

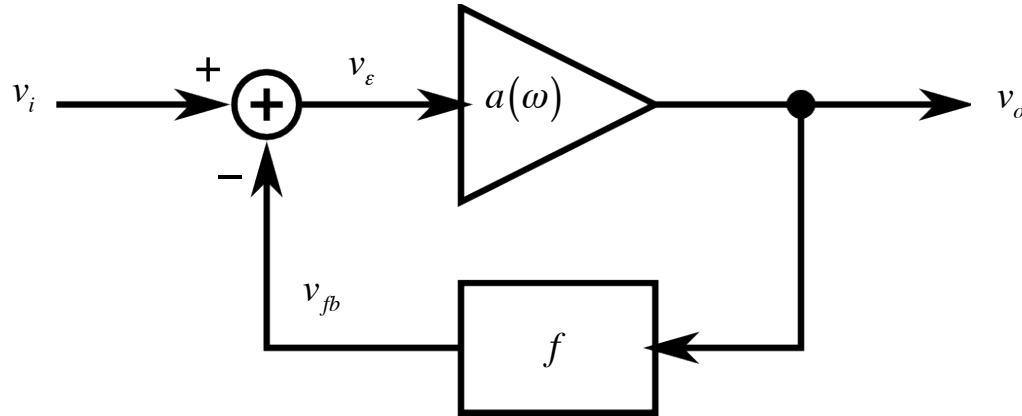


EEE 51: Second Semester 2017 - 2018

Lecture 21

Feedback Frequency Response

Pole and Zero Locations



$$a(s) = \frac{N(s)}{D(s)}$$

$$A_{CL}(s) = \frac{\frac{N(s)}{D(s)}}{1 + \frac{N(s)}{D(s)}f} = \frac{N(s)}{D(s) + N(s) \cdot f}$$

