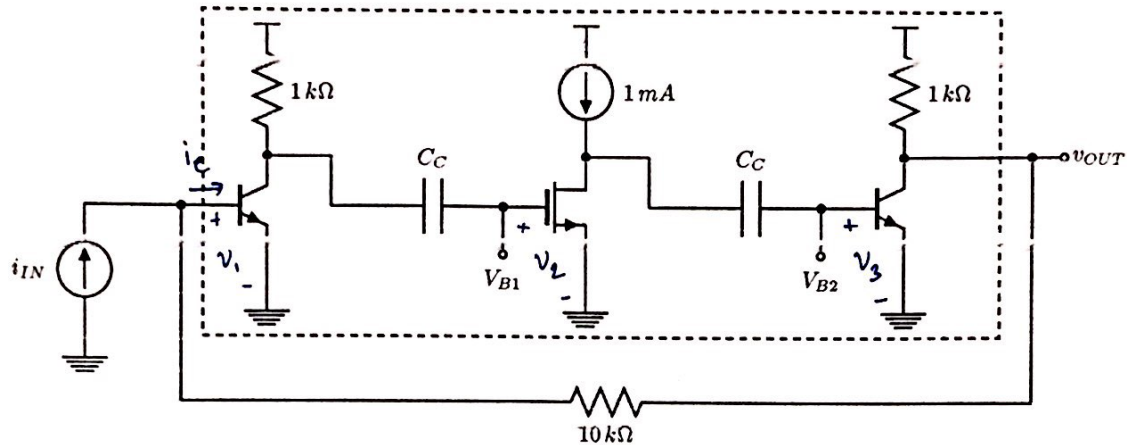


ANSWER KEY

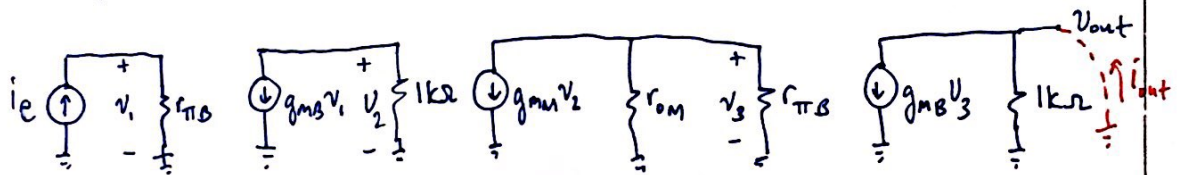
Part I:

(20 points) The cascaded amplifier circuit in the figure below, shown inside the dashed box, is connected in a feedback amplifier employing **shunt-shunt** feedback. The BJT parameters are as follows: $g_m = 1 \text{ mS}$, $\beta = 200$, and $V_A \rightarrow \infty$. The MOSFET parameters are as follows: $k = 1 \frac{\text{mA}}{\text{V}^2}$ and $\lambda = \frac{1}{50} \text{ V}^{-1}$. Note that the coupling capacitors, C_C , are very large and that the voltages, V_{B1} and V_{B2} , are purely DC voltages.



1. Draw the Norton two-port network representation of the cascaded amplifier. Label all components with their calculated values. (5 points)

BJT: $g_{mB} = 1 \text{ mS}$, $r_{\pi B} = \frac{\beta}{g_m} = 200 \text{ k}\Omega$, $r_{oB} \rightarrow \infty$ (since $V_A \rightarrow \infty$)
 MOSFET: $g_{mM} = \sqrt{4kI_D} = 2 \text{ mS}$, $r_{oM} = \frac{1}{\lambda I_D} = 50 \text{ k}\Omega$



$$R_{in} = \frac{v_1}{i_{in}} \Big|_{v_{out}=0} = r_{\pi B} = 200 \text{ k}\Omega$$

