# 机器人学导论作业11-12

SZ170320207

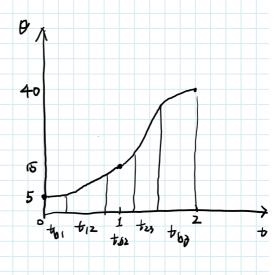
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# **Question1**

# 推导

7 年 13-14.

1、
$$\theta_1 = 3^\circ$$
 ,  $\theta_2 = 6^\circ$  ,  $\theta_3 = 40^\circ$ 
 $\theta_{0} = \theta_{0}^\circ / s^2$ 



# 起始段

$$\frac{\partial}{\partial s} = -80 = sgn(\theta_2 - \theta_3) \frac{\partial b}{\partial b} 
+ b_3 = + d_{23} - ) + d_{23} + \frac{2(\theta_3 - \theta_2)}{\theta_3} = 0.3876$$

$$\frac{\partial}{\partial s} = \frac{\theta_3 - \theta_2}{\theta_3 - \frac{\theta_3}{\theta_3}} = 31.0102$$

## 结果

 $\dot{\theta}_{12} = 10.7180$ 

 $\dot{\theta}_{\,23} = 31.0102$ 

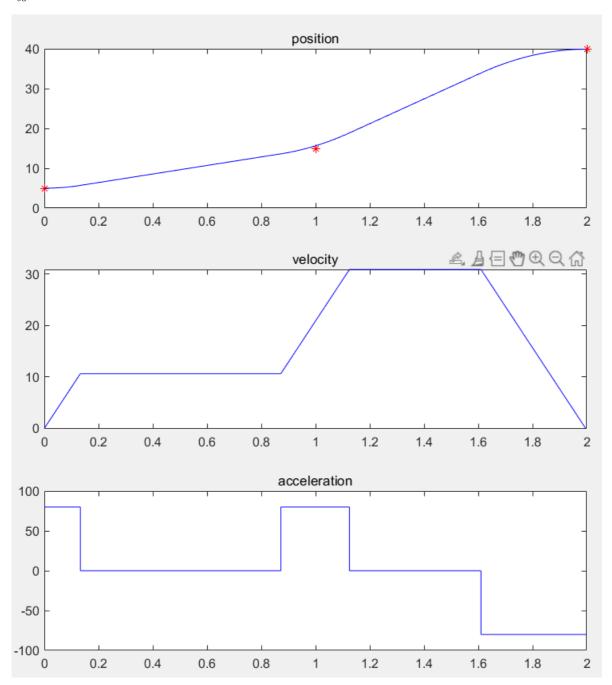
 $t_{b1}=0.1340$ 

 $t_{12} = 0.7392$ 

 $t_{b2} = 0.2537$ 

```
t_{23}=0.4855
```

 $t_{b3} = 0.3876$ 



```
theta1 = 5;
theta2 = 15;
theta3 = 40;

acceleration_b = 80;

td12 = 1;
td23 = 1;

subplot(3,1,1)
plot(0,theta1,'r*');
hold on;
plot(td12,theta2,'r*');
```

```
hold on;
plot(td12+td23, theta3, 'r*');
hold on;
acceleration_1 = acceleration_b;
tb1 = td12 - sqrt(td12^2-2*(theta2-theta1)/acceleration_1)
velocity12 = (theta2-theta1)/(td12-tb1/2)
acceleration_3 = -acceleration_b;
tb3 = td23 - sqrt(td23^2 + 2*(theta3-theta2)/acceleration_3)
velocity23 = (theta3-theta2)/(td23-tb3/2)
acceleration_2 = acceleration_b;
tb2 = (velocity23-velocity12)/acceleration_2
t23 = td23 - tb2/2 - tb3
t12 = td12 - tb2/2 - tb1
t_b1 = 0:0.001:tb1;
p_b1 = theta1 + 1/2*acceleration_1*t_b1.^2;
v_b1 = acceleration_1*t_b1;
a_b1 = acceleration_1 + 0*t_b1;
t = t_b1;
p = p_b1;
v = v_b1;
a = a_b1;
t_12 = 0:0.001:t12;
p_12 = p_b1(end) + velocity12.*t_12;
v_12 = v_b1(end) + 0 * t_12;
a_12 = 0*t_12;
t = [t t_12+t(end)];
p = [p p_12];
v = [v \ v_12];
a = [a \ a_{12}];
t_b2 = 0:0.001:tb2;
p_b2 = p_12(end) + v_12(end)*t_b2 + 1/2*acceleration_2*t_b2.^2;
v_b2 = v_12(end) + acceleration_2*t_b2;
a_b2 = acceleration_2 +0*t_b2;
t = [t t_b2+t(end)];
p = [p \ p_b2];
v = [v \ v_b2];
a = [a \ a_b2];
t_23 = 0:0.001:t23;
p_23 = p_b2(end) + velocity23*t_23;
v_23 = v_b2(end) + 0*t_23;
a_23 = 0*t_23;
t = [t t_23+t(end)];
p = [p \ p_23];
v = [v \ v_23];
a = [a \ a_23];
t_b3 = 0:0.001:tb3;
p_b3 = p_23(end) + v_23(end)*t_b3 + 1/2*acceleration_3*t_b3.^2;
v_b3 = v_23(end) + acceleration_3*t_b3;
```

```
a_b3 = acceleration_3 + 0*t_b3;
t = [t t_b3+t(end)];
p = [p p_b3];
v = [v v_b3];
a = [a a_b3];

subplot(3,1,1)
plot(t,p,'b')
title('position')
subplot(3,1,2)
plot(t,v,'b')
title('velocity')
subplot(3,1,3)
plot(t,a,'b')
title('acceleration')
```

# **Question2**

## 推导

2. 
$$\theta_0=5^{\circ}$$
  $\theta_V=5^{\circ}$   $\theta_g=10^{\circ}$ 
 $td_{0V}=td_{0g}=25=td$ 
 $\hat{\theta}_0=\hat{\theta}_0=\hat{\theta}_0=0^{\circ}/s$ 
 $td_{0}R=\hat{\theta}_0=\hat{\theta}_0=0^{\circ}/s$ 
 $td_{0}R=\hat{\theta}_0=\hat{\theta}_0=0^{\circ}/s$ 
 $td_{0}R=\hat{\theta}_0=0$ 
 $td_{0}R=\hat{\theta}_0=0$ 
 $d_{0}R=\hat{\theta}_0=0$ 
 $d_{0}R=\hat{\theta}_0=0$ 

