



EEE 51: Second Semester 2017 - 2018

Lecture 15

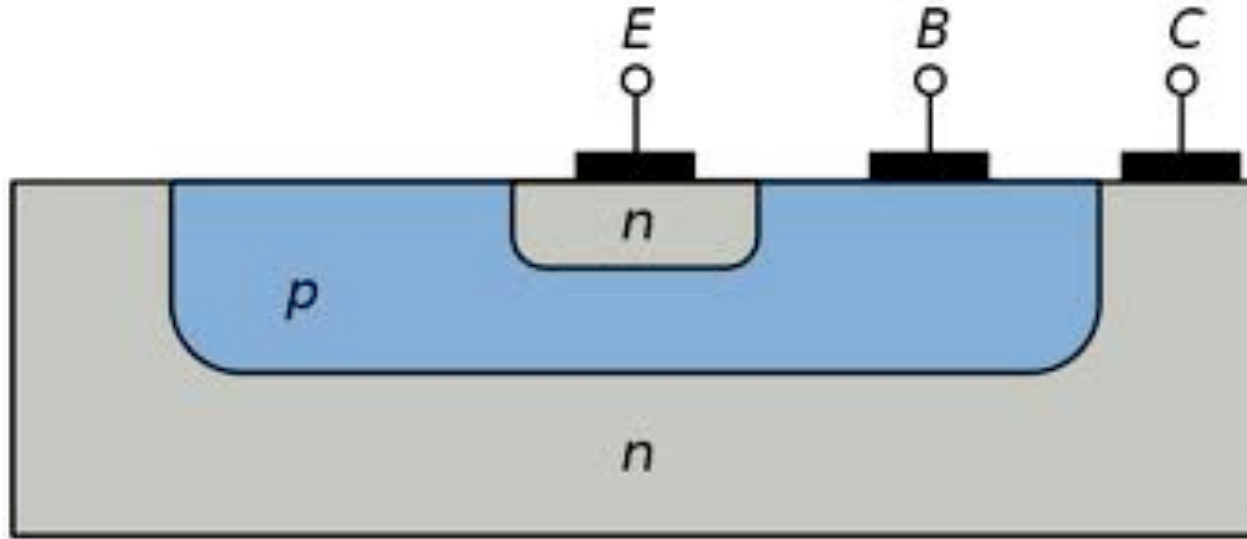
Frequency Response

Frequency Characteristics of Transistor Circuits

- Due to frequency-dependent impedances
 - Capacitors, inductors
- BJT Parasitic Capacitances
 - Junction capacitances
 - Nonlinear (voltage dependent)
 - Base-Charging capacitance (C_b)
 - Base-Emitter junction capacitance (C_{je})
 - Base-Collector junction capacitance (C_{μ})



BJT Capacitances

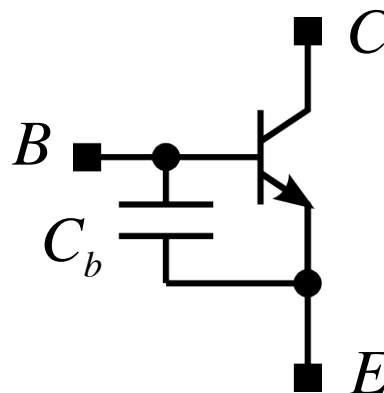


[http://commons.wikimedia.org/wiki/File:Npn_bjt_cross_section.svg]

BJT Base-Charging Capacitance

- Capacitance due to the change in majority carrier charge inside the base of the BJT
 - Cancels out the change in minority carriers in the base due to v_{BE}
 - ~ 100 's of fF

$$C_b = \tau_F g_m$$



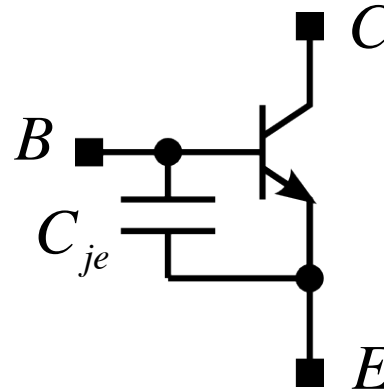
- τ_F – forward base transit time
 - Represents the average time (per carrier) spent crossing the base

BJT Base-Emitter Junction Capacitance

- PN junction capacitance ~ 10 's of fF
- In a BJT in the forward active region, BE junction is forward-biased

$$C_{je} = \frac{C_{je0}}{\sqrt{1 - \frac{V_{BE}}{V_{j,BE}}}}$$

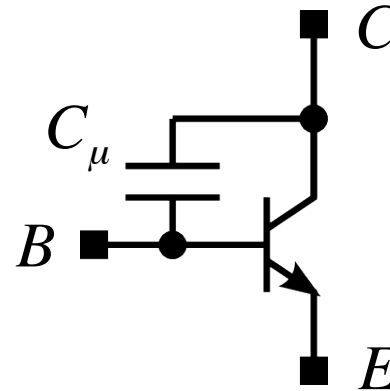
$$C_{je} \approx 2C_{je0}$$



BJT Base-Collector Junction Capacitance

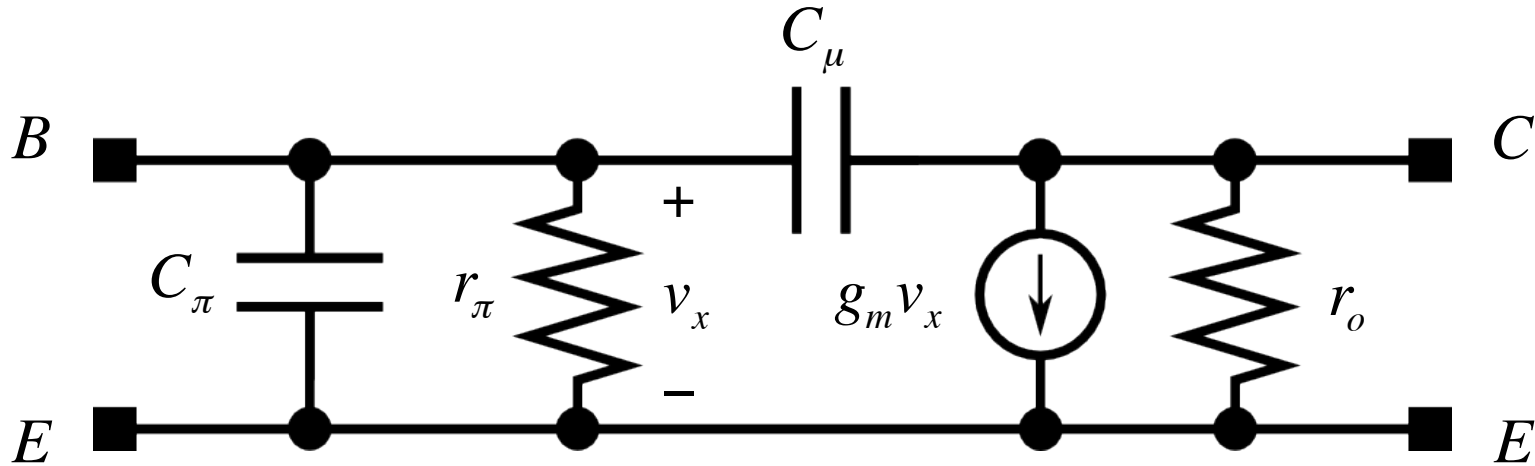
- PN junction capacitance 5 to 10 fF
- Reversed-biased in forward active BJTs

$$C_{\mu} = \frac{C_{\mu 0}}{\sqrt{1 + \frac{V_{CB}}{V_{j,CB}}}}$$



Can be amplified by the Miller effect

BJT Small Signal Model (with Capacitances)