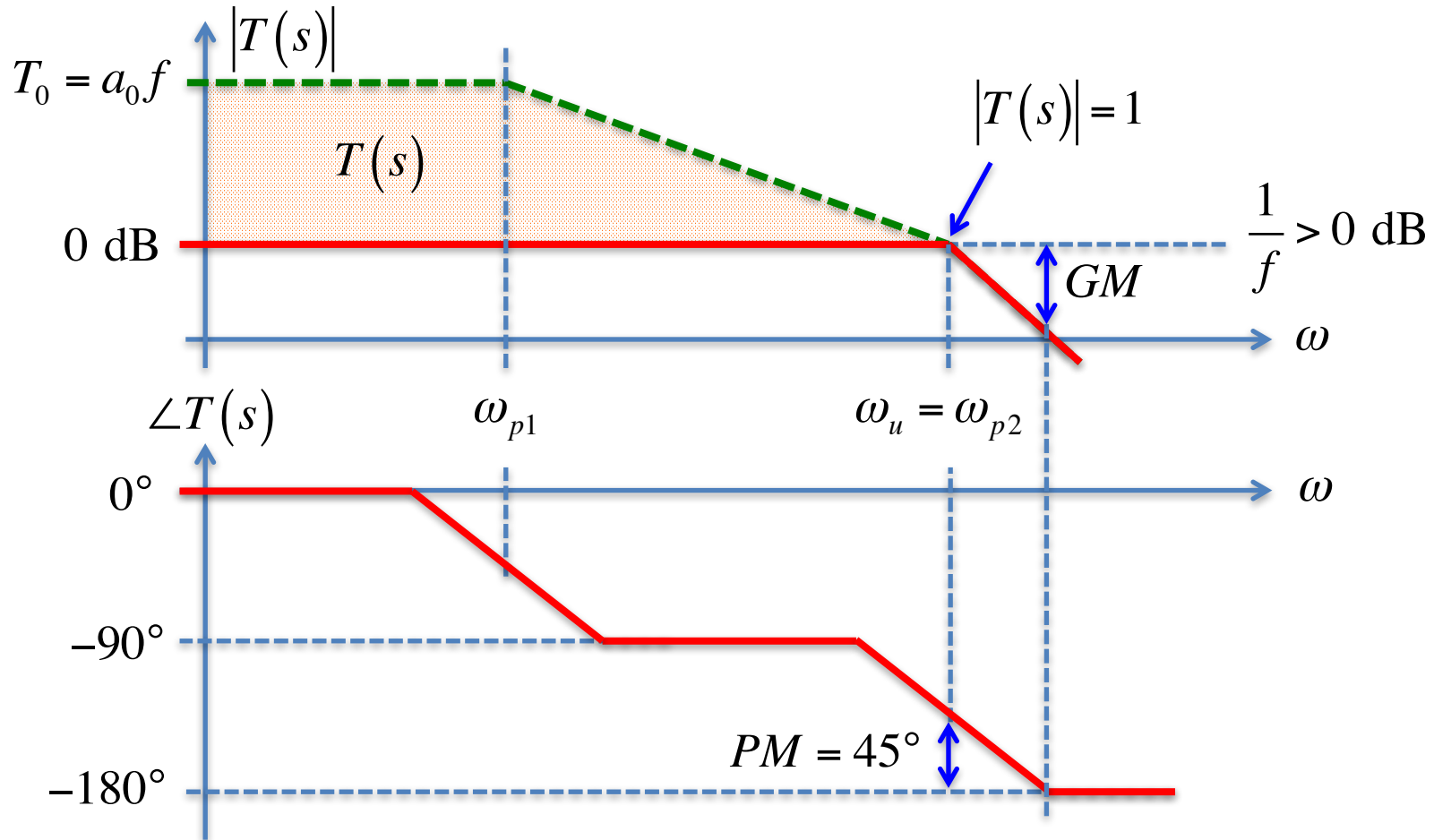
← Zeros of $a(s)$

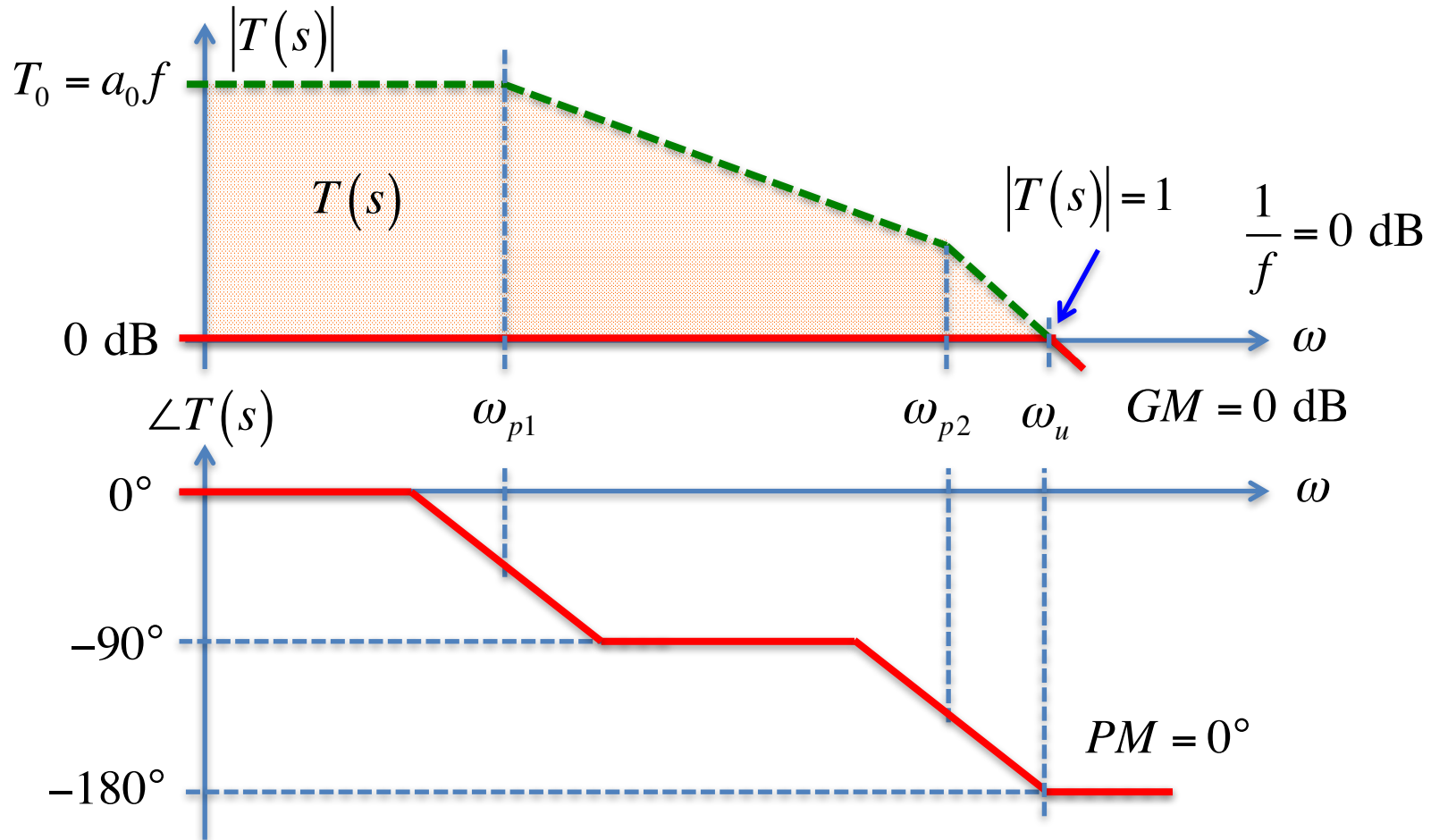
← Poles of $a(s)$

Compensation

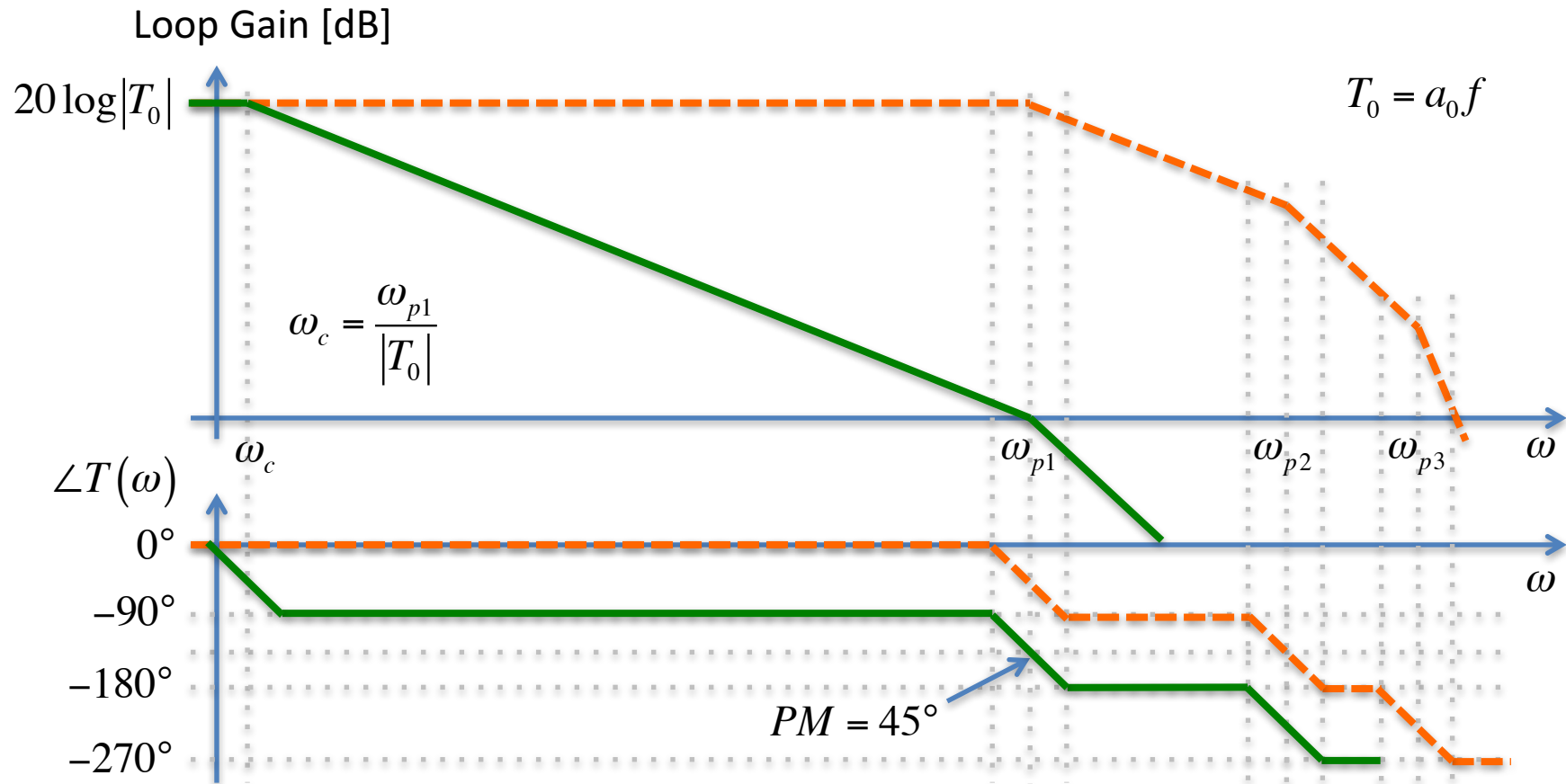
- A method where an amplifier is modified so that it is stable
- Main Idea:
 - At the frequency ω_{180} where loop gain phase is equal