

Rethinking the analysis.

18/12/22

So zero crossings points move as a function of speed.

lets assume we have 14 poles therefore $\frac{14}{2} \cdot 6 = 36$

zero crossing. 360° in 1 electrical cycle, 7 electrical cycles per mechanical cycle. Thus if the encoder & the motor shaft are calibrated such that 0° from the encoder is 0° in terms of electrical cycles then we could easily know the zero crossing points (ideal) but the real zero-crossing points are a function of speed (voltage supply changes)

To know the real points we can just do this from geometry, we need to convert from encoder values to electrical angle.

Assuming the encoder gives us 2^{14} bit values,

we can convert from encoder step to mechanical angle:

$$\frac{\text{encoder-step}}{2^{14}} \cdot 360^\circ_{\text{mech}} = \alpha_{\text{mech}}^\circ$$

$\alpha_{\text{mech}}^\circ$ goes from $0 \rightarrow 359^\circ$ before looping, by this point we would have gone through 7 electrical cycles.

So a full electrical cycle of $0 \rightarrow 359^\circ$ elctric every

$$360^\circ / 7 = 51.428^\circ_{\text{electrical}}$$

A $360^\circ_{\text{elctric}}$ is a transition from "north", "south", "north" a 6 pole motor has 3 south & 3 north poles so for a full electrical cycles the shaft has rotated $\frac{360}{(6/2)} = \frac{360}{3} = 120^\circ$ mechanical degrees, for a 14 pole motor $\frac{360}{2} = 51.428^\circ_{\text{mech}}$

$$\frac{6 \times \text{pdes}}{2} = 3 \times \text{pdes} \quad 42 \text{ zero crossings for } 14$$

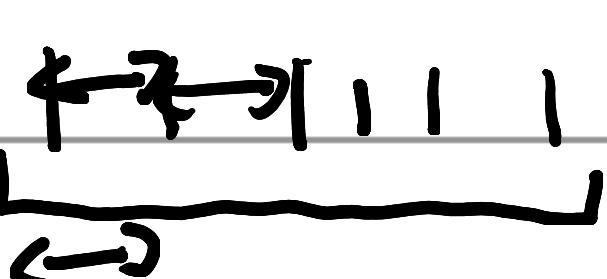
poles. So for 360° mechanical we could have

$$\frac{360^\circ \text{ mech}}{\text{zero crossings}} = \frac{360^\circ \text{ mech}}{3 \times \text{pdes}} \text{ in reverse} \quad \frac{360^\circ \text{ mech}}{42}$$

$= 8.78^\circ$ mechanical deg per zero crossing.

$$\frac{360^\circ}{6 \text{ electrical revs}} = 60^\circ$$

$$360^\circ \text{ elect}$$



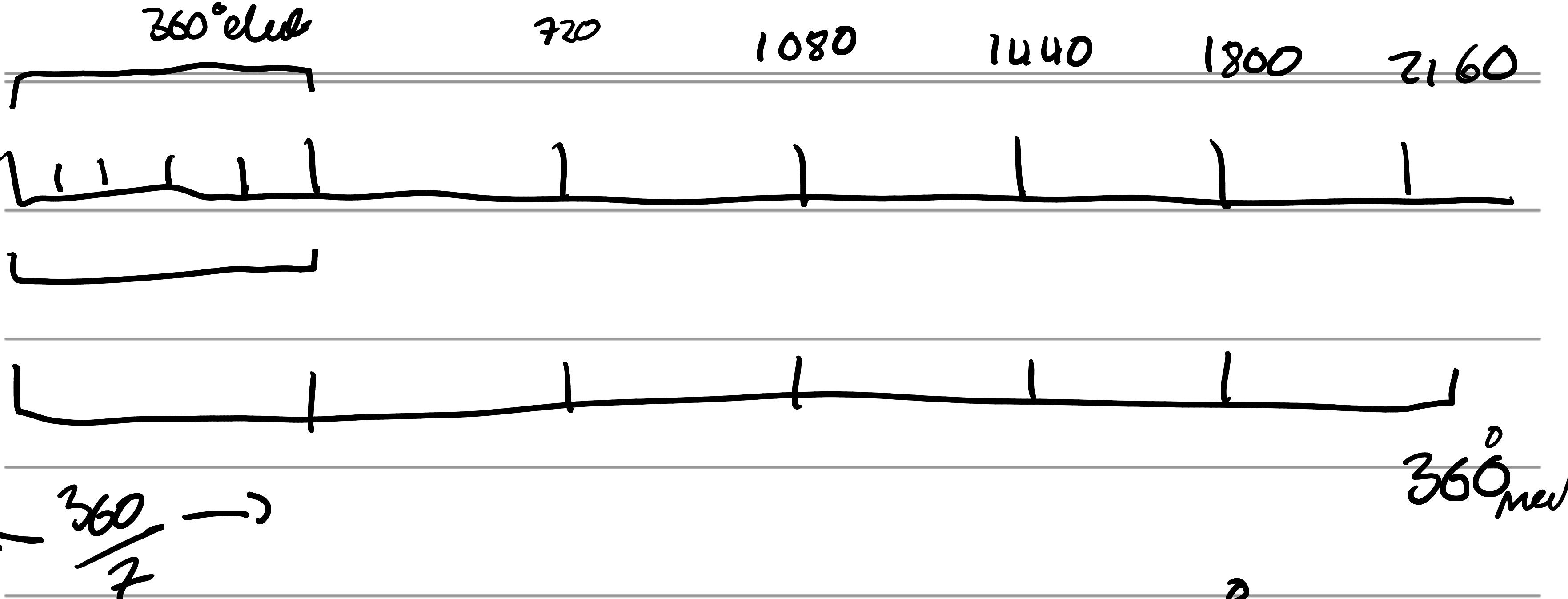
$$8.58^\circ \text{ mech} \quad 51.42^\circ \text{ mech}$$

$$360^\circ \text{ mech}$$

It would be good to convert $^\circ$ mech to $^\circ$ electrical

$$\text{elect} = \frac{(\text{mech}^\circ \times \text{pdes})}{(\text{phases} \times 2)} = \frac{\text{mech}^\circ \times \text{pdes}}{\text{phases} \times 2} = \frac{1^\circ \times 14}{3 \times 2} = \frac{7}{3} \text{ mech}^\circ$$

check $8.58^\circ \text{ mech} \rightarrow 39.999 \text{ electrical?}$ should be 60



