



## ECE 486 Control Systems

Lecture 20: Nyquist Stability Examples;  
Phase and Gain Margins from Nyquist Plots.

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# Schedule check

## Frequency Response

## State-Space

Week	Topic	Ref.
1	Introduction to feedback control	Ch. 1
	State-space models of systems; linearization	Sections 1.1, 1.2, 2.1–2.4, 7.2, 9.2.1
2	Linear systems and their dynamic response	Section 3.1, Appendix A
	Transient and steady-state dynamic response with arbitrary initial conditions	Section 3.1, Appendix A
3	System modeling diagrams; prototype second-order system	Sections 3.1, 3.2, lab manual
	Transient response specifications	Sections 3.3, 3.14, lab manual
4	National Holiday Week	
5	Effect of zeros and extra poles; Routh-Hurwitz stability criterion	Sections 3.5, 3.6
	Basic properties and benefits of feedback control	Section 4.1, lab manual
6	Introduction to Proportional-Integral-Derivative (PID) control	Sections 4.1–4.3, lab manual
	Review A	
7	Term Test 1	
	Introduction to Root Locus design method	Ch. 5
8	Root Locus continued; introduction to dynamic compensation	Ch. 5
	Lead and lag dynamic compensation	Ch. 5
9	Introduction to frequency-response design method	Sections 5.1–5.4, 6.1
	Bode plots for three types of transfer functions	Section 6.1

## Root Locus

Week	Topic	Ref.
10	Stability from frequency response; gain and phase margins	Section 6.1
	Control design using frequency response	Ch. 6
11	Control design using frequency response continued; PI and lag, PID and lead-lag	Ch. 6
	Nyquist stability criterion	Ch. 6
12	<b>Gain and phase margins from Nyquist plots</b>	Ch. 6
	<b>Term Test II (Review B)</b>	
13	Introduction to state-space design	Ch. 7
	Controllability, stability, and pole-zero cancellations; similarity transformation; conversion of controllable systems to Controller Canonical Form	Ch. 7
14	Pole placement by full state feedback	Ch. 7
	Observer design for state estimation	Ch. 7
15	Joint observer and controller design by dynamic output feedback I; separation principle	Ch. 7
	Dynamic output feedback II (Review C)	Ch. 7
16	END OF LECTURES	
	Finals	



# Lecture Overview

- Review: Nyquist stability criterion
- Today's topic: Phase and Gain Margin from Nyquist Plot



