

$$y = \ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2 x.$$

$$H(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}.$$

By the quadratic formula, the poles are:

$$s = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

$$= -\omega_n \left( \zeta \pm \sqrt{\zeta^2 - 1} \right)$$

The nature of the poles changes depending on  $\zeta$ :

damping coefficient/ratio  $\rightarrow$   $\left\{ \begin{array}{ll} \blacktriangleright \zeta > 1 & \text{both poles are real and negative (overdamped).} \\ \blacktriangleright \zeta = 1 & \text{one negative pole} \\ \blacktriangleright \zeta < 1 & \text{two complex poles with negative real parts (underdamped).} \end{array} \right.$

$\zeta = 0$ : no damping.

$$s = -\sigma \pm j\omega_d$$

where

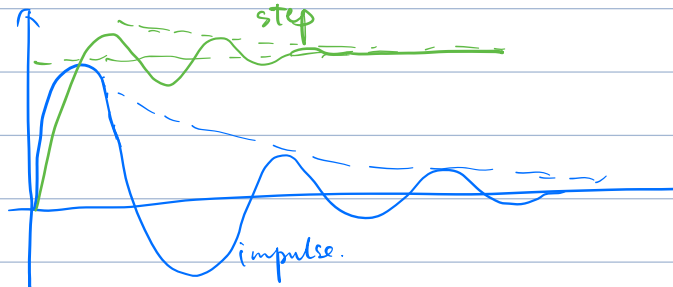
$$\sigma = \zeta\omega_n, \quad \omega_d = \omega_n\sqrt{1 - \zeta^2}$$

$$\Rightarrow H(s) = \frac{\omega_n^2}{(s + \sigma)^2 + \omega_d^2}$$

Impulse response:  $y(t) = \mathcal{L}^{-1}\{H(s)\} = \frac{\omega_n^2}{\omega_d} e^{-\sigma t} \sin(\omega_d t).$

$$\mathcal{L}\{1(t)\} = \frac{1}{s}.$$

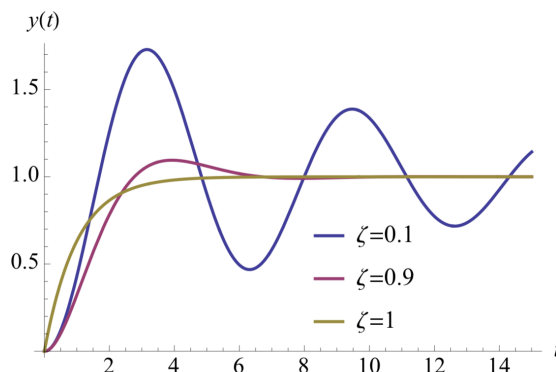
Step response:  $y(t) = \mathcal{L}^{-1}\left\{\frac{H(s)}{s}\right\} = 1 - e^{-\sigma t} \left( \cos(\omega_d t) + \frac{\sigma}{\omega_d} \sin(\omega_d t) \right).$



$$H(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} = \frac{\omega_n^2}{(s + \sigma)^2 + \omega_d^2}$$

$$u(t) = 1(t) \quad \rightarrow \quad y(t) = 1 - e^{-\sigma t} \left( \cos(\omega_d t) + \frac{\sigma}{\omega_d} \sin(\omega_d t) \right)$$

where  $\sigma = \zeta\omega_n$  and  $\omega_d = \omega_n\sqrt{1 - \zeta^2}$  (damped frequency)



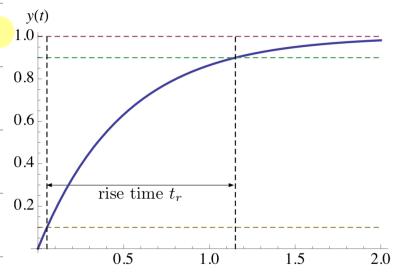
The parameter  $\zeta$  is called the *damping ratio*

- $\blacktriangleright \zeta > 1$ : system is overdamped
- $\blacktriangleright \zeta < 1$ : system is underdamped
- $\blacktriangleright \zeta = 0$ : no damping ( $\omega_d = \omega_n$ )

Rise time:  $t_r$ ,  $y$  from 10% to 90% of steady-state time.

1st-order:  $H(s) = \frac{s}{s+a}$ ,  $t_r = \frac{\ln 0.9 - \ln 0.1}{a} \approx \frac{2.2}{a}$

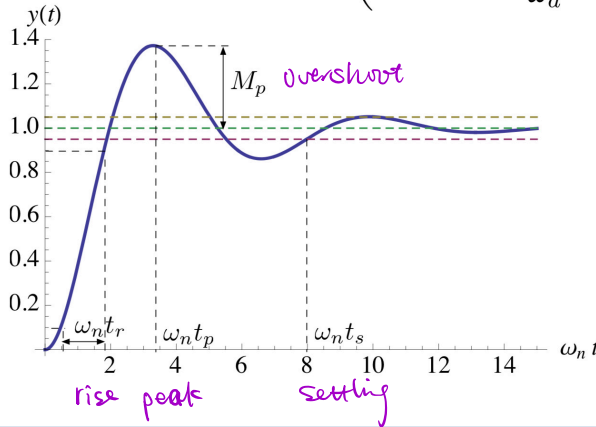
Step response:  $y(t) = 1(t) - e^{-at}$



2nd-order:

Step response:

$$y(t) = 1 - e^{-\sigma t} \left( \cos(\omega_d t) + \frac{\sigma}{\omega_d} \sin(\omega_d t) \right)$$



①  $t_r, t_p, t_s$  should be small.

