

## Response to Reviewer's Comments

Authors appreciate careful reading of the manuscript by the reviewers, and are thankful for helpful suggestions for its improvement. Authors have modified the manuscript substantially in light of the reviewer's comments. All the modifications and changes made are highlighted in the Marked Revised Manuscript. Issues and concerns raised by the reviewers are discussed as follows:

### Reviewer #1

*This manuscript provides a meshfree thin shell formulation based on the Hu-Washizu variational principle. The essential boundary conditions in the present formulation do not require additional artificial parameters, which can be considered insensitive to those in Nitsche and Penalty's approaches. The derivation is rigorous however several issues must be properly addressed before the publication. I recommend a major revision.*

**Comment 1.** *After Eq. 5, the formulation of theta needs to be provided.*

**Response:** Authors thank the reviewer for the suggestion. The expression to calculate rotation ( $\theta$ ) is derived as follows:

$$\begin{aligned} \epsilon_{3i} = 0 &\Rightarrow \begin{cases} \theta \cdot \mathbf{a}_\alpha = -\mathbf{v}_{,\alpha} \cdot \mathbf{a}_3 \\ \theta \cdot \mathbf{a}_3 = 0 \end{cases} \\ \Rightarrow \theta &= \underbrace{\theta \cdot \mathbf{a}_\alpha}_{-\mathbf{v}_{,\alpha} \cdot \mathbf{a}_3} \mathbf{a}^\alpha + \underbrace{\theta \cdot \mathbf{a}_3}_0 \mathbf{a}^3 = -\mathbf{v}_{,\alpha} \cdot \mathbf{a}_3 \mathbf{a}^\alpha \end{aligned} \quad (1)$$

Based on reviewer's suggestion Eq. (9) on Page 6 (lines 151) has been modified to provide more clarity regarding the calculation of rotation ( $\theta$ ).

**Comment 2.** *Consider using different symbols for the mid-surface displacement,  $v$  is always referring to velocity.*

**Response:** Authors appreciate reviewer's suggestion regarding the representation of mid-surface displacement. However, it has to be noted that present

research article doesnot deal with the calculation of velocity. Therefore, the authors believe that the use of notation  $\mathbf{v}$  to represent mid-surface displacement will not create confusion.

**Comment 3.**  $\boldsymbol{\theta}$  is the variation of  $\mathbf{a}_3$ , so  $\boldsymbol{\theta} \cdot \mathbf{a}_3 = 0$ . This relationship does not come from  $\epsilon_{3i} = 0$ , which was in Eq. (9).

**Response:** Authors appreciate the reviewer's insight regarding the calculation of rotation ( $\boldsymbol{\theta}$ ). In the authors' opinion, the equation  $\epsilon_{3i} = 0$  is equivalent with  $\boldsymbol{\theta} \cdot \mathbf{a}_3$ , which follows the Kirchhoff hypothesis of shear deformation. Previousy, Benzaken et al. [4] also adopted similar approach to calculate the rotation.

**Comment 4.** Eq. (10) seems to be wrong. Where is  $\mathbf{a}_{3,\alpha}$  and where is the most complicated term  $\boldsymbol{\theta}_{,\alpha}$ ?

**Reply:** Authors are thankful to the reviewer for the careful observation. The detailed derivation of curvature given in Eq. (10) is appended below:

$$\begin{aligned}
\kappa_{\alpha\beta} &= \frac{1}{2} (\mathbf{a}_{3,\alpha} \cdot \mathbf{v}_{,\beta} + \mathbf{v}_{,\alpha} \cdot \mathbf{a}_{3,\beta} + \mathbf{a}_\alpha \cdot \boldsymbol{\theta}_{,\beta} + \boldsymbol{\theta}_{,\alpha} \cdot \mathbf{a}_\beta) \\
&= \frac{1}{2} \left( \begin{aligned} &\underbrace{(\mathbf{a}_3 \cdot \mathbf{v}_{,\beta})_{,\alpha} - \mathbf{a}_3 \cdot \mathbf{v}_{,\alpha\beta}}_{\mathbf{a}_{3,\alpha} \cdot \mathbf{v}_{,\beta}} \\ &+ \underbrace{(\mathbf{a}_3 \cdot \mathbf{v}_{,\alpha})_{,\beta} - \mathbf{a}_3 \cdot \mathbf{v}_{,\alpha\beta}}_{\mathbf{v}_{,\beta} \cdot \mathbf{a}_{3,\alpha}} \\ &- \mathbf{a}_\alpha \cdot \underbrace{((\mathbf{v}_{,\gamma} \cdot \mathbf{a}_3)_{,\beta} \mathbf{a}^\gamma + \mathbf{v}_{,\gamma} \cdot \mathbf{a}_3 \mathbf{a}_{,\beta}^\gamma)}_{-\boldsymbol{\theta}_{,\beta}} \\ &- \mathbf{a}_\beta \cdot \underbrace{((\mathbf{v}_{,\gamma} \cdot \mathbf{a}_3)_{,\alpha} \mathbf{a}^\gamma + \mathbf{v}_{,\gamma} \cdot \mathbf{a}_3 \mathbf{a}_{,\alpha}^\gamma)}_{-\boldsymbol{\theta}_{,\alpha}} \end{aligned} \right) \tag{2} \\
&= \frac{1}{2} \left( \begin{aligned} &\underbrace{(\mathbf{a}_3 \cdot \mathbf{v}_{,\beta})_{,\alpha} + (\mathbf{a}_3 \cdot \mathbf{v}_{,\alpha})_{,\beta} - (\mathbf{v}_{,\alpha} \cdot \mathbf{a}_3)_{,\beta} - (\mathbf{v}_{,\beta} \cdot \mathbf{a}_3)_{,\alpha}}_0 \\ &- 2\mathbf{a}_3 \cdot \mathbf{v}_{,\alpha\beta} - \mathbf{v}_{,\gamma} \cdot \mathbf{a}_3 \underbrace{\mathbf{a}_\alpha \cdot \mathbf{a}_{,\beta}^\gamma}_{-\Gamma_{\alpha\beta}^\gamma} - \mathbf{v}_{,\gamma} \cdot \mathbf{a}_3 \underbrace{\mathbf{a}_\beta \cdot \mathbf{a}_{,\alpha}^\gamma}_{-\Gamma_{\alpha\beta}^\gamma} \end{aligned} \right) \\
&= (\Gamma_{\alpha\beta}^\gamma \mathbf{v}_{,\gamma} - \mathbf{v}_{,\alpha\beta}) \cdot \mathbf{a}_3
\end{aligned}$$

It has to bring to the notice of the reviewer that the detailed derivation of curvature can be found in previous studies by Benzaken et al. [4]. For the conciseness, a statement related to the derivation of curvature has been added in the revised manuscript on page 6 (line151).

**Comment 5.** Patchtest: table 2 is interesting. Eq. (62) assumes the solution is only polynomials on the mid-surface, which is already not a polynomial in the Cartesian coordinate. The flat model is simple, in this case, the parametric

domain is the same as Cartesian. I believe the error in the curved case is due to bad parametrization. In general, the solution should be able to reproduce the parametric polynomials if the integration and parametrization are both good.

**Response:** Authors are thankful to the reviewer for the careful insight. In the present study, the proposed approach as given in Eqs. (32, 33, 35, 36) was used to designate polynomial strains and stresses. It can be found from Eqs. (7) and (8), of the revised manuscript the strains were expressed by the in-plane covariant base ( $\mathbf{a}_i$ ) and the derivatives of displacement ( $\mathbf{v}_{,i}$ ). For the flat surface model, both of  $\mathbf{a}_i$  and  $\mathbf{v}_{,i}$  are polynomials, so the meshfree formulation can easily pass the patch test. However, in the case of the curved surface model, the  $\mathbf{a}_i$  turns to be non-polynomial due the parametrization of curvilinear coordinate system. As a result, even though the integration and parametrization are well poised, the approximated smoothed stresses cannot exactly reproduce the non-polynomial stresses. For this reason, the adopted approach in the present study was termed as "quasi-consistent".