## 结果

第一段参数

 $a_{01} = 5$ 

 $a_{11} = 0$ 

 $a_{21} = 7.5000$ 

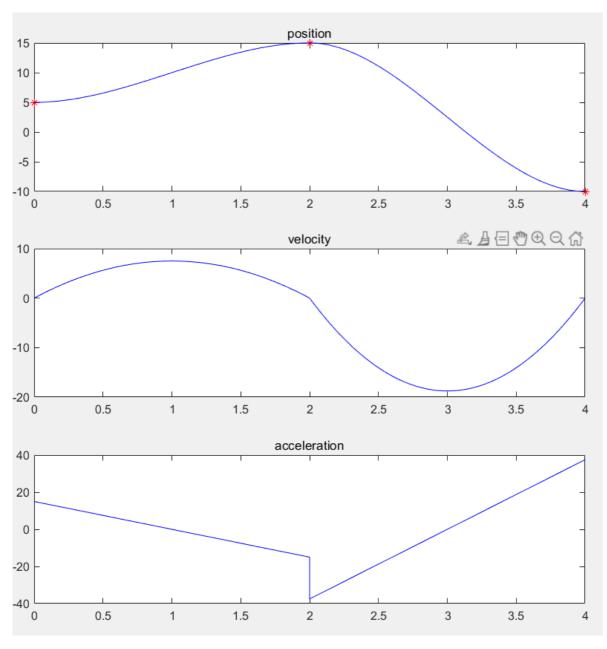
 $a_{31} = -2.5000$ 

```
第一段参数
```

```
a_{02} = 15 a_{12} = 0
```

$$a_{22} = -18.7500$$

 $a_{32} = 6.2500$ 



```
theta0 = 5;
thetav = 15;
thetag = -10;

td = 2;

subplot(3,1,1)
plot(0,theta0,'r*');
hold on;
plot(td,thetav,'r*');
hold on;
```

```
plot(td+td,thetag,'r*');
hold on;
v0 = 0;
vv = 0;
vg = 0;
h0v = thetav - theta0;
a01 = theta0;
a11 = v0;
a21 = (3*h0v-(2*v0+vv)*td)/td^2;
a31 = (-2*h0v+(v0+vv)*td)/td^3;
t1 = 0:0.01:td;
p1 = a01 + a11*t1 + a21*t1.^2 + a31*t1.^3;
v1 = a11 + 2*a21*t1 + 3*a31*t1.^2;
a1 = 2*a21 + 6*a31*t1;
t = t1;
p = p1;
v = v1;
a = a1;
h1v = thetag - thetav;
a02 = thetav;
a12 = vv;
a22 = (3*h1v-(2*vv+vg)*td)/td^2;
a32 = (-2*h1v+(vv+vg)*td)/td^3;
t2 = 0:0.01:td;
p2 = a02 + a12*t2 + a22*t2.^2 + a32*t2.^3;
v2 = a12 + 2*a22*t2 + 3*a32*t2.^2;
a2 = 2*a22 + 6*a32*t2;
t = [t t2+t(end)];
p = [p p2];
v = [v \ v2];
a = [a a2];
subplot(3,1,1)
plot(t,p,'b')
title('position')
subplot(3,1,2)
plot(t,v,'b')
title('velocity')
subplot(3,1,3)
plot(t,a,'b')
title('acceleration')
```

# Question3

```
	heta(t) = 10 + 90t^2 - 60t^3 \dot{	heta}(t) = 180t - 180t^2 \ddot{	heta}(t) = 180 - 360t 所以
```

### 起始点:

$$t_0 = 0$$

$$p_0 = heta(0) = 10$$

$$v_0=\dot{ heta}(0)=0$$

$$a_0=\ddot{ heta}(0)=180$$

## 终止点:

$$t_f = 1$$

$$p_f = \theta(1) = 40$$

$$v_f = \dot{\theta}(1) = 0$$

$$a_f = \ddot{ heta}(1) = -180$$

# **Question4**

# 推导

$$\vec{\partial}(b) = \begin{pmatrix} \vec{\partial}_0 + \vec{\lambda} \cdot \vec{\partial}_0 & (t - t_0)^2 \\ \vec{\partial}_0 + \vec{\partial}_0 + \vec{\partial}_0 \cdot (t - t_0 - t_0) \end{pmatrix}, \quad bo + tb \leq t < tf - to$$

$$\vec{\partial}_0 + \vec{\lambda} \cdot \vec{\partial}_0 \cdot (t - t_0 - t_0) + tb \leq t \leq tf$$

$$P_1 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
,  $P_2 = \begin{bmatrix} 2 \\ 1 \end{bmatrix}$   $P_3 = \begin{bmatrix} 3 \\ 3 \end{bmatrix}$ 

$$a_b = \begin{bmatrix} 6 \\ 6 \end{bmatrix}$$

$$a_1 = a_b = \begin{bmatrix} 6 \\ 6 \end{bmatrix} = sgn(P_2 - P_1)a_b$$

$$a_1 = a_b = \begin{bmatrix} 6 \\ 6 \end{bmatrix} = sgn(P_2 - P_1)a_b$$

$$tb_1 = td_{12} - \int td_{12} - \frac{2(P_2 - P_1)}{a_1} = \begin{bmatrix} 0.4226 \\ 0.1835 \end{bmatrix}$$

$$V_{12} = \frac{P_2 - P_1}{td_1 - \frac{to_1}{2}} = \begin{bmatrix} 2.5359 \\ 1.1010 \end{bmatrix}$$

# 终业钱

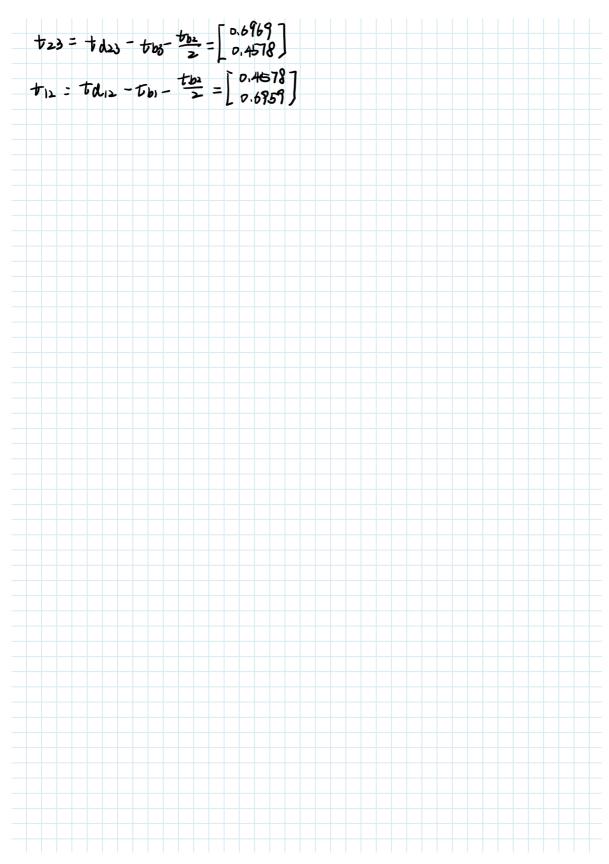
$$a_3 = -a_0 = \begin{bmatrix} -6 \\ -6 \end{bmatrix} = sgn(t_2 - t_3)a_0$$

$$t_{b3} = td_{23} - \int td_{13} + \frac{z(P_3 - P_2)}{a_{13}} = \begin{bmatrix} 0.1835 \\ 0.4216 \end{bmatrix}$$

