MCOES Assignment 20/21 - Hydraulic PTO modelling

1 Objectives

This assignment aims to demonstrate the modelling of an hydraulic power take-off (PTO) system for a wave energy converter. The PTO system show in Fig. 1 comprises an hydraulic cylinder, a control manifold, an high pressure accumulator, an hydraulic motor connected to an electrical generator, and a low pressure accumulator.

2 Definition of the problem

The goal of the present is study and select a set PTO parameters described in Listing 1 that maximize the energy extracted for a given irregular excitation force.

A base case is given with a regular excitation force. The results obtained for the irregular excitation force should be compared with the regular case for the selected set of parameters.

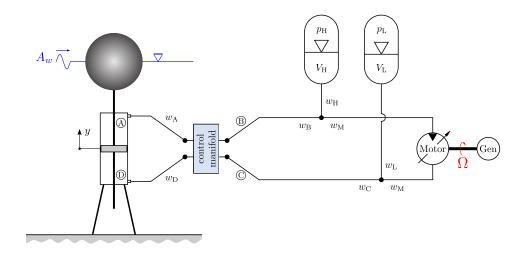


Figure 1: unidirectional hydraulic system simulator.

Listing 1: Parameters to be changed in the study.

```
// hydraulic cylinder
2
    parameter Real p_Rp( unit = "m" ) = 0.4 "cylinder radius";
    parameter Real p_lp( unit = "m" ) = 16.0 "cylinder height";
3
4
5
    // accumulators data
    // p_Vacc should be a positive constant times p_Vacc
7
    parameter Real p_Vacc( unit = "m3" ) = 2.0 * p_Vh0 "total acc. volume";
    parameter Real p_V0( unit = "m3" ) = 0.5 * p_Vacc "initial hydraulic fluid volume";
    parameter Real p_pOH( unit = "Pa" ) = 1.1 * c_pOA "initial pressure chamber A";
9
    parameter Real p_pOL( unit = "Pa" ) = 0.9 * c_pOD "initial pressure chamber D";
11
12
    // PTO system
    parameter Real p_Dv( unit = "m3/rad" ) = 0.0008 "hydraulic motor volumetric disp.";
13
    parameter Real p_a( unit = "Nm/(rad2/s2)" ) = 0.1 "generator control parameter";
```

3 System of equations

The power take-off system can de modelled using the following system of differential-algebraic equations (DAEs):

• Control manifold chamber A

if $p_{\rm A} \geq p_{\rm H}$ then

$$s_{A\to B} = 1; \ \tilde{s}_{A\to B} = 0; \ s_{C\to A} = 0;$$
 (1)

else if $p_{\mathrm{A}} \leq p_{\mathrm{L}}$ then

$$s_{A\to B} = 0; \ \tilde{s}_{A\to B} = 1; \ s_{C\to A} = 1;$$
 (2)

else

$$s_{A\to B} = 0; \ \tilde{s}_{A\to B} = 1; \ s_{C\to A} = 0;$$
 (3)

endif

• Control manifold chamber D

if $p_{\rm D} \geq p_{\rm H}$ then

$$s_{D\to B} = 1; \ \tilde{s}_{D\to B} = 0; \ s_{C\to D} = 0;$$
 (4)

else if $p_{\mathrm{D}} \leq p_{\mathrm{L}}$ then

$$s_{D\to B} = 0; \ \tilde{s}_{D\to B} = 1; \ s_{C\to D} = 1;$$
 (5)

else

$$s_{D\to B} = 0; \ \tilde{s}_{D\to B} = 1; \ s_{C\to D} = 0;$$
 (6)

endif

• Piston motion $(m_{\rm sph} \gg m_{\rm p})$

$$m_{\rm sph}\dot{v} = F_{\rm exc} - A_{\rm p} \left(p_{\rm A} - p_{\rm D} \right) \tag{7}$$

$$\dot{y} = v \tag{8}$$

$$F_{\rm exc} = A_{\rm w} \Gamma_{\rm exc} \sin\left(\frac{2\pi}{T_{\rm w}}t\right)$$

