

# A Microwave Scattering Model for Layered Vegetation

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**Abstract**—A microwave scattering model has been developed for layered vegetation based on an iterative solution of the radiative transfer equation up to the second order to account for multiple scattering within the canopy and between the ground and the canopy. The model is designed to operate over a wide frequency range for both deciduous and coniferous forest and to account for the branch size distribution, leaf orientation distribution, and branch orientation distribution for each size. The canopy is modeled as a two-layered medium above a rough interface. The upper layer is the crown containing leaves, stems, and branches. The lower layer is the trunk region modeled as randomly positioned cylinders with a preferred orientation distribution above an irregular soil surface. Comparisons of this model with measurements from deciduous and coniferous forests show good agreements at several frequencies for both like and cross polarizations. Major features of the model needed to realize the agreement include allowance for (1) branch size distribution, (2) second-order effects, and (3) tree component models valid over a wide range of frequencies.

## I. INTRODUCTION

NATURAL phenomena such as the atmospheric carbon dioxide concentration, the hydrologic cycle, and the energy balance in the biosphere are related to the forest. Hence accurate and timely measurements of the forest structure and type through remote sensing are of interest [1]. Of the many ways to measure forest properties, microwave remote sensing is one way which is independent of both weather conditions and the time of day when the measurements can be acquired [2, Chapter 1]. The analysis of these measured data could yield biophysical characteristics of the forest [3]–[5] or its components such as leaves, branches, and trees [6]–[8].

In parallel to the experimental studies, scattering models have been developed to interpret the collected data [9]–[24].

These models may be divided into two categories: i) phenomenological models and ii) physical models.

The phenomenological models are based upon an intuitive understanding of the relative importance of different forest components. Then a scattering model is constructed by summing up the contributions from forest components believed to be important [10]–[12]. The physical models are based upon the interaction of electromagnetic waves with the forest canopy. A canopy can be modeled either as a discrete or a continuous inhomogeneous medium. As a discrete medium the canopy is treated as a collection of randomly distributed discrete scatterers assuming average sizes and shapes of various forest components [13]–[23]. These scatterers may be embedded in one or two layers or a half space medium. For continuous medium modeling, the canopy is treated as a continuous medium with a fluctuating permittivity function [24]. The radiative transfer theory [13]–[20], the distorted Born approximation [21], [22], or the Monte Carlo technique [23] have been used to study electromagnetic interaction with discrete media. The first-order Born and renormalization methods have been applied to study wave scattering from continuous media [24].

Most of the existing scattering models are restricted by assumptions regarding the shape of the scatterers [15]–[21] or the applicable frequency [9], [17]. Some models account only for leaves but not branches or vice versa [16]–[21] and others treat branches and soil surfaces but not leaves [18]. In all these models the scatterers were embedded in one layer above the soil interface or a half space medium.

Recently, a two-layer phenomenological model has been proposed by Richard *et al.* [1987] for a coniferous forested canopy at *L*-band [11]. In this model the foliage is represented by a cloud of water droplets and the trunk-ground interaction is modeled by dihedral corner reflectors. To avoid issues of tractability and complexity, the individual scattering mechanisms within the forested canopy were modeled separately utilizing empirical or analytical description as appropriate. This model is simple but its domain of applicability is limited. Durden *et al.* [1989] improved this model by replacing the dihedral corner reflector by a finite-length cylinder over a rough interface. The branches are modeled by a layer of randomly oriented cylinders [12]. Several scattering mechanisms are identified and the corresponding Stokes matrices were calculated. The Stokes parameter matrices were then combined to give the total Stokes matrix and resulting polarization signature. The leaf effect was not taken into consideration.

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Ulaby *et al.* [1990] proposed a two-layer physical model based on the first-order solution of the radiative transfer theory [13]. This model was used [14], [15] to model multiangle and temporal backscatter from a walnut orchard. It involves the following assumptions:

1. The contribution from trunks in the backscattering direction can be ignored and trunk-ground interaction can be accounted for by considering reflections from the trunks and a flat ground.
2. The cross-polarized term in the trunk phase matrix has been ignored.
3. In the canopy-ground interaction calculation, the ground can be taken to be a specular surface.
4. The forward scattering theorem (optical theorem) can be applied to calculate the extinction coefficient within the canopy. This theorem is accurate to the extent the field scattering amplitude is accurate. Under low frequency approximations this theorem can only provide the loss due to absorption [25]. Hence, scattering loss is not included.
5. The physical optics approach is used to calculate scattering from a leaf. Thus, only leaves larger than a wavelength are considered.

In view of the current status in forest scattering models, there is room for further generalization. The aim of the present study is to develop a scattering model with a wider range of applicability than those available in the literature. In particular, we want to develop a fairly complete but simple physical model which can be applied to both deciduous and coniferous forest over a wide range of frequencies by

1. including coherent and incoherent surface scattering in computation of canopy-soil interactions,
2. using a leaf scattering model which holds for leaves smaller or comparable to the wavelength,
3. accounting for the various branch sizes and their orientation distributions,
4. accounting for cross polarized scattering due to the trunk-ground interactions,
5. using an extinction formulation which accounts for both ohmic and scattering losses where low frequency approximation is made.
6. including the second order radiative transfer solution to account for multiple scattering within the canopy.

A description of the scattering model for a forest canopy is given in Section II. For a linearly polarized incident wave, the explicit expressions for the bistatic scattering coefficient associated with different scattering mechanisms discussed in Section II are given in Section III. In like polarization the second-order volume scattering is generally small compared with the first. However, in cross polarization second-order contribution can be important. Hence, the second-order volume scattering term due to the crown layer is also given.

