

# Eddy Covariance Method

for Scientific, Industrial, Agricultural,  
and Regulatory Applications



George Burba

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LI-COR® Biosciences



G. Burba

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A Field Book on Measuring  
Ecosystem Gas Exchange and  
Areal Emission Rates



LI-COR® Biosciences

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This book has been created to familiarize a reader with general theoretical principles, requirements, applications, as well as planning and processing steps of the eddy covariance method. It is intended to assist readers in furthering of their understanding of the method, and provide references such as micrometeorology textbooks, network guidelines and journal papers. In particular, it is designed to help scientific, industrial, agricultural, and regulatory research projects and monitoring programs in the field deployment of the eddy covariance method in applications beyond micrometeorology.

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# Table of Contents

<b>Part One: Overview of Eddy Covariance Principles</b>	<b>7</b>
Flux measurements	9
State of methodology	10
What is flux?	11
Airflow in ecosystems	12
Eddies at a single point	13
Surface with no flux	14
Surface with flux	15
Actual fast data	16
How to measure flux	17
Basic derivations	18
Classical equation	19
Practical formulas	20
Major assumptions	21
Major sources of errors	22
Error treatment	24
Use in non-traditional terrains	26
Summary of the theory	27
From theory to workflow	28
Typical workflow	29
<b>Part Two: Designing An Eddy Covariance Experiment</b>	<b>31</b>
<b>Section 2.1 Setting Purpose and Selecting Variables</b>	<b>31</b>
2.1.1 Scientific applications	36
<i>Climate change research</i>	36
<i>Ecosystem gas exchange for various purposes</i>	37
<i>Hydrology</i>	39
<i>Oceanography</i>	39
2.1.2 Industrial applications	40
2.1.3 Agricultural applications	42
2.1.4 Regulatory applications	44
<b>Section 2.2 Instrument Principles Helpful in Designing the Station</b>	<b>45</b>
<i>Outline</i>	46
<i>Sonic anemometer: key elements of design</i>	47
<i>Gas analyzers: key elements of optical design</i>	49
<i>Gas analyzers: key elements of physical design</i>	54
<i>Implications of gas analyzer design for eddy covariance</i>	59

<b>Section 2.3 Selecting Eddy Covariance Instrumentation</b>	<b>61</b>
<i>Essential criteria</i>	62
<i>Understanding essential specifications</i>	63
<i>Other important criteria</i>	65
<i>Flow distortion considerations</i>	67
<i>Power considerations</i>	70
<i>Carbon footprint considerations</i>	71
<i>Setup and maintenance considerations</i>	72
<i>Hardware summary</i>	73
<b>Section 2.4 Details for Some Specific Instrument Models</b>	<b>75</b>
2.4.1 Sonic anemometer models	76
2.4.2 Open path LI-7500A CO <sub>2</sub> /H <sub>2</sub> O analyzer	78
<i>Specifications</i>	79
<i>Installation and maintenance</i>	80
<i>Applications</i>	81
2.4.3 Open path LI-7700 CH <sub>4</sub> gas analyzer	82
<i>Specifications</i>	83
<i>Installation</i>	84
<i>Maintenance</i>	85
<i>Applications</i>	86
2.4.4 Enclosed LI-7200 gas analyzer	89
<i>Specifications</i>	91
<i>Installation</i>	92
<i>Tube length</i>	94
<i>Insulation and heating</i>	95
<i>Maintenance</i>	97
<i>Applications</i>	99
2.4.5 Closed path LI-7000 gas analyzer	101
<i>Specifications</i>	102
<i>Installation and maintenance</i>	103
<i>Applications</i>	104
2.4.6 Auxiliary measurements	105
2.4.7 Complete eddy covariance stations	106
<b>Section 2.5 Selecting Software</b>	<b>107</b>
<i>Types of software</i>	108
<i>Software models</i>	109
<i>EddyPro®</i>	110



<i>Frequent pitfalls</i> .....	113
<b>Section 2.6 Selecting Location of the Study and Position of the Station</b> .....	<b>115</b>
<i>Location requirements</i> .....	116
<i>Power and access considerations</i> .....	117
<i>Measurement height, atmospheric layers, and footprint</i> .....	118
<b>Section 2.7 Importance of Flux Footprint</b> .....	<b>121</b>
<i>Visualizing the concept</i> .....	123
<i>Models</i> .....	124
<i>Effect of measurement height</i> .....	125
<i>Height near the station</i> .....	126
<i>Measurement height summary</i> .....	127
<i>Effect of surface roughness</i> .....	128
<i>Roughness near the station</i> .....	129
<i>Roughness summary</i> .....	130
<i>Height at different roughness</i> .....	131
<i>Roughness at different heights</i> .....	132
<i>Height and roughness summary</i> .....	133
<i>Effect of thermal stability</i> .....	134
<i>Stability summary</i> .....	135
<i>Summary of footprint</i> .....	136
<b>Section 2.8 Planning Contingencies and Long-Term Maintenance</b> .....	<b>137</b>
<i>Key activities</i> .....	138
<i>Frequent pitfalls</i> .....	139
<b>Section 2.9 Summary of Experimental Design</b> .....	<b>141</b>
<b>Part Three: Implementing An Eddy Covariance Experiment</b> .....	<b>145</b>
<b>Section 3.1 Placing the Tower</b> .....	<b>145</b>
<b>Section 3.2 Placing the Instrumentation</b> .....	<b>149</b>
<i>Sensor height and footprint</i> .....	150
<i>Sensor height and frequency response</i> .....	151
<i>Sensor orientation and flow distortion</i> .....	152
<i>Sensor separation and flow distortion</i> .....	153
<i>Rules of thumb</i> .....	154
<b>Section 3.3 Initial Testing of Data Collection and Retrieval</b> .....	<b>157</b>
<i>Data collection and data quality</i> .....	158
<i>Data retrieval</i> .....	160
<b>Section 3.4 Continuous Maintenance</b> .....	<b>161</b>

<b>Section 3.5 Experiment Implementation Summary .....</b>	<b>163</b>
<b>Part Four: Processing Eddy Covariance Data .....</b>	<b>165</b>
<b>Section 4.1 Pre-conditioning of Raw Data .....</b>	<b>165</b>
Unit conversion .....	167
Despiking .....	168
Calibration coefficients .....	169
Coordinate rotation .....	170
Time delay .....	172
De-trending .....	174
Choosing time average .....	175
<b>Section 4.2 Applying Frequency Response Corrections .....</b>	<b>177</b>
Main contributors .....	179
Cospectra .....	181
Transfer functions .....	184
Applying frequency response corrections .....	185
Time response .....	186
Tube attenuation .....	187
Path and volume averaging .....	191
Sensor separation .....	192
Sensor response mismatch .....	193
Low-pass filtering .....	194
High-pass filtering .....	195
Digital sampling .....	196
Total transfer function .....	197
Frequency response summary .....	198
<b>Section 4.3 Applying Sonic Anemometer Corrections .....</b>	<b>199</b>
Air temperature .....	200
Sonic sensible heat flux .....	201
Angle of attack .....	202
<b>Section 4.4 Applying Webb-Pearman-Leuning Terms .....</b>	<b>203</b>
Concept .....	204
Full equation .....	205
Open-path .....	207
Closed-path .....	208
Enclosed .....	209
<b>Section 4.5 WPL and Spectroscopic Corrections .....</b>	<b>211</b>

Spectroscopic effects .....	212
Concept .....	213
Example .....	214
Equation .....	215
Algorithm .....	217
<b>Section 4.6 WPL and Open-path Instrument Surface Heating .....</b>	<b>219</b>
Fundamental equation .....	221
Supplementary equation .....	222
Deciding on the corrections .....	223
Methods of correction .....	224
<b>Section 4.7 Calculating Flux From Dry Mole Fraction without WPL Terms .....</b>	<b>227</b>
Concept .....	228
Requirements .....	229
Example .....	230
Pressure effects .....	231
Summary .....	232
<b>Section 4.8 Other Corrections and Flux Storage .....</b>	<b>233</b>
<b>Section 4.9 Summary of Corrections .....</b>	<b>237</b>
<b>Section 4.10 Quality Control of Eddy Covariance Flux Data .....</b>	<b>241</b>
Key reasons .....	242
Key steps .....	243
Quality control during nighttime .....	245
Energy budget closure .....	246
Cospectral analysis .....	248
Other methods .....	251
Filling-in missing data .....	252
Long-term integration .....	253
<b>Section 4.11 Summary of Eddy Covariance Workflow .....</b>	<b>255</b>
Experiment design .....	257
Experiment implementation .....	258
Data processing and analysis .....	259
<b>Part Five: Overview of Alternative Flux Methods .....</b>	<b>261</b>
Eddy accumulation .....	264
Relaxed eddy accumulation .....	265
Bowen ratio method .....	266
Aerodynamic approach .....	267

Resistance approach .....	268
Chamber measurements .....	269
<b>Part Six: Future Developments .....</b>	<b>271</b>
Expansion in disciplines .....	273
Expansion in applications .....	274
Expansion in species .....	275
Expansion in terrains .....	276
Expansion in scale: long-range devices .....	277
Expansion in scale: mobile .....	278
Expansion in scale: global networks .....	279
Expansion in scale: planetary .....	280
<b>Part Seven: Summary of Eddy Covariance Method .....</b>	<b>281</b>
<b>Part Eight: Useful Resources .....</b>	<b>285</b>
Printed books .....	286
Electronic books, lectures, and guides .....	287
Websites .....	288
Resources at LI-COR: training .....	289
Resources at LI-COR: knowledge base .....	290
Resources at LI-COR: support .....	291
<b>Appendix 1. Example of Eddy Covariance Site: Overview of LERS .....</b>	<b>293</b>
Purpose .....	294
Products to variables .....	296
Variables to hardware and software .....	297
Planning hardware arrangement .....	299
Selecting location .....	300
Maintenance and usage planning .....	301
Tower and instrument implementation .....	302
Data testing, collection, and processing .....	303
Data examples .....	304
<b>References and Further Reading .....</b>	<b>305</b>
<b>Index .....</b>	<b>319</b>
<b>Credits .....</b>	<b>329</b>



# Introduction

- Measurements of gas fluxes in and out of an ecosystem, quantifying evaporative water losses from an agricultural field, or monitoring of gas emission rates over a carbon sequestration injection site can be done with a wide variety of techniques
- Of these techniques, the eddy covariance method is one of the most accurate, direct and defensible approaches available to date for determining emission and consumption rates of various gases and water vapor over areas with sizes ranging from a few hundred to millions of square meters
- The method relies on direct and fast measurements of actual gas transport by a 3-dimensional wind in real time *in situ*, resulting in calculations of turbulent fluxes within the atmospheric boundary layer

The eddy covariance method provides measurements of gas emission and consumption rates, and also allows measurements of momentum, sensible heat, and latent heat (*e.g.*, evapotranspiration, evaporative water loss, *etc.*) fluxes integrated over areas of various sizes.

