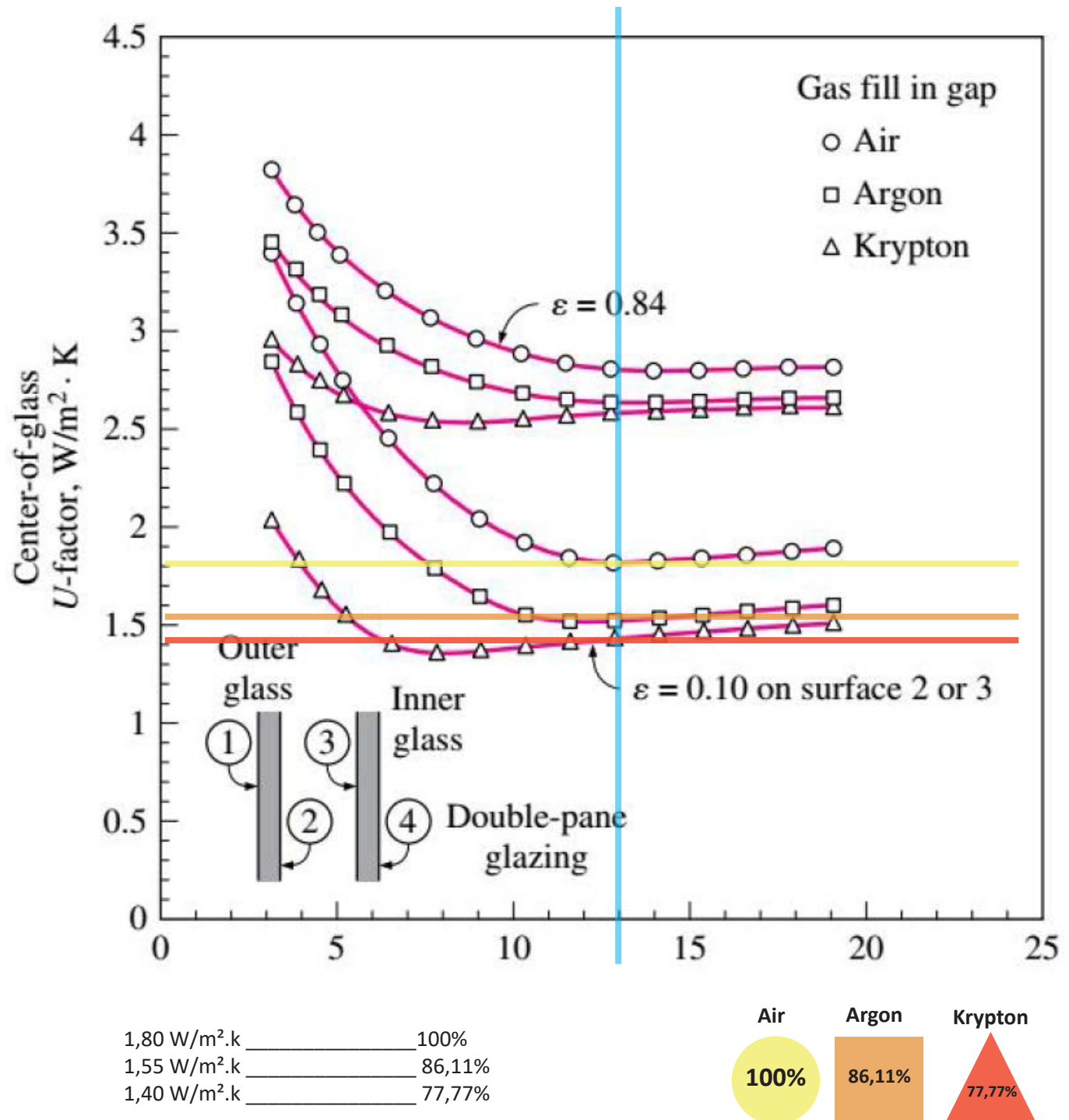


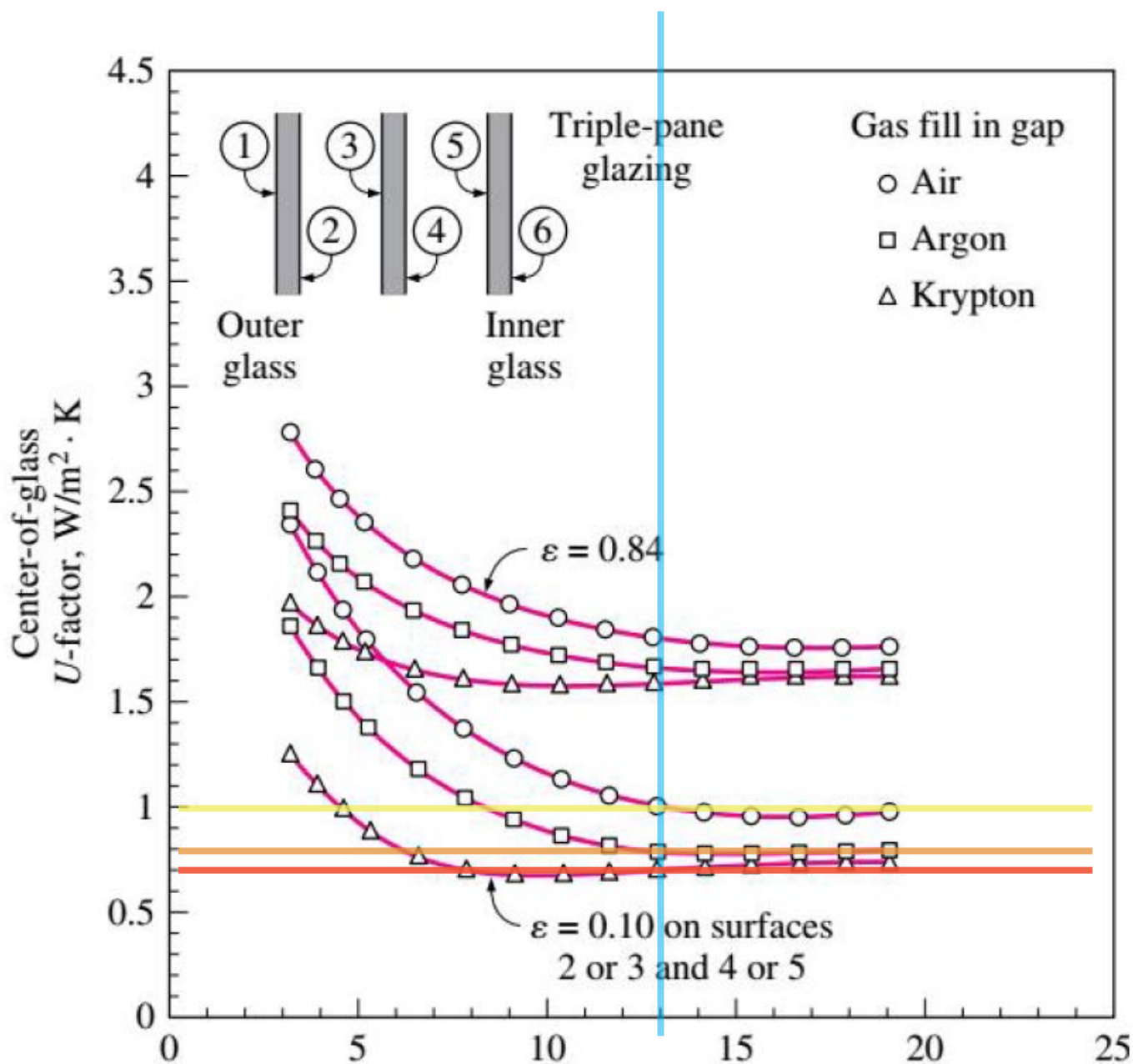
**Task 1.** Using the diagrams given in the presentation calculate how much (%) is the effect of applying different modifications (changing the gas, adding an extra panel, using a low emissivity coating) on the U value with respect to a benchmark case of double layer with air and no coating ? ( keep the gap thickness to be 13 mm)

### Study case changing the Gas

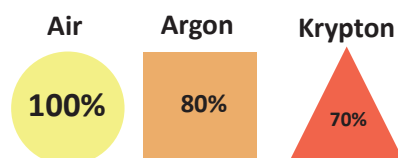


Changing the air for Argon improve the conditions in a 13,89%.  
Changing the air for Krypton improve the conditions in a 22,23%.

## Study case adding an extra panel



1,00  $W/m^2 \cdot k$  \_\_\_\_\_ 100%  
 0,80  $W/m^2 \cdot k$  \_\_\_\_\_ 80%  
 0,70  $W/m^2 \cdot k$  \_\_\_\_\_ 70%



Adding a extra panel in the case of Argon, respect to a triple panel fill with air, would improve the conditions in a 20%.

