

SOEC/Electrolyzer Supplementary Model Details

Below details various parameters used in the electrolyzer model. Many parameters are the same as used in [1].

Table 1. Electrolyzer parameters.

| Description | Value |
|---|----------------------|
| Cell Length (m) | 0.225 |
| Cell Width (m) | 0.1 |
| Number of cells | 534,857 |
| Cathode flow channel height, h_C , (m) | 1×10^{-3} |
| Anode flow channel height, h_A , (m) | 1×10^{-3} |
| Interconnect height, h_I , (m) | 5×10^{-4} |
| Height electric conducting structure, h_S , (m) | 5.7×10^{-4} |
| Porous cathode thickness (m) | 5×10^{-4} |
| Porous anode thickness (m) | 2×10^{-5} |
| Electrolyte thickness (m) | 5×10^{-5} |
| Interconnect heat capacity, $C_{p,I}$, (J/kg-K) | 500 |
| Electric conducting structure heat capacity, $C_{p,S}$, (J/kg-K) | 500 |
| Density of electric conducting structure, ρ_S , (kg/m ³) | 5900 |
| Density of interconnect material, ρ_I , (kg/m ³) | 8000 |
| Electric conducting structure thermal conductivity, λ_S , (W/m-K) | 2 |
| Interconnect thermal conductivity, λ_I , (W/m-K) | 25 |
| Porous cathode electric conductivity, (1/ohm-m) | 8×10^4 |
| Porous anode electric conductivity, (1/ohm-m) | 8.4×10^3 |
| Electrolyte electric conductivity, (1/ohm-m) | 1.9 |
| Electric conducting structure emissivity ϵ_S , (unitless) | 0.8 |
| Interconnect emissivity, ϵ_I , (unitless) | 0.1 |

SOEC/Electrolyzer Control

The electrolyzer conversion is controlled based on a simple proportional-integral (PI) controller. The controller reads the measured H₂O conversion and compares it to the setpoint of 72.5% (which is the conversion for thermoneutral operation of the cell at design conditions found by trial and error) and then outputs an average current density, j_{avg} , to be applied to a single cell. The average current density then calculates the potential and conversion of the cell until the setpoint is reached.

SOEC/Electrolyzer Discretization

The SOEC cell energy and mass balances are PDEs which need to be discretized in space to form ODEs in time that MATLAB/Simulink can solve. The mass balances are discretized with a first order backward difference (looking upwind) for the first derivatives. The energy balance for the cathode and anode stream is also discretized with a first order upwind difference for the first derivatives. The interconnect material and the electric conducting structure include second

derivatives for space and they are discretized with a first order backward difference (looking upwind).

Parabolic Trough Collector Supplementary Model Details

Full detail with parameters and more information is supplied in [2].

References

- [1] J. S. Kim, R. D. Boardman, and S. M. Bragg-Sitton, "Dynamic performance analysis of a high-temperature steam electrolysis plant integrated within nuclear-renewable hybrid energy systems," *Appl. Energy*, vol. 228, no. July, pp. 2090–2110, 2018, doi: 10.1016/j.apenergy.2018.07.060.
- [2] J. Immonen and K. M. Powell, "Dynamic optimization with flexible heat integration of a solar parabolic trough collector plant with thermal energy storage used for industrial process heat," *Energy Convers. Manag.*, vol. 267, no. June, p. 115921, 2022, doi: 10.1016/j.enconman.2022.115921.