Fluxes of  $H_2O$ ,  $CO_2$ ,  $CH_4$ ,  $N_2O$  and other gases are characterized above soil and water surfaces, plant canopies, and urban or industrial areas, from a single-point measurement using permanent or mobile stations.

This method was widely used in micrometeorology for over 30 years, but now, with firmer methodology and advanced instrumentation, it is available to any discipline, including

science, industry, agriculture, environmental monitoring and inventory, and emission regulations.

While the applications are quite diverse in scope and requirements, there are many methodological commonalities in using the eddy covariance technique in all of these applications.

This book focuses primarily on these commonalities, and then explains the specific steps needed to tailor the method for a particular application or research project.

Below are a few examples of books that broadly cover and compare various flux measurement methods, including the eddy covariance technique.

## References

Monteith, J., and M. Unsworth, 2008. Principles of Environmental Physics. Academic Press, Elsevier, Burlington, San Diego, London, 434 pp.

Hatfield, J., and J. Baker (Eds.), 2005. Micrometeorology in Agricultural Systems. ASA-CSSA-SSSA, Madison, Wisconsin, 588 pp.

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Baldocchi, D., 2013. A Brief History on Eddy Covariance Flux Measurements: A Personal Perspective. FluxLetter, 5(2):1-8

- Modern instruments and software make the eddy covariance method easily available and widely-used in studies beyond micrometeorology, such as ecology, hydrology, environmental and industrial monitoring, agricultural and regulatory applications, *etc.*
- The main remaining challenge of the eddy covariance method for a non-expert is the sheer complexity of system design and implementation, and processing of the large volume of data
- Although modern instrument systems and software take care of most of these complexities, some basic understanding of eddy covariance principles and resulting requirements may still be helpful in successful implementation of the method

The specific applications of the eddy covariance method are numerous, and may require specific mathematical approaches and processing workflows.

Thus, there is no one single recipe for using the method, and it is helpful to further study key aspects of the method in relation to a specific measurement site and a specific measurement purpose.

The basic information presented in this book is intended to provide a foundational understanding of the eddy covariance method, and to help new eddy covariance users design experiments for their specific needs.

A deeper understanding of the method can be obtained via more advanced sources, such as micrometeorology textbooks, flux network guidelines, and journal papers.

Below are a few examples of such sources of information focused specifically on the eddy covariance methodology and field deployment.

## References

Aubinet, M., T. Vesala, and D. Papale (Eds.), 2012. Eddy Covariance: A Practical Guide to Measurement and Data Analysis. Springer, Dordrecht, Heidelberg, London, New York, 442 pp.

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Yamanoi, K., et al. (Eds.), 2012. *Practical Handbook of Tower Flux Observations*. Hokkaido Research Center, Forestry and Forest Products Research Institute, Sapporo, Japan, 196 pp. (Electronic Edition in English)



- To help those new to eddy covariance gain a basic understanding of the method and to point out valuable references
- To provide explanations in a simplified manner first, and then elaborate with specific details
- To promote a further understanding of the method via more advanced sources (micrometeorology textbooks, scientific papers, *etc.*)
- To help design experiments for the specific needs of a new eddy covariance user for scientific, industrial, agricultural and regulatory applications

In this book, we will try to help those new to eddy covariance understand the general principles, requirements, applications, and processing steps.

Explanations are given in a simplified manner first, and are then elaborated on with specific examples. Alternatives to the traditionally used approaches are also mentioned.

Each page is divided into a top portion, with key points and summaries, and a bottom portion, with explanations, details, and recommended further reading.

In most cases, the top part of the page describes the concept or formulation, or lists what needs to be done, and how. The bottom part of the page explains the reasoning behind the steps that need to be performed.

For those who prefer to read this book in electronic format on an e-reader, illustrations and text are formatted such that they are easily read in daylight and in black-and-white text. Links throughout the text are [hyperlinked](#), and can be clicked to navigate to other pages in the electronic version of the book.

We intend to keep the content of this book current and easy to use, so please do not hesitate to write with any questions, updates and suggestions to 'george.burba@licor.com' with the subject '2013 EC Book'.

The following icons are used throughout the text to indicate critical moments and key literature:



An exclamation point icon indicates warnings, information of high importance, or describes potential pitfalls related to the topic on a specific page.



A book icon indicates scientific references and other useful sources of information related to the topic on a specific page. These are listed, when possible, in order from most relevant or easy to understand, to broader or more complex.

<b>Part 1.</b>	Overview of Eddy Covariance Principles
<b>Part 2.</b>	Designing an Eddy Covariance Experiment
<b>Part 3.</b>	Implementing an Eddy Covariance Experiment
<b>Part 4.</b>	Processing Eddy Covariance Data
<b>Part 5.</b>	Overview of Alternative Flux Methods
<b>Part 6.</b>	Future Developments
<b>Part 7.</b>	Summary of the Eddy Covariance Method
<b>Part 8.</b>	Useful Resources
<b>Appendix I.</b>	Example of an Eddy Covariance Site

There are eight main parts in this book. The first part, Overview of Eddy Covariance Principles, explains the basics of the eddy covariance theory, key derivations and assumptions, resulting requirements for the method, and main steps in the workflow to address all of the key requirements.

The second part, Designing an Eddy Covariance Experiment, provides a detailed description of each sequential step in the design of the eddy covariance experiment, highlights the most critical moments in this process and the most important concepts to consider before moving to the field.

Part 3, Implementing an Eddy Covariance Experiment, describes key steps during the field installation of the eddy covariance station.

Part 4, Processing Eddy Covariance Data, explains the data processing steps. These steps are usually done in software, but it is helpful to understand what exactly is being done to the data, and why, in order to make sure that the software is configured correctly and the results make sense.

Part 5, Overview of Alternative Flux Methods, briefly outlines the principles, and the pros and cons of other meteorological methods that can be used in cases where eddy covariance is not suitable or may provide unreliable results.

Part 6, Future Developments, describes the very latest upcoming developments of the eddy covariance method, its use, and scope.

Part 7 provides a brief summary of the book, and Part 8 describes further resources on the topic, such as books, lectures, guides, and web-sites.

The Appendix contains a detailed example of a fairly comprehensive eddy covariance field facility at LI-COR Biosciences to give the reader a more practical feel for the method and its implementation.

We would like to acknowledge a number of scientists who have contributed to this book directly via valuable advice and indirectly via scientific collaborations, papers, textbooks, data sets, and personal communications.

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We thank FluxNet and its regional networks, both past and active (*e.g.*, AmeriFlux, AsiaFlux, CCP and FluxNet-Canada, Carbo-Europe, Japan-Flux, IMECC, OzFlux, *etc.*), as well as ICOS, NEON, InGos, iLEAPS and other organizations, and their members, for providing access to the field data, setup guidelines, collection and processing instructions, and formats for their eddy covariance stations.

We particularly thank Dr. James Kathilankal, and Mr. Israel Begashaw for peer-reviewing the book, Dr. Gerardo Fratini for reviewing parts of the book related to EddyPro® and flux processing, and Mr. Bill Miller for reviewing parts related to analyzer specifications. We would also like to thank Dr. Dayle McDermitt for valuable advice for sections on instrument principles and surface heating.

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Also, we would like to thank numerous other researchers, technicians and students who, through years of use in the field, have developed the eddy covariance method to its present level and have proven its effectiveness with studies and scientific publications.

Part One:

# Overview of Eddy Covariance Principles

- Flux measurements
- State of the methodology
- Air flow in ecosystems
- How to measure flux
- Derivation of key equations
- Major assumptions
- Major sources of errors
- Use in non-traditional terrains
- Summary of the theory
- Resulting workflow



The first part of this book is dedicated to the basics of the eddy covariance theory.

The following topics are discussed: flux measurements; state of methodology; air flow in ecosystems; surface with and without a flux; how to measure flux; derivation of key equations; major assumptions; major sources of

errors; error treatment overview; use in non-traditional terrains; and summary of the resulting workflow when designing the experiment and conducting eddy covariance measurements.

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Swinbank, W., 1951. The measurement of vertical transfer of heat and water vapor by eddies in the lower atmosphere. *Journal of Meteorology*, 8: 135-145

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Hoover, C. (Ed.), 2008. *Field measurements for forest carbon monitoring: A landscape-scale approach*. Springer, New York, 242 pp.

