.43 μS

5.2 A three-phase transposed transmission line is composed of one ACSR conductor per phase with flat horizontal spacing of 11 m between adjacent conductors. The conductors have a diameter of 3.625 cm and a GMR of 1.439 cm each. The line is to be replaced by a 3-conductor bundle of ACSR conductors having a diameter of 2.1793 cm and a GMR of 0.8839 cm each. The replaced line will also have a flat horizontal configuration, but it is to be operated at a higher voltage and therefore the phase spacing is increased to 14 m between adjacent bundles. The spacing between the conductors in the bundle is 45cm ($\varepsilon = 8.85 \times 10^{-12}$ F/m).

Determine:

(i) the percentage change in the line inductance, and
(ii) the percentage change in the line capacitance.

Ans.: (i) 27.53% (decrease); (ii) 35.25% (increase)

5.3 A 3-phase, 765-kV, 60-Hz transmission line is composed of four ACSR conductors per phase with a flat horizontal spacing of 14 m between adjacent conductors. The conductors have a diameter of 3.625 cm, and a GMR of 1.439 cm. The bundle spacing is 45 cm, and the line is 400 km long. Assume the line to be lossless and model it as a nominal-π equivalent with base values of 765 kV and 2000 MVA ($\varepsilon = 8.85 * 10^{-12}$ F/m).

(a) Determine the receiving-end voltage, current and complex power when 1920 MW and 600 MVar (lag) are being transmitted at 765 kV at the sending end.

(b) If the line is energized with 765 kV at the sending end when the load at the receiving end is removed, what will be the receiving-end voltage?

Ans.: (a) 654.86 kV, 1732.31 A, 1920 MW, 417.64 Mvar (lag), 1964.86 MVA; (b) 877.39 kV

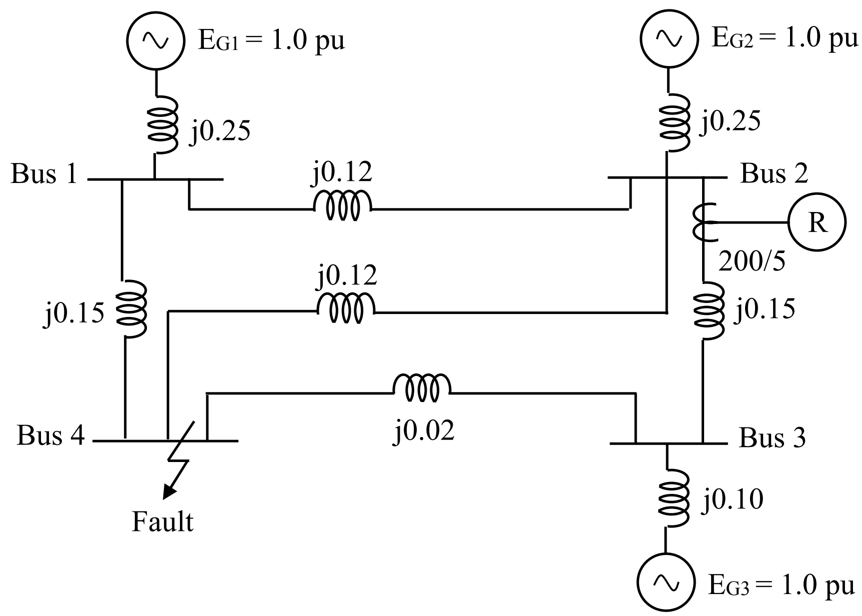
EE3015 (Power Systems & Protection)

Tutorial 6/Week 7 (Z_{Bus} Matrix and Shunt Compensation)

6.1 The figure below shows a 4-bus power system where all the pu values are based on 33 kV, 100 MVA bases.

(a) Form the bus admittance matrix for the system.

(b) Find the total fault current, the voltages at all the buses and the fault currents in all the lines, for a 3-phase fault at Bus 4 (as shown). Assume that the voltage throughout the network is 1.0 pu before the fault. The impedance matrix for the system is given below.



