

Automated Long-Term Stability of a High Energy Laser

Contact: pedro.oliveira@stfc.ac.uk

Jack Morse, Will Carter, Pedro Oliveira, Marco Galimberti
Central Laser Facility,
STFC Rutherford Appleton Laboratory,
OX11 0QX

Key words: stability, laser-stabilisation, monitoring, feedback-loop.

Abstract

We present a method for regulating laser energy output with a software-controlled waveplate-polariser configuration. By implementing this technology, we have effectively eliminated energy output fluctuations over time, allowing for the laser to reach its nominal energy up to 2 hours earlier. Our testing demonstrates a stability of 2.8% (RMS), verifying the system's reliability. We provide an overview of the software and its basic operation, along with practical evidence of the system's efficacy in maintaining stable laser energy output.

Introduction

In this article we describe a method to stabilise the output energy of an initially unstable laser within a complex laser system. Similar techniques have been implemented in different situations[13].

We discovered for the laser used in our system that the output energy varies over the course of the day, specifically with a significantly higher energy output at the beginning of the day, before levelling off to a more stable operational level. This warm-up period, to a point where the output is more stable, is around two hours, and is believed to be due to thermal effects inside the laser.

This warm up time is problematic since the laser is the pump laser of an Optical Parametric Chirped Pulse Amplification (OPCPA) system[10, 5, 11, 3]; these are inherently sensitive to the energy of the pump pulse, with output energy varying exponentially with input pump energy away from saturation, and linearly thereafter. In order to maintain a stable energy output of the OPCPA, we must be pumping with a laser of constant energy. OPCPA depends on other factors aside from pump energy, such as temporal overlapping of the seed and pump, the phase-matching angle between the seed and pump, and the intensity of each pulse. In order to maximise the stability of a system, each of these conditions need to be satisfied and controlled. However, away from saturation, the exponential dependence of the pump intensity makes it the most important parameter to control in order to keep a stable energy output. We investigate only the effect of this

technology on the laser itself, and do not present any results relating to an increased stability in the entire laser system for which this pump is one part. With the advent of new scientific facilities that use OPCPA incorporated in their systems coming online [9, 6, 2, 12] stabilization of the pump energy is crucial. Moreover we can envision that this same system could be applied to a wide range of lasers as long as they are not single shot lasers. In fact applications from 3D printing [4] to laser plasma accelerators [8] or shearography [1] imply a careful control of the laser energy, this is especially problematic for low repetition rate high energy lasers [7, 14] that do intricate highly nonlinear physics at the same time as comporting a high thermal load that is due to changes in the environment, but also due to the heating of the laser components during pumping. A full description of the sub-system this pump laser is included in can be found in [10].

As such, we present the work undertaken to regulate the energy of this laser, by varying the polarisation of the pulses before it is redefined later on in the laser cavity. We believe this technique could be easily implemented on any complex laser system where a constant pump energy is an important factor.

Method and Code Logic

Figure 1 shows a schematic of the laser cavity.

A laser temporally shaped by a fibre EOM is delivered by fibre to the amplification system. It is then magnified to match the pre-amplifier size of 5 mm (the amplifier diameter is 6 mm) with a gain of 20. Our energy control waveplate (WP) is after the pre-amplifier and before injection into a regenerative amplifier with a SSG of 20 per pass with relay imaging and a pinhole in the far-field. Therefore the power incident on WP is low. The output energy is 30 mJ at the output of the amplifier is then magnified with a positive-negative telescope to a 12 mm diameter before passing the power amplifiers which amplify it to 1 J; this is converted to the second harmonic using a KDP crystal for an output energy of 0.5 J. The pulse duration is 4.5 ns and the repetition rate is 2 Hz.