- Flux measurements are widely used to estimate the exchange of heat, water, and carbon dioxide, as well as methane and other trace gases
- The eddy covariance method is one of the most direct and defensible ways to measure such fluxes
- The method is mathematically complex, and requires a lot of care setting up and processing data – *but it is worth it!*

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Aubinet, M., T. Vesala, and D. Papale (Eds.), 2012. Eddy Covariance: A Practical Guide to Measurement and Data Analysis. Springer, Dordrecht, Heidelberg, London, New York, 442 pp.

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Munger, B., and H. Loescher, 2008. AmeriFlux Guidelines for Making Eddy Covariance Flux Measurements. AmeriFlux: [http://public.ornl.gov/ameriflux/measurement\\_standards\\_020209.doc](http://public.ornl.gov/ameriflux/measurement_standards_020209.doc)



- Uniform terminology and a single methodology are still being developed for the eddy covariance method
- Much of the effort is being done by networks (*e.g.*, FluxNet, ICOS, NEON, *etc.*) to unify various approaches
- Here we present one of the conventional ways to implement the eddy covariance method

In the past several years, efforts of the flux networks have led to significant progress in unifying the terminology and general standardization of processing steps.

The methodology itself, however, is more difficult to unify. Various experimental sites and different purposes of studies dictate different treatments. For example, if turbulence is the focus of the studies, the gas density corrections may not be necessary.

Meanwhile, if CO<sub>2</sub> and CH<sub>4</sub> emission rates are measured for the purpose of cap-and-trade compliance, then computing momentum fluxes and wind components' spectra may not be crucial.

Here we will describe the conventional ways of implementing the eddy covariance method and give some information on newer, less established venues.

## References .....

Aubinet, M., T. Vesala, and D. Papale (Eds.), 2012. Eddy Covariance: A Practical Guide to Measurement and Data Analysis. Springer, Dordrecht, London, New York, 442 pp.

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- Flux – how much of something moves through a unit area per unit time
- Flux is dependent on:
  1. the number of things crossing the area
  2. the size of the area being crossed
  3. the time it takes to cross this area

In very simple terms, flux describes how much of something moves through a unit area per unit time.

For example, if 100 birds fly through a 1 x 1 meter window each minute – the flux of birds is 100 birds per 1 square meter per 1 minute ( $100 \text{ B m}^{-2} \text{ min}^{-1}$ ). If the window was 10 x 10 meters, the flux would be 1 bird per 1 square meter per 1 minute, because  $100 \text{ birds}/100 \text{ sq. meters} = 1$ , so now the flux is  $1 \text{ B m}^{-2} \text{ min}^{-1}$ .

Flux is dependent on: (1) the number of things crossing an area, (2) the size of an area being crossed, and (3) the time it takes to cross this area.

In more scientific terms, flux can be defined as an amount of an entity that passes through a closed (*i.e.*, a Gaussian) surface per unit of time.

If net flux is away from the surface, the surface may be called a source. For example, a lake surface is a source of  $\text{H}_2\text{O}$  released into the atmosphere in the form of water vapor through the process of evaporation.

If the opposite is true, the surface is called a sink. For example, a green canopy may be a sink of  $\text{CO}_2$  during the day, because green leaves take up  $\text{CO}_2$  from the atmosphere through the process of photosynthesis.





- Air flow can be imagined as a horizontal flow of numerous rotating eddies
- Each eddy has 3-D components, including a vertical wind component
- The diagram looks chaotic, but components can be measured from a tower

Air flow can be imagined as a horizontal flow of numerous rotating eddies. Each eddy has 3-D components, including vertical movement of the air. The situation looks chaotic at first, but these components can be easily measured from the tower. On the diagram above, the air flow is represented by the large arrow that passes through the tower, and consists of differently sized eddies.

Conceptually, this is the framework for atmospheric eddy transport.

Closer to the ground, there is a stronger probability of smaller eddies being responsible for the transport of most of the flux. Smaller eddies rotate faster, and hence, more transport is done by higher frequency movements of air.

Further away from the ground, there is a stronger probability of larger eddies being responsible for the transport of most of the flux. Larger eddies rotate slower, and hence, more transport is done by lower frequency movements of air.

In practical terms, there is always a mix of different eddy sizes, so some transport is done at higher frequencies and some at lower ones, covering the whole range of frequencies: from large movements on the order of hours, to small ones on the order of 1/10 of a second.

Closer to the ground, the flux transport is shifted to higher frequencies, and further away from the ground it is shifted to lower frequencies.

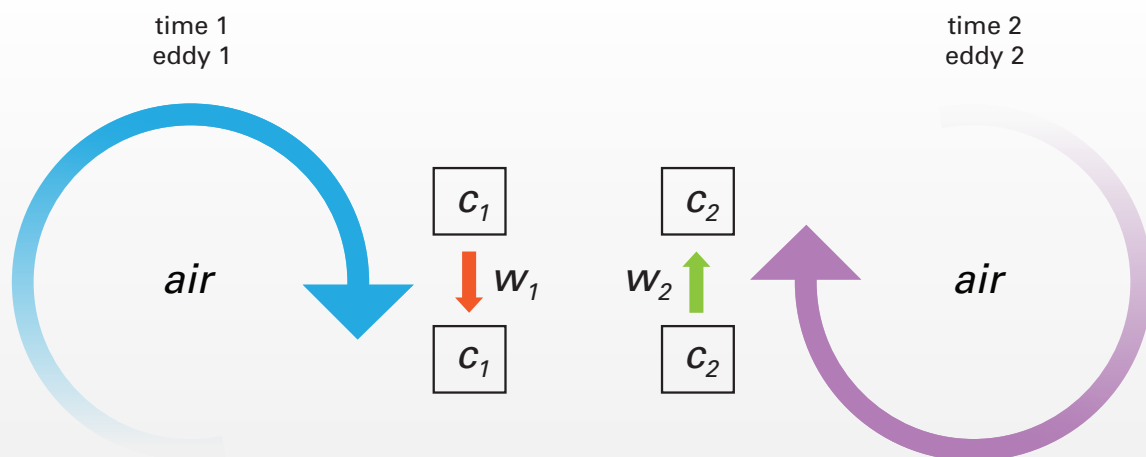
Conceptually, this is the mechanism of atmospheric eddy transport.

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### At a single point on the tower:

Eddy 1 moves parcel of air  $c_1$  down with the speed  $w_1$ ,  
then eddy 2 moves parcel  $c_2$  up with the speed  $w_2$

Each parcel has concentration, temperature, humidity;  
if we know these and the speed – we know the flux

On the previous page, the air flow was shown to consist of numerous rotating eddies. Here, let us look closely at the eddies at a single point on the tower.

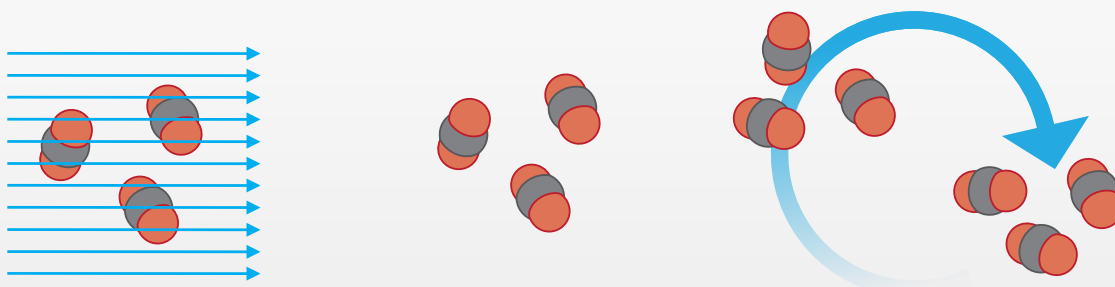
At one moment (time 1), eddy number 1 moves air parcel  $c_1$  downward with the speed  $w_1$ . At the next moment (time 2) at the same point, eddy number 2 moves air parcel  $c_2$  upward with speed  $w_2$ . Each air parcel has its own characteristics, such as gas concentration, temperature, humidity, *etc.*

If we can measure these characteristics and the speed of the vertical air movement, we will know the vertical upward or downward fluxes of gas and water vapor concentrations, temperature, and humidity.

For example, if at one moment we know that three molecules of  $\text{CO}_2$  went up, and in the next moment only two molecules of  $\text{CO}_2$  went down, then we know that the net flux over this time was upward, and equal to one molecule of  $\text{CO}_2$ .

This is the general principle of eddy covariance measurements: covariance between the concentration of interest and vertical wind speed.

- The eddy covariance method works by measuring vertical turbulent transport of gas to and from the surface
- With no flux added into the mean flow by the measured area, the eddies move the same number of gas molecules up and down



Mean flow carries gas molecules over the measured area

Measured area adds no molecules into the mean flow (= no flux)

Eddy motions carry the same number of molecules up and down

Another way to visualize the key physical principle behind the eddy covariance measurements is to first imagine an area that adds *no* molecules of the gas of interest to the mean flow, and then compare it to the same area that adds molecules into the flow.

For example, let us imagine a mean flow that carries 3 molecules of  $\text{CO}_2$  over the area of interest from left to right, as shown in the diagram above.

Since the area in the middle did not add anything to the flow, the eddy movements at the downwind measurement point on the right would carry, on average, 3 molecules upwards, and 3 molecules downward, with no net flux. Thus, over a long period, such as a half hour or an hour, the eddy covariance station would measure a flux of zero from the area of interest in the middle.

