

A regime diagram of a slurry F-layer

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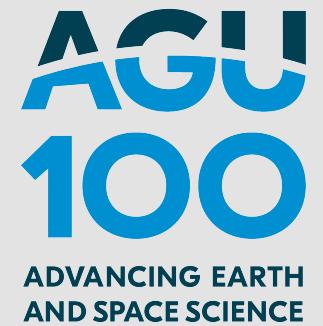
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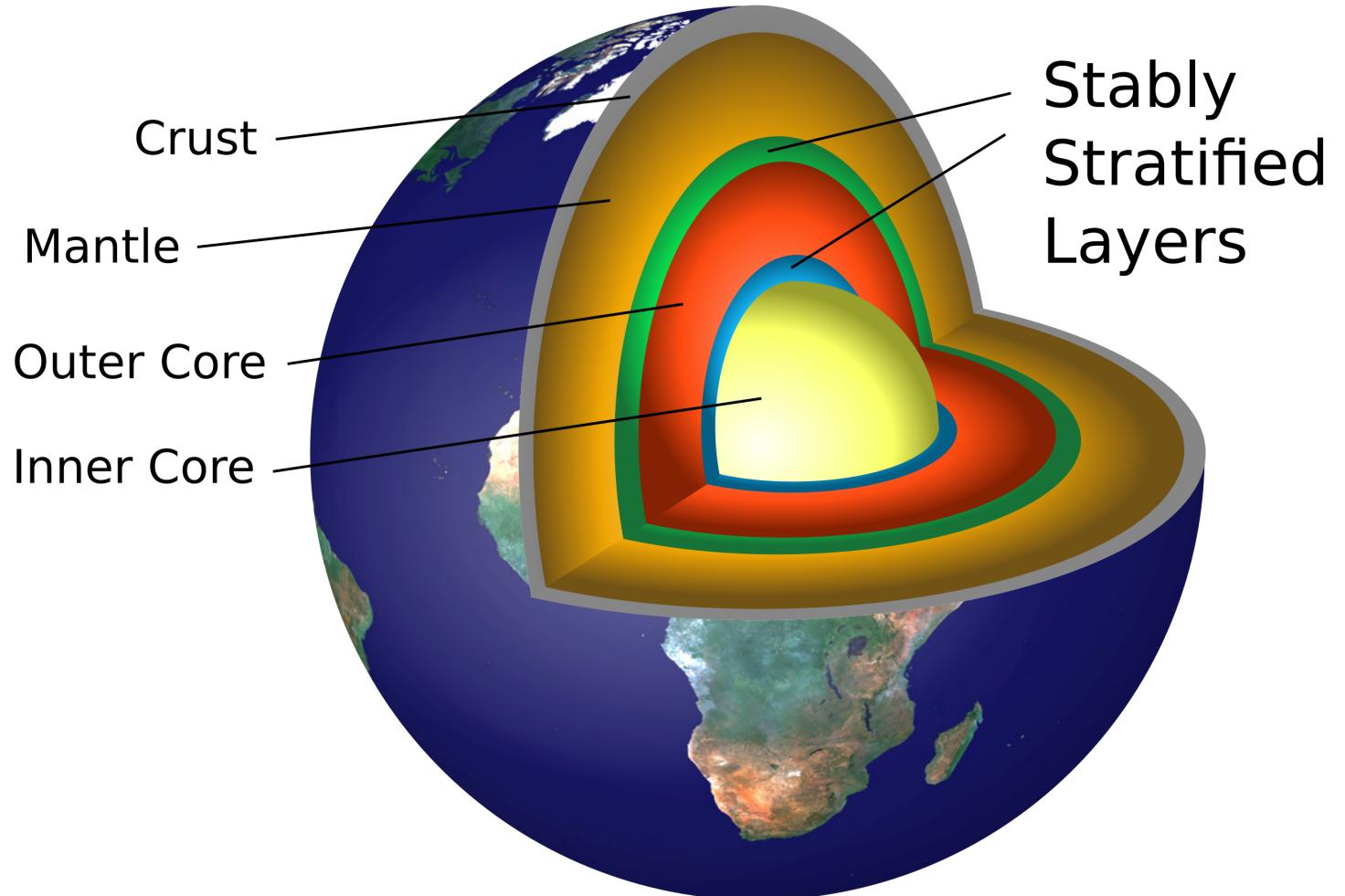


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Stratified layers in the core?

- Classic picture: vigorous convection \Rightarrow well-mixed, liquid, metallic alloy
- Adiabatically stratified and homogeneous
- Thin boundary layers
- Recent picture: stably stratified layers exist beneath the CMB and above ICB
- How did they develop? How are they sustained? How do they impact core dynamics?

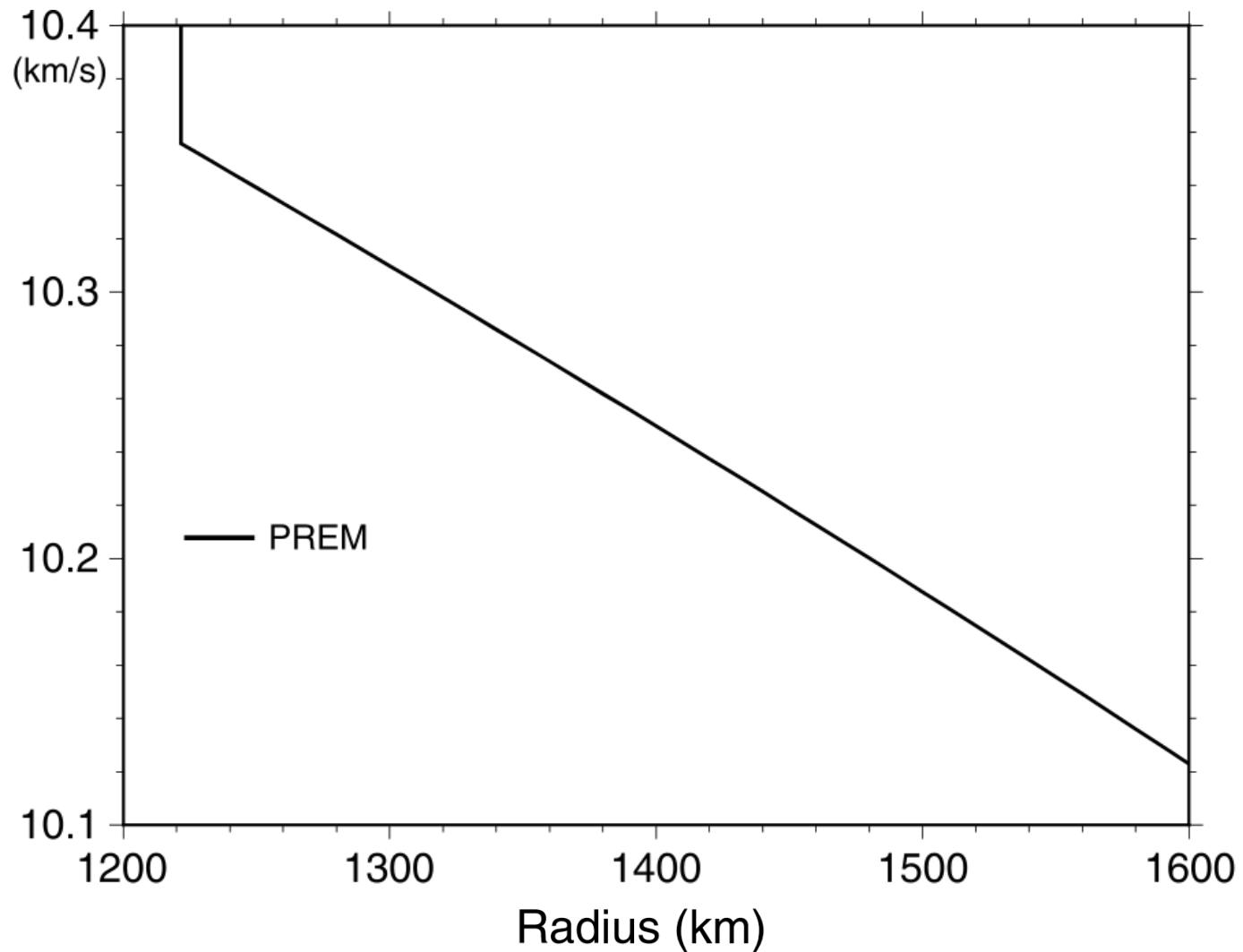


Hardy and Wong (2019)

Seismic observations of the F-layer

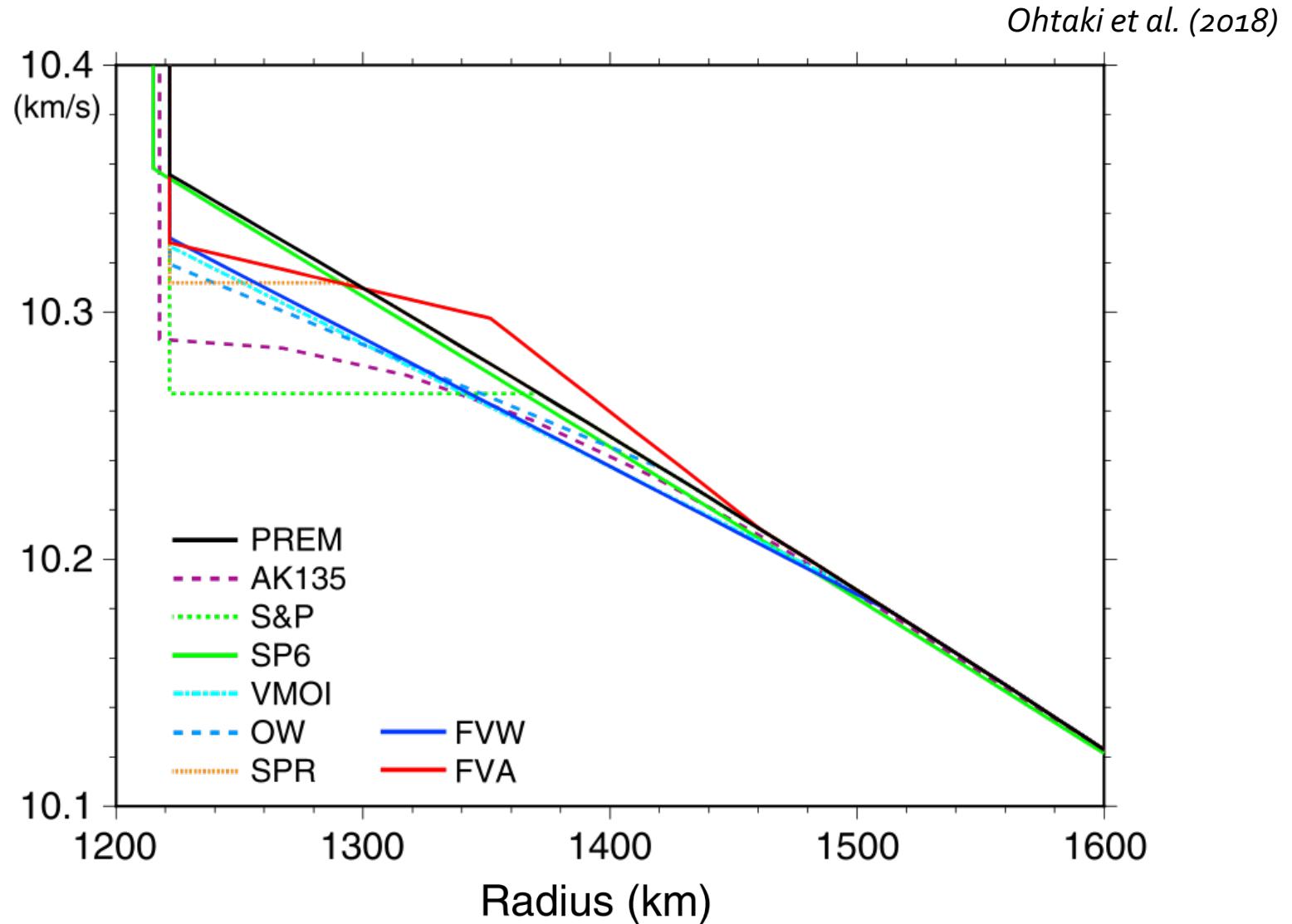
- PREM assumes that the liquid core is adiabatically stratified
- Slower than expected P wave speed observed
- P wave speed is inversely proportional to density