Adding a extra panel in the case of Krypton, respect to a triple panel fill with air, would improve the conditions in a 30%.

**Task 2.** Consider the house that we analysed in the last two examples, calculate the heating and cooling load of the other windows which are fixed 14.4 m<sup>2</sup> on the west, fixed 3.6 m<sup>2</sup> on the south and an operable 3.6 m<sup>2</sup> on the south (the same window and frame type). How much does the total value change if I change the frame of the window from wooden one to aluminium ?

#### Heating case A (fixed 14,40 m<sup>2</sup> on the west)

From the class example:  $\Delta T_{\text{heating}} = 24,8^{\circ}\text{C}$

$$U_{\text{windowwest}} = 2,84 \text{ W/m}^2 \cdot \text{K}$$

$$HF = U_{\text{windowwest}} \times \Delta T_{\text{heating}}$$

$$2,84 \text{ W/m}^2 \times 24,8^{\circ}\text{C}$$

$$70,43 \text{ W/m}^2$$

$$Q_{\text{windowwest}} = HF_{\text{windowwest}} \times A_{\text{windowwest}}$$

$$70,43 \text{ W/m}^2 \times 14,40 \text{ m}^2$$

$$1014,19 \text{ W}$$

Answer:

The heating value for the fixed window of 14,40m<sup>2</sup>, on the west is 1014,19W

#### Heating case B (fixed 3,60 m<sup>2</sup> on the south)

$$Q_{\text{windowssouth}} = HF_{\text{windowssouth}} \times A_{\text{windowssouth}}$$

$$70,43 \text{ W/m}^2 \times 3,60 \text{ m}^2$$

$$1014,19 \text{ W}$$

Answer:

The heating value for the fixed window of 3,60m<sup>2</sup>, on the south is 1014,19W

#### Heating case C (operable 3.6 m<sup>2</sup> on the south)

$$Q_{\text{windowssouth}} = HF_{\text{windowssouth}} \times A_{\text{windowssouth}}$$

$$70,43 \text{ W/m}^2 \times 3,60 \text{ m}^2$$

$$1014,19 \text{ W}$$

Answer:

The heating value for the operable window of 3,60m<sup>2</sup>, on the south is 1014,19W

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#### Cooling case A (fixed 14,40 m<sup>2</sup> on the west)

From the class example:  $\Delta T_{\text{cooling}} = 7,9^{\circ}\text{C}$

$$U_{\text{windowwest}} = 2,84 \text{ W/m}^2 \cdot \text{K}$$

$$HF = U_{\text{windowwest}} \times \Delta T_{\text{cooling}}$$

$$2,84 \text{ W/m}^2 \times 7,9^{\circ}\text{C}$$

$$22,43 \text{ W/m}^2$$

$$Q_{\text{windowwest}} = HF_{\text{windowwest}} \times A_{\text{windowwest}}$$

$$22,43 \text{ W/m}^2 \times 14,40 \text{ m}^2$$

$$322,99 \text{ W}$$

$$CF_{\text{windowwest}} = (U_{\text{windowwest}} \times (\Delta T - (0,46DR))) + (PXI \times SHGC \times IAC \times FFs)$$

$$2,84 \text{ W/m}^2 \cdot \text{C} \times (7,9^{\circ}\text{C} - 0,46 \times 11,90^{\circ}\text{C})$$

$$2,84 \text{ W/m}^2 \cdot \text{C} \times (7,9^{\circ}\text{C} - 5,47^{\circ}\text{C})$$

$$2,84 \text{ W/m}^2 \cdot \text{C} \times 2,43^{\circ}\text{C}$$

$$6,90 \text{ W/m}^2$$

$$(P_{XI} \times SHGC \times IAC \times FF_s) =$$

$$747 \times 0,54 \times 1 \times 0,56 =$$

$$225,89 \text{ W/m}^2$$

$$\text{Total CF} = 6,90 \text{ W/m}^2 + 225,89 \text{ W/m}^2 =$$

$$232,79 \text{ W/m}^2$$

$$\text{TOTAL Q} = CF_{\text{windowssouth}} \times A_{\text{windowssouth}}$$

$$232,79 \text{ W/m}^2 \times 14,40 \text{ m}^2 = 3352,17 \text{ W}$$

Answer:

The cooling value for the fixed window of 14,40m<sup>2</sup>, on the west is 3352,17W