In this example, we make several assumptions to keep the situation simple for now. These assumptions are addressed later in the mathematical expressions for eddy covariance, and are primarily dealt with by proper site selection, installation and flux processing. They do not fundamentally affect the visualization of the main physical principle of how instruments on the station measure the eddy transport of flux.

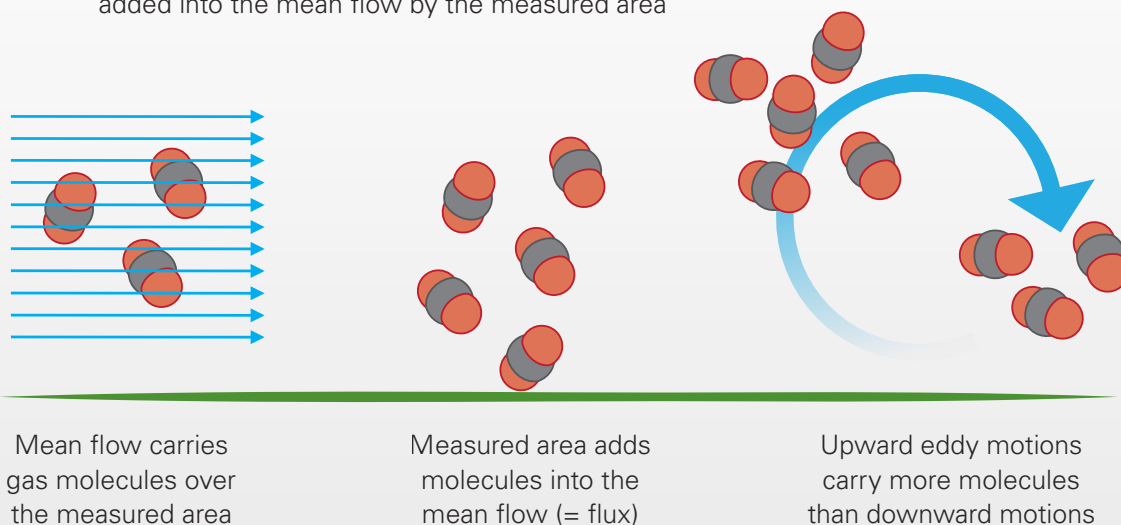
For now, we assume that the surface has the same temperature as the air, such that no temperature flux (*e.g.*, sensible heat flux) is added to the air, and thus, no thermal expansions or contractions affect the density of the air or the  $\text{CO}_2$  content.

We also assume that the surface does not add any water molecules to the mean flow, such that no water vapor flux (*e.g.*, latent heat flux) is added to the air, and thus, no water dilution affects the density of the air or the  $\text{CO}_2$  content.

Furthermore, we assume that surface does not move with the wind, and does not make air pressure fluctuate in synch with the wind, such that no pressure-related expansions or contractions affect the density of the air or the  $\text{CO}_2$  content.

Finally, we assume that no additional air flow or  $\text{CO}_2$  injection comes from the sides (*e.g.*, from the direction perpendicular to this page or the picture above) or from above, and there is no convergence of two different flows into one, or divergence of a single flow into multiple flows that occurs over the surface shown.

- With flux added into the mean flow by the measured area, the eddies move more gas up than down, transporting it from the surface into the atmosphere
- If we know the bias between up and down motions, we know how much was added into the mean flow by the measured area



In the previous page, we imagined a mean flow that carried 3 molecules of  $\text{CO}_2$  over the area of interest from left to right, and *no* molecules of the  $\text{CO}_2$  were added to the mean flow.

Now let us imagine the same situation, but with the surface in the middle adding 2 molecules to the mean flow. Since the area in the middle added 2 molecules to the mean flow, the eddy motions at the downwind measurement point on the right would carry, on average, more molecules upward than downward, with some net  $\text{CO}_2$  flux.

Thus, over a long period, such as 30-60 minutes, the eddy covariance station located on the right would measure some flux from the area of interest in the middle.

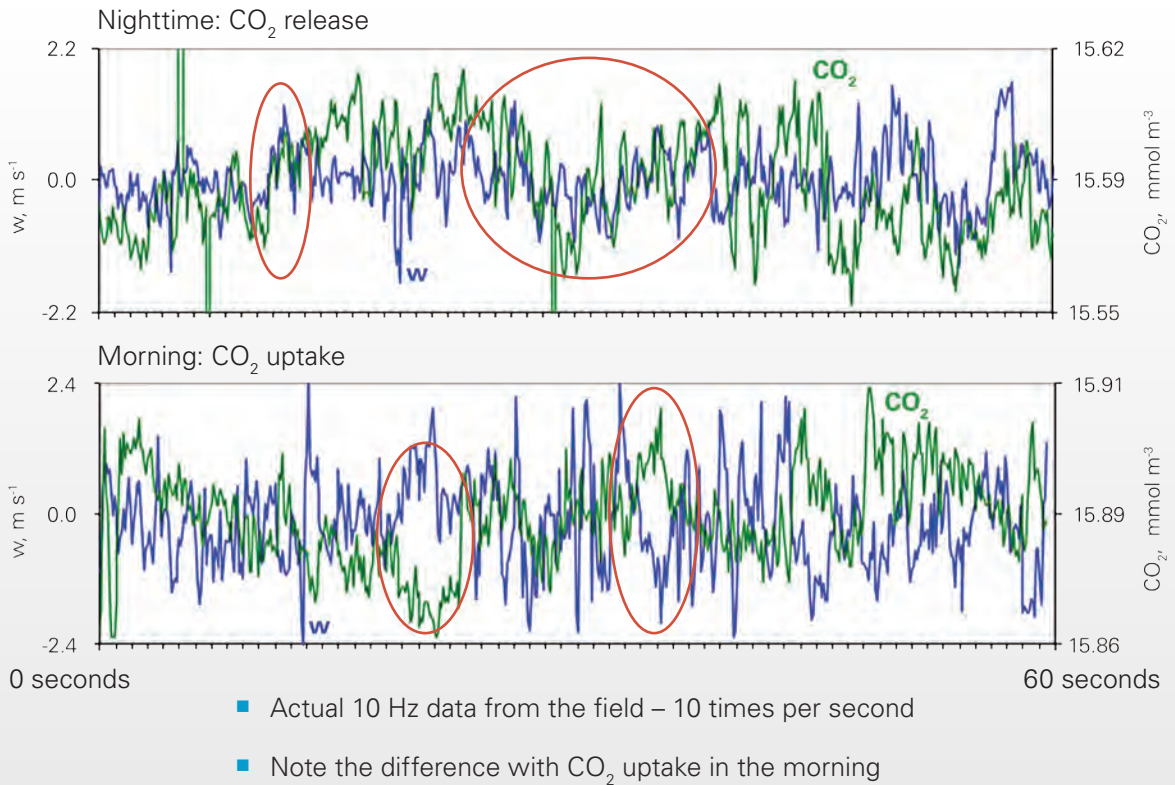
Compare the situation when no molecules of  $\text{CO}_2$  are added to the mean flow by the area of interest with the situation when such an area adds molecules into the mean flow; this describes the physical essence of eddy covariance measurements. Flux is measured from the area of interest,

which adds gas or energy to the mean flow or takes them away.

It is also important to note that in this way we only measure the turbulent transport of the  $\text{CO}_2$ , and must have well-developed turbulence such that other mechanisms of transport (*e.g.*, molecular diffusion, advection, *etc.*) are negligibly small. This generally is the case during the day, and during nights with wind speeds above 1.0 meter per second or 2.2 miles per hour.

Alternatively, the impact of other mechanisms of transport can be estimated, or measured directly using gas concentration and wind speed profiles and transects.

The ability of the eddy covariance method to provide direct measurements of half-hourly or hourly fluxes integrated over an area of interest, continuously throughout the years, covering most of the days and significant portions of the nights, is an important practical advantage over other present flux measurement methods.



The actual field data look remarkably similar to the thought experiments described on the previous three pages. The picture above shows vertical wind speed ( $w$ ) and CO<sub>2</sub> measured simultaneously at a fast rate by an eddy covariance station located in the middle of a field covered with green vegetation.

At night, photosynthesis is not occurring, and respiration from the soil and the canopy adds a small CO<sub>2</sub> flux to the atmosphere. This process can be observed in the top plot by looking at what happens to the CO<sub>2</sub> content when wind is moving upwards (positive  $w$ ) and downwards (negative  $w$ ).

On many occasions, the upward movement of the wind carries a higher CO<sub>2</sub> content than the downward movement. The covariance is not very strong due to small nighttime fluxes, but is still visible at higher frequency movements (smaller red oval on the left) and at lower frequency movements (large red oval on the right). In such situations, the covariance of  $w$  and CO<sub>2</sub> is positive, and the flux of CO<sub>2</sub> is away from the canopy and soil surface.

In the morning, the sun is up and canopy photosynthesis is occurring, overcoming respiration. This process removes CO<sub>2</sub> from the atmosphere, and also can be observed in the bottom plot by watching what happens to the CO<sub>2</sub> content and vertical wind speed.

On many occasions, the upward movement of the wind carries a lower CO<sub>2</sub> content than the downward movement. The covariance is still not very strong due to a small flux rate, but is visible at lower frequency movements (smaller red oval on the left) and at higher frequency movements (large red oval on the right). In such situations, the covariance of  $w$  and CO<sub>2</sub> is negative, and the flux of CO<sub>2</sub> is directed toward the canopy.

Please notice the scale on the x-axes above, and note how rapidly the turbulent transport happens. This will have significant implications for the experiment and system design described later in the book in [Part 2](#).