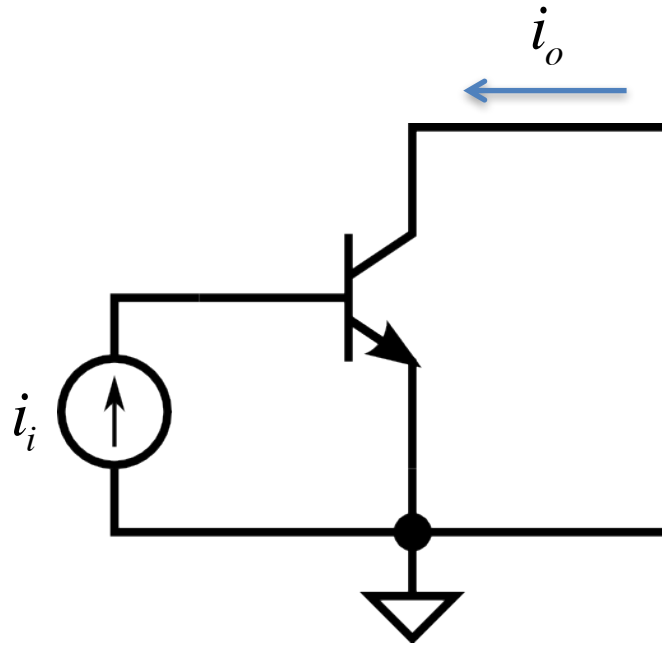
$$C_\pi = C_b + C_{je}$$
$$C_b = \tau_F g_m$$
$$C_{je} = \frac{C_{je0}}{\sqrt{1 - \frac{V_{BE}}{V_{j,BE}}}}$$

$$C_\mu = \frac{C_{\mu0}}{\sqrt{1 + \frac{V_{CB}}{V_{j,CB}}}}$$



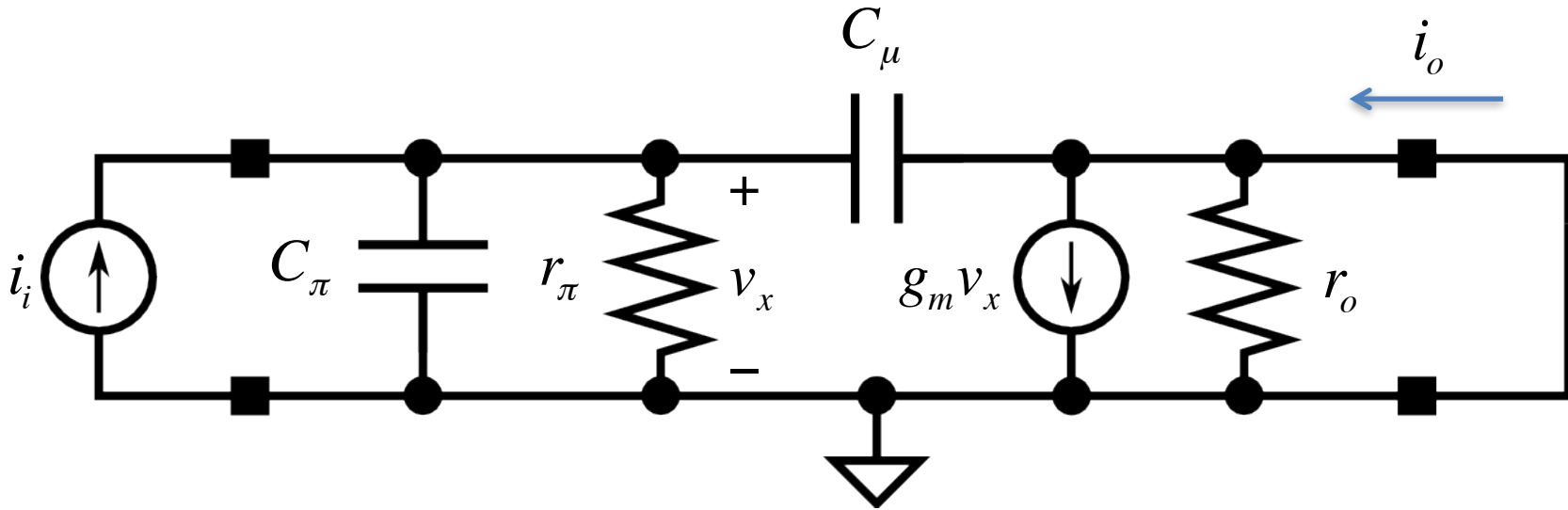
BJT Transition Frequency (f_T)

- Frequency at which the short-circuit common emitter current gain falls to unity



BJT f_T

- Small signal model



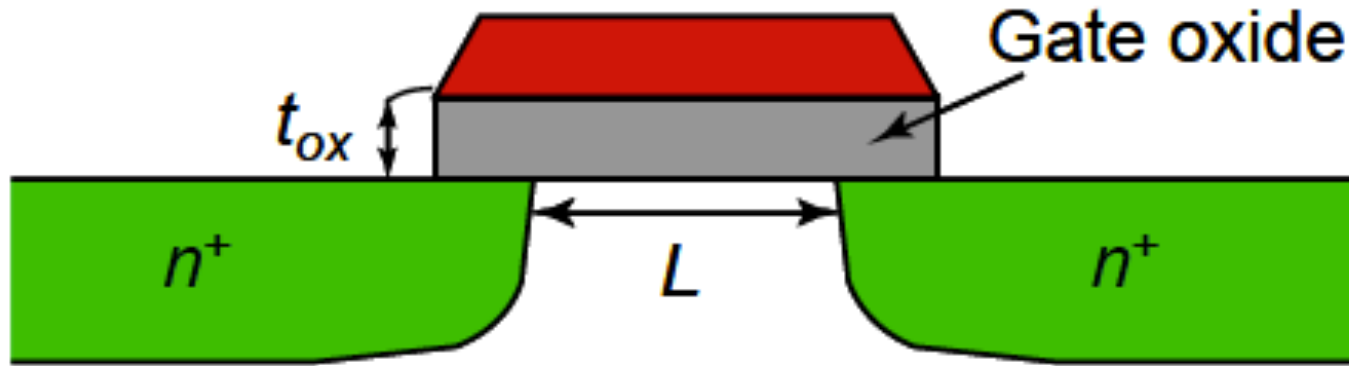
$$\frac{i_o}{i_i} = 1 \Rightarrow \omega_T \approx \frac{g_m}{C_\mu + C_\pi} = 2\pi f_T$$