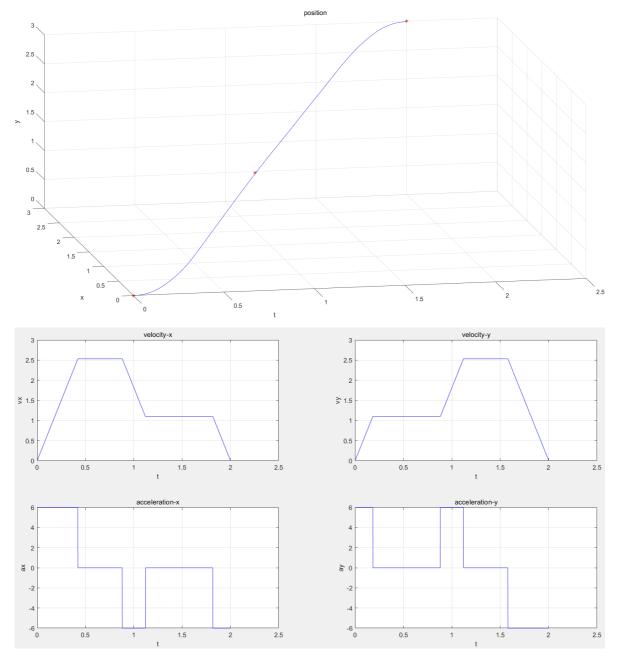
$$a_{2} = sgn_{L} V_{23} - V_{12} a_{b} = \begin{bmatrix} -6 \\ 6 \end{bmatrix}$$

$$tb_{2} = \frac{V_{23} - V_{12}}{a_{1}} = \begin{bmatrix} v.2391 \\ 0.2391 \end{bmatrix}$$

$$t_{b2} = \frac{V_{23} - V_{12}}{a_2} = \begin{bmatrix} 0.2391 \\ 0.2391 \end{bmatrix}^2$$



# 结果



```
P1 = [0;0];

P2 = [2;1];

P3 = [3;3];

acceleration_b = [6;6];

td12 = 1;

td23 = 1;

plot3(0,P1(1),P1(2),'r*');

hold on;

plot3(td12,P2(1),P2(2),'r*');

hold on;

plot3(td12+td23,P3(1),P3(2),'r*');

hold on;

acceleration_1 = sign(P2 - P1).*acceleration_b;

tb1 = td12 - sqrt(td12^2-2*(P2-P1)./acceleration_1)
```

```
velocity12 = (P2-P1)./(td12-tb1/2)
acceleration_3 = sign(P2 - P3).*acceleration_b
tb3 = td23 - sqrt(td23^2 + 2*(P3-P2)./acceleration_3)
velocity23 = (P3-P2)./(td23-tb3/2)
acceleration_2 = sign(velocity23-velocity12).*acceleration_b
tb2 = (velocity23-velocity12)./(acceleration_2)
t23 = td23 - tb2/2 - tb3
t12 = td12 - tb2/2 - tb1
t_b1x = 0:0.001:tb1(1);
p_b1x = P1(1) + 1/2*acceleration_1(1)*t_b1x.^2;
v_b1x = acceleration_1(1)*t_b1x;
a_b1x = acceleration_1(1) + 0*t_b1x;
tx = t_b1x;
px = p_b1x;
vx = v_b1x;
ax = a_b1x;
t_b1y = 0:0.001:tb1(2);
p_b1y = P1(2) + 1/2*acceleration_1(2)*t_b1y.^2;
v_b1y = acceleration_1(2)*t_b1y;
a_b1y = acceleration_1(2) + 0*t_b1y;
ty = t_b1y;
py = p_b1y;
vy = v_b1y;
ay = a_b1y;
t_12x = 0:0.001:t12(1);
p_12x = px(end) + velocity12(1).*t_12x;
v_12x = vx(end) + 0 * t_12x;
a_{12x} = 0*t_{12x};
tx = [tx t_12x+tx(end)];
px = [px p_12x];
vx = [vx v_12x];
ax = [ax a_12x];
t_12y = 0:0.001:t12(2);
p_12y = py(end) + velocity12(2).*t_12y;
v_12y = vy(end) + 0 * t_12y;
a_12y = 0*t_12y;
ty = [ty t_12y+ty(end)];
py = [py p_12y];
vy = [vy v_12y];
ay = [ay a_12y];
t_b2x = 0:0.001:tb2(1);
p_b2x = px(end) + vx(end)*t_b2x + 1/2*acceleration_2(1)*t_b2x.^2;
v_b2x = vx(end) + acceleration_2(1)*t_b2x;
a_b2x = acceleration_2(1) +0*t_b2x;
tx = [tx t_b2x+tx(end)];
px = [px p_b2x];
vx = [vx v_b2x];
ax = [ax a_b2x];
```

```
t_b2y = 0:0.001:tb2(2);
p_b2y = py(end) + vy(end)*t_b2y + 1/2*acceleration_2(2)*t_b2y.^2;
v_b2y = vy(end) + acceleration_2(2)*t_b2y;
a_b2y = acceleration_2(2) +0*t_b2y;
ty = [ty t_b2y+ty(end)];
py = [py p_b2y];
vy = [vy v_b2y];
ay = [ay a_b2y];
t_23x = 0:0.001:t23(1);
p_23x = px(end) + velocity23(1)*t_23x;
v_23x = vx(end) + 0*t_23x;
a_23x = 0*t_23x;
tx = [tx t_23x+tx(end)];
px = [px p_23x];
vx = [vx v_23x];
ax = [ax a_23x];
t_23y = 0:0.001:t23(2);
p_23y = py(end) + velocity23(2)*t_23y;
v_23y = vy(end) + 0*t_23y;
a_23y = 0*t_23y;
ty = [ty t_23y+ty(end)];
py = [py p_23y];
vy = [vy v_23y];
ay = [ay a_23y];
t_b3x = 0:0.001:tb3(1);
p_b3x = px(end) + vx(end)*t_b3x + 1/2*acceleration_3(1)*t_b3x.^2;
v_b3x = v_23x(end) + acceleration_3(1)*t_b3x;
a_b3x = acceleration_3(1) + 0*t_b3x;
tx = [tx t_b3x+tx(end)];
px = [px p_b3x];
vx = [vx v_b3x];
ax = [ax a_b3x];
t_b3y = 0:0.001:tb3(2);
p_b3y = py(end) + vy(end)*t_b3y + 1/2*acceleration_3(2)*t_b3y.^2;
v_b3y = v_23y(end) + acceleration_3(2)*t_b3y;
a_b3y = acceleration_3(2) + 0*t_b3y;
ty = [ty t_b3y+ty(end)];
py = [py p_b3y];
vy = [vy v_b3y];
ay = [ay a_b3y];
t = 0:0.001:2.001;
plot3(t,px,py,'b')
xlabel('t')
ylabel('x')
zlabel('y')
grid on
title('position')
% subplot(2,2,1)
% plot(t,vx,'b')
% xlabel('t')
% ylabel('vx')
% grid on
% title('velocity-x')
```

```
% subplot(2,2,2)
% plot(t,vy,'b')
% xlabel('t')
% ylabel('vy')
% grid on
% title('velocity-y')
% subplot(2,2,3)
% plot(t,ax,'b')
% xlabel('t')
% ylabel('ax')
% grid on
% title('acceleration-x')
% subplot(2,2,4)
% plot(t,ay,'b')
% xlabel('t')
% ylabel('ay')
% grid on
% title('acceleration-y')
```

# **Question5**

(a)

δ.