## The physical principle:

If we know how many molecules went up with eddies at time 1, and how many molecules went down with eddies at time 2 at the same point – we can calculate vertical flux at that point and over that time period

## The mathematical principle:

Vertical flux can be represented as a covariance of the vertical velocity and concentration of the entity of interest

## The instrument challenge:

Turbulent fluctuations occur very rapidly, so measurements of up-and-down movements and of the number of molecules should be done very rapidly

Overall, the general physical principle for eddy flux measurement is to measure how many molecules are moving upward and downward over time, and how fast they travel.

Mathematically such vertical flux can be represented as a covariance between measurements of vertical velocity, the upward and downward movements, and the concentration of the entity of interest.

Such measurements require very sophisticated instrumentation, because turbulent fluctuations happen very quickly, and respective changes in concentration, density or temperature are quite small, and must be measured both very fast and very well.

The traditional eddy covariance method (also known as eddy correlation method, or EC) calculates only turbulent vertical flux, involves a lot of assumptions, and requires high-end instruments. On the other hand, it provides nearly direct continuous flux measurements if the assumptions are satisfied, or corrected for.

In the next few pages, we will discuss the math behind the method, and its major assumptions.



Strictly speaking, there is a difference between the terms “eddy covariance” and “eddy correlation”, and “eddy covariance” is a proper term for the commonly used method of flux measurements described in this book. Please refer to the textbook entitled ‘Micrometeorology’ by T. Foken (2008) for detailed explanations of the differences between these two terminologies.



In turbulent flow, vertical flux can be presented as:  
(s is the dry mole fraction of the gas of interest in the air)

$$F = \overline{\rho_d w s}$$

Reynolds decomposition is then used to break terms into means and deviations:

$$F = \overline{(\bar{\rho}_d + \rho'_d)(\bar{w} + w')(\bar{s} + s')}$$

Opening the parentheses:

$$F = (\bar{\rho}_d \bar{w} \bar{s} + \cancel{\bar{\rho}_d \bar{w} s'} + \cancel{\bar{\rho}_d w' \bar{s}} + \bar{\rho}_d w' s' + \cancel{\rho'_d \bar{w} \bar{s}} + \rho'_d \bar{w} s' + \rho'_d w' \bar{s} + \rho'_d w' s')$$

*averaged deviation from the average is zero*

Equation is simplified:

$$F = (\bar{\rho}_d \bar{w} \bar{s} + \bar{\rho}_d \bar{w}' s' + \bar{w} \rho'_d \bar{s}' + \bar{s} \rho'_d \bar{w}' + \rho'_d w' s')$$

In very simple terms, when we have turbulent flow, vertical flux can be represented by the equation at the top of this page: flux is equal to a mean product of air density ( $\rho_d$ ), vertical wind speed ( $w$ ), and the dry mole fraction ( $s$ ) of the gas of interest. The dry mole fraction is often called the mixing ratio.

Reynolds decomposition can be used to break the right-hand side of the top equation into means and deviations from these means. Air density is presented now as a sum of a mean over some time (a half hour, for example) and an instantaneous deviation from this mean, for example for every 0.05 or 0.1 seconds (denoted by a prime). A similar procedure is done with vertical wind speed, and with dry mole fraction of the substance of interest.

In the third equation, the parentheses are opened, and averaged deviations from the average are removed, because averaged deviation from an average is zero. So, the flux equation is simplified into the form at the bottom.



The term 'mixing ratio' is historically defined differently in chemistry and in micrometeorology. In chemistry, it describes the ratio of the constituent to the total mixture without this constituent. For example, moles of CO<sub>2</sub> would be divided by moles of non-dried air without CO<sub>2</sub>.

In micrometeorology, it usually describes the ratio of the constituent to the dry air. For example, moles (or grams) of CO<sub>2</sub> in the air would be divided by moles (or grams) of dry air with CO<sub>2</sub>.


Perhaps, the better, more universally understood alternative term to use in the context of this book would be 'dry mole fraction', or 'mole fraction in dry air'.

## References

For detailed and thorough calculations of this portion of the derivations, please see Lecture #3 (Part 1) in: Baldocchi, D., 2012. Advanced Topics in Biometeorology and Micro-

meteorology. Department of Environmental Science, UC-Berkeley, California:  
<http://nature.berkeley.edu/biometlab/espm228>

Now an important assumption is made (for conventional eddy covariance) – air density fluctuations are assumed to be negligible:



$$F = (\overline{\rho_d w s} + \overline{\rho_d w' s'} + \overline{w \rho_d' s'} + \overline{s \rho_d' w'} + \overline{\rho_d' w' s'}) = \overline{\rho_d w s} + \overline{\rho_d w' s'}$$

Then another important assumption is made – mean vertical flow is assumed to be negligible for horizontal homogeneous terrain (no divergence/convergence):

$$F \approx \overline{\rho_d} \overline{w' s'}$$

'Eddy Flux'

On this page, we see two important assumptions that are made in the conventional eddy covariance method.

First, the air density fluctuations are assumed to be negligible. Theoretically, with strong winds over a mountain ridge, for example, density fluctuations in the member  $\overline{s \rho_d' w'}$  may be non-negligible in comparison with the gas flux. However, in most cases when eddy covariance is used conventionally over reasonably flat and vast spaces, such as fields or plains, the air density fluctuations can be safely assumed to be negligible, for the purposes of this derivation.

Secondly, the mean vertical flow is assumed to be negligible for horizontal homogeneous terrain, so that no flow diversions or conversions occur.

With diversion and conversions assumed negligible, we arrive at the classical equation for eddy flux. Flux is equal to the product of the mean air density and the mean covariance between instantaneous deviations in vertical wind speed and mixing ratio.



There is increasing evidence, however, that if the experimental site is located on even a small slope, then the second assumption might not hold on some occasions. Thus, one needs to examine the specific experimental site in terms of flow diversions or conversions, and decide how to best correct for their effects.

## References

For a more detailed derivation up to this point, please refer to: Baldocchi, D., 2012. Advanced Topics in Biometeorology and Micrometeorology. Department of Environmental Science, UC-Berkeley, California (Lecture 3, Part 1): <http://nature.berkeley.edu/biometlab/espm228>

For the advanced reader, the complex derivation of a fundamental flux equation can be found in: Gu, L., W. Massman, R. Leuning, S. Pallardy, T. Meyers, *et al.*, 2012. The fundamental equation of eddy covariance and its application in flux measurements. *Agricultural and Forest Meteorology*, 152: 135–148



Any gas (CO<sub>2</sub>, CH<sub>4</sub>, N<sub>2</sub>O, H<sub>2</sub>O, *etc.*):

$$F = \overline{\rho_d} \overline{w's'}$$

Sensible heat flux:

$$H = \overline{\rho} C_p \overline{w'T'}$$

Traditional H<sub>2</sub>O flux:

$$E = \frac{M_w / M_a}{\overline{P}} \overline{\rho_d w'e'}$$

Latent heat flux (H<sub>2</sub>O flux in energy units):

$$LE \equiv \lambda E = \lambda \frac{M_w / M_a}{\overline{P}} \overline{\rho_d w'e'}$$

The top equation describes a classical formula for the eddy flux of virtually any gas of interest, such as CO<sub>2</sub>, CH<sub>4</sub>, N<sub>2</sub>O, O<sub>3</sub>, *etc.* The flux is computed from the mean dry air density multiplied by the mean covariance between deviations in instantaneous vertical wind speed and dry mole fraction (*e.g.*, mixing ratio).

Sensible heat flux is equal to the mean air density multiplied by the covariance between deviations in instantaneous vertical wind speed and temperature; conversion to energy units is accomplished by including the specific heat term.

There are multiple forms of the flux equation for water vapor, depending on the units of fast water vapor content. One typical example is shown in the third equation above. In addition, the water vapor flux is often computed in energy units (W m<sup>-2</sup>), and called latent heat flux, as shown in the last equation above. Latent heat flux describes the energy used in the process of evaporation, transpiration, or evapotranspiration.

## References

More details on practical formula are given in: Rosenberg, N., B. Blad, and S. Verma, 1983. *Microclimate. The biological environment*. A Wiley-Interscience, New York: 255-257

More details on mixing ratio and other relevant units are given by Foken *et al.* in Table 1.2, and resulting forms of

Hourly or integrated values of latent heat flux can be converted into other frequently used units (*e.g.*, mm d<sup>-1</sup>, inches ha<sup>-1</sup>, kg m<sup>-2</sup> h<sup>-1</sup>, *etc.*). When converted to volume or mass units, the latent heat flux is often called evapotranspiration rate (ET), evaporation rate (over wet non-vegetated surfaces), or evaporative water loss.



Please note that older instruments usually do not output fast dry mole fraction (fast mixing ratio), but rather measure fast density. So, the density corrections are required in post-processing as described in [Section 4.4](#). These corrections are not required for instruments outputting true mixing ratio at high speed, for example, the enclosed LI-7200 CO<sub>2</sub>/H<sub>2</sub>O gas analyzer.

the flux equation are given by Rebmann *et al.* in Table 3.1 in: Aubinet, M., T. Vesala, and D. Papale (Eds.), 2012. *Eddy Covariance: A Practical Guide to Measurement and Data Analysis*. Springer, Dordrecht, Heidelberg, London, New York, 442 pp.