MOS Capacitances

- MOS parasitic capacitances
 - Nonlinear
- Gate oxide capacitance (“parallel plate”)
- Gate overlap capacitance (fringe)
- Drain/Source-Bulk junction capacitance (PN junction)



MOS Capacitances



Cross section

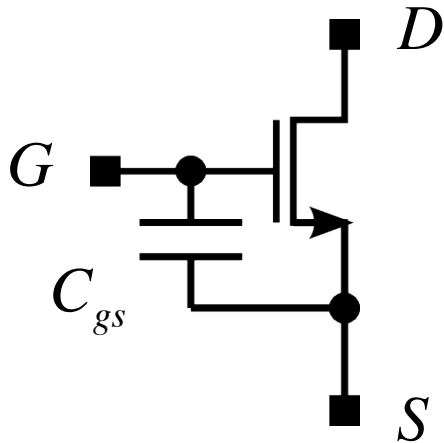
MOS Capacitances

- Gate Capacitance
 - Dependent on the thickness of the gate oxide and area of the gate
 - Nonlinear
 - Dependent on the gate and source/drain voltages
- Gate Overlap Capacitance
 - “parallel-plate” and fringing fields



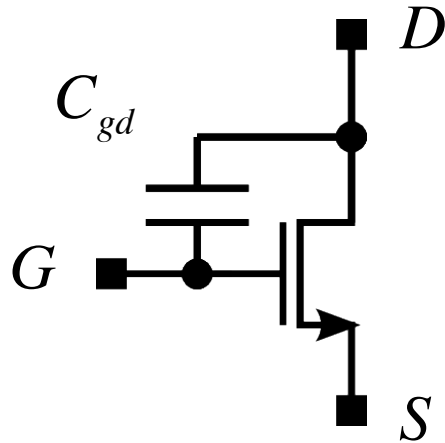
MOS Gate-Source Capacitance

- Components:
 - gate “parallel plate” capacitance
 - Gate-source overlap capacitance



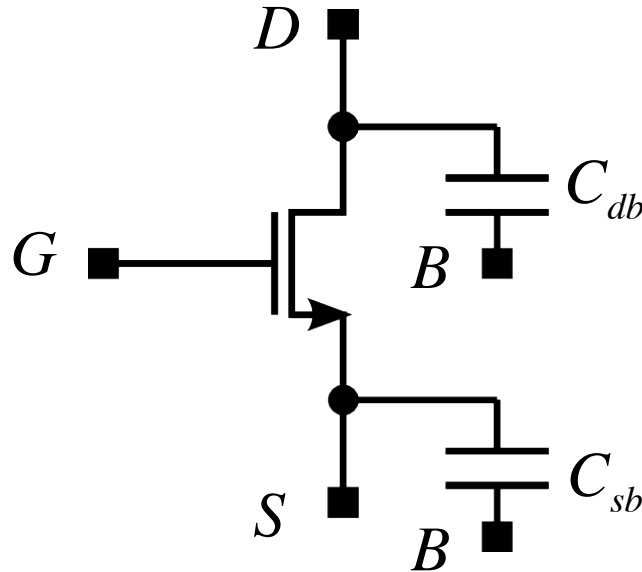
MOS Gate-Drain Capacitance

- Composed of the overlap capacitance between the gate and drain



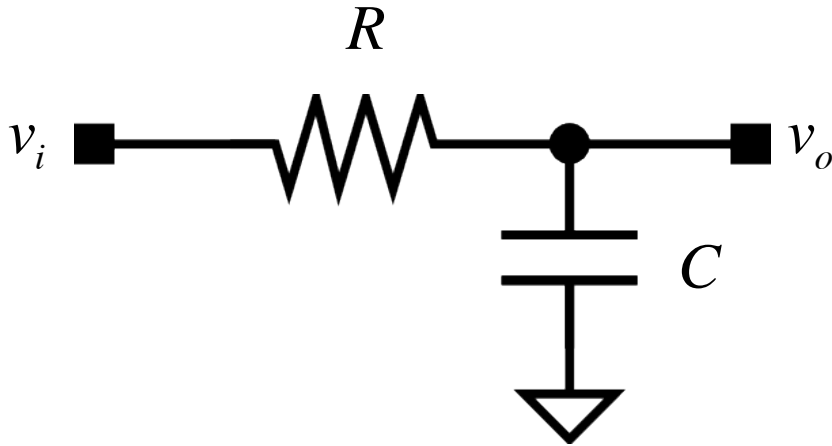
MOS Source/Drain Junction Capacitance

- Formed by the drain/source PN junction (to the substrate)
- Normally reversed biased



Capacitance Effects

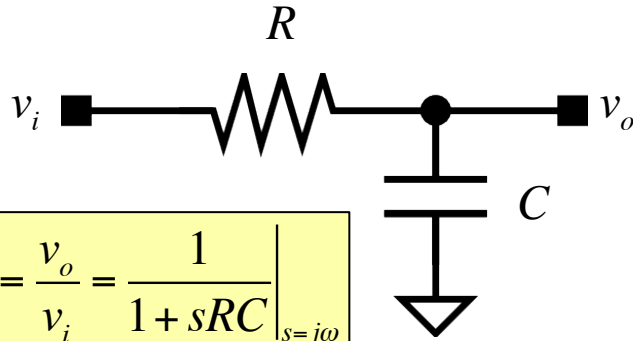
- A Simple RC Circuit



$$v_o = \frac{\frac{1}{sC}}{\frac{1}{sC} + R} v_i = \frac{1}{1 + sRC} v_i$$

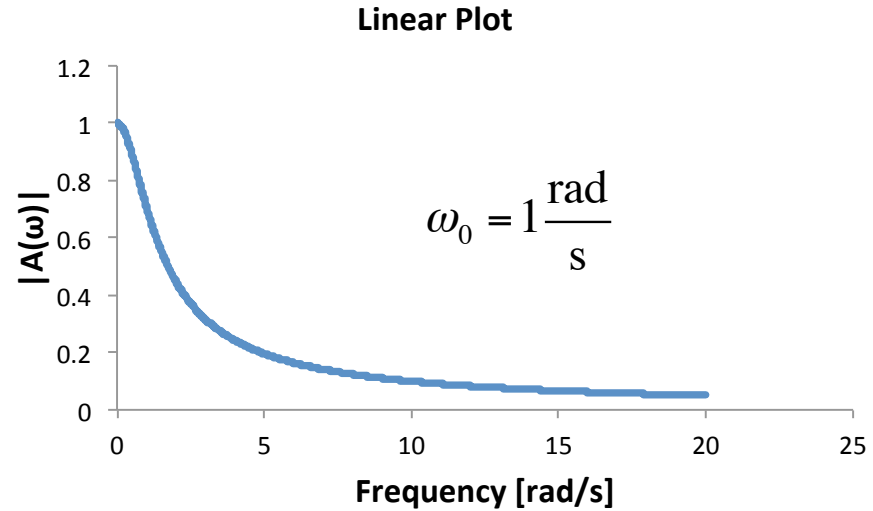
$$A_v(\omega) = \frac{v_o}{v_i} = \frac{1}{1 + sRC} \Big|_{s=j\omega}$$

