

Linear Stability Analysis of a submerged cylinder.

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This Letter describes how the results of a global stability analysis of a classical circular cylinder are affected when the cylinder is submerged in a two phase gravitational flow. The flow behavior is governed by both the Reynolds and Froude numbers, while the depth of the cylinder has been varied to create different scenarios for the stability analysis. The baseflow obtained by the Navier-Stokes equations has been analyzed, and the Hopf bifurcation has been obtained for a fixed Froude number. The critical Reynolds number and the frequency of the most unstable mode have been compared to the classical solution without free surface and gravity effects. The most unstable mode is deformed and distorted according to the free surface location, while the critical frequency and the critical Reynolds numbers are both affected by the gravity and the free surface presence.

INTRODUCTION

The interaction between the viscous wake of a submerged object and the free surface position is a problem that deserves attention. Several reasons sustain its importance, [1] justifies the study due to its potential relevance for the remote sensing of the ocean surface from satellites, while [2, 3] outline its application to the design of offshore structures and vessels. It is well known that in the absence of free surface and gravity, the von Karman vortex street generated by flow past an infinitely long circular cylinder produces a two dimensional time periodic flow for Reynolds numbers between approximately 47 and 189 [4–7]. This work focuses on the changes produced in the stability of this flow when the cylinder is submerged and a free surface separating two different fluids in the presence of gravity. Different steady baseflows have been studied and a linear global stability analysis has been performed in order to quantify the differences when free surface and gravity are added to the problem. Previous authors performed stability analysis of idealized problems such as simple vortex structures [8, 9] and analytic shear flows [1]. To the authors knowledge, this constitutes the first study where a global stability analysis is performed on a Navier-Stokes computed solution in the presence of high discontinuities in density caused by the free surface. In order to gain insight about the basic physics of the interaction, the limits of steady solution where the velocity, the pressure and the free surface finally reach a stationary state are analyzed. The problem depends on two non-dimensional numbers, such as the Reynolds and the Froude numbers and one geometrical parameter which is the cylinder depth. The classical case when in the absence of gravity only one fluid is used has a very well studied solution and the steady separation bubble

breaks its stability when the only non-dimensional parameter, increases its value over $Re_c \approx 47$ (based on the cylinder diameter). For Reynolds values above this critical number perturbations amplify and the stability of the separation bubble breaks. Taking the critical Reynolds number, Re_c as a reference value without free surface, in our study the Reynolds number has been increased from subcritical to supercritical values while the Froude number based on the cylinder diameter has been kept constant along the study for three different cylinder depths. Two causes could trigger the first instability of these flows: typical vortex shedding instability or a free surface Rayleigh-Taylor instability. In our study the range of parameters Reynolds, Froude and cylinder depth has been selected such that the vortex shedding is the cause of instability while the free surface instabilities are not feasible due to fluid setup where the heavier is placed at the bottom. This hypothesis is confirmed by the Dynamic Mode Decomposition (DMD)[15] tests performed on the supercritical range, where no intrinsic free-surface instability is found and vortex shedding modes are reproduced. Similarly with the work presented by [1], the purpose is to analyze the stability of the wake of a floating two-dimensional object. However, a few differences can be found between both methodologies: first, in our case no analytic hypothesis of the flow or weakly parallel assumptions have been used for the baseflow construction, instead, the base flow has been computed solving the Navier-Stokes equations for both fluids. Second, no boundary conditions have been used for the free surface, and a scalar VOF function [10] has been added to the simulation to represent density and viscosity changes. Third, a two dimensional global analysis has been performed consequently not assuming any harmonic dependance of the perturbation in the flow direction.

METHODOLOGY

The governing equations are the incompressible Navier–Stokes equations in laminar regime, which are supplemented with the conventional boundary conditions on solid and/or open boundaries. The computational domain Ω contains both fluids, the first one denoted by subscript 1 is placed at the top of the domain, and the second one placed at the bottom denoted by the subscript 2. Let us name their corresponding densities and kinematic viscosities as ρ_i and ν_i ($i=1,2$), respectively, where $\rho_2 \gg \rho_1$. The non dimensional governing equations, written in a Lagrangian framework, are:

$$\nabla \cdot \left(\frac{1}{\beta} \mathbf{v} \right) = 0 \quad (1)$$

$$\frac{D\mathbf{v}}{Dt} = -\beta \nabla p + \nabla \cdot (\alpha \nabla \mathbf{v}) + \frac{1}{Fr_D^2} \mathbf{u}_g \quad (2)$$

