## Chemical Engineering Thermodynamics CHE F213

## **Chemical-Reaction Equilibria**

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### **Outline**

- Introduction
- Reaction co-ordinate
- Multiple reaction stoichiometry
- Standard Gibbs free energy and Standard Enthalpy change for a reaction
- Equilibrium constant (K)
- Relation of equilibrium constant to composition
- Effect of temperature and pressure on K



## **Chemical reaction Equilibria**

- □ Reactor: Heart of chemical plant : Raw materials get converted to product
- □ Chemical Engineers design reactors
- Need to understand degree of conversion at equilibrium
- □ Thermodynamics (equilibrium) and Kinetics (rate) then go hand in hand
- □ Equilibrium conversion: f (T, P and composition)
- Maximizing yield from a reactor under optimum pressure and temperature is the objective



### **Reaction coordinate**

The general chemical reaction is written as:

$$|v_1|A_1 + |v_2|A_2 + \dots \rightarrow |v_3|A_3 + |v_4|A_4 + \dots$$

where  $|v_i|$  is stoichiometric coefficient (sign convention + for product, - for reactant and 0 for inert) and  $A_i$  is chemical formula

 As the reaction progresses, the change in the number of moles of species present in the reaction is directly proportional to their respective stoichiometric numbers

$$\frac{dn_1}{v_1} = \frac{dn_2}{v_2} = \frac{dn_3}{v_3} = \frac{dn_4}{v_4} \equiv d\varepsilon$$

 Here ε represents the amount of reaction and is called reaction coordinate, characterize the extent/degree of reaction

### Reaction coordinate

$$dn_i = v_i d\varepsilon$$
 (i = 1,2,... N)

Integrating above eqn. from an initial unreacted state where  $\epsilon = 0$  and  $n_i = n_{io}$  to a state reached after an arbitrary amount of reaction gives,

$$\int_{n_{i0}}^{n_i} dn_i = v_i \int_{0}^{\varepsilon} d\varepsilon$$

$$n_i = n_{io} + \varepsilon v_i$$

total number of moles  $n = \sum n_{io} + \epsilon \sum v_i$ 

$$n_o = \sum n_{io} \& v = \sum v_i$$

$$y_i = n_i/n = (n_{io} + v_i \epsilon) / (n_o + v \epsilon)$$



## Illustration 1 (Example 13.1)

The following reaction takes place in a system containing 2 moles of methane, 1 mol water, 1 mol CO and 4 mol hydrogen

$$CH_4 + H_2O \rightarrow CO + 3H_2$$

- Identify the mol numbers
- Identify the total number of moles
- Identify the stoichiometric number of each species
- Indentify the sum of the stoichiometric number
- If the extent of reaction is  $\epsilon$ , what is the mole fraction in terms of  $\epsilon$ ?



## **Multi-reaction Stoichiometery**

For two or more independent reactions, subsript j serves as reaction index

For species i : 
$$n_i = n_{io} + \sum v_{i,j} \varepsilon_j$$

Total number of moles 
$$n = n_o + \sum v_j \epsilon_j$$
  
 $n_o = \sum n_{io} \& v = \sum v_{io}$ 

$$y_i = n_i/n = (n_{io} + \sum v_{i,j} \varepsilon_j) / (n_o + \sum v_j \varepsilon_j)$$
  
Here  $v_j = \sum v_{i,j}$  for a single reaction

## Illustration 2 (Example 13.3)



A system initially charged with 2 mol of CH<sub>4</sub> and 3 mol of water is undergoing the following reaction

$$CH_4 + H_2O \rightarrow CO + 3H_2$$
 eq. (1)

 $CH_4 + 2H_2O \rightarrow CO_2 + 4H_2$  eq. (2)

If the extent of reaction is  $\varepsilon_1$  and  $\varepsilon_2$ , for reaction 1 and 2 respectively, determine expressions for the  $y_i$ , as functions of  $\varepsilon_1$  and  $\varepsilon_2$ .