Frequency Response

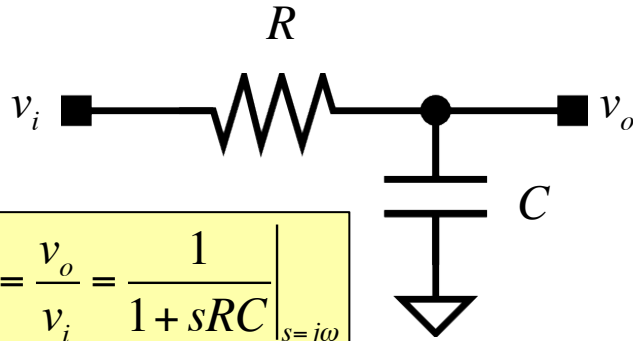


$$A_v(\omega) = \frac{v_o}{v_i} = \frac{1}{1 + sRC} \Big|_{s=j\omega}$$

$$\begin{aligned} |A_v(\omega)| &= \frac{1}{\sqrt{1 + \omega^2 R^2 C^2}} \\ &= \frac{1}{\sqrt{1 + \left(\frac{\omega}{\omega_0}\right)^2}} \end{aligned}$$

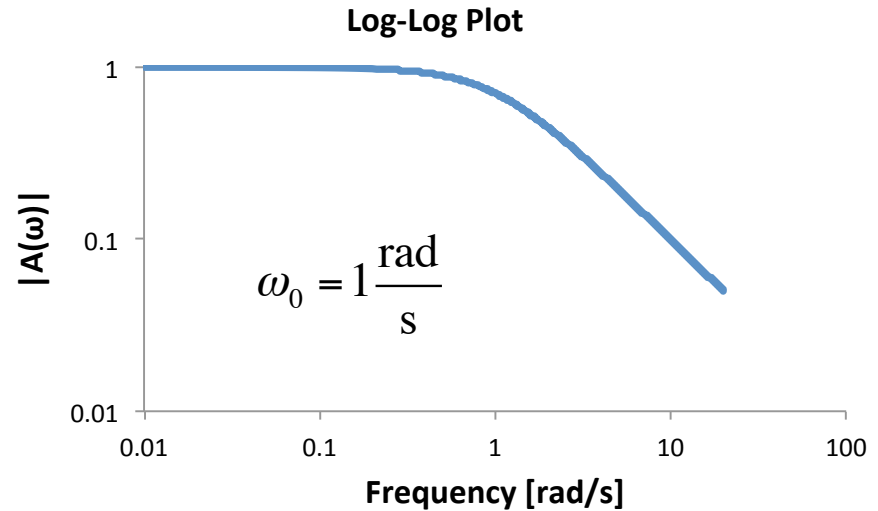


Frequency Response



$$A_v(\omega) = \frac{v_o}{v_i} = \frac{1}{1 + sRC} \Big|_{s=j\omega}$$

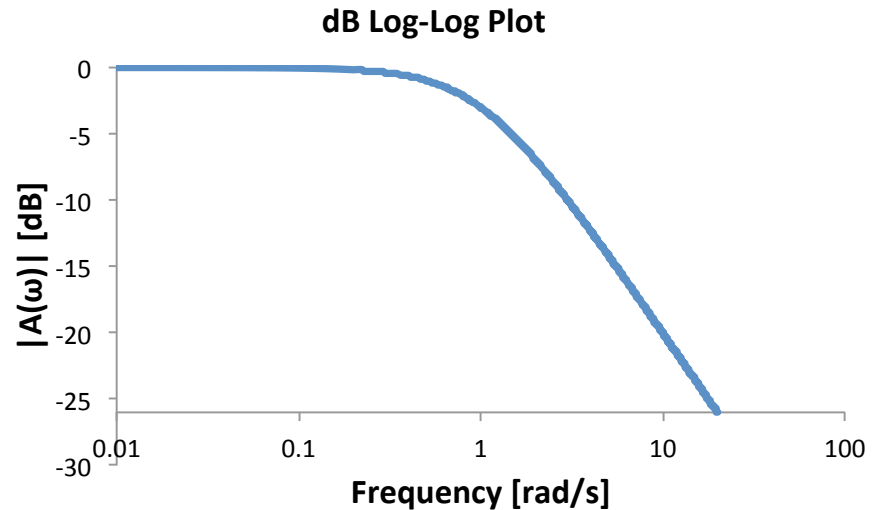
$$\begin{aligned} |A_v(\omega)| &= \frac{1}{\sqrt{1 + \omega^2 R^2 C^2}} \\ &= \frac{1}{\sqrt{1 + \left(\frac{\omega}{\omega_0}\right)^2}} \end{aligned}$$