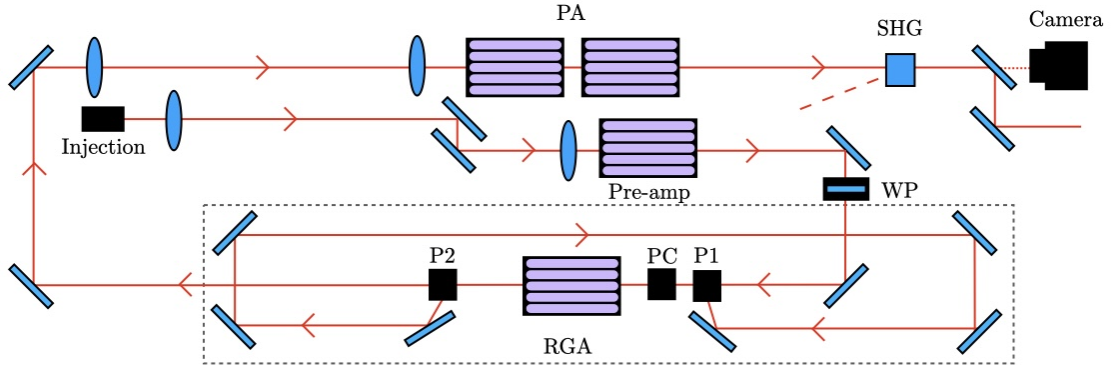


Figure 1: A schematic of the laser cavity. WP is the controllable waveplate, P1 and P2 are polarisers, PC is a Pockels' cell, RGA is the regenerative amplifier, SHG is the second harmonic KDP crystal. The camera takes a leak of the penultimate mirror.

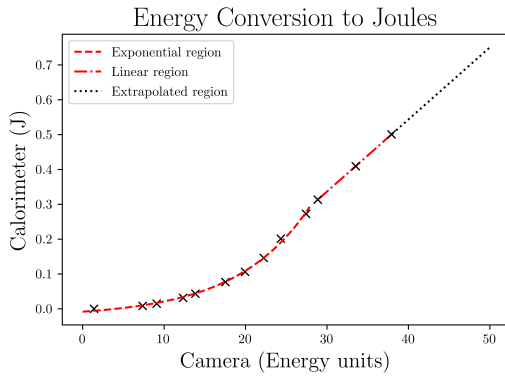


Figure 2: Practical measurement of uEye camera's calorimetry response using a Gentec MAESTRO energy detector. The extrapolated region is assumed linear.

The output of the laser is monitored by a camera (in our case a uEye USB camera) and controlled by the movement of a $\lambda/2$ waveplate, which has been mounted on a motorised rotational mount purchased from Thor-Labs¹. The energy is calculated by averaging the reading from each pixel in the acquired image. A camera was used due to its sensitivity at low energies, low cost and ability to encompass the entirety of the beam. Alternative sensors could include a wide sensor photodiode; or a more costly solution could be a calibrated Gentec energy sensor.

To convert energy measurements in camera units to Joules, measurements of the pump energy in the system were taken with a calorimeter. Obtaining for multiple set energies an average energy with the camera and with the calorimeter, one is able to determine the camera's calorimetry response (see Figure 2). We found this function to be non-linear for low energies and well-

approximated to the piecewise function

$$\begin{cases} 0.0145 \times \exp(0.1104x) - 0.0228, & x < 27.89, \\ 0.0207x - 0.2843, & x \geq 27.89 \end{cases} \quad (1)$$

with x being the camera energy and the output in Joules. The rms error for the fit in the exponential and linear regions are 4.4 mJ and 0.3 mJ respectively.

Giving the software a calibration function [see subsection 'Obtaining a Calibration Function'] and a set energy, it is able to move WP to a calculated angle, which by altering the polarisation in turn changes the transmission through the polariser. For a standard $\lambda/2$ waveplate, we would expect the transmission through the polariser to follow a sinusoidal-squared curve as per to the well-known Malus' Law.