(6) ΚΛΛΛΕ ΜΙΘ) 
$$\ddot{\theta} + C(\theta, \dot{\theta}) \dot{\theta} + J(\theta) = T$$

$$\frac{d}{dt} \frac{\partial L}{\partial \dot{q}} - \frac{\partial L}{\partial \dot{q}} = T$$

$$L = T - V$$

$$T(\theta, \dot{\theta}) = \frac{1}{2} m_1 |V_1|^{\frac{1}{2}} + \frac{1}{2} \omega_1^T J_1 \omega_1 + \frac{1}{2} m_2 |V_2|^{\frac{1}{2}} + \frac{1}{2} \omega_2^T J_2 \omega_2$$

$$\omega_1 = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \qquad p_1 = V_1 = \begin{bmatrix} -r_1 \sin \theta_1 & 0 & 0 \\ r_1 \cos \theta_1 & r_2 \sin \theta_1 & 0 \end{bmatrix}$$

$$P_1 = \begin{bmatrix} r_1 \cos \theta_1 + r_2 \cos \theta_1 + r_3 \sin \theta_1 & 0 & 0 \\ r_1 \sin \theta_1 & r_2 \sin \theta_1 & 0 \end{bmatrix} \qquad p_2 = V_2 = \begin{bmatrix} -h_1 s_1 & 0 & -r_2 s_2 & 0 & 0 \\ h_1 s_1 & 0 & 1 & 0 \end{bmatrix}$$

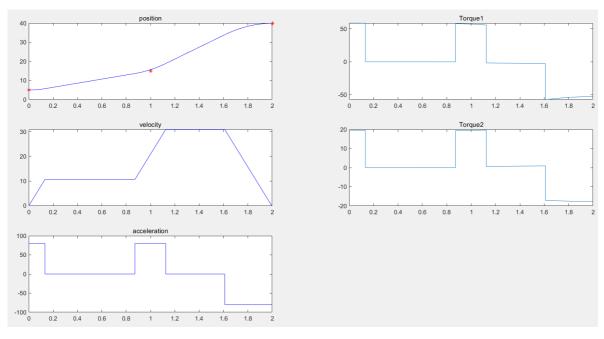
$$P_2 = V_2 = \begin{bmatrix} -h_1 s_1 & 0 & -r_2 s_2 & 0 & 0 \\ h_1 s_1 & 0 & 1 & 0 \end{bmatrix} \qquad p_2 = V_2 = \begin{bmatrix} -h_1 s_1 & 0 & -r_2 s_2 & 0 & 0 \\ h_1 c_1 & 0 & 1 & 0 & 0 \\ h_2 c_1 & 0 & 1 & 0 \end{bmatrix} \qquad p_2 = V_2 = \begin{bmatrix} -h_1 s_1 & 0 & -r_2 s_2 & 0 & 0 \\ h_1 c_1 & 0 & 1 & 0 & 0 \\ h_2 c_1 & 0 & 1 & 0 & 0 \\ h_1 c_2 & 0 & 0 & 0 & 0 \\ h_1 c_1 & 0 & 0 & 0 & 0 \\ h_2 c_1 & 0 & 0 & 0 & 0 \\ h_1 c_2 & 0 & 0 & 0 \\ h_1 c_2 & 0 & 0 & 0 \\ h_2 c_1 & 0 & 0 & 0 \\ h_1 c_2 & 0 & 0 & 0 \\ h_1 c_2 & 0 & 0 & 0 \\ h_2 c_1 & 0 & 0 & 0 \\ h_1 c_2 & 0 & 0 \\ h_1 c_2 & 0 & 0 & 0 \\ h_1 c_2 &$$

$$\frac{\partial L}{\partial \theta} = \begin{bmatrix} 0 \\ -652\dot{\theta}^{2} - 652\dot{\theta}^{2} - 652\dot{\theta}^{2} \end{bmatrix}$$

$$\frac{\partial L}{\partial \theta} = \frac{\partial L$$

(b)