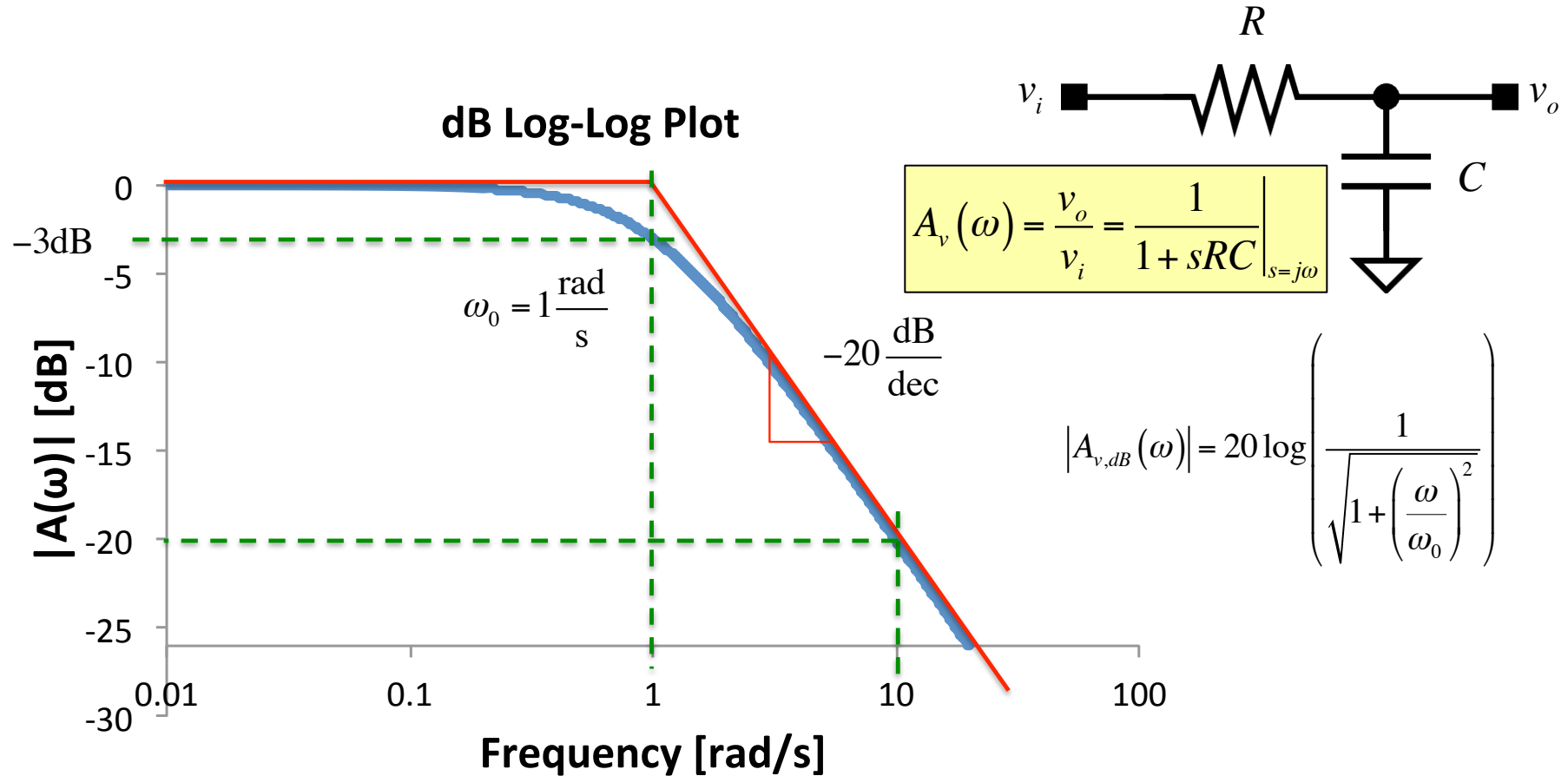
Decibels (dB)

- Voltage gain:

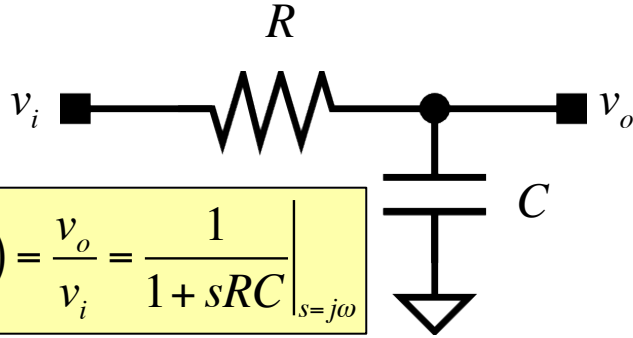
$$\begin{aligned} |A_{v,dB}(\omega)| &= 20 \log \left(\left| \frac{v_o}{v_i} \right| \right) \\ &= 20 \log \left(\frac{1}{\sqrt{1 + \left(\frac{\omega}{\omega_0} \right)^2}} \right) \end{aligned}$$



Frequency Response: Magnitude

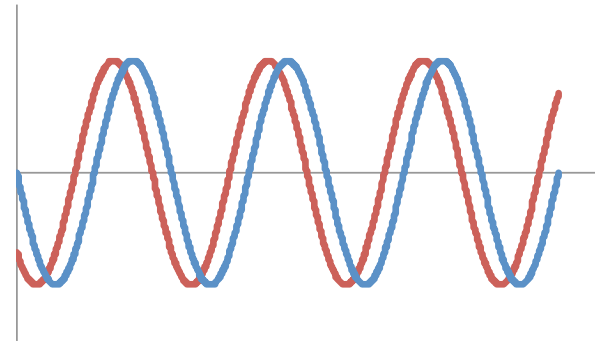
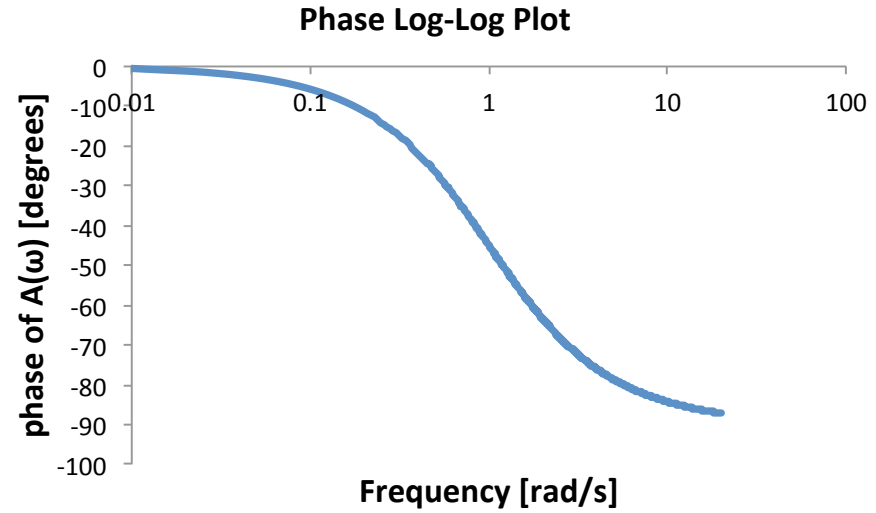


Phase Response

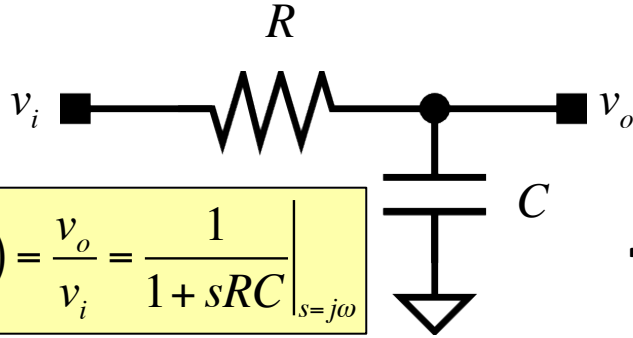


$$A_v(\omega) = \frac{v_o}{v_i} = \frac{1}{1 + sRC} \Big|_{s=j\omega}$$

$$\begin{aligned} \angle A_v(\omega) &= \tan^{-1} \left(\frac{\text{Im}[A(\omega)]}{\text{Re}[A(\omega)]} \right) \\ &= \tan^{-1} \left(\frac{0}{1} \right) - \tan^{-1} \left(\frac{\omega RC}{1} \right) \\ &= -\tan^{-1}(\omega RC) = -\tan^{-1} \left(\frac{\omega}{\omega_0} \right) \end{aligned}$$