$\leftarrow \frac{360}{7} \rightarrow$

51.42

$$1 \text{ electrical cycle} = \frac{360^\circ \text{ mech}}{(p_{des}/2)}$$

$$360^\circ \text{ electrical} = \frac{360^\circ \text{ mech}}{(p_{des}/2)}$$

$$\therefore 1^\circ \text{ electrical} = 1^\circ \text{ mechanical} \times \frac{2}{\text{poles}}$$

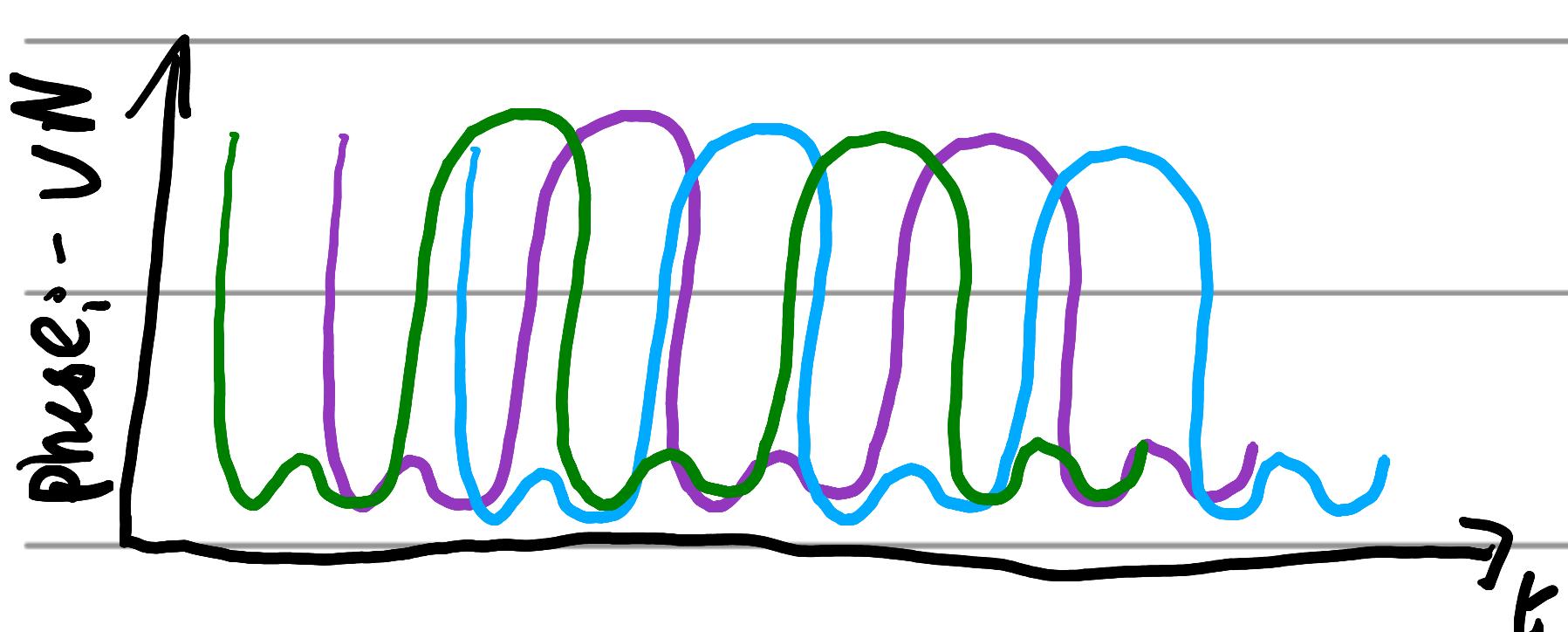
think 360° electrical should be 51.42°_{mech} ✓

or

$$1^\circ \text{ electrical} = 1^\circ \text{ mech} \times \frac{\text{Pdes}}{2 \cdot \text{phases}}$$

clerk transformation?

To calibrate the motor/encoder system one must calibrate the encoder such that step 0 lines up with 0° electrical, that way 0° mech 0° elect. To do this one could take the voltage / encoder values, we already have:



Note this is somewhat problematic
(virtual natural)

the ADC phase; - V_n signals
are not simple sine waves as the ADC only measures the voltages
thus half of the waveform for phase; is cut off... it leads
to a periodic pattern, but not a simple sinusoid.

When we start calibration the encoder angle is random vs
the motors 0° shaft angle, we will need to find the offset.

We will need to fit some model to the recorded data & the

use such a model & to calculate optimal values for the parameters

for angular displacement offset & the current displacement between the

3 phases (in an ideal world should be 120°).

To start with we need a model, now we know the function is periodic our model will generate the phase currents ($A-U_n, B-U_n, C-U_n$) from encoder position, angular offset (displacement of encoder from ideal shaft position) & phase current displacement (ideally 120°).