**Problem1** 

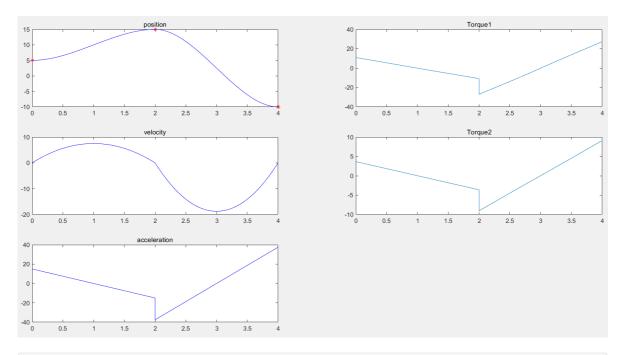


```
degree2rad = pi/180;
theta1 = 5;
theta2 = 15;
theta3 = 40;
acceleration_b = 80;
td12 = 1;
td23 = 1;
subplot(3,2,1)
plot(0,theta1,'r*');
hold on;
plot(td12,theta2,'r*');
hold on;
plot(td12+td23,theta3,'r*');
hold on;
acceleration_1 = acceleration_b;
tb1 = td12 - sqrt(td12^2-2*(theta2-theta1)/acceleration_1)
velocity12 = (theta2-theta1)/(td12-tb1/2)
acceleration_3 = -acceleration_b;
tb3 = td23 - sqrt(td23^2 + 2*(theta3-theta2)/acceleration_3)
velocity23 = (theta3-theta2)/(td23-tb3/2)
acceleration_2 = acceleration_b;
tb2 = (velocity23-velocity12)/acceleration_2
t23 = td23 - tb2/2 - tb3
t12 = td12 - tb2/2 - tb1
t_b1 = 0:0.001:tb1;
p_b1 = theta1 + 1/2*acceleration_1*t_b1.^2;
v_b1 = acceleration_1*t_b1;
a_b1 = acceleration_1 + 0*t_b1;
t = t_b1;
```

```
p = p_b1;
v = v_b1;
a = a_b1;
t_12 = 0:0.001:t12;
p_12 = p_b1(end) + velocity12.*t_12;
v_12 = v_b1(end) + 0 * t_12;
a_12 = 0*t_12;
t = [t t_12+t(end)];
p = [p \ p_12];
v = [v \ v_12];
a = [a \ a_{12}];
t_b2 = 0:0.001:tb2;
p_b2 = p_12(end) + v_12(end)*t_b2 + 1/2*acceleration_2*t_b2.^2;
v_b2 = v_12(end) + acceleration_2*t_b2;
a_b2 = acceleration_2 +0*t_b2;
t = [t t_b2+t(end)];
p = [p p_b2];
v = [v \ v_b2];
a = [a \ a_b2];
t_23 = 0:0.001:t23;
p_23 = p_b2(end) + velocity23*t_23;
v_23 = v_b2(end) + 0*t_23;
a_23 = 0*t_23;
t = [t t_23+t(end)];
p = [p \ p_23];
v = [v \ v_23];
a = [a \ a_23];
t_b3 = 0:0.001:tb3;
p_b3 = p_23(end) + v_23(end)*t_b3 + 1/2*acceleration_3*t_b3.^2;
v_b3 = v_23(end) + acceleration_3*t_b3;
a_b3 = acceleration_3 + 0*t_b3;
t = [t t_b3+t(end)];
p = [p \ p_b3];
v = [v \ v_b3];
a = [a \ a_b3];
subplot(3,2,1)
plot(t,p,'b')
title('position')
subplot(3,2,3)
plot(t,v,'b')
title('velocity')
subplot(3,2,5)
plot(t,a,'b')
title('acceleration')
% 机械臂参数
m1 = 12;
m2 = 12;
11 = 1;
12 = 1;
r1 = 0.5;
```

```
r2 = 0.5;
I1 = [0.0125, 0, 0; 0, 1.0025, 0; 0, 0, 1.01];
I2 = I1;
% 运动学方程
alpha = I1(3,3)+I2(3,3)+m1*r1^2+m2*(11^2+r2^2)
beta = m2*11*r2
delta = I2(3,3) + m2*r2^2
torque = zeros(2,length(t(:)));
for k=1:length(t(:))
    theta1 = p(1,k)*degree2rad;
    theta2 = p(1,k)*degree2rad;
    dtheta1 = v(1,k)*degree2rad;
    dtheta2 = v(1,k)*degree2rad;
    ddtheta1 = a(1,k)*degree2rad;
    ddtheta2 = a(1,k)*degree2rad;
    M = [alpha+2*beta*cos(theta2), delta+beta*cos(theta2);
        delta+beta*cos(theta2), delta];
    C = [-beta*sin(theta2)*dtheta2,-beta*sin(theta2)*(dtheta1+dtheta2);
        beta*sin(theta2)*dtheta1,0];
    torque(:,k) = M*[ddtheta1;ddtheta2]+C*[dtheta1;dtheta2];
end
subplot(3,2,2)
plot(t,torque(1,:));
title('Torque1');
subplot(3,2,4)
plot(t,torque(2,:));
title('Torque2');
```

#### Problem2



```
degree2rad = pi/180;

theta0 = 5;
thetav = 15;
thetag = -10;
```

```
td = 2;
subplot(3,2,1)
plot(0, theta0, 'r*');
hold on;
plot(td,thetav,'r*');
hold on;
plot(td+td,thetag,'r*');
hold on;
v0 = 0;
vv = 0;
vg = 0;
h0v = thetav - theta0;
a01 = theta0
a11 = v0
a21 = (3*h0v-(2*v0+vv)*td)/td^2
a31 = (-2*h0v+(v0+vv)*td)/td^3
t1 = 0:0.01:td;
p1 = a01 + a11*t1 + a21*t1.^2 + a31*t1.^3;
v1 = a11 + 2*a21*t1 + 3*a31*t1.^2;
a1 = 2*a21 + 6*a31*t1;
t = t1;
p = p1;
v = v1;
a = a1;
h1v = thetag - thetav;
a02 = thetav
a12 = vv
a22 = (3*h1v-(2*vv+vg)*td)/td^2
a32 = (-2*h1v+(vv+vg)*td)/td^3
t2 = 0:0.01:td;
p2 = a02 + a12*t2 + a22*t2.^2 + a32*t2.^3;
v2 = a12 + 2*a22*t2 + 3*a32*t2.^2;
a2 = 2*a22 + 6*a32*t2;
t = [t t2+t(end)];
p = [p p2];
v = [v \ v2];
a = [a \ a2];
subplot(3,2,1)
plot(t,p,'b')
title('position')
subplot(3,2,3)
plot(t,v,'b')
title('velocity')
subplot(3,2,5)
plot(t,a,'b')
title('acceleration')
% 机械臂参数
m1 = 12;
m2 = 12;
```

```
11 = 1;
12 = 1;
r1 = 0.5;
r2 = 0.5;
I1 = [0.0125, 0, 0; 0, 1.0025, 0; 0, 0, 1.01];
I2 = I1;
% 运动学方程
alpha = I1(3,3)+I2(3,3)+m1*r1^2+m2*(11^2+r2^2)
beta = m2*11*r2
delta = I2(3,3) + m2*r2^2
torque = zeros(2,length(t(:)));
for k=1:length(t(:))
    theta1 = p(1,k)*degree2rad;
    theta2 = p(1,k)*degree2rad;
    dtheta1 = v(1,k)*degree2rad;
    dtheta2 = v(1,k)*degree2rad;
    ddtheta1 = a(1,k)*degree2rad;
    ddtheta2 = a(1,k)*degree2rad;
    M = [alpha+2*beta*cos(theta2), delta+beta*cos(theta2);
        delta+beta*cos(theta2), delta];
    C = [-beta*sin(theta2)*dtheta2,-beta*sin(theta2)*(dtheta1+dtheta2);
        beta*sin(theta2)*dtheta1,0];
    torque(:,k) = M*[ddtheta1;ddtheta2]+C*[dtheta1;dtheta2];
end
subplot(3,2,2)
plot(t,torque(1,:));
title('Torque1');
subplot(3,2,4)
plot(t,torque(2,:));
title('Torque2');
```

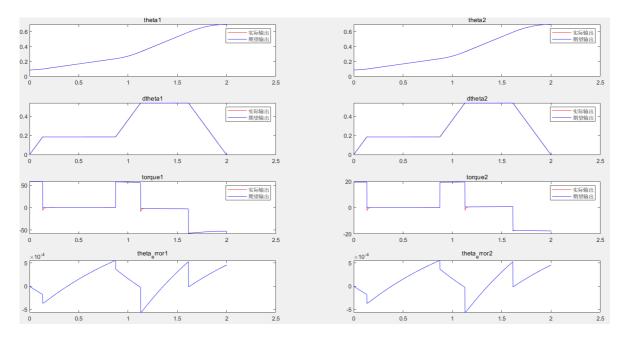
(c)