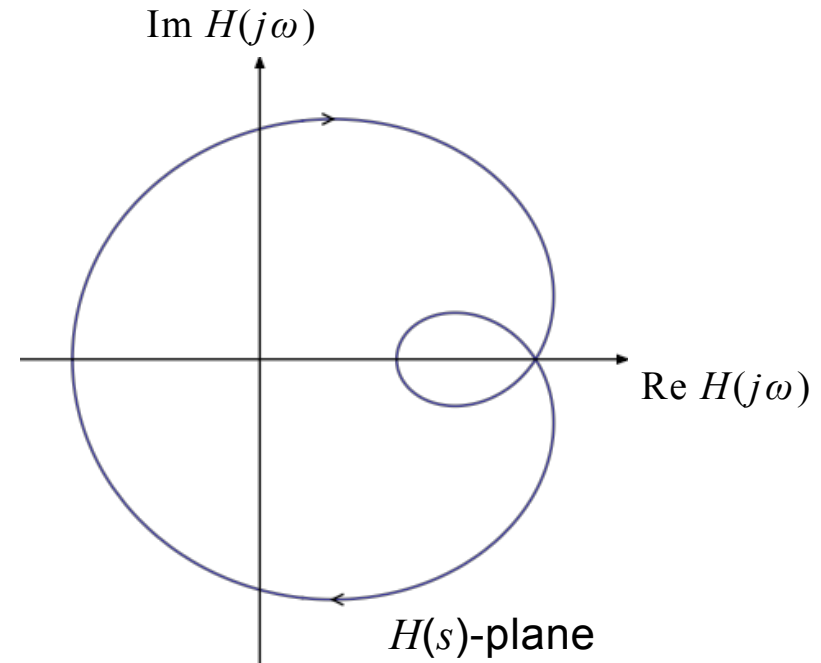
# Review: Nyquist Plot

# Review: Nyquist Plot

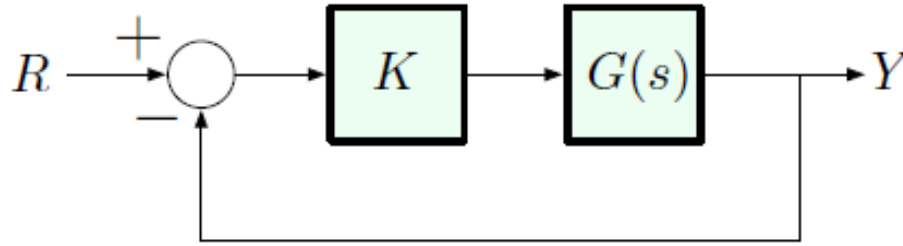
Consider an arbitrary *strictly proper* transfer function  $H$ :

$$H(s) = \frac{(s - z_1) \dots (s - z_m)}{(s - p_1) \dots (s - p_n)}, \quad m < n$$

**Nyquist plot:**  $\text{Im } H(j\omega)$  vs.  $\text{Re } H(j\omega)$   
as  $\omega$  varies from  $-\infty$  to  $\infty$



# Review: Nyquist Stability Criterion

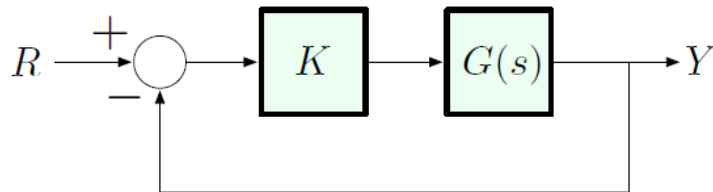


**Goal:** count the number of RHP poles (if any) of the closed-loop transfer function

$$\frac{KG(s)}{1 + KG(s)}$$

based on frequency-domain characteristics of the plant transfer function  $G(s)$

# Review: The Nyquist Theorem



**Nyquist Theorem (1928)** Assume that  $G(s)$  has no poles on the imaginary axis\*, and that its Nyquist plot does not pass through the point  $-1/K$ . Then

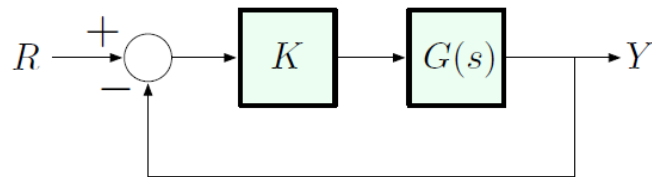
$$N = Z - P$$

$$\#(\odot \text{ of } -1/K \text{ by Nyquist plot of } G(s))$$

$$= \#(\text{RHP closed-loop poles}) - \#(\text{RHP open-loop poles})$$

\* Easy to fix: draw an infinitesimally small circular path that goes *around* the pole and stays in RHP

# Review: The Nyquist Stability Criterion



$$\underbrace{N}_{\#(\odot \text{ of } -1/K)} = \underbrace{Z}_{\#(\text{unstable CL poles})} - \underbrace{P}_{\#(\text{unstable OL poles})}$$

$$Z = N + P$$

$$Z = 0 \iff \boxed{N = -P}.$$

**Nyquist Stability Criterion.** Under the assumptions of the Nyquist theorem, the closed-loop system (at a given gain  $K$ ) is stable *if and only if* the Nyquist plot of  $G(s)$  encircles the point  $-1/K$   $P$  times *counterclockwise*, where  $P$  is the number of unstable (RHP) open-loop poles of  $G(s)$ .