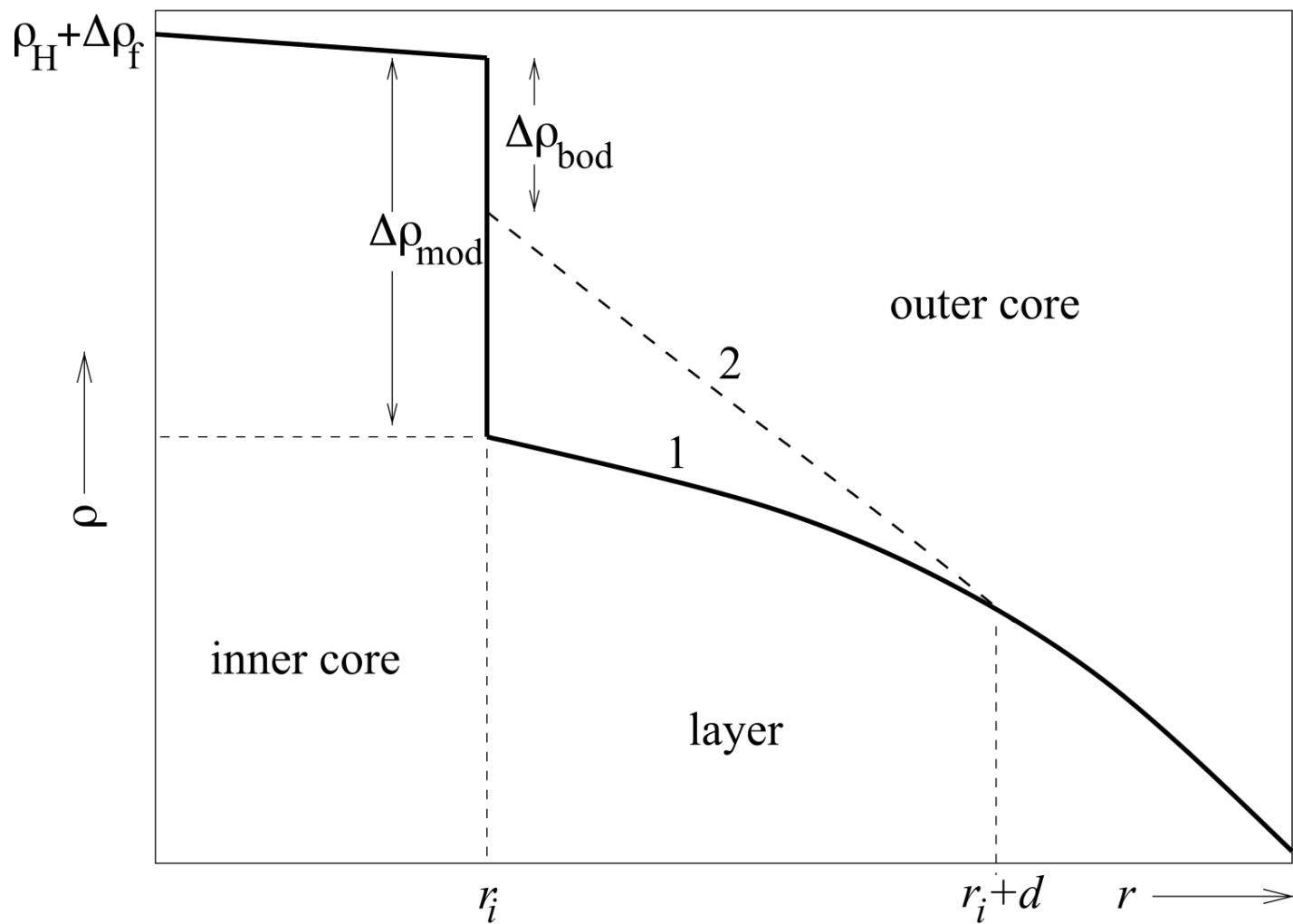
Ohtaki et al. (2018)



Seismic observations of the F-layer

- PREM assumes that the liquid core is adiabatically stratified
 - Slower than expected P wave speed observed
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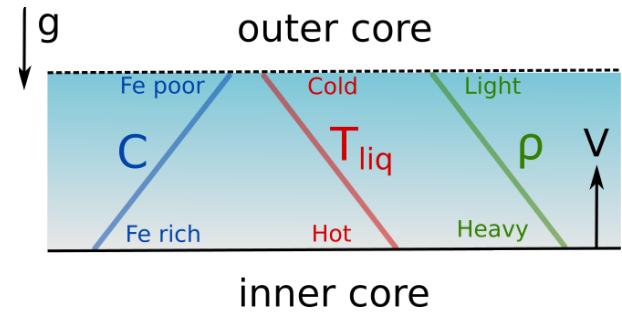


Gubbins et al. (2008)

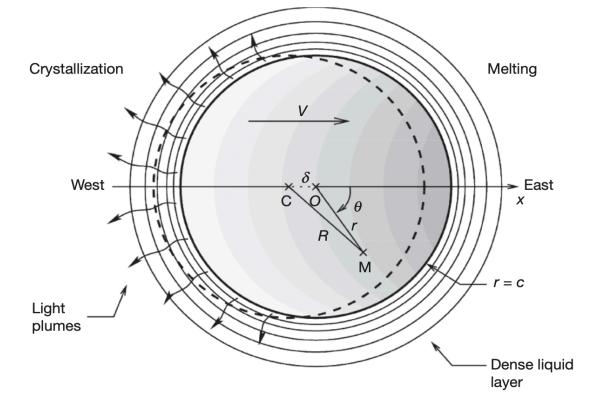
Seismic density structure

- Discrepancy between $\Delta\rho_{mod}$ and $\Delta\rho_{bod}$
- This infers a stably stratified layer exists
- How can light elements pass through the layer and out into the bulk of the core?
- Layer is not a thermal boundary layer

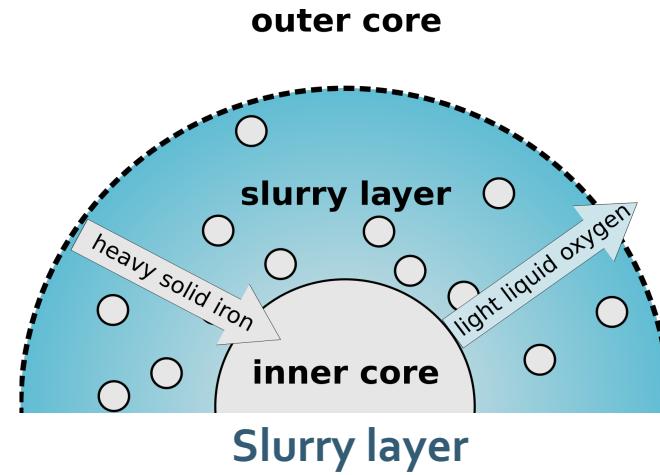
Possible scenarios



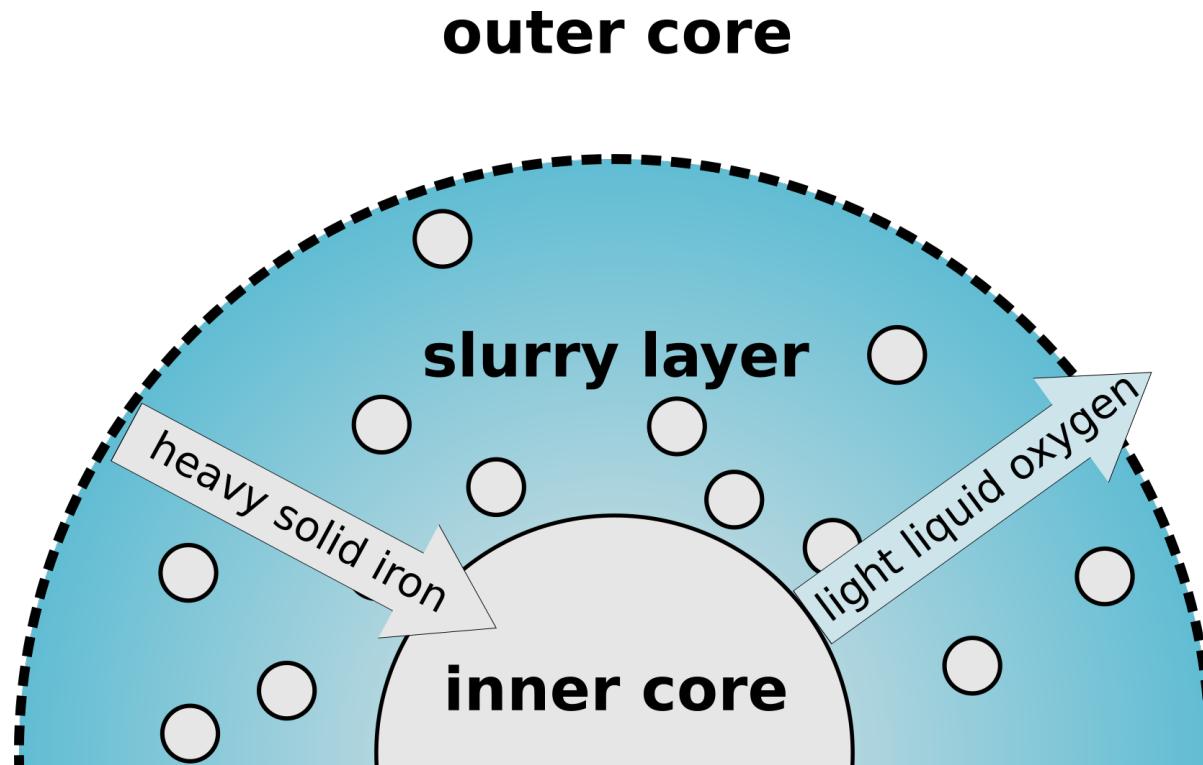
Thermochemical layer on the liquidus
(Gubbins *et al.* 2008)