### Cooling case B (fixed 3,60 m<sup>2</sup> on the south)

$$CF_{\text{windowssouth}} = (U_{\text{windowssouth}} \times (\Delta T - (0,46DR))) + (P_{XI} \times SHGC \times IAC \times FF_s)$$

$$2,84 \text{ W/m}^2 \cdot C \times (7,9^\circ\text{C} - 0,46 \times 11,90^\circ\text{C})$$

$$2,84 \text{ W/m}^2 \cdot C \times (7,9^\circ\text{C} - 5,47^\circ\text{C})$$

$$2,84 \text{ W/m}^2 \cdot C \times 2,43^\circ\text{C}$$

$$6,90 \text{ W/m}^2$$

$$(P_{XI} \times SHGC \times IAC \times FF_s) =$$

$$557 \times 0,46 \times 1 \times 0,47 =$$

$$120,20 \text{ W/m}^2$$

$$\text{Total CF} = 6,90 \text{ W/m}^2 + 120,20 \text{ W/m}^2 =$$

$$127,10 \text{ W/m}^2$$

$$\text{TOTAL Q} = CF_{\text{windowssouth}} \times A_{\text{windowssouth}}$$

$$127,10 \text{ W/m}^2 \times 3,60 \text{ m}^2 = 457,56 \text{ W}$$

Answer:

The cooling value for the fixed window of 3,60m<sup>2</sup>, on the south is 457,56W

### Cooling case C (operable 3.6 m<sup>2</sup> on the south)

$$U_{\text{windowssouth}} = 2,87 \text{ W/m}^2 \cdot K$$

$$HF = U_{\text{windowssouth}} \times \Delta T_{\text{cooling}}$$

$$2,87 \text{ W/m}^2 \times 7,9^\circ\text{C}$$

$$22,67 \text{ W/m}^2$$

$$Q_{\text{windowssouth}} = HF_{\text{windowssouth}} \times A_{\text{windowssouth}}$$

$$22,67 \text{ W/m}^2 \times 14,40 \text{ m}^2$$

$$326,44 \text{ W}$$

$$CF_{\text{windowssouth}} = (U_{\text{windowssouth}} \times (\Delta T - (0,46DR))) + (P_{XI} \times SHGC \times IAC \times FF_s)$$

$$2,87 \text{ W/m}^2 \cdot C \times (7,9^\circ\text{C} - 0,46 \times 11,90^\circ\text{C})$$

$$2,87 \text{ W/m}^2 \cdot C \times (7,9^\circ\text{C} - 5,47^\circ\text{C})$$

$$2,87 \text{ W/m}^2 \cdot C \times 2,43^\circ\text{C}$$

$$6,97 \text{ W/m}^2$$

$$(P_{XI} \times SHGC \times IAC \times FF_s) =$$

$$556 \times 0,46 \times 1 \times 0,47 =$$

$$120,20 \text{ W/m}^2$$

$$\text{Total CF} = 6,97 \text{ W/m}^2 + 120,20 \text{ W/m}^2 = 127,17 \text{ W/m}^2$$

$$\text{TOTAL Q} = CF_{\text{windowssouth}} \times A_{\text{windowssouth}}$$

$$127,17 \text{ W/m}^2 \times 3,60 \text{ m}^2 = 457,81 \text{ W}$$

Answer:

The cooling value for the operable window of 3,60m<sup>2</sup>, on the south is 457,81W

$$P_{XI_{\text{windowssouth}}} = ED + Ed = 559 + 188 = 747$$

$$SHGC = 0,54$$

$$IAC \text{ (we assume there are no shading)} = 1$$

$$FF_s = 0,56$$

$$P_{XI_{\text{windowssouth}}} = ED + Ed = 348 + 209 = 557$$

$$SHGC = 0,54$$

$$IAC \text{ (we assume there are no shading)} = 1$$

$$FF_s = 0,47$$

$$P_{XI_{\text{windowssouth}}} = ED + Ed = 348 + 208 = 556$$

$$SHGC = 0,46$$

$$IAC \text{ (we assume there are no shading)} = 1$$

$$FF_s = 0,47$$

### Heating case A (fixed 14,40 m2 on the west) in aluminium.

From the class example:  $\Delta T_{\text{heating}} = 24,8^{\circ}\text{C}$

$$U_{\text{windowwest}} = 4,62 \text{ W/m}^2 \cdot \text{K}$$

$$\begin{aligned} \text{HF} &= U_{\text{windowwest}} \times \Delta T_{\text{heating}} \\ &= 4,62 \text{ W/m}^2 \times 24,8^{\circ}\text{C} \\ &= 114,57 \text{ W/m}^2 \end{aligned}$$

$$\begin{aligned} Q_{\text{windowwest}} &= \text{HF}_{\text{windowwest}} \times A_{\text{windowwest}} \\ &= 114,57 \text{ W/m}^2 \times 14,40 \text{ m}^2 \\ &= 1649,80 \text{ W} \end{aligned}$$

