

Review: Frequency Domain Design Method

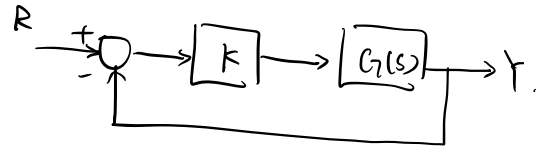
Design based on Bode plots is **not good for**:

- exact closed-loop pole placement (root locus is more suitable for that)
- deciding if a given K is stabilizing or not ...
 - we can only measure *how far* we are from instability (using GM or PM), if we know that we are stable
 - however, we don't have a way of checking whether a given K is stabilizing from frequency response data

Nyquist criterion- A frequency-domain substitute for the Routh-Hurwitz criterion

Nyquist Stability Criterion.

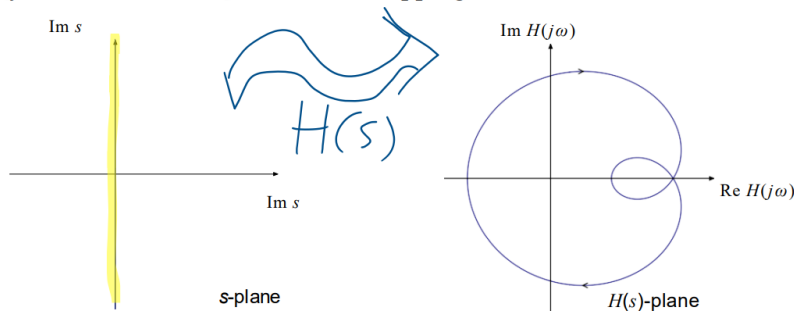
Goal : count # of RHP poles of $H_{cl} = \frac{KG}{1+KG}$.



Nyquist plot: $\text{Im}\{H(s)\}$ v.s. $\text{Re}\{H(s)\}$; for $s=j\omega$,
(ω from $-\infty$ to ∞).

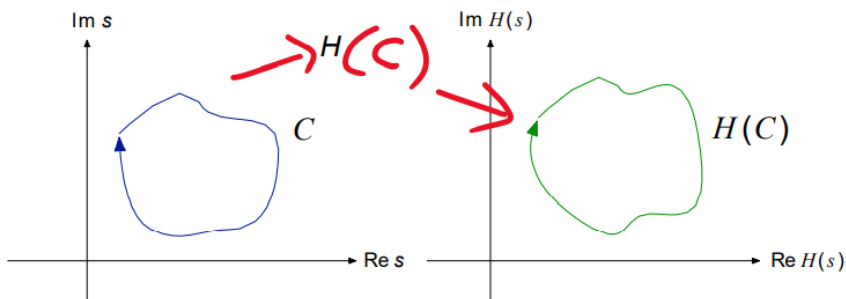
Nyquist Plot: Mapping of the s-Plane

- View the Nyquist plot of H as the image of the imaginary axis $\{j\omega : -\infty < \omega < \infty\}$ under the mapping $H : \mathbb{C} \rightarrow \mathbb{C}$



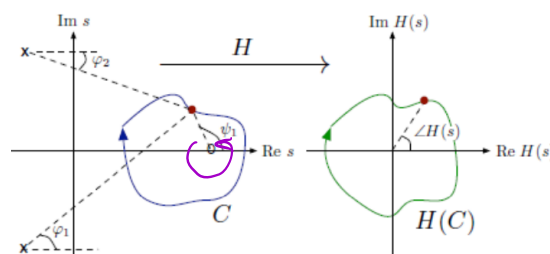
★ For ω from $-\infty$ to ∞ :
Nyquist plot **symmetric**
about real axis.