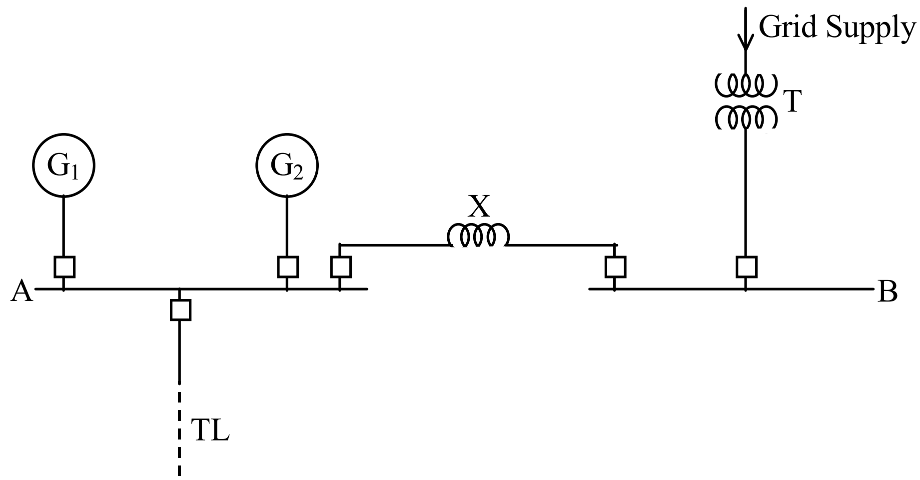
$$Z_{Bus} = j\begin{bmatrix} 0.0929 & 0.0532 & 0.0416 & 0.0483 \\ 0.0532 & 0.08 & 0.0467 & 0.0517 \\ 0.0416 & 0.0467 & 0.0647 & 0.06 \\ 0.0483 & 0.0517 & 0.06 & 0.0731 \end{bmatrix}$$

Ans.: (a) $Y = -j\begin{bmatrix} 19 & -8.33 & 0 & -6.67 \\ -8.33 & 27.33 & -6.67 & -8.33 \\ 0 & -6.67 & 66.67 & -50 \\ -6.67 & -8.33 & -50 & 65 \end{bmatrix}$;

(b) $I_f = 23.934$ kA, $V_1 = 11.2$ kV, $V_2 = 9.66$ kV, $V_3 = 5.91$ kV, $I_{12} = 0.679$ kA, $I_{14} = 3.957$ kA, $I_{23} = 1.324$ kA, $I_{24} = 4.267$ kA, $I_{34} = 15.676$ kA

6.2 Consider the three-phase power system shown below. Generators G_1 and G_2 are connected in parallel to a 30-kV busbar A. The ratings of G_1 and G_2 are 100 MVA, 30 kV, X = 20% and 50 MVA, 30 kV, X = 15% respectively. Busbar A feeds a transmission line TL. A grid supply is connected to the station busbar B through a transformer T rated for 500 MVA, 400/30 kV, X = 20%.

Determine the reactance (in ohms) of a current limiting reactor X to be connected between the grid system (busbar B) and the 2-generator busbar (busbar A) such that the short-circuit MVA at bus A does not exceed 1250 MVA.



Ans.: 1.8 ohms

6.3 A feeder from a distribution transformer is 500 feet long. It consists of three wires having an impedance of 0.052 + j0.069 ohms per 1,000 feet and current capacity of 225 amps. The three-phase load is balanced and draws 120 kW at 440 volts with a 60% lagging power factor.

(a) Determine the kVA rating of capacitors capable of correcting the power factor to allow rated current to flow in the feeder.
(b) Draw the phasor diagram of the feeder current before and after power factor correction and compute the new power factor.
(c) Determine the voltage at the sending end of the feeder.
(d) Determine the voltage regulation of the feeder.