**Comment 6.** *Example 5.2, figure (7) is distracting. The purpose of the newly designed method is to get rid of the penalty parameters. In general, the final penalty parameter should be  $E/h \times C$ , where  $C$  is a dimensionless coefficient. If one is testing the convergence rate of Nitsche or penalty methods, the penalty parameter needs to be scaled by the mesh size  $h$ , when the model is refined.*

**Response:** Based on the reviewer's suggestion, the artificial parameters shown in Figure (7) were scaled by shape function support size ( $s$ ) which can measure the grid size of discrete model ( $h$ ). In accordance with reference Benzaken et al. [4], the modified parameters were set as  $\alpha_{v\alpha} = \bar{\alpha}_v/s$ ,  $\alpha_{v3} = \bar{\alpha}_v/s^3$  and  $\alpha_\theta = \bar{\theta}/s$ . The parameters  $\alpha_{v\alpha}$ 's and  $\alpha_{v3}$  were redefined to represent in-plane displacements  $\mathbf{v} \cdot \mathbf{a}_\alpha$  and deflection  $\mathbf{v} \cdot \mathbf{a}_3$  respectively. After the parameters were scaled by support size ( $s$ ), both Nitsche's method and penalty method observed less parameter sensitivity. However, the scaled up parameters cannot completely eliminate the parameter sensitivity problem. To provide further clarity, the related statements are added in revised manuscript on Pages 17, 18 and 21.

**Comment 7.** *In Example 5.2, the authors provided the wrong reference value.  $-0.3024$  is the one under RM shell theory. In this case, I believe the value should be  $-0.3006$ . See [1] for more information.*

**Response:** Authors are thankful to the reviewer for pointing out the wrong reference value. The reference value has been changed to  $-0.3006$ . Accordingly, the related statement on Page 21 has been modified in the revised manuscript.

**Comment 8.** *In Example 6.2, also check if the reference value provided in this study is for RM shells [2].*

**Response:** Following the reviewer's suggestion, the reference values (0.094)

has been updated in Fig. 10 on Page 26. In order to show a better convergence performance, the meshfree discretizations were modified ranging from  $16 \times 16$  to  $40 \times 40$ . The related discussions were updated in the revised manuscript on Page 21.

**Comment 9.** *Scodelis-Lo roof, pinched hemisphere, and pinched cylinder are the most famous shell benchmark problems. In [3], the authors named them "shell obstacle course". These 3 examples are even harder than those finite deformation shell simulations. So a good shell formulation should be capable of passing these three challenges. It is strongly suggested that the authors add the pinched cylinder simulation to this manuscript.*

**Response:** Authors appreciate reviewer's suggestion. Authors also believe the pinched cylinder is one of the most common benchmark example for thin shell formulation. Besides, this example was also based on cylindrical coordinate system, which is similar to that of Scodelis-Lo roof problem. Therefore, taking into account the limitations of the content of current manuscript, the pinched cylinder problem was not considered. It will be considered as a further prospective.

## Reviewer #2

*With the aid of the Hu-Washizu variational principle and reproducing kernel smoothed gradients, an efficient and quasi-consistent meshfree Galerkin method is presented in this manuscript to solve thin shell problems. An outstanding merit of the method is that the essential boundary conditions can be enforced naturally. Computational formulas of the method are presented with some details. Numerical results are given to demonstrate the efficiency of the method.*

*The current manuscript is well presented and contains material worthy of publication. Acceptance of the manuscript is recommended. The authors are, however, encouraged to address the comments listed below.*

**Comment 1.** *Please check the grammar of the sentence below Eq. (22).*

**Response:** Authors are thankful to the reviewer for identifying the grammatical error. The sentence below Eq. (22) has been modified in the revised manuscript on Page 9 as "~~in which~~ where  $\Psi_I$  and  $d_I$  ~~is~~ represent the shape function and nodal coefficient tensor related by node  $\xi_I$ ". Besides, the manuscript was double checked to address other grammatical and typo issues.

**Comment 2.** *Why is only the quadratic function used for the basis function vector  $p$  in Eq. (23)?*

**Response:** In the present study, the proposed method is in the context of RKGSF framework that can be easily extended for the high order basis functions. However, for conciseness, only quadratic basis function was considered in this study which can be considered as a limitation. The formulation with high order basis functions will be considered in the further work and the related statements has been added in the conclusion of the revised manuscript on Page 28.