# Review: Apply Nyquist Criterion

Workflow:

Bode  $M$  and  $\phi$ -plots  $\longrightarrow$  Nyquist plot

## Advantages of Nyquist over Routh–Hurwitz

- ▶ can work directly with experimental frequency response data (e.g., if we have the Bode plot based on measurements, but do not know the transfer function)
- ▶ less computational, more geometric (came 55 years after Routh)

# Example 1

$$G(s) = \frac{1}{(s+1)(s+2)} \quad (\text{no open-loop RHP poles})$$

Characteristic equation:

$$(s+1)(s+2) + K = 0 \quad \Longleftrightarrow \quad s^2 + 3s + K + 2 = 0$$

From Routh, we already know that the closed-loop system is stable for  $K > -2$ .

**We will now reproduce this answer using the Nyquist criterion.**

Strategy:

- ▶ Start with the Bode plot of  $G$
- ▶ Use the Bode plot to graph  $\text{Im } G(j\omega)$  vs.  $\text{Re } G(j\omega)$  for  $0 \leq \omega < \infty$
- ▶ This gives only a *portion* of the entire Nyquist plot

$$(\text{Re } G(j\omega), \text{Im } G(j\omega)), \quad -\infty < \omega < \infty$$

- ▶ Symmetry:

$$G(-j\omega) = \overline{G(j\omega)}$$

— Nyquist plots are always *symmetric w.r.t. the real axis*!!

# Example 1

$$= \frac{1}{j\omega^2 + 3(j\omega) + 2} = \frac{1}{2} \cdot \frac{1}{(\frac{j\omega}{\sqrt{2}})^2 + \frac{3}{\sqrt{2}}(j\omega) + 1} \quad , \quad \omega_n = \sqrt{2} \cdot \quad 2\zeta\omega_n = \frac{3}{\sqrt{2}} \Rightarrow \zeta = \frac{3}{4} \times \frac{1}{\sqrt{2}} = \frac{3}{8}\sqrt{2}$$

$$G(s) = \frac{1}{(s+1)(s+2)}$$

(no open-loop RHP poles)

Strategy:

- ▶ Start with the Bode plot of  $G$
- ▶ Use the Bode plot to graph  $\text{Im } G(j\omega)$  vs.  $\text{Re } G(j\omega)$  for  $0 \leq \omega < \infty$
- ▶ This gives only a *portion* of the entire Nyquist plot

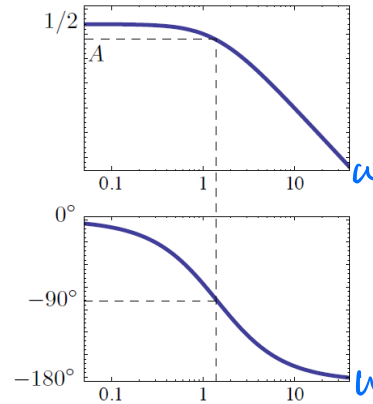
$$(\text{Re } G(j\omega), \text{Im } G(j\omega)), \quad -\infty < \omega < \infty$$

- ▶ Symmetry:

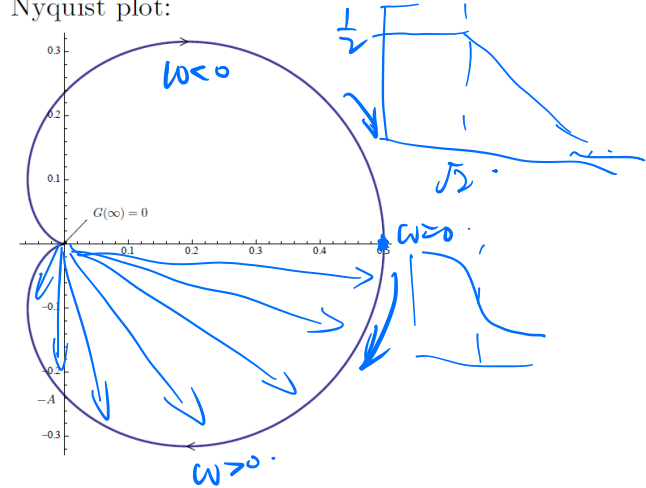
$$G(-j\omega) = \overline{G(j\omega)}$$

— Nyquist plots are always *symmetric w.r.t. the real axis*!!

