Node Method

- 1) relecta reference node, ground, defined to be OV potential
- 2 label potential of remaining nodes wit ground node. Nodes connected to ground via an independent source is labelled with the voltage of the source (with appropriate ground via an independent source is labelled with the voltage of the source (polanty)
- 3) Remaining unknown labelled
- unte (KCL) for nodes nigh unknown voltage applying element lans/ KUL
- solve for unknown potentials and back solve /substitute for branch voltage / current

Actively 1

OR by quoting whate divider principle:

$$v_{\alpha} = \frac{p_2}{p_1 + p_2} v_1$$

Applying KCL at node
$$Va: i_1 = i_2$$

$$\frac{V_1 - V_{\alpha}}{R_1} = \frac{V_{\alpha} - O}{R_2}$$

$$Va\left(\frac{1}{R_2} + \frac{1}{R_1}\right) = \frac{V_1}{R_1}$$

$$V_{\alpha} = \frac{R^2}{R_1 + R_2} V_1$$

Applying ICCL at node Vb: 1's = 2'4

$$\frac{V_1 - V_b}{R_3} = \frac{V_b - 0}{R_4}$$

$$V_h = \frac{p_4}{p_3 + p_4} V_1$$

not equivalent
$$V_{AB} = V_a - V_b = V_1 \left(\frac{R_2}{R_1 + R_2} - \frac{R_4}{R_2 + R_4} \right)$$

yevere polantiti. $V_{BA} = V_b - V_a = V_1 \left(\frac{I^2 q}{R_2 + R_4} - \frac{R_2}{R_1 + R_2} \right)$

Suppore
$$R_1, R_2, R_3 = R$$

$$R_4 = R + \triangle R$$

$$V_{Al3} = V_1 \left(\frac{R}{R+R+\Delta R} - \frac{R+\Delta R}{R+R+\Delta R} \right)$$

$$= V_1 \left(\frac{1}{2} - \frac{1+\frac{\Delta R}{R}}{1+1+\frac{\Delta R}{R}} \right)$$

$$= V_1 \left(\frac{1}{2} - \frac{1+X}{2+X} \right)$$

$$= \left(\frac{-X}{4+2X} \right) V_1$$

$$4V_{A13} + 2 \times V_{A13} = - \times V_1$$

$$\times$$
 ($2V_{A13} + V_1$) = $-4V_{A13}$

$$X = \frac{\Delta R}{12} = \frac{-4VAI3}{2V_{AI3} + V_{I}}$$

Supernodes

troat the group of elements as a black box / super node current going into the supernode = current coming out of super node (KCL)

independent where source

$$e_2 = e_1 - V$$

$$V_1 = 5.12 \text{ V}$$

from activity 1:
$$\frac{\Delta R}{R} = \frac{-4V_{A13}}{2V_{A13} + V_{1}}$$

$$\Delta R = \frac{-4V_{AB}}{2V_{AB}+V_{I}} \cdot |2$$

			(190
Resistance Ry/SL	WHage VAI3/mV	DR wing precing equation/sh	OR using linear approximation / IL
480	53	-20128	- 20, 70
490 N	26	- 10.05	- 10, 16
510 1	- 25	9.86	9,77
20 N	- 52	20.73	21,31
		1	

~ see sound of emor in discussion behind ~

Linear approximation

when
$$\Delta R << R$$
, $\frac{\Delta R}{R} \approx 0$

from activity 1:
$$V_{AB} = \left(\frac{-x}{4+2x}\right)V_1$$
 where $x = \frac{312}{12}$

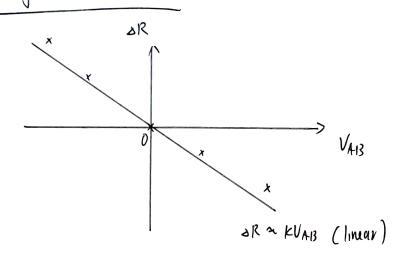
If we allow the x in the denominator to \rightarrow \cup , we can obtain a linear approximation of $\triangle R$

◆ we cannot let the numerator in the equation to → 0 as the equation $V_{AB} = 0.V_1$ would have no ureful. Meaning

VAB
$$\approx \frac{12}{4}$$
 VI
 $\Delta R \approx -\frac{4V_{AB} \cdot R}{V_{I}}$ $= -390.625 \Omega/V$
 $\Delta R \approx KV_{AB}$ where $k = -\frac{4R}{V_{I}}$ $= -390.625 \Omega/V$

a fill in the fable ~

Analysis and Observations



The equation from activity 1 is non linear, with value of BR curing away from the linear approximation a, VAR gets larger

company 212 value, obtained using the linear approx and precise equation, they follow closely for smaller values for VAIS | but dways more when [VAB] is larger.

However, assuming we are operating in the range where DR is relately small compared to R, wing a linear approximation is very much appropriate

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 and there might be uncertaing to getting each variable reportor to exactly 500 DI was challenging and there might be uncertaing to
- @ even if the readings on the shmete read 500_D, there might be uncertainly in the equipment
- (3) Initial VAB for reference was not exactly o 3 ImV which would affect late measurement, of VAB when JSR in arean)