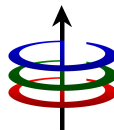


# ECE 113: Communication Electronics

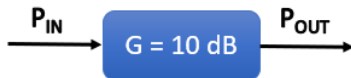
## Meeting 2: Noise in Communication System

January 18, 2019



# Dynamic Range

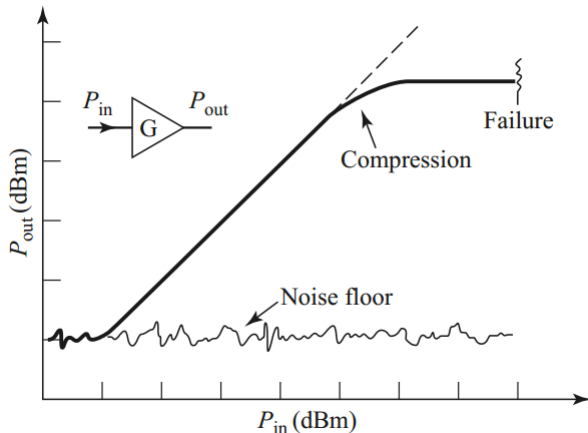
Consider an amplifier having a gain ( $G_{dB} = 10dB$ )



- Ideally ( $P_{out} = G * P_{in}$ )
- Realistically ( $P_{out} \neq G * P_{in}$ )
  - $P_{out} \neq 0$  when  $P_{in} = 0$  due to non-zero noise power
  - $P_{out} \neq G * P_{in}$  for very large  $P_{in}$  due to saturation of nonlinear devices

## Dynamic Range

Range of signal Levels over which linear relationship between input and output is valid

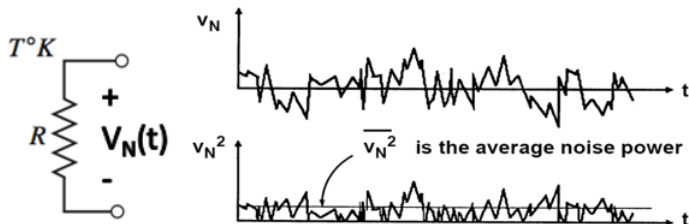


# Electronic Noise

- Caused by random motion of charges in devices and materials
- Various sources of noise
  - Thermal Noise (Johnson or Nyquist Noise)- caused by thermal vibration of bound charges
  - Shot Noise - applicable to electron tube and solid-state devices
  - Flicker Noise -  $\frac{1}{f}$  noise that occurs in most electronic devices
  - Plasma Noise, Quantum Noise, etc.

# Thermal Noise in Resistors

Consider a resistor at a temperature ( $T$ ) degrees Kelvin (K).



- Planck's black body radiation law.

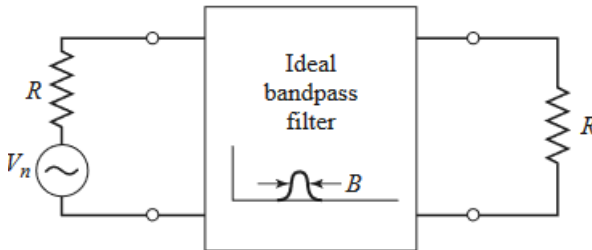
$$v_n = \sqrt{\frac{4hfBR}{e^{hf/kT} - 1}}$$

# Thermal Noise at RF

- At microwave frequencies,  $hf \ll kT$ .

$$v_n = \sqrt{4kTBR} \quad \text{Rayleigh-Jeans approximation}$$

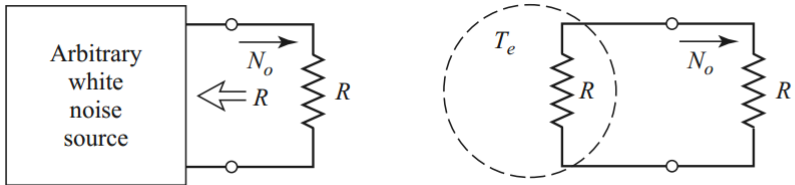
- Equivalent circuit for a noisy resistor