The closest model we know for the phase currents is something like

$$\text{current-}a = \sin(\text{angular-position} + \text{angular-displacement})$$

$$-b = \sin(\text{angular-position} + \text{angular-displacement} + \text{phase-current-displacement})$$

$$-c = \sin(\text{angular-pos} + \text{angular-disp} + 2 \times \text{phase-current-disp})$$

but the amplitude will not be 1 & the function is periodic but not a simple sin wave. One could do a series expansion (Fourier)

I model the system as a sum of sine waves with some number of coefficients which we could call the Fourier coefficients thus we could obtain for some number coefficients & thus our

$f(\text{angular-pos}, \text{phase-disp}, \text{coefficients}) \xrightarrow{\text{Fourier}} \text{currents}$

for i , current in coefficients:

$$\text{plus-d } t = (\text{coefficient} \times \sin((i+1) \times \text{angular-pos}))$$

$$-b + = (\text{coefficient} \times \sin((i+1) \times (\text{angular-pos} + \text{phase-disp})))$$

$$-c - = (\text{coefficient} \times \sin((i+1) \times (\text{angular-pos} + 2 \times \text{phase-disp})))$$

Then using some curve-fitting function it could shift the quantified phase currents by the angular-position & optimising the phase displacement like angular-disp & Fourier coefficients until the model fits the data..

at this point we will have some good approximation of the model coefficients.

Now with coefficients we can create a new model & optimise one final time this time keeping the coefficients constant & optimising only for the angular-disp & phase-disp.

Furier

f (cyclic-pos, cyclic-dsp, phase-dsp, coefficients) \rightarrow current data
FIXED!

for coefficient in furier-coefficients

$$\text{phase-a-current} += \text{coefficient} \times \sin((i+1) \times (\text{cyclic-pos} + \text{cyclic-dsp}))$$

$$-b- += \text{coefficient} \times \sin(i+1) \times \text{cyclic-pos} + \text{cyclic-dsp} + \text{phase-dsp}^3)$$

$$-c- += (\text{coefficient} \times \sin(i+1) \times \text{cyclic-pos} + \text{cyclic-dsp} + 2 \times \text{phase-dsp})$$

The optimised cyclic-dsp will then represent the offset & the phase-dsp represents the ideal phase current drop (this accounts better for errors & manufacturing defects of the motor, away from 180° separation)

If the optimisation fitting function generates a covariance matrix then the diagonal elements can be summed with a trace,

over the variances of the estimated errors. $\sqrt{\text{trace}(\text{cov})}$ would be the errors for the optimised parameters.

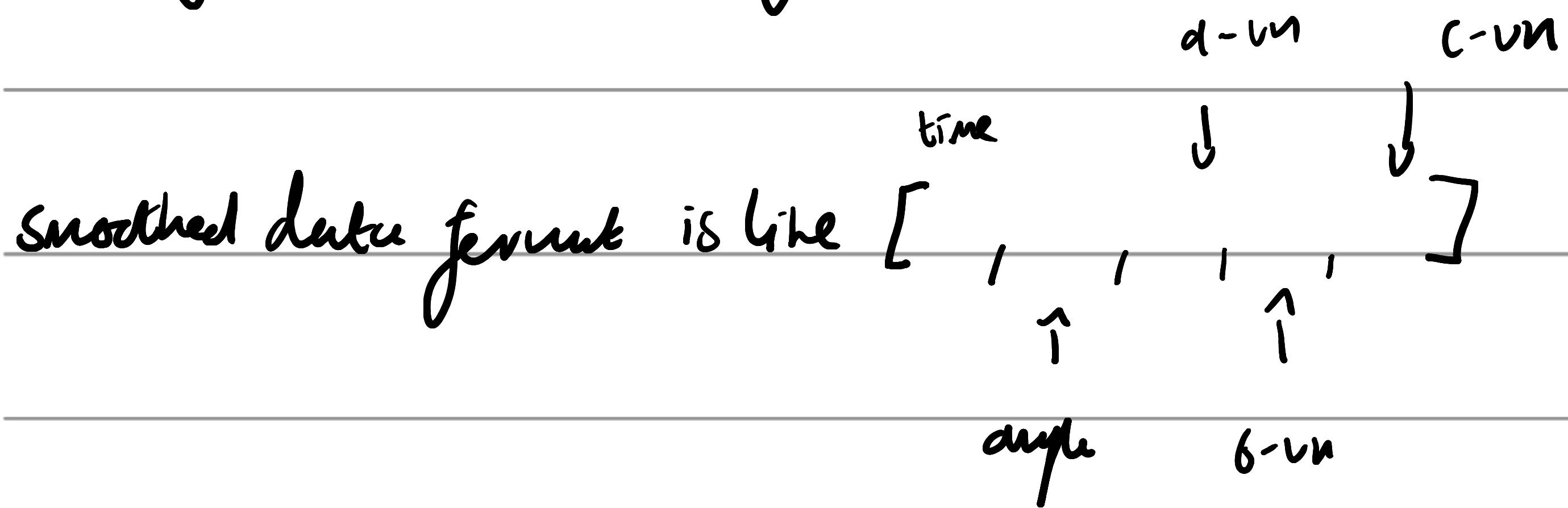
To make sure the model & fit are sensible, it would be a good idea to display a graph of the model & the experimental data points & make sure the fit looks sensible.

Artifacts / bad runs from the system would have a-periodic issues that could ruin the fitting system. (would be reflected in the errors)

5/1/23

Finally have a new working laptop so can continue project
laptop powersupply failed.

Looking at alternative fitting method.



13/11/23

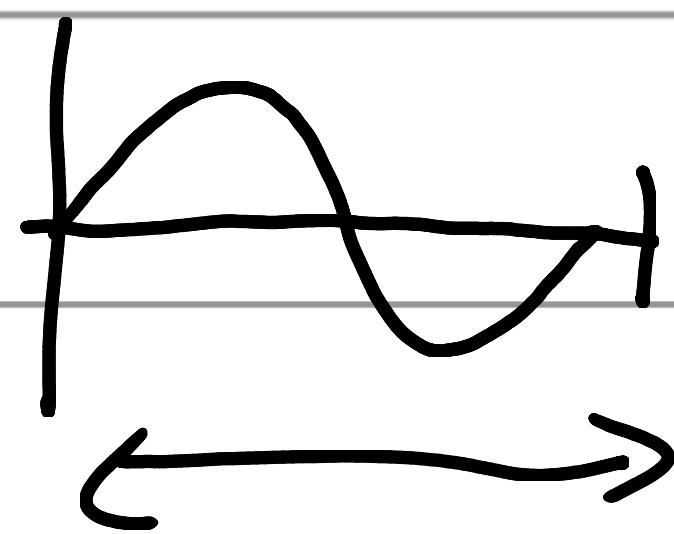
So wrote analysis-test 3, initial results frequency of sin waves over angular period is wrong, model does not account for # poles.

