

MEMS1045

Automatic control

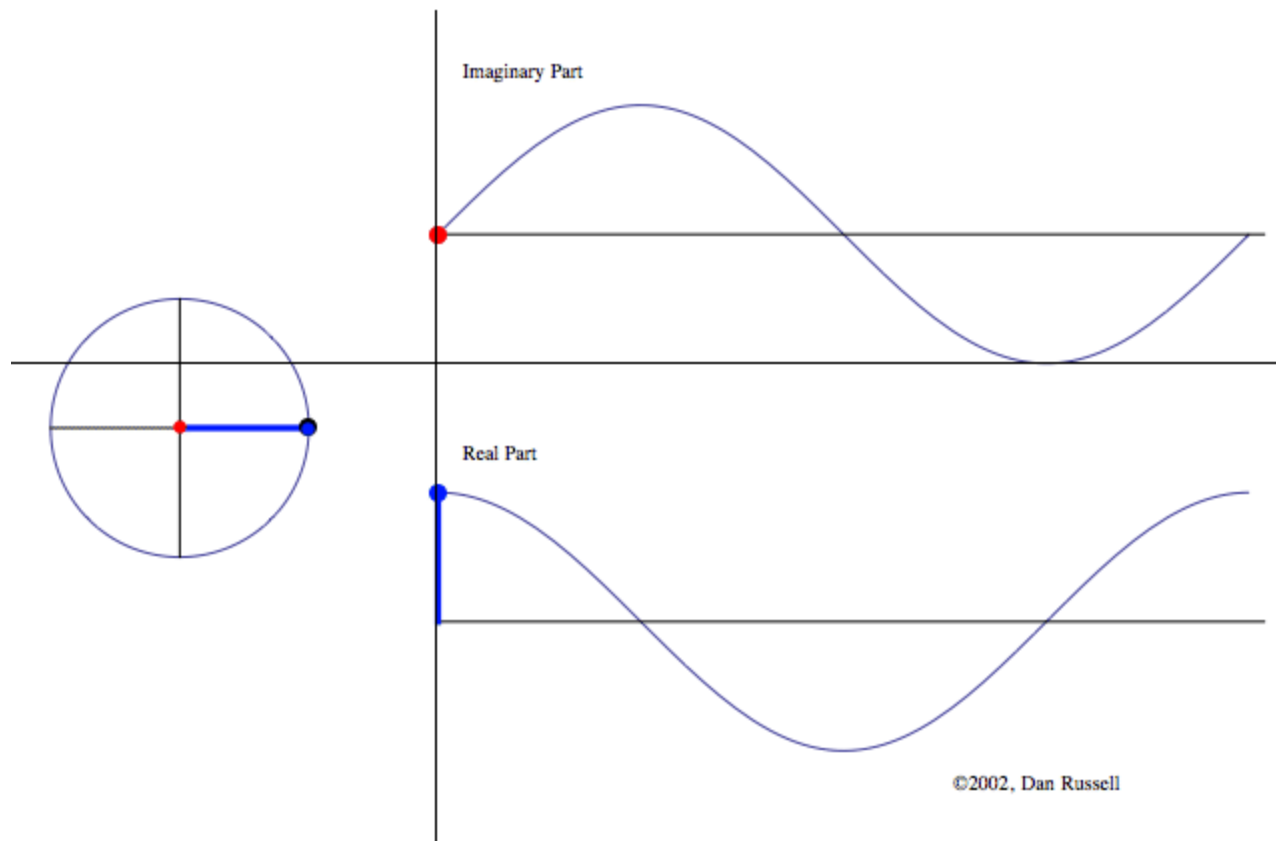
Lecture 11

Frequency response 1

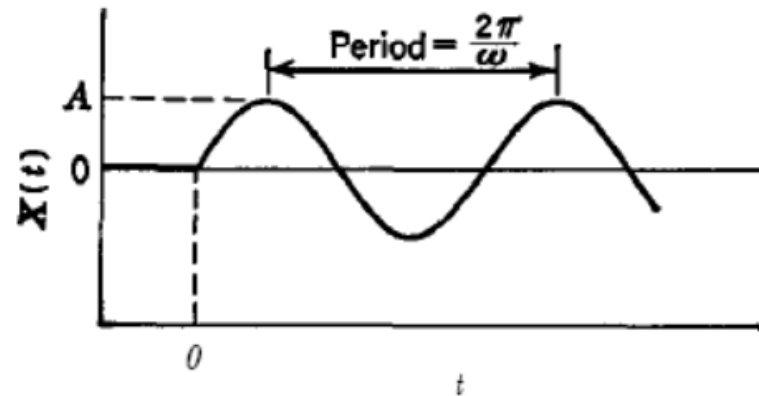
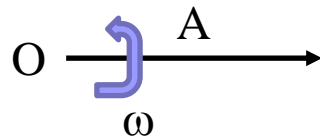
Objectives

- Explain the concept of frequency response
- Determine frequency response from transfer functions
- Represent the frequency response graphically using Bode diagrams
- Sketch the Bode diagrams from transfer functions
- Represent the frequency response graphically using Nichols chart and Nyquist diagram

Revision - trigonometry



Sinusoidal signal

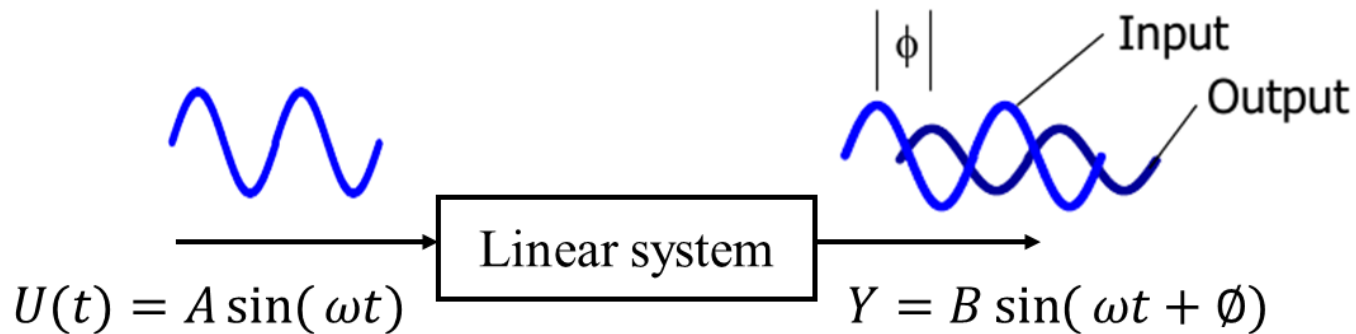


Consider the sinusoidal input:

- ❖ At $t < 0$: $x(t) = 0$;
- ❖ For $t \geq 0$: $x(t) = A \sin(\omega t)$
- ❖ Input frequency ω (rad/s) = $2\pi f$; where f = frequency in cycles/sec (Hz)
- ❖ Period $T = \frac{1}{f} = \left(\frac{2\pi}{\omega}\right)$ sec.
- ❖ Sinusoids can be represented as rotating phasors using complex numbers

$$Ae^{j\omega t} = |A|\angle$$

Frequency response



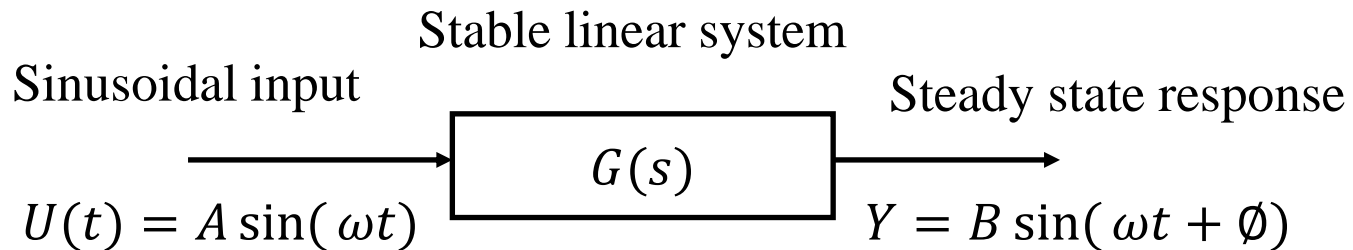
In the steady state, a sine input will generate a sine output

- ❖ Output signal will oscillate at the same frequency as input signal
- ❖ The magnitude of the output signal is different from the input signal
- ❖ The magnitude (or amplitude) ratio is defined as $M = \frac{B}{A}$
- ❖ There is a phase shift (or difference) ϕ between the input and output signals