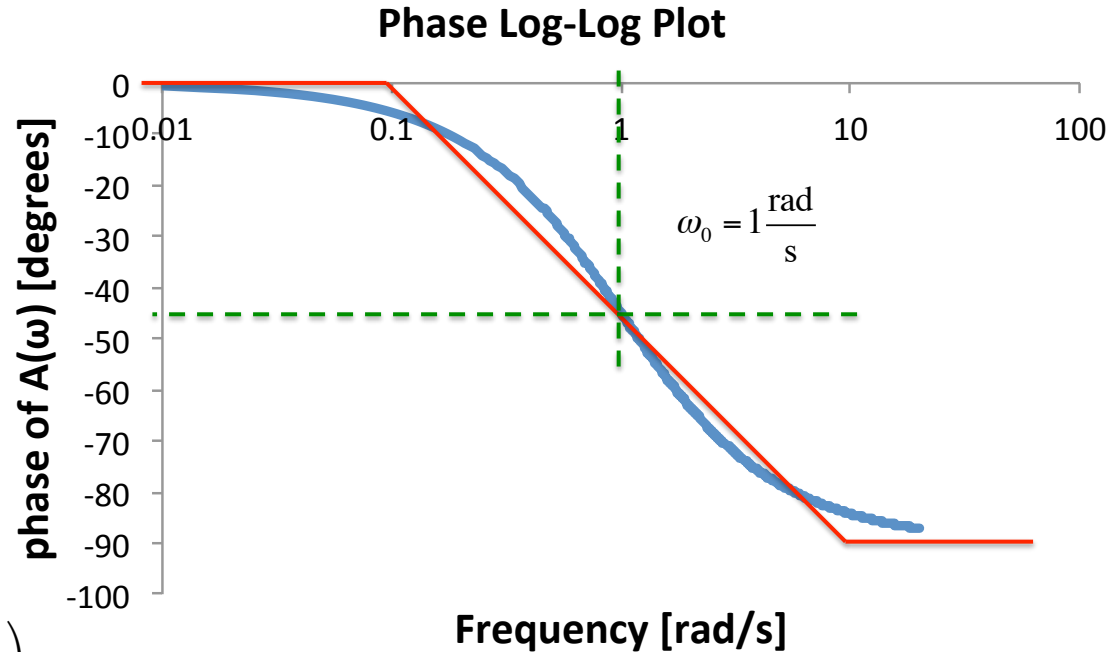


Phase Response

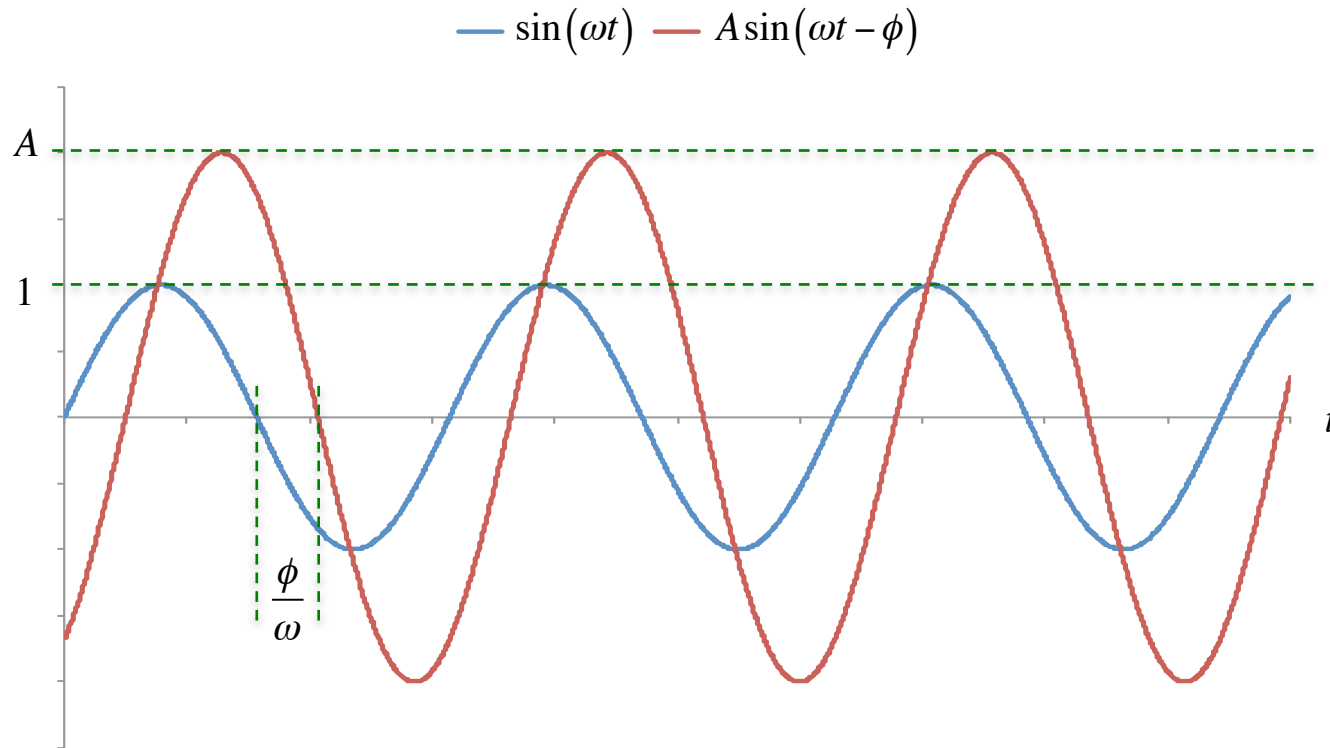


$$A_v(\omega) = \frac{v_o}{v_i} = \frac{1}{1 + sRC} \Big|_{s=j\omega}$$

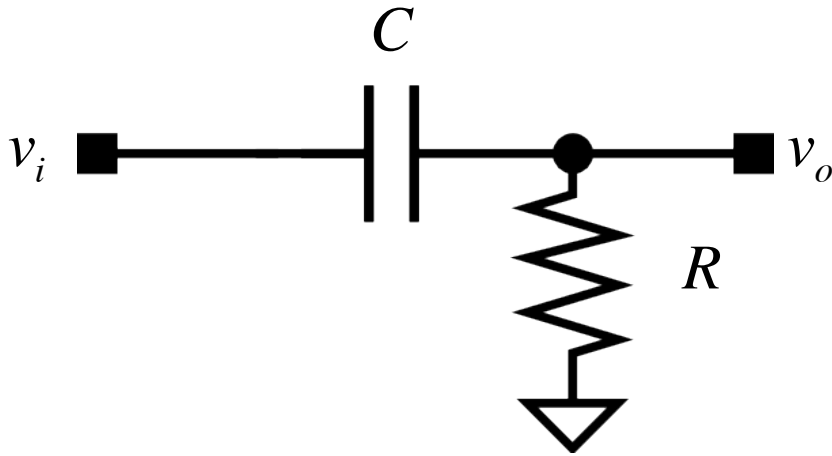
$$\begin{aligned} \angle A_v(\omega) &= \tan^{-1} \left(\frac{\text{Im}[A(\omega)]}{\text{Re}[A(\omega)]} \right) \\ &= \tan^{-1} \left(\frac{0}{1} \right) - \tan^{-1} \left(\frac{\omega RC}{1} \right) \\ &= -\tan^{-1}(\omega RC) = -\tan^{-1} \left(\frac{\omega}{\omega_0} \right) \end{aligned}$$