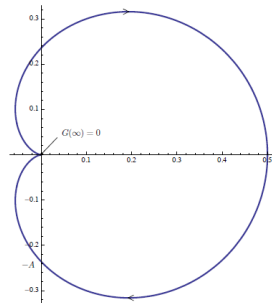
Bode plot:



Nyquist plot:



Nyquist plot:



$\#(\odot \text{ of } -1/K)$

$$= \#(\text{RHP CL poles}) - \underbrace{\#(\text{RHP OL poles})}_{=0}$$

$\Rightarrow K \in \mathbb{R}$  is stabilizing if and only if

$$\#(\odot \text{ of } -1/K) = 0$$

- ▶ If  $K > 0$ ,  $\#(\odot \text{ of } -1/K) = 0$
- ▶ If  $0 < -1/K < 1/2$ ,  
 $\#(\odot \text{ of } -1/K) > 0 \Rightarrow$   
closed-loop stable for  $K > -2$

# Example 2

$$G(s) = \frac{1}{(s-1)(s^2+2s+3)} = \frac{1}{s^3+s^2+s-3}$$

#(RHP open-loop poles) = 1      at  $s = 1$

Routh: the characteristic polynomial is

$$s^3 + s^2 + s + K - 3 \quad \text{— 3rd degree}$$

— stable if and only if  $K - 3 > 0$  and  $1 > K - 3$ .

Stability range:       $3 < K < 4$

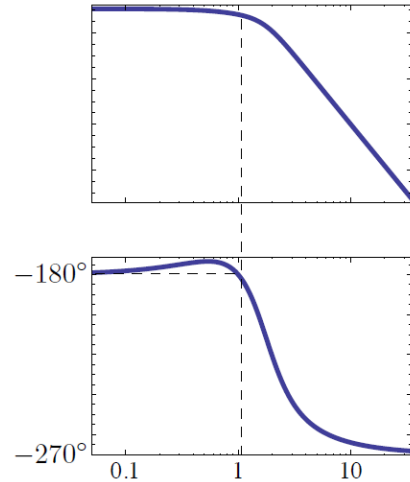
Let's see how to spot this using the Nyquist criterion ...

# Example 2

$$G(s) = \frac{1}{(s-1)(s^2+2s+3)}$$

(1 open-loop RHP pole)

Bode plot:

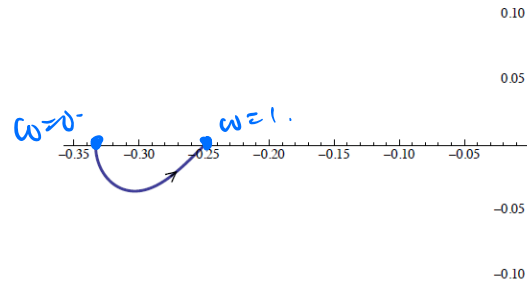


Nyquist plot:

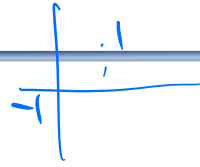
$$\omega = 0 \quad M = 1/3, \phi = -180^\circ$$

$$\omega = 1 \quad M = 1/4, \phi = -180^\circ$$

$$\omega \rightarrow \infty \quad M \rightarrow 0, \phi \rightarrow -270^\circ$$



# Example 2

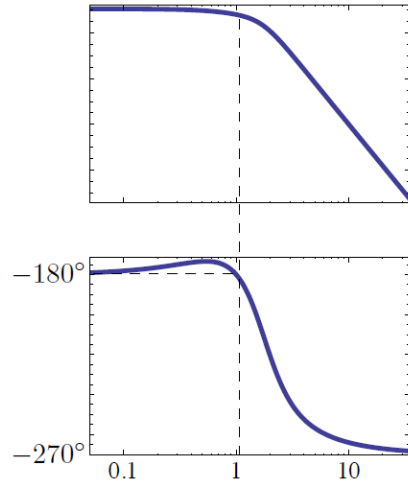


$$= \underbrace{(j\omega - 1)}_{\text{RHP pole}} \cdot (s^2 + 2s + 3)$$

(1 open-loop RHP pole)