Note:

- Only 2 parameters are needed to describe the frequency response: amplitude ratio M and phase difference ϕ
- Linear system can be represented using transfer functions

Frequency response



Given the transfer function, to determine the amplitude ratio and phase shift:

❖ Substitute $s = j\omega$ into the transfer function $G(s)$

Note: $s = j\omega$ is a complex variable with ω = input signal frequency

❖ The amplitude ratio is the magnitude of the complex function $G(j\omega)$, i.e.

$$M = |G(j\omega)|$$

❖ The phase shift is the phase angle of the complex function $G(j\omega)$, i.e.

$$\phi = \angle G(j\omega)$$

Note: for complex numbers $z_1 = a_1 + b_1j = M_1 e^{j\phi_1}$, $z_2 = a_2 + b_2j = M_2 e^{j\phi_2}$, ...

$$z = \frac{z_1 z_2}{z_3 z_4} = \frac{M_1 M_2}{M_3 M_4} e^{j(\phi_1 + \phi_2 - \phi_3 - \phi_4)} = |z| e^{j\phi}$$

Example 1

Find the steady state response for $y(t)$ for input $f(t) = 5\sin(0.2t)$ given the transfer function

$$G(s) = \frac{Y(s)}{F(s)} = \frac{20}{(10s + 1)(4s + 1)}$$

Note: input signal frequency is $\omega = 0.2$ and system is stable;

❖ Substitute $s = j\omega = 0.2j$ into the transfer function $G(s)$

$$G(j\omega) = \frac{Y(j\omega)}{F(j\omega)} = \frac{20}{(2j + 1)(0.8j + 1)}$$

$$|G(j\omega)| = \frac{|Y(j\omega)|}{|F(j\omega)|} = \frac{20}{(\sqrt{4 + 1})(\sqrt{0.64 + 1})} = 7$$

$$\angle G(j\omega) = 0 - \tan^{-1}(2/1) - \tan^{-1}(0.8) = -102.1^\circ \text{ or } -1.78 \text{ rad.}$$

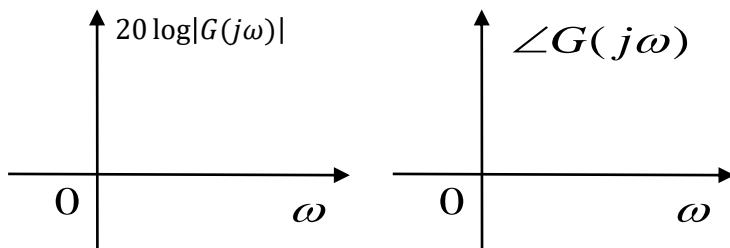
$$|Y(j\omega)| = 7|F(j\omega)| = 7(5) = 35$$

$$\text{Output signal is } |Y(j\omega)| \sin(\omega t + \phi) = 35 \sin(0.2t - 1.78)$$

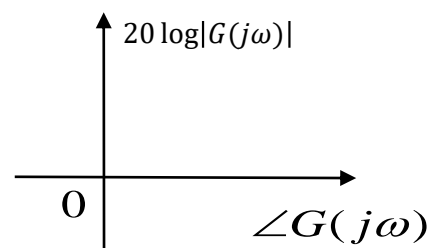
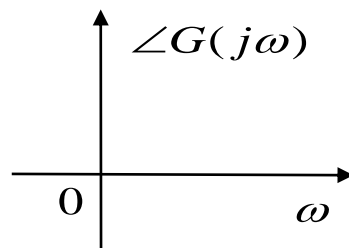
Graphical representation

Consider a system given by transfer function $G(s)$

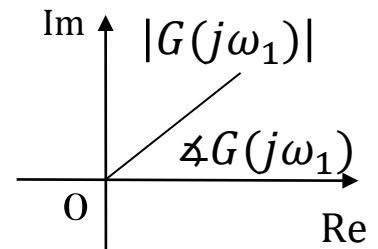
- ❖ The frequency response is described by amplitude ratio $M = |G(j\omega)|$ and phase shift $\phi = \angle G(j\omega)$
- ❖ There are three graphical methods of representing the system frequency response:
 - 1) Bode diagram – separately plot $20 \log|G(j\omega)|$ vs. ω and plot ϕ vs. ω
 - 2) Nichols chart – plot $20 \log|G(j\omega)|$ vs. $\angle G(j\omega)$
 - 3) Nyquist (or polar) diagram – plot (M, ϕ) as ω changes



Bode
diagram



Nichols
chart



Nyquist
diagram

Bode diagram

Sketch the Bode diagram for the following system:

$$G(s) = \frac{1}{s + 2}$$

$$G(j\omega) = \frac{1}{2 + j\omega}$$

$$G(j\omega) = \frac{1 \angle 0^\circ}{\sqrt{4 + \omega^2} \angle \tan^{-1}(\omega/2)}$$

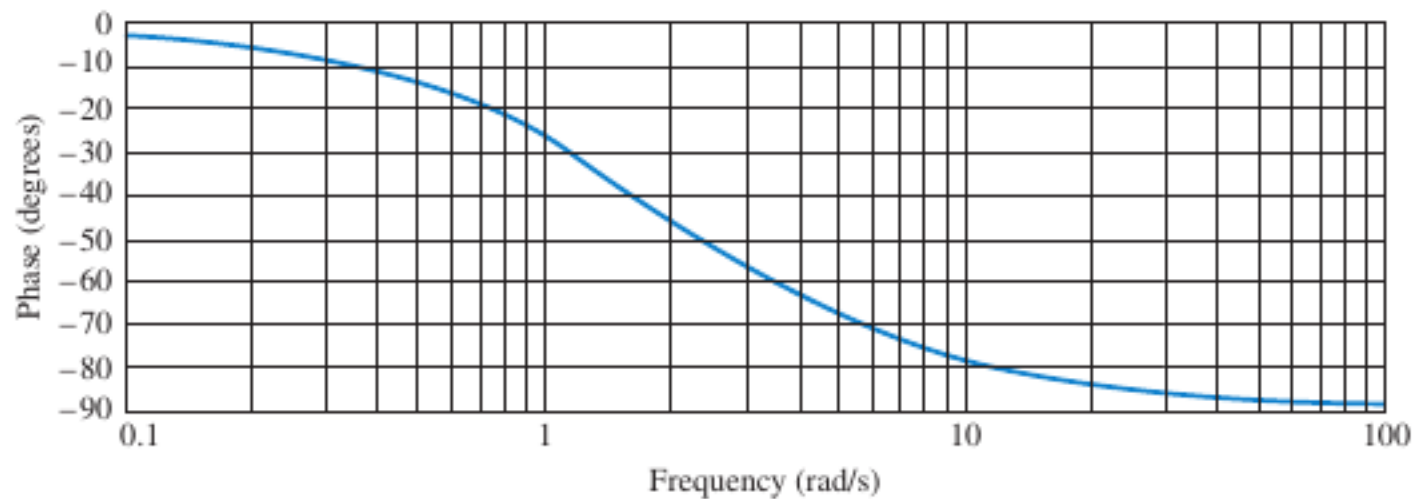
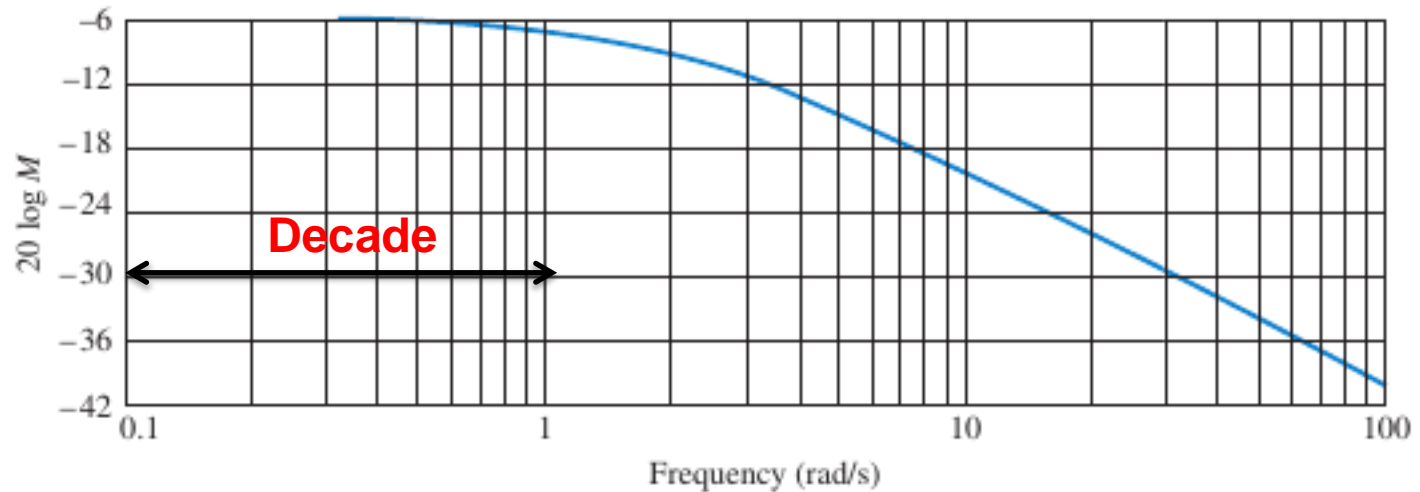
$$|G(j\omega)| = \frac{1}{\sqrt{4 + \omega^2}}$$