Think about it 3 phases, $\frac{\text{Poles}}{2} \times 6$

$$\frac{14}{2} \times 6 = 7 \times 6 = 42$$

42 crosses for 3 phases $\frac{42}{3} = 14$ zero's per angular period

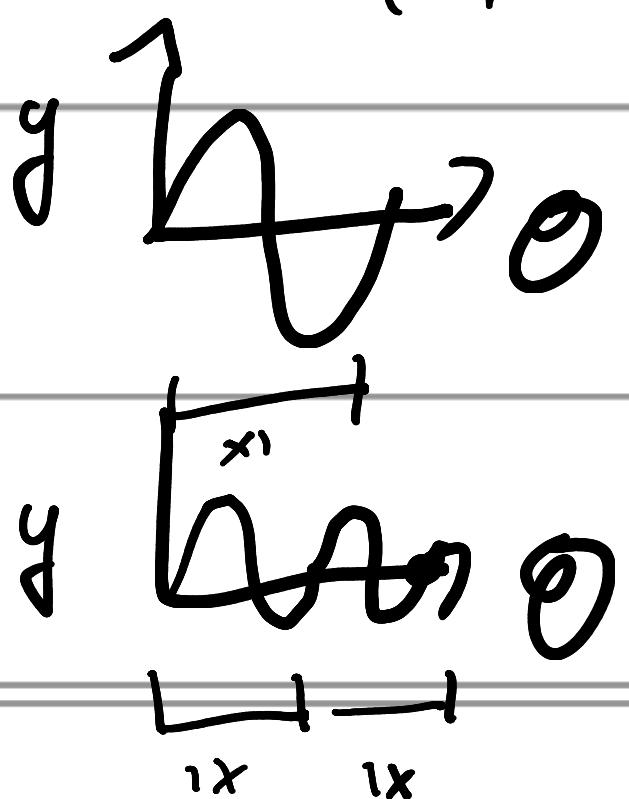
or $\frac{\text{Poles}}{2} \times 6 \dots \frac{\text{poles} \times 3}{\text{phases}} \text{ zero's per phase}$



1 period in 360°

How many electrical cycles per angular cycle? 6 steps $7 \left(\frac{\text{Poles}}{2} \right)$ cycles

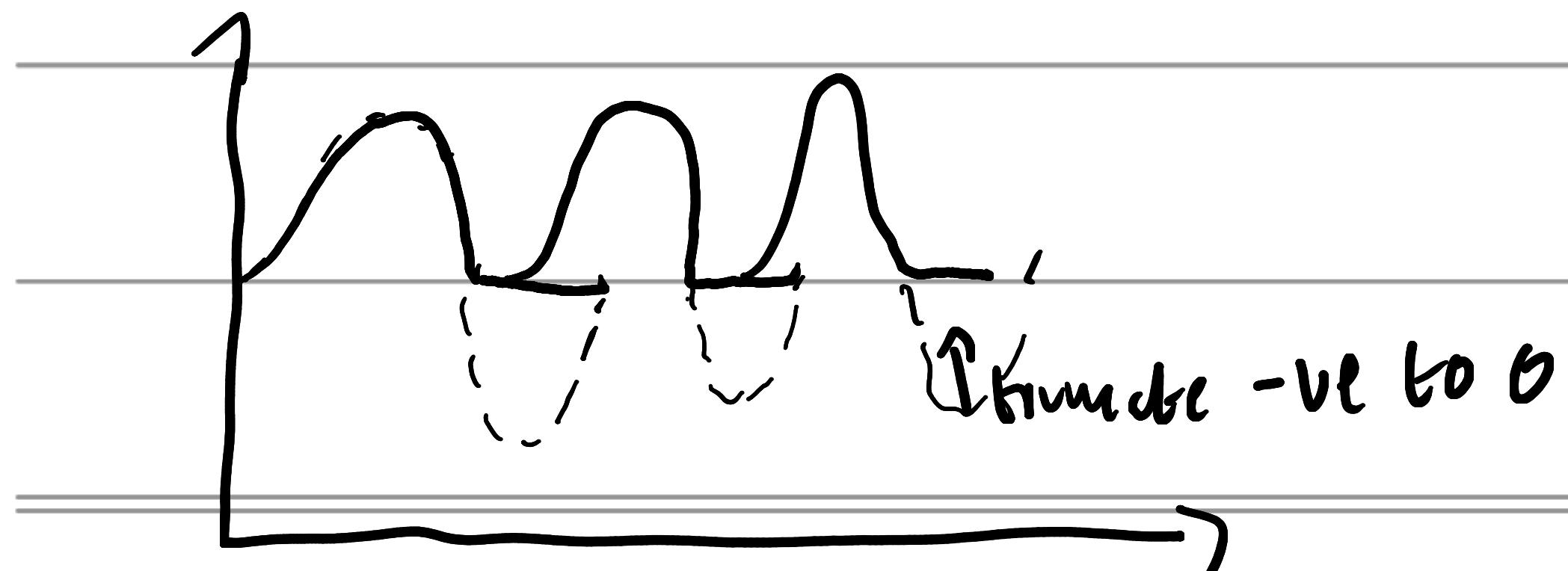
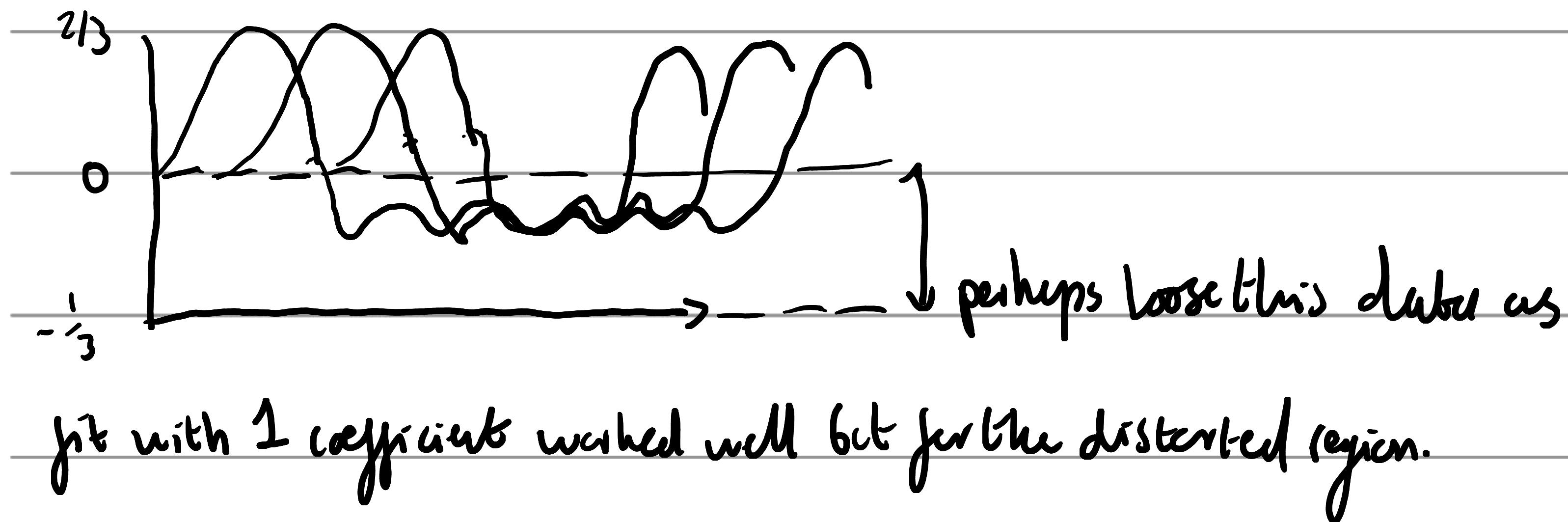
$$y = A \sin \frac{2\pi}{\kappa} \theta$$



