

EEE 51: Second Semester 2017 - 2018 Lecture 9

Differential Circuits

Today

• Differential Circuits



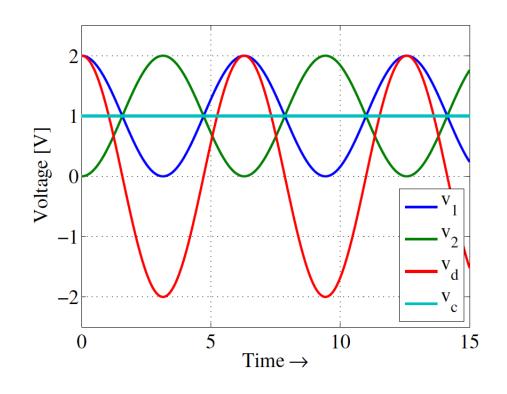
Differential Signals Revisited

Limit analysis to sinusoids → easier analysis

$$v_{i1} = \frac{\widehat{V}}{2}\cos(\omega t) + V_{cm}$$
$$v_{i2} = -\frac{\widehat{V}}{2}\cos(\omega t) + V_{cm}$$

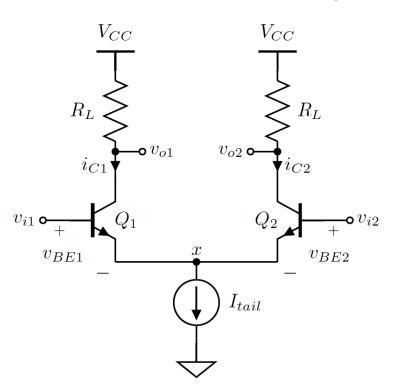
$$v_{id} = v_{i1} - v_{i2} = \hat{V}\cos(\omega t)$$
$$v_{ic} = \frac{v_{i1} + v_{i2}}{2} = V_{cm}$$

Common-mode ≈ DC Offset



Recall: The Differential Pair (1)

BJT: The emitter-coupled pair DC Analysis



KVL at the input loop:
$$V_{i1} - V_{BE1} + V_{BE2} - V_{i2} = 0$$

$$V_{i1} - V_{i2} = V_{BE1} - V_{BE2}$$

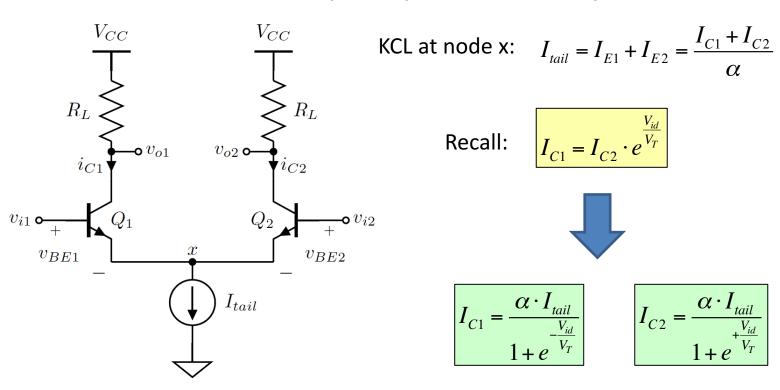
$$V_{id} = V_T \ln \left(\frac{I_{C1}}{I_S}\right) - V_T \ln \left(\frac{I_{C2}}{I_S}\right) = V_T \ln \left(\frac{I_{C1}}{I_{C2}}\right)$$



$$I_{C1} = I_{C2} \cdot e^{\frac{V_{id}}{V_T}}$$

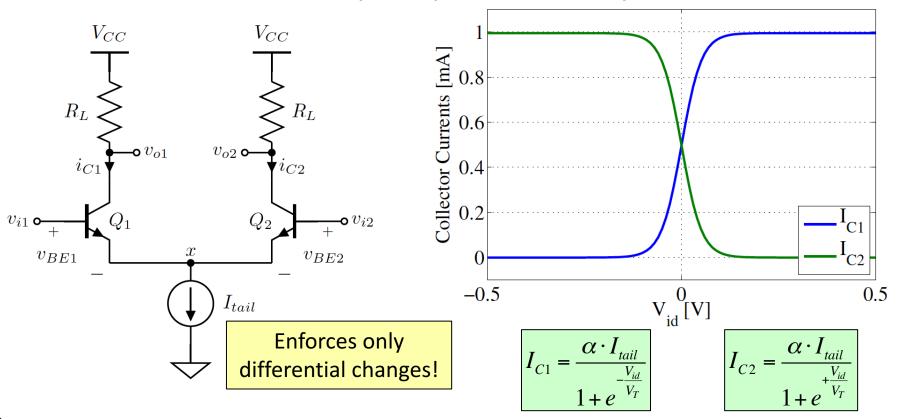
Recall: The Differential Pair (2)