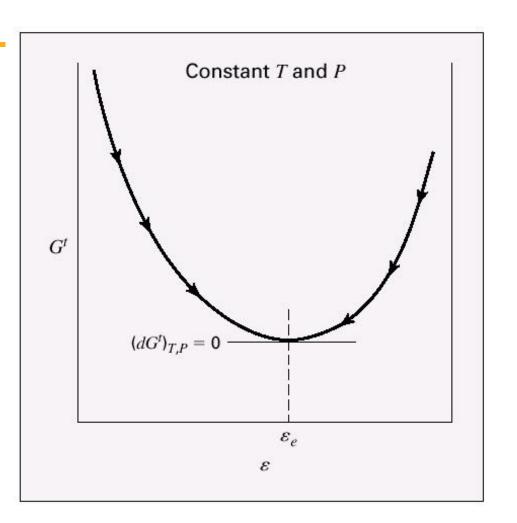
# Equilibrium criterion for a chemical reaction



- A Chemical reaction must proceed in the direction of decreasing total Gibbs free energy (G<sup>t</sup>).
- At equilibrium state, (dGt)<sub>T,P</sub> = 0

$$(dG)_{T,P} = 0 = \sum \mu_i dn_i = \sum \mu_i v_i d\epsilon = 0$$

CRITERION FOR EQUILIBRIUM



**Figure 13.1**: The total Gibbs energy in relation to the reaction coordinate.

# The standard Gibbs-Energy change and the Equilibrium constant



The fundamental property relation for single-phase systems, provides an expression for the total Gibbs energy

$$d(nG) = (nV)dP - (nS)dT + \sum_{i} \mu_{i} dn_{i}$$

For changes in the mole numbers n<sub>i,</sub> as the result of a single chemical reaction

$$d(nG) = (nV)dP - (nS)dT + \sum_{i} v_{i} \mu_{i} d\varepsilon$$

$$or..\sum_{i} v_{i} \mu_{i} = \left[\frac{\partial (nG)}{\partial \varepsilon}\right]_{T,P} = \left[\frac{\partial (G^{t})}{\partial \varepsilon}\right]_{T,P}$$

Thus the quantity  $\sum v_i \mu_i$  represent the change in total Gibbs energy of the system with respect to the reaction coordinate at T,P.



### **Equilibrium Constant K**

A criterion of chemical-reaction equilibrium is

$$\sum_{i} v_{i} \mu_{i} = 0$$

Recall the definition of the fugacity of a species in solution:

$$\mu_i = \Gamma_i(T) + RT \ln \hat{f}_i$$

The Gibbs free energy of species i in standard state (1 atm and 25°C)

$$G_i^0 = \Gamma_i(T) + RT \ln f_i^0$$

The difference between the two equations is

$$\mu_i - G_i^0 = RT \ln \frac{\hat{f}_i}{f_i^0}$$

Put μ<sub>i</sub> expression from above equation to reaction equilibrium criteria

$$\sum \mu_i v_i d\varepsilon = 0$$



### **Equilibrium Constant**

$$\sum_{i} v_{i} \left[ G_{i}^{0} + RT \ln \frac{\hat{f}_{i}}{f_{i}^{0}} \right] = 0 \qquad \Rightarrow \qquad \ln \prod_{i} \left( \frac{\hat{f}_{i}}{f_{i}^{0}} \right)^{v_{i}} = \frac{-\sum_{i} v_{i} G_{i}^{0}}{RT}$$

Introducing a new term equilibrium constant K as:

$$\prod_{i} \left( \frac{\hat{f}_{i}}{f_{i}^{0}} \right)^{v_{i}} = K$$

$$K \equiv \exp\left(\frac{-\Delta G^0}{RT}\right)$$
 or  $\ln K = \left(\frac{-\Delta G^0}{RT}\right)$ 

where 
$$\Delta G^0 = \sum_i v_i G_i^0$$

Standard Gibbs-energy change of reaction

 $\Delta$ G° is pure species property at fixed pressure, it depends only on temperature and hence K are also functions of temperature only.

## Standard state Gibbs Energy from Enthalpy



Standard property (M) change of reaction is defined as

$$\Delta M^{o} \equiv \sum_{i} v_{i} \Delta M^{o}$$

For example,

$$\Delta H_{rxn}^{0}(T = 25^{0}C) = \sum_{i} v_{i} \Delta H_{f_{i}}^{0}(T = 25^{0}C) \quad \text{and} \quad \Delta C_{P}^{o}(T = \sum_{i} v_{i} C_{P_{i}}^{o})$$

$$\Delta C_P^o(T = \sum_i v_i C_{P_i}^o)$$

The relation between the standard heat of reaction  $\Delta H_i^{\circ}$ and the standard Gibbs energy change of reaction for species i in standard state:

$$\Delta H_i^0 = -RT^2 \frac{d(\Delta G_i^0 / RT)}{dT}$$
$$\Delta H^0 = -RT^2 \frac{d(\Delta G^0 / RT)}{dT}$$