Magnitude and Phase



Another RC Example

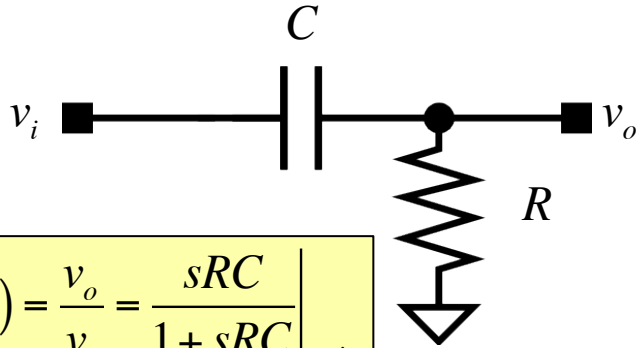


$$v_o = \frac{R}{\frac{1}{sC} + R} v_i = \frac{sRC}{1 + sRC} v_i$$

$$A_v(\omega) = \frac{v_o}{v_i} = \frac{sRC}{1 + sRC} \Big|_{s=j\omega}$$

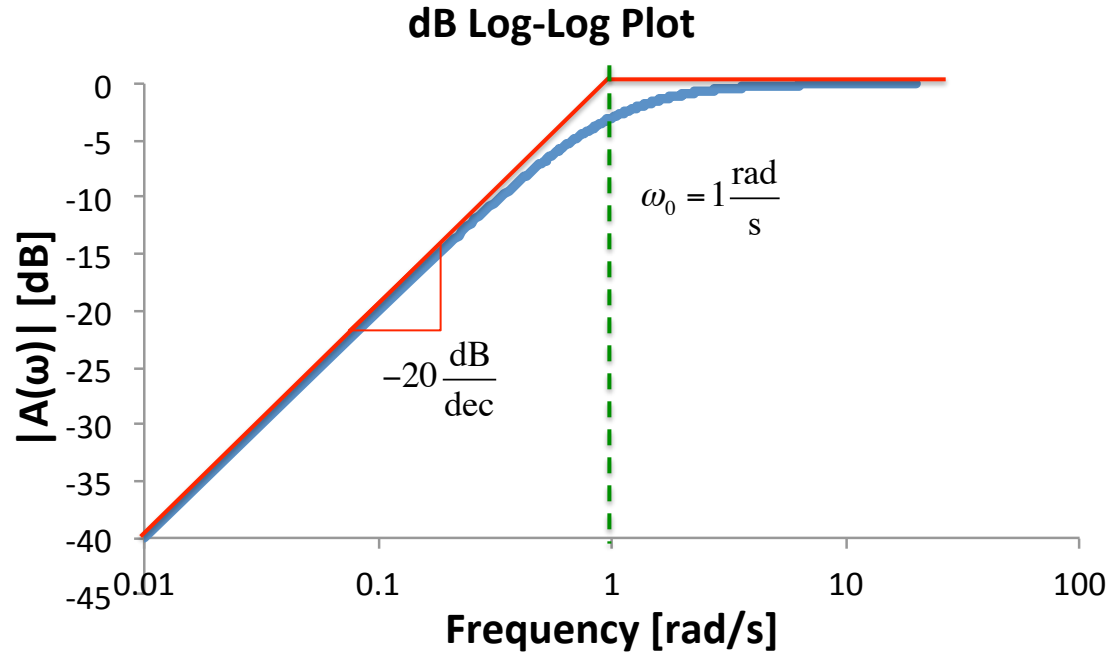


Frequency Response: Magnitude Response

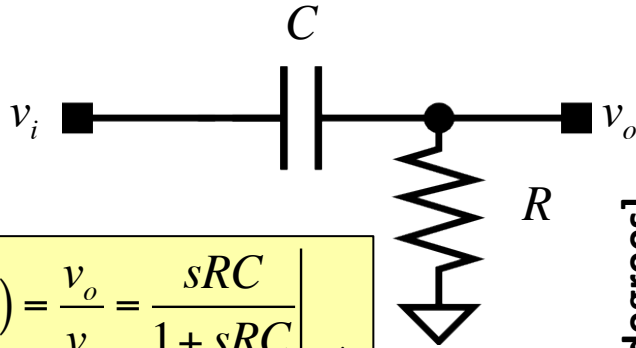


$$A_v(\omega) = \frac{v_o}{v_i} = \frac{sRC}{1 + sRC} \Big|_{s=j\omega}$$

$$\begin{aligned} |A_v(\omega)| &= \frac{\omega RC}{\sqrt{1 + \omega^2 R^2 C^2}} \\ &= \frac{\omega}{\omega_0} \\ &= \frac{\omega}{\sqrt{1 + \left(\frac{\omega}{\omega_0}\right)^2}} \end{aligned}$$