## (i)Computed torque

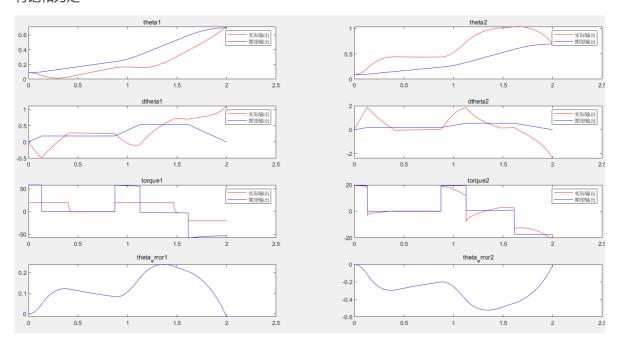
#### Problem1

```
Kp = 80; Kv = 100;
```

无饱和力矩



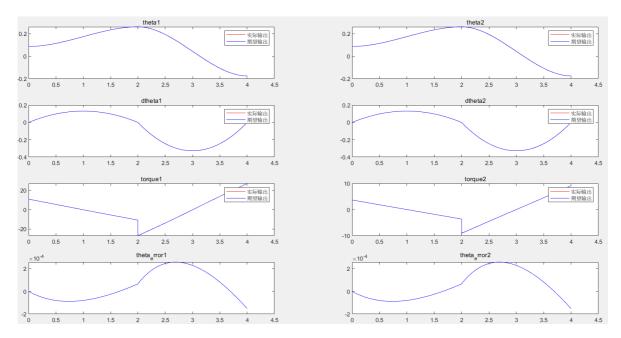
#### 有饱和力矩



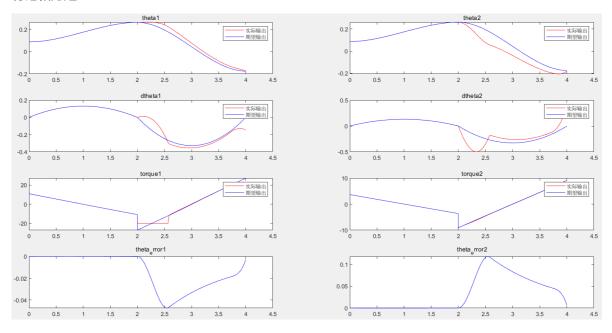
## **Problem2**

Kp = 80; Kv = 100;

无饱和力矩



#### 有饱和力矩



```
clc
clear
% 初始化机械臂参数
theta = [deg2rad(5);deg2rad(5)];
dtheta = [0;0];
ddtheta = [0;0];

% 获取期望轨迹
[theta_desired,dtheta_desired,ddtheta_desired] = trajectory_problem2();

for t = 0:0.001:4.001
% 计算误差
k = int16(t*1000+1);
theta_error = theta_desired(:,k) - theta;
dtheta_error = dtheta_desired(:,k) - dtheta;
theta_error_plot(:,k) = theta_error;
```

```
% 更新M, C矩阵
    [M,C]=compute_MC(theta,dtheta);
    [M_desired, C_desired] = compute_MC(theta_desired(:,k), dtheta_desired(:,k));
         更新期望加速度
    ddtheta_desired_t = ddtheta_desired(:,k);
        获取无饱和的期望力矩
    torque_desired(:,k) =
M_desired*ddtheta_desired(:,k)+C_desired*dtheta_desired(:,k);
    % 获取ComputedTorque控制器的输出力矩
    Kp = 80;
    KV = 100;
    torque = M*(ddtheta_desired_t+Kv*dtheta_error+Kp*theta_error)+C*dtheta;
    if abs(torque(1,1)) >= 20
        torque(1,1) = torque(1,1)/abs(torque(1,1))*20;
    end
    if abs(torque(2,1)) >= 20
        torque(2,1) = torque(2,1)/abs(torque(2,1))*20;
    end
    torque_plot(:,k) = torque;
          真实关节加速度
    ddtheta = inv(M)*(torque-C*dtheta);
    ddtheta_plot(:,k) = ddtheta;
    dtheta = dtheta + ddtheta*0.001;
    dtheta_plot(:,k) = dtheta;
    theta = theta + dtheta*0.001 + ddtheta*0.001^2/2;
    theta_plot(:,k) = theta;
end
t = 0:0.001:4.001;
subplot(4,2,1)
plot(t,theta_plot(1,:),'r');
hold on
plot(t,theta_desired(1,:),'b');
title('theta1')
legend('实际输出','期望输出');
subplot(4,2,3)
plot(t,dtheta_plot(1,:),'r');
hold on
plot(t,dtheta_desired(1,:),'b');
legend('实际输出','期望输出');
title('dtheta1')
subplot(4,2,5)
plot(t,torque_plot(1,:),'r');
hold on
plot(t,torque_desired(1,:),'b');
title('torque1')
legend('实际输出','期望输出');
subplot(4,2,7)
plot(t,theta_error_plot(1,:),'b');
title('theta_error1')
subplot(4,2,2)
plot(t,theta_plot(2,:),'r');
hold on
plot(t,theta_desired(2,:),'b');
title('theta2')
legend('实际输出','期望输出');
subplot(4,2,4)
plot(t,dtheta_plot(2,:),'r');
```

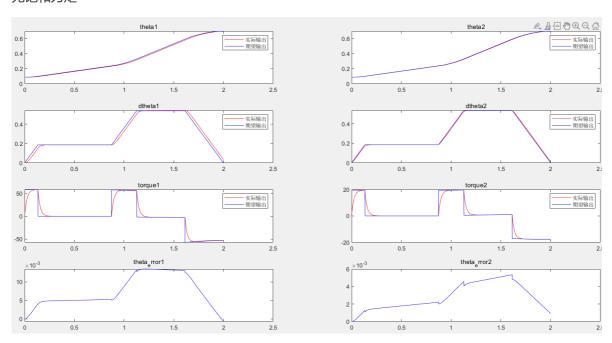
```
hold on
plot(t,dtheta_desired(2,:),'b');
legend('实际输出','期望输出');
title('dtheta2')
subplot(4,2,6)
plot(t,torque_plot(2,:),'r');
hold on
plot(t,torque_desired(2,:),'b');
title('torque2')
legend('实际输出','期望输出');
subplot(4,2,8)
plot(t,theta_error_plot(2,:),'b');
title('theta_error2')
```

## (ii)PD Control

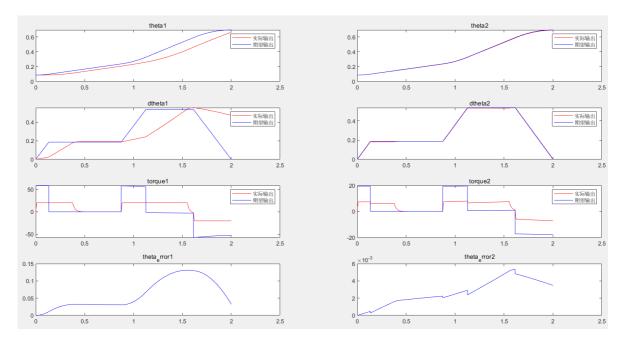
#### Problem1

Kp = 200; Kv = 1500;