However, a theoretical curve of this form could not be used in our case due to the presence of amplifiers in between the control and detection devices, as well as a non-linear camera calorimetry response (see Figures 1 & 2). This adds complication which would be impractical to formulate in this case, since, as in most real world situations with a feedback loop, a practical calibration serves a more accurate method for optimising the response. As such, we used a polynomial of order 3 due to its good fit to the calibration data (see Figure 4).

1. Calculating the new angle

Many forms of feedback loop exist, each with their own benefits and drawbacks depending on the situation. For example, a simple proportional p -loop could be used to minimise the error, $\varepsilon = \text{Measured Energy} - \text{Setpoint Energy}$. Instead, we decided to use a method whose next guess is calculated so as to converge to the correct value very rapidly. In some circumstances, e.g. where a very short loop time is desired, this method may be too computationally intensive. However, there were no concerns of this nature here as the repetition rate of the oscillator itself is (only) 2 Hz, slow enough for a

¹Model KDC101

computer to complete this calculation and be ready to go again. Furthermore, it is much more important to converge rapidly when the feedback loop time is larger, simply because fewer iterations occur for a given time period. Therefore, for our system to have a fast response to change and minimise the presence of instability in the output, the following method was selected.

First, an image is acquired from the camera, and a value for the current energy E_{cur} (labelled ‘Current’ in Figure 3) is computed.

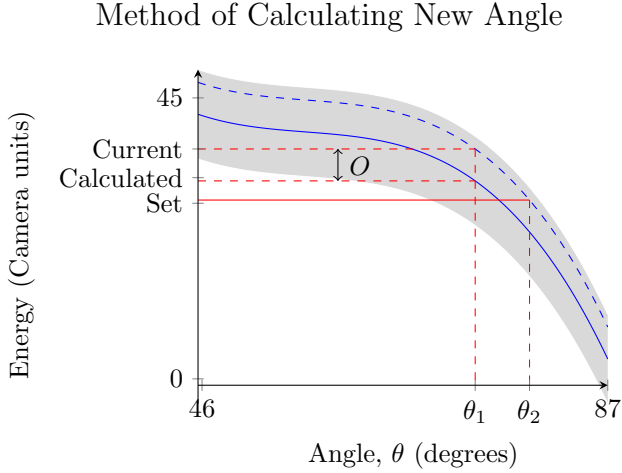


Figure 3: The blue curve represents the original calibration function; the dashed blue curve represents the translated calibration function; θ_1 = current angle; θ_2 = calculated angle.

Next, a calculation of the energy is made from the calibration function, $f(\theta)$, using the current angle (labelled ‘Calculated’ in Figure 3), which is given by

$$E_{\text{calc}} = A \cdot \theta_{\text{cur}}^3 + B \cdot \theta_{\text{cur}}^2 + C \cdot \theta_{\text{cur}} + D, \quad (2)$$

where E_{calc} is the calculated energy, θ_{cur} is the current angle, and A, B, C, D are the calibration function coefficients. This then gives a value for the offset O , which as Figure 3 shows is the difference between the theoretical value we would expect from the calibration function, and the value we actually measure:

$$O = E_{\text{cur}} - E_{\text{calc}}. \quad (3)$$

This can be visualised as a translation of the calibration function to a new position, where the translation is exactly equal to O .

We then define an updated calibration function $\hat{f}(\theta) := f(\theta) + O$, equal to the dashed blue curve in Figure 3. From this, we solve for θ_2 , which is our to be calculated angle, by finding the value of theta such that $\hat{f}(\theta) = \text{Set Energy}$. I.e.

$$A \cdot \theta^3 + B \cdot \theta^2 + C \cdot \theta + (D - O - \text{Set Energy}) = 0. \quad (4)$$

A correct calibration function will only lead to one real solution in the range $[\theta_i, \theta_f]$, which is the angle

(θ_2) WP is commanded to move to.