**Comment 3.** *Please provide the meaning of the symbol  $s_{\alpha I}$  in Eq. (25). What is the parameter value used in this paper?*

**Response:** The parameter  $s_{\alpha I}$  represents the support size of the shape function  $\Psi_I$ . Accordingly, the statements related to support size has been added on Page 9 (line 209). Besides, the authors have also checked the definitions of all the symbols in the revised manuscript. The value of characterized support size of shape function is taken as 2.5 for all the considered examples, which is reported on Page 20 (line 342).

**Comment 4.** *Fig. 2 contains two sets of integration points. Considering the computational burden, using only one set of integration points may be more beneficial for Galerkin meshfree methods. Therefore, it is recommended to provide some explanations.*

**Response:** In the present study, two integration schemes (blue circular integration points and red cross integration points) were considered depending on their contribution. For instance, in the case of blue circular integration scheme both domain integration and boundary integration were existed in each integration cell. Further, the total number of these blue integration points has been optimized from a global point of view to reduce the computation of meshfree shape functions and their first order derivatives [5]. On the other hand, the red cross integration scheme was employed for the assembly of stiffness matrix which involve only the integration accuracy and does not consider any boundary integration. Thus, the traditional 3-point integration scheme is sufficient to carry out this task. Therefore, if the Galerkin formulation adopts the identical points with the blue circular integration scheme, the number of integration points for assembly were increased by two-fold. This will reduce the efficiency of the Galerkin meshfree method. Taking into account the computational burden, the two different integration schemes adopted in the present study were found to be the ideal choice for the proposed method. To provide more clarity, the related discussion has been added in the revised manuscript on Page 16 (lines 297).

**Comment 5.** *On page 13, the authors stated that "Even with  $p$ -th order variational consistency, the proposed formulation can not exactly reproduce the solution spanned by basis functions". The reproducibility is important for Galerkin meshfree methods. So, just suggestion, is it possible to give some more explicit explanations.*

**Response:** The reproducibility is one of the essential requirement for the Galerkin formulation variational consistency to achieve an optimal accuracy. Based on reviewer’s suggestion, the discussion related to the reproducibility and consistency conditions were added on Page 2 of the revised manuscript.

*6. Numerical results of Nitsche’s method and penalty method are also shown in Section 5.1. The values of penalty parameters used in the two methods should be provided. In addition, it is encouraged to provide some observations on numerical results of the RKGSI-penalty in Figure 4 and Tables 1 and 2.*

**Reply:** Based on reviewer’s suggestion, to provide further clarity the artificial parameters used in Nitsche’s method and penalty method were updated on Page 19. Additional discussions for RKGSI-penalty were also added on Pages 19 and 20 of the revised manuscript.

*7. On pages 32-34, some reference information such as journal title and year of publication is missed.*

**Reply:** Authors thank the reviewer for the careful observation. All the reference information were checked and modified in the revised manuscript.

## References

- [1] P. Krysl, J.S. Chen, Benchmarking computational shell models, *Archives of Computational Methods in Engineering* 30 (2023) 301–315.
- [2] J. Kiendl, K.U. Bletzinger, J. Linhard, R. Wüchner, Isogeometric shell analysis with Kirchhoff–Love elements, *Computer Methods in Applied Mechanics and Engineering* 198 (2009) 3902–3914.
- [3] T. Belytschko, H. Stolarski, W.K. Liu, Stress projection for membrane and shear locking in shell finite elements, *Computer Methods in Applied Mechanics and Engineering* 51 (1985) 221–258.
- [4] J. Benzaken, J.A. Evans, S.F. McCormick, R. Tamstorf, Nitsche’s method for linear Kirchhoff–Love shells: Formulation, error analysis, and verification, *Computer Methods in Applied Mechanics and Engineering* 374 (2021) 113544.
- [5] D. Wang, J. Wu, An inherently consistent reproducing kernel gradient smoothing framework toward efficient Galerkin meshfree formulation with explicit quadrature, *Computer Methods in Applied Mechanics and Engineering* 349 (2019) 628–672.