$$20 \log |G(j\omega)| = 20 \log \frac{1}{\sqrt{4 + \omega^2}}$$

$$\angle G(j\omega) = -\tan^{-1}(\omega/2)$$

ω	$20 \log G(j\omega) $	$\angle G(j\omega)$
0	-6.02	0
1	-6.99	-26.57°
5	-14.6	-68.2°
10	-20.17	-78.69°
50	-33.99	-87.71°
∞	0	-90°

Bode diagram



Bode approximation

The four different factors that may occur in a transfer function are:

- 1) Constant gain, i.e. K
- 2) Poles (or zeros) at the origin, i.e. s
- 3) Poles (or zeros) on the real axis; i.e. $(Ts + 1)$
- 4) Complex conjugate poles (or zeros), i.e. $(s^2 + 2\zeta\omega_n s + \omega_n^2)$

Given $G(s) = \frac{G_1(s)G_2(s)}{G_3(s)G_4(s)}$

- ❖ Amplitude ratio $(M, \text{db}) = 20 \log|G(s)| = 20 \log \left\{ \frac{|G_1(s)||G_2(s)|}{|G_3(s)||G_4(s)|} \right\}$
 $(M, \text{db}) = 20 \log|G_1(s)| + 20 \log|G_2(s)| - 20 \log|G_3(s)| - 20 \log|G_4(s)|$
- ❖ Phase shift $\phi = \angle G(j\omega) = \phi_1 + \phi_2 - \phi_3 - \phi_4$
- ❖ We will determine the logarithmic magnitude plot and phase angle for the four factors and then use them to approximate the Bode diagram for any general form of a transfer function

Bode approximation

1) Constant gain $G(s) = K$, or $G(j\omega) = K \neq 0$

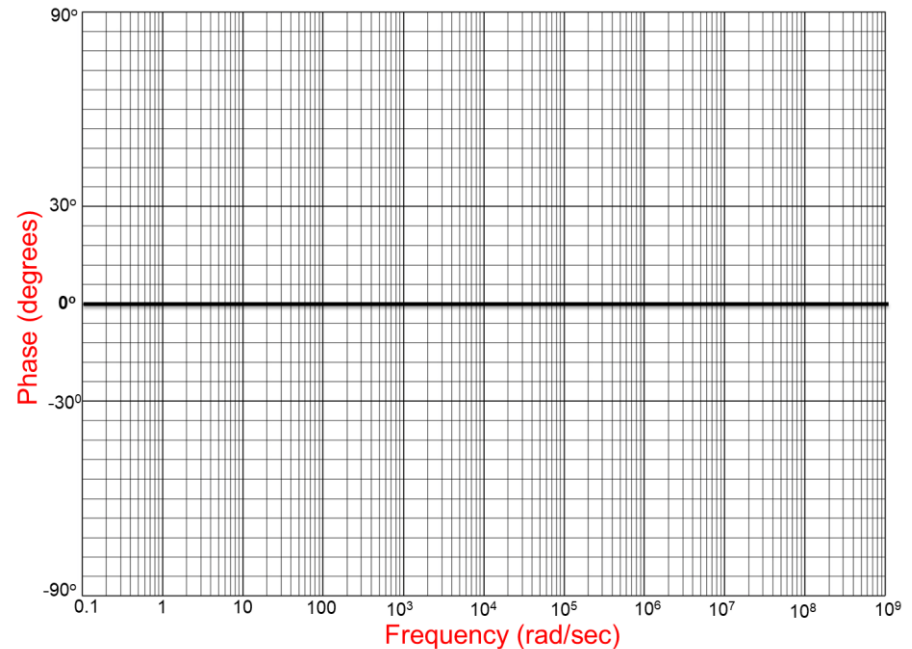
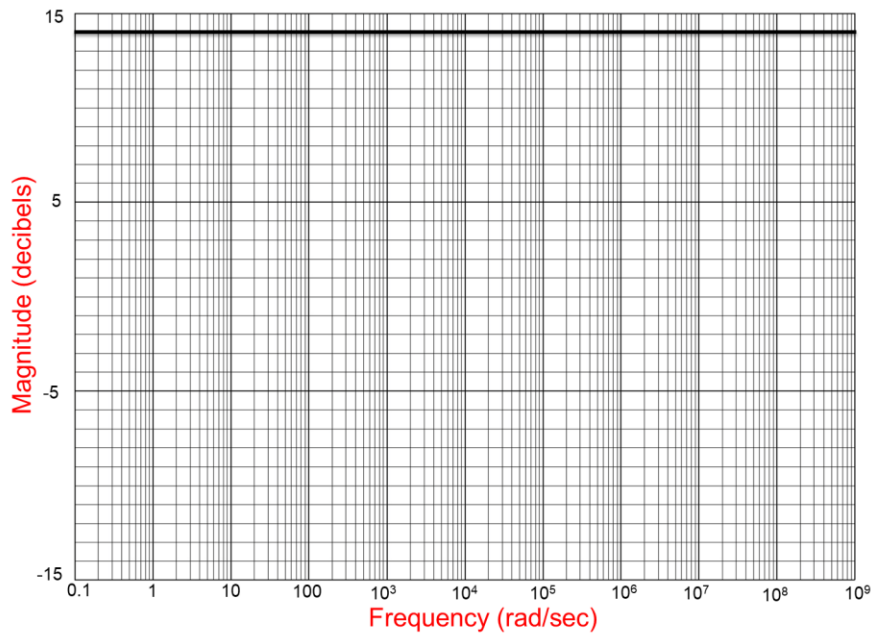
❖ $(M, \text{db}) = 20 \log|K| = \text{constant}$

❖ $\phi = 0$

- The log-magnitude curve for a constant gain K is a horizontal straight line at the magnitude of $20 \log(K)$ decibels.
- The phase angle of the gain K is zero.
- The effect of varying the gain K in the transfer function is that it raises or lowers the log-magnitude curve of the transfer function by the corresponding constant amount, but it has no effect on the phase curve.

Bode approximation

If $K = 5$, then $20 \log(5) = 14\text{db}$ and $\phi = 0$



Bode approximation

2) Poles (or zeros) at the origin:

❖ For pole $G(s) = \frac{1}{s}$, or $G(j\omega) = \frac{1}{j\omega} = \frac{1 \angle 0}{\omega \angle 90^\circ}$