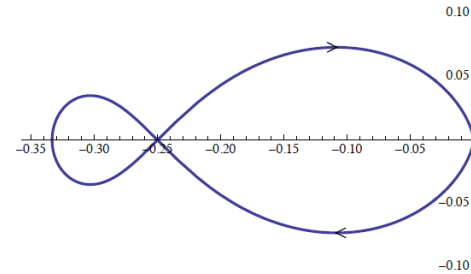
$$G(s) = \frac{1}{(s-1)(s^2+2s+3)}$$

Bode plot:



Nyquist plot:

$$\begin{aligned} \omega = 0 \quad M = 1/3, \phi &= -180^\circ \\ \omega = 1 \quad M = 1/4, \phi &= -180^\circ \\ \omega \rightarrow \infty \quad M &\rightarrow 0, \phi \rightarrow -270^\circ \end{aligned}$$



$K \in \mathbb{R}$  is stabilizing if and only if

$$\#(\odot \text{ of } -1/K) = -1$$

Which points  $-1/K$  are encircled once  $\odot$  by this Nyquist plot?

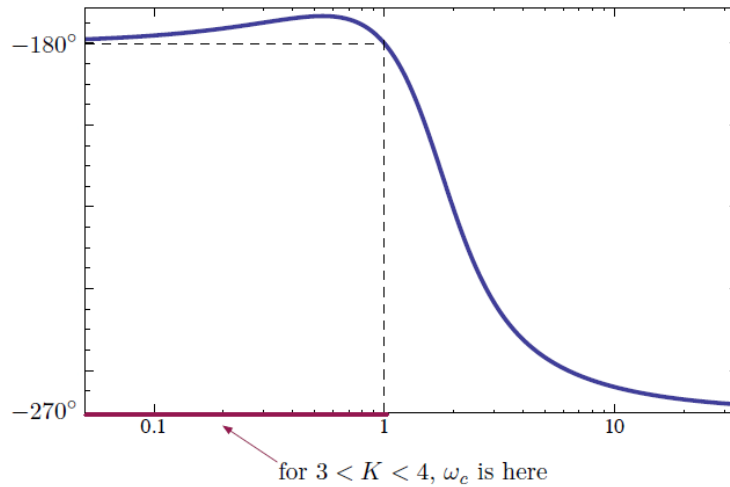
$$\begin{aligned} \#(\odot \text{ of } -1/K) &= \#(\text{RHP CL poles}) \\ &\quad - \underbrace{\#(\text{RHP OL poles})}_{=1} \end{aligned}$$

$$\begin{aligned} \text{only } -1/3 < -1/K < -1/4 \\ \implies 3 < K < 4 \end{aligned}$$

# Example 2

Closed-loop stability range for  $G(s) = \frac{1}{(s-1)(s^2+2s+3)}$  is  $3 < K < 4$  (using either Routh or Nyquist).

We can interpret this in terms of phase margin:



So, in this case,  $\text{stability} \iff \text{PM} > 0$  (typical case).