If we choose any closed curve (or **contour**) C on the left, it will get mapped by H to some other curve (contour) on the right:



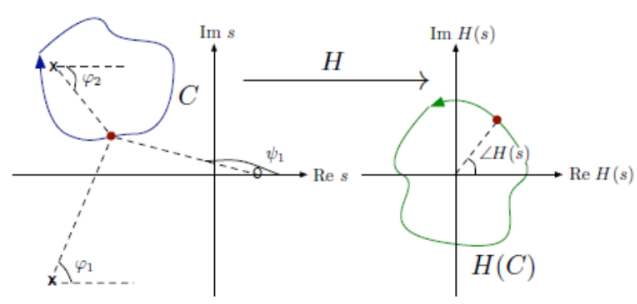
Phase of H : $\angle H(s) = \angle \frac{(s-z_1)\dots(s-z_m)}{(s-p_1)\dots(s-p_n)} = \sum_{i=1}^m \underbrace{\gamma_i}_{\angle \text{zero}} - \sum_{j=1}^n \underbrace{\psi_j}_{\angle \text{pole}} = \sum \angle \text{zeros} - \sum \angle \text{poles}$

I. Contour encircles a zero:



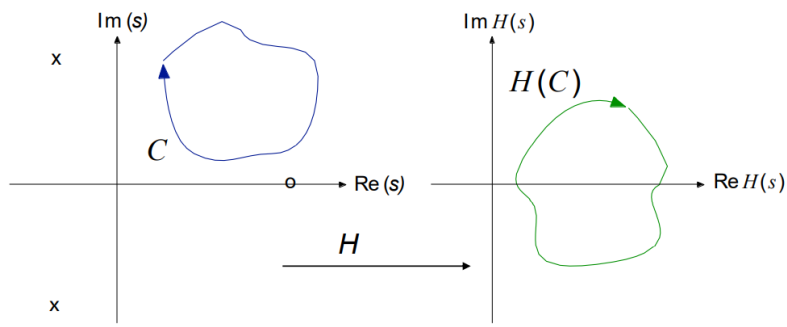
1. γ_1, ψ_2 return to original value.
 2. γ_1 net change of -360° .
 $\Rightarrow \angle H(s) - 360^\circ$.
- $\gamma_1, \angle H(s)$ same direction.

II. Contour encircles a pole.



1. ϕ_1, ϕ_2 return.
 2. \nrightarrow net change: -360°
 $\Rightarrow \angle H(s) - 360^\circ$.
 $H(C)$ encircles the origin once counterclockwise.

III. Contour encircles no poles, no zeros.



$\rightarrow \phi_1, \phi_2, \psi_1$ all return to their original values
 \rightarrow therefore, no net change in $\angle H(s)$, so $H(C)$ does not encircle the origin

The Argument Principle.

The Argument Principle. Let C be a closed, clockwise \odot oriented contour not passing through any zeros or poles* of $H(s)$. Let $H(C)$ be the image of C under the map $s \mapsto H(s)$:

$$H(C) = \{H(s) : s \in C\}.$$

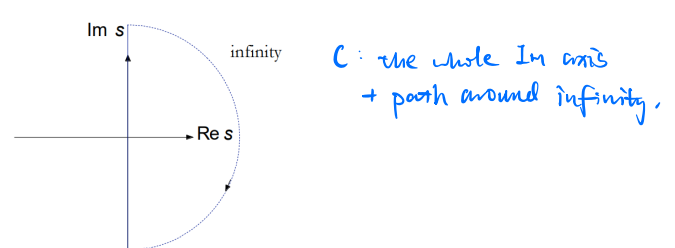
Then:

$\#(\text{clockwise encirclements } \odot \text{ of } 0 \text{ by } H(C))$
 $= \#(\text{zeros of } H(s) \text{ inside } C) - \#(\text{poles of } H(s) \text{ inside } C).$

More succinctly,

$$N = Z - P$$

- \rightarrow If $N < 0$, it means that $H(C)$ encircles the origin counterclockwise (\ominus).
- \rightarrow We do not want C to pass through any pole of H because then $H(C)$ would not be defined.
- \rightarrow We also do not want C to pass through any zero of H because then $0 \in H(C)$, so $\#(\text{encirclements})$ is not well-defined.