$$(M, \text{db}) = 20 \log|1| - 20 \log|\omega| = -20 \log(\omega)$$

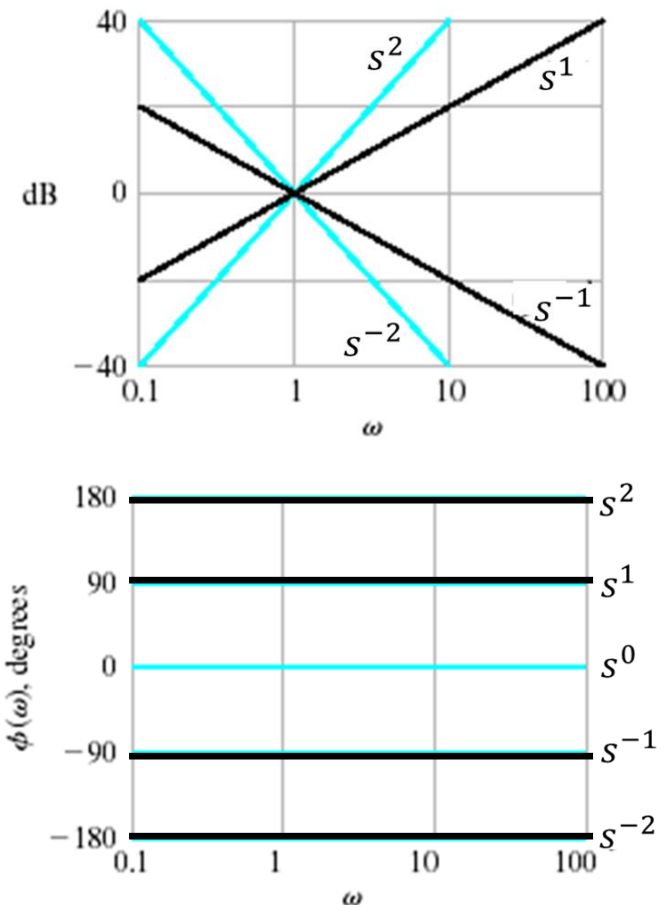
$$\phi = -90^\circ$$

❖ For zero $G(s) = s$, or $G(j\omega) = j\omega = \omega \angle 90^\circ$

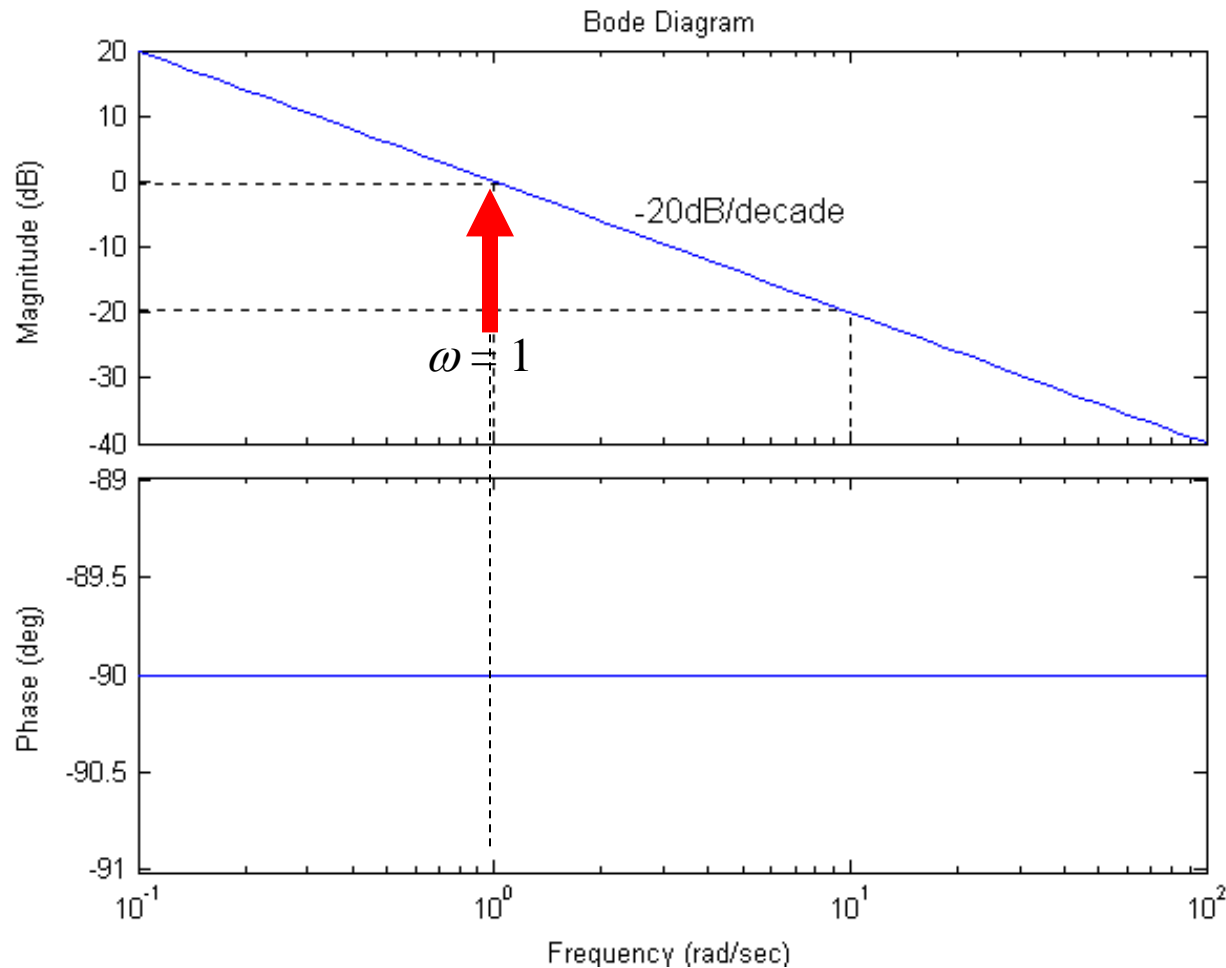
$$(M, \text{db}) = 20 \log|\omega|$$

$$\phi = 90^\circ$$

- The factor $s^{\pm k}$ has a magnitude diagram which is a straight line with slope equal to $\pm 20k$ [dB/decade] and constant phase, equal to $\pm k\pi/2$. This line crosses the horizontal axis (0[dB]) at $\omega = 1$



Bode approximation



$$G(s) = \frac{1}{s}$$

Bode approximation

3) Poles (or zeros) on the real axis; i.e. $(Ts + 1)$:

❖ For pole $G(s) = \frac{1}{Ts+1}$, or $G(j\omega) = \frac{1}{j\omega T+1} = \frac{1 \angle 0}{\sqrt{1+\omega^2 T^2} \angle \tan^{-1}(\omega T)}$

$$(M, \text{db}) = 20 \log|1| - 20 \log \left| \sqrt{1 + \omega^2 T^2} \right| = -20 \log(\sqrt{1 + \omega^2 T^2})$$

$$\phi = -\tan^{-1}(\omega T)$$

As $\omega \rightarrow 0$, $(M, \text{db}) \rightarrow 0$ and $\phi \rightarrow 0$;

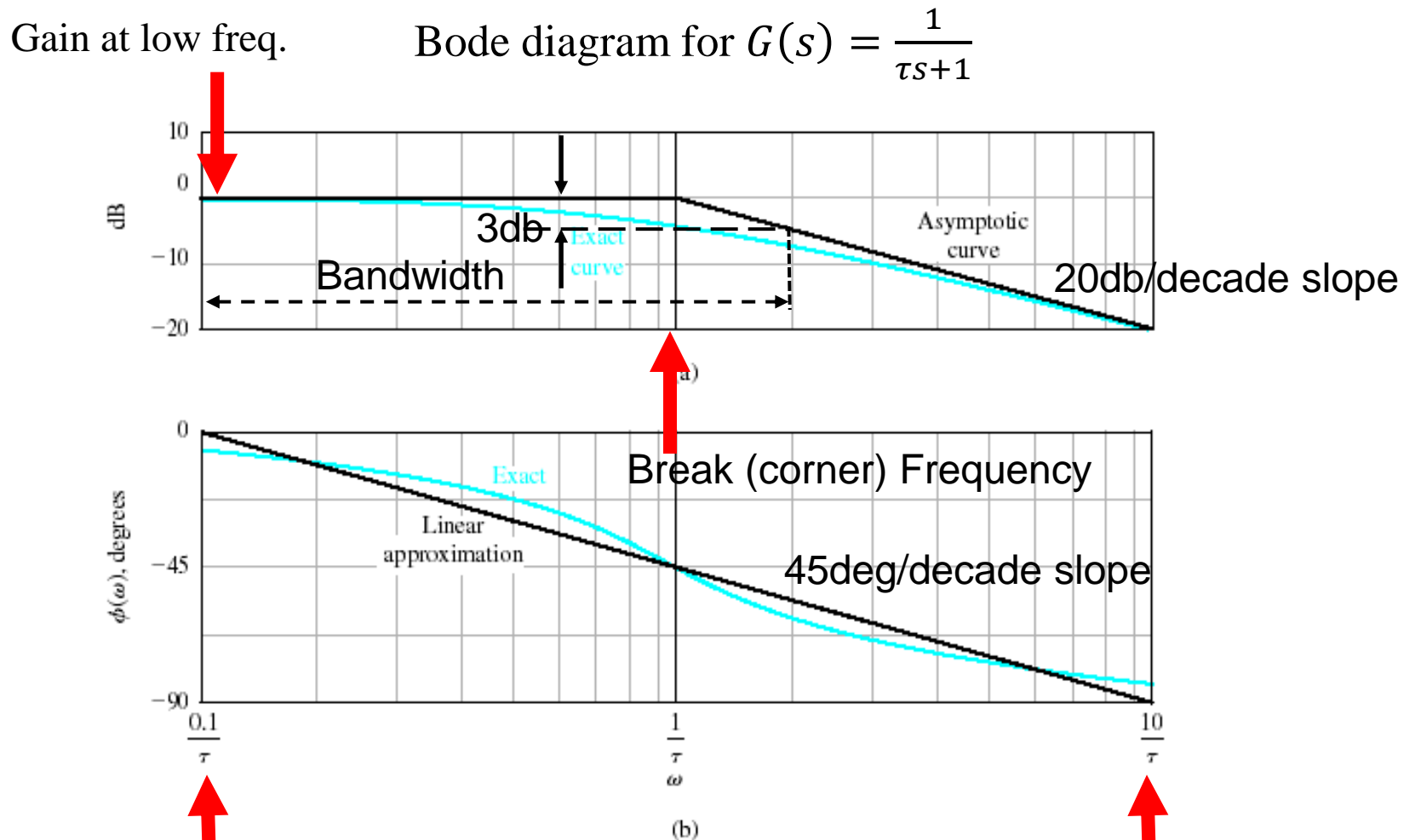
At $\omega = \left(\frac{1}{T}\right)$, $\phi = -45^\circ$ with slope $\approx -45^\circ/\text{decade}$;