- Measurements at a point can represent an upwind area
- Measurements are done inside the boundary layer of interest
- Fetch/footprint is adequate – fluxes are measured from the area of interest
- Flux is fully turbulent – most of the net vertical transfer is done by eddies
- Terrain is horizontal and uniform: average of fluctuations of  $w'$  is zero, air density fluctuations, flow convergence and divergence are negligible
- Instruments can detect very small changes at high frequency
- Air flow is not distorted by the installation structure or the instruments

In addition to the assumptions listed on the previous three pages, there are other important assumptions in the eddy covariance method:

- Measurements at a point are assumed to represent an upwind area
- Measurements are assumed to be done inside the boundary layer of interest, and inside the constant flux layer (details in Sections 2.6 and 3.2)
- Fetch and footprint are assumed adequate, so flux is measured from the area of interest (details in Section 2.7)
- Flux is fully turbulent
- Terrain is horizontal and uniform

- Air density fluctuations are negligible
- Flow divergences and convergences are negligible
- The instruments can detect very small changes at very high frequency
- Mean air flow and turbulence at the measurement point are not appreciably distorted by the installation structure or the instruments themselves

The degree to which some of these assumptions hold true depends on proper site selection and experimental setup. For others, it will largely depend on atmospheric conditions and weather. We will go into the details of these assumptions later.

## References .....

Aubinet, M., T. Vesala, and D. Papale (Eds.), 2012. Eddy Covariance: A Practical Guide to Measurement and Data Analysis. Springer, Dordrecht, Heidelberg, London, New York, 442 pp.

Baldocchi, D., 2012. Advanced Topics in Biometeorology and Micrometeorology. Department of Environmental Science, UC-Berkeley, California: <http://nature.berkeley.edu/biometlab/espm228>

Lee, X., W. Massman, and B. Law (Eds.), 2004. Handbook of Micrometeorology: A Guide for Surface Flux Measurement and Analysis. Kluwer Academic Publishers, Dordrecht, The Netherlands, 252 pp.

Measurements are not perfect: due to assumptions, physical phenomena, instrument problems, and specifics of terrain and setup

Fluxes could be over- or underestimated if errors are not prevented during the design and setup, or not corrected during data processing

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## Frequency response errors can be due to:

- System time response
- Tube attenuation
- Path and volume averaging
- Sensor separation
- Sensor response mismatch
- Low-pass filtering
- High-pass filtering
- Digital sampling
- *etc.*

Measurements are of course never perfect, due to assumptions, physical phenomena, instrument problems, and specifics of the particular terrain or setup. As a result, there are a number of potential flux errors, but they can be prevented, minimized, or corrected out.

First, there is a family of errors called frequency response errors. They include errors due to instrument time response, tube attenuation, path and volume averaging, sensor separation, sensor response mismatch, low and high pass filtering, and digital sampling.

Time response errors occur because instruments may not be fast enough to catch all the rapid changes that result from the eddy transport. Tube attenuation error is observed

in closed-path analyzers, and is caused by attenuation of the instantaneous fluctuation of the concentration in the sampling tube. Path averaging error is caused by the fact that the sensor path is not a point measurement, but rather is an integration over some distance; therefore, it can average out some of the changes caused by eddy transport.

Sensor separation errors occur due to the physical separation between the places where wind speed and concentration are measured, so covariance is computed for parameters that were not measured at the same point. There can also be frequency response errors caused by sensor response mismatch, and by filtering and digital sampling.

## Other key error sources:

- Spikes and noise
- Unleveled anemometer
- Wind angle of attack
- Sensor time delay
- Sonic heat flux errors
- Density fluctuations (WPL)
- Spectroscopic effects for LASERs
- Band-broadening for NDIR
- Oxygen in the ‘krypton’ path
- Gas flux storage
- Data filling
- *etc.*

In addition to frequency response errors, other key sources of errors include spikes and noise in the measurements, unleveled anemometer, wind angle of attack, sensor time delay (especially important in closed-path analyzers with long intake tubes), sonic heat flux errors, the Webb-Pearman-Leuning

density terms (WPL), spectroscopic effects (for LASER-based measurements), band-broadening effects (for NDIR measurements), oxygen sensitivity, gas flux storage, and data filling errors. Later in [Part 4](#), we will go through each of these terms and errors in greater detail.

## References

Fuehrer, P., and C. Friehe, 2002. Flux corrections revisited. *Boundary-Layer Meteorol*, 102: 415-457

Massman, W., and X. Lee, 2002. Eddy covariance flux corrections and uncertainties in long-term studies of carbon and energy exchanges. *Agricultural and Forest Meteorology*, 113(4): 121-144

Billesbach, D., 2011. Estimating uncertainties in individual eddy covariance flux measurements: a comparison of methods and a proposed new method. *Agricultural and Forest Meteorology*, 151: 394-405

Moncrieff, J., Y. Malhi, and R. Leuning, 1996. The propagation of errors in long term measurements of land atmosphere fluxes of carbon and water, *Global Change Biology*, 2: 231-240

- These errors are not trivial - they may sum up to over 100% of the flux
- To minimize or avoid such errors a number of procedures can be performed

Errors due to	Affected fluxes	Approximate range
Spikes and noise	all	0-15%
Unleveled anemometer	all	0-25%
Wind angle of attack	all	0-25%
Time delay	mostly closed path	0-50%
Frequency response	all	0-50%
Sonic heat flux error	sensible heat flux	0-10%
Density fluctuations	any gas	0-50%
Spectroscopic effects for LASERS	any gas	0-25%
Band-broadening for NDIR	mostly CO <sub>2</sub>	0-5%
Oxygen in the path	some H <sub>2</sub> O	0-10%
Gas flux storage under tower	any gas	0-5%
Missing data filling	all	0-20%

None of these errors are trivial. Combined, they may sum up to over 100% of the initial measured flux value. To minimize such errors, a number of procedures exist within the eddy covariance technique. Here we show the relative size of errors on a typical summer day over a green vegetative canopy, and then provide a brief overview of the remedies for such errors.

Step-by-step instructions on how to minimize or eliminate these and other errors with proper experimental planning, design, and implementation are provided in [Parts 2 and 3](#) of this book. Detailed descriptions of how to apply the corrections in data processing software are provided in [Part 4](#). Below are a few highlights.

Spikes and noise may affect all fluxes, but usually not by more than fifteen percent of the flux. Proper instrument selection, maintenance, along with a spike removal routine and filtering in data processing software, help to minimize the effect of such errors.

An unleveled sonic anemometer will affect all fluxes as well, because of contamination of the vertical wind speed with a horizontal component. The error can be twenty-five percent or more, but it is easily reduced by having a steady tower, and by leveling the anemometer during the station

setup. The remaining error can be fixed relatively easily by using a processing procedure called coordinate rotation.

Errors due to unadjusted time delay can affect all fluxes, but are most severe in closed-path systems with long intake tubes, especially for water vapor and other “sticky” gases (*e.g.*, ammonia). These errors can be up to 25% for non-sticky gases, and may exceed 50% for H<sub>2</sub>O and NH<sub>3</sub>. Time delay errors can be minimized by using shorter tubes when possible, by using instruments with matching clocks, and by minimizing the separation distance between the intake of the gas analyzer and the sonic anemometer.

The time delay errors can be virtually eliminated by adjusting the delay during data processing. This is implemented by shifting the two time series in such a way that the covariance between them is maximized. Alternatively, the delay between two time series can be computed from the known flow rate and tube diameter.

Frequency response errors also affect all fluxes. Usually they range between 5% (for example, in fast open-path devices) and 50% of the flux (in long-tube closed-path or any slower devices), and can be partially remedied by choosing fast instrumentation, and by proper experimental setup. They can be further corrected by applying frequency response corrections in the data processing software.

- Many of the potential errors can be minimized or eliminated by proper station and experimental design, data collection settings, and site maintenance; the remainder can be corrected by proper software setup during data processing

Errors	Planning and design remedy	Data processing remedy
Spikes and noise	Instrument selection and setup	Spike removal
Unleveled anemometer	Tower and instrument installation	Coordinate rotation
Wind angle of attack	Instrument selection, setup	Angle-of-attack correction
Time delay	Instrument selection, setup, clocks	Time delay adjustment
Frequency response	Instrument selection, system setup, and data collection settings	Frequency response corrections
Sonic heat flux error	--	Sonic heat flux correction
Density fluctuations	Type of instrument selection	Dry mole fraction output, or WPL density terms
Spectroscopic effects for LASERs	--	Instrument-specific correction; no standardized widely used form
Band-broadening for NDIR	--	Band-broadening correction
Oxygen in the path	--	Oxygen correction
Gas flux storage	Gas profile measurements	Gas flux storage term
Missing data filling	Instrument selection, well-planned maintenance	Methodology/tests: Monte-Carlo <i>etc.</i>

Sonic heat errors affect sensible heat flux, but usually by no more than ten percent, and they are fixed by applying a straightforward sonic heat flux correction.

The density fluctuations mostly affect gas and water fluxes, and only when instruments output fast density, as opposed to the fast dry mole fraction. Size and direction of the related errors vary greatly. It can be three hundred percent of the small flux in winter, or it could be only a few percent in summer. These errors can be eliminated by choosing instruments that output fast dry mole fraction, or can be corrected using Webb-Pearman-Leuning density terms.

Spectroscopic effects for recent laser-based technologies may affect fast concentrations and fluxes. The extent is generally specific to the technology, little studied in eddy covariance applications, and should be treated with caution.

Band-broadening errors affect gas fluxes measured by the NDIR technique, and depend greatly on the instrument used. The error is usually on the order of zero to five percent, and corrections are either applied in the instrument's software, or described by the instrument manufacturer. Oxygen in the path affects krypton hygrometer readings, but usually not more than ten percent, and the error is fixed with an oxygen correction.