## Effect of temperature on K

Standard Heat (enthalpy) of reaction and Standard Gibbs free energy change are related by property relation (at constant P and composition)

$$\frac{d(\Delta G^{0}/RT)}{dT} = -\frac{\Delta H_{rxn}^{0}}{RT^{2}}$$

In terms of equilibrium constant

$$\frac{d \ln K}{dT} = \frac{\Delta H_{rxn}^0}{RT^2}$$

•The effect of temperature on the equilibrium constant K is determined by the sign of  $\Delta H_{rxn}^{\ \ o}$ 

 $\Delta H_{rxn}^{\circ} > 0$  (Endothermic reaction) : increase in T increases K

 $\Delta H_{rxn}^{o} < 0$  (Exothermic reaction): increase in T decreases K

# Effect of temperature on K

 $\frac{d \ln K}{dT} = \frac{\Delta H_{rxn}^{0}}{RT^{2}}$  can be integrated between two temperature  $T_{1}$  and  $T_{2}$ :

$$\ln \frac{K(T_2)}{K(T_1)} = \int_{T_1}^{T_2} \frac{\Delta H_{rxn}^0(T)}{RT^2} dT$$

If  $\Delta H_{rxn}^{0}$  is constant over a temperature range, integration of the above equation for two temperature limits, result

$$\ln \frac{K(T_2)}{K(T_1)} = -\frac{\Delta H^0}{R} \left( \frac{1}{T_2} - \frac{1}{T_1} \right)$$

PLOT OF In K vs 1/T will be a straight line

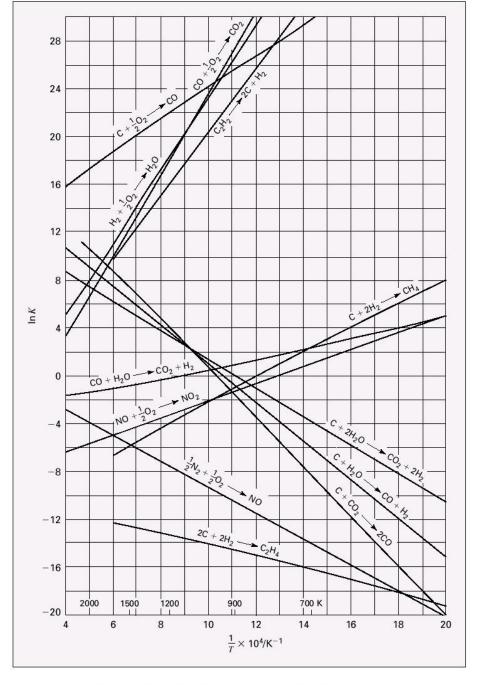


Figure 13.2: Equilibrium constants as a function of temperature.

# Calculation of effect of temperature on K



The development of the effect of temperature on equilibrium constant is based on definition of  $G_i^{\circ}$ 

$$G_i^o = H_i^o - TS_i^o$$

Multiplication by  $v_i$  and summation over all species gives

$$\sum_{i} v_{i} G_{i}^{o} = \sum_{i} v_{i} H_{i}^{o} - T \sum_{i} v_{i} S_{i}^{o}$$
$$\Delta G^{o} = \Delta H^{o} - T \Delta S^{o}$$

The standard heat of reaction is related to temperature (T)

$$\Delta H^{o}(T) = \Delta H_{0}^{o}(T = 25^{\circ}C) + R \int_{T_{0}}^{T} \frac{\Delta C_{P}^{o}}{R} dT$$

$$-\ln K = \frac{\Delta G^{o}(T)}{RT} = \frac{\Delta G_{0}^{o} - \Delta H_{0}^{o}(T = 25^{0}C)}{RT_{0}} + \frac{\Delta H_{0}^{o}}{RT} + \frac{1}{T} \int_{T_{0}}^{T} \frac{\Delta C_{P}^{o}}{R} dT - \int_{T_{0}}^{T} \frac{\Delta C_{P}^{o}}{R} \frac{dT}{T}$$

# Relation of Equilibrium constants to composition



#### Gas Phase reactions

$$\prod_{i} \left( \frac{\hat{f}_{i}}{P^{o}} \right)^{v_{i}} = K \qquad \text{Here P}_{0} \text{ is standard state pressure of 1 bar}$$

$$\hat{f}_i = \hat{\phi}_i y_i P \quad \Rightarrow \quad \prod_i (y_i \hat{\phi}_i)^{v_i} = \left(\frac{P}{P^o}\right)^{-\nu} K$$