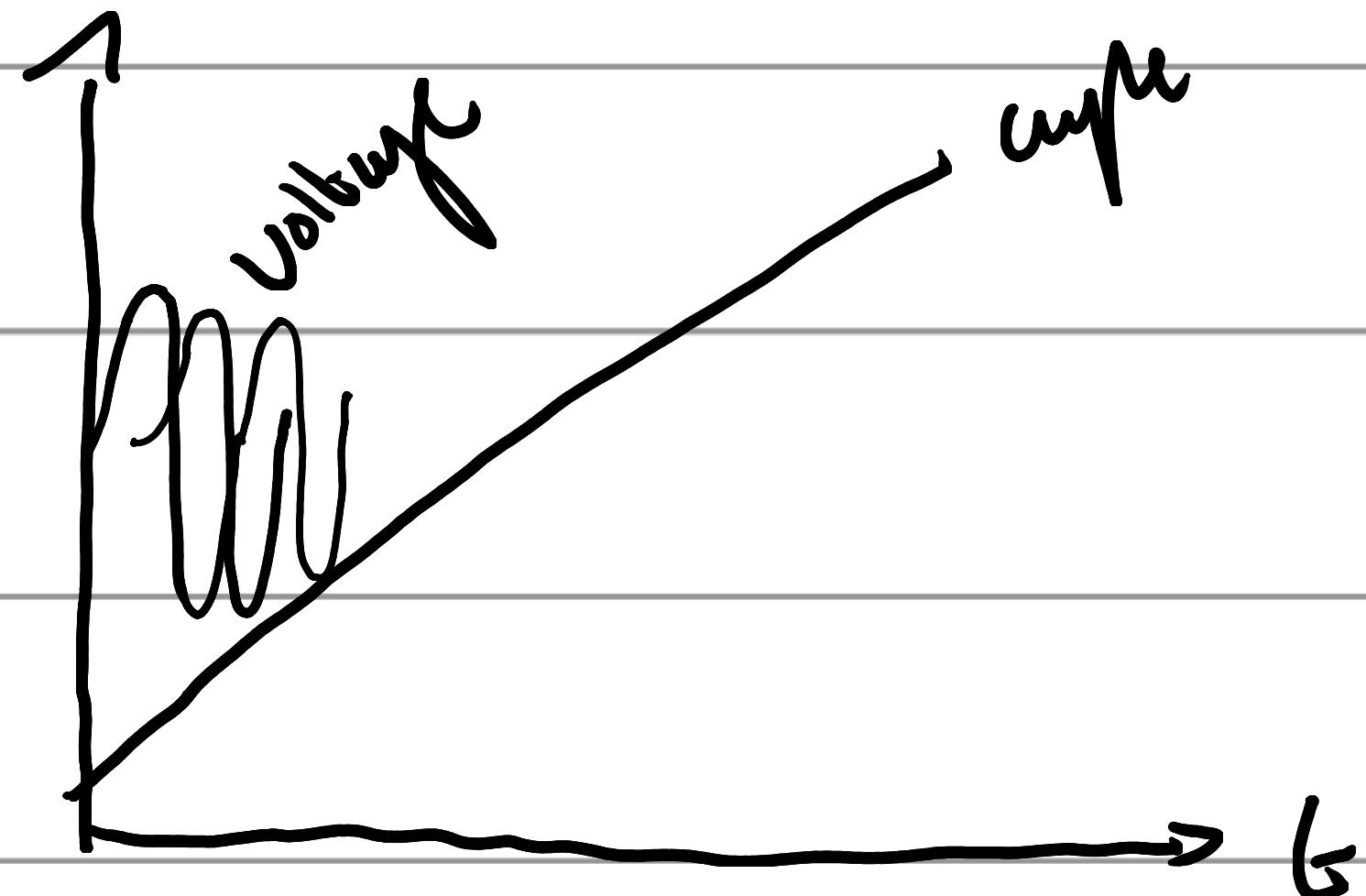
so each needs 7 periods
within each 360° mech
 $2\pi^\circ$ mech