As a test for the present model comparisons are made between the measured and the predicted values of the backscattering coefficients from both walnut and cypress trees [4], [26]. Two of the authors, Lang and Chauhan have participated in the collection of the walnut tree geometry and ground truth [26].

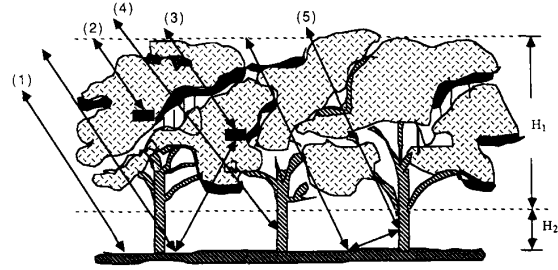


Fig. 1. Geometry of a forest canopy and the backscattering processes for the zero and first-order solutions of the radiative transfer equation: (1) zero order, (2) crown scattering, (3) crown-ground interaction, (4) trunk scattering, (5) trunk-ground interaction.

The cypress tree ground truth is available in the literature [4]. Hence, arbitrary choices of most of the model parameters are avoided.

## II. FOREST SCATTERING MODEL DESCRIPTION

The geometry of the scattering problem is given in Fig. 1. It consists of a crown layer and a trunk layer above an irregular surface. Within the crown layer the branches are grouped into different sizes each with an orientation distribution. They are modeled as randomly oriented finite-length dielectric cylinders. The scattering matrix ( $S$  matrix) for such cylinders can be obtained by estimating the inner field by that of corresponding infinite cylinder [18]. The validity of this approach for calculating the branch scattering matrix was verified experimentally for branches having length to diameter ratio greater than 5 [27], [28]. The extinction coefficient for the branch model is obtained via the forward scattering theorem since the model does not use low frequency approximation [18]. The deciduous leaves are modeled as randomly oriented circular discs. The coniferous leaves and the stems are modeled as randomly oriented needles. The scattering matrix for a needle or a disc is obtained by applying the Generalized Rayleigh-Gans approximation. This approximation holds for thin leaves and for leaf surface dimension smaller or comparable to the wavelength [27]. Thus, for leaves the extinction coefficients are calculated by summing both the absorption and the scattering coefficients [29]. In summary, the crown layer consists of several groups of scatterers, namely, the leaves and a few different sizes of branches. Scatterers belonging to the same group are identical in size.

Each group of scatterers within the crown layer is a collection of identical scatterers with number density  $n_m(m^{-3})$  and a probability density function  $P_m(a, h, \alpha, \beta)$  where " $a$ " and " $2h$ " are the radius and length or thickness of a scatterer within the  $m$ th group. The angles  $\alpha$  and  $\beta$  are the scatterer azimuthal and inclination angles, respectively (Fig. 2). In this study the polar coordinates are used to describe the scatterer orientation with respect to the reference frame and the radial coordinate is parallel to the scatterer axis of symmetry. All the crown constituents are taken to be uniformly oriented in the azimuthal direction. Consequently, the probability density function for the scatterers within the  $m$ th group reduces to

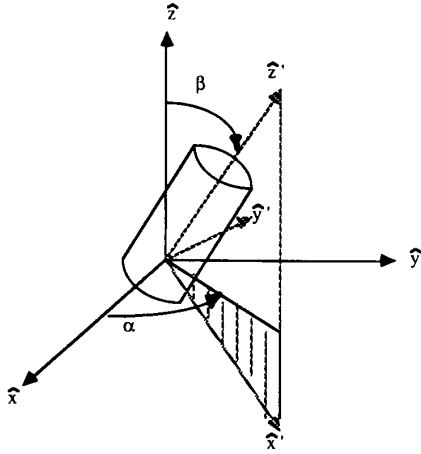


Fig. 2. The polar angles of orientation (defined with respect to the reference frame).

the form,

$$P_m(a, h, \alpha, \beta) = \frac{1}{2\pi} P_m(a, h, \beta). \quad (1)$$

Similarly, the trunk layer may also have several groups of scatterers. Each group is modeled by randomly positioned and vertically oriented identical cylinders with number density  $n_m(m^{-3})$ . Each group has its own orientation distribution function. Since a trunk can also be modeled as a dielectric cylinder, the scattering amplitude matrix is the same as the branches [18] and so is the representation for the extinction coefficient.

The Kirchhoff model under the scalar approximation is used to represent the scattering properties of the rough soil surface [2]. The surface correlation function is taken to be a Gaussian function with variance  $\sigma^2$  and correlation length,  $L$ .