$$P_n = kTB$$

# Equivalent Noise Temperature

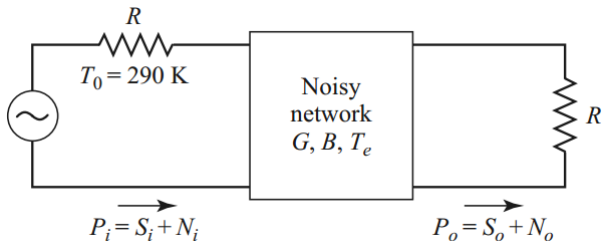
- A white noise source can be replaced by a noisy resistor of value  $R$  at temperature  $T_e$  so that the same noise power is delivered to the load.



$$T_e = \frac{N_o}{kB}$$

# Noise Factor (F)

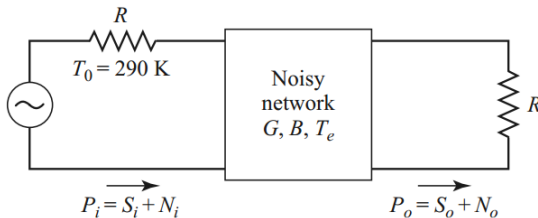
- Measure of degradation of the signal-to-noise ratio between input and output of the component
- When noise and a desired signal are applied to the input of a **noiseless network**, both noise and desired signal will be amplified/attenuated by the same factor



- If the network is **noisy**, the output noise power will be **increased more than** the desired signal power



# Noise Factor



- Input noise power results from a matched resistor at  $T_o = 290\text{ K}$ 
  - $N_i = kT_oB$
- $N_o = kG(T_o + T_e)B$
- With  $S_o = GS_i$

$$F = \frac{S_i}{kT_oB} \frac{kG(T_o + T_e)B}{GS_i} = 1 + \frac{T_e}{T_o} \geq 1$$

# Noise Figure (NF)

- Identical with Noise Factor, except that it is given in **dB**

if 
$$F = \frac{SNR_{in}}{SNR_{out}}$$

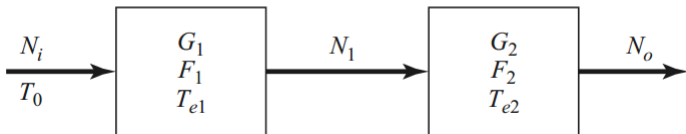
$$NF = 10\log(F) = 10\log\left(\frac{SNR_{in}}{SNR_{out}}\right)$$

- Noise figure and equivalent noise temperatures are interchangeable characterizations of noise properties of component (in practice, NF is used)
- Noise figure for passive components
  - At thermal equilibrium,  $F = L$
  - Example: a 6 dB attenuator has a NF of 6 dB

# Cascaded Systems

- Typical microwave system consists of multiple stages - each of which can degrade SNR to varying degrees
- Consider a cascade of 2 components

$$N_1 = G_1 k T_0 B + G_1 k T_{e1} B,$$



- The cascaded equivalent noise temperature

$$T_{cas} = T_{e1} + \frac{1}{G_1} T_{e2}$$

- It can also be shown that

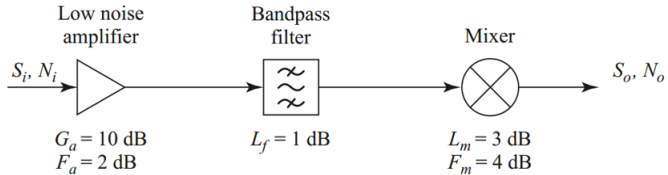
$$F_{cas} = F_1 + \frac{1}{G_1} (F_2 - 1)$$

- Extending it to arbitrary number of stages,

$$F_{cas} = F_1 + \frac{F_2 - 1}{G_1} + \frac{F_3 - 1}{G_1 G_2} + \dots$$

# Examples

- Compute the overall NF of the system



- If the input noise power from a feeding antenna is  $N_i = kT_A B$  where  $T_A = 150K$ , then find the output noise power in dBm. Assume system is at temperature  $T_o = 290K$  and bandwidth of 10 MHz
- If  $SNR = 20$  dB is required at the output of receiver, what is the minimum input signal power (in dBm)?

**END**