#### 无饱和力矩



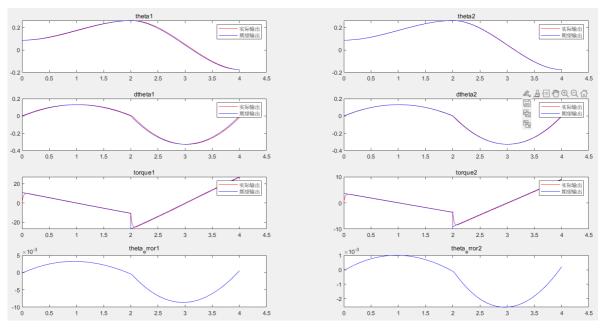
有饱和力矩



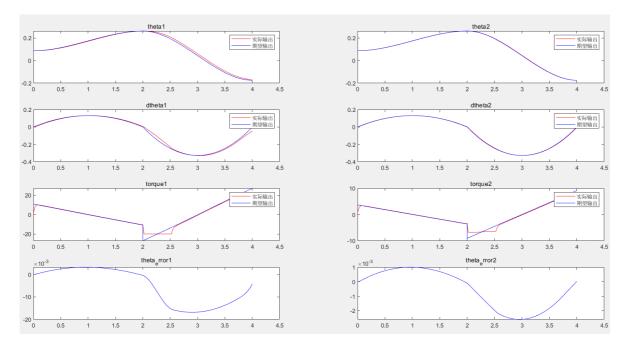
## Problem2

Kp = 200; Kv = 1500;

#### 无饱和力矩



有饱和力矩



```
c1c
clear
% 初始化机械臂参数
theta = [deg2rad(5);deg2rad(5)];
dtheta = [0;0];
ddtheta = [0;0];
% 获取M, C矩阵
[M,C]=compute_MC(theta,dtheta);
% 获取期望轨迹
[theta_desired,dtheta_desired,ddtheta_desired] = trajectory_problem2();
for t = 0:0.001:4.001
   %
         计算误差
    k = int16(t*1000+1);
    theta_error = theta_desired(:,k) - theta;
    dtheta_error = dtheta_desired(:,k) - dtheta;
    theta_error_plot(:,k) = theta_error;
   % 更新M, C矩阵
    [M,C]=compute_MC(theta,dtheta);
    [M_desired,C_desired]=compute_MC(theta_desired(:,k)),dtheta_desired(:,k));
         更新期望加速度
    ddtheta_desired_t = ddtheta_desired(:,k);
       获取无饱和的期望力矩
    torque_desired(:,k) =
M_desired*ddtheta_desired(:,k)+C_desired*dtheta_desired(:,k);
    % 获取PD控制器的输出力矩
   Kp = 200;
    KV = 1500;
    torque = Kp*theta_error+Kv*dtheta_error;
         饱和函数
    if abs(torque(1,1)) >= 20
       torque(1,1) = torque(1,1)/abs(torque(1,1))*20;
    end
    if abs(torque(2,1)) >= 20
        torque(2,1) = torque(2,1)/abs(torque(2,1))*20;
```

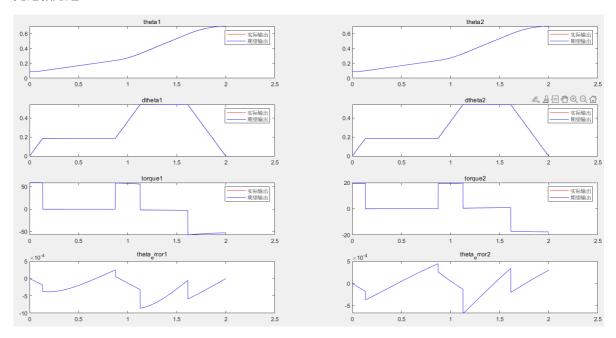
```
end
    torque_plot(:,k) = torque;
          真实关节加速度
    ddtheta = inv(M)*(torque-C*dtheta);
    ddtheta_plot(:,k) = ddtheta;
    dtheta = dtheta + ddtheta*0.001;
    dtheta_plot(:,k) = dtheta;
    theta = theta + dtheta*0.001 + ddtheta*0.001^2/2;
    theta_plot(:,k) = theta;
end
t = 0:0.001:4.001;
subplot(4,2,1)
plot(t,theta_plot(1,:),'r');
hold on
plot(t,theta_desired(1,:),'b');
title('theta1')
legend('实际输出','期望输出');
subplot(4,2,3)
plot(t,dtheta_plot(1,:),'r');
hold on
plot(t,dtheta_desired(1,:),'b');
legend('实际输出','期望输出');
title('dtheta1')
subplot(4,2,5)
plot(t,torque_plot(1,:),'r');
plot(t,torque_desired(1,:),'b');
title('torque1')
legend('实际输出','期望输出');
subplot(4,2,7)
plot(t,theta_error_plot(1,:),'b');
title('theta_error1')
subplot(4,2,2)
plot(t,theta_plot(2,:),'r');
plot(t,theta_desired(2,:),'b');
title('theta2')
legend('实际输出','期望输出');
subplot(4,2,4)
plot(t,dtheta_plot(2,:),'r');
hold on
plot(t,dtheta_desired(2,:),'b');
legend('实际输出','期望输出');
title('dtheta2')
subplot(4,2,6)
plot(t,torque_plot(2,:),'r');
hold on
plot(t,torque_desired(2,:),'b');
title('torque2')
legend('实际输出','期望输出');
subplot(4,2,8)
plot(t,theta_error_plot(2,:),'b');
title('theta_error2')
```

## (iii)Augmented PD control

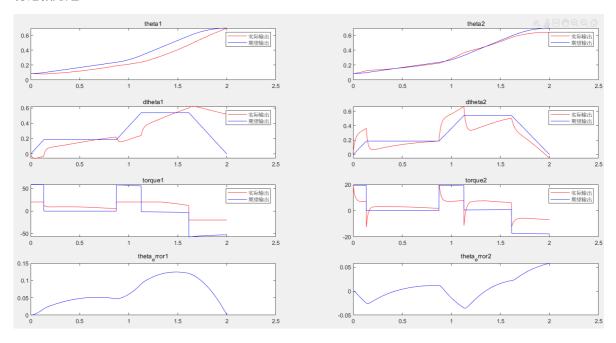
## Problem1

Kp = 150; Kv = 50;