Here \mathbf{v} , p are the velocity and fluid pressure and \mathbf{u}_g is a unitary vector parallel to the gravity force. The equations are computed in non-dimensional form using the cylinder diameter D , the inflow velocity U and the density and viscosity of the bottom fluid. The Reynolds $Re_D = \frac{UD}{\nu_2}$ and the Froude numbers $Fr_D = \frac{U}{\sqrt{gD}}$ will be defined using the fluid properties of the bottom fluid. It is important to remark that compared to the case where only one fluid is involved, two non dimensional coefficients α and β (both specially relevant when including the free surface interface) appear explicitly in the mass and momentum conservation equations 1 and 2.

$$\alpha = \frac{(\phi + 1) - \left(\frac{\nu_1}{\nu_2}\right)(\phi - 1)}{2Re_D} \quad (3)$$

$$\frac{1}{\beta} = \frac{(\phi + 1)}{2} - \frac{\rho_1}{\rho_2} \frac{(\phi - 1)}{2} \quad (4)$$

where ϕ is the scalar function such that: $\phi = -1$ in the fluid 1 and $\phi = 1$ in the fluid 2. An efficient and accurate methodology, called PFEM-2[11], has been used to numerically simulate the dynamics of an incompressible flow during the baseflow computation. It is important to remark that both density and viscosity are discontinuous functions that are accurately transported according to the techniques described in [11]. We choose a sufficiently large domain size to minimize the undesirable boundary effects, where the inflow and exit boundaries are each located at $18D$ and $35D$ towards the fore and aft of the cylinder, respectively. The far field boundary is located at $15D$ on either side of the central axis. A uniform inflow boundary condition, together with a natural boundary condition for the far field and outflow, are applied for the velocity. The no-slip boundary condition is

employed for the cylinder. A Neumann boundary condition is imposed for the pressure in all boundaries except the outflow where zero Dirichlet condition is imposed.

After a complete mesh converge process based on the drag and lift forces, a final mesh has been selected. The mesh used for the simulations is a linear triangular mesh that contains 65834 triangles and 132542 nodes, the default mesh size is $0.655D$ while in the cylinder proximities and the free surface area the mesh size has been refined to $0.0016D$. See FIG. 1 to appreciate the computational domain and the mesh configuration near the cylinder.

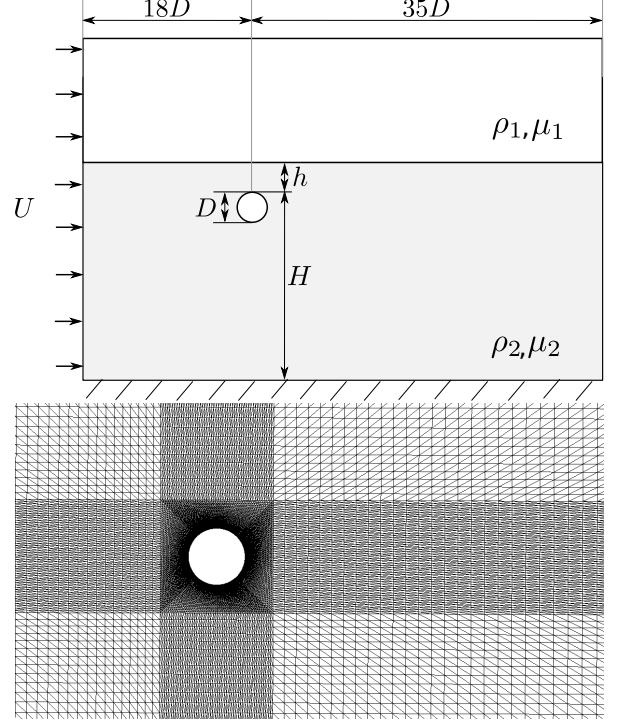


FIG. 1: Computational domain (top) and zoomed view around the cylinder of the mesh used (bottom) for the baseflow computation and subsequent stability analysis.

An accurate and efficient simulation of the interface evolution is crucial when simulating free-surface flows. During the flow evolution, it is essential that the interface remains sharp. Large jumps of fluid density and viscosity across the interface should be correctly captured by the numerical algorithm in order to satisfy the momentum balance at the vicinity of the interface. Readers interested in more details of the PFEM-2 method and the enrichment technique used for the free surface definition may see [11].