As $\omega \rightarrow \infty$, $\phi \rightarrow -90^\circ$; $(M, \text{db}) \approx -20 \log(\omega T)$;

We can approximate the amplitude ratio as

$(M, \text{db}) \approx -20 \log \omega - 20 \log T$; after $\omega = \frac{1}{T}$ it has -20db/decade slope.

Bode approximation



Bode approximation

3) Poles (or zeros) on the real axis; i.e. $(Ts + 1)$:

❖ For zero $G(s) = Ts + 1$, or $G(j\omega) = j\omega T + 1 = \sqrt{1 + \omega^2 T^2} \angle \tan^{-1}(\omega T)$

$$(M, \text{db}) = 20 \log \left| \sqrt{1 + \omega^2 T^2} \right|$$
$$\phi = \tan^{-1}(\omega T)$$

As $\omega \rightarrow 0$, $(M, \text{db}) \rightarrow 0$ and $\phi \rightarrow 0$;

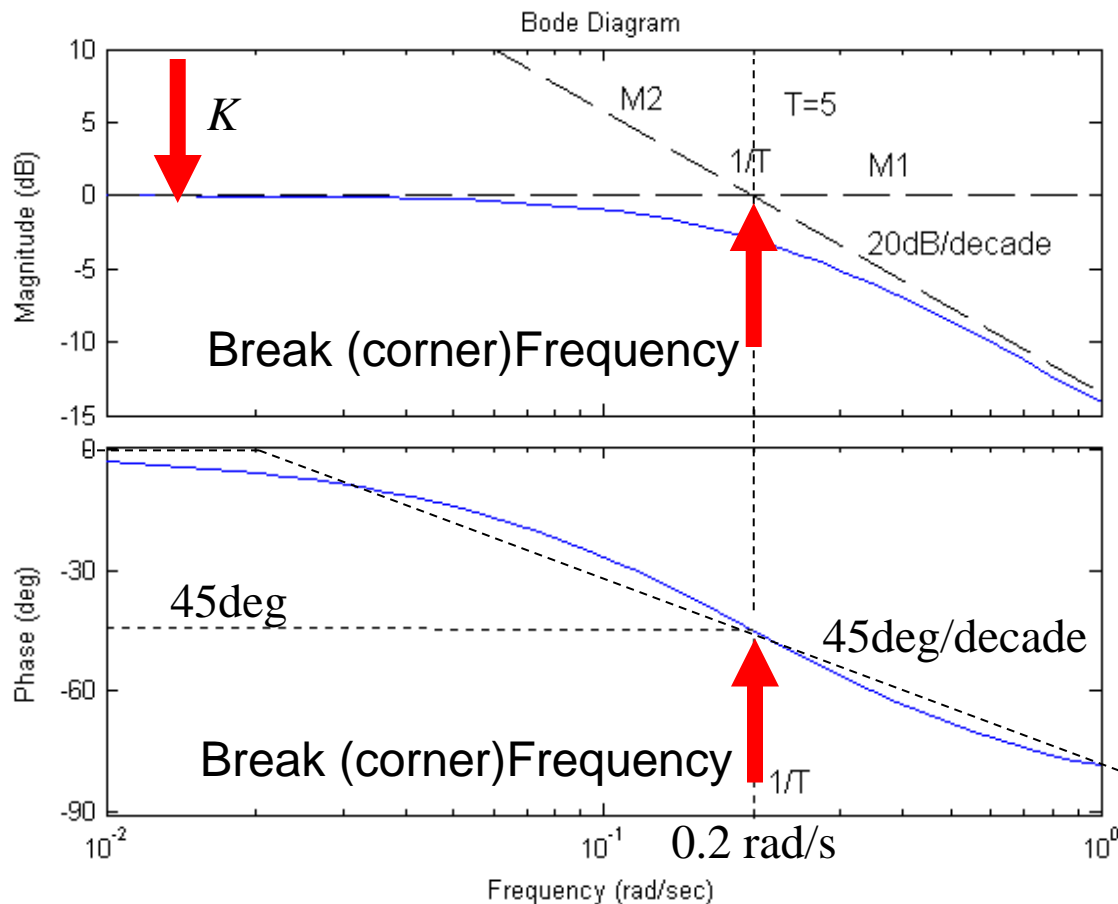
At $\omega = \left(\frac{1}{T}\right)$, $\phi = 45^\circ$ with slope $\approx 45^\circ/\text{decade}$;

As $\omega \rightarrow \infty$, $\phi \rightarrow 90^\circ$ and $(M, \text{db}) \approx 20 \log(\omega T)$;

We can approximate the amplitude ratio as

$(M, \text{db}) \approx 20 \log \omega + 20 \log T$; after $\omega = \frac{1}{T}$ it has 20db/decade slope

Bode approximation



$$G(s) = \frac{1}{5s + 1}$$

Corner frequency at

$$\omega = \left(\frac{1}{T}\right) = \frac{1}{5} = 0.2 \text{ rad/s}$$

Note: K and corner freq.

Bode approximation

4) Complex conjugate poles (or zeros), i.e. $(s^2 + 2\zeta\omega_n s + \omega_n^2)$:

❖ For pole $G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$, or $G(j\omega) = \frac{\omega_n^2}{\omega_n^2 - \omega^2 + 2\zeta\omega_n \omega j} = \frac{1}{1 - \left(\frac{\omega}{\omega_n}\right)^2 + 2\zeta\left(\frac{\omega}{\omega_n}\right)j}$

$$(M, \text{db}) = -20 \log \left| \sqrt{\left\{1 - \left(\frac{\omega}{\omega_n}\right)^2\right\}^2 + \left\{2\zeta \frac{\omega}{\omega_n}\right\}^2} \right|$$

$$\phi = -\tan^{-1} \left\{ \frac{2\zeta \frac{\omega}{\omega_n}}{1 - \left(\frac{\omega}{\omega_n}\right)^2} \right\}$$

As $\omega \rightarrow 0$, $(M, \text{db}) \rightarrow 0$ and $\phi \rightarrow 0$;

At $\omega = \omega_n$, $(M, \text{db}) = -20 \log(2\zeta)$ and $\phi = -90^\circ$; slope $\approx -90^\circ/\text{decade}$

As $\omega \rightarrow \infty$, $(M, \text{db}) \approx -20 \log \left(\frac{\omega}{\omega_n}\right)^2 = -40 \log \omega + 40 \log \omega_n$ and $\phi \rightarrow -180^\circ$;

Note after $\omega = \omega_n$ it has -40db/decade slope

Bode approximation

4) Complex conjugate poles (or zeros), i.e. $(s^2 + 2\zeta\omega_n s + \omega_n^2)$:

❖ For zero $G(s) = \frac{s^2 + 2\zeta\omega_n s + \omega_n^2}{\omega_n^2}$, or $G(j\omega) = 1 - \left(\frac{\omega}{\omega_n}\right)^2 + 2\zeta\left(\frac{\omega}{\omega_n}\right)j$

$$(M, \text{db}) = 20 \log \left| \sqrt{\left\{1 - \left(\frac{\omega}{\omega_n}\right)^2\right\}^2 + \left\{2\zeta \frac{\omega}{\omega_n}\right\}^2} \right|$$

$$\phi = \tan^{-1} \left\{ \frac{2\zeta \frac{\omega}{\omega_n}}{1 - \left(\frac{\omega}{\omega_n}\right)^2} \right\}$$

