

MORTAR-BASED ENTROPY STABLE DISCONTINUOUS GALERKIN METHODS

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1. Introduction. Boilerplate introduction on high order + stability

2. Mortar methods for hybrid and non-conforming meshes. This work is motivated by complications which arise when designing entropy stable couplings between elements which do not share the same boundary nodes. This can arise, for example, for hybrid and non-conforming meshes.

Hybrid meshes: It was shown in [1] that an entropy stable

Non-conforming meshes. On conforming meshes, it is most efficient to utilize both Gauss quadrature for volume integrals and Gauss quadrature for face or surface integrals. For solutions represented in terms of their values at tensor product volume Gauss nodes, extrapolation to face Gauss nodes can be done in an efficient line-by-line manner using one-dimensional interpolation matrices.

For non-conforming meshes, it can be advantageous to use composite Gauss quadratures on non-conforming interfaces. [Reference JK and LCW's paper on full-side vs split side mortars.](#) However, interpolating the solution at volume Gauss nodes to split-side Gauss nodes is no longer a one-dimensional operation.

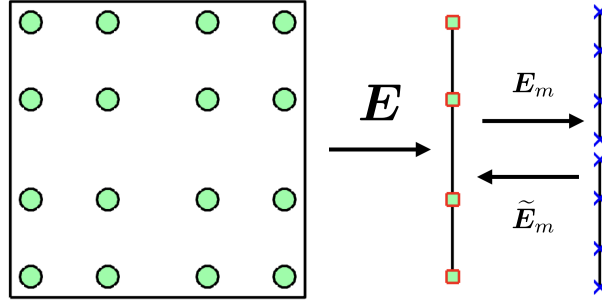


Fig. 1: Illustration of mortar operators. The matrix E maps from volume quadrature points to surface quadrature points, E_m maps from surface to mortar surface points, and \tilde{E}_m maps from mortar surface points to surface points.

3. Mortar formulation. Let V_q and V_f denote interpolation matrices which evaluate at volume and surface quadrature points, respectively, and let W, W_f denote diagonal matrices whose entries consist of volume and surface quadrature weights

[add defs of matrices](#)

Let $E = V_f P_q$ denote the polynomial mapping which extrapolates values from volume quadrature points to values at surface quadrature points. We also define B_i as the diagonal matrix containing products of quadrature weights and the i th component of the outward normal vector \hat{n}_i

$$B_i = W_f \text{diag}(\hat{n}_i).$$

28 An entropy stable skew-symmetric formulation can be given on the reference
 29 element \hat{D} as follows:

$$30 \quad M \frac{d\mathbf{u}_N}{dt} + \begin{bmatrix} \mathbf{V}_q \\ \mathbf{V}_f \end{bmatrix}^T \left(\begin{bmatrix} \mathbf{Q}_i - \mathbf{Q}_i^T & \mathbf{E}^T \mathbf{B}_i \\ -\mathbf{B}_i \mathbf{E} & \mathbf{0} \end{bmatrix} \circ \mathbf{F}_S \right) \mathbf{1} + \mathbf{V}_f^T \mathbf{B}_i \mathbf{f}_i^* = 0.$$

31 We incorporate mortars by modifying this formulation. Let \mathbf{V}_m denote the matrix
 32 which maps volume quadrature points to values at surface *mortar* points. We also
 33 need to introduce interpolation operators $\mathbf{T}_f, \mathbf{T}_m$ for surface trace spaces. Here, \mathbf{T}_f
 34 maps from polynomials on the surface $\partial\hat{D}$ to surface quadrature points, while \mathbf{T}_m
 35 maps from polynomials on $\partial\hat{D}$ to mortar quadrature points. We can then define
 36 surface and mortar mass and projection matrices

$$37 \quad \mathbf{M}_m = \mathbf{T}_m^T \mathbf{W}_m \mathbf{T}_m, \quad \mathbf{P}_m = \mathbf{M}_m^{-1} \mathbf{T}_m^T \mathbf{W}_m \\ 38 \quad \mathbf{M}_f = \mathbf{T}_f^T \mathbf{W}_f \mathbf{T}_f, \quad \mathbf{P}_f = \mathbf{M}_m^{-1} \mathbf{T}_f^T \mathbf{W}_f.$$

40 Note that we have used the mortar mass matrix \mathbf{M}_m in the above definition of the
 41 face projection. This is only necessary if the surface and mortar quadratures do not
 42 exactly integrate degree $2N$ polynomials. If both the surface and mortar quadratures
 43 are exact for polynomials of degree $2N$, then $\mathbf{M}_m = \mathbf{M}_f$, and no distinction is
 44 necessary between the two mass matrices.