BJT: The emitter-coupled pair DC Analysis



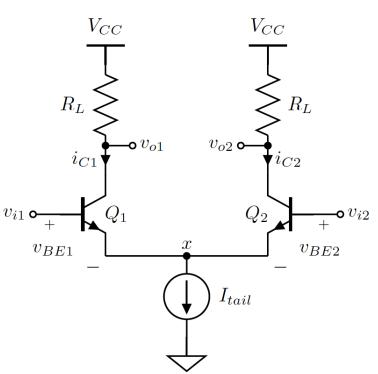
Recall: The Differential Pair (3)

BJT: The emitter-coupled pair DC Analysis



Recall: The Differential Pair (4)

Output Voltage



$$I_{C1} = \frac{\alpha \cdot I_{tail}}{1 + e^{\frac{-V_{id}}{V_T}}}$$

$$I_{C2} = \frac{\alpha \cdot I_{tail}}{1 + e^{+\frac{V_{id}}{V_T}}}$$

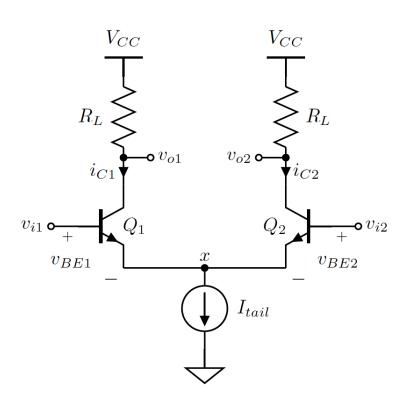
KVL at the output loop:

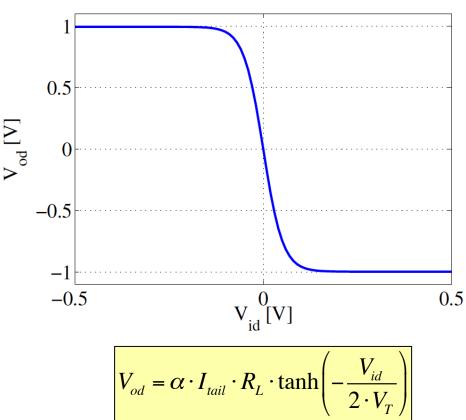
$$V_{od} = V_{o1} - V_{o2} = R_L (I_{C2} - I_{C1})$$

$$V_{od} = \alpha \cdot I_{tail} \cdot R_L \cdot \left(\frac{1}{1 + e^{\frac{V_{id}}{V_T}}} - \frac{1}{1 + e^{\frac{V_{id}}{V_T}}} \right)$$
$$= \alpha \cdot I_{tail} \cdot R_L \cdot \tanh\left(-\frac{V_{id}}{2 \cdot V_T}\right)$$

Recall: The Differential Pair (5)

• Transfer Characteristic

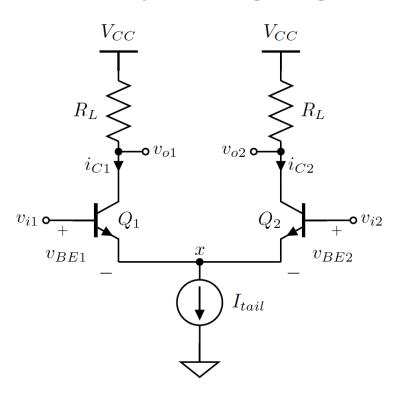




$$V_{od} = \alpha \cdot I_{tail} \cdot R_L \cdot \tanh\left(-\frac{V_{id}}{2 \cdot V_T}\right)$$

Common-Mode Input Range (1)

BJT Operating Region?



Assume zero differential input

$$\mathsf{KVL:} \qquad V_{CE1} = V_{CC} - I_{C1} R_L - V_X > V_{CE,sat}$$

Note:
$$V_X = V_{I1} - V_{BE1}$$

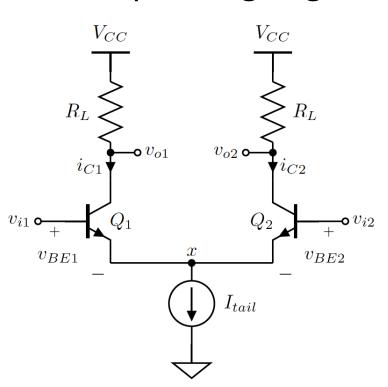
$$= V_{I1} - V_T \ln \left(\frac{I_{C1}}{I_S} \right)$$

V_X is controlled by the input common-mode (DC input)!

$$V_{CE1} = V_{CC} - I_{C1}R_L - V_{I1} + V_T \ln\left(\frac{I_{C1}}{I_S}\right)$$

Common-Mode Input Range (2)

BJT Operating Region?