• Piston's chamber A

$$V_{\rm A} = V_0 - A_{\rm p} y \tag{9}$$

$$m_{\rm A} = \rho_{\rm A} V_{\rm A} \tag{10}$$

$$w_{\rm VA} = -\rho_{\rm A} A_{\rm p} v \tag{11}$$

$$w_{\rm A} = -s_{\rm A\to B} C_{\rm d} A_{\rm acc} \sqrt{2\rho_{\rm A} \max(p_{\rm A} - p_{\rm H}, 0)} + s_{\rm C\to A} C_{\rm d} A_{\rm acc} \sqrt{2\rho_{\rm L} \max(p_{\rm L} - p_{\rm A}, 0)}$$
(12)

$$\frac{\dot{\rho}_{\rm A}}{\rho_{\rm A}} + \frac{w_{\rm VA}}{m_{\rm A}} = \frac{w_{\rm A}}{m_{\rm A}} \tag{13}$$

$$\frac{\dot{p}_{\rm A}}{\beta} = \frac{\dot{\rho}_{\rm A}}{\rho_{\rm A}} \tag{14}$$

• Piston's chamber D

$$V_{\rm D} = V_0 + A_{\rm p} y \tag{15}$$

$$m_{\rm D} = \rho_{\rm D} V_{\rm D} \tag{16}$$

$$w_{\rm VD} = \rho_{\rm D} A_{\rm p} v \tag{17}$$

$$w_{\rm D} = -s_{\rm D\to B} C_{\rm d} A_{\rm acc} \sqrt{2\rho_{\rm D} \max(p_{\rm D} - p_{\rm H}, 0)} + s_{\rm C\to D} C_{\rm d} A_{\rm acc} \sqrt{2\rho_{\rm L} \max(p_{\rm L} - p_{\rm D}, 0)}$$
(18)

$$\frac{\dot{\rho}_{\rm D}}{\rho_{\rm D}} + \frac{w_{\rm VD}}{m_{\rm D}} = \frac{w_{\rm D}}{m_{\rm D}} \tag{19}$$

$$\frac{\dot{p}_{\rm D}}{\beta} = \frac{\dot{\rho}_{\rm D}}{\rho_{\rm D}} \tag{20}$$

• Motor/Generator

$$w_{\rm M} = (s_{\rm A\to B} \,\rho_{\rm A} + s_{\rm D\to B} \,\rho_{\rm D} + \tilde{s}_{\rm A\to B} \tilde{s}_{\rm D\to B} \,\rho_{\rm H}) \,D_{\rm v}\Omega \tag{21}$$

$$T_{\rm M} = D_{\rm v} \left(p_H - p_L \right) \tag{22}$$

$$P_{\rm M} = T_{\rm M}\Omega \tag{23}$$

$$T_{\rm G} = a\Omega^2 \tag{24}$$

$$I\dot{\Omega} = T_{\rm M} - T_{\rm G} \tag{25}$$

• High-pressure accumulator

$$w_{\rm H} = (s_{\rm A \to B} w_{\rm A} + s_{\rm D \to B} w_{\rm D}) - w_{\rm M} \tag{26}$$

$$m_{\rm H} = \rho_{\rm H} V_{\rm H} \tag{27}$$

$$\dot{m}_{\rm H} = w_{\rm H} \tag{28}$$

$$\dot{V}_{\rm gH} + \dot{V}_{\rm H} = 0 \tag{29}$$

$$\frac{\dot{p}_{\rm H}}{p_{\rm H}} + \gamma \frac{\dot{V}_{\rm gH}}{V_{\rm gH}} = 0 \tag{30}$$

$$\frac{\dot{p}_{\rm H}}{\beta} = \frac{\dot{\rho}_{\rm H}}{\rho_{\rm H}} \tag{31}$$

• Low-pressure accumulator

Note that w_A and w_D have negative signs at chambers A/D inlet.

$$w_{\mathcal{L}} = w_{\mathcal{M}} + (s_{\mathcal{C} \to \mathcal{A}} w_{\mathcal{A}} + s_{\mathcal{C} \to \mathcal{D}} w_{\mathcal{D}}) \tag{32}$$

$$m_{\rm L} = \rho_{\rm L} V_{\rm L} \tag{33}$$

$$\dot{m}_{\rm L} = w_{\rm L} \tag{34}$$

$$\dot{V}_{\rm gL} + \dot{V}_{\rm L} = 0 \tag{35}$$

$$\frac{\dot{p}_{\rm L}}{p_{\rm L}} + \gamma \frac{\dot{V}_{\rm gL}}{V_{\rm gL}} = 0 \tag{36}$$

$$\frac{\dot{p}_{\rm L}}{\beta} = \frac{\dot{\rho}_{\rm L}}{\rho_{\rm L}} \tag{37}$$