### III. THE BISTATIC SCATTERING COEFFICIENTS

Consider a plane wave incident in  $\hat{i}(\pi - \theta_i, \phi_i)$  direction with electric field polarized along  $\hat{q}$  direction,

$$\vec{E}_i(\vec{r}) = \hat{q} E_0 e^{-jk\hat{i} \cdot \vec{r}} \quad j = \sqrt{-1} \quad (2)$$

where  $k$  is the background medium wavenumber;  $\hat{q} = \hat{v}_i$  or  $\hat{h}_i$ ; which are the polarization unit vectors (Fig. 3) defined as follows:

$$\begin{aligned} \hat{i} &= \sin \theta_i (\hat{x} \cos \phi_i + \hat{y} \sin \phi_i) - \hat{z} \cos \theta_i \\ \hat{h}_i &= \frac{\hat{z} \times \hat{i}}{|\hat{z} \times \hat{i}|} = \hat{y} \cos \phi_i - \hat{x} \sin \phi_i \\ \hat{v}_i &= \hat{h}_i \times \hat{i} = -\cos \theta_i (\hat{x} \cos \phi_i + \hat{y} \sin \phi_i) - \hat{z} \sin \theta_i. \end{aligned} \quad (3)$$

For the incident field given in (2) and using the albedo as an iteration parameter, the bistatic scattering coefficient from the canopy in  $\hat{s}(\theta_s, \phi_s)$  direction can be written as [Appendix A]

$$\sigma_{pq} = \sum_{v=0} \sigma_{pq}^v. \quad (4)$$

In (4)  $v$  is the order of the iterative solution of the radiative transfer equation. In the following sections we will consider

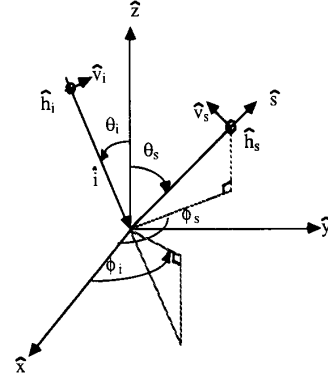


Fig. 3. The polarization vectors of the incident and scattered fields.

the zero, the first, and the second-order contribution to the bistatic scattering coefficient.

#### A. The Zero-Order Solution (Ground Scattering)

The zero-order solution of the radiative transfer equation is due to ground scattering as illustrated in the backscattering direction by 1 in Fig. 1. The bistatic scattering coefficient of the ground can be written as

$$\sigma_{pq}^0 = L_{1p}(\theta_s) L_{2p}(\theta_s) \sigma_{pq}^s(\theta_s, \phi_s; \pi - \theta_i, \phi_i) L_{2q}(\theta_i) L_{1q}(\theta_i) \quad (5)$$

where  $\sigma_{pq}^s(\theta_s, \phi_s; \pi - \theta_i, \phi_i)$  is the  $pq$  element of the surface bistatic scattering coefficient matrix given in [2, Chapter 13, pp. 1085–1200]. Its explicit expression depends on the surface parameters and the approximation used to derive it. For a plane interface  $\sigma_{pq}^s(\theta_s, \phi_s; \pi - \theta_i, \phi_i)$  reduces to Fresnel reflectivity [2, Chapter 12].  $L_{1q}(\theta_i)$  and  $L_{2q}(\theta_i)$  are the  $q$  polarized crown and the trunk attenuation factors in the incident direction,

$$L_{tq}(\theta_i) = \exp[-k_{tq}(\theta_i) H_t \sec \theta_i] \quad (t = 1, 2) \quad (6)$$

where  $k_{1q}(\theta_i)$  and  $k_{2q}(\theta_i)$  are the crown and trunk layer extinction coefficients, respectively [18], [29].  $H_1$  and  $H_2$  are the heights of the crown and trunk layers. Similar definitions apply to  $L_{1p}(\theta_s)$  and  $L_{2p}(\theta_s)$  in the scattering direction. The extinction coefficient within the crown region can be written as

$$k_{1p}(\theta_i) = \sum_{m=1}^{N_1} n_m \langle \kappa_{mp}(\theta_i) \rangle \quad (7)$$

where  $N_1$  is the number of groups within the crown layer and  $\kappa_{mp}(\theta_i)$  is the extinction cross section for a scatterer within the  $m$ th group [18], [29]. The ensemble average  $\langle \cdot \rangle$  in (7) is taken over the  $m$ th group orientation distribution in the following manner:

$$\langle \kappa_{mp}(\theta_i) \rangle = \frac{1}{2\pi} \int d\beta \int d\alpha P_m(\alpha, \beta) \kappa_{mp}(\theta_i). \quad (8)$$

For a discrete probability density function, the integration in (8) reduces to a summation.

Within the trunk layer the extinction coefficient is

$$k_{2p}(\theta_i) = \sum_{m=1}^{N_2} n_m \langle \kappa_{mp}(\theta_i) \rangle \quad (9)$$

where  $N_2$  is the group number within the trunk layer, and  $\kappa_{mp}(\theta_i)$  is the extinction cross section for a scatterer within the  $m$ th group. The ensemble average in (9) is defined in a way similar to the ensemble average in (8) but with density function describing the trunk orientation distribution.

The backscattering coefficient associated with ground scattering can be obtained from (5) by letting  $\theta_s = \theta_i$  and  $\phi_s = \phi_i + \pi$ , i.e.,  $\hat{s} = -\hat{i}$ .

### B. First-Order Solution (Crown and Trunk Scattering)

The first-order solution of the radiative transfer equation leads to a bistatic scattering coefficient in the form

$$\sigma_{pq}^1 = \sigma_{pq}(c) + \sigma_{pq}(c \leftrightarrow g) + \sigma_{pq}(t) + \sigma_{pq}(t \leftrightarrow g). \quad (10)$$

The first term in (10) accounts for crown scattering, the second term for the crown-ground interaction, and the last two terms for the trunk and the trunk-ground scattering, respectively. In the following subsections explicit expressions for those terms will be given along with the physical meaning of each term.