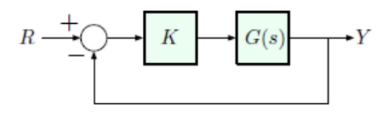
$H(C) = \text{Nyquist plot of } H$

By Argument Principle:

- $N = \#$ (CW \odot of 0 by Nyquist plot of $1+KG(s)$).
 ① \odot of -1 by Nyquist Plot of $KG(s)$.
 ② CW \odot of $-1/K$ by Nyquist plot of $G(s)$.

$$N = Z - P$$

- $Z = \#$ ① zeros of $1+KG(s)$ inside C
 ② $\#$ (RHP zeros of $1+KG$).
 ③ $\#$ (RHP closed-loop poles).
 $P = \#$ ① poles of $1+KG(s)$ inside C .
 ② $\#$ (RHP poles of $1+KG(s)$)
 ③ $\#$ (RHP roots of $p(s)$)
 ④ $\#$ (RHP open-loop poles).



$$G(s) = \frac{q(s)}{p(s)}, \quad \deg(q) \leq \deg(p)$$

$$1 + KG(s) = \frac{p(s) + Kq(s)}{p(s)}$$

$$\text{closed-loop t.f.} = \frac{KG(s)}{1 + KG(s)} = \frac{Kq(s)}{p(s) + Kq(s)}$$

The Nyquist Thm: $N = Z - P$

Nyquist Stability Criterion:

The Nyquist Plot of $G(s)$ ccw $\odot -\frac{1}{K}$ for P times, where $P = Z - N$.

\Updownarrow
stable.

\Updownarrow
N = -P

Example 1

$$G(s) = \frac{1}{(s+1)(s+2)} \quad (\text{no open-loop RHP poles})$$

Characteristic equation:

$$(s+1)(s+2) + K = 0 \quad \Longleftrightarrow \quad s^2 + 3s + K + 2 = 0$$

From Routh, we already know that the closed-loop system is stable for $K > -2$.

We will now reproduce this answer using the Nyquist criterion.

Strategy:

- ▶ Start with the Bode plot of G
- ▶ Use the Bode plot to graph $\text{Im } G(j\omega)$ vs. $\text{Re } G(j\omega)$ for $0 \leq \omega < \infty$
- ▶ This gives only a *portion* of the entire Nyquist plot

$$(\text{Re } G(j\omega), \text{Im } G(j\omega)), \quad -\infty < \omega < \infty$$

- ▶ Symmetry:

$$G(-j\omega) = \overline{G(j\omega)}$$

— Nyquist plots are always *symmetric w.r.t. the real axis*!!

Example 1

$$= \frac{1}{s^2 + 3s + 2} = \frac{1}{2} \cdot \frac{1}{(\frac{j\omega}{\sqrt{2}})^2 + \frac{3}{\sqrt{2}}(j\omega) + 1} \quad , \quad \omega_n = \sqrt{2} \cdot \quad 2\zeta\omega_n = \frac{3}{\sqrt{2}} \Rightarrow \zeta = \frac{3}{4} \times \frac{1}{\sqrt{2}} = \frac{3}{8}\sqrt{2}$$

$$G(s) = \frac{1}{(s+1)(s+2)}$$

(no open-loop RHP poles)

Strategy:

- ▶ Start with the Bode plot of G
- ▶ Use the Bode plot to graph $\text{Im } G(j\omega)$ vs. $\text{Re } G(j\omega)$ for $0 \leq \omega < \infty$
- ▶ This gives only a *portion* of the entire Nyquist plot

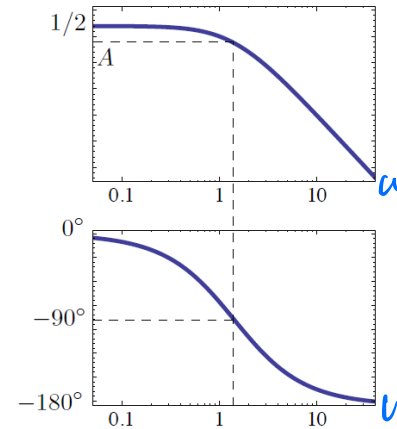
$$(\text{Re } G(j\omega), \text{Im } G(j\omega)), \quad -\infty < \omega < \infty$$

▶ Symmetry:

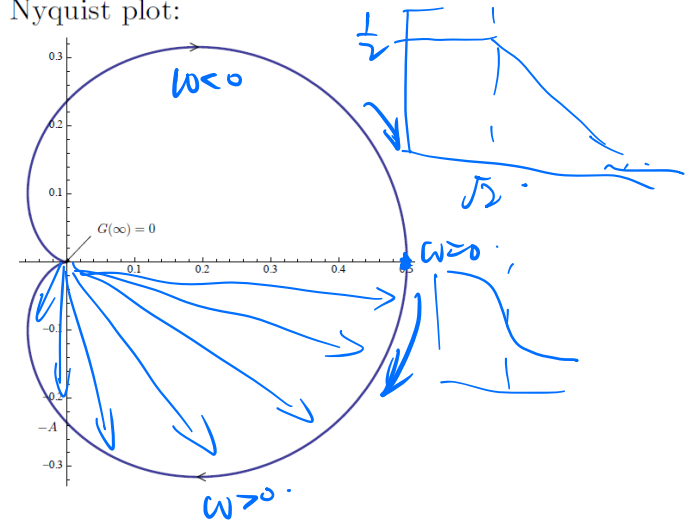
$$G(-j\omega) = \overline{G(j\omega)}$$

— Nyquist plots are always *symmetric w.r.t. the real axis*!!

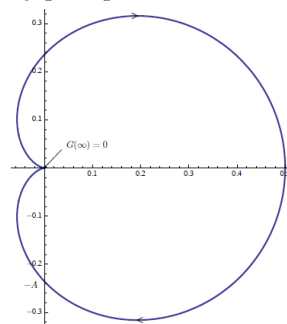
Bode plot:



Nyquist plot:



Nyquist plot:



$$\begin{aligned} \#(\odot \text{ of } -1/K) \\ &= \#(\text{RHP CL poles}) - \underbrace{\#(\text{RHP OL poles})}_{=0} \end{aligned}$$

$\Rightarrow K \in \mathbb{R}$ is stabilizing if and only if

$$\#(\odot \text{ of } -1/K) = 0$$

- ▶ If $K > 0$, $\#(\odot \text{ of } -1/K) = 0$
- ▶ If $0 < -1/K < 1/2$,
 $\#(\odot \text{ of } -1/K) > 0 \Rightarrow$
closed-loop stable for $K > -2$

Example 2

$$G(s) = \frac{1}{(s-1)(s^2+2s+3)} = \frac{1}{s^3+s^2+s-3}$$

$\#(\text{RHP open-loop poles}) = 1 \quad \text{at } s = 1$

Routh: the characteristic polynomial is

$$s^3 + s^2 + s + K - 3 \quad \text{— 3rd degree}$$

— stable if and only if $K - 3 > 0$ and $1 > K - 3$.

Stability range: $3 < K < 4$

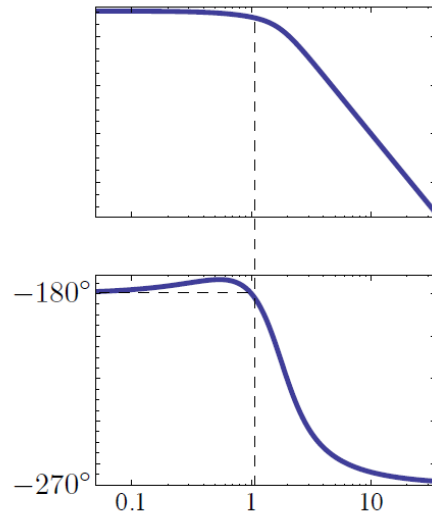
Let's see how to spot this using the Nyquist criterion ...

Example 2

$$G(s) = \frac{1}{(s-1)(s^2+2s+3)}$$

(1 open-loop RHP pole)

Bode plot:

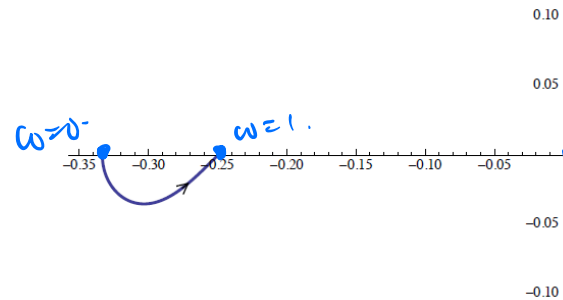


Nyquist plot:

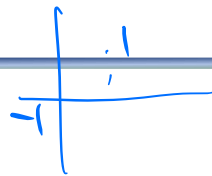
$$\omega = 0 \quad M = 1/3, \phi = -180^\circ$$

$$\omega = 1 \quad M = 1/4, \phi = -180^\circ$$

$$\omega \rightarrow \infty \quad M \rightarrow 0, \phi \rightarrow -270^\circ$$



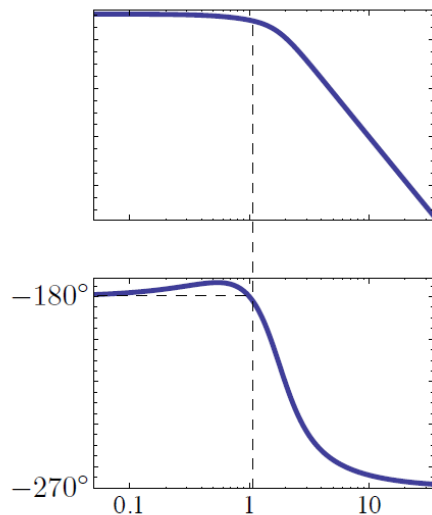
Example 2



$$G(s) = \frac{1}{(s-1)(s^2+2s+3)}$$

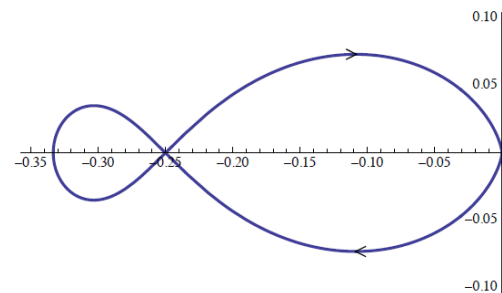
(1 open-loop RHP pole)

Bode plot:



Nyquist plot:

$$\begin{aligned} \omega = 0 & \quad M = 1/3, \phi = -180^\circ \\ \omega = 1 & \quad M = 1/4, \phi = -180^\circ \\ \omega \rightarrow \infty & \quad M \rightarrow 0, \phi \rightarrow -270^\circ \end{aligned}$$



$K \in \mathbb{R}$ is stabilizing if and only if

$$\#(\odot \text{ of } -1/K) = -1$$

Which points $-1/K$ are encircled once \odot by this Nyquist plot?

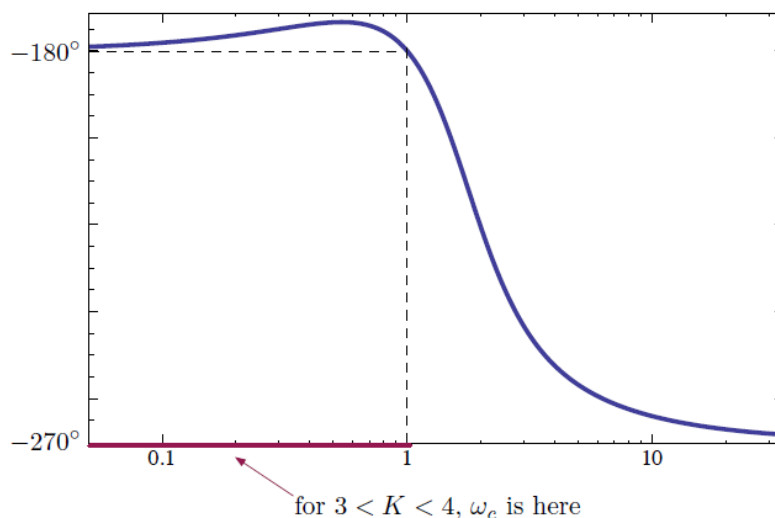
$$\begin{aligned} \#(\odot \text{ of } -1/K) & \\ &= \#(\text{RHP CL poles}) \\ &\quad - \underbrace{\#(\text{RHP OL poles})}_{=1} \end{aligned}$$

$$\begin{aligned} \text{only } -1/3 < -1/K < -1/4 \\ \implies 3 < K < 4 \end{aligned}$$

Example 2

Closed-loop stability range for $G(s) = \frac{1}{(s-1)(s^2+2s+3)}$ is
 $3 < K < 4$ (using either Routh or Nyquist).