 \bullet System checking - the total system mass $m_{\rm T}$ must be constant in time

$$m_{\rm T} = m_{\rm A} + m_{\rm D} + m_{\rm H} + m_{\rm L}$$
 (38)

A Modelica source code

Listing 2: Implementation of the unidirectional hydraulic system simulator of Fig. 1 in OpenModelica.

```
1 //----
2 // Joao C.C. Henriques 2021 | IST Ocean Energy Systems and Technology Course
3 // email: joaochenriques@tecnico.ulisboa.pt
6 model PTOsim_2021
   //----
9
   // Constants (prefix "c_" )
   //-----
11
   constant Real c_pi( unit = "Pa" ) = Modelica.Constants.pi;
12
   constant Real c_gamma( unit = "1" ) = 1.4 "nitrogen specific heat ratio";
   constant Real c_patm( unit = "Pa" ) = 101325.0 "atmospheric pressure";
   constant Real c_beta( unit = "Pa" ) = 1.0E9 "atmospheric pressure [Pa]";
15
   constant Real c_rho_oil( unit = "kg/m3" ) = 850.0 "hydraulic fluid density";
   constant Real c_floater_mass( unit = "kg" ) = 140000.0 "floater mass";
   constant Real c_Racc( unit = "m" ) = 0.05 "acc. inlet/outlet hose radius";
19
   constant Real c_Cd( unit = "1" ) = 0.65 "acc. inlet/outlet discharge coef.";
20
21
   constant Real c_Inertia( unit = "kgm2" ) = 2.0 "motor/generator inertia";
23
   constant Real c_p0A( unit = "Pa" ) = 80 * c_patm "initial pressure chamber A";
   constant Real c_pOD( unit = "Pa" ) = 80 * c_patm "initial pressure chamber D";
24
   // floater excitation force
27
   //-----
   // First frequency
   constant Real c_Aexc1( unit = "N" ) = 6000E3 "exc. force amplitude";
   constant Real c_Texc1( unit = "s" ) = 8.0 "exc. force period";
   constant Real c_omega1_exc( unit = "rad/s" ) = 2.0*c_pi/c_Texc1 "exc. force freq.";
31
   // Second frequency
   constant Real c_Aexc2( unit = "N" ) = 2500E3 "exc. force amplitude";
   constant Real c_Texc2( unit = "s" ) = 13.0 "exc. force period";
   constant Real c_omega2_exc( unit = "rad/s" ) = 2.0*c_pi/c_Texc2 "exc. force freq.";
   constant Real c_phase2_exc( unit = "rad" ) = c_pi * 0.37 "exc. force freq.";
38
39
   // Third frequency
   constant Real c_Aexc3( unit = "N" ) = 3500E3 "exc. force amplitude";
   constant Real c_Texc3( unit = "s" ) = 11.0 "exc. force period";
   constant Real c_omega3_exc( unit = "rad/s" ) = 2.0*c_pi/c_Texc3 "exc. force freq.";
42
43
   constant Real c_phase3_exc( unit = "rad" ) = c_pi * 0.67 "exc. force freq.";
44
45
   //-----
   // Parameters (prefix "p_" )
46
   //-----
47
   // hydraulic cylinder
   parameter Real p_Rp( unit = "m" ) = 0.4 "cylinder radius";
50
   parameter Real p_lp( unit = "m" ) = 16.0 "cylinder height";
51
53
   // accumulators data
```

```
54
     parameter Real p_Vacc( unit = "m3" ) = 2.0 * p_Vh0 "total acc. volume";
    // p_VO should be a positive constant times p_Vacc
     parameter Real p_V0( unit = "m3" ) = 0.5 * p_Vacc "initial hydraulic fluid volume";
     parameter Real p_pOH( unit = "Pa" ) = 1.1 * c_pOA "initial pressure chamber A";
57
     parameter Real p_pOL( unit = "Pa" ) = 0.9 * c_pOD "initial pressure chamber D";
60
     // PTO system
     parameter Real p_Dv( unit = "m3/rad" ) = 0.0008 "hydraulic motor volumetric disp.";
61
62
     parameter Real p_a( unit = "Nm/(rad2/s2)" ) = 0.1 "generator control parameter";
63
64
     //-----
     // do not change these parameters
65
66
     //-----