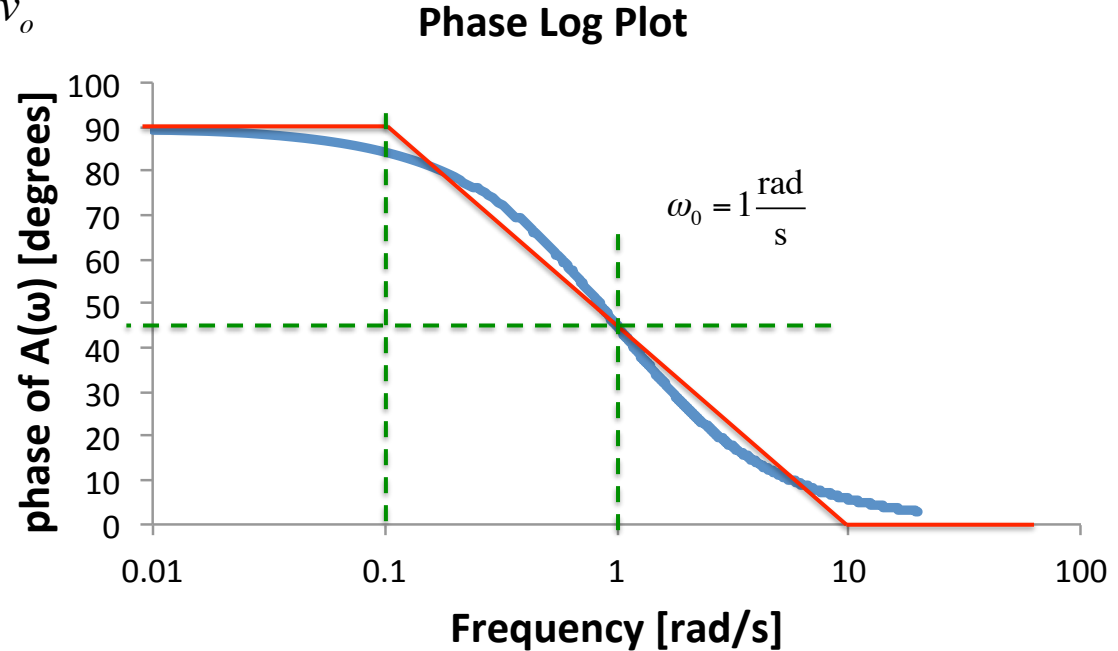


Phase Response



$$A_v(\omega) = \frac{v_o}{v_i} = \frac{sRC}{1 + sRC} \bigg|_{s=j\omega}$$

$$\begin{aligned} \angle A_v(\omega) &= \tan^{-1} \left(\frac{\text{Im}[A(\omega)]}{\text{Re}[A(\omega)]} \right) \\ &= \tan^{-1} \left(\frac{1}{0} \right) - \tan^{-1} \left(\frac{\omega RC}{1} \right) \\ &= 90^\circ - \tan^{-1}(\omega RC) = 90^\circ - \tan^{-1} \left(\frac{\omega}{\omega_0} \right) \end{aligned}$$



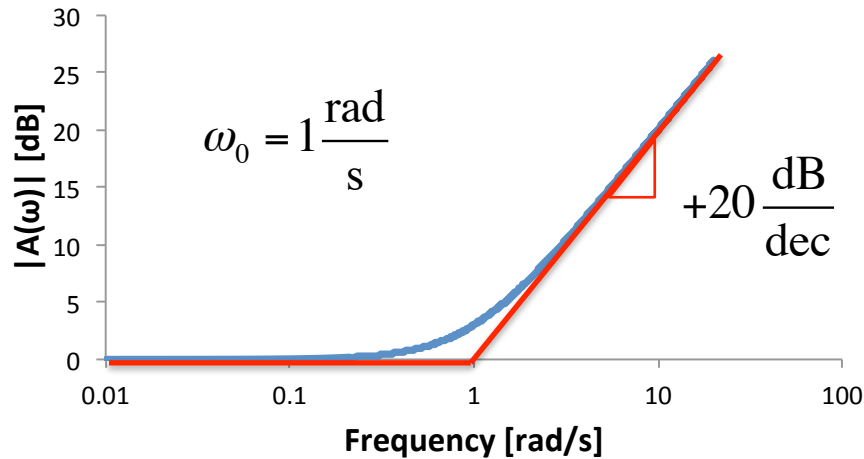
A General Zero Term

$$A(\omega) = 1 + j \frac{\omega}{\omega_0}$$

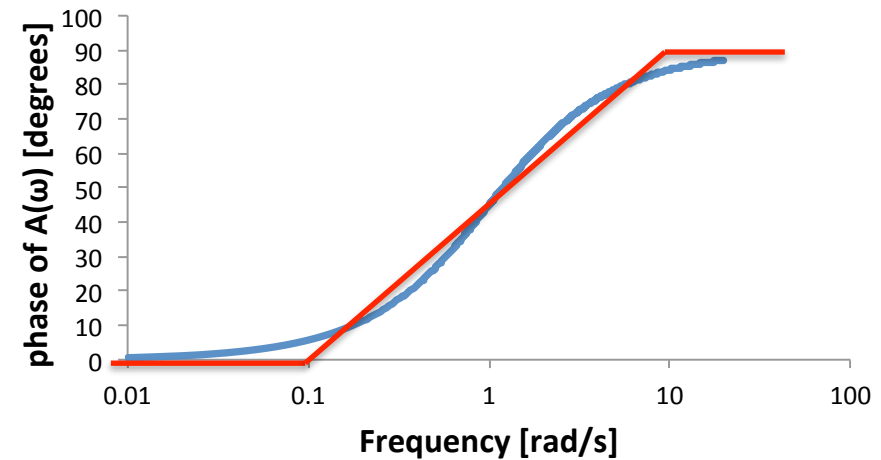
$$20 \log [|A(\omega)|] = 20 \log \left[\sqrt{1 + \left(\frac{\omega}{\omega_0} \right)^2} \right]$$

$$\angle A(\omega) = \tan^{-1} \left(\frac{\omega}{\omega_0} \right)$$

dB Log-Log Plot



Phase Log Plot



Generalized Transfer Function

- Factor the numerator and denominator to get the poles and zeros of the system

$$A(s) = A_0 \frac{\left(1 + \frac{s}{z_1}\right) \left(1 + \frac{s}{z_2}\right) \cdots \left(1 + \frac{s}{z_N}\right)}{\left(1 + \frac{s}{p_1}\right) \left(1 + \frac{s}{p_2}\right) \cdots \left(1 + \frac{s}{p_D}\right)}$$

$$A(\omega) = A_0 \frac{\left(1 + j \frac{\omega}{\omega_{z_1}}\right) \left(1 + j \frac{\omega}{\omega_{z_2}}\right) \cdots \left(1 + j \frac{\omega}{\omega_{z_N}}\right)}{\left(1 + j \frac{\omega}{\omega_{p_1}}\right) \left(1 + j \frac{\omega}{\omega_{p_2}}\right) \cdots \left(1 + j \frac{\omega}{\omega_{p_D}}\right)}$$



Magnitude Response Using the dB Scale

$$\begin{aligned} |A_{dB}(\omega)| &= 20 \log \left[\left| A_0 \frac{\left(1 + j \frac{\omega}{\omega_{z_1}}\right) \left(1 + j \frac{\omega}{\omega_{z_2}}\right) \cdots \left(1 + j \frac{\omega}{\omega_{z_N}}\right)}{\left(1 + j \frac{\omega}{\omega_{p_1}}\right) \left(1 + j \frac{\omega}{\omega_{p_2}}\right) \cdots \left(1 + j \frac{\omega}{\omega_{p_D}}\right)} \right| \right] \\ &= 20 \log [|A_0|] + \sum_N 20 \log \left[\left| 1 + j \frac{\omega}{\omega_{z_i}} \right| \right] + \sum_D 20 \log \left[\left| \frac{1}{1 + j \frac{\omega}{\omega_{p_i}}} \right| \right] \end{aligned}$$



Phase Response

$$A(\omega) = A_0 \frac{\left(1 + j\frac{\omega}{\omega_{z_1}}\right)\left(1 + j\frac{\omega}{\omega_{z_2}}\right)\cdots\left(1 + j\frac{\omega}{\omega_{z_N}}\right)}{\left(1 + j\frac{\omega}{\omega_{p_1}}\right)\left(1 + j\frac{\omega}{\omega_{p_2}}\right)\cdots\left(1 + j\frac{\omega}{\omega_{p_D}}\right)}$$

$$\angle A(\omega) = \sum_N \angle \left(1 + j\frac{\omega}{\omega_{z_i}}\right) + \sum_D \angle \left(\frac{1}{1 + j\frac{\omega}{\omega_{p_i}}}\right)$$



Next Meeting

- Frequency Response of Amplifiers