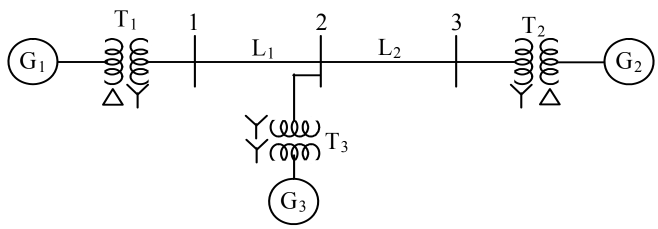
Ans.: (a) 37.513 kVA; (b) 0.7 lag; (c) 456.7 V; (d) 4.49%

Extra Problems

1. The single-line diagram of an unloaded three-phase power system is shown below. The component ratings are as follows:

   Generator G_1: 20 MVA, 13.8 kV, X = 0.2pu
   Generator G_2: 30 MVA, 18 kV, X = 0.2pu
   Generator G_3: 30 MVA, 20 kV, X = 0.2pu
   Transformer T_1: 25 MVA, 220Y/13.8Δ kV, X = 10%
   Transformer T_2: 3 single-phase units, each rated 10 MVA, 127/18 kV, X = 10%
   Transformer T_3: 35 MVA, 220Y/22Y kV, X = 10%
   Line L_1: j80 Ω per phase; Line L_2: j100 Ω per phase

   Draw the per unit impedance diagram using 50 MVA, 13.8 kV bases in the circuit of generator G_1. Clearly mark all impedance values on the diagram.



   Ans.: G_1: j0.5, T_1: j0.2, L_1: j0.0826, L_2: j0.1033, T_2: j0.1667, G_2: j0.3332, T_3: j0.1428, G_3: j0.2755

2. Two three-phase, Y-connected synchronous generators have per-phase generated voltages of $120\angle 10°$ V and $120\angle 20°$ V under no load, and reactances of j5 ohms/phase and j8 ohms/phase, respectively. They are connected in parallel to a load impedance of (4+j3) ohms/phase. Determine

   (a) the per-phase terminal voltage
   (b) the armature current of each generator
   (c) the power supplied by each generator, and
   (d) the total power output.

   Ans.: (a) 82 V/ph; (b) $I_{a1} = 9.36\angle -51.17°$ A, $I_{a2} = 7.31\angle -32.06°$ A; (c) P_{G1} = 1624 W, P_{G2} = 1617 W; (d) 3241 W

3. A 500-kVA, 2300-V, three-phase, Y-connected synchronous generator is operated at its rated speed to obtain its rated voltage on no-load. When a short-circuit is established, the phase current is 150 A. The average resistance of each phase is 0.5 ohms.

   (a) Determine the synchronous reactance in ohms per phase.
   (b) Using the per unit system, determine the percentage regulation when the generator delivers 500 kVA at its rated voltage and 0.8 pf lagging.

Ans.: 8.84ohms, 66.67%

4. A 3-phase, 345-kV, 50-Hz, 96 km long transmission line has a series impedance of (0.21 + j0.85) ohms/km. The load at the receiving end draws 120 MW at the rated voltage. Calculate the following for each of the three conditions (1) 0.8 pf lag, (2) unity pf, and (3) 0.8 pf lead:

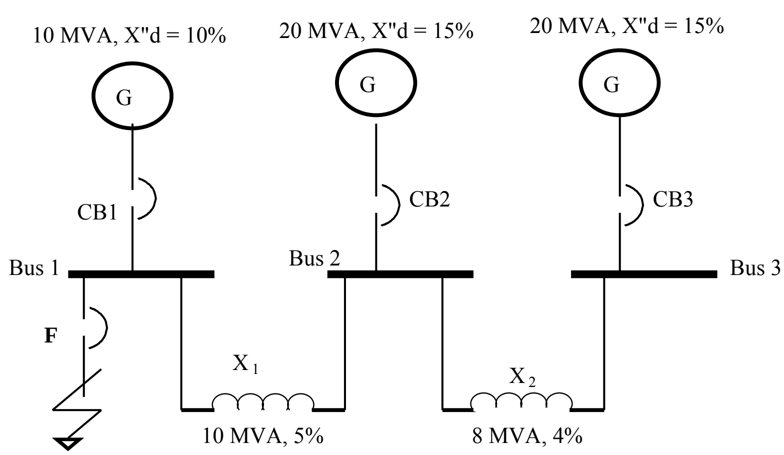
   (a) The sending end voltage.
   (b) The sending end real and reactive powers.
   (c) The real power loss in the line.
   (d) Sketch the phasor diagrams for cases (1), (2) and (3).