As $\omega \rightarrow 0$, $(M, \text{db}) \rightarrow 0$ and $\phi \rightarrow 0$;

At $\omega = \omega_n$, $(M, \text{db}) = 20 \log(2\zeta)$ and $\phi = 90^\circ$; slope $\approx 90\text{deg/decade}$

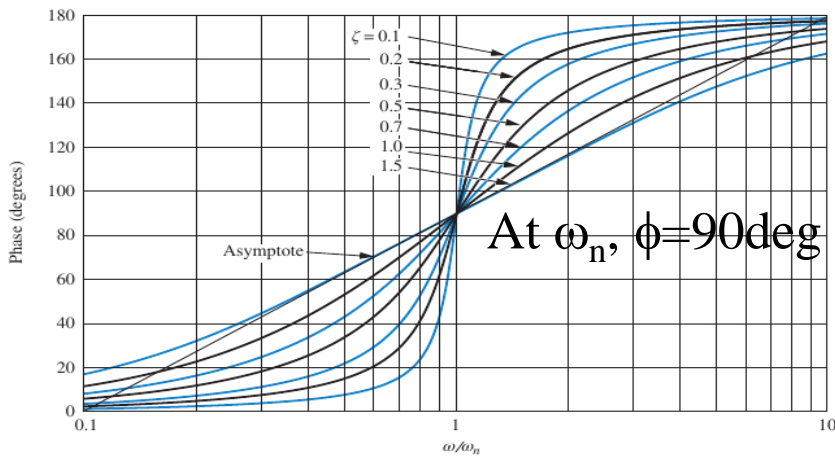
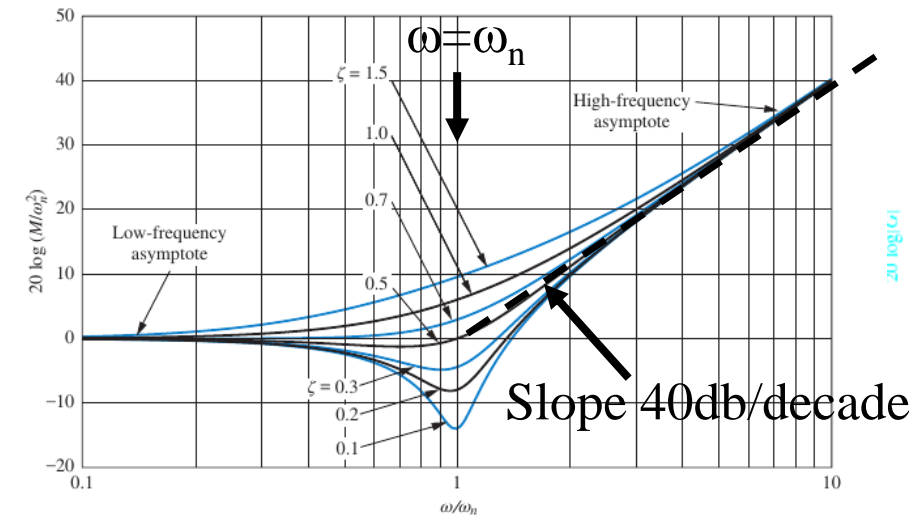
As $\omega \rightarrow \infty$, $(M, \text{db}) \approx 20 \log \left(\frac{\omega}{\omega_n}\right)^2 = 40 \log \omega - 40 \log \omega_n$ and $\phi \rightarrow -180^\circ$;

Note after $\omega = \omega_n$ it has 40db/decade slope

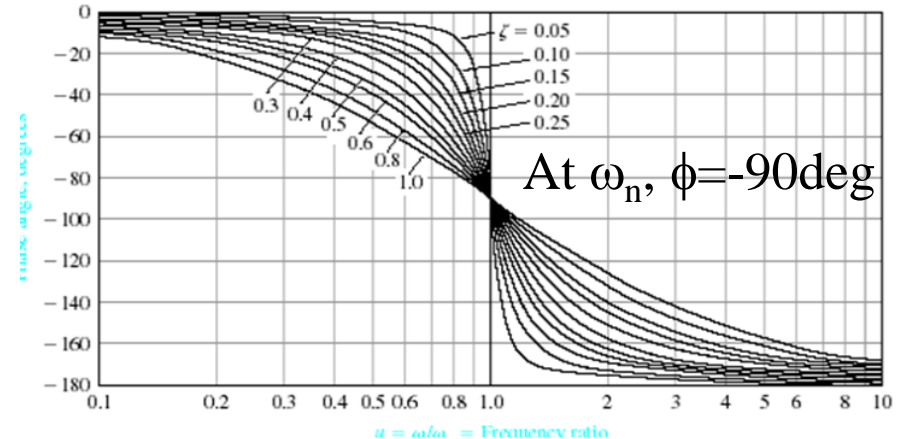
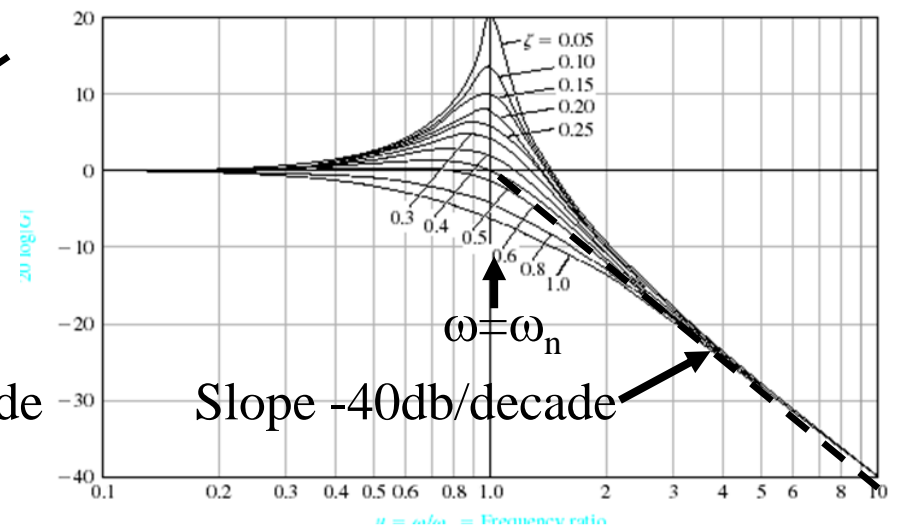
Resonance frequency $\omega_r = \omega_n \sqrt{1 - 2\zeta^2}$