The complete analysis requires two steps: during the first one, the two-dimensional Navier-Stokes equations are solved for those Re_D and Fr_D values that finally reach a steady or periodic state $(\bar{\mathbf{v}}, \bar{p}, \bar{\phi})$ known as base flow. For those cases where the Reynolds number is above the critical value and no steady state is obtained turning

to a periodic case, a time averaged solution is analyzed, see [12] and the result will be confirmed by DMD analysis. During the second step, the base flow is perturbed by the product of a small parameter $\varepsilon \ll 1$ by the amplitude velocity $\hat{\mathbf{v}}$ and kinematic pressure \hat{p} perturbations, as follows:

$$\mathbf{v} = \bar{\mathbf{v}} + \varepsilon \hat{\mathbf{v}} \exp(\omega t) \quad p = \bar{p} + \varepsilon \hat{p} \exp(\omega t) \quad (5)$$

where the complex number $\omega = \omega_r + i\omega_i$ contains the growth rate as real part and the oscillation frequency as complex part. The stability analysis of the equations implies the linearization of the Navier-Stokes equations around a steady or mean base flow. This process has been done following the same methodology explained in [13] which implies the resolution of a large generalized eigenvalue problem by an iterative Arnoldi method. The baseflow can be considered unstable when any of the ω_r are positive. When the Navier-Stokes equations are solved and perturbed, new terms coming from the α and β gradients are important and must be specially taken into account on free surface proximities. However, two important considerations should be remarked when the analysis step is performed:

- For subcritical Reynolds numbers, the steady baseflow implies a final distribution of both fluids determined by the values of the VOF function. As usual, the free surface is represented by VOF function isosurface $\phi = 0$. The VOF function distribution is not perturbed for the analysis, assuming that the vortex shedding will be the cause of instability. This will be later confirmed by DMD analysis.
- For supercritical cases where the baseflow is unsteady, either a frequency damping algorithm or an averaged process is required to obtain a baseflow suitable for analysis [12, 14]. In our case, the linear global stability analysis results using an averaged baseflow have been confirmed by a DMD analysis using no less than 10 snapshots per period.

RESULTS

For the case where the liquid (bottom fluid) density and fluid viscosity is 100 times their respective top fluid value, we have analyzed a range of Reynolds $Re = (30, 70)$ in the proximities of Re_c . The Froude number has been kept fixed to $Fr_D = 3$ and three different water depth values were studied $h/D = 0.55, 1, 2$. Despite the Reynolds number difference, the free surface elevation at the top of the cylinder is similar to the one presented by Bouscasse [3]. For the sake of code validation, the global

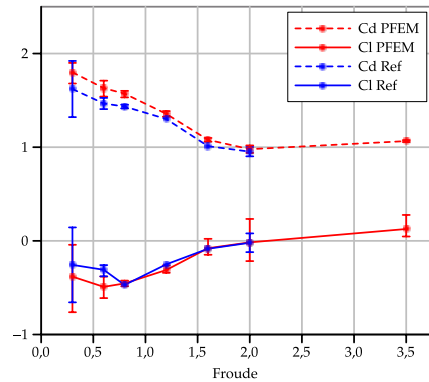


FIG. 2: Drag and Lift coefficients calculated with PFEM-2 at $Re_D = 180$ and $h/D = 0.55$ for different Fr_D numbers, comparison with the reference work of Bouscasse [3].

drag and lift forces have been compared against previous results[3] at the standard $Re_D = 180, h/D = 0.55$ and different Froude numbers being the agreement very satisfactory, see FIG. 2.