to -180° , make sure that $|T(\omega_{180})| < 1$
- Alternate:
 - At $|T(\omega_u)| = 1$, make the loop gain phase less than -180°







Narrowbanding: Adding a Dominant Pole



Narrowbanding

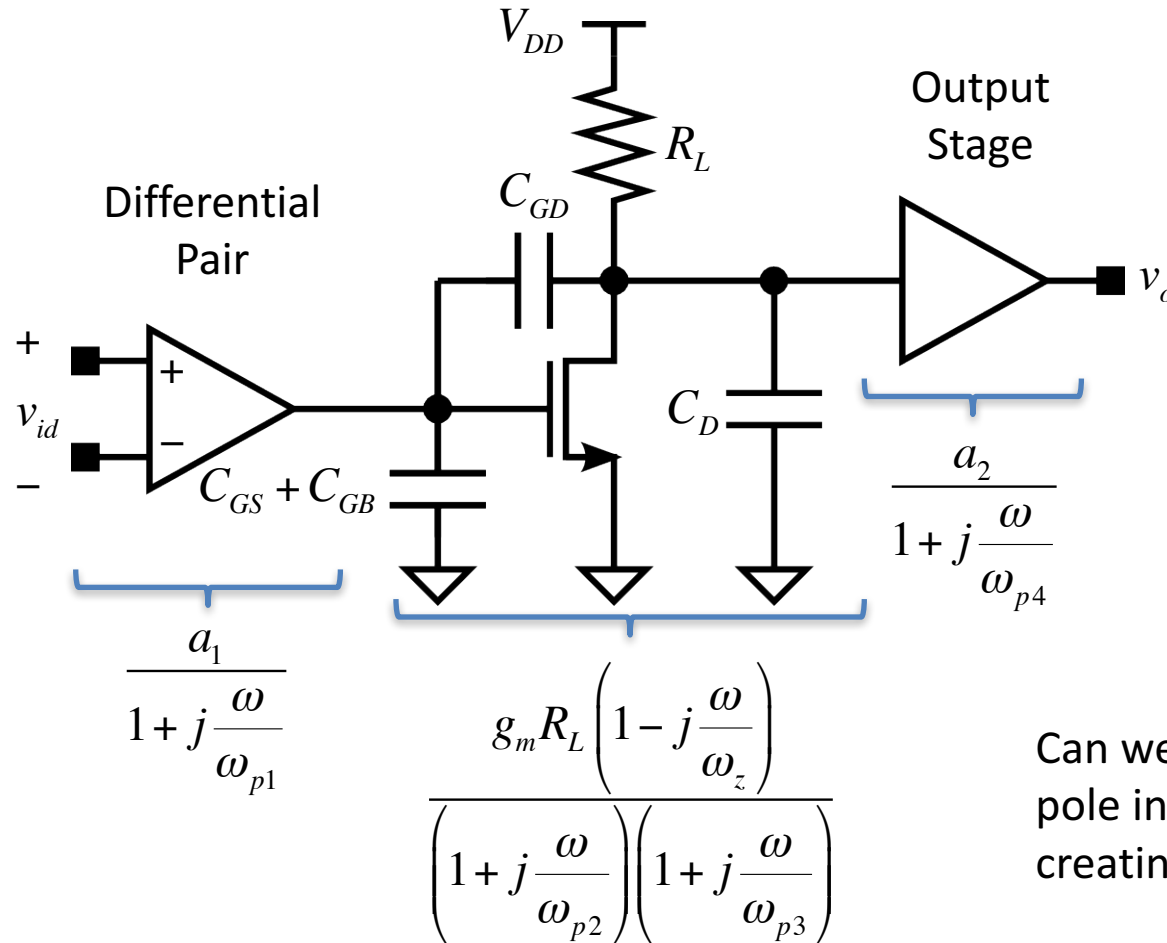
- In order to get a phase margin of 45°
 - Add a compensation pole at