1) *The Crown Scattering*: The bistatic coefficient of the crown is (illustrated in the backscattering direction by 2 in Fig. 1):

$$\sigma_{pq}(c) = 4\pi Q_{1pq}(\theta_s, \phi_s; \pi - \theta_i, \phi_i) \cdot \left\{ \frac{1 - L_{1p}(\theta_s)L_{1q}(\theta_i)}{k_{1p}(\theta_s)\sec\theta_s + k_{1q}(\theta_i)\sec\theta_i} \right\} \quad (11)$$

$$Q_{1pq}(\theta_s, \phi_s; \pi - \theta_i, \phi_i) = \sum_{m=1}^{N_1} n_m \langle |F_{mpq}(\hat{s}, \hat{i})|^2 \rangle$$

where  $F_{mpq}(\hat{s}, \hat{i})$  is the element of the scattering amplitude matrix for a scatterer within the  $m$ th group [18], [29]. The ensemble average  $\langle \rangle$  is taken in a way similar to (8). In (11) the quantity  $Q_{1pq}(\theta_s, \phi_s; \pi - \theta_i, \phi_i)$  represents scattering from a unit volume within the crown region. The quantity within the bracket is the resultant of the integration of the loss factor,  $\exp[(k_{1p}(\theta_i)\sec\theta_i + k_{1q}(\theta_s)\sec\theta_s)z]$ , associated with a unit volume located at  $z$  over the crown depth (note that  $z$  is negative within the crown region).

The backscattering coefficient is a special case of (11) when we let  $\hat{s} = -\hat{i}$ . From (11) it is clear that the crown scattering includes  $N_1$  types of scatterers. They are attenuated by the leaves, the stems and the branches. From (7) and (11) we can see that the interaction between the crown constituents appears only in the loss factors and not in the scattering matrix.

2) *The Crown-Ground Interaction*: The bistatic scattering coefficient due to the crown-ground interaction can be written as a sum of two separate terms:

$$\sigma_{pq}(c \leftrightarrow g) = \sigma_{pq}(c \rightarrow g) + \sigma_{pq}(g \rightarrow c). \quad (12)$$

The first term in (12) represents scattering from the crown followed by scattering from the ground while the second term is associated with scattering from the ground followed by scattering from the crown. The explicit contents of these terms are

$$\sigma_{pq}(c \rightarrow g) =$$

$$L_{1p}(\theta_s)L_{2p}(\theta_s) \int_0^{2\pi} d\phi_t \int_0^{\pi/2} \sin\theta_t d\theta_t \sum_{u=v,h} L_{2u}(\theta_t) \cdot \sigma_{pu}^s(\theta_s, \phi_s; \theta_t, \phi_t) Q_{1uq}(\pi - \theta_t, \phi_t; \pi - \theta_i, \phi_i) \cdot \cos\theta_i \left( \frac{L_{1u}(\theta_t) - L_{1q}(\theta_i)}{k_{1q}(\theta_i)\cos\theta_t - k_{1u}(\theta_t)\cos\theta_i} \right) \quad (13a)$$

$$\sigma_{pq}(g \rightarrow c) =$$

$$L_{1q}(\theta_i)L_{2q}(\theta_i) \int_0^{2\pi} d\phi_t \int_0^{\pi/2} \sin\theta_t d\theta_t \sum_{u=v,h} L_{2u}(\theta_t) \cdot Q_{1pu}(\theta_s, \phi_s; \theta_t, \phi_t) \sigma_{uq}^s(\theta_t, \phi_t; \pi - \theta_i, \phi_i) \cdot \cos\theta_s \left( \frac{L_{1p}(\theta_s) - L_{1u}(\theta_t)}{k_{1u}(\theta_t)\cos\theta_s - k_{1p}(\theta_s)\cos\theta_t} \right). \quad (13b)$$

The physical meaning of (13a) can be explained as follows. The quantity  $Q_{1uq}(\pi - \theta_t, \phi_t; \pi - \theta_i, \phi_i)$  represents the scattered signal from a unit volume located at  $z$  within the crown layer in  $(\pi - \theta_t, \phi_t)$  direction. Such a volume scattering generally causes depolarization. The incident wave on a scatterer at  $z$  is attenuated by a loss factor equal to  $\exp[k_{1q}(\theta_i)z\sec\theta_i]$ . For the scattered signal to reach the crown-trunk interface it is attenuated by a loss factor equal to  $\exp[-k_{1u}(\theta_t)(z + d_1)\sec\theta_t]$ . The integration of these two loss factors over the crown depth gives the quantity in the bracket in (13a). The  $L_{2u}(\theta_t)$  is the loss factor associated with the scattered signal passing through the trunk layer to the soil interface. For this signal to be scattered by the ground and to propagate to the receiver through the trunk and the crown layers, it should be modified by  $L_{1p}(\theta_s)L_{2p}(\theta_s)\sigma_{pu}^s(\theta_s, \phi_s; \theta_t, \phi_t)$ . The integration over  $d\theta_t$  and  $d\phi_t$  accounts for all possible scattering directions through which the signal is scattered from the canopy and propagates toward the ground. The summation over  $u$  in (13a) accounts for the possible polarization combinations. It is clear that in the plane of incidence or for a specular soil surface, there is no cross-polarized scattering from the surface and  $u$  takes on only one value. Similar interpretation is applicable to (13b). The backscattering coefficient corresponding to (13) is found by letting  $\hat{s} = -\hat{i}$ . The integrals in (13) can be evaluated numerically by applying Gaussian quadrature technique [30].