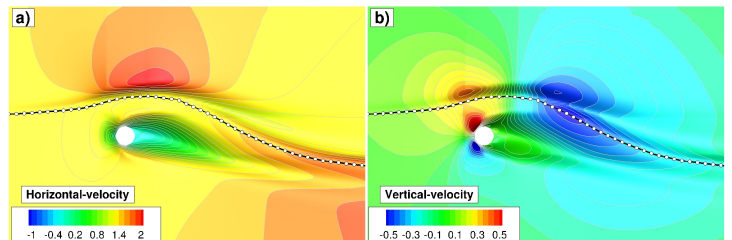


FIG. 3: Steady state solution for $Re_D = 45$, $h/D = 0.55$ and $Fr_D = 3$

For the stability study, a collection of steady baseflows has been obtained varying the Reynolds number and the cylinder depth. As example, the horizontal and vertical velocity components of the baseflow and the free surface position corresponding to $Re_D = 45$, $h/D = 0.55$ and $Fr_D = 3$ are shown in FIG. 3. For each one a stability analysis based of the resolution of the large eigenvalue problem mentioned before has been computed, and the evolution of the most unstable mode monitored. The evolution of the growth/damping rate and the angular frequencies of the most unstable mode is shown in FIG. 4, where the value without free surface $h/D = \infty$ is also represented as reference. It can be observed that similarly to what happens in the absence of free surface and gravity the most unstable mode moves towards the unstable region $\omega_r < 0$ when the Reynolds number is increased. For a Reynolds number very close to the one found in the absence of free surface and gravity $Re_c \approx 47$ the mode turns to be unstable and vortex shedding pro-

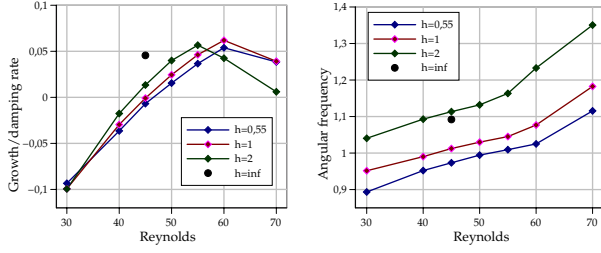


FIG. 4: Growth rate and frequency for different Re numbers and h/D values. The isolated black dot represents the case with gravity and without free surface ($h/D = \infty$). The classic result in the absence of free surface and gravity has $Re_c = 47$ and $\omega_c = 0.7414$ as critical values.

cess develops. This critical Reynolds value depends on the h/D parameter, increasing when h/D decreases. A black dot representing the less stable pure gravitational case without free surface ($h/D = \infty$) has been included in FIG. 4 for comparison. Consequently, a first evidence is that the free surface presence increases the stability of the flow. An increasing oscillation is appreciated by the presence of the gravity field, being the critical frequencies for all cylinder depths noticeably higher than the one associated to the classical case without both free surface and gravity $\omega_c = 0.7414$. It can be hence concluded that both gravity and free surface affect the vortex shedding onset. A second fact is that the frequency associated to this oscillating unstable mode increases with the cylinder depth, having the case $h/D = 2$ a frequency very close to the single phase case.

In order to confirm if the averaged baseflows obtained for highest supercritical Reynolds values were correct, a DMD analysis has been performed for each cylinder depth. In FIG. 5, the critical frequencies from the most unstable mode DMD analysis are compared to the ones coming from the global analysis. As can be observed the values of the frequencies agree and the leading frequency was in all cases attributed to the vortex shedding phenomena aft the cylinder.

The mode corresponding to this oscillating unstable mode for the case $Re_D = 45$ $Fr_D = 3$ and $h/D = 0.55$ is shown in FIG. 6, where the shape of the mode is visibly influenced by the free surface modulation.

In the future, these results will be also extended to higher Reynolds values by DMD analysis. The possibility of having situations where growing instabilities are caused by the free surface oscillations, similar to what occurs in a Rayleigh-Taylor instability, will be also analyzed. This work was supported by the Technical University of Madrid by the project (PID) "Combination of Eulerian and Lagrangian methodologies for the solution

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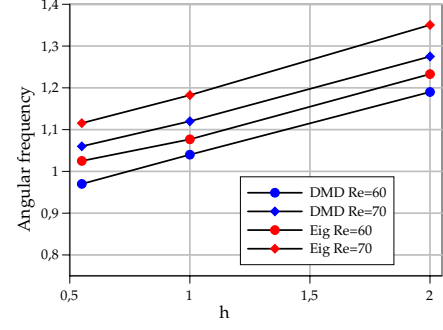


FIG. 5: Critical frequencies for different cylinder depths and Reynolds numbers are compared between DMD and global analysis.

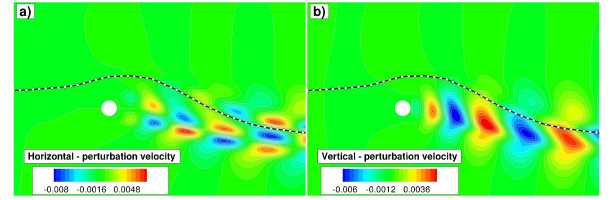


FIG. 6: Unstable mode for the case $Re = 45$ $Fr_D = 3$ and $h/D = 0.55$

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