Convective translation
(Alboussière *et al.* 2010)



(Wong *et al.* 2018, Loper and Roberts 1977)



Slurry (iron snow) layer

- Two component (iron and oxygen), two phase (solid and liquid) system
- Formation and transport of solid phase provides a way for light element to cross a stably stratified layer
- Solid fraction is small

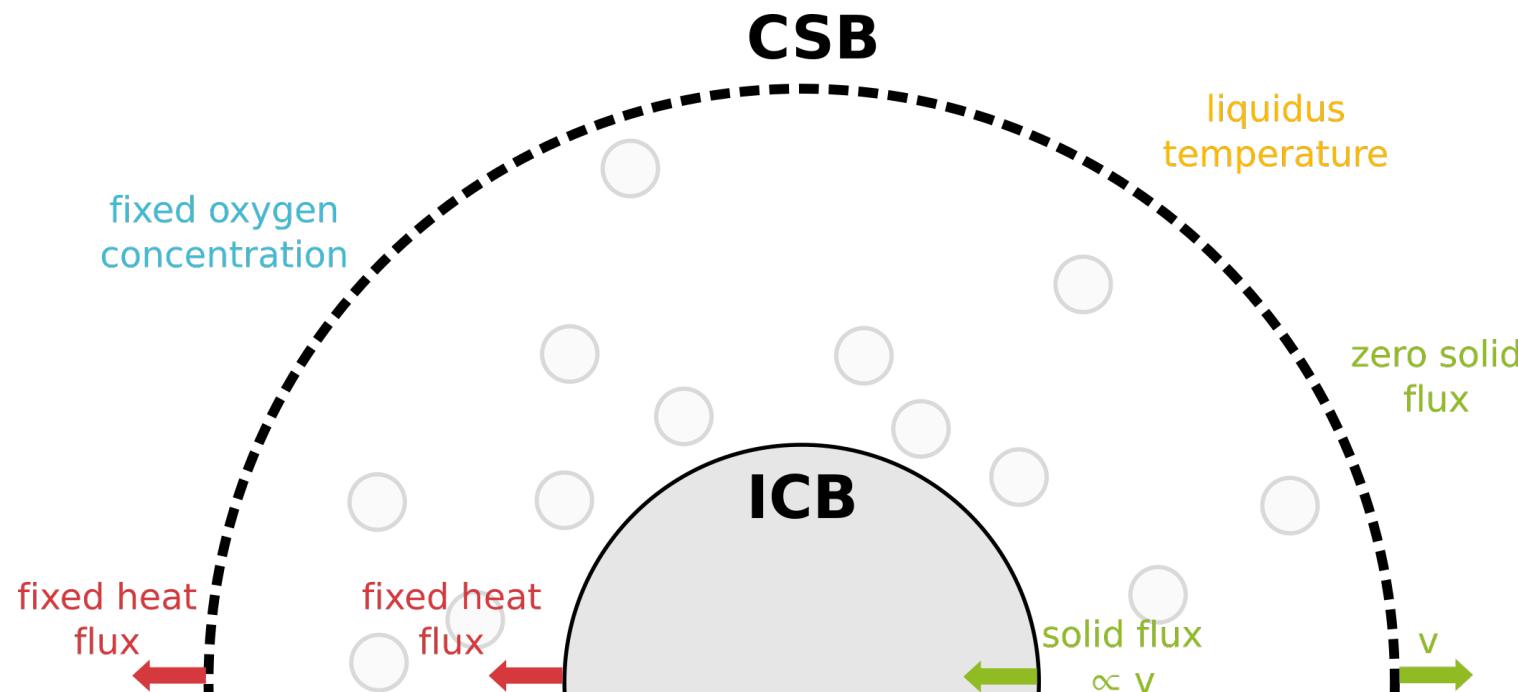
For full details see: Wong et al. (2018)
<https://doi.org/10.1093/gji/ggy245>

Dimensionless parameters:

$$\text{P\'eclet} \sim Q_i$$

$$\text{Stefan} \sim \frac{Q_{sl}}{Q_i}$$

$$\text{Lewis} \sim k$$



Slurry (iron snow) layer

- Governing equations:
 - Liquidus
 - Conservation of oxygen
 - Conservation of energy
- Reference frame of fixed layer thickness moving at IC growth rate
- Static slurry, 1D and spherical geometry

Geophysical constraints

	$\Delta\rho_{mod} \text{ (kg m}^{-3}\text{)}$	$\Delta\rho_{bod} \text{ (kg m}^{-3}\text{)}$
Maximum	1000 (Masters and Gubbins 2003)	1100 (Tkalčić et al. 2009)
Minimum	600 (PREM)	520 ± 240 (Koper and Dombrovský 2005)

- Seismic density jump across the layer

$$\Delta\rho \equiv \rho_{sl}(r_i) - \rho_{PREM}(r_{sl}) \equiv \Delta\rho_{mod} - \Delta\rho_{bod} < 720 \text{ kg m}^{-3}$$

- CMB heat flow (*Lay et al. 2008*)

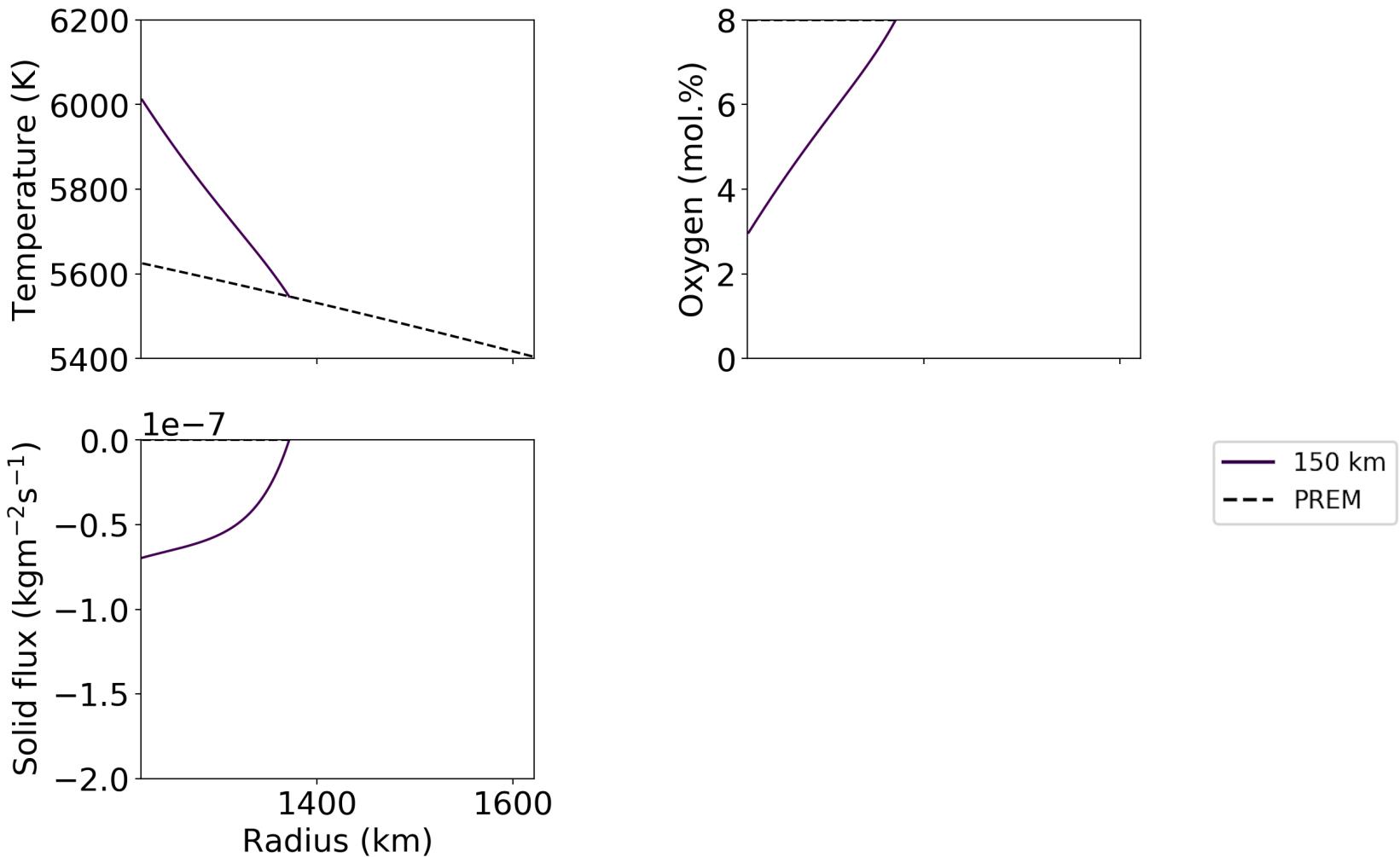
$$5 < Q^c < 15 \text{ TW}$$

- ICB heat flow (*Pozzo et al. 2014*)