$$\omega_c = \frac{\omega_{p1}}{|T_0|} = \frac{\omega_{p1}}{|a_0 f|}$$

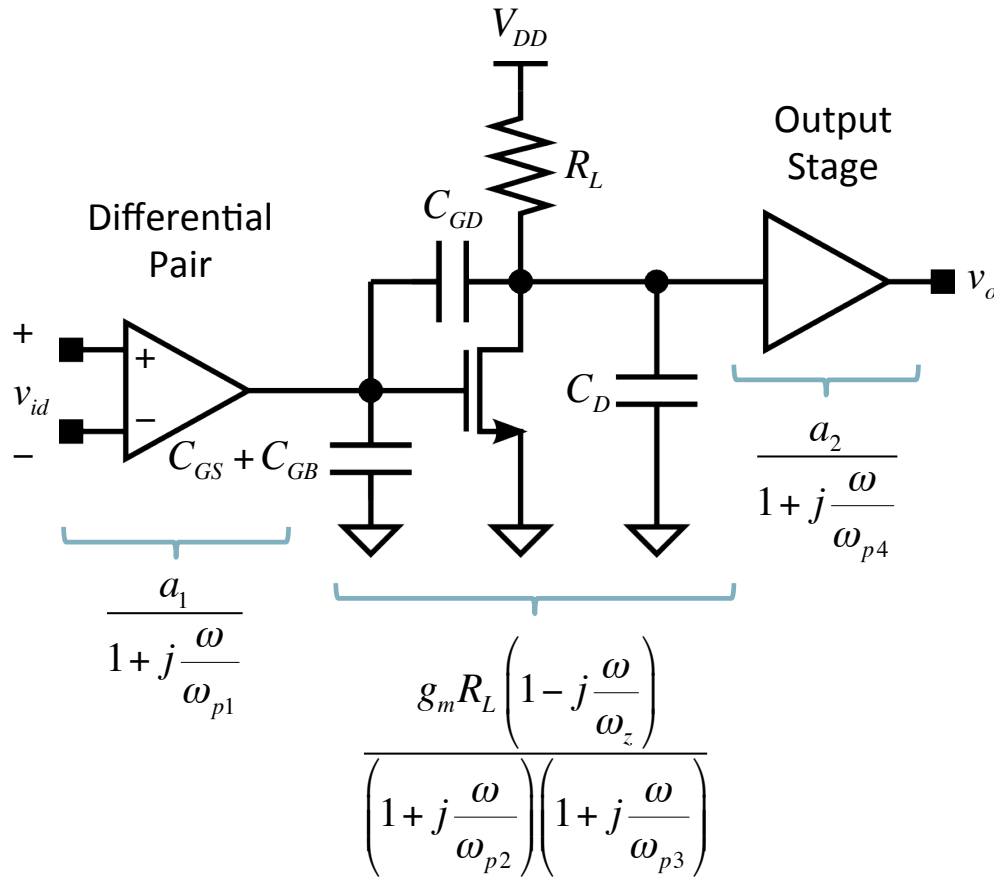
- Example: $f_{p1} = 1 \text{ MHz}$, $|a_0 f| = 10^4$
 - $f_c = 100 \text{ Hz}$
 - -90° phase shift from the new compensation pole
 - -45° from the original (and now second) pole