Answer:

The heating value for the fixed window of 14,40m2, on the west is 1649,80W

### Heating case B (fixed 3,60 m2 on the south) in aluminium.

$$\begin{aligned} Q_{\text{windowssouth}} &= \text{HF}_{\text{windowssouth}} \times A_{\text{windowssouth}} \\ &= 114,57 \text{ W/m}^2 \times 3,60 \text{ m}^2 \\ &= 412,45 \text{ W} \end{aligned}$$

Answer:

The heating value for the fixed window of 3,60m2, on the south is 412,45W

### Heating case C (operable 3.6 m2 on the south) in aluminium.

$$\begin{aligned} Q_{\text{windowssouth}} &= \text{HF}_{\text{windowssouth}} \times A_{\text{windowssouth}} \\ &= 114,57 \text{ W/m}^2 \times 3,60 \text{ m}^2 \\ &= 412,45 \text{ W} \end{aligned}$$

Answer:

The heating value for the operable window of 3,60m2, on the south is 412,45W

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### Cooling case A (fixed 14,40 m2 on the west) in aluminium.

From the class example:  $\Delta T_{\text{cooling}} = 7,9^{\circ}\text{C}$

$$U_{\text{windowwest}} = 3,22 \text{ W/m}^2 \cdot \text{K}$$

$$\begin{aligned} \text{HF} &= U_{\text{windowwest}} \times \Delta T_{\text{cooling}} \\ &= 3,22 \text{ W/m}^2 \times 7,9^{\circ}\text{C} \\ &= 25,44 \text{ W/m}^2 \end{aligned}$$

$$\begin{aligned} Q_{\text{windowwest}} &= \text{HF}_{\text{windowwest}} \times A_{\text{windowwest}} \\ &= 25,44 \text{ W/m}^2 \times 14,40 \text{ m}^2 \\ &= 366,33 \text{ W} \end{aligned}$$

$$\begin{aligned} \text{CF}_{\text{windowwest}} &= (U_{\text{windowwest}} \times (\Delta T - (0,46 \text{ DR}))) + (\text{PXi} \times \text{SHGC} \times \text{IAC} \times \text{FFs}) \\ &= 3,22 \text{ W/m}^2 \cdot \text{C} \times (7,9^{\circ}\text{C} - 0,46 \times 11,90^{\circ}\text{C}) \\ &= 3,22 \text{ W/m}^2 \cdot \text{C} \times (7,9^{\circ}\text{C} - 5,47^{\circ}\text{C}) \\ &= 3,22 \text{ W/m}^2 \cdot \text{C} \times 2,43^{\circ}\text{C} \\ &= 7,82 \text{ W/m}^2 \end{aligned}$$

$$\begin{aligned} (\text{PXi} \times \text{SHGC} \times \text{IAC} \times \text{FFs}) &= \\ 747 \times 0,56 \times 1 \times 0,56 &= \\ 234,25 \text{ W/m}^2 & \end{aligned}$$

$$\begin{aligned} \text{Total CF} &= 7,82 \text{ W/m}^2 + 234,25 \text{ W/m}^2 = \\ &= 242,07 \text{ W/m}^2 \end{aligned}$$

$$\begin{aligned} \text{PXi}_{\text{windowwest}} &= \text{ED} + \text{Ed} = 559 + 188 = 747 \\ \text{SHGC} &= 0,56 \\ \text{IAC (we assume there are no shading)} &= 1 \\ \text{FFs} &= 0,56 \end{aligned}$$

$$\text{TOTAL Q} = C_{\text{windowsswest}} \times A_{\text{windowsswest}}$$

$$242,07 \text{ W/m}^2 \times 14,40 \text{ m}^2 = 3485,80 \text{ W}$$

Answer:

The cooling value for the fixed window of 14,40m<sup>2</sup>, on the west, in aluminium is 3485,80W