For ideal solution case:

$$\prod_{i} (y_{i} \phi_{i})^{\nu_{i}} = \left(\frac{P}{P^{o}}\right)^{-\nu} K$$

For low pressures and/or high temperatures, the equilibrium mixture behaves as an ideal gas

$$\prod_{i} (y_i)^{\nu_i} = \left(\frac{P}{P_0}\right)^{-\nu} K \qquad (13.28)$$

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# Effect of pressure and temperature on equilibrium constant

$$\prod_{i} (y_i)^{\nu_i} = \left(\frac{P}{P_0}\right)^{-\nu} K \qquad (13.28)$$

- Equation shows that an increase in K at constant P result in increase in left term, which implies a shift of reaction to the right and an increase in ε<sub>e</sub> and vice versa.
- If the total stoichiometric number v is negative, an increase in P at constant T causes an increase in left side term, implying a shift of reaction to the right and an increase in ε<sub>e</sub> and vice versa.

\*\*\* Validates Le Chatelier's Principle

## Liquid phase reaction

For a reaction occurring in the liquid phase,

$$\prod_{i} \left( \frac{\hat{f}_{i}}{f_{i}^{o}} \right)^{v_{i}} = K$$

$$\hat{f}_i = \gamma_i x_i f_i \quad \Rightarrow \quad \frac{\hat{f}_i}{f_i^o} = \gamma_i x_i \left( \frac{f_i}{f_i^o} \right)$$

For pure liquid i,

$$G_i - G_i^o = RT \ln \frac{f_i}{f_i^o} = \int_{P^o}^P V_i dP$$

As V<sub>i</sub> changes little with change in pressure for liquids

$$\ln \frac{f_i}{f_i^o} = \frac{V_i (P - P^o)}{RT}$$

# **Equilibrium Constant for Liquid Phase Reaction**



General expression for liquid phase equilibrium constant

$$\prod_{i} (x_{i} \gamma_{i})^{\nu_{i}} = K \exp \left[ \frac{(P^{o} - P)}{RT} \sum_{i} (\nu_{i} V_{i}) \right]$$

For low to moderate pressures, exponential term is unity

$$\prod_{i} (x_i \gamma_i)^{\nu_i} = K$$

If the equilibrium mixture is an ideal solution, then  $\gamma_i$  is unity

$$\prod_{i} (x_i)^{\nu_i} = K$$

This simple equation is known as *law of mass action*.

# Equilibrium conversion for single reaction



For gas phase reaction:

$$\prod_{i} (y_{i} \hat{\phi}_{i})^{\nu_{i}} = \left(\frac{P}{P^{o}}\right)^{-\nu} K$$

For liquid phase reaction

$$\prod_{i} (x_{i} \gamma_{i})^{\nu_{i}} = K \exp \left[ \frac{(P^{o} - P)}{RT} \sum_{i} (\nu_{i} V_{i}) \right]$$

Relation of reaction extent to mole fractions

$$y_i = n_i/n = (n_{io} + \sum v_{i,j} \varepsilon_j) / (n_o + \sum v_j \varepsilon_j)$$



## Illustration (Problem 13.9)

For the ammonia synthesis reaction written as

$$1/2 N_2(g) + 3/2 H_2(g) \rightarrow NH_3(g)$$

with 0.5 mol N<sub>2</sub> and 1.5 mol H<sub>2</sub>, as the initial amounts of reactants and with the assumption that the equilibrium mixture is an ideal gas, show that

$$\varepsilon_e = 1 - \left(1 + 1.299K \frac{P}{P^o}\right)^{-1/2}$$

### **Problems**

Example 1. Write the equilibrium constant expression for the reaction in terms of partial pressures (assume ideal gas mixture)

$$N_2(g) + 3H_2(g) ---> 2NH_3(g)$$

Solution. All species are gases, so we use their partial pressures

$$K_{eq} = P_{NH3}^2 / P_{H2}^3 P_{N2}$$

# Equilibrium constant (Hess law)



#### Rule 1

Multiplication of a reaction by a constant

•If all of the stoichiometric coefficients of an equation are multiplied by the same constant, the new equilibrium constant expression is obtained by raising the old one to a power equal to the constant  $(K_2 = K_1^n)$ 

#### Rule 2

Reversing a reaction. If a reaction is reversed (turned around), its equilibrium constant is reciprocated (inverted).