For a slightly rough surface, the coherent field is dominating and it will peak around the specular direction [2]. This allows the following approximation of the surface phase function for the coherent component,

$$\sigma_{qq}^s(\theta_i, \phi_i; \pi - \theta_i, \phi_i) = 4\pi \cos\theta_i R_{qq}(\theta_t) \delta(\cos\theta_t - \cos\theta_i) \cdot \delta(\phi_t - \phi_i) \exp(-4k^2\sigma^2 \cos^2\theta_i) \quad (14)$$

where  $R_{qq}(\theta_t)$  is the Fresnel reflectivity. In this case the backscattering coefficients due to the crown-soil interaction reduce to

$$\begin{aligned} \sigma_{pq}(c \rightarrow g) = & 4\pi \cos \theta_i L_{1p}(\theta_i) L_{2p}^2(\theta_i) R_{pp}(\theta_i) \exp(-4k^2 \sigma^2 \cos^2 \theta_i) \\ & \cdot Q_{1pq}(\pi - \theta_i; \pi + \phi_i; \pi - \theta_i, \phi_i) \left( \frac{L_{1p}(\theta_i) - L_{1q}(\theta_i)}{k_{1q}(\theta_i) - k_{1p}(\theta_i)} \right) \end{aligned} \quad (15a)$$

$$\begin{aligned} \sigma_{pq}(g \rightarrow c) = & 4\pi \cos \theta_i L_{1q}(\theta_i) L_{2q}^2(\theta_i) R_{qq}(\theta_i) \exp(-4k^2 \sigma^2 \cos^2 \theta_i) \\ & \cdot Q_{1pq}(\theta_i, \pi + \phi_i; \theta_i, \phi_i) \left( \frac{L_{1p}(\theta_i) - L_{1q}(\theta_i)}{k_{1q}(\theta_i) - k_{1p}(\theta_i)} \right). \end{aligned} \quad (15b)$$

It is clear that (15a) and (15b) satisfy the reciprocity,  $\sigma_{pq}(c \rightarrow g) = \sigma_{qp}(g \rightarrow c)$ . Hence, only one expression in (15) is needed. For like polarization the direct substitution of  $L_{1p}(\theta_i)$  and  $L_{1q}(\theta_i)$  in (15) gives an undetermined value for the backscattering coefficient. To find this value we let

$$\zeta = \left\{ \frac{L_{1p}(\theta_i) - L_{1q}(\theta_i)}{k_{1q}(\theta_i) - k_{1p}(\theta_i)} \right\}. \quad (16)$$

Then, substitution of (6) into (16) yields

$$\zeta = L_{1p}(\theta_i) \left\{ \frac{1 - e^{-(k_{1q}(\theta_i) - k_{1p}(\theta_i)) \cdot H_1 \sec \theta_i}}{k_{1q}(\theta_i) - k_{1p}(\theta_i)} \right\}. \quad (17)$$

By using Taylor expansion for the exponent within the bracket in (17) and keeping the first two terms of the expansion we get

$$\zeta = H_1 \sec \theta_i L_{1p}(\theta_i). \quad (18)$$

From (15) and (18) the like polarized backscattering coefficient for a slightly rough surface due to the crown-ground interaction can be approximated as

$$\begin{aligned} \sigma_{pp}(g \rightarrow c) = & 4\pi H_1 Q_{1pp}(\theta_i, \pi + \phi_i; \theta_i, \phi_i) \\ & \cdot R_{pp}(\theta_i) \exp(-4k^2 \sigma^2 \cos^2 \theta_i) \\ & \cdot [L_{1p}(\theta_i) L_{2p}(\theta_i)]^2. \end{aligned} \quad (19)$$

This above result will also hold for  $\sigma_{pp}^o(c \rightarrow g)$  due to reciprocity.

3) *Trunk Scattering*: The bistatic scattering coefficient of the trunk can be written as (illustrated in the backscattering direction by 3 in Fig. 1);

$$\begin{aligned} \sigma_{pq}(t) = & 4\pi L_{1p}(\theta_s) L_{1q}(\theta_i) Q_{2pq}(\theta_s, \phi_s; \pi - \theta_i, \phi_i) \\ & \cdot \left\{ \frac{1 - L_{2p}(\theta_s) L_{2q}(\theta_i)}{k_{2p}(\theta_s) \sec \theta_s + k_{2q}(\theta_i) \sec \theta_i} \right\} \\ Q_{2pq}(\theta_s, \phi_s; \pi - \theta_i, \phi_i) = & \sum_{m=1}^{N_2} n_m \langle |F_{mpq}(\hat{s}, \hat{i})|^2 \rangle \end{aligned} \quad (20)$$

where  $F_{mpq}(\hat{s}, \hat{i})$  is the element of the scattering amplitude matrix for a scatterer within a trunk group  $m$  ( $m = 1, \dots, t$ ). The scattering mechanism in (20) is similar to that in (11) except the scattered signal from the trunk layer is modified by an attenuation factor  $[L_{1p}(\theta_s) L_{1q}(\theta_i)]$  due to the crown layer.