Pole Splitting



Pole Splitting



Assume $\omega_{p4} \gg \omega_{p1}$:

$$\omega_{p2} = \frac{1}{R_{o,diff} C_{GS}}$$

$$\omega_{p3} = \frac{1}{R_L C_D}$$

$$\omega_z = \frac{g_m}{C_{GD}}$$

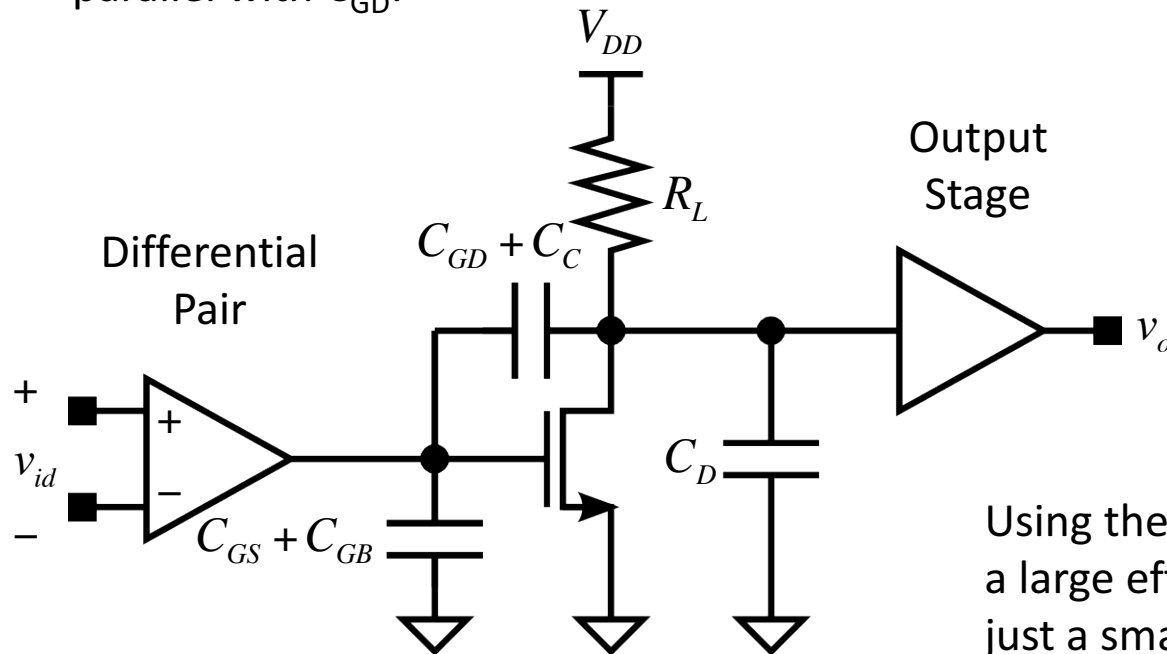
Since there are 4 poles, we must make sure that the amplifier is stable

Can we do this by just making one of the existing poles the dominant pole?



Pole Splitting

Add a compensation capacitance C_C in parallel with C_{GD} :



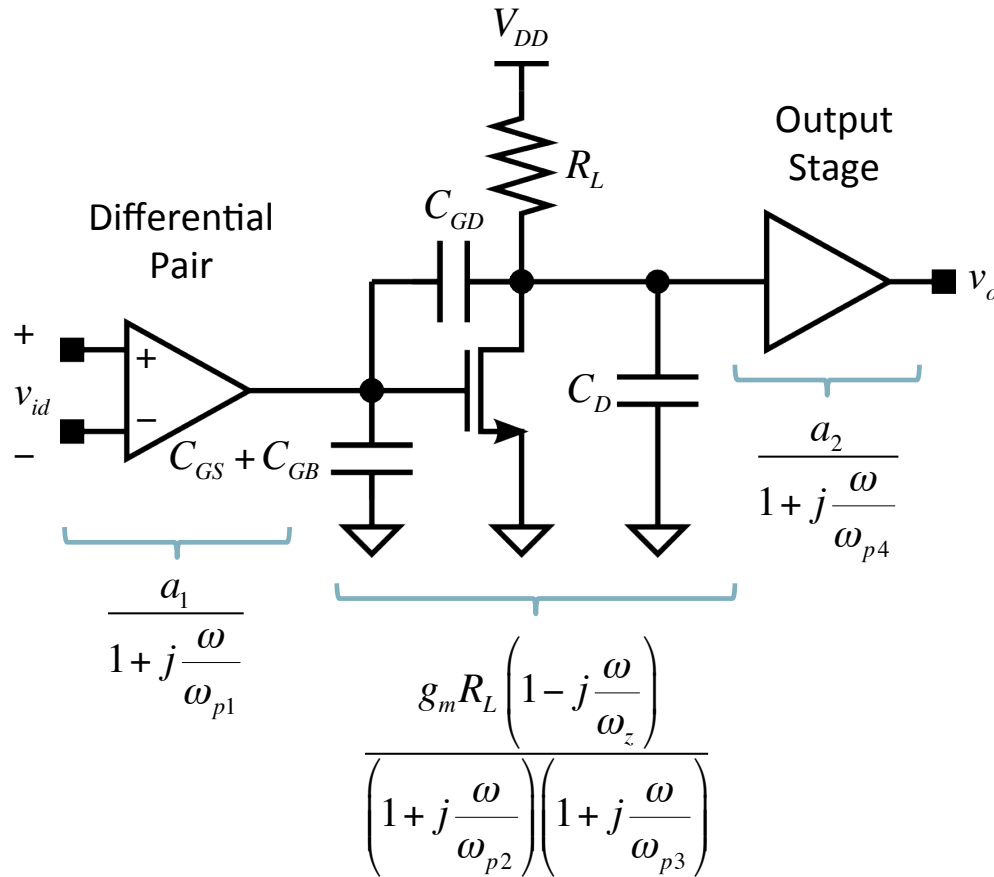
$$\omega_{p2} = \frac{1}{R_{o,diff} (1 + g_m R_L) C_C}$$

$$\omega_{p3} = \frac{g_m}{C_{GS} + C_D}$$

$$\omega_z = \frac{g_m}{C_C}$$

Using the Miller effect, we can add a large effective capacitance using just a small physical capacitance