# Example 3

$$G(s) = \frac{s-1}{(s+2)(s^2-s+1)} = \frac{s-1}{s^3+s^2-s+2}$$

Open-loop poles:

$$s = -2 \quad (\text{LHP})$$

$$s^2 - s + 1 = 0$$

$$\left(s - \frac{1}{2}\right)^2 + \frac{3}{4} = 0$$

$$s = \frac{1}{2} \pm j\frac{\sqrt{3}}{2} \quad (\text{RHP})$$

$\therefore$  2 RHP poles

$$G(s) = \frac{s-1}{(s+2)(s^2-s+1)} = \frac{s-1}{s^3+s^2-s+2}$$

Routh:

$$\begin{aligned} \text{char. poly. } & s^3 + s^2 - s + 2 + K(s-1) \\ & s^3 + s^2 + (K-1)s + 2 - K \quad (3\text{rd-order}) \end{aligned}$$

— stable if and only if

$$K-1 > 0$$

$$2-K > 0$$

$$K-1 > 2-K$$

— stability range is  $3/2 < K < 2$

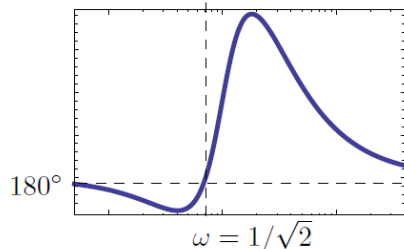
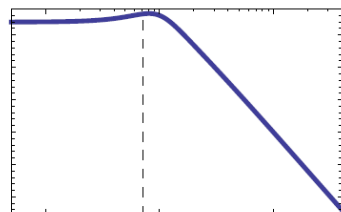


# Example 3

$$G(s) = \frac{s-1}{(s+2)(s^2-s+1)}$$

(2 open-loop RHP poles)

Bode plot (tricky, RHP poles/zeros)



$\phi = 180^\circ$  when:

- ▶  $\omega = 0$  and  $\omega \rightarrow 0$
- ▶  $\omega = 1/\sqrt{2}$ :

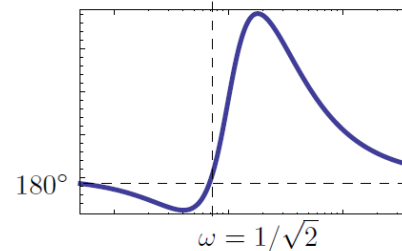
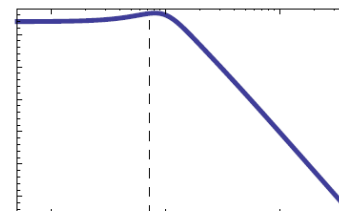
$$\begin{aligned} & \left. \frac{j\omega - 1}{(j\omega - 1)((j\omega)^2 - j\omega + 1)} \right|_{\omega=1/\sqrt{2}} \\ &= \frac{\frac{j}{\sqrt{2}} - 1}{\left(\frac{j}{\sqrt{2}} + 2\right)\left(-\frac{1}{2} - \frac{j}{\sqrt{2}} + 1\right)} \\ &= \frac{\frac{j}{\sqrt{2}} - 1}{-\frac{3}{2}\left(\frac{j}{\sqrt{2}} - 1\right)} = -\frac{2}{3} \end{aligned}$$

(need to guess this, e.g., by mouseclicking in Matlab)

$$G(s) = \frac{s-1}{s^3 + s^2 - s + 2}$$

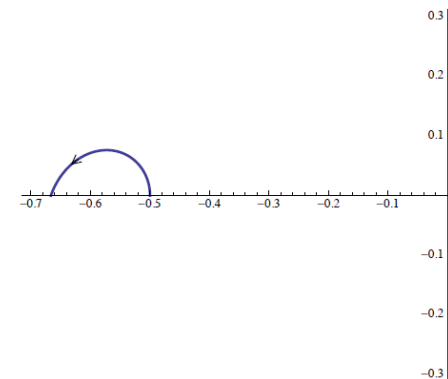
(2 open-loop RHP poles)

Bode plot:



Nyquist plot:

$$\begin{aligned} \omega = 0 & \quad M = 1/2, \phi = 180^\circ \\ \omega = 1/\sqrt{2} & \quad M = 2/3, \phi = 180^\circ \\ \omega \rightarrow \infty & \quad M \rightarrow 0, \phi \rightarrow 180^\circ \end{aligned}$$

