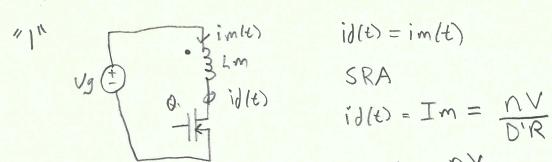


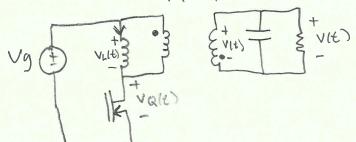
On state switch current



$$id(t) = Im = \frac{nV}{D'R}$$

b) $\frac{10(t) = \frac{n \vee}{D' R}}{} + 1$

42"



$$V_Q(t) = V_g - V_L(t)$$

$$V_Q(t) = V_Q + \frac{V(t)N1}{N2}$$

a)
$$V_Q(t) = Vg + \frac{V}{N}$$

+1

c) If applying small ripple approximation:

$$Idrms = \frac{nV}{DR} \sqrt{D}$$

+0.5

HW4

$$-Vg + V_L(t) = 0$$

$$V_L(t) = Vg$$

$$ic(t) + \frac{V(t)}{R} = 0$$

$$ic(t) = \frac{V(t)}{R}$$

$$\frac{V_L(t)}{N_I} = \frac{-V(t)}{N_A}$$

$$\frac{V_L(t)}{N_A} = \frac{-V(t)}{N_A}$$

$$\frac{V_L(t)}{N_A} = \frac{-V(t)}{N_A}$$

$$i_2(t) = i_2(t) + \frac{v_1(t)}{R}$$

$$A = \frac{1}{12}(t) + \frac{1}{12}(t$$

ict = im(t) - V(t)

HW4 a cont) Voit-Second Balance 0 = Vg D1+ - \ D2+ O(D3) Vg D1= - D2 $\frac{\vee}{\vee q} = \frac{D_1}{D_2} N$ +2b) In DCM, since you cannot apply SRA, apply charge balance in a manner that results in an expression in terms of average output current "Charge Balance" iott $-\frac{1}{\sqrt{Victer}} + \frac{1}{\sqrt{Victer}} + \frac{1}{\sqrt{Vi$ ZiD(t)>= K to Dats (1) (1) (2) (3) (3) (4) (4) (5) (5) (6) (7) (7) (7) (8) (1) (1) (1) (1) (1) (2) (3) (4) (4) (5) (5) (7) (7) (7) (8) (1)iz(t) relates to i, (t) during "2" iap = ia (t=D, Ts) 0 = i,(t)n, + i2(t)n2 at t=D,TS $O = -im(t=D_1TS)n_1 + i_2(t=D_1TS)n_2$ $O = -i|p_1 + i_2p_1$ $O = -i|p_1 + i_2p_1$

HW 4

$$b cont$$
)

 $i_1'p = \frac{Vg}{Lm} D_1 Ts$
 $O = -\frac{Vg}{Lm} D_1 Ts N_1 + iap N_2$
 $i_2 p = \frac{Vg}{Lm} D_1 Ts N_1 = \frac{Vg}{Lm} \frac{D_1 Ts}{N}$ (a)

 $solve (1) + (a) for iap + Da$
 $+2 Da = \frac{a Lm Vn}{D_1 R Ts Vg}$; $iap = \frac{D_1 T Vg}{Lm N}$
 $c) imtb$
 $c) imtb$
 $at boundary of CCM/DCM D_3 = 0$
 $adil = i_1'p = \frac{Ug}{Lm} D_1 Ts$
 $at boundary of complete D_1 Ts$
 $at boundary of$

HW4

Simuliak at critical conduction

 $D_1 = .3333$

+1.5

D2= .6667

if eak = 1, p = 0.64 A

Rcrit = 28.1251