4) *Trunk-Ground Interaction*: Similar to the crown-ground interaction, the trunk-ground interaction consists of two terms (illustrated in the backscattering direction by 5 in Fig. 1)

$$\sigma_{pq}(t \leftrightarrow g) = \sigma_{pq}(t \rightarrow g) + \sigma_{pq}(g \rightarrow t). \quad (21)$$

The first term in (21) represents scattering from the trunk followed by scattering from the ground. The second term represents scattering from the ground followed by scattering from the trunk. The explicit expressions for these two terms are

$$\begin{aligned} \sigma_{pq}(t \rightarrow g) = & L_{1p}(\theta_s) L_{1q}(\theta_i) L_{2p}(\theta_s) \int_0^{2\pi} d\phi_t \int_0^{\pi/2} \sin \theta_t d\theta_t \\ & \sum_{u=v,h} \sigma_{pu}^s(\theta_s, \phi_s; \theta_t, \phi_t) \cdot Q_{2uq}(\pi - \theta_t, \phi_t; \pi - \theta_i, \phi_i) \\ & \cdot \cos \theta_i \left[ \frac{L_{2u}(\theta_t) - L_{2q}(\theta_i)}{k_{2q}(\theta_i) \cos \theta_t - k_{2u}(\theta_t) \cos \theta_i} \right] \end{aligned} \quad (22a)$$

$$\begin{aligned} \sigma_{pq}(g \rightarrow t) = & L_{1p}(\theta_s) L_{1q}(\theta_i) L_{2q}(\theta_i) \int_0^{2\pi} d\phi_t \int_0^{\pi/2} \sin \theta_t d\theta_t \\ & \sum_{u=v,h} Q_{2pu}(\theta_s, \phi_s; \theta_t, \phi_t) \sigma_{uq}^s(\theta_t, \phi_t; \pi - \theta_i, \phi_i) \\ & \cdot \cos \theta_s \left[ \frac{L_{2p}(\theta_s) - L_{2u}(\theta_t)}{k_{2u}(\theta_t) \cos \theta_s - k_{2p}(\theta_s) \cos \theta_t} \right]. \end{aligned} \quad (22b)$$

The quantity  $Q_{2uq}(\theta_s, \phi_s; \theta_t, \phi_t)$  in (22b) is the scattered intensity per unit volume within the trunk layer. The quantity in bracket is the loss factor for volume scattering in the trunk region. Similar interpretation applies to quantities in (22a).

Similar to the crown-ground interaction (13) the integration over  $\theta_t$  and  $\phi_t$  can be performed by Gaussian quadrature [30]. For a specular or a slightly rough surface and backscattering direction, (22) can be approximated by

$$\begin{aligned} \sigma_{pq}(t \rightarrow g) = & 4\pi \cos \theta_i L_{1p}(\theta_i) \cdot L_{1q}(\theta_i) \cdot R_{pp}(\theta_i) \exp(-4k^2 \sigma^2 \cos^2 \theta_i) \\ & \cdot Q_{2pq}(\pi - \theta_i, \pi + \phi_i; \pi - \theta_i, \phi_i) \cdot \left[ \frac{L_{2p}(\theta_i) - L_{2q}(\theta_i)}{k_{2q}(\theta_i) - k_{2p}(\theta_i)} \right] \cdot L_{2p}(\theta_i) \\ = & \sigma_{qp}(g \rightarrow t). \end{aligned} \quad (23)$$

Following the derivation indicated in (16)–(18) we obtain the like polarized coefficients in the backward direction due to trunk-ground interaction as

$$\begin{aligned} \sigma_{pp}(g \rightarrow t) = & 4\pi H_2 Q_{2pp}(\theta_i, \pi + \phi_i; \theta_i, \phi_i) [L_{1p}(\theta_i) \cdot L_{2p}(\theta_i)]^2 \\ & \cdot R_{pp}(\theta_i) \exp(-4k^2 \sigma^2 \cos^2 \theta_i). \end{aligned} \quad (24)$$

C. *The Second-Order Solution* The second-order solution of the radiative transfer equation with respect to the crown layer albedo is obtained by using the first-order intensity within the canopy as an exciting source. This solution contains many terms, but most of these terms are small compared to the first-order solution. In this study only two dominant terms are kept. These terms are due to scattering within the crown layer. One significant difference between the first- and second-order terms is that the input to the first-order scattering usually involves only one Stokes parameter while the input to the second-order

scattering consists of all four Stokes parameters. The scattering process associated with each term is illustrated in Fig. 4 and their contribution to the bistatic scattering coefficient is given by

$$\sigma_{pq}^2 = \sigma_{pq}(+, +, -) + \sigma_{pq}(+, -, -) \quad (25)$$

where

$$\begin{aligned} \sigma_{pq}(+, +, -) = & 4\pi \int_0^{\pi/2} \sin \theta_t d\theta_t \int_0^{2\pi} d\phi_t \\ & \cdot \left[ \sum_{u=v,h} \frac{\cos \theta_i Q_{1pu}(\theta_s, \phi_s; \theta_t, \phi_t)}{k_{1u}(\theta_t) \cos \theta_i + k_{1q}(\theta_i) \cos \theta_t} \right. \\ & \cdot Q_{1uq}(\theta_t, \phi_t; \pi - \theta_i, \phi_i) \left\{ \frac{1 - L_{1p}(\theta_s) L_{1q}(\theta_i)}{k_{1p}(\theta_s) \sec \theta_s + k_{1q}(\theta_i) \sec \theta_i} \right. \\ & + L_{1q}(\theta_i) \frac{L_{1u}(\theta_t) - L_{1p}(\theta_s)}{k_{1u}(\theta_t) \sec \theta_t - k_{1p}(\theta_s) \sec \theta_s} \left. \right\} \\ & + 2\text{Re} \left( \frac{\cos \theta_i Q_{1p3}(\theta_s, \phi_s; \theta_t, \phi_t)}{k_{13}(\theta_t) \cos \theta_i + k_{1q}(\theta_i) \cos \theta_t} \right. \\ & \cdot Q_{13q}(\theta_t, \phi_t; \pi - \theta_i, \phi_i) \left\{ \frac{1 - L_{1p}(\theta_s) L_{1q}(\theta_i)}{k_{1p}(\theta_s) \sec \theta_s + k_{1q}(\theta_i) \sec \theta_i} \right. \\ & + L_{1q}(\theta_i) \frac{L_{13}(\theta_t) - L_{1p}(\theta_s)}{k_{13}(\theta_t) \sec \theta_t - k_{1p}(\theta_s) \sec \theta_s} \left. \right\} \left. \right] \quad (26a) \end{aligned}$$

$$\begin{aligned} \sigma_{pq}(+, -, -) = & 4\pi \int_0^{\pi/2} \sin \theta_t d\theta_t \int_0^{2\pi} d\phi_t \\ & \cdot \left[ \sum_{u=v,h} \frac{\cos \theta_s Q_{1pu}(\theta_s, \phi_s; \pi - \theta_t, \phi_t)}{k_{1u}(\theta_t) \cos \theta_s + k_{1p}(\theta_s) \cos \theta_t} \right. \\ & \cdot Q_{1uq}(\pi - \theta_t, \phi_t; \pi - \theta_i, \phi_i) \left\{ \frac{1 - L_{1p}(\theta_s) L_{1q}(\theta_i)}{k_{1p}(\theta_s) \sec \theta_s + k_{1q}(\theta_i) \sec \theta_i} \right. \\ & + L_{1p}(\theta_s) \frac{L_{1u}(\theta_t) - L_{1q}(\theta_i)}{k_{1u}(\theta_t) \sec \theta_t - k_{1q}(\theta_i) \sec \theta_i} \left. \right\} \\ & + 2\text{Re} \left( \frac{\cos \theta_s Q_{1p3}(\theta_s, \phi_s; \pi - \theta_t, \phi_t)}{k_{13}(\theta_t) \cos \theta_s + k_{1p}(\theta_s) \cos \theta_t} \right. \\ & \cdot Q_{13q}(\pi - \theta_t, \phi_t; \pi - \theta_i, \phi_i) \left\{ \frac{1 - L_{1p}(\theta_s) L_{1q}(\theta_i)}{k_{1p}(\theta_s) \sec \theta_s + k_{1q}(\theta_i) \sec \theta_i} \right. \\ & + L_{1p}(\theta_s) \frac{L_{13}(\theta_t) - L_{1q}(\theta_i)}{k_{13}(\theta_t) \sec \theta_t - k_{1q}(\theta_i) \sec \theta_i} \left. \right\} \left. \right] \quad (26b) \end{aligned}$$

where  $\text{Re}(\cdot)$  is the real part operator and,

$$\begin{aligned} Q_{1v3}(\theta_s, \phi_s; \theta_t, \phi_t) &= \sum_{m=1}^{N_1} n_m \langle F_{m vv}(\hat{s}, \hat{i}) F_{m v h}^*(\hat{s}, \hat{i}) \rangle \\ Q_{13v}(\theta_s, \phi_s; \theta_t, \phi_t) &= \sum_{m=1}^{N_1} n_m \langle F_{m vv}(\hat{s}, \hat{i}) F_{m h v}^*(\hat{s}, \hat{i}) \rangle \\ Q_{13h}(\theta_s, \phi_s; \theta_t, \phi_t) &= \sum_{m=1}^{N_1} n_m \langle F_{m v h}(\hat{s}, \hat{i}) F_{m h h}^*(\hat{s}, \hat{i}) \rangle \\ Q_{1h3}(\theta_s, \phi_s; \theta_t, \phi_t) &= \sum_{m=1}^{N_1} n_m \langle F_{m h v}(\hat{s}, \hat{i}) F_{m h h}^*(\hat{s}, \hat{i}) \rangle \end{aligned} \quad (27)$$

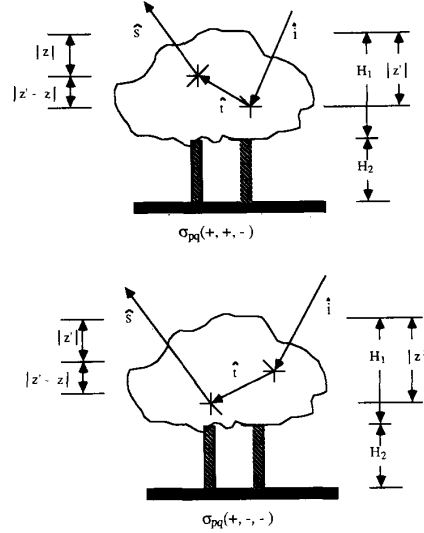


Fig. 4. The scattering processes in (26) associated with the second-order solution of the radiative transfer equation.

with  $*$  is the complex conjugate operator. In addition

$$\begin{aligned} k_{13}(\theta_t) &= \frac{1}{2} [k_{1v}(\theta_t) + k_{1h}(\theta_t)] \\ &+ \frac{2\pi j}{k} \text{Re} \left[ \sum_{m=1}^{N_1} n_m \langle F_{m vv}(\hat{t}, \hat{t}) - F_{m hh}(\hat{t}, \hat{t}) \rangle \right] \\ L_{13}(\theta_t) &= \exp[-k_{13}(\theta_t) H_1 \sec \theta_t]. \end{aligned} \quad (28)$$

The processes of scattering in (26a) are illustrated in Fig. 4. From this figure we see that  $\sigma_{pq}(+, +, -)$  represents scattering by a unit volume first from direction  $\hat{i}(\pi - \theta_i, \phi_i)$  to direction  $\hat{t}(\theta_t, \phi_t)$  and then by another unit volume from direction  $\hat{t}(\theta_t, \phi_t)$  to the observation direction  $\hat{s}(\theta_s, \phi_s)$ . These two processes are represented by the quantities  $Q_{1pu}(\theta_s, \phi_s; \theta_t, \phi_t)$   $Q_{1uq}(\theta_t, \phi_t; \pi - \theta_i, \phi_i)$  for the first two Stokes parameters and by  $Q_{1p3}(\theta_s, \phi_s; \theta_t, \phi_t)$   $Q_{13q}(\theta_t, \phi_t; \pi - \theta_i, \phi_i)$  for the last two Stokes parameters. To reach the first scattering volume the incident wave is attenuated by  $e^{k_{1q}(\theta_i) z' \sec \theta_i}$ . In going from the first to the second scattering volume, the wave is further attenuated by  $e^{k_{1u}(\theta_i)(z' - z) \sec \theta_i}$ . After the second scattering the scattered wave with  $p$  polarization is attenuated by  $e^{k_{1p}(\theta_s) z \sec \theta_s}$  before it reaches the canopy-air interface. The integration of the product of these loss factors over  $dz'$  and  $dz$  ( $-H_1 \leq z' \leq z$ , and  $-H_1 \leq z \leq 0$ ) gives the other quantities in (26a). The summation in (26a) accounts for the first and second Stokes' parameters of the scattered wave in  $\hat{t}(\theta_t, \phi_t)$  direction. The  $\text{Re}(\cdot)$  comes from summing the last two Stokes' parameters  $\hat{i}(\theta_i, \phi_i)$ . The integration over  $d\theta_t$  and  $d\phi_t$  accounts for all possible scattering directions through which the signal scattered from location  $z'$  toward location  $z$ . Similar interpretation is applicable to  $\sigma_{pq}(+, -, -)$  in (26b).

From (26)–(28) it is clear that the second-order solution requires all the four Stokes parameters. Also we can see that

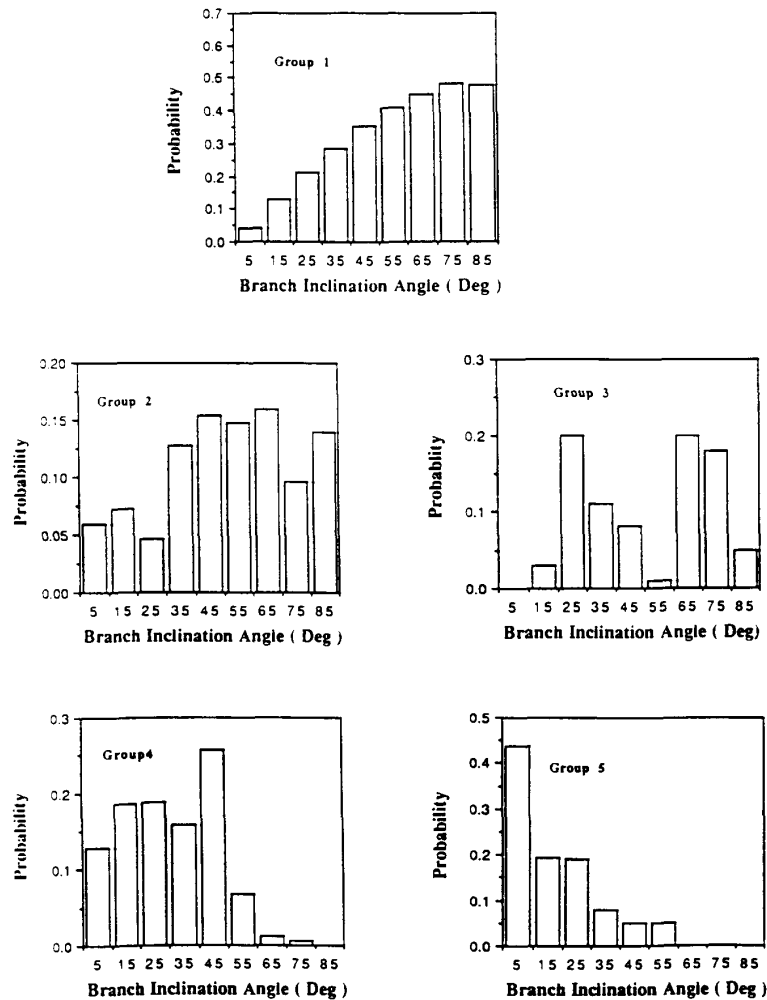


Fig. 5. The probability distributions of the inclination angles for different groups of branches.

TABLE I  
THE PARAMETER FOR EACH BRANCH GROUP

Branch Group	Diameter Range (cm)	Average Diameter (cm)	Average Length (cm)	Number density ( $\text{m}^{-3}$ )
1 /stems	0.0–0.40	0.10	18	250
2	0.5–1.90	1.28	14	11.4
3	2.0–2.90	2.60	32	0.43
4	3.0–6.90	5.00	58	0.33
5 /trunk	7.0–17.1	9.00	76	0.14

the second-order solution includes scattering due to interaction between the forest components.

#### IV. GROUND TRUTH DATA, NUMERICAL RESULTS AND ANALYSIS

In this section comparisons of this model with backscattering measurements from both deciduous and coniferous forest, are carried out to verify the model validity. In addition, the

effects of frequency, second-order interaction, and surface roughness as it impacts tree-ground interaction are illustrated to indicate the