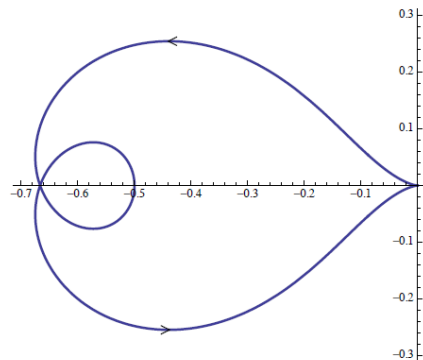


# Example 3

$$G(s) = \frac{s-1}{s^3 + s^2 - s + 2}$$

(2 open-loop RHP poles)

Nyquist plot:



$$\begin{aligned} \#(\odot \text{ of } -1/K) \\ = \#(\text{RHP CL poles}) \\ - \underbrace{\#(\text{RHP OL poles})}_{=2} \end{aligned}$$

$K \in \mathbb{R}$  is stabilizing if  
and only if

$$\#(\odot \text{ of } -1/K) = -2$$

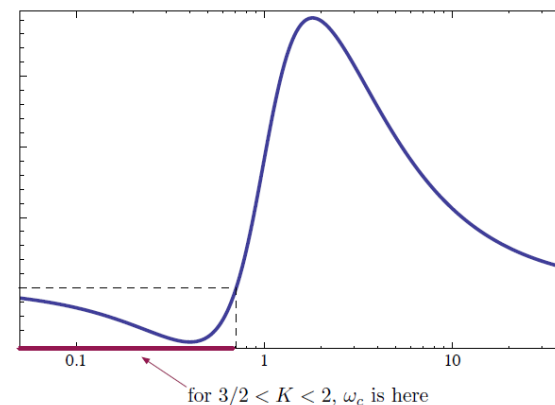
Which points  $-1/K$  are  
encircled twice  $\odot$  by this  
Nyquist plot?

only  $-2/3 < -1/K < -1/2$

$$\Rightarrow \frac{3}{2} < K < 2$$

CL stability range for  $G(s) = \frac{s-1}{s^3 + s^2 - s + 2}$ :  $K \in (3/2, 2)$

We can interpret this in terms of phase margin:

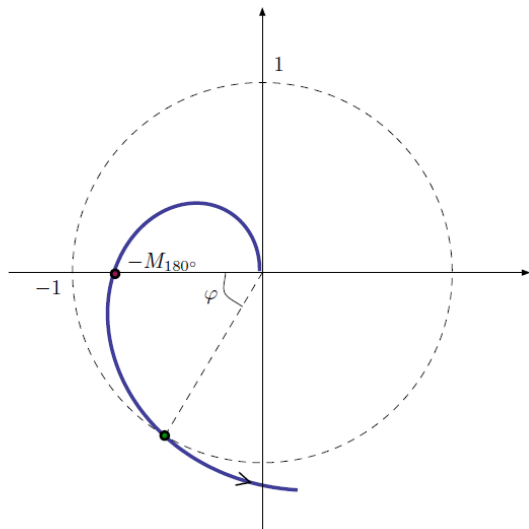


So, in this case, **stability**  $\iff$  **PM**  $< 0$  (atypical case; Nyquist  
criterion is the only way to resolve this ambiguity of Bode  
plots).

# Stability Margins

How do we determine stability margins (GM & PM) from the Nyquist plot?

GM & PM are defined relative to a given  $K$ , so consider Nyquist plot of  $KG(s)$  (we only draw the  $\omega > 0$  portion):



How do we spot GM & PM?

- ▶ GM =  $1/M_{180^\circ}$ 
  - if we divide  $K$  by  $M_{180^\circ}$ , then the Nyquist plot will pass through  $(-1, 0)$ , giving  $M = 1, \phi = 180^\circ$
- ▶ PM =  $\varphi$ 
  - the phase difference from  $180^\circ$  when  $M = 1$