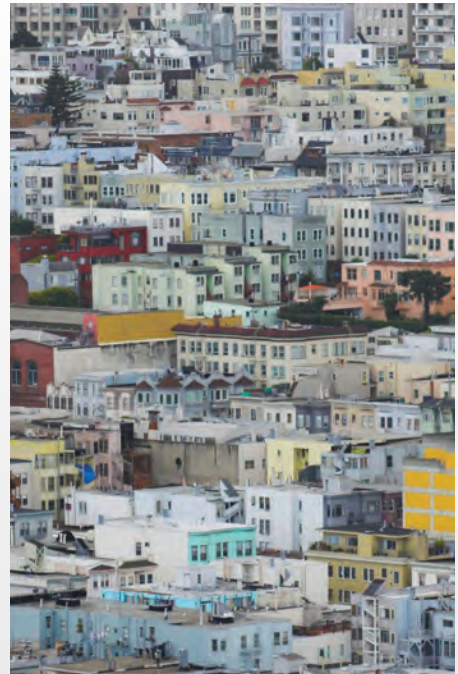
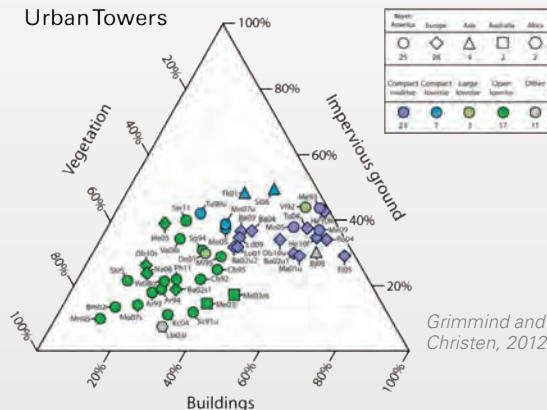
Missing data will affect all fluxes, especially if they are integrated over long periods of time. The effects can be minimized by choosing the proper instrument for the site conditions, and by a well-planned maintenance schedule. For example, in a rainy site, an enclosed or closed-path instrument will lose significantly less data than an open-path instrument, while having a spare instrument as part of the maintenance plan may also reduce the data gaps due to malfunctions, lightning strikes, *etc.*

There are also a number of different mathematical methods to test and compute what the resulting errors would be for a specific set of data due to gap-filling. One good example is the Monte Carlo Method. Other methods are mentioned in [Section 4.10](#) of this book.



Please note that even though modern flux programs will automatically correct most of the errors as part of the standard flux processing sequence, it is still extremely important to minimize or eliminate the majority of these errors during the experiment setup, and only then to correct the remaining errors during data processing. This is especially important for small fluxes and for yearly integrations.

- All principles described previously were developed and tested for traditional settings: reasonably horizontal and uniform terrain, with negligible air density fluctuations, negligible flow convergence and divergence, and with prevailing turbulent flux transport
- The latest developments of the eddy covariance method have revisited these assumptions to measure over complex sites, such as urban or hilly terrains



All principles described previously were developed and tested for traditional settings, over reasonably horizontal and uniform terrains, with negligible air density fluctuations, negligible flow convergence and divergence, and with prevailing turbulent flux transport.

The latest developments of the method have revisited many of these assumptions in order to be able to use the method in complex terrains: over cities, on hills, and under conditions of various flow obstructions.

There are several groups in the FluxNet and other networks who work specifically in complex terrains, and have become experts in this area of the eddy covariance method.

Success of these latest applications is growing, with over 60 urban flux stations deployed in 2012 for both scientific and regulatory purposes (<http://www.geog.ubc.ca/urbanflux>). At least 25 additional stations operate in complex mountainous terrains across the globe.

## References

Great review of the modern urban flux measurements and related literature is provided by: Grimmond, S., and A. Christen, 2012. Flux measurements in urban ecosystems. FluxLetter, 5(1): 1-8 [http://fluxnet.ornl.gov/sites/default/files/FluxLetter\\_Vol5\\_no1.pdf](http://fluxnet.ornl.gov/sites/default/files/FluxLetter_Vol5_no1.pdf)

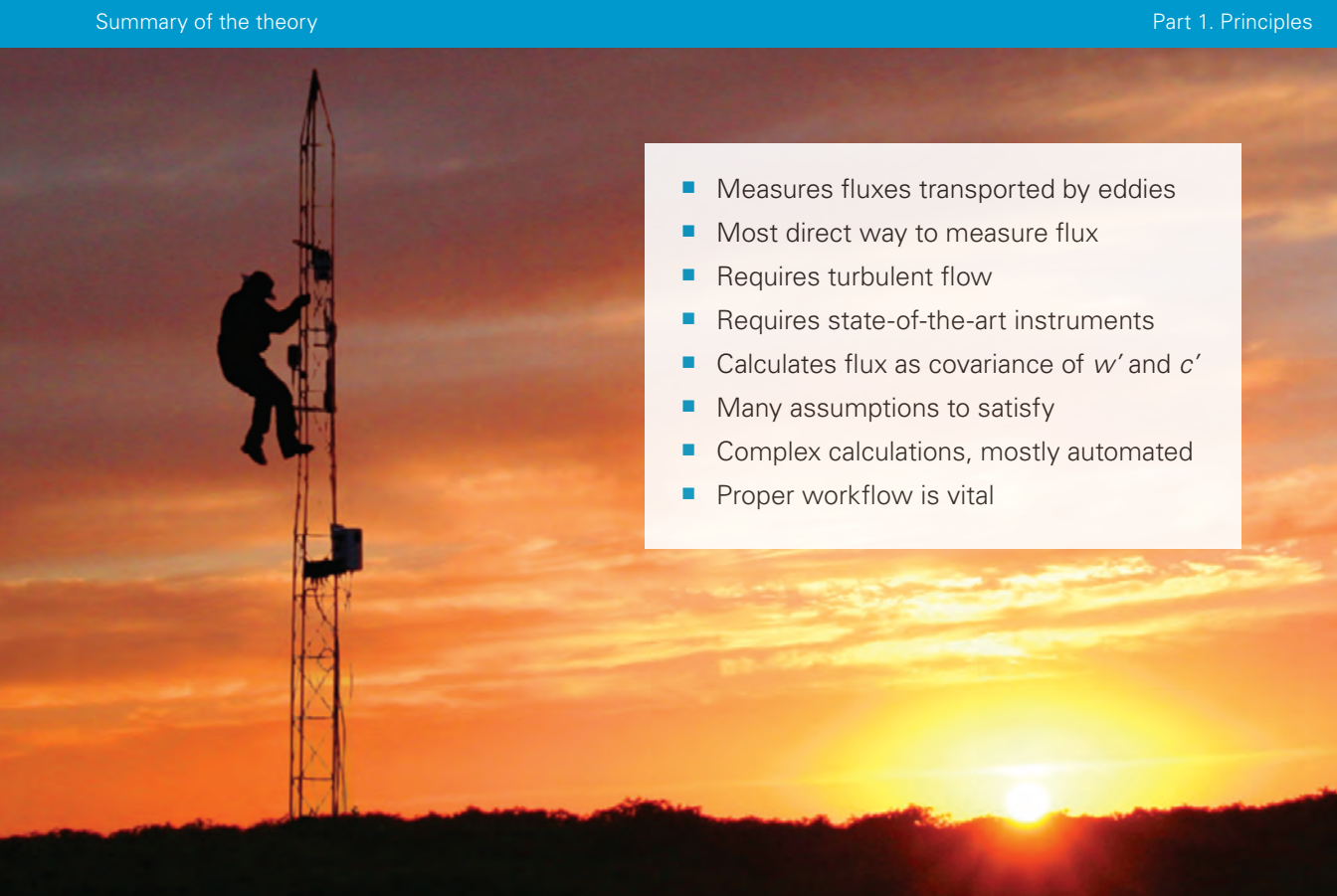
Other measurements in complex conditions described in: Gu, L., W. Massman, R. Leuning, S. Pallardy, T. Meyers, *et al.*, 2012. The fundamental equation of eddy covariance and its application in flux measurements. Agricultural and Forest Meteorology, 152: 135-148

Lee, X., W. Massman, and B. Law (Eds.), 2004. Handbook of Micrometeorology: A Guide for Surface Flux Measurement and Analysis. Kluwer Academic Publishers, Dordrecht, Netherlands, 252 pp.

McMillen, R., 1988. An eddy correlation technique with extended applicability to non-simple terrain. Boundary-Layer Meteorology, 43: 231-245

Raupach, M., and J. Finnigan, 1997. The influence of topography on meteorological variables and surface-atmosphere interactions. Hydrology, 190: 182-213



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- Measures fluxes transported by eddies
  - Most direct way to measure flux
  - Requires turbulent flow
  - Requires state-of-the-art instruments
  - Calculates flux as covariance of  $w'$  and  $c'$
  - Many assumptions to satisfy
  - Complex calculations, mostly automated
  - Proper workflow is vital

Eddy covariance is the most direct approach to measure vertical fluxes of water vapor, trace gases (*e.g.*,  $\text{CO}_2$ ,  $\text{CH}_4$ ,  $\text{N}_2\text{O}$ , *etc.*), heat and momentum between the soil, vegetation, urban or industrial terrains and the atmosphere.

Flux is calculated as a covariance of instantaneous deviations in vertical wind speed and instantaneous deviations in the entity of interest.

The method relies on the prevalence of the turbulent transport, and requires state-of-the-art instruments. It uses complex calculations, and utilizes many assumptions.