For zero differential input: $v_{ic} = V_{I1} = V_{I2} = V_{cm}$

$$I_{C1} = I_{C2} = \frac{I_{tail}}{2}$$



For a range of common-mode inputs!

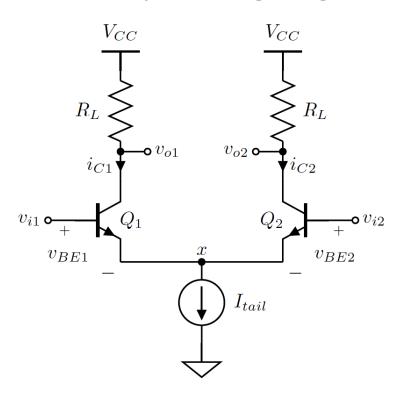
$$V_{CE1} = V_{CC} - I_{C1}R_L - V_{I1} + V_T \ln\left(\frac{I_{C1}}{I_S}\right)$$



$$V_{CE1} = V_{CC} - \frac{I_{tail}R_L}{2} - V_{cm} + V_T \ln\left(\frac{I_{tail}}{2 \cdot I_S}\right) > V_{CE,sat}$$

Common-Mode Input Range (3)

BJT Operating Region?



$$V_{CE1} = V_{CC} - \frac{I_{tail}R_L}{2} - V_{cm} + V_T \ln\left(\frac{I_{tail}}{2 \cdot I_S}\right) > V_{CE,sat}$$

$$V_{cm} < V_{CC} - \frac{I_{tail}R_L}{2} + V_T \ln\left(\frac{I_{tail}}{2 \cdot I_S}\right) - V_{CE,sat}$$

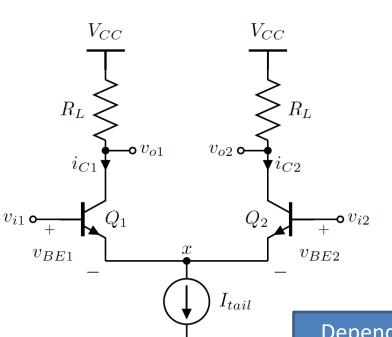
Maximum common-mode input voltage:

$$V_{cm,\text{max}} = V_{CC} - \frac{I_{tail}R_L}{2} + V_T \ln\left(\frac{I_{tail}}{2 \cdot I_S}\right) - V_{CE,sat}$$

Common-Mode Input Range (4)

BJT Operating Region?

If the tail current is not ideal $\rightarrow V_{min}$



$$\begin{split} V_X &= V_{I1} - V_{BE1} \\ &= V_{I1} - V_T \ln \left(\frac{I_{C1}}{I_S} \right) = V_{cm} - V_T \ln \left(\frac{I_{tail}}{2 \cdot I_S} \right) > V_{\min} \\ &\qquad \qquad V_{cm} > V_{\min} + V_T \ln \left(\frac{I_{tail}}{2 \cdot I_S} \right) \end{split}$$

Minimum common-mode input voltage:

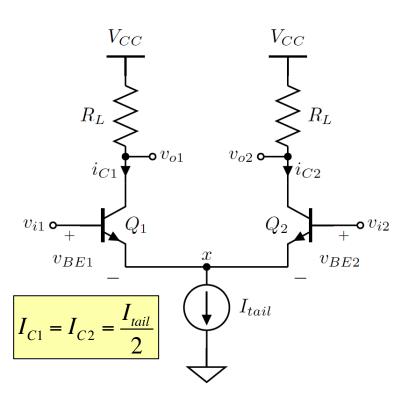
Dependent on the tail current source

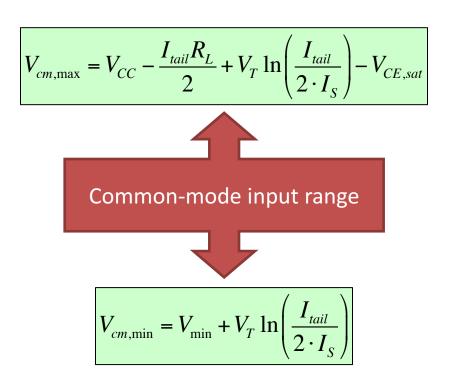


$$V_{cm,\min} = V_{\min} + V_T \ln \left(\frac{I_{tail}}{2 \cdot I_S} \right)$$

Common-Mode Input Range (5)

BJT Operating Region → set by the input common-mode!





Next Meeting

Continue with Differential Circuits