$$R_{out} = \frac{v_{out}}{i_{out}} \Big|_{i_e=0} = 1 \text{ k}\Omega$$

$$G_m = \frac{i_{out}}{v_1} \Big|_{v_{out}=0}$$

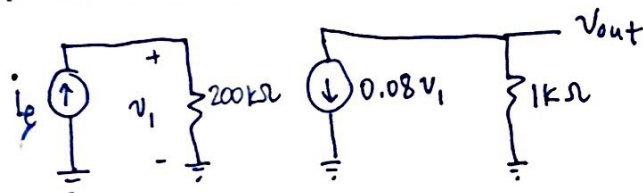
$$i_{out} = g_{mB} v_3 = g_{mB} (-g_{mM} v_2 (r_{oM} \parallel r_{\pi B}))$$

$$= g_{mB} [-g_{mM} (-g_{mB} v_1 (1 \text{ k}\Omega) (r_{oM} \parallel r_{\pi B}))]$$

$$G_m = g_{mB}^2 g_{mM} (1 \text{ k}\Omega) (r_{oM} \parallel r_{\pi B})$$

$$= 80 \text{ mS}$$

Equivalent 2-Port Circuit:



2. Draw the **Norton** two-port network representation of the feedback network. Label all components with their calculated values. (3 points)

$$R_{if} = \frac{v_e}{i_e} \Big|_{v_{fb}=0} = 10k\Omega$$

$$R_{of} = \frac{v_{fb}}{i_{fb}} \Big|_{v_e=0} = 10k\Omega$$

$$f = \frac{i_{fb}}{v_{out}} \Big|_{v_{fb}=0} = \frac{-1}{10k\Omega} = -100\mu S$$

Equivalent 2-Port Circuit:

3. Calculate the open-loop gain of the cascaded amplifier with loading of the feedback network. (4 points)

from #1 + loading effects of fb circuit:

$$a_R = \frac{v_{out}}{i_{e'}} \Big|_{i_{out}=0}$$

$$v_{out} = -0.08 v_1 (1k\Omega // 10k\Omega)$$

$$= -0.08 (i_{e'}) (10k\Omega // 200k\Omega) (1k\Omega // 10k\Omega)$$

$$\frac{v_{out}}{i_{e'}} = -692.64 k\Omega$$

loaded open-loop amplifier gain =
 $-692.64 k\Omega$

4. Calculate the closed-loop gain of the feedback amplifier. (2 points)

$$T = a_R \cdot f = 69.264$$

$$A_R = \frac{v_{out}}{i_{in}} = \frac{a_R}{1+T} = -9858 \Omega$$

$$\text{closed-loop amplifier gain} = -9858 \Omega$$

5. Calculate the closed-loop output resistance of the amplifier, $R_{o,CL}$. (2 points)

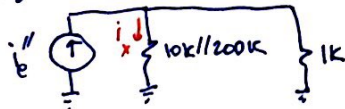
$$\text{from \#3, } R_o \text{ with loading} = 1k\Omega // 10k\Omega = 909 \Omega$$

$$\text{since topology is shunt-shunt, } R_{o,CL} = \frac{R_{o,loaded}}{1+T} = 12.94 \Omega$$

$$R_{o,CL} = 12.94 \Omega$$

6. If the input current source has a source resistance of $1k\Omega$ in parallel with to it, what would be the new closed-loop output resistance of the circuit? (4 points)

from #3:



$$R_{o,CL(new)} = \frac{R_{o,loaded}}{1+T_{new}} = 119.91 \Omega$$

$$R_{o,CL(new)} \approx 120 \Omega$$

$$a_R^{old} = \frac{v_o}{i_x} = -692.64 k\Omega$$

$$a_R^{new} = \frac{v_o}{i_x} \cdot \frac{i_x}{i_e''}$$

$$\text{from current division, } i_x = \frac{1k}{1k + (10k // 200k)} i_e''$$

$$\frac{i_x}{i_e''} = 0.095$$

$$\therefore a_R^{new} = -65.82 k\Omega$$

$$T_{new} = a_R^{new} \cdot f = 6.582$$