We can interpret this in terms of phase margin:



So, in this case, $\text{stability} \iff \text{PM} > 0$ (typical case).

Example 3

$$G(s) = \frac{s-1}{(s+2)(s^2-s+1)} = \frac{s-1}{s^3+s^2-s+2}$$

Open-loop poles:

$$s = -2 \quad (\text{LHP})$$

$$s^2 - s + 1 = 0$$

$$\left(s - \frac{1}{2}\right)^2 + \frac{3}{4} = 0$$

$$s = \frac{1}{2} \pm j\frac{\sqrt{3}}{2} \quad (\text{RHP})$$

\therefore 2 RHP poles

$$G(s) = \frac{s-1}{(s+2)(s^2-s+1)} = \frac{s-1}{s^3+s^2-s+2}$$

Routh:

$$\begin{aligned} \text{char. poly. } & s^3 + s^2 - s + 2 + K(s-1) \\ & s^2 + s^2 + (K-1)s + 2 - K \quad (3\text{rd-order}) \end{aligned}$$

— stable if and only if

$$K - 1 > 0$$

$$2 - K > 0$$

$$K - 1 > 2 - K$$

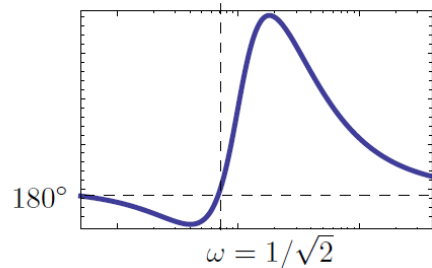
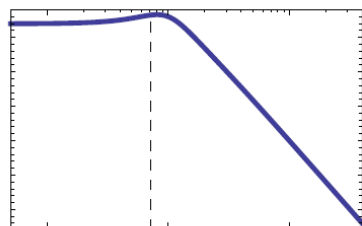
— stability range is $3/2 < K < 2$

Example 3

$$G(s) = \frac{s-1}{(s+2)(s^2-s+1)}$$

(2 open-loop RHP poles)

Bode plot (tricky, RHP poles/zeros)



$\phi = 180^\circ$ when:

- ▶ $\omega = 0$ and $\omega \rightarrow \infty$
- ▶ $\omega = 1/\sqrt{2}$:

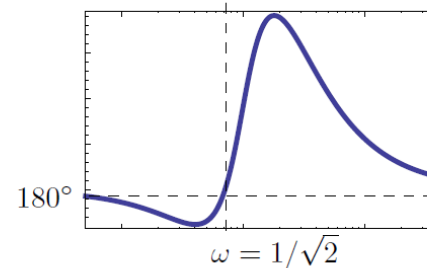
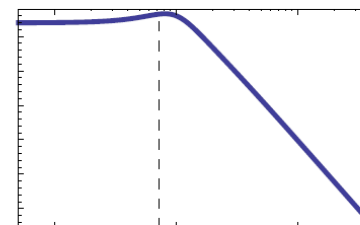
$$\begin{aligned} & \left. \frac{j\omega - 1}{(j\omega - 1)((j\omega)^2 - j\omega + 1)} \right|_{\omega=1/\sqrt{2}} \\ &= \frac{\frac{j}{\sqrt{2}} - 1}{\left(\frac{j}{\sqrt{2}} + 2\right)\left(-\frac{1}{2} - \frac{j}{\sqrt{2}} + 1\right)} \\ &= \frac{\frac{j}{\sqrt{2}} - 1}{-\frac{3}{2}\left(\frac{j}{\sqrt{2}} - 1\right)} = -\frac{2}{3} \end{aligned}$$

(need to guess this, e.g., by mouseclicking in Matlab)

$$G(s) = \frac{s-1}{s^3 + s^2 - s + 2}$$

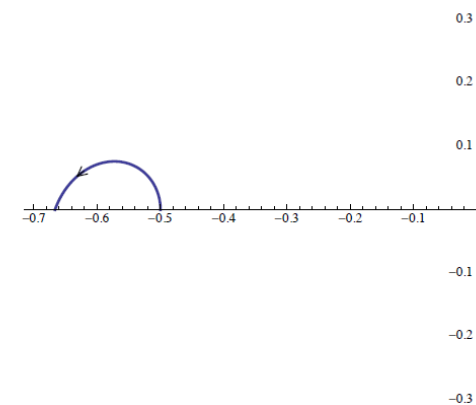
(2 open-loop RHP poles)