#### 无饱和力矩



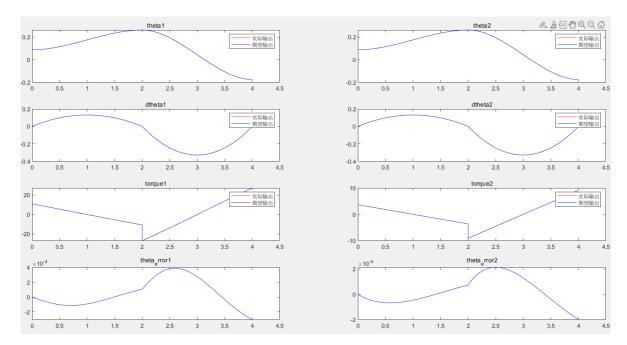
#### 有饱和力矩



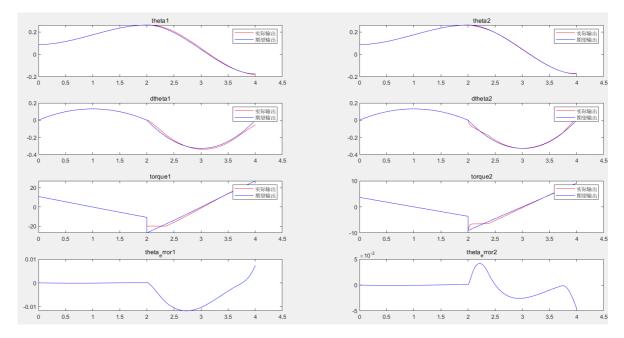
#### Problem2

Kp = 150; Kv = 50;

无饱和力矩



#### 有饱和力矩



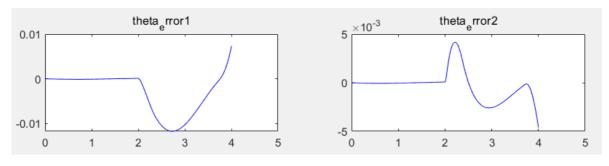
```
dtheta_error = dtheta_desired(:,k) - dtheta;
    theta_error_plot(:,k) = theta_error;
    % 更新M, C矩阵
    [M,C]=compute_MC(theta,dtheta);
    [M_desired,C_desired]=compute_MC(theta_desired(:,k),dtheta_desired(:,k));
         更新期望速度
    dtheta_desired_t = dtheta_desired(:,k);
          更新期望加速度
    ddtheta_desired_t = ddtheta_desired(:,k);
      获取无饱和的期望力矩
    torque_desired(:,k) =
M_desired*ddtheta_desired(:,k)+C_desired*dtheta_desired(:,k);
    % 获取AugmentedPD控制器的输出力矩
    Kp = 150;
    Kv = 50;
    torque = M*ddtheta_desired_t + C*dtheta_desired_t + Kp*theta_error +
Kv*dtheta_error;
         饱和函数
    if abs(torque(1,1)) >= 20
       torque(1,1) = torque(1,1)/abs(torque(1,1))*20;
    end
    if abs(torque(2,1)) >= 20
       torque(2,1) = torque(2,1)/abs(torque(2,1))*20;
    end
    torque_plot(:,k) = torque;
         真实关节加速度
    ddtheta = inv(M)*(torque-C*dtheta);
    ddtheta_plot(:,k) = ddtheta;
    dtheta = dtheta + ddtheta*0.001;
    dtheta_plot(:,k) = dtheta;
    theta = theta + dtheta*0.001 + ddtheta*0.001^2/2;
    theta_plot(:,k) = theta;
end
t = 0:0.001:4.001;
subplot(4,2,1)
plot(t,theta_plot(1,:),'r');
hold on
plot(t,theta_desired(1,:),'b');
title('theta1')
legend('实际输出','期望输出');
subplot(4,2,3)
plot(t,dtheta_plot(1,:),'r');
hold on
plot(t,dtheta_desired(1,:),'b');
legend('实际输出','期望输出');
title('dtheta1')
subplot(4,2,5)
plot(t,torque_plot(1,:),'r');
hold on
plot(t,torque_desired(1,:),'b');
title('torque1')
legend('实际输出','期望输出');
subplot(4,2,7)
plot(t,theta_error_plot(1,:),'b');
title('theta_error1')
subplot(4,2,2)
plot(t,theta_plot(2,:),'r');
```

```
hold on
plot(t,theta_desired(2,:),'b');
title('theta2')
legend('实际输出','期望输出');
subplot(4,2,4)
plot(t,dtheta_plot(2,:),'r');
hold on
plot(t,dtheta_desired(2,:),'b');
legend('实际输出','期望输出');
title('dtheta2')
subplot(4,2,6)
plot(t,torque_plot(2,:),'r');
hold on
plot(t,torque_desired(2,:),'b');
title('torque2')
legend('实际输出','期望输出');
subplot(4,2,8)
plot(t,theta_error_plot(2,:),'b');
title('theta_error2')
```

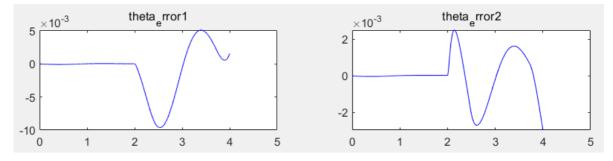
## 控制参数与位置误差的关系

以Augmented PD控制器为例

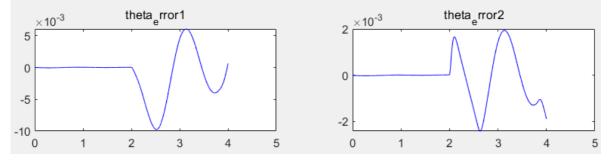
Kp = 150; Kv = 50;



Kp = 500; Kv = 50;

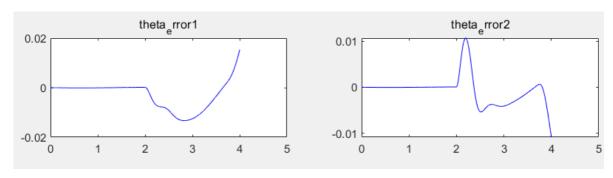


Kp = 1000; Kv = 50;

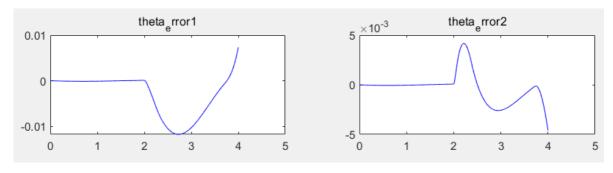


比例系数的增大可有效降低跟踪误差,但可能会导致震荡

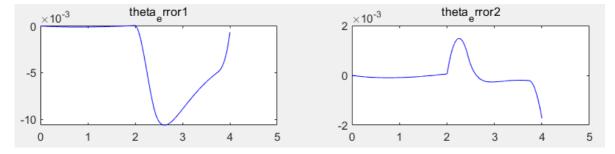
Kp = 150; Kv = 10;



Kp = 150; Kv = 50;



Kp = 150; Kv = 200;



微分系数的增大可有效降低跟踪误差,但可能会对变化大的输入响应剧烈导致饱和。同时随着微分系数 的增大,其对降低跟踪误差的效率也下降

## 结论

综上,可以看出在相同参数下,使用三次多项式规划的轨迹比使用LFPB规划的轨迹在实际控制中可以获得更加平滑且更加优异的跟踪性能。

而对于不同的控制器, Augmented PD控制器最优