Example:



$$R_{o,diff} = 10\text{M}\Omega$$

$$R_L = 5\text{M}\Omega$$

$$C_{GS} = C_D = 0.1\text{pF}$$

$$g_m = 10^{-3}\text{S}$$

$$\omega_{p1} = 10 \frac{\text{Mrad}}{\text{s}}$$

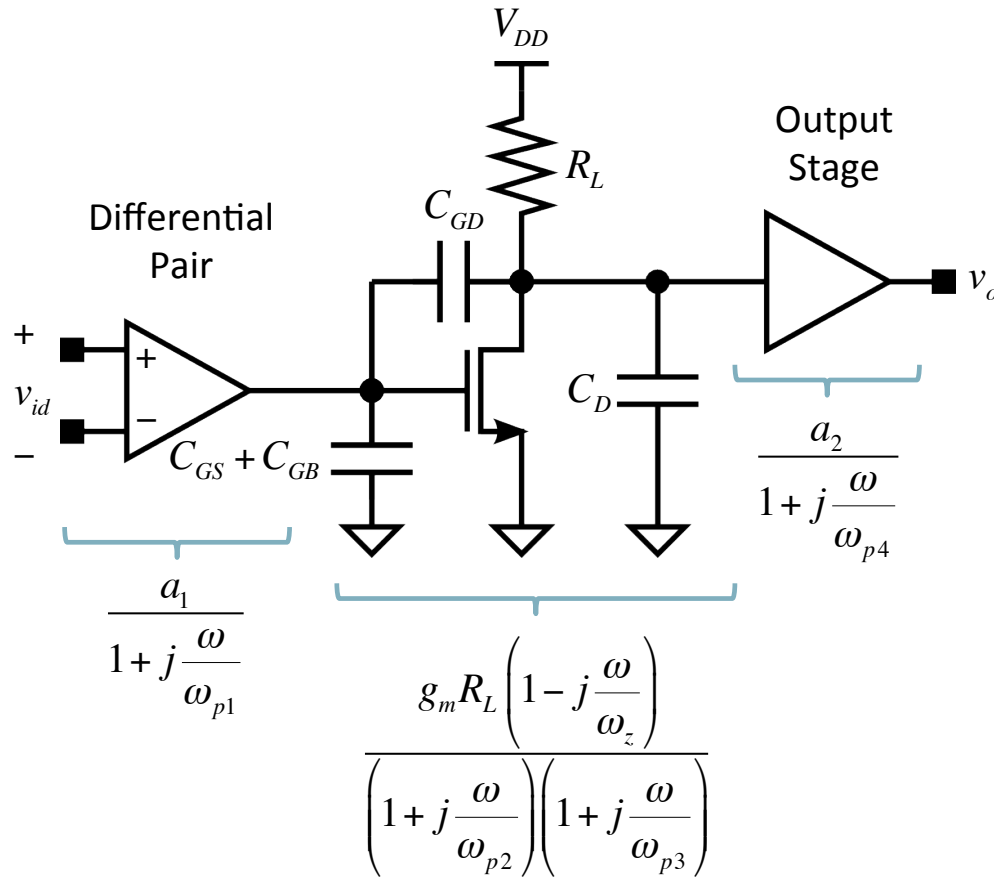
$$\omega_{p4} = 100 \frac{\text{Mrad}}{\text{s}}$$

$$a_1 = 10^3$$

$$a_2 = 1$$



Before Compensation and with $C_{GD} = 0$:

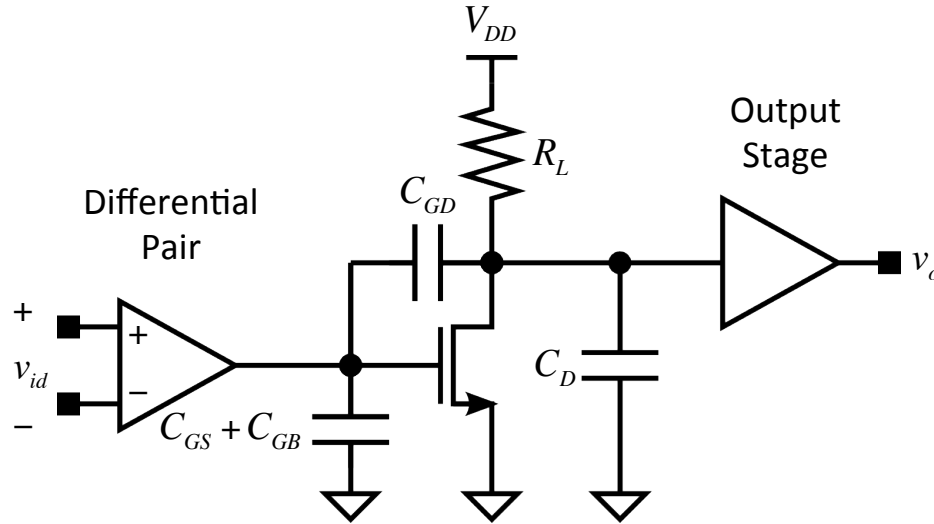


$$\omega_{p2} = \frac{1}{R_{o,diff} C_{GS}} = 1 \frac{\text{Mrad}}{s}$$

$$\omega_{p3} = \frac{1}{R_L C_D} = 2 \frac{\text{Mrad}}{s}$$

$$\omega_z = \frac{g_m}{C_{GD}} \rightarrow \infty$$

Before Compensation and with $C_{GD} = 0$:



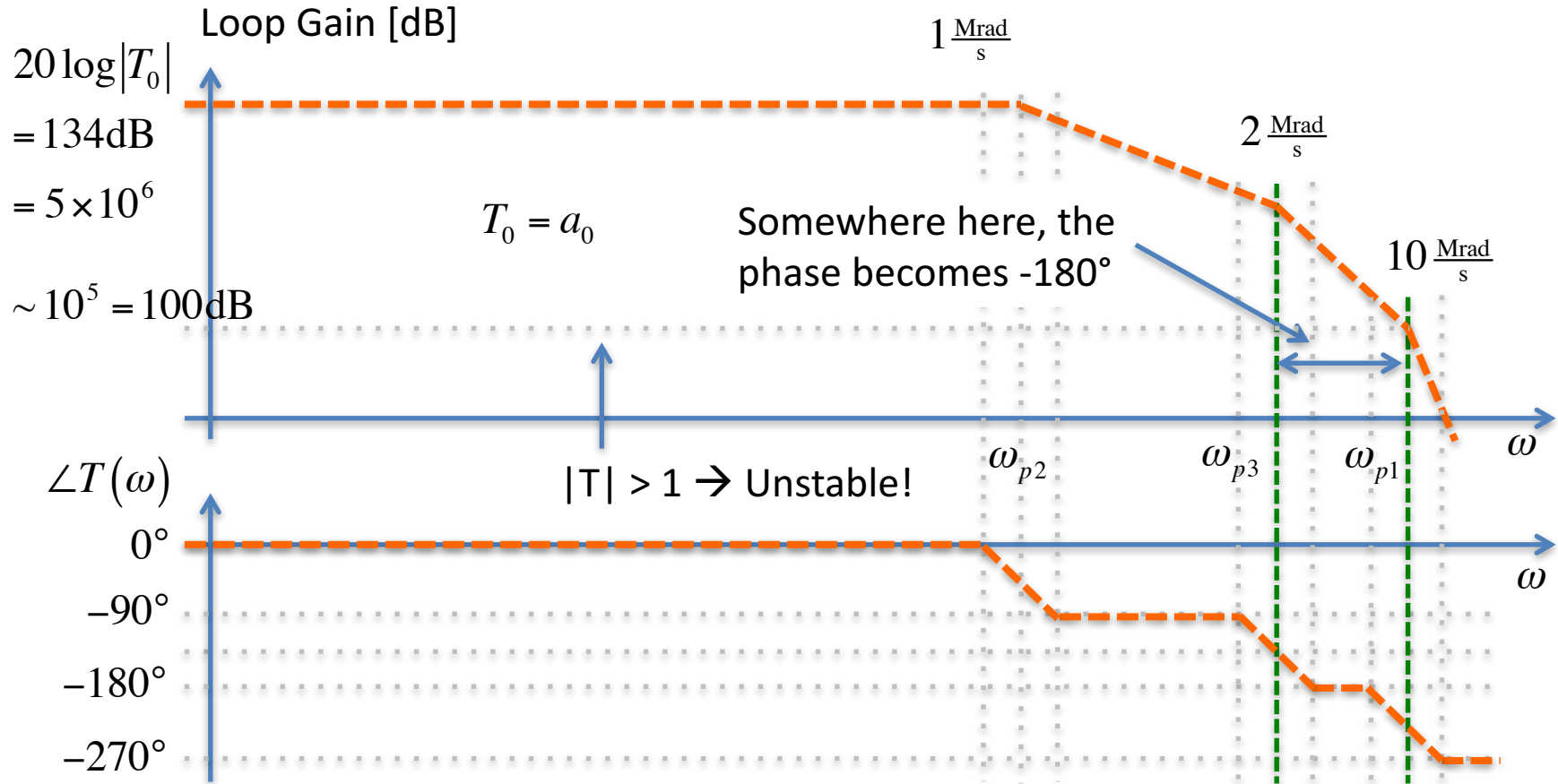
$$\omega_{p2} = \frac{1}{R_{o,diff} C_{GS}} = 1 \frac{\text{Mrad}}{\text{s}}$$

$$\omega_{p3} = \frac{1}{R_L C_D} = 2 \frac{\text{Mrad}}{\text{s}}$$

$$\omega_z = \frac{g_m}{C_{GD}} \rightarrow \infty$$

$$a(\omega) = \frac{10^3 \cdot (10^{-3} \cdot 5 \times 10^6) \cdot 1}{\left(1 + j \frac{\omega}{10 \times 10^6}\right) \left(1 + j \frac{\omega}{1 \times 10^6}\right) \left(1 + j \frac{\omega}{2 \times 10^6}\right) \left(1 + j \frac{\omega}{100 \times 10^6}\right)}$$