Bode plot:



Nyquist plot:

$$\begin{aligned} \omega = 0 & \quad M = 1/2, \phi = 180^\circ \\ \omega = 1/\sqrt{2} & \quad M = 2/3, \phi = 180^\circ \\ \omega \rightarrow \infty & \quad M \rightarrow 0, \phi \rightarrow 180^\circ \end{aligned}$$

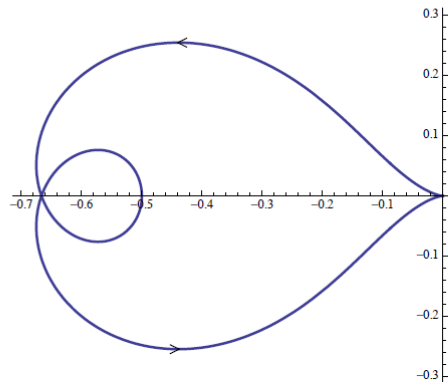


Example 3

$$G(s) = \frac{s-1}{s^3 + s^2 - s + 2}$$

(2 open-loop RHP poles)

Nyquist plot:



$$\begin{aligned} \#(\odot \text{ of } -1/K) \\ &= \#(\text{RHP CL poles}) \\ &\quad - \underbrace{\#(\text{RHP OL poles})}_{=2} \end{aligned}$$

$K \in \mathbb{R}$ is stabilizing if
and only if

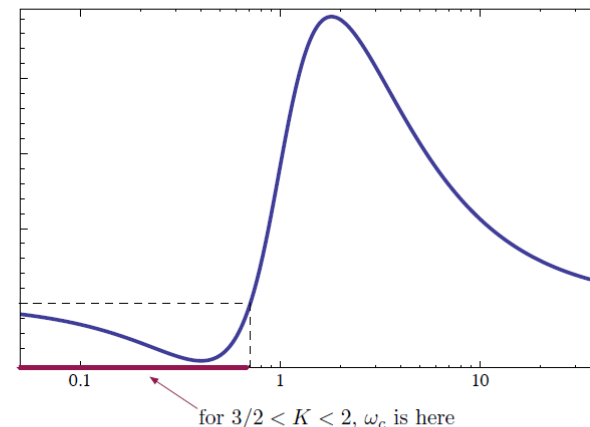
$$\#(\odot \text{ of } -1/K) = -2$$

Which points $-1/K$ are
encircled twice \odot by this
Nyquist plot?

$$\begin{aligned} \text{only } -2/3 < -1/K < -1/2 \\ \implies \frac{3}{2} < K < 2 \end{aligned}$$

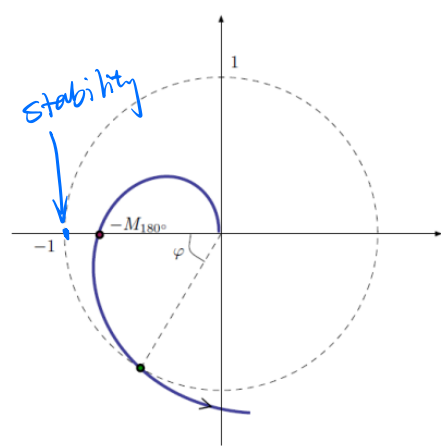
CL stability range for $G(s) = \frac{s-1}{s^3 + s^2 - s + 2}$: $K \in (3/2, 2)$

We can interpret this in terms of phase margin:



So, in this case, **stability** \iff **PM** < 0 (atypical case; Nyquist
criterion is the only way to resolve this ambiguity of Bode
plots).

Stability Margin.



$$GM = \frac{1}{M_{180^\circ}}.$$
$$\Rightarrow \frac{K}{M_{180^\circ}} = 1.$$

$$PM = \varphi$$