$$Q^i < 2 \text{ TW}$$

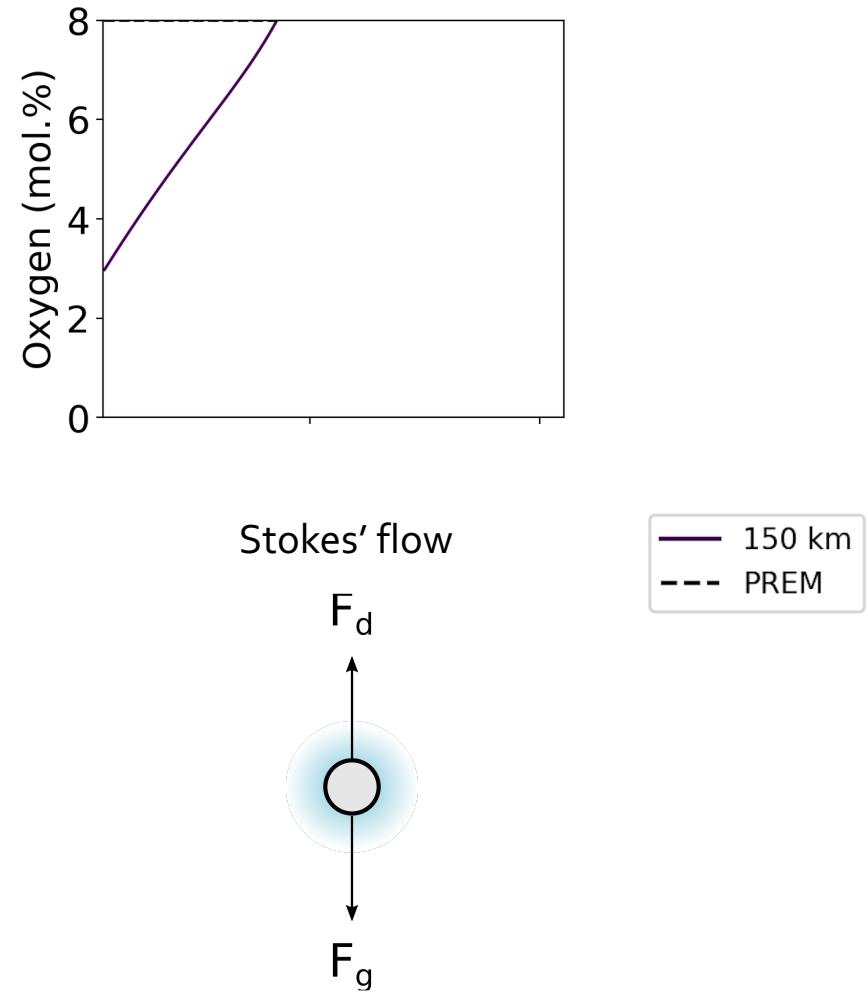
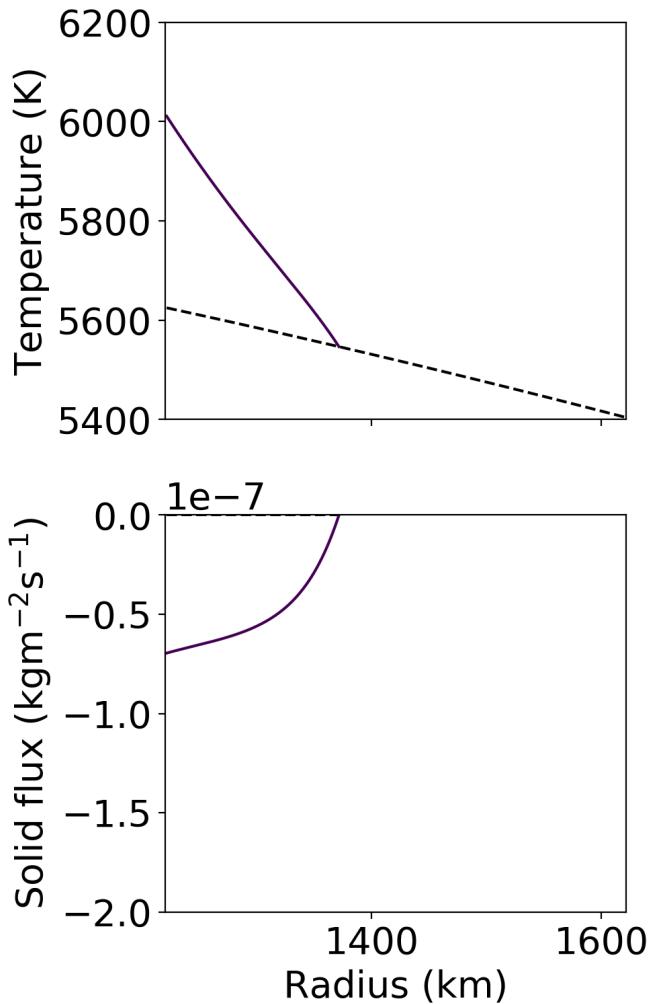
Results

- Temperature gradient is “locked” to the oxygen gradient via the liquidus
- Solid flux is negative down towards ICB



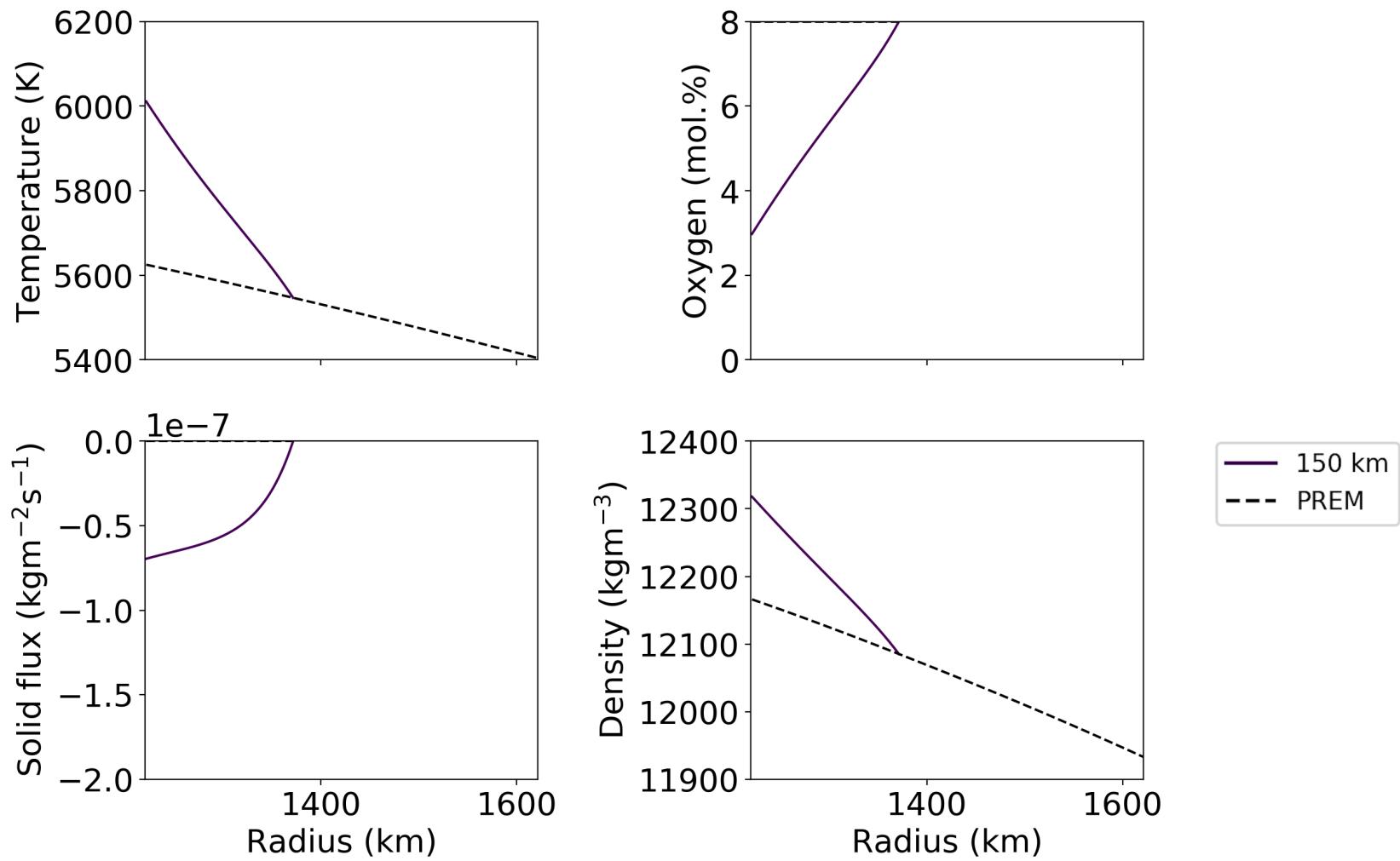
Results

- Temperature, oxygen and solid fraction contribute to density anomaly
- Solid fraction obtained from solid flux by assuming Stokes' flow



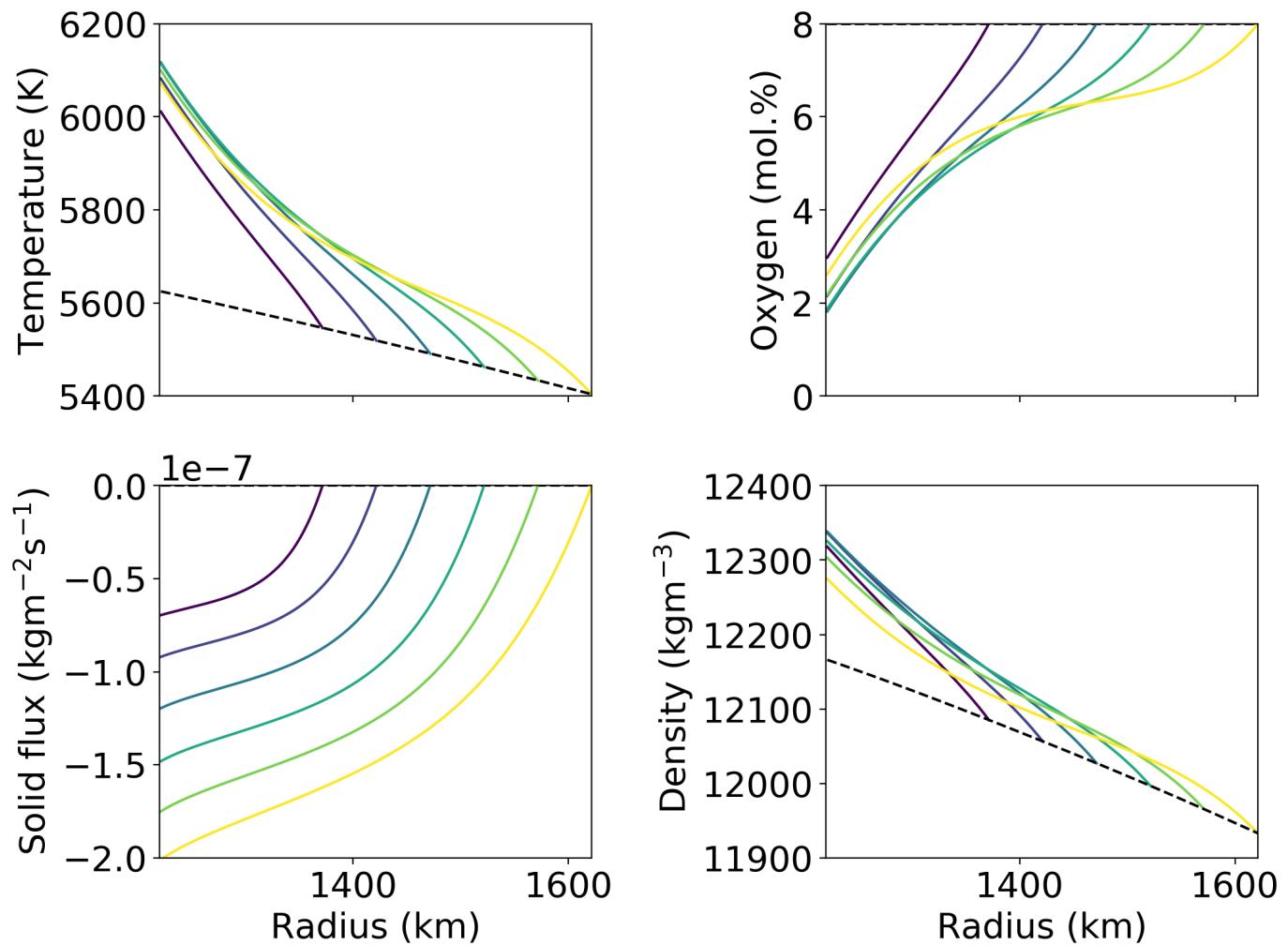
Results

- Slurry density and density gradient exceeds PREM \Rightarrow a stably stratified layer