   Ans.: (1) 374 kV, 123.81 MW, 105.4 MVar, 3.81 MW; (2) 353.1kV, 122.43MW, 9.9MVar, 2.43MW; (3) 332.4kV, 123.81MW, -74.6MVar, 3.81MW

5. A 3-phase synchronous generator is rated 50 MVA, 13.2 kV, 0.8 pf lagging, and has a synchronous reactance of 20%. The generator is connected to a 60 MVA, 13.4/138 kV, 3-phase transformer having a reactance of 15%. The generator is initially operating on no load and at rated terminal voltage. A 3-phase symmetrical fault occurs on the high-voltage terminals of the transformer. Determine the short-circuit current supplied by the generator and its terminal voltage.

   Ans.: 6650.9 A, 5.17 kV

6. Three generators are interconnected through fault-current-limiting reactors as shown below. If the busbar line-to-line voltage is 11 kV, calculate the fault level and the fault current for a 3-phase symmetrical fault at F. Assume a base MVA of 20 MVA.



   Ans.: 203.23 MVA, 10.67 kA

Apr/May 2016

Q1 Ans.: (a) X_{G1} = 0.3 pu, X_{G2} = 0.1098 pu, X_M = 0.4 pu, X_{T1} = 0.1333 pu, X_{T2} = 0.08 pu, X_{T3} = 0.24 pu, , X_{12} = 0.6826 pu, X_{13} = 0.4201 pu, X_{23} = 0.5251 pu; (b) Y_{11} = -j6.1531 pu, Y_{22} = -j8.6382 pu, Y_{33} = -j5.8474 pu, $Y_{12} = Y_{21}$ = j1.4649 pu, $Y_{13} = Y_{31}$ = j2.3805 pu, $Y_{23} = Y_{32}$ = j1.9044 pu; (c) See the steps in page 136 of your lecture notes. You need to multiply the pu short-circuit current by the base current to obtain the actual short-circuit current,; (d) I_f = 3.3584 kA, $Z_{11} = jX_{th}$ = j0.2491 pu

Q2 Ans.: (a) δ = 30°, Q = 0.7846 Mvar delievered to infinite bus; (b) δ = 38.682°, Q = 5.012 Mvar absorbed by generator; (c) δ = 15.568°, P = 6.441 MW, Q = 3.1195 Mvar delivered to infinite bus

Nov/Dec 2015

Q1 Ans.: (a) (i) X_G = 0.2 pu, X_{T1} = 0.2 pu, X_{T2} = 0.15 pu, X_{T3} = 0.16 pu, X_{T4} = 0.2 pu, X_{L1} = 0.1 pu, X_{L2} = 0.51 pu, X_M = 0.251 pu, Z_L = (0.95 + j1.267) pu; (ii) V_t = 27.83 kV; (b) (i) and (ii) $P_\Delta = P_Y$ = 14.52 kW

Q2 Ans.: (a) (i) P = 490 MW. Q = 499.8 Mvar (lag), E = 22.62 kV, δ = 16.76°; (ii) Q = 483.7 Mvar (lag), δ = 18.51°; (b) V_S = 19.931 kV (phase voltage)

Apr/May 2015

Q1 Ans.: (a) X_{G1} = 0.2 pu, X_{G2} = 0.1029 pu, X_{T1} = 0.05 pu, X_{T2} = 0.025 pu, X_{L1} = 0.1 pu, X_{L2} = 0.1 pu; (b) V_2 = 13.5984 kV, Z_L = (1.62 - j0.7845) pu; (c) I_f = 2.2662 kA; (d) $S_{f,G1}$ = 322.611 MVA, $S_{f,G2}$ = 580.161 MVA

