

1 Introduction

2 MLS/RK meshfree approximation

In accordance with Moving Least Square approximation (MLS) [1] or Reproducing Kernel approximation (RK) [2], the domain Ω is discrete by a set of meshfree nodes $\{\mathbf{x}_I\}_{I=1}^{n_p}$, n_p is the total number of meshfree nodes. And then, a variable u in Ω can be approximated as follow:

$$u^h(\mathbf{x}) = \sum_{I=1}^{n_p} \Psi_I(\mathbf{x}) d_I \quad (1)$$

where Ψ_I and d_I are the meshfree shape function and the nodal coefficient associated with meshfree node \mathbf{x}_I . This RK shape function Ψ_I is constructed by the undetermined coefficient vector \mathbf{c} , the basis function vector \mathbf{p} and the kernel function ϕ :

$$\Psi_I(\mathbf{x}) = \mathbf{c}^T(\mathbf{x}) \mathbf{p}(\mathbf{x}_I - \mathbf{x}) \phi(\mathbf{x}_I - \mathbf{x}) \quad (2)$$

For instance in 2D case, the basis function vector \mathbf{p} contains the p th order complete monomials:

$$\mathbf{p}(\mathbf{x}) = \{1, x, y, x^2, \dots, y^p\}^T \quad (3)$$

The kernel function ϕ determines the support size and continuity of shape function, and the cubic and quintic spline functions is chosen herein for elasticity problems and thin plate problems respectively.

$$\phi(\mathbf{x}_I - \mathbf{x}) = \varphi\left(\frac{x_I - x}{h_x}\right) \varphi\left(\frac{y_I - y}{h_y}\right) \quad (4)$$

where h_i is the

- Cubic spline function:

$$\varphi(r) = \frac{1}{3!} \begin{cases} (2-2r)^3 - 4(1-2r)^3, & r \leq \frac{1}{2} \\ (2-2r)^3, & \frac{1}{2} < r \leq 1 \\ 0, & r > 1 \end{cases} \quad (5)$$

- Quintic spline function:

$$\varphi(r) = \frac{1}{5!} \begin{cases} (3-3r)^5 - 6(2-3r)^5 + 15(1-3r)^5, & r \leq \frac{1}{3} \\ (3-3r)^5 - 6(2-3r)^5, & \frac{1}{3} < r \leq \frac{2}{3} \\ (3-3r)^5, & \frac{2}{3} < r \leq 1 \\ 0, & r > 1 \end{cases} \quad (6)$$

in which h_i is the support size in x_i axis direction.

The undetermined vector \mathbf{c} can be attained by enforcing the following consistency condition:

$$\sum_{I=1}^{n_p} \Psi_I(\mathbf{x}) \mathbf{p}(\mathbf{x}_I) = \mathbf{p}(\mathbf{x}) \quad (7)$$

or with a shift-form

$$\sum_{I=1}^{n_p} \Psi_I(\mathbf{x}) \mathbf{p}(\mathbf{x}_I - \mathbf{x}) = \mathbf{p}(\mathbf{0}) \quad (8)$$

substituting Eq. 2 into the consistency condition leads to:

$$\mathbf{c}(\mathbf{x}) = \mathbf{A}^{-1}(\mathbf{x}) \mathbf{p}(\mathbf{0}) \quad (9)$$

with moment matrix \mathbf{A}

$$\mathbf{A}(\mathbf{x}) = \sum_{I=1}^{n_p} \mathbf{p}^T(\mathbf{x}_I - \mathbf{x}) \mathbf{p}(\mathbf{x}_I - \mathbf{x}) \phi(\mathbf{x}_I - \mathbf{x}) \quad (10)$$

It is noted that, to ensure the invertibility of moment matrix, a well-posed meshfree nodal distribution should be required, i.e. there should be sufficient meshfree nodes be covered by their support, as shown in Fig. ???. Under this circumstance,

$$\|u - u^i\|_{H_k} \leq Ch^{p-k+1} |u|_{H_{p+1}}, \quad \forall k \leq p+1 \quad (11)$$

3 Hellinger-Reissner based RK gradient smoothing meshfree formulation

In this section, the Hellinger-Reissner reproducing kernel gradient smoothing meshfree formulations for second order elasticity problems and fourth order thin plate problems are briefly introduced here.