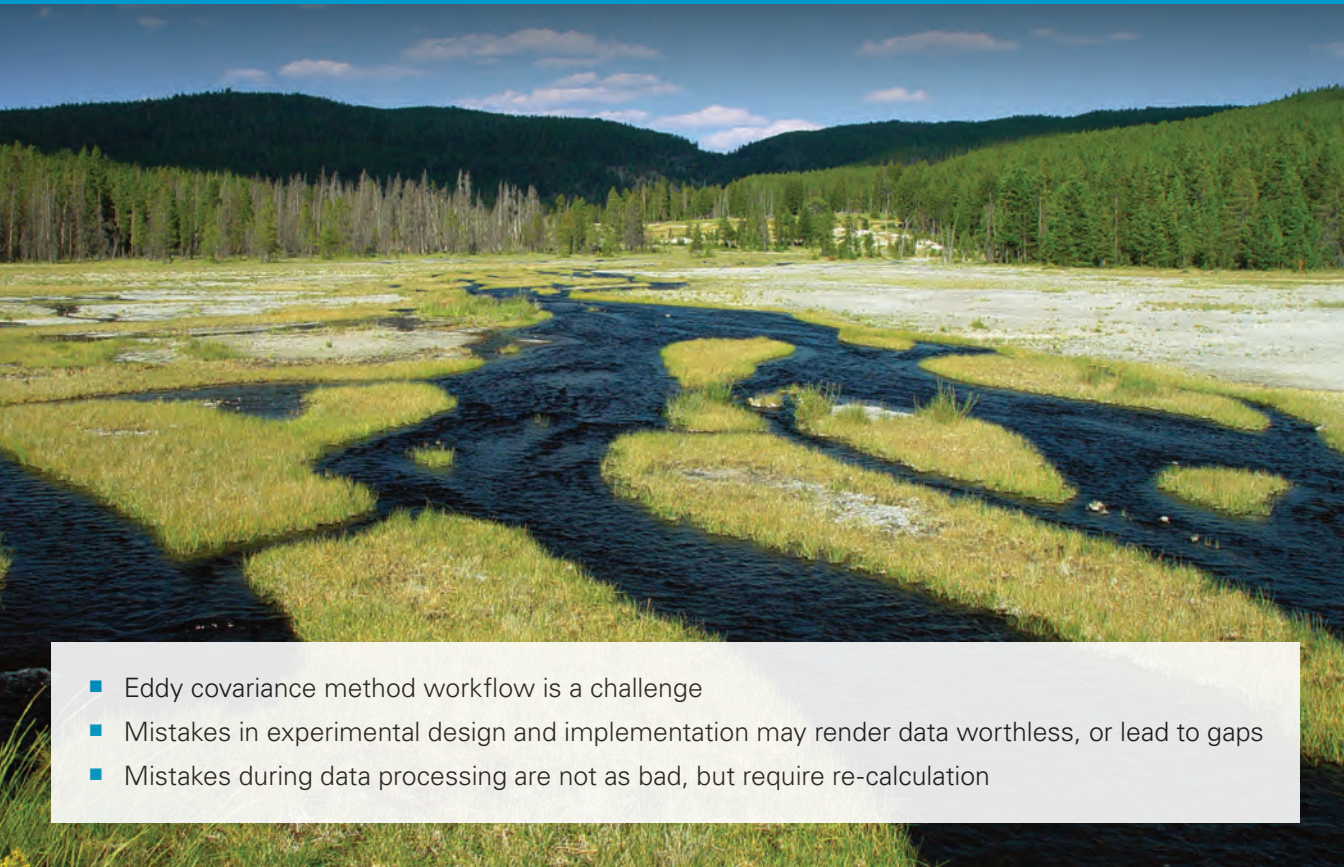
Modern instrument systems and processing software take care of most of the challenges when using the eddy covariance method. Nevertheless, proper station design, experiment planning and execution, and correct data processing steps help to minimize or eliminate the errors resulting from failure to meet theoretical assumptions, and system deficiencies.

In this way the method can be tuned to the particular purpose (scientific, industrial, agricultural, regulatory, *etc.*), and to the particular measurement site (maize field, forest, wetland, ocean, city, landfill, *etc.*) to provide reliable hourly or half-hourly fluxes continuously over months and years.

Proper execution of the eddy covariance method is perhaps the second biggest challenge for a novice, after mastering the theoretical part of the method.

The rest of this book is primarily dedicated to providing a sequential step-by-step description of the method's workflow, from designing and implementation of the experiment, to processing the data.





- Eddy covariance method workflow is a challenge
- Mistakes in experimental design and implementation may render data worthless, or lead to gaps
- Mistakes during data processing are not as bad, but require re-calculation

Proper execution of the workflow may become a significant challenge for a novice, second only to mastering the theoretical part of the eddy covariance method.

Oversights in experimental design and implementation may lead to collecting bad data for a prolonged period of time, and can result in large data gaps.

These are especially undesirable for the integration of the long-term data sets, which is the prime goal for measuring fluxes of carbon dioxide, methane or other greenhouse gases in scientific applications.

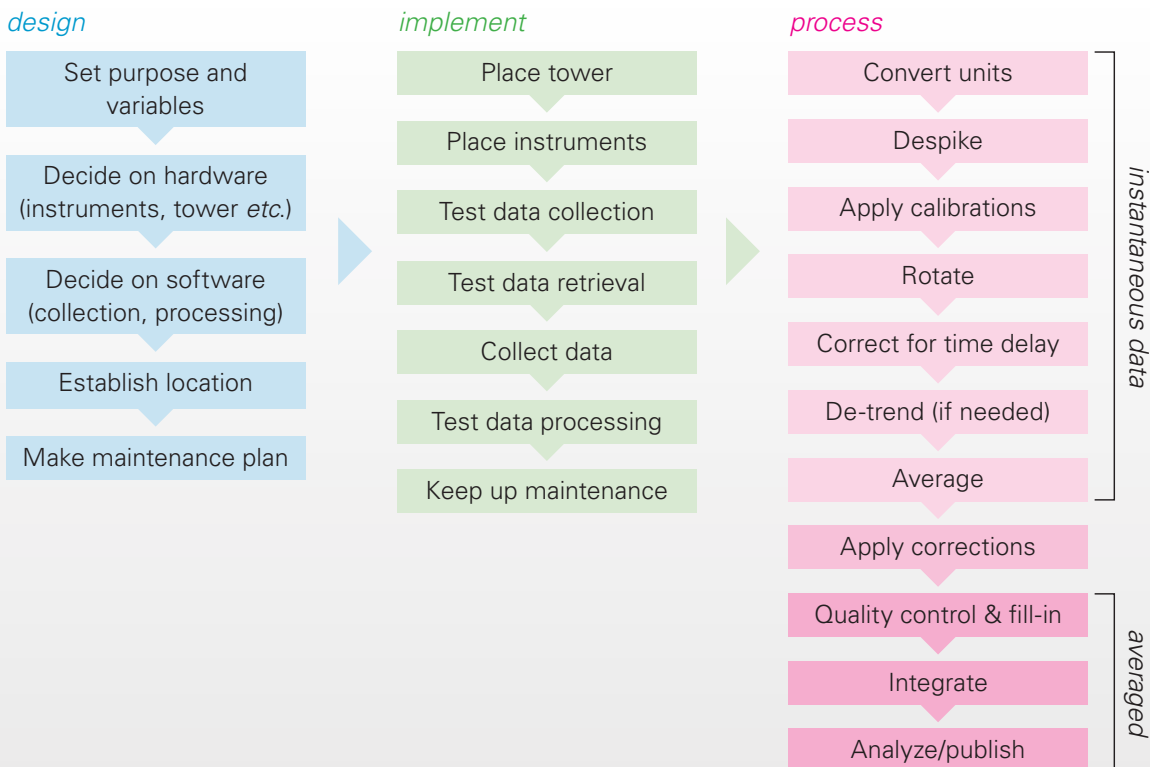
Errors in data processing may not be as bad, as long as there is a backup of the original raw data files, but they can also lead to time-consuming re-calculations, or to wrong data interpretation.

There are several different ways to execute the eddy covariance method and get substantially the same results. Here we will give an example of one traditional sequence of actions needed for successful experimental setup, data collection and processing.

This sequence may not fit some specific measurements goals, but it will provide a general understanding of what is involved in eddy covariance study, and will point out the most difficult parts and frequent pitfalls.



It is extremely important to always keep and store original 10Hz or 20Hz data collected using the eddy covariance method. The data can then be reprocessed at any time using, for example, new frequency response correction methods, or correct calibration coefficients. Some of the processing steps cannot be confidently recalculated without the original high-frequency data.



Above is an example of one traditional sequence of actions needed for successful experimental setup, data collection, and processing. One can break the workflow into three major parts: design of the experiment, implementation, and data processing.

The key elements of the design portion of eddy covariance experiment are as follows: setting the purpose and variables for the study, deciding on instruments and hardware to be used, creating new or adjusting existing software to collect and process the data, establishing appropriate experiment location and a feasible maintenance plan.

The major elements of the implementation portion are: placing

the tower, placing the instruments on the tower, testing data collection and retrieval, collecting data, and keeping up the maintenance schedule.

The processing portion includes: processing the real time, “instantaneous” data (usually at a 10-20 Hz sample rate), processing averaged data (usually from 0.5 hrs to 2 hrs), quality control, and long-term integration and analysis.

The main elements of data processing include: converting voltages into units, de-spiking, applying calibrations, rotating the coordinates, correcting for time delay, de-trending if needed, averaging, applying corrections, quality control, gap filling, integrating, and finally, data analysis and publication.

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