Q2 Ans.: (a) δ = 27.288°; (b) VR = -18.334%

Nov/Dec 2014

Q1 Ans.: (a) $X_{G1} = X_{G2}$ =0.8 pu, X_{G3} = 0.6 pu, X_T = 0.16 pu; (b) $Z_{Bus}(1,1) = Z_{Bus}(1,2) = Z_{Bus}(2,1)$ = j0.24, $Z_{Bus}(2,2)$ = j0.4, Fault MVA at Bus 2 = 250 MVA, Fault MVA supplied by G_1 or G_2 = 75 MVA, Fault MVA supplied by G_3= 100 MVA; (c) Fault MVA supplied by G_1 or G_2 = 75 MVA, Fault MVA supplied by G_3= 100 MVA

Q2 Ans.: (a) E = 0.7305 kV; (b) E_i = 0. 8725 kV, E_{ii} = 0.6012 kV; (c) E is normally excited, E_i is overexcited, E_{ii} is underexcited

Apr/May 2014

Q1 Ans.: (a) X_s = 1.45 pu, X_{tr} = 0.06 pu, Z = j0.07429 pu, Y = j0.4896 pu, $Z_L = 2\angle 36.87°$ pu; (b) V_S = 346.57 kV, I_S = 0.1096 kA, $|S_S|$ = 65.78 MVA, P_S = 60 MW, Q_S = 26.953 Mvar flowing towards the transformer; (c) V_1 = 21.870 kV, E = 20.882 kV

Q2 Ans.: (a) E_2 = 19.511 kV, δ_2 = 26.81°, Q_2 = 0.417 Mvar absorbed by the generator, θ_2 = 27.529° lead becsue Q_2 is negative or absorbed by the generator; (b) δ = 29.069°

Nov/Dec 2013

Q1 Ans.: (a) X_G = 1.093 pu, X_{T1} = 0.4 pu, X_{T2} = 0.667 pu, X_{Line} = 0.386 pu, X_{M1} = 3.267 pu, X_{M2} = 3.267 pu; (b) V_t = 13.753 kV, E_G = 14.85 kV, $E_{M1} = E_{M2}$ = 11.698 kV; (c) Q_C = -2.125 Mvar

Q2 Ans.: (a) $f_{nlA} = f_{nlB}$ = 62.206 Hz, f_{nlC} = 61.177 Hz; (b) f_{sys} = 59.804 Hz, (c) f_{nlSWG} = 61.765; (d) f_{sys} = 59.118 Hz but at this frequency, $P_A = P_B$ = 105 MW are overloaded and their protective relays may trip

Apr/May 2013

Q1 Ans.: (a) X_G = 0.2 pu, X_T = 0.05 pu, Z = $0.1712\angle 83.66°$ pu, Y/2 = j0.045 pu, $Z_{LD} = 2\angle 36.87°$ pu; (b) V_2 = 242.17 kV, η = 98.95%; (c) I_f = 1.498 kA

Q2 Ans.: (a) E = 19.68 kV, VR = -10.56%; (b) δ_2 = 45.69°, Q_2 = 0.7504 MVar absorbed

Nov/Dec 2012

Q1 Ans.: (a) $X_{12} = X_{13} = X_{23}$ = 0.1 pu, X_{GT1} = 0.15 pu, X_{GT2} = 0.075 pu; (b) Diagonal matrix elements = -j26.67, -j33.33, -j20 pu, off-diagonal matrix elements = j10 pu for all; (c) I_f = 1.2374 kA, V_1 = 103.673 kV, V_2 = 123.106 kV, V_3 = 0, $I_{12} = I_{21}$ = 0.1061 kA, $I_{13} = I_{31}$ = 0.5657 kA, $I_{23} = I_{32}$ = 0.6718 kA; (d) I_f = 1.2374 kA

Q2 Ans.: (a) E = 36.204 kV, δ = 27.113°; (b) E_2 = 39.8247 kV, δ_2 = 24.476°, Q_2 = 43.169 MVar generated, pf = 0.7569 lag; (c) δ_3 = 30.206°, P_3 = 60.716 MW, Q_3 = 37.628 Mvar generated; (d) P_{max} = 120.681 MW