Results

- Increasing layer thickness increases the density jump across the layer
- Layer becomes destabilised at mid-depths



Regime diagram

Layer thickness = 150 km

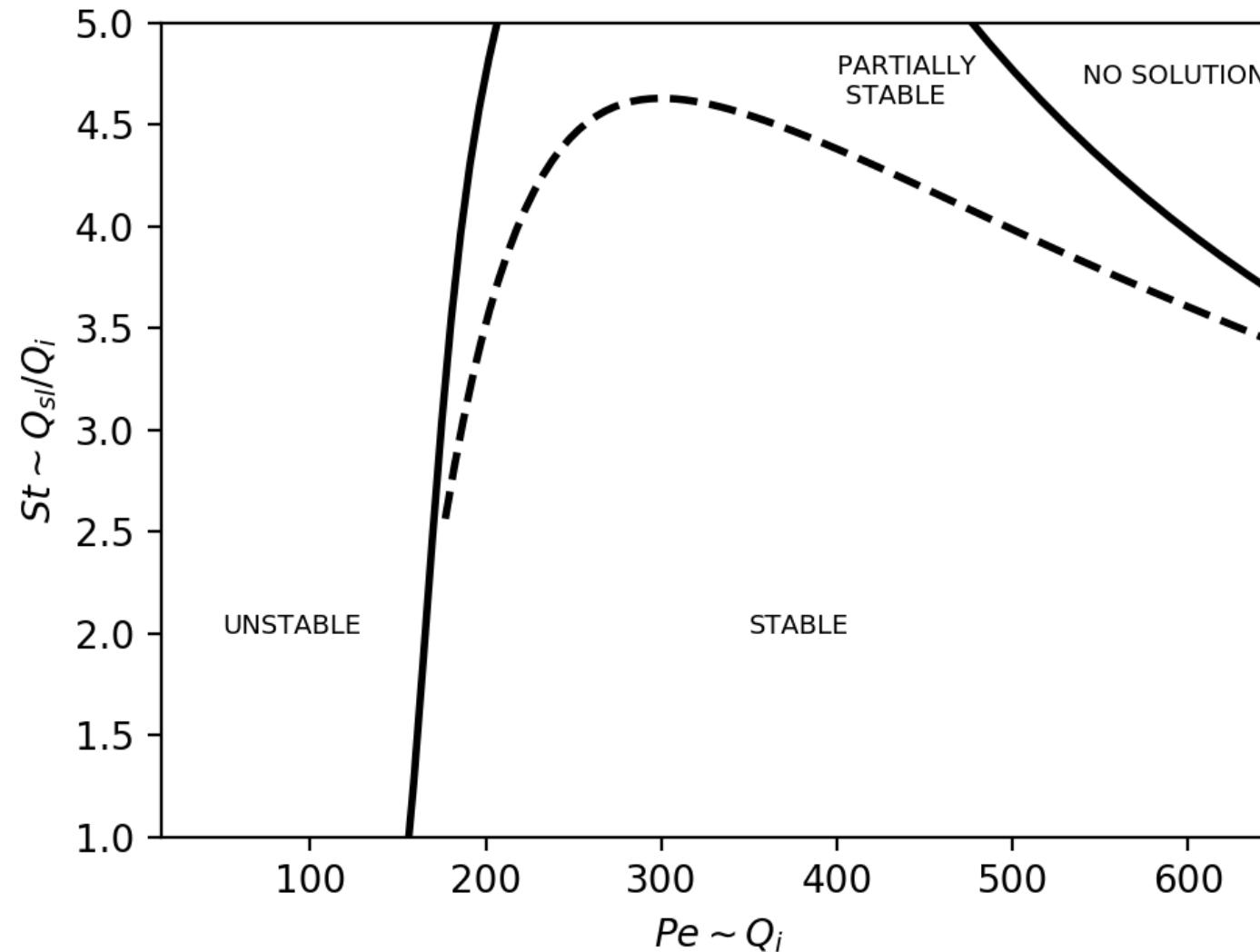
STABLE: slurry density and density gradient exceed PREM

PARTIALLY STABLE: slurry density and density gradient exceeds PREM over 100+ km

UNSTABLE: slurry density or density gradient is below PREM

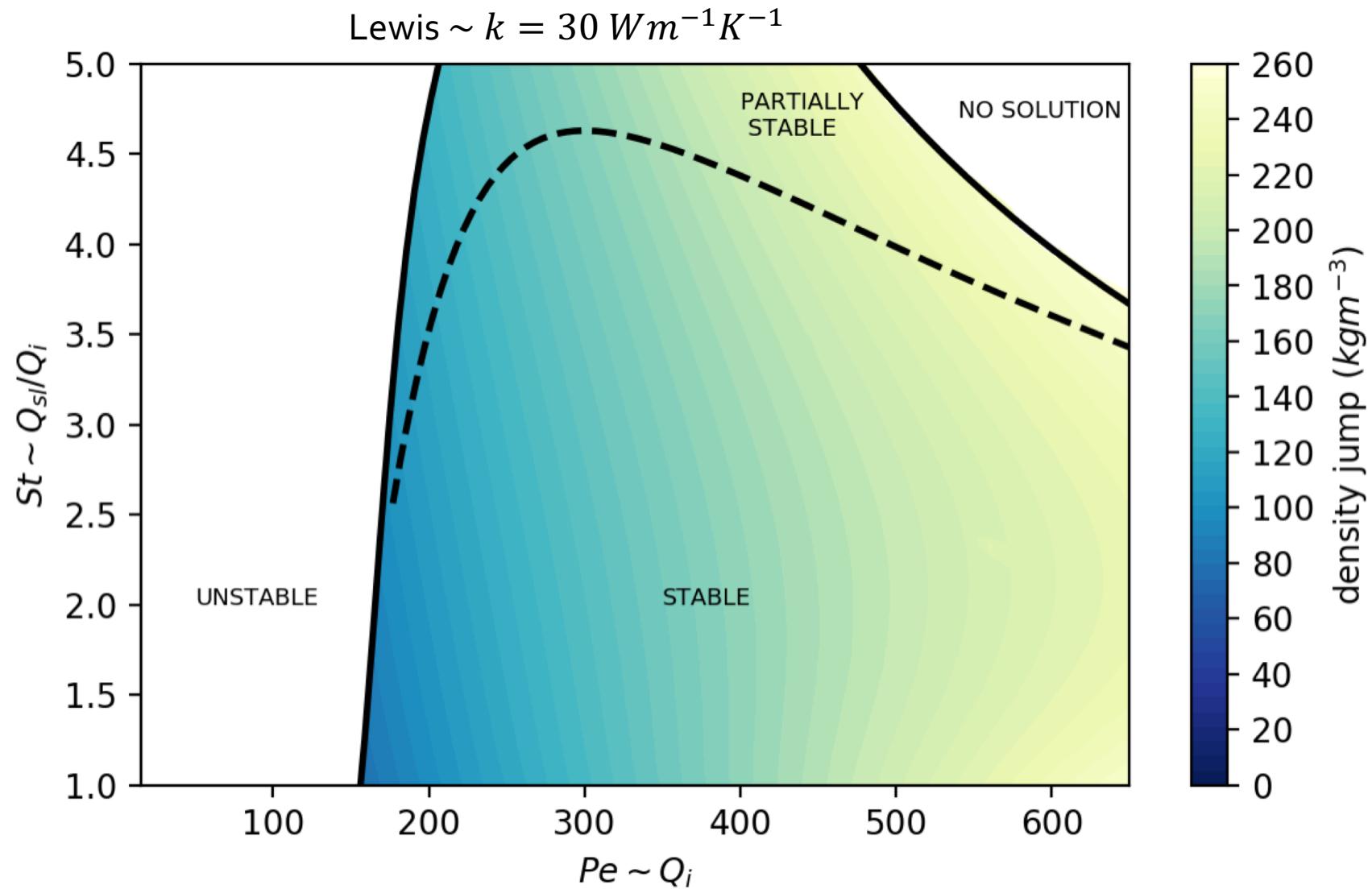
NO SLURRY

$$\text{Lewis} \sim k = 30 \text{ W m}^{-1} \text{ K}^{-1}$$



Regime diagram

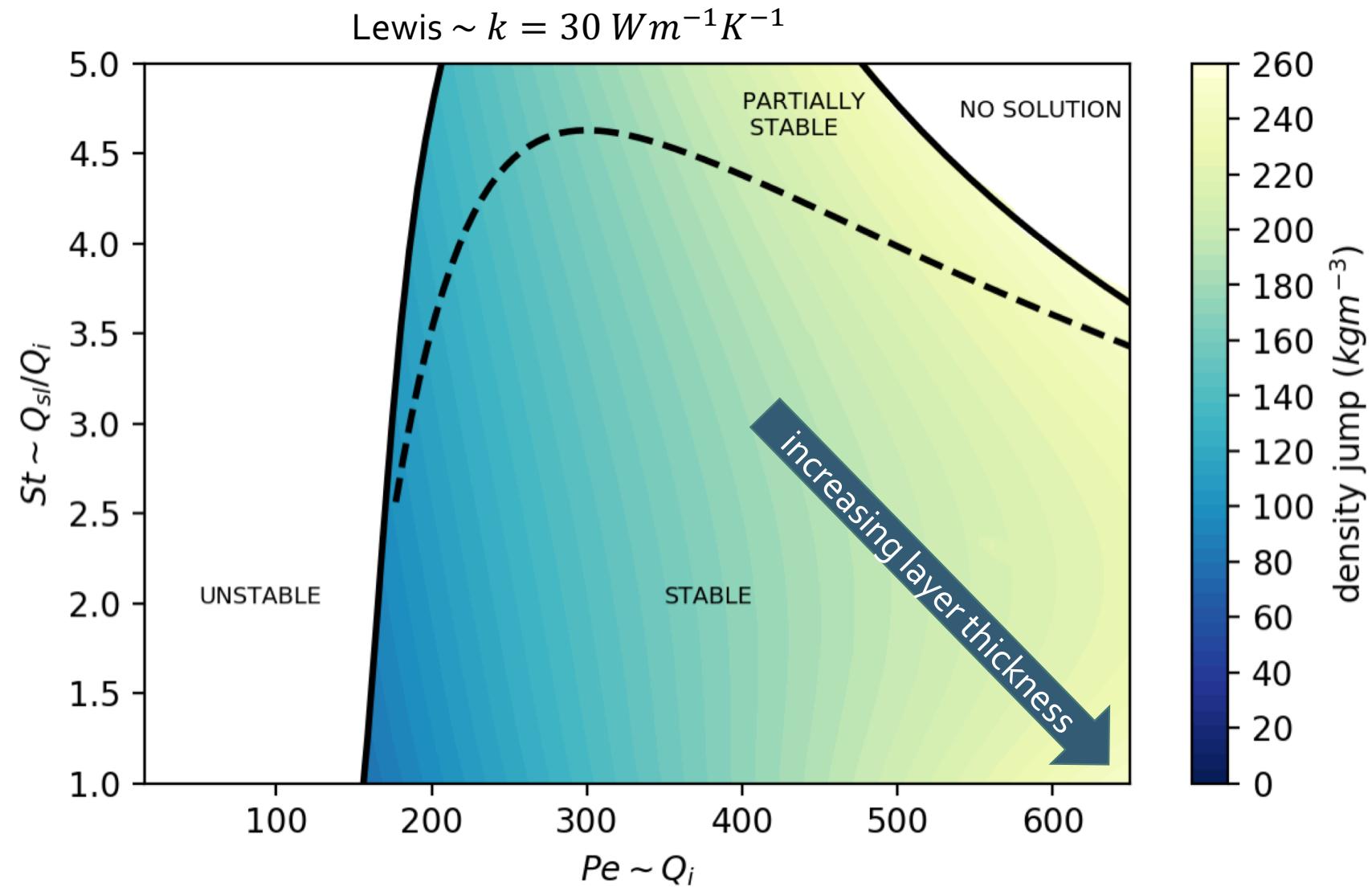
The greatest density jumps are found in the high Peclet, high Stefan number region.