### **Problems**



Combining reactions by addition or subtraction. We use Hess's Law to obtain a desired reaction by adding (subtracting) two or more other reactions. How is  $K_{eq}$  for the sum related to the  $K_{eq}$ 's of the combined reactions? Again, example illustrates this clearly.

Example 12-6. The third reaction below can be obtained by adding the first two reactions.

(1) 
$$C(s) + 1/2 O_2(g) ---> CO(g)$$
  
 $K_1 = P_{CO}/P_{O2}^{1/2}$ 

(2) 
$$CO(g) + 1/2 O_2(g) ---> CO_2(g)$$
  
 $K_2 = P_{CO2}/P_{CO}P_{O2}^{1/2}$ 

(3) = (1) + (2) C(s) + 
$$O_2(g)$$
 --->  $CO_2(g)$   
 $K_3 = P_{CO2}/P_{O2}$  How is  $K_3$  related to  $K_1$  and  $K_2$ ?

<u>Solution.</u> Inspection of the equilibrium constant expressions shows that  $K_3$  is the product of  $K_1$  and  $K_2$ . Generalizing, when two reactions are added to give a third, their  $K_{eq}$ 's must be multiplied to obtain  $K_{eq}$  for the third:

$$(3) = (1) + (2)$$
  $K_3 = K_1K_2$ 



#### For the reaction represented by

$$SO_2(g) + 1/2O_2(g) \rightarrow SO_3(g)$$
,  $K_P = 1.7 \times 10^{12}$  at 300 K.

Calculate K<sub>p</sub> for the following reactions at 300K

• 
$$SO_3(g) \rightarrow SO_2(g) + 1/2O_2(g)$$

• 
$$2SO_3(g) \rightarrow 2SO_2(g) + O_2(g)$$

• 
$$2SO_2(g) + O_2(g) \rightarrow 2SO_3(g)$$

### **Solution**

$$K_{P(i)} = \frac{p_{SO_2} \cdot p_{O_2}^{1/2}}{p_{SO_3}}$$

This is reverse of reaction (A). Therefore

$$K_{P(i)} = \frac{1}{K_P} = \frac{1}{1.7 \times 10^{12}} = 0.588 \times 10^{-12}$$

Consider reaction (ii). This equation has been obtained when equation (i) is multiplied by 2. Therefore

$$K_{P(ii)} = \frac{p_{SO_2}^2 p_{O_2}}{p_{SO_3}^2} = KP_{(i)}^2 = 0.334 \times 10^{-24}$$

For reaction (iii)

$$K_{P(iii)} = \frac{p_{SO_3}^2}{p_{SO_2}^2 \cdot p_{O_2}} = K_p^2 = \frac{1}{K_{P(i)}^2} = \frac{1}{K_{P(ii)}}$$
  
= 2.89 × 10<sup>24</sup>.



## Illustration (Problem 13.13)

The following reaction reaches equilibrium at 350°C and 3 bar:

$$CH_3CHO(g) + H_2(g) \rightarrow C_2H_5OH(g)$$

If the system initially contains 1.5 mol H2 and 1 mol of acetaldehyde, what is the composition of the system at equilibrium? What would be the effect of reducing the pressure to 1 bar? Assume ideal gases.

### **Solution**

p4

Κ

ΔG T

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| ΔG_298.15K | -39630J/ma  | οl |
|------------|-------------|----|
| ΔH_298.15K | -68910J/ma  | οl |
| Cp/R       |             |    |
| ΔΑ         | -1.424      |    |
| ΔΒ         | 0.001601    |    |
| ΔC         | 0.00000146  | _  |
| ΔD         | -8300       |    |
| Т          | 623.15 K    |    |
| Р          | 3 bar       | H  |
|            |             |    |
| p1         | 11.81207616 |    |
| p2         | -13.3008572 |    |
| р3         | -0.36451219 |    |

-0.54357444

-1.30971878

3.705131616

$$-\ln K = \frac{\Delta G^{o}(T)}{RT} = \frac{\Delta G_{0}^{o} - \Delta H_{0}^{o}(T = 25^{\circ}C)}{RT_{0}}$$

$$+ \frac{\Delta H_{0}^{o}}{RT} + \frac{1}{T} \int_{T_{0}}^{T} \frac{\Delta C_{P}^{o}}{R} dT - \int_{T_{0}}^{T} \frac{\Delta C_{P}^{o}}{R} \frac{dT}{T}$$

$$-\ln K = P1 + P2 + p3 - p4$$