Model fitting results:

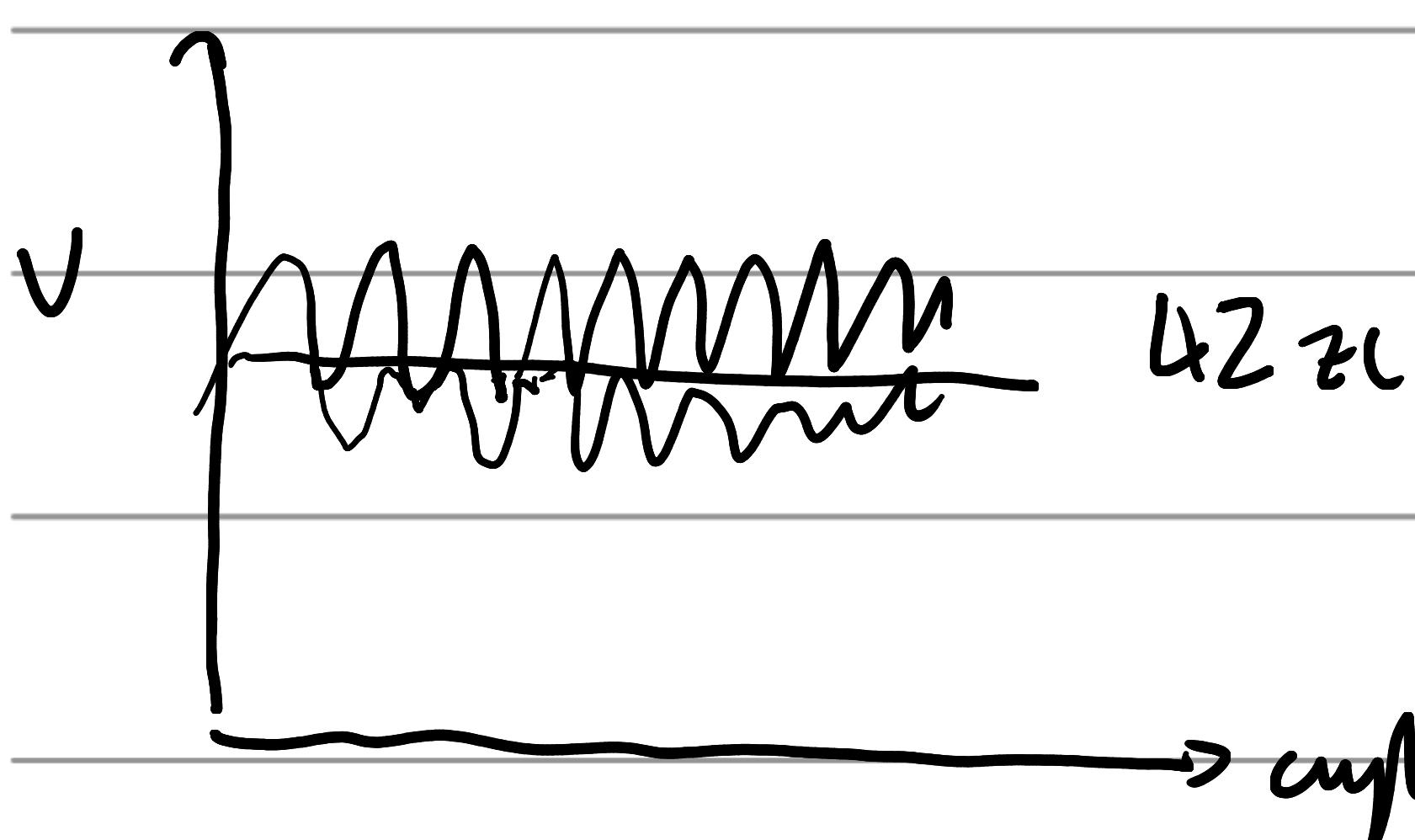
So the Fourier idea didn't pan out so well, fit is best with a single coefficient. Perhaps adding a lot of coefficients would eventually work but the single coefficient fit is very slow. If I wish to continue the perhaps looking at a GPU fitting library. The other alternative is to create a bespoke filter for the fit data to exclude -ve results:



Another question is if switching points are really a function of speed.



I agree that as a function of time, the frequency would change



But if we have it in terms of cycles dependent although the rate at which cycles would be swept through would inverse the voltage frequency per cycle sweep might not.

Next to try would be remove the -ve data, or where all the phase ABCC are near zero. Filter this data & attempt to fit the curves.