45 *REMARK. In order to show stability, we require that both \mathbf{P}_f and \mathbf{P}_m are defined*
 46 *using the same mass matrix. We have used the mortar mass matrix \mathbf{M}_m here; how-*
 47 *ever, we could also use the surface mass matrix \mathbf{M}_f in both \mathbf{P}_f and \mathbf{P}_m . We use the*
 48 *mortar mass matrix in this work, as the mortar quadrature is generally more accu-*
 49 *rate than the surface quadrature for our use cases (e.g. hybrid and non-conforming*
 50 *meshes).*

51 We can now define operators which map between surface and mortar quadrature
 52 points. Let \mathbf{E}_f denote the map from surface to mortar points, and let $\tilde{\mathbf{E}}_f$ denote
 53 the map from mortar to surface points. Both operators are defined through an L^2
 54 projection to the trace space and interpolation to appropriate points

$$55 \quad \mathbf{E}_f = \mathbf{T}_m \mathbf{P}_f, \quad \tilde{\mathbf{E}}_f = \mathbf{T}_f \mathbf{P}_m.$$

56 We also define a mortar boundary matrix

$$57 \quad \tilde{\mathbf{B}}_i = \mathbf{W}_m \text{diag}(\hat{\mathbf{n}}_i).$$

58 Then, a mortar-based formulation can be given as follows:

$$59 \quad (1) \quad M \frac{d\mathbf{u}_N}{dt} + \begin{bmatrix} \mathbf{V}_q \\ \mathbf{V}_f \\ \mathbf{V}_m \end{bmatrix}^T \left(\begin{bmatrix} \mathbf{Q}_i - \mathbf{Q}_i^T & \mathbf{E}^T \mathbf{B}_i & \\ -\mathbf{B}_i \mathbf{E} & \mathbf{B}_i \tilde{\mathbf{E}}_f & \\ & -\tilde{\mathbf{B}}_i \mathbf{E}_f & \end{bmatrix} \circ \mathbf{F}_S \right) \mathbf{1} + \mathbf{V}_m^T \tilde{\mathbf{B}}_i \mathbf{f}_i^* = 0.$$

60 Here, we have appended an extra row and column to the decoupled SBP matrix, and
 61 the inter-element numerical flux \mathbf{f}^* is now computed in terms of the *mortar* nodes.

62 We first note that

$$63 \quad \mathbf{B}_i \tilde{\mathbf{E}}_f = \text{diag}(\mathbf{W}_f) \mathbf{T}_f \mathbf{P}_m = \text{diag}(\hat{\mathbf{n}}) \mathbf{W}_f \mathbf{T}_f \mathbf{M}_m^{-1} \mathbf{T}_m \mathbf{W}_m \\ 64 \quad = \mathbf{W}_f \mathbf{T}_f \mathbf{M}_m^{-1} \mathbf{T}_m^T \mathbf{W}_m \text{diag}(\hat{\mathbf{n}}_i) = \mathbf{P}_f^T \mathbf{T}_m^T \tilde{\mathbf{B}}_i = \left(\tilde{\mathbf{B}}_i \mathbf{E}_f \right)^T \\ 65$$

66 where we have used that \mathbf{W}_m is diagonal and that the outward normal $\hat{\mathbf{n}}_i$ on the
 67 reference element is constant over each face. This implies skew-symmetry of the
 68 decoupled SBP operator and entropy stability of the overall system.

69 **Finish**

4. A mortar-based implementation. While the formulation presented above is convenient for analysis, it is computationally expensive to implement. However, using properties of the mortar matrices $\mathbf{E}_f, \tilde{\mathbf{E}}_f$, we can rewrite the above formulation in a way which reflects a traditional mortar-based finite element implementation. In other words, we wish to implement (1) such that the only modification from the implementations in [2] is a pre-processing step on mortar faces.

We first note that, since \mathbf{E}_f maps from surface nodes to mortar nodes, $\mathbf{V}_m = \mathbf{E}_f \mathbf{V}_f$. Thus, we can rewrite the numerical flux contribution as

$$\begin{aligned} \mathbf{V}_m^T \tilde{\mathbf{B}}_i \mathbf{f}_i^* &= \mathbf{V}_f^T \mathbf{E}_f^T \mathbf{W}_m \text{diag}(\hat{\mathbf{n}}_i) \mathbf{f}_i^* = \mathbf{V}_f^T \mathbf{P}_f^T \mathbf{T}_m^T \mathbf{W}_m \text{diag}(\hat{\mathbf{n}}_i) \mathbf{f}_i^* \\ &= \mathbf{V}_f^T \mathbf{W}_f \text{diag}(\hat{\mathbf{n}}_i) \mathbf{T}_m \mathbf{M}_m^{-1} \mathbf{T}_m^T \mathbf{W}_m \mathbf{f}_i^* = \mathbf{V}_f^T \mathbf{B}_i \tilde{\mathbf{E}}_f \mathbf{f}_i^*. \end{aligned}$$

REFERENCES

- [1] Jesse Chan. Skew-symmetric entropy stable discontinuous Galerkin formulations. 2018. In preparation.
- [2] Jesse Chan. On discretely entropy conservative and entropy stable discontinuous Galerkin methods. *Journal of Computational Physics*, 362:346 – 374, 2018.