### Cooling case B (fixed 3,60 m<sup>2</sup> on the south) in aluminium.

$$U_{\text{windowssouth}} = 3,22 \text{ W/m}^2 \cdot \text{K}$$

$$C_{\text{windowssouth}} = (U_{\text{windowssouth}} \times (\Delta T - (0,46 \text{ DR}))) + (P_{\text{XI}} \times \text{SHGC} \times \text{IAC} \times \text{FFs})$$

$$3,22 \text{ W/m}^2 \cdot \text{K} \times (7,9^\circ\text{C} - 0,46 \times 11,90^\circ\text{C})$$

$$3,22 \text{ W/m}^2 \cdot \text{K} \times (7,9^\circ\text{C} - 5,47^\circ\text{C})$$

$$3,22 \text{ W/m}^2 \cdot \text{K} \times 2,43^\circ\text{C}$$

$$7,82 \text{ W/m}^2$$

$$(P_{\text{XI}} \times \text{SHGC} \times \text{IAC} \times \text{FFs}) =$$

$$557 \times 0,56 \times 1 \times 0,47 =$$

$$146,60 \text{ W/m}^2$$

$$\text{Total CF} = 7,82 \text{ W/m}^2 + 146,60 \text{ W/m}^2 =$$

$$154,42 \text{ W/m}^2$$

$$\text{TOTAL Q} = C_{\text{windowssouth}} \times A_{\text{windowssouth}}$$

$$154,42 \text{ W/m}^2 \times 3,60 \text{ m}^2 = 555,91 \text{ W}$$

Answer:

The cooling value for the fixed window of 3,60m<sup>2</sup>, on the south, in aluminium is 555,91W

### Cooling case C (operable 3.6 m<sup>2</sup> on the south) in aluminium.

$$U_{\text{windowsswest}} = 4,62 \text{ W/m}^2 \cdot \text{K}$$

$$\text{HF} = U_{\text{windowsswest}} \times \Delta T_{\text{cooling}}$$

$$4,62 \text{ W/m}^2 \times 7,9^\circ\text{C}$$

$$36,49 \text{ W/m}^2$$

$$Q_{\text{windowssouth}} = \text{HF}_{\text{windowssouth}} \times A_{\text{windowssouth}}$$

$$36,49 \text{ W/m}^2 \times 3,60 \text{ m}^2$$

$$131,36 \text{ W}$$

$$C_{\text{windowssouth}} = (U_{\text{windowssouth}} \times (\Delta T - (0,46 \text{ DR}))) + (P_{\text{XI}} \times \text{SHGC} \times \text{IAC} \times \text{FFs})$$

$$4,62 \text{ W/m}^2 \cdot \text{K} \times (7,9^\circ\text{C} - 0,46 \times 11,90^\circ\text{C})$$

$$4,62 \text{ W/m}^2 \cdot \text{K} \times (7,9^\circ\text{C} - 5,47^\circ\text{C})$$

$$4,62 \text{ W/m}^2 \cdot \text{K} \times 2,43^\circ\text{C}$$

$$11,22 \text{ W/m}^2$$

$$(P_{\text{XI}} \times \text{SHGC} \times \text{IAC} \times \text{FFs}) =$$

$$557 \times 0,55 \times 1 \times 0,47 =$$

$$143,98 \text{ W/m}^2$$

$$\text{Total CF} = 11,22 \text{ W/m}^2 + 143,98 \text{ W/m}^2 =$$

$$155,20 \text{ W/m}^2$$

$$\text{TOTAL Q} = C_{\text{windowssouth}} \times A_{\text{windowssouth}}$$

$$155,20 \text{ W/m}^2 \times 3,60 \text{ m}^2 = 558,72 \text{ W}$$

Answer:

The cooling value for the operable window of 3,60m<sup>2</sup>, on the south is 558,72W

$$P_{\text{XIwindowssouth}} = E_{\text{D}} + E_{\text{d}} = 348 + 209 = 557$$

$$\text{SHGC} = 0,56$$

$$\text{IAC (we assume there are no shading)} = 1$$

$$\text{FFs} = 0,47$$

$$P_{\text{XIwindowssouth}} = E_{\text{D}} + E_{\text{d}} = 348 + 209 = 557$$

$$\text{SHGC} = 0,55$$

$$\text{IAC (we assume there are no shading)} = 1$$

$$\text{FFs} = 0,47$$