3.1 Elasticity problems

For elasticity problems, the Hellinger-Reissner energy functional is given by:

$$\begin{aligned} \mathcal{L}(\boldsymbol{\sigma}, \mathbf{u}) = & \int_{\Omega} \frac{1}{2} \boldsymbol{\varepsilon}(\boldsymbol{\sigma}) : \boldsymbol{\sigma} d\Omega - \int_{\Gamma_u} \mathbf{n} \cdot \boldsymbol{\sigma} \cdot \bar{\mathbf{u}} d\Gamma \\ & - \int_{\Gamma_t} \mathbf{u} \cdot (\boldsymbol{\sigma} \cdot \mathbf{n} - \bar{\mathbf{t}}) d\Gamma + \int_{\Omega} \mathbf{u} \cdot (\boldsymbol{\sigma} \cdot \nabla + \bar{\mathbf{b}}) d\Omega \end{aligned} \quad (12)$$

where $\boldsymbol{\varepsilon}$ and $\boldsymbol{\sigma}$ stands for the strain and stress tensor respectively. Γ_u and Γ_t are the essential boundary and natural boundary satisfying that $\Gamma_u \cup \Gamma_t = \partial\Omega$, $\Gamma_u \cap \Gamma_t = \emptyset$. $\bar{\mathbf{u}}$ and $\bar{\mathbf{t}}$ are the prescribed displacement and traction on Γ_u

and Γ_t . $\bar{\mathbf{b}}$ denotes to the prescribed body force in Ω . Introducing the standard variation argument to Eq.12 leads to the following HR weak form:

$$\text{find } \boldsymbol{\sigma}, \mathbf{u} \in H_1 \quad \begin{aligned} a(\delta \boldsymbol{\sigma}, \boldsymbol{\sigma}) + b(\delta \boldsymbol{\sigma}, \mathbf{u}) &= g(\delta \boldsymbol{\sigma}) \quad \forall \delta \boldsymbol{\sigma} \in H_1 \\ b(\boldsymbol{\sigma}, \delta \mathbf{u}) &= f(\delta \mathbf{u}) \quad \forall \delta \mathbf{u} \in H_1 \end{aligned} \quad (13)$$

where $a : L_2 \times L_2 \rightarrow \mathbb{R}$, $b : L_2 \times L_2 \rightarrow \mathbb{R}$ are bilinear forms:

$$a(\delta \boldsymbol{\sigma}, \boldsymbol{\sigma}) = \int_{\Omega} \boldsymbol{\varepsilon}(\delta \boldsymbol{\sigma}) : \boldsymbol{\sigma} d\Omega \quad (14)$$

$$b(\boldsymbol{\sigma}, \mathbf{u}) = - \int_{\Gamma} \mathbf{u} \cdot \boldsymbol{\sigma} \cdot \mathbf{n} d\Gamma + \int_{\Omega} \mathbf{u} \cdot \boldsymbol{\sigma} \cdot \nabla d\Omega + \int_{\Gamma_u} \mathbf{u} \cdot \boldsymbol{\sigma} \cdot \mathbf{n} d\Gamma \quad (15)$$

and g, f are the linear operators evaluated by

$$g(\delta \boldsymbol{\sigma}) = \int_{\Gamma_u} \mathbf{n} \cdot \delta \boldsymbol{\sigma} \cdot \bar{\mathbf{u}} d\Gamma \quad (16)$$

$$f(\delta \mathbf{u}) = - \int_{\Gamma_t} \delta \mathbf{u} \cdot \bar{\mathbf{t}} d\Gamma - \int_{\Omega} \delta \mathbf{u} \cdot \bar{\mathbf{b}} d\Omega \quad (17)$$