At resonance $M_r = \frac{1}{2\zeta\sqrt{1-\zeta^2}}$

Complex Zero



Complex Pole



Example 2

Sketch the Bode diagram for the transfer function

$$G(s) = \frac{2500(s + 10)}{s(s + 2)(s^2 + 30s + 2500)}$$

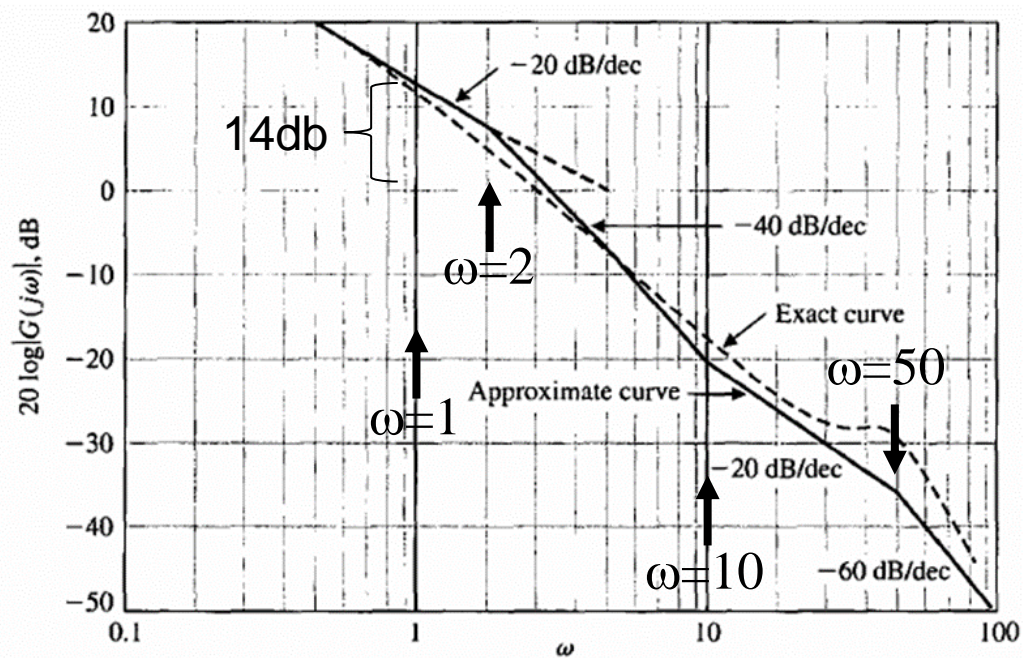
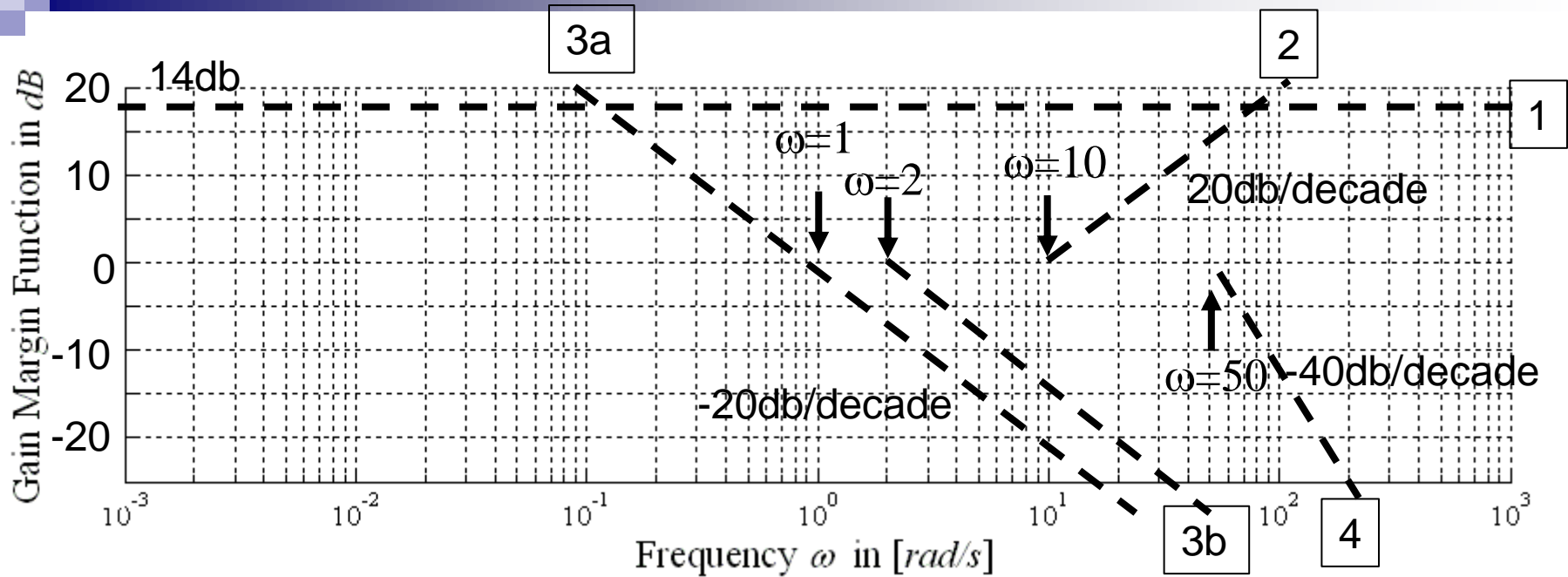
Reformat the transfer function:

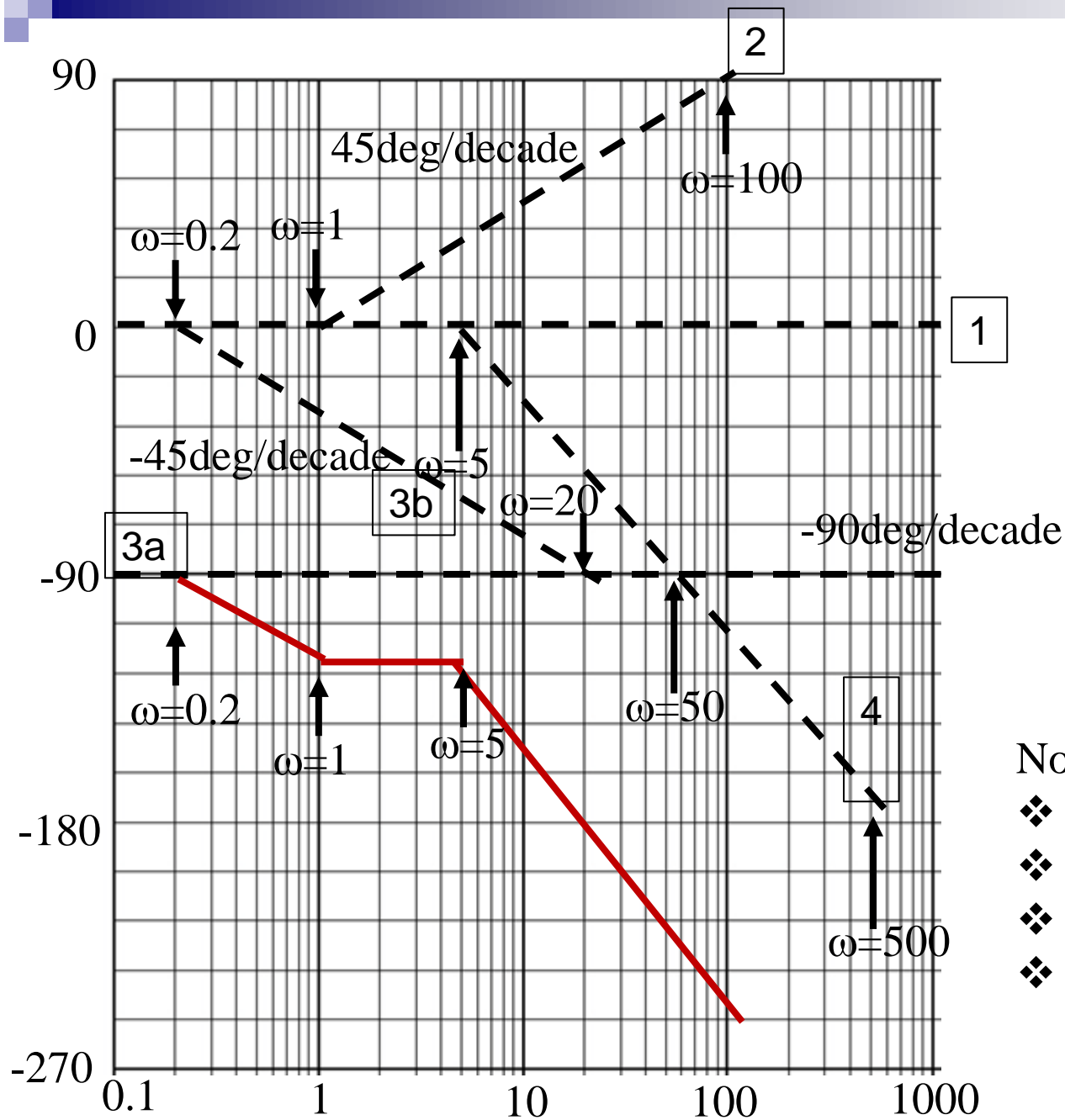
$$G(s) = \frac{5(0.1s + 1)}{s(0.5s + 1) \left(\frac{1}{50^2} s^2 + \frac{0.6}{50} s + 1 \right)}$$

$$G(j\omega) = \frac{5(0.1\omega j + 1)}{j\omega(0.5j\omega + 1) \left(0.6 \left(\frac{\omega}{50} \right) j + 1 - \left(\frac{\omega}{50} \right)^2 \right)}$$

Factors:

- ❖ Gain $K = 5$ or $20 \log 5 = 14\text{db}$
- ❖ Zero at $\omega = 10$
- ❖ Pole at origin and pole at $\omega = 2$
- ❖ A pair of complex pole at $\omega_n = 50$