2. Obtaining a Calibration Function

The method in the previous section only yields

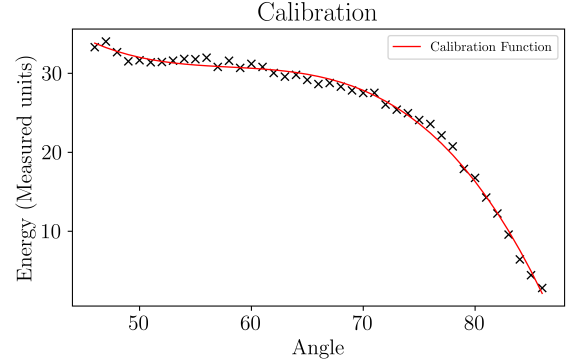


Figure 4: A cubic calibration function (red) fit to measured energies from the camera as a function of angle.

useful values when an appropriate calibration function is provided. This software, written in C#, has the functionality of self-calibration. To obtain a valid calibration curve, an energy scan taken over a short time scale (relative to any drifts in the laser output) is taken. In our case the scan takes approximately 2 minutes. The scan commences at the smallest angle, θ_i , and steps each degree until the largest angle, θ_f , is reached. At each step, an energy measurement is taken, with the ability to average over n images to reduce the error introduced from a single measurement. A cubic curve is then fit to the data points, and the coefficients (A, B, C, D) are stored in the application. Calibration only needs to be taken once for the feedback loop to work until there is a change to the setup. A cubic was chosen as it fits the range well; and a quartic provided little extra accuracy. The range $[\theta_i, \theta_f]$ was selected as it gives a full range of transmission, from maximum to minimum, of the waveplate-polariser configuration.

3. Software Development

The UI was developed in .NET Framework, primarily due to its built-in charting libraries. The application saves the last connected ThorLabs motor serial number and uEye camera ID to attempt an automatic connection next time the software is launched. An automatic run/stop functionality was added so that the code was not capturing images overnight when the laser was turned off, but was able to stabilise as soon as the laser was automatically turned on at the beginning of an operational day. This also allows the system to work within an operational environment without daily intervention from operators. The user has control of all key parameters so that the functionality of the software can be optimised to the setup. The ‘set energy’ parameter is given in arbitrary units which correspond to those the camera



Figure 5: A capture of the UI of the Stability2 Hz software, developed in C#.

gives intensity values in. We found a set energy of 29 camera units (316 mJ) to be optimal for operations. An ‘average over’ parameter reduces the systems ability to respond pulse-to-pulse, but increases its precision when responding to longer-term changes. The user can also choose to add a tolerance for delta theta, so that if the calculated change in angle is small WP is not commanded to move. The energy threshold parameter gives a minimum energy for the camera to detect for movement of WP to occur. This should be set to be slightly greater than the maximum energy measurement when the laser is on but the waveplate-polariser is at minimum transmission, so that WP does not get commanded to go to its maximum when the laser is turned off and thus preventing excessive light from passing through the next time the laser is enabled. The history graph is useful for monitoring, as it displays the last m measurements, where m is the number of iterations, which the user can specify.

Analysis of Results

To assess the effectiveness of this method, we ran the system without active stabilization and an entire day with active stabilization. In the first case the software to measure energy output with the waveplate stabilisation was scheme turned off. The second test ran for the same length of time, but with stabilisation running. The software was run as usual for operations on the day before testing, and the waveplate was then left at its final angle. It is then expected that if there is no drift or warm-up period, this angle being fixed would lead to a flat line in the energy reading with respect to time, i.e. the energy would be unchanging and equal to the energy measured at the end of the previous day, which was 29 energy units, or 316 mJ. On the day of the non-stabilising test, the laser was turned on at 7:00 AM but the internal shutter to the pump remained closed until 7:20 AM; this meant that no energy measurements could be captured during this time. This 20 minute warm-up period was given to ensure that no internal damage to the system was caused,

since it is expected that the energy would be far higher during these first few minutes. Figure 6 shows how the system has a higher energy at the start of the day, and gradually tailed off to the level of the set energy from the previous day. The period from start to the point where we would consider using the laser without any stabilisation is around 2 hours.