Regime diagram

The greatest density jumps are found in the high Peclet, high Stefan number region.

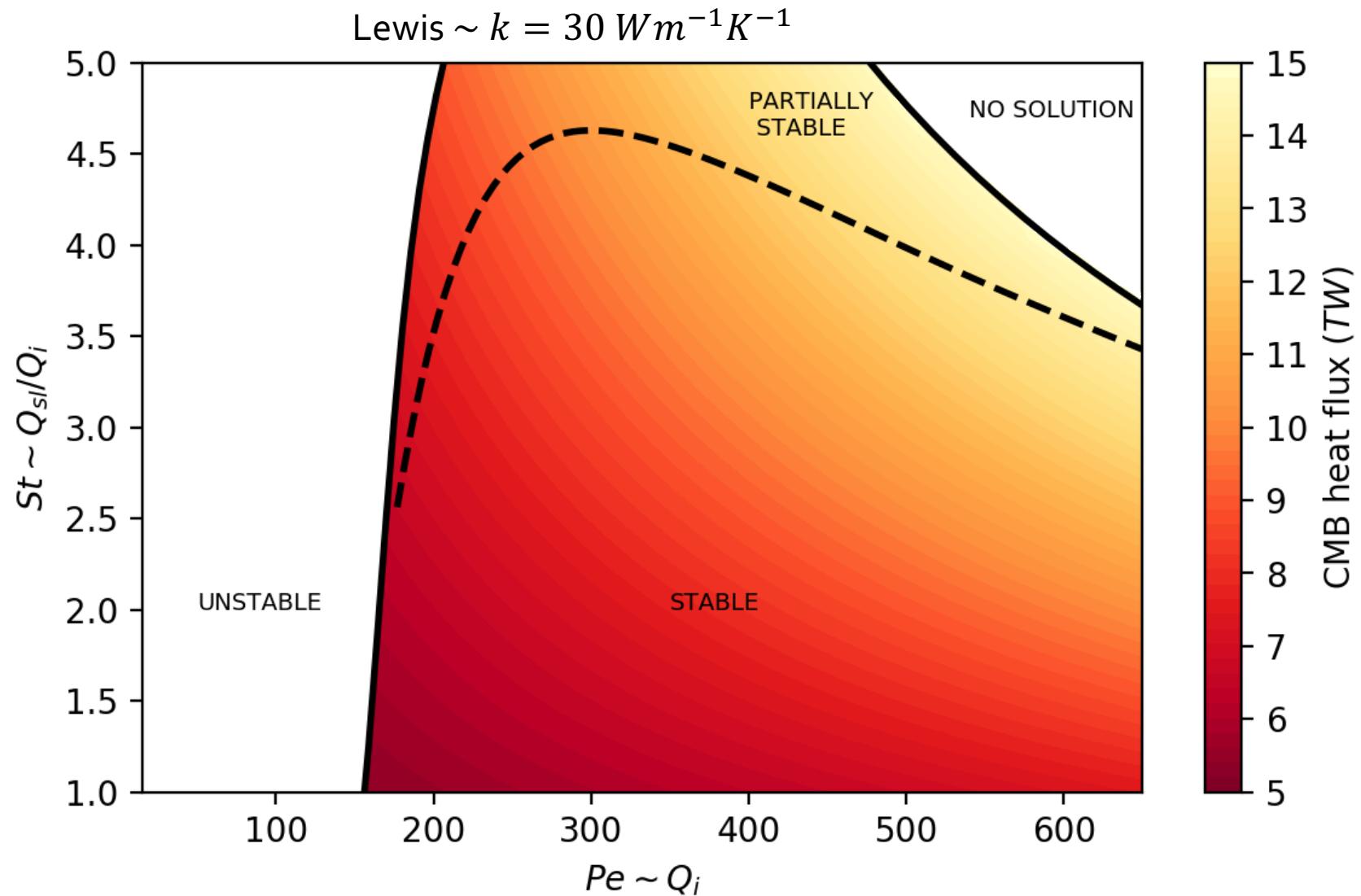
Increasing layer thickness is in high Peclet, low Stefan number region.



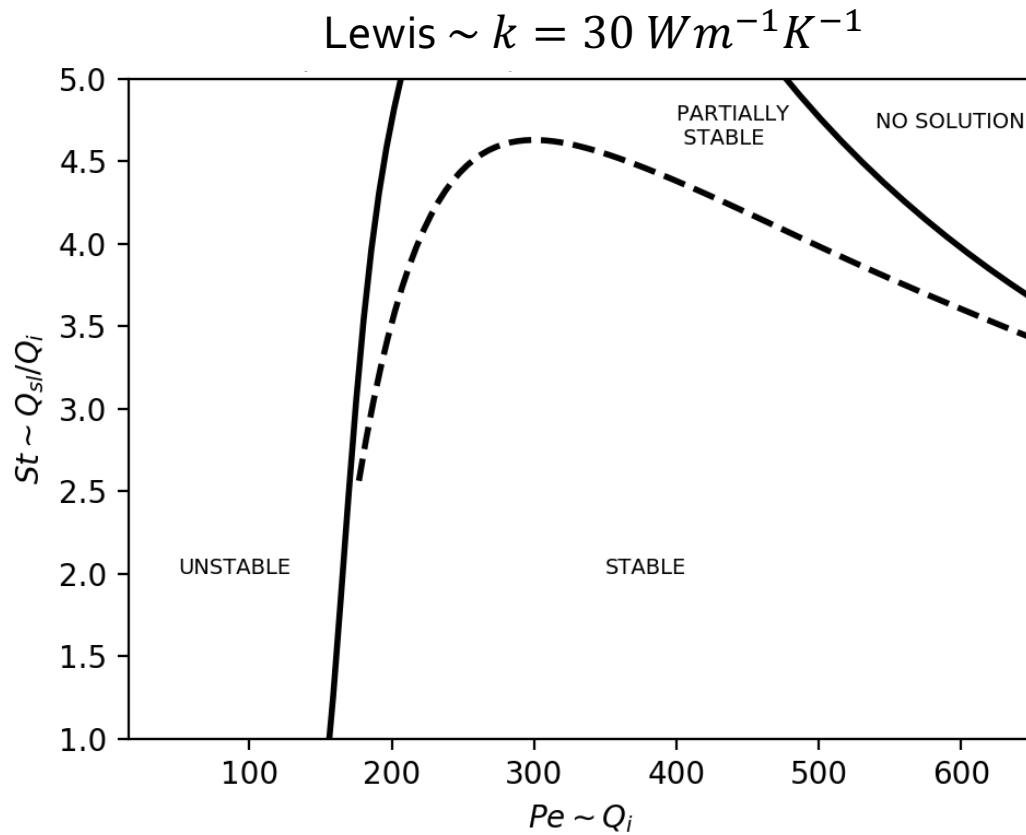
Regime diagram

CMB heat flow is proportional to the imposed CSB heat flow.

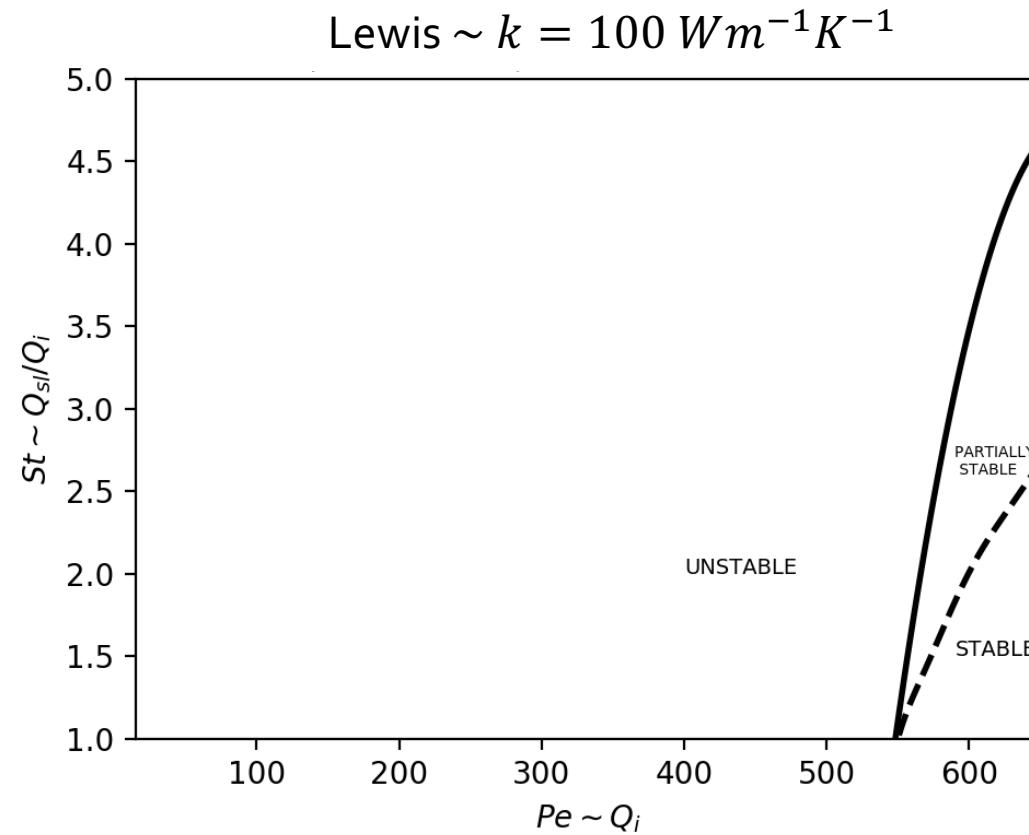
Within constraint of
 $5 < Q_c < 15 \text{ TW}$.