16/11/23

(chopped off all -ve (phase $X_i - V_n$) values. Fit yields

239.96 ± 1.0 phase current displacement $\ell - 27.17 \pm 1.03^\circ$

angular-shape displacement. Data was from a counter clockwise
run sept-x-ccw, phase current of ~ 240 mches sense as

fit was against CW model, ℓ a phase current displacement

of 240 swaps the order from black, yellow, red (cw)
 $a \quad b \quad c$

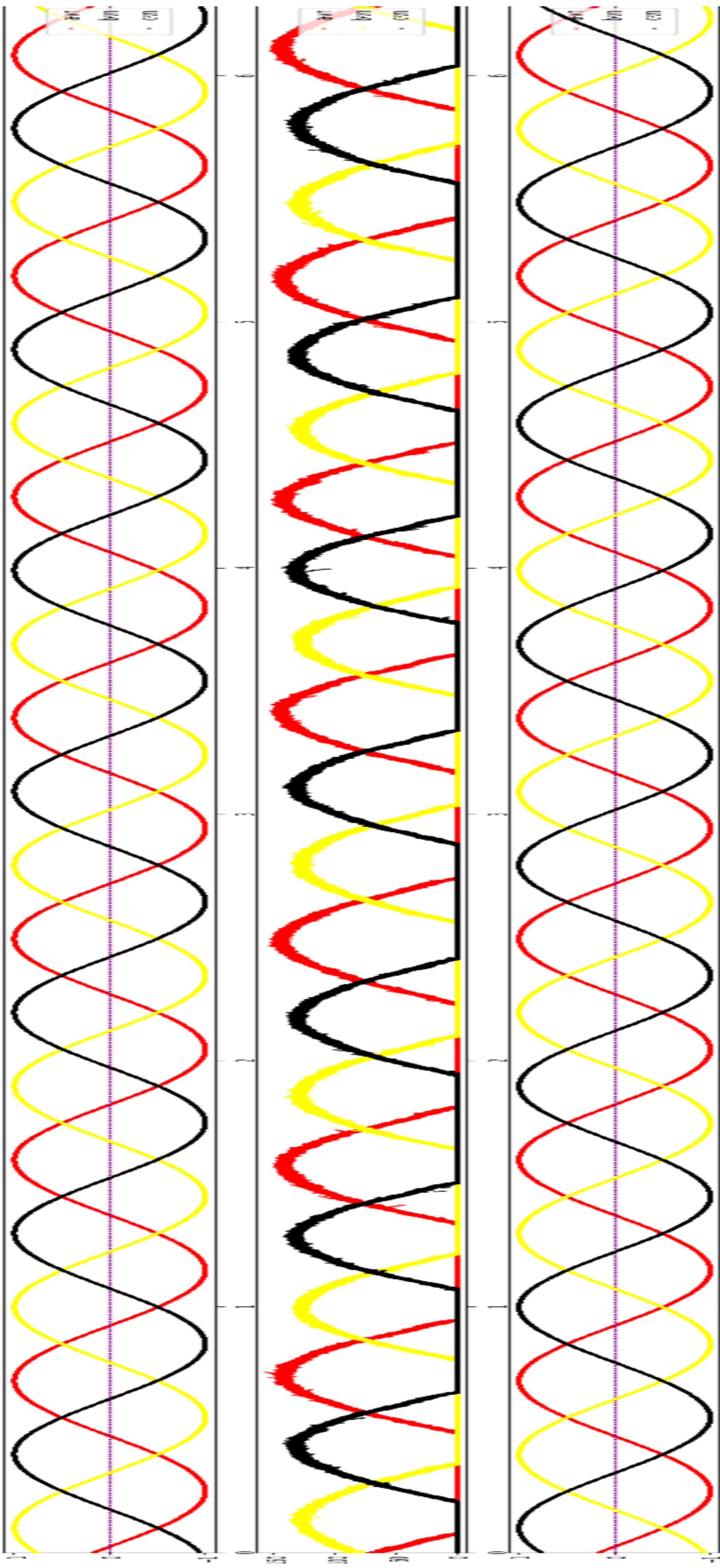
to red, yellow, black (ccw) while still maintaining a 120°

separation

$$0^\circ + 240^\circ$$

$$240^\circ + 240^\circ = 480^\circ / 360 = 120^\circ$$

Parameters:
alpha [type=1111111111111111]
beta [type=1111111111111111]



Tried sept-2-cw & sept-4-cw

$$d-d = -2.4 \pm 1$$

$$\downarrow$$
$$d-d = -2.4 \pm 1$$

$$p-c-d = 137.1 \pm 0.9$$

$$p-c-d = 137.1 \pm 0.8$$

hm ... this makes much less sense, each cw run is consistent

& quite far from 120° , angular displacement disagree for cw & ccw!

Need to rethink the model maybe? Not sure what to conclude.

cw pattern

→ direction
in graph

A B C

R, Y, B

ccw pattern

← direction
in graph

A C B

R B Y

← direction
in graph

A C B

R, B, Y

→ direction
in graph

A B C

R Y B

See if cycle repeats

clearly in point

and cheap start! stick on
to end of plot... is it continuous?

17/11/23

Thinking about old analysis, could use zc data & try to fit a model to the limited data. Need to do data recovery on the dd disk. The combined reports attempted had an average between them. Could try & extract state maps generated from the h5mt files

Name disk is a M.2 NVMe 2280 (SIE 3.0) ^(ben) x4

File under S10. Ordered an adaptor.

M key S

28/11/23

Recovered data successfully.

Things to do 1 → Implement FSC assuming analysis 1 is correct, 2 → export binary spike train data.

lets do 2) :

- Reinstall project dir on new laptop.
- update project packages.
- re run analysis - all works
- Need to adapt code to export a JSON file of the ZC data (binary sprite brain)
- New mem / new scd

process is take new-mean... get ordered 1kv list,
for each channel filters 1kv list of rising/falling edges & store
in 3 lists 2 for each channel, convert into kv map. Next
of each list of rising/falling get pairs of item i & i+1,
for each pair find midpoint & emit 3 entries
(channel-name, value^{+1.0/-1.0%}, cycle value) do this
for the first, midpoint & second. (do it these for all)

channels & gotten & order. At this point we have not just ZC values but max & min values. Finally we can process the filtered list & collect a npy of data $\{a_{\text{yles}}:[], a:[], f:[], c:[]\}$ & errors $\{a:[], b:[], c:[]\}$ errors are taken as 1.0 channel where we have a ZC or a midpoint, if we had to pad a zero for the remaining channels then the error is taken as infinity

Next steps... could take the combined id or just the folder run names, combine all data for all runs, chop off -ve data... fit curve... compare Z methods.