In Hellinger-Reissner reproducing kernel gradient smoothing framework, the displacement \mathbf{u} is approximated by traditional meshfree shape functions, namely \mathbf{u}^h :

$$\mathbf{u}^h(\mathbf{x}) = \sum_{I=1}^{n_p} \Psi_I(\mathbf{x}) \mathbf{d}_I \quad (18)$$

On the other hand, the components of stress tensor is assumed as a polynomial in each background cells:

$$\sigma_{ij}^h(\mathbf{x}) = \mathbf{q}^T(\mathbf{x}) \mathbf{c}_{ij}, \quad \text{in } \Omega_C \quad (19)$$

with

$$\mathbf{q}(\mathbf{x}) = \{1, x, y, \dots, y^{p-1}\}^T \quad (20)$$

Theorem 1.

$$\sup_{\boldsymbol{\sigma}^h \in Q} \|\boldsymbol{\sigma} - \boldsymbol{\sigma}^h\|_e \leq Ch^p |\boldsymbol{\sigma}| \quad (21)$$

Proof.

$$\sigma_{ij}(\mathbf{x}) = \sigma_{ij}(\mathbf{0}) + x\sigma_{ij} \quad (22)$$

□

3.2 Thin plate problems

$$\begin{aligned}
\mathcal{L}(\mathbf{M}, w) = & \int_{\Omega} \frac{1}{2} \boldsymbol{\kappa}(\mathbf{M}) : \mathbf{M} d\Omega \\
& - \int_{\Gamma_w} V_{\mathbf{n}}(\mathbf{M}) \bar{w} d\Gamma + \int_{\Gamma_{\theta}} M_{\mathbf{nn}}(\mathbf{M}) \bar{\theta}_{\mathbf{n}} d\Gamma - P(\mathbf{M}) \bar{w}|_{\Gamma_c} \\
& + \int_{\Gamma_M} \theta_{\mathbf{n}}(w) (M_{\mathbf{nn}} - \bar{M}_{\mathbf{nn}}) d\Gamma - \int_{\Gamma_V} w (V_{\mathbf{n}} - \bar{V}_{\mathbf{n}}) d\Gamma \\
& - w(P - \bar{P})|_{\Gamma_p} + \int_{\Omega} w(\nabla \cdot \mathbf{M} \cdot \nabla + \bar{q}) d\Omega
\end{aligned} \tag{23}$$

$$\text{find } \mathbf{M}, w \in H_2 \quad \begin{aligned} a(\delta \mathbf{M}, \mathbf{M}) + b(\delta \mathbf{M}, w) &= g(\delta \mathbf{M}) & \forall \delta \mathbf{M} \in L_2 \\ b(\mathbf{M}, \delta w) &= f(\delta w) & \forall \delta w \in H_2 \end{aligned} \tag{24}$$

$$a(\delta \mathbf{M}, \mathbf{M}) = \int_{\Omega} \boldsymbol{\kappa}(\delta \mathbf{M}) : \mathbf{M} d\Omega \tag{25}$$

4 Error analysis for HR gradient smoothing mesh-free formulation

Appendix A

In this appendix, we define some functional operator used in the main sections. Firstly, the energy norms for elasticity problems and thin plate problems are defined by:

$$\|\boldsymbol{\sigma}\|_e = \frac{1}{2} a_2(\boldsymbol{\sigma}, \boldsymbol{\sigma}) = \int_{\Omega} \frac{1}{2} \boldsymbol{\varepsilon}(\boldsymbol{\sigma}) : \boldsymbol{\sigma} d\Omega \tag{26}$$

$$\|\mathbf{M}\|_e = \frac{1}{2} a_4(\mathbf{M}, \mathbf{M}) = \int_{\Omega} \frac{1}{2} \boldsymbol{\kappa}(\mathbf{M}) : \mathbf{M} d\Omega \tag{27}$$

References

- [1] T. Belytschko, Y. Y. Lu, L. Gu, Element-free Galerkin methods 37 (2) 229–256.
- [2] W. K. Liu, S. Jun, Y. F. Zhang, Reproducing kernel particle methods 20 (8-9) 1081–1106.