Low thermal conductivity

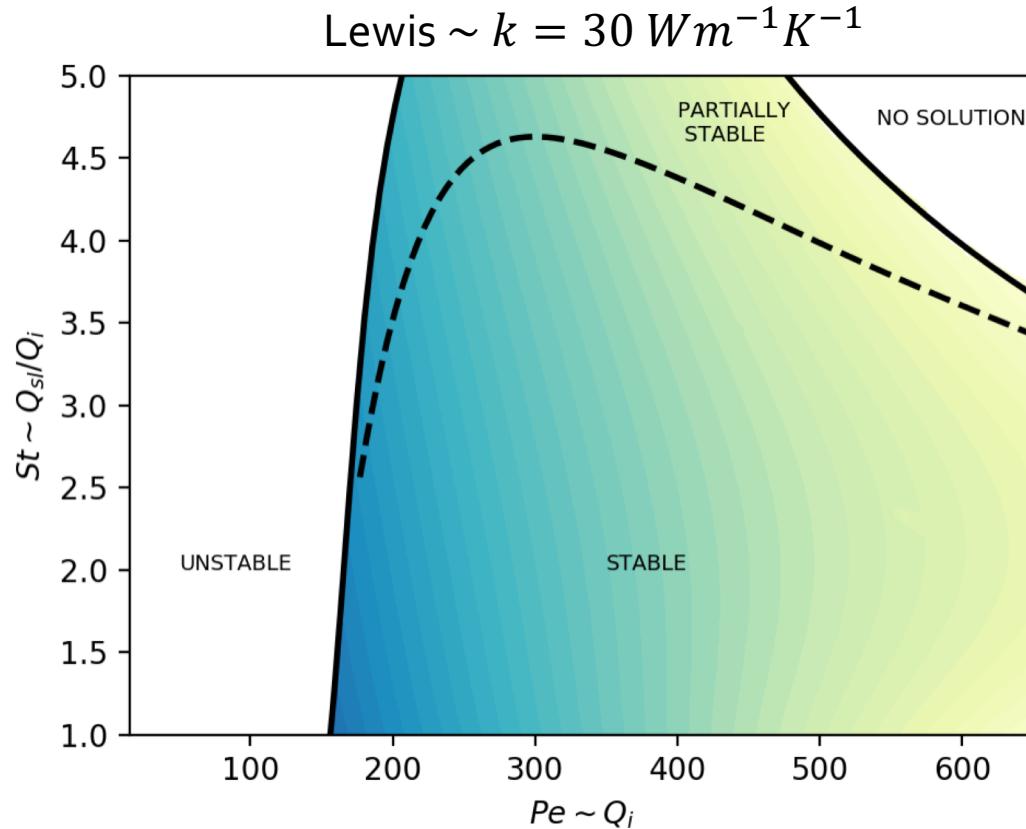


High thermal conductivity

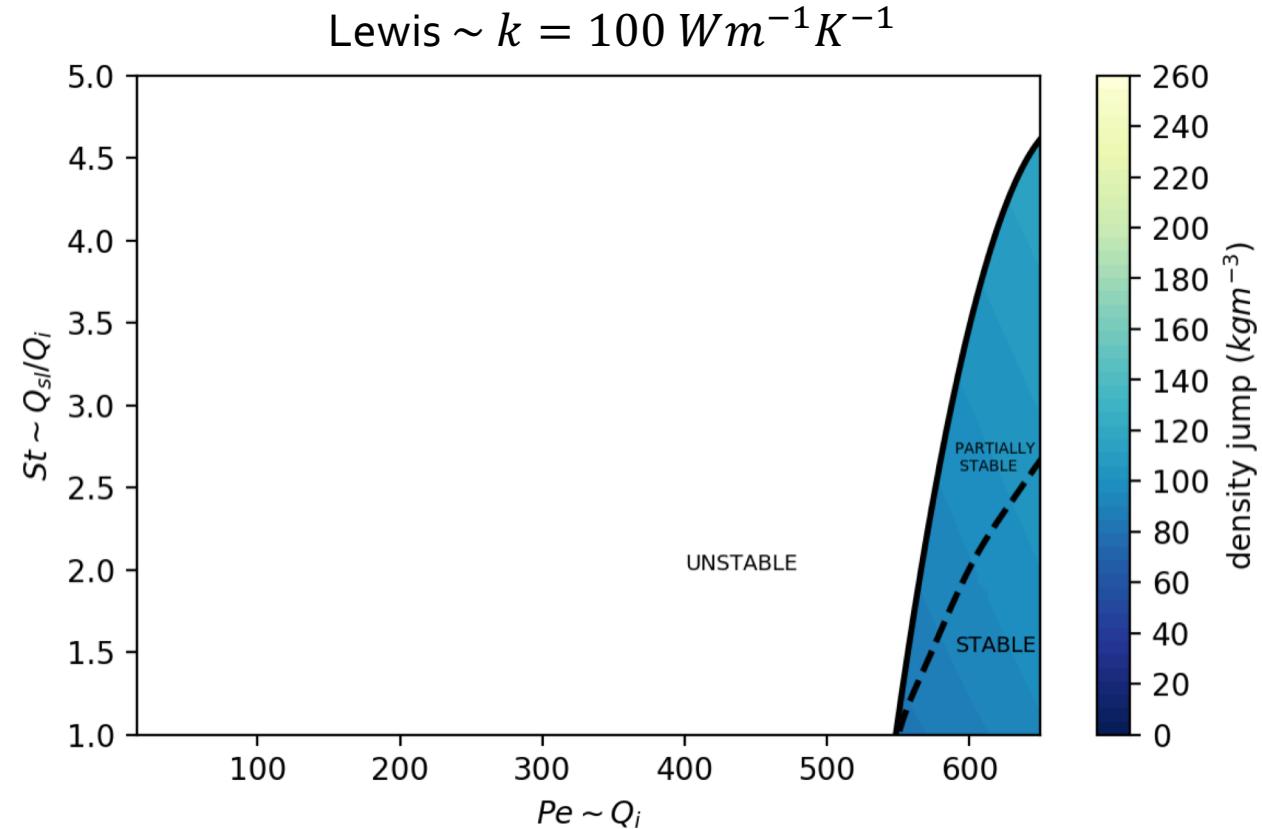


Stably stratified layers found when ICB heat flux is closer to 2 TW.

Low thermal conductivity



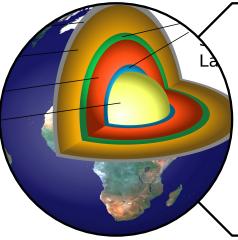
High thermal conductivity



The density jump is smaller and the greatest values are also found at higher Stefan number.

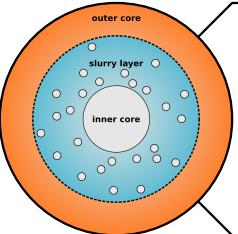
Taking $\Delta\rho_{bod} = \Delta\rho_{mod} - \Delta\rho_{slurry}$ then $350 < \Delta\rho_{bod} < 750 \text{ kg m}^{-3}$ for low thermal conductivity,
 $500 < \Delta\rho_{bod} < 900 \text{ kg m}^{-3}$ for high thermal conductivity.

Summary



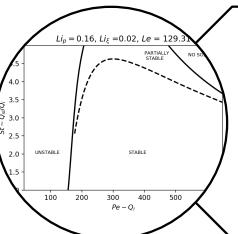
Stratified layers in the core?

Consensus on slowdown in P-wave speed at the base of the core.



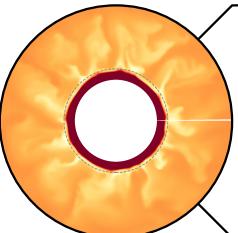
Slurry (iron snow) layer

A slurry provides a thermodynamic explanation of the stratified F-layer.



Regime diagram

High density jumps for low thermal conductivity, high ICB and CSB heat fluxes.

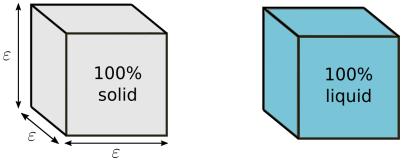


Future work

How does a stratified F-layer impact core dynamics and the dynamo?

Model assumptions

Fast melting

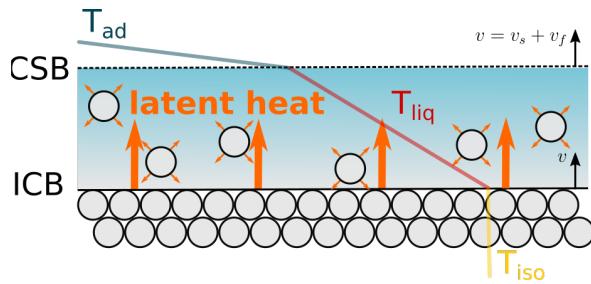


Binary alloy

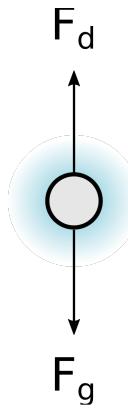
Fe-O liquid



Isothermal inner core

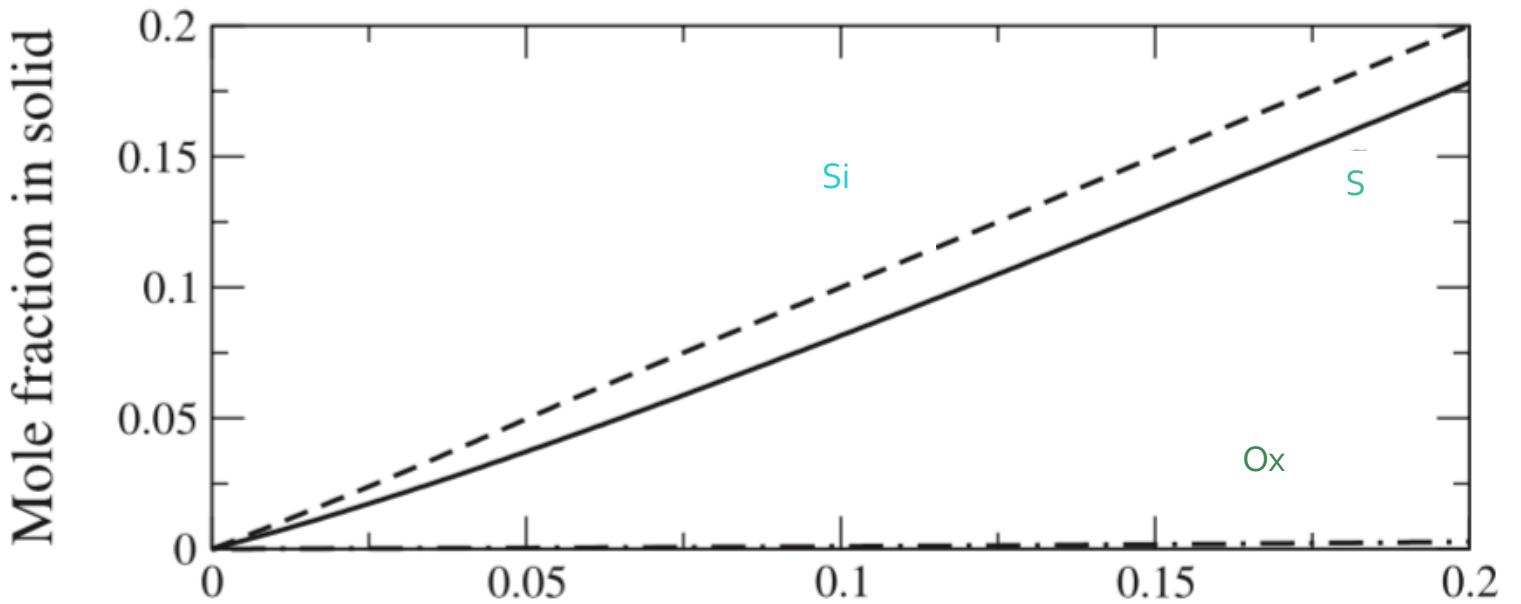


Stokes' flow



Model details

Alf  et al. (2002)