26/11/23

Before I try & fit the covariance Kalman condition with a model I need to revisit work yesterday.

The ZC analyser only detects ZC events in the +ve cycler (cw) direction. So to fit for (ccw (-ve) cycler direction we need to flip rising to falling & refit.

Works ok by reversing cw duba to form ccw duba. Fit with 240° initial is very close 239.99 for both if 120° initial we get 137.13° for both.

Now reverse analysis for all these runs & fit use the raw kulman voltage duba merge & flip!

Done, with drop (plus) 240 get somewhat similar fit params, visually very similar & consistent.

27/11/23

Main files analysis - raw - recursive.py

Other main analysis analysis - zc - recursive

For combined runs would be nice to just stick
to the id file convention, change the code in repeat
to always generate an id file.

Reports should be able to generate a file with
a chosen name (single) (title, file-name, file-pattern
, run-ids)

Combined reports should be given a file name
pattern & the code should produce an id

Tested to work with 2 args, working with 3 args!

Tested & download zc & run fitting.

Next need to check stube map as in ccw rising

should be seen as falling edges vice versa

| Counter-clockwise rotation (-ve) | | | | | | clockwise rotation (+ve) | | | | | | | |
|----------------------------------|---|---|---|---|---|--------------------------|---------|---|---|---|---|---|---|
| | 5 | 4 | 3 | 2 | 1 | 0 | | 0 | 1 | 2 | 3 | 4 | 5 |
| ESC | C | C | B | B | A | A | IN | A | A | B | B | C | C |
| IN | B | A | A | C | C | B | SD | B | C | C | A | A | B |
| SD | X | X | C | X | B | X | RISING | C | X | A | X | B | X |
| RISING | X | B | X | A | X | C | PULLING | X | B | X | C | X | A |
| PULLING | | | | | | | | | | | | | |

This is expected to trigger this state

Rising / Falling indicates the NEXT expected edge.

| | | | | | |
|---|---|---|---|---|---|
| 0 | 1 | 2 | 3 | 4 | 5 |
| A | A | B | B | C | C |
| B | C | C | A | A | B |

For each direction there are 6 total steps

So CCW sequence

| Step Fall | 5 4 3 2 10 | (w seq) | Step Rise Fall |
|--------------|-------------|---------|-------------------|
| ↑ ↓ ↑ ↓ ↑ ↓ | | | ↑ ↓ ↑ ↓ ↓ |
| phase detect | A B C A B C | | C B A C B A |

Phase detect

CW checks out.

100

A↑

- 4

But we should

1

-75

Hip rising following
deceleration.

create - bi-directional - state-cycle-map is the function which derives its state from function channel-name-and-direction

| | Counter-clockwise rotation (-ve) | | | | | |
|---------|--|---|---|---|---|---|
| ESC | 5 | 4 | 3 | 2 | 1 | 0 |
| IN | C | C | B | B | A | A |
| SD | B | A | A | C | C | B |
| RISING | A | X | C | X | B | X |
| FALLING | X | B | X | A | X | C |
| | This is expected to trigger this state | | | | | |
| | 5 | 4 | 3 | 2 | 1 | 0 |

so this needs correcting a ZC
detector always goes in
CW direction & thus sees
 $A \uparrow$ as $A \downarrow$.

CORRECTED

| | Counter-clockwise rotation (-ve) | | | | | |
|---------|--|---|---|---|---|---|
| ESC | 5 | 4 | 3 | 2 | 1 | 0 |
| IN | C | C | B | B | A | A |
| SD | B | A | A | C | C | B |
| RISING | X | B | X | A | X | C |
| FALLING | A | X | C | X | B | X |
| | This is expected to trigger this state | | | | | |
| | 5 | 4 | 3 | 2 | 1 | 0 |

- $A \uparrow \rightarrow 1$ 2
- $A \downarrow \rightarrow 4$ 5
- $B \uparrow \rightarrow 3$ 4
- $B \downarrow \rightarrow 0$ 1
- $C \uparrow \rightarrow 5$ 6
- $C \downarrow \rightarrow 2$ 3

Re check ccw post analysis
as on cubics Translated (flipped) (strike up) we get should have

$A \uparrow \dots A \downarrow$

0

1

$A \downarrow \dots A \uparrow$

3

2

we need

| | ccw |
|----------------|-----|
| $A \uparrow$ | 3 |
| $A \downarrow$ | 0 |
| $B \uparrow$ | 5 |
| $B \downarrow$ | 2 |
| $C \uparrow$ | 1 |
| $C \downarrow$ | 4 |

values in map logic

ult veget

| | ccw | white in logic | weights |
|----------------|-----|----------------|---------|
| $A \uparrow$ | 1 | 6 | 1 |
| $A \downarrow$ | 4 | 3 | 4 |
| $B \uparrow$ | 3 | 2 | 3 |
| $B \downarrow$ | 0 | 5 | 0 |
| $C \uparrow$ | 5 | 4 | 7 |
| $C \downarrow$ | 2 | 1 | 2 |

we get 1 more

changes applied... retaining

Counter-clockwise rotation (-ve)

| | 5 | 4 | 3 | 2 | 1 | 0 |
|---------|---|---|---|---|---|---|
| ESC | | | | | | |
| IN | C | C | B | B | A | A |
| SD | B | A | A | C | C | B |
| RISING | A | X | C | X | B | X |
| FALLING | X | B | X | A | X | C |

This is expected to trigger this state

S 4 3 2 1 0

Remember when reading of
the chart to inverse interpretation
of rising / falling when going
CLW

check above

A ↑ looking for A↑ in const up

A ↓ A↑ in ccw state

B ↑ B↓ in const state

B ↓ B↑ in ccw state

C ↑ C↓ in const state

C ↓ C↑ in ccw state

4 ✓

1 ✓

0 ✓

3 ✓

2 ✓

5 ✓

checks out.

Added dark theme.