Apr/May 2012

Q1 Ans.: (a) X_{G1} = 0.4 pu, X_{G2} = 0.6 pu, X_T = 0.16 pu, X_{TL} = 0.1 pu, $Z_{LD} = 2\angle 36.87°$ pu; (b) V_1 = 32.49 kV; (c) I_f = 320.75 A, S_F = 222.222 MVA; (d) S_{G1} = 133.333 MVA, S_{G2} = 88.888 MVA

Q2 Ans.: (a) A = D = $0.9924\angle 0.0491°$ pu, B = $0.1705\angle 83.684°$ pu, C = j0.08993; (b) V_s = 248.208 kV, I_s = 0.4962 kA, S_s = 163.912 MW + j136.505 Mvar; (d) η = 97.613%

Nov/Dec 2011

Q1 Ans.: (a) X_{G1} = 0.15 pu, X_{G2} = 0.25 pu, X_{T1} = 0.1 pu, X_{T2} = 0.1 pu, X_L = 0.1736 pu, Z_{LD} = 0.6667 $\angle 36.87°$ pu; (b) E_{G1} = 14.475 kV, E_{G2} = 15.163 kV; (c) I_f = 0.6325 kA, S_{G1} = 74.227 MVA, S_{G2} = 57.234 MVA

Q2 Ans.: (a) f_{sys} = 50.615 Hz, P_{GA} = 18.769 MW, P_{GB} = 21.231 MW; (b) PF_B = 0.7125 lagging; (c) f'_{nlB} = 50.1667 Hz

May 2011

Q1 Ans.: (a) X_{GT1} = 0.15 pu, X_{GT2} = 0.075 pu, $X_{12} = X_{13} = X_{23}$ = 0.1 pu; (b) I_f = 13.736 pu; (c) S_{G1} = 333.59 MVA, S_{G2} = 353.21 MVA

Q2 Ans.: (a) A = 1 pu, B = $0.06605\angle 76.905°$ pu, C = 0, D = 1 pu, VR = 5.143%; (b) PF = 0.966 leading; (c) 98.474%

December 2010

Q1 Ans.: (a) X_{T1} = 0.06667 pu, X_{T2} = 0.07841 pu, X_L = 0.05377 pu, Z_{LD} = 1.3443 $\angle 36.87°$ pu; (b) V_1 = 37.9378 kV; (c) I_f = 1.7888 kA

Q2 Ans.: (a) δ = 22.293°, P = 69.376 MW, Q = 52.033 Mvar delivered; (b) δ = 50.152°, P = 140.414 MW; (c) P_{max} = 182.891 MW

Apr/May 2010

Q1 Ans.: (a) X_G = 0.15 pu, X_{T1} = 0.08571 pu, X_{T2} = 0.1 pu, X_L = 0.1134 pu, X_M = 0.2 pu; (b) E_M = 12.6724 kV, E_G = 14.7349 kV; (c) I_f in LV side of T2 = 3.0851 kA, I_f in line L = 0.3353 kA

Q2 Ans.: (a) L = 10.4241 x 10^{-2} H, C_n = 1.0911 μF; (b) A = 0.9919 pu, B = j0.1644 pu, C = j0.09791 pu, D = 0.9919 pu; (c) V_s = 348.58 kV, I_s = 0.6648 kA, S_s = 401.355 MVA

Nov/Dec 2009

Q1 Ans.: (a) X_{T1} = 0.1 pu, X_{T2} = 0.1 pu, X_L = 0.09452 pu; (b) and (c) S_f = 378.524 MVA, S_{G1} = 128.523 MVA, S_{G2} = 250 MVA

Q2 Ans.: (a) E = 17.99 kV, VR = 63.55%; (b) P_{max} = 197.892 MW, I_a = 12.174 kA, PF = 0.8532 leading, Q = 121 Mvar absorbed by the generator