Before Compensation (use $f = 1$):



Compensate for $f = 1$ and $PM = 45^\circ$

We want:

$$\omega_{p2} = \frac{\omega_{p1}}{T_0} = \frac{10 \times 10^6}{5 \times 10^6} = 2 \frac{\text{rad}}{\text{s}}$$

For $C_C \gg C_{GS}, C_D$ and C_{GD}

$$\omega_{p2} = \frac{1}{R_{o,diff} (1 + g_m R_L) C_C}$$

$$\begin{aligned} C_C &= \frac{1}{R_{o,diff} (1 + g_m R_L) \omega_{p2}} = \frac{T_0}{R_{o,diff} (1 + g_m R_L) \omega_{p1}} \\ &= \frac{1}{10 \times 10^6 \cdot (5 \times 10^3) \cdot 2} = 10 \text{pF} \end{aligned}$$

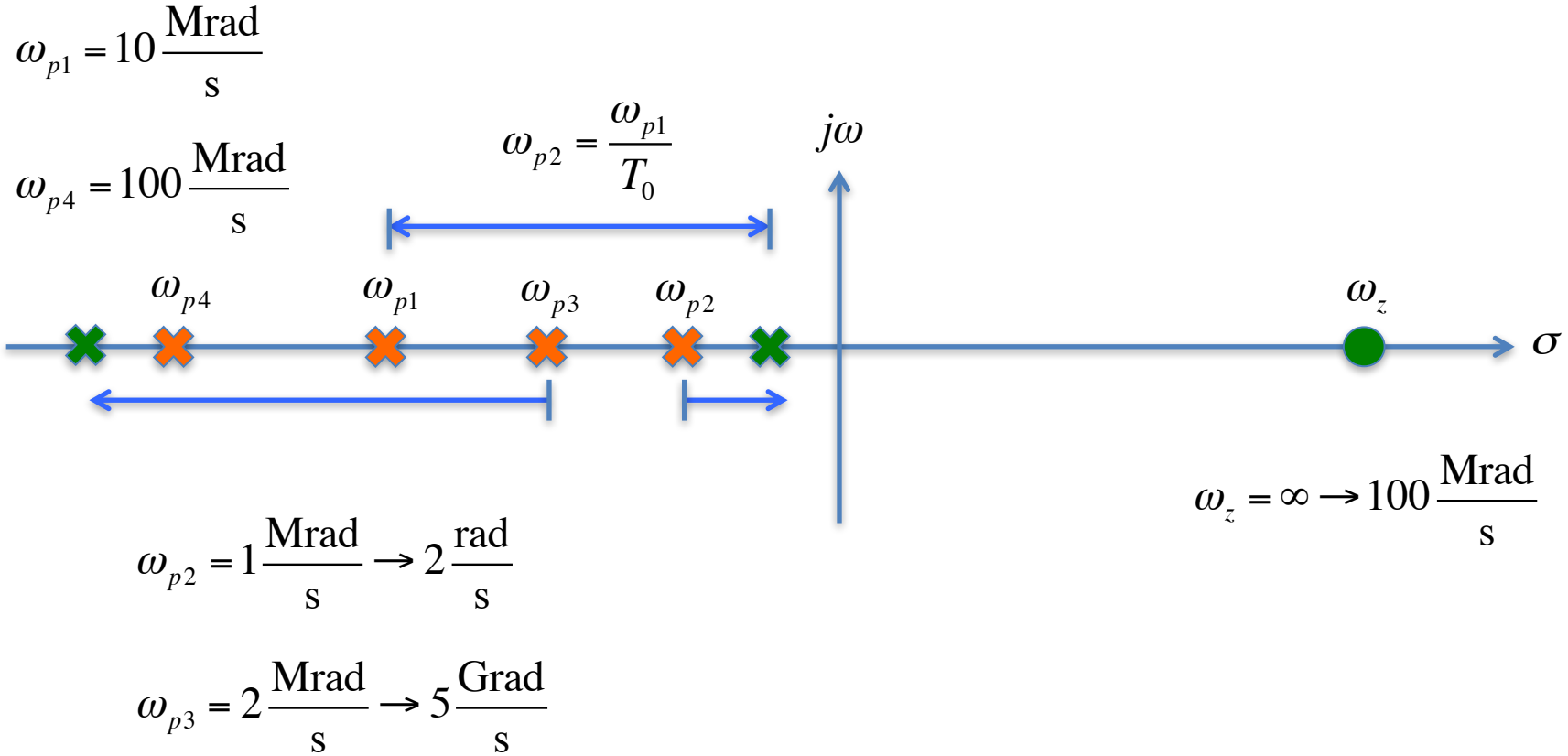
Thus,

$$\begin{aligned} \omega_{p3} &= \frac{g_m}{C_{GS} + C_D} = \frac{10^{-3}}{0.2 \times 10^{-12}} \\ &= 5 \frac{\text{Grad}}{\text{s}} \end{aligned}$$

$$\omega_z = \frac{g_m}{C_C} = \frac{10^{-3}}{10 \times 10^{-12}} = 100 \frac{\text{Mrad}}{\text{s}}$$



Compensate for $f = 1$ and $PM = 45^\circ$



Next Meeting

- Feedback Amplifier Step Response
- Introduction to Oscillators