     parameter Real p_VgO( unit = "m3" ) = p_Vacc - p_V0 "initial gas volume";
68
     parameter Real p_Aacc( unit = "m2" ) = c_pi*c_Racc^2 "acc. inlet/outlet area";
69
70
     parameter Real p_Ap( unit = "m2" ) = c_pi * p_Rp^2 "cylinder/piston area";
     parameter Real p_Vh0( unit = "m3" ) = 0.5 * p_lp * p_Ap "cylinder chamber volume";
71
72
73
     74
     // Variables (no prefix)
     \ensuremath{//} Equations of differential equations must have initial conditions ( start)
75
76
77
78
    // algebraic equations
     Real Fexc( unit = "N" ) "excitation force";
     Real smoothing( unit = "1" ) "initial smoothing ramp";
80
     Real y( start = 0, unit = "m", fixed = true ) "piston position";
81
     Real v( start = 0, unit = "m/s", fixed = true ) "piston velocity";
83
84
     // Control manifold (Integers have no units)
85
     Integer sAB "connection A->B open [1/0]";
     Integer tilde_sAB "connection A->B closed [1/0]";
87
     Integer sCA "connection C->A open [1/0]";
88
     Integer sDB"connection D->B open [1/0]";
     Integer tilde_sDB "connection D->B closed [1/0]";
89
     Integer sCD "connection C->D open [1/0]";
91
92
     // cylinder chamber A
93
     Real VA( unit = "m3" ) "volume";
     Real mA( unit = "kg" ) "hydraulic fluid mass";
     Real wVA( unit = "kg/s" ) "piston pump mass flow rate";
95
     Real wA( unit = "kg/s" ) "inlet/outlet mass flow rate";
96
97
     Real rhoA( start = c_rho_oil, unit = "kg/m3", fixed = true ) "hyd. fluid density";
     Real pA( start = p_pOH, unit = "Pa", fixed = true ) "hydraulic fluid pressure";
98
99
100
     // cylinder chamber D
101
     Real VD( unit = "m3" ) "volume";
     Real mD( unit = "kg" ) "hydraulic fluid mass";
102
     Real wVD( unit = "kg/s") "piston pump mass flow rate";
103
     Real wD( unit = "kg/s" ) "inlet/outlet mass flow rate";
104
     Real rhoD( start = c_rho_oil, unit = "kg/m3", fixed = true ) "hyd. fluid density";
105
106
     Real pD( start = c_pOD, unit = "Pa", fixed = true ) "hydraulic fluid pressure";
107
108
     // PTO system
109
     Real wM( unit = "m3/s" ) "hydraulic motor flow rate";
110
     Real TM( unit = "Nm" ) "hydraulic motor torque";
     Real PM( unit = "W" ) "hydraulic motor power";
111
```

```
112
     Real TG( unit = "Nm" ) "generator electromagnetic shaft torque";
113
     Real PG( unit = "W" ) "generator electromagnetic shaft power";
     Real Omega( start = 100, unit = "rad/s", fixed = true ) "PTO rotational speed";
114
115
     Real EG( start = 0.0, unit = "J", fixed = true ) "generator electromagnetic shaft
        power";
116
117
     // High-pressure accumulator
     Real wH( unit = "kg/s" ) "inlet/outlet mass flow rate";
118
     Real mH( unit = "kg" ) "hydraulic fluid mass";
119
120
     Real VH( start = p_V0, unit = "m3", fixed = true ) "hydraulic fluid volume";
     Real rhoH( start = c_rho_oil, unit = "kg/m3", fixed = true ) "hyd. fluid density";
121
     Real VgH( start = p_VgO, unit = "m3/s", fixed = true ) "gas volume";
122
     Real pH( start = p_pOH, unit = "Pa", fixed = true ) "accumulator pressure";
123
124
125
     // Low-pressure accumulator
126
     Real wL( unit = "kg/s" ) "inlet/outlet mass flow rate";
     Real mL( unit = "kg" ) "hydraulic fluid mass";
127