② small error, small  $M_p$ .

Note: ① empirically,  $\omega_n t_r \approx 1.8$  (exact when  $\zeta = 0.5$ ). ← approx.

②  $y(t_p) = 0 \Rightarrow t_p = \frac{\pi}{\omega_d}$

③  $M_p = y(t_p) - 1 = e^{-\sigma \pi / \omega_d} = e^{-\frac{\pi \zeta}{\sqrt{1-\zeta^2}}}$  ← exact

④ need to define when is steady-state.

$$t_s = \min \left\{ t > 0: \frac{|y(t') - y(\infty)|}{y(\infty)} \leq 0.01 \text{ for all } t' \geq t \right\}$$

may vary.  
defined by designer.

$$\approx \frac{3}{\sigma}$$

☆☆

$t_r \approx \frac{1.8}{\omega_n}$  (good when  $\zeta = 0.5$ ).

$t_p = \frac{\pi}{\omega_d}$

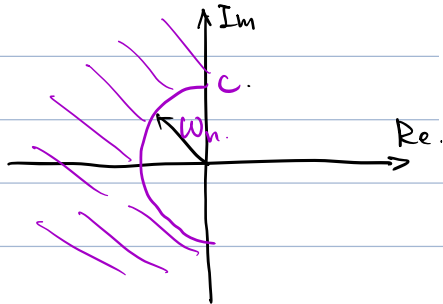
$M_p = \exp \left( -\frac{\pi \zeta}{\sqrt{1-\zeta^2}} \right)$

$t_s \approx \frac{3}{\sigma}$

# Specifications in Frequency Domain

1. Rise:  $\Delta$  want:  $t_r \leq c$  ( $c$  is a desired value).

suppose,  $\Rightarrow \omega_n \geq \frac{1.8}{c}$ .



2. overshoot:  $M_p = \exp\left(-\frac{\pi \zeta}{\sqrt{1-\zeta^2}}\right) \leq c$ .

$$\omega_n^2 = \sigma^2 + \omega_d^2$$

$$\zeta = \cos \varphi$$

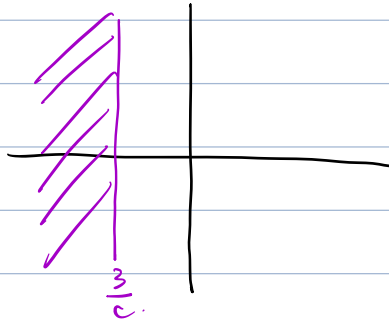
$$\Rightarrow \frac{c}{\sqrt{1-\zeta^2}} = \frac{\omega_n \zeta}{\omega_n \sqrt{1-\zeta^2}}$$

$$= \frac{\sigma}{\omega_d} = \tan \varphi \approx \zeta$$

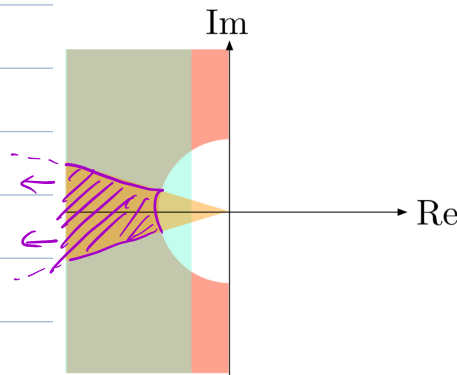
$\Rightarrow \varphi$  should be small, in which case  $\cos \varphi = \zeta$ .

3. settling time.

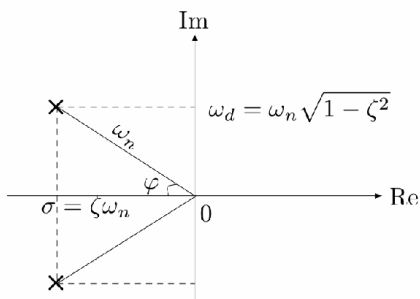
$$t_s = \frac{3}{\sigma} \leq c \Rightarrow \sigma \geq \frac{3}{c}$$



4. combination of 1~3:



Step response:  $y(t) = 1 - e^{-\sigma t} \left( \cos(\omega_d t) + \frac{\sigma}{\omega_d} \sin(\omega_d t) \right)$



$$\omega_n^2 = \sigma^2 + \omega_d^2$$

$$\zeta = \cos \varphi$$