The system being operated with stabilisation shows

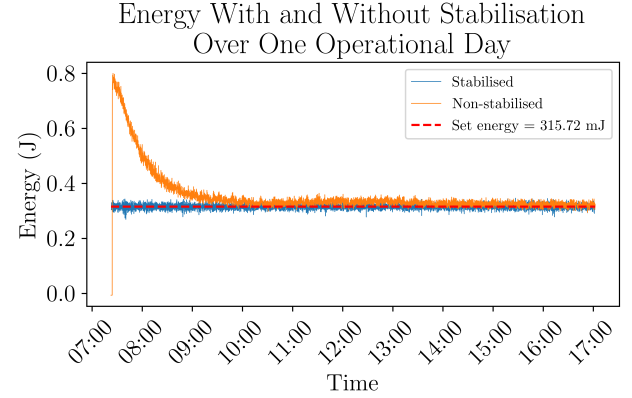


Figure 6: The plot shows how the laser has a warm up period of around 2 hours (orange trace). The blue curve sits at the same level as the set energy (red dashed line) for the duration of the day. Both plots have been converted to Joules using (1).

limited improvement over the warmed-up oscillator energy between 10:00 AM (when the non-stabilised output energy has settled) and 17:00 PM (when the test was concluded). The standard deviation in this period for the non-stabilising and stabilising arrangements were $\sigma_{ns} = 9.20$ mJ (2 d.p.) and $\sigma_s = 8.85$ (2 d.p.) respectively. The intention of this system was never to improve the pulse-to-pulse stability, but only to minimise longer term deviations meaning this is not concerning. However, the mean energy for the stabilised system from 10:00 AM to 17:00 PM was $\mu_s = 315.70$ (2 d.p.), when aiming for 315.72; whereas it was $\mu_{ns} = 328.48$ mJ (2 d.p.) for the non-stabilised system over the same period. This shows the stabilised system operates with a very high precision in the output, leading to operational benefits in energy predictability. All of this is summarised in Figure 6. The set energy (red dashed line) is added to show how good the two configurations are at reaching the set energy. We can see that in the non-stabilized case the laser has an exponential decay to the reference energy over the first 2 hours and is visible that even afterwards there is a slow decay over almost all day to the reference energy.

Conclusion

Successful implementation of this system has decreased the laser warm-up time by 2-3 hours, allowing the laser to be operational sooner. We have also proved the

quadratic and then linear dependence of the energy to camera pixel value which is to be expected for a system based in p-n junctions. We have also proven a calibration mechanism that is iterative and could be applied to any high energy solid state laser system. The energy rms has also decreased to 2.8% from a previous 3%.

The system also allows the energy output to be easily changed through software controls and calibration ensures that the same energy can be achieved each day.

This technique could be easily replicated in any laser system encountering fluctuations in laser energy and long warmup times.