     Real VL( start = p_V0, unit = "m3", fixed = true ) "hydraulic fluid volume";
129
     Real rhoL( start = c_rho_oil, unit = "kg/m3", fixed = true ) "hyd. fluid density";
     Real VgL( start = p_Vg0, unit = "m3", fixed = true ) "gas volume";
130
     Real pL( start = p_pOL, unit = "Pa", fixed = true ) "accumulator pressure";
131
132
133
     // numerical model checking
134
    Real mT( unit = "kg" ) "total system mass";
135
136 equation
137
138
    //-----
139
     // control manifold chamber A
140
    if (pA > pH) then
141
     sAB = 1;
142
     tilde_sAB = 0;
143
      sCA = 0;
144
    elseif (pA < pL) then
145
      sAB = 0;
      tilde_sAB = 1;
146
147
      sCA = 1;
148
    else
149
     sAB = 0;
150
     tilde_sAB = 1;
151
     sCA = 0;
152
    end if;
153
    //-----
154
     // control manifold chamber D
156
    if (pD > pH) then
     sDB = 1;
157
158
     tilde_sDB = 0;
      sCD = 0;
    elseif (pD < pL) then
160
      sDB = 0;
161
162
      tilde_sDB = 1;
163
      sCD = 1;
164
    else
165
     sDB = 0;
166
     tilde_sDB = 1;
167
     sCD = 0;
168
    end if;
```

```
169
170
    //-----
171
    // Cylinder/piston motion
172
    smoothing = min(time / (2.0 * c_Texc1), 1.0); // 2 periods smoothing ramp
173
174
    Fexc = c_Aexc1 * sin( c_omega1_exc * time )
175
        + c_Aexc2 * sin( c_omega2_exc * time + c_phase2_exc )
176
        + c_Aexc3 * sin( c_omega3_exc * time + c_phase3_exc );
177
178
    c_floater_mass * der(v) = smoothing * Fexc - p_Ap * (pA - pD);
179
    der(y) = v;
180
181
    //-----
182
    // Cylinder's chamber A
183
    VA = p_Vh0 - p_Ap * y;
184
    mA = rhoA * VA;
185
186
    wVA = -rhoA * p_Ap * v;
187
    wA = +sAB * c_Cd * p_Aacc * sqrt( 2 * rhoA * max(pA - pH,0.0) )
        -sCA * c_Cd * p_Aacc * sqrt( 2 * rhoL * max(pL - pA,0.0) );
188
189
190
    der(rhoA) / rhoA + wVA / mA = -wA / mA;
191
    der(pA) / c_beta = der(rhoA) / rhoA;
192
193
    //-----
194
    // Cylinder's chamber D
195
    VD = p_Vh0 + p_Ap * y;
    mD = rhoD * VD;
196
197
198
    wVD = rhoD * p_Ap * v;
199
    wD = +sDB * c_Cd * p_Aacc * sqrt( 2 * rhoD * max(pD - pH,0.0) )
        -sCD * c_Cd * p_Aacc * sqrt( 2 * rhoL * max(pL - pD,0.0) );
200
201
202
    der(rhoD) / rhoD + wVD / mD = -wD / mD;
203
    der(pD) / c_beta = der(rhoD) / rhoD;
204
205
    //-----
206
    // PTO system
207
    wM = ( sAB * rhoA + sDB * rhoD + tilde_sAB * tilde_sDB * rhoH ) * p_Dv * Omega;
208
    TM = p_Dv * max( pH - pL, 0.0 ); // non-reversible motor
209
    PM = TM * Omega;
210
211
    TG = p_a * Omega^2;
212
    PG = TG * Omega;
213
214
    c_Inertia * der(Omega) = TM - TG;
215
    der(EG) = PG;
216
    //-----
217
218
    // high-pressure accumulator
    wH = sAB * wA + sDB * wD - wM;
219
220
    mH = rhoH * VH;
221
222
    der(mH) = wH;
223
    der(VgH) + der(VH) = 0.0;
224
    der(pH) / pH + c_gamma * der(VgH) / VgH = 0.0;
225
    der(pH) / c_beta = der(rhoH) / rhoH;
226
```

```
227
  //-----
228 // low-pressure accumulator
229 wL = wM + ( sCA * wA + sCD * wD ); // NOTE: wA and wD have negative signs
230 \quad mL = rhoL * VL;
231
232
  der(mL) = wL;
233
   der(VgL) + der(VL) = 0.0;
234
  der(pL) / pL + c_gamma * der(VgL) / VgL = 0.0;
235 der(pL) / c_beta = der(rhoL) / rhoL;
236
237 //-----
239 mT = mA + mD + mH + mL;
240
241 end PTOsim_2021;
```