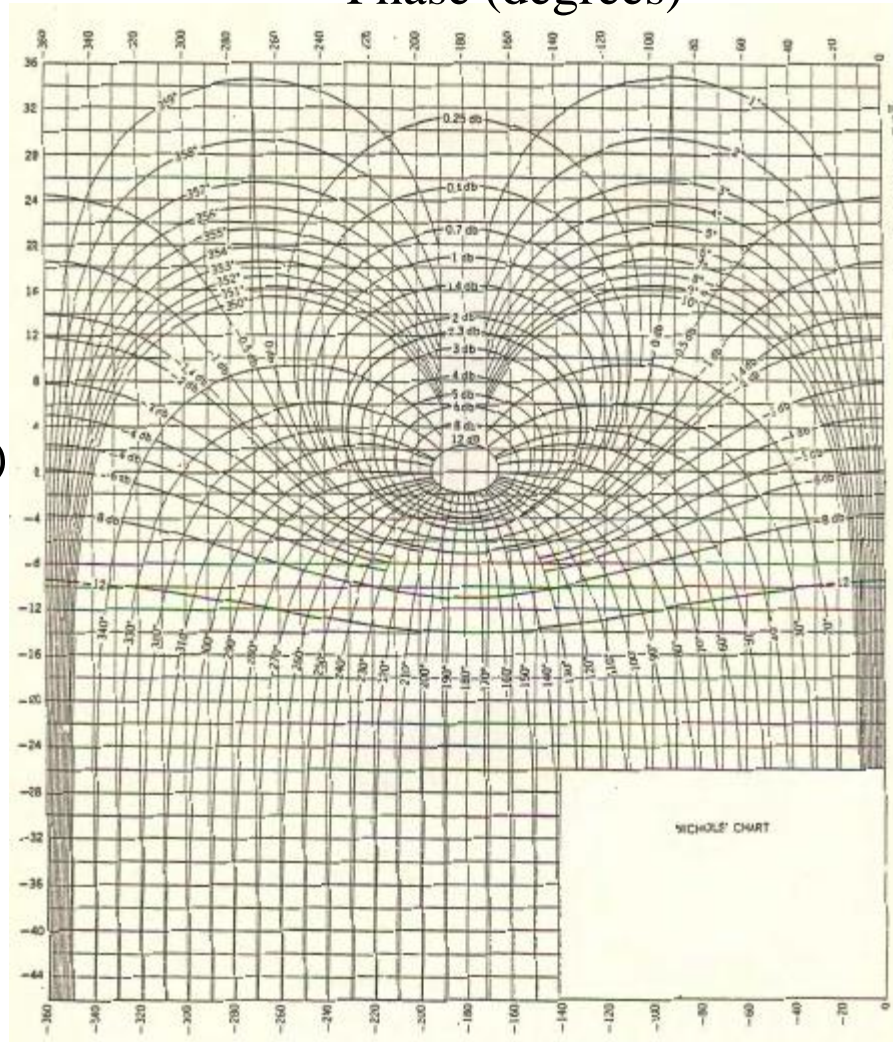


Note critical frequencies at

- ❖ $\omega = 2$
- ❖ $\omega = 10$
- ❖ $\omega = 50$
- ❖ Add the contributions

Nichols chart

Phase (degrees)



Nichols chart

Sketch the Nichols chart for the following system:

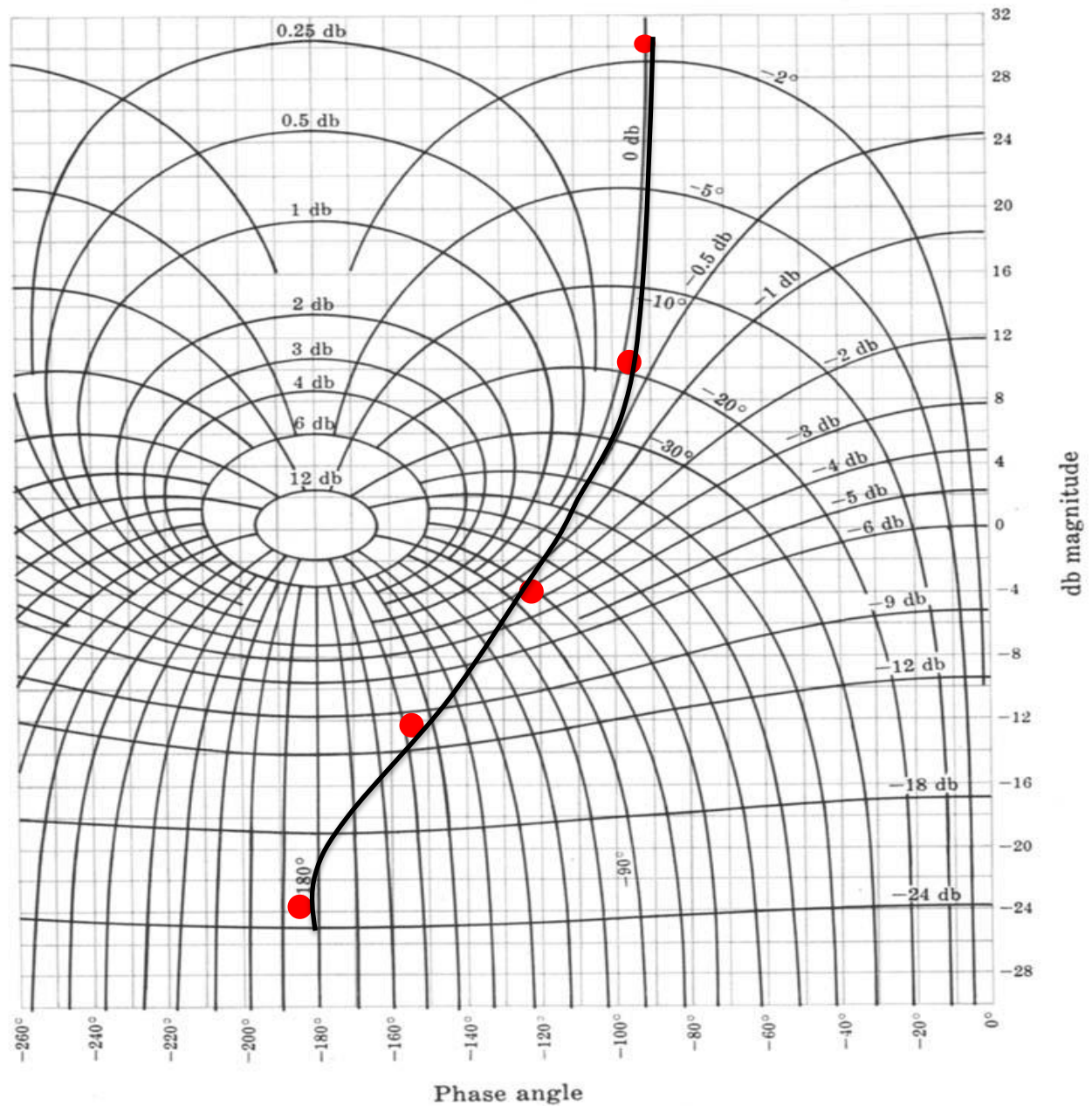
$$G(s) = \frac{1}{s(s+1)(s+3)}$$

ω	$ G(j\omega) _{db}$	$\angle G(j\omega)$
0.01	30.4	-90.7°
0.1	10.4	-97.6°
0.5	-4.6	-126°
1	-13	-153°
2	-24.1	-187°

$$G(j\omega) = \frac{1}{(j\omega)(j\omega+1)(j\omega+3)}$$

$$G(j\omega) = \frac{1\angle 0^\circ}{\omega(\sqrt{1+\omega^2})(\sqrt{9+\omega^2})\angle 90^\circ + \tan^{-1}\omega + \angle \tan^{-1}(\omega/3)}$$

ω	$ G(j\omega) _{db}$	$\angle G(j\omega)$
0.01	30.4	-90.7°
0.1	10.4	-97.6°
0.5	-4.6	-126°
1	-13	-153°
2	-24.1	-187°



Nyquist diagram

Sketch the Nyquist diagram for the following system:

$$G(s) = \frac{1}{0.2s + 1}$$

$$G(j\omega) = \frac{1}{1 + j\omega 0.2}$$

$$G(j\omega) = \frac{1 \angle 0^\circ}{\sqrt{1 + \omega^2 0.04} \angle \tan^{-1} \omega 0.2}$$

$$|G(j\omega)| = \frac{1}{\sqrt{1 + \omega^2 0.04}}$$

$$\angle G(j\omega) = -\tan^{-1}(\omega 0.2)$$

ω	$ G(j\omega) $	$\angle G(j\omega)$
0	1	0
1	0.96	-11.31°
5	0.5	-45°
10	0.2	-63.43°
30	0.02	-80.54°
∞	0	-90°

Nyquist Diagram