References

- [1] K. M. Abedin, A. R. Al Jabri, and S. Mujibur Rahman. Power stability of different lasers and its effect on the outcome of phase-stepping shearography experiments. *Results in Optics*, 12:100490, 2023.
- [2] C. Alexandridi, X. Délen, F. Druon, P. Georges, L. Martin, F. Mathieu, and D. Papadopoulos. Generation of optically synchronized pump–signal beams for ultrafast opcpa via the optical kerr effect. *Opt. Lett.*, 46(9):2035–2038, May 2021.
- [3] A. Dubietis, G. Jonušauskas, and A. Piskarskas. Powerful femtosecond pulse generation by chirped and stretched pulse parametric amplification in bbo crystal. *Optics Communications*, 88(4):437–440, 1992.
- [4] J. C. Haley, B. Zheng, U. S. Bertoli, A. D. Dupuy, J. M. Schoenung, and E. J. Lavernia. Working distance passive stability in laser directed energy deposition additive manufacturing. *Materials Design*, 161:86–94, 2019.
- [5] C. Hernandez-Gomez, J. Collier, M. Csatari, and J. Smith. Commissioning of the vulcan opcpa preamplifier. *Annual Report CLF Rutherford*, 175:2001–2002, 2001.
- [6] Z. Hubka, R. Antipenkov, R. Boge, E. Erdman, M. Greco, J. T. Green, M. Horáček, K. Majer, T. Mazanec, P. Mazurek, J. A. Naylon, J. Novák, V. Šobr, P. Strkula, M. Torun, B. Tykalewicz, P. Bakule, and B. Rus. 120mj, 1khz, picosecond laser at 515nm. *Opt. Lett.*, 46(22):5655–5658, Nov 2021.
- [7] S. Ji, W. Huang, J. Guo, J. Wang, X. Lu, D. Huang, H. Wei, W. Fan, and X. Li. Lamp-pumped eight-pass neodymium glass laser amplifier with high beam quality. *Optical and Quantum Electronics*, 53(6):277, May 2021.
- [8] A. R. Maier, N. M. Delbos, T. Eichner, L. Hübner, S. Jalas, L. Jeppe, S. W. Jolly, M. Kirchen, V. Leroux, P. Messner, M. Schnepf, M. Trunk, P. A. Walker, C. Werle, and P. Winkler. Decoding sources of energy variability in a laser-plasma accelerator. *Phys. Rev. X*, 10:031039, Aug 2020.
- [9] K. Murari, G. Cirmi, H. Cankaya, G. J. Stein, B. Debord, F. Gérôme, F. Ritzkosky, F. Benabid, O. Muecke, and F. X. Kärtner. Sub-50fs pulses at 2050nm from a picosecond hofy laser using a two-stage kagome-fiber-based compressor. *Photon. Res.*, 10(3):637–645, Mar 2022.
- [10] B. Parry, P. Oliveira, A. Boyle, W. Shaikh, and I. Musgrave. A new ns opcpa front end for vulcan petawatt. *CLF Annual Report*, 2014, 2013.
- [11] I. Ross, P. Matousek, M. Towrie, A. Langley, and J. Collier. The prospects for ultrashort pulse duration and ultrahigh intensity using optical parametric chirped pulse amplifiers. *Optics Communications*, 144(1):125–133, 1997.
- [12] M. Seidel, F. Pressacco, O. Akcaalan, T. Binhammer, J. Darvill, N. Ekanayake, M. Frede, U. Grosse-Wortmann, M. Heber, C. M. Heyl, D. Kutnyakhov, C. Li, C. Mohr, J. Müller, O. Puncken, H. Redlin, N. Schirmel, S. Schulz, A. Swiderski, H. Tavakol, H. Tünnermann, C. Vidoli, L. Wenthaus, N. Wind, L. Winkelmann, B. Manschwetus, and I. Hartl. Ultrafast mhz-rate burst-mode pump–probe laser for the flash fel facility based on nonlinear compression of ps-level pulses from an yb-amplifier chain. *Laser & Photonics Reviews*, 16(3):2100268, 2022.
- [13] B. Zhao, S. Banerjee, W. Yan, P. Zhang, J. Zhang, G. Golovin, C. Liu, C. Fruhling, D. Haden, S. Chen, and D. Umstadter. Control over high peak-power laser light and laser-driven x-rays. *Optics Communications*, 412:141–145, 2018.
- [14] J. Zhu, J. Zhu, X. Li, B. Zhu, W. Ma, X. Lu, W. Fan, Z. Liu, S. Zhou, G. Xu, and et al. Status and development of high-power laser facilities at the nlhplp. *High Power Laser Science and Engineering*, 6:e55, 2018.