- Oxygen partitions entirely into the liquid

Dimensionless equations

$$\frac{\partial \theta}{\partial r} = -Li_p g \rho \theta - Li_\xi St^* \theta^2 \frac{\partial \Xi}{\partial r},$$

$$\Xi \frac{\partial j}{\partial r} = \frac{1}{r^2} \frac{\partial}{\partial r} \left(\frac{Li_p}{Li_\xi St^* Pe^*} \frac{g \rho r^2}{\theta} \exp \left[\frac{F(r_{sl}r - r_i)}{d} \right] \right) - \frac{v_s}{v_f} \frac{\partial \Xi}{\partial r} - \left(\frac{\partial \Xi}{\partial r} + \frac{2}{r} \Xi \right) j$$

$$\frac{\partial^2 \theta}{\partial r^2} = -\frac{Pe^*}{St^* Le^*} \left(\frac{\partial j}{\partial r} + \frac{2}{r} j \right) - \left(\frac{v_s}{v_f} \frac{Pe^*}{Le^*} + \frac{2}{r} \right) \frac{\partial \theta}{\partial r}$$

Dimensionless parameters

$$Li_p \equiv \frac{\Delta V_{Fe}^{s,l} g_{sl} \rho_{sl} r_{sl}}{L},$$

$$Li_\xi \equiv \frac{1000 R \xi_O}{a_O c_p},$$

$$Pe^* \equiv \frac{v_f r_{sl} \Delta V_{Fe}^{s,l}}{D_O \Delta V_{Fe,O}^{s,l}}$$

$$St^* \equiv \frac{Q^{sl}}{4\pi r_{sl}^2 \rho_{Fe}^l v_f L},$$

$$Le^* \equiv \frac{k \Delta V_{Fe}^{s,l}}{\rho_{Fe}^l c_p D_O \Delta V_{Fe,O}^{s,l}}.$$

Dimensionless boundary conditions

$$\theta(1) = \frac{T_l c_p}{St^* L},$$

$$\frac{\partial \theta}{\partial \hat{r}} \Big|_{\hat{r}=\frac{r_i}{r_{sl}}} = -\frac{Pe^* St^* \rho_{Fe}^s}{Le^* \rho_{Fe}^l},$$

$$\frac{\partial \theta}{\partial \hat{r}} \Big|_{\hat{r}=1} = -\frac{Pe^*}{Le^*},$$

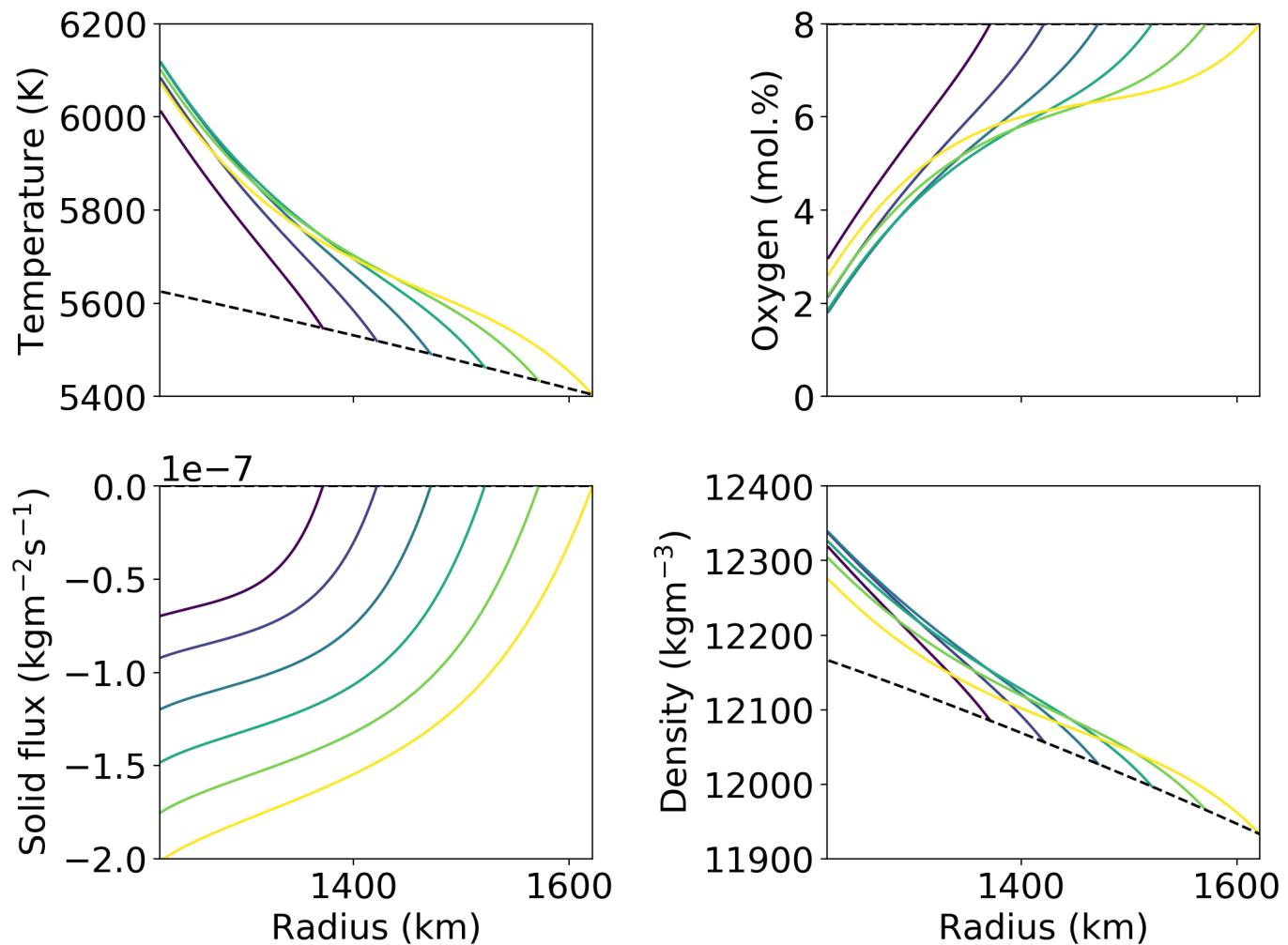
$$\Xi(1) = 1,$$

$$\hat{j} \left(\frac{r_i}{r_{sl}} \right) = -\frac{v_s \rho_{Fe}^s}{v_f \rho_{Fe}^l},$$

$$\hat{j}(1) = 0.$$

Results

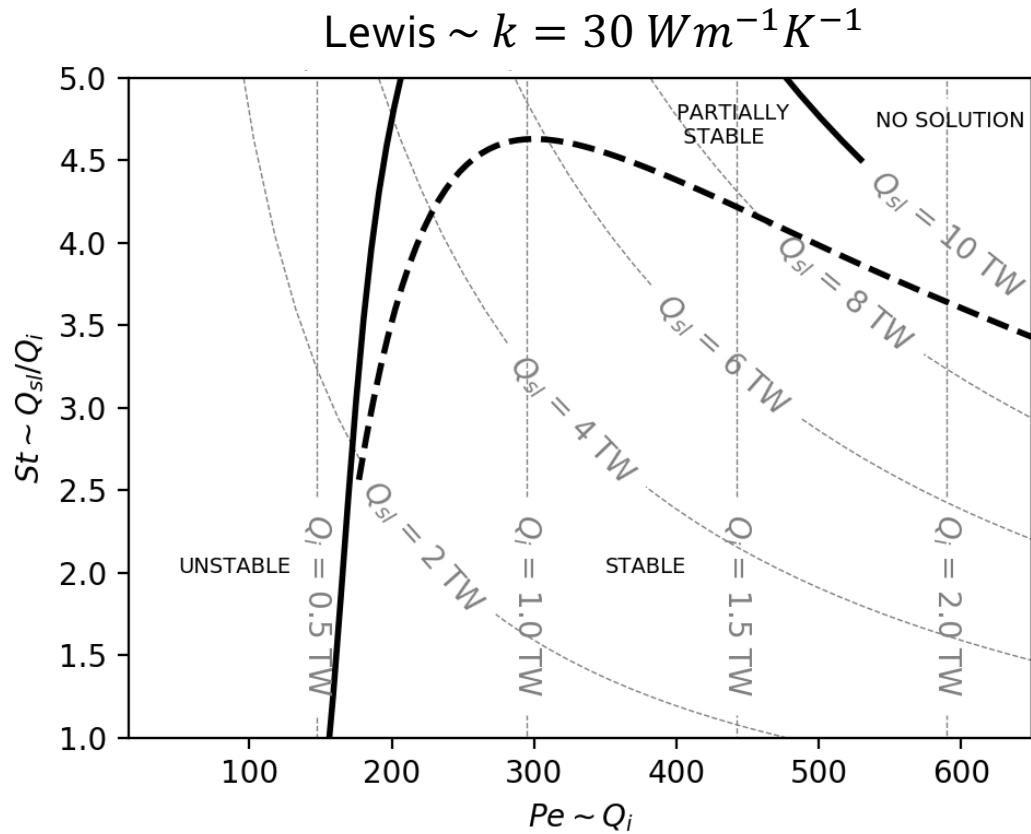
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Parameter space

Dimensional	Dimensionless
ICB heat flux	$0.01 - 2 \text{ TW}$
CSB heat flux	$0.1 - 10 \text{ TW}$
Thermal conductivity	$30/100 \text{ W m}^{-1} \text{ K}^{-1}$
Layer thickness	150 km
Bulk oxygen concentration	8 mol.\%

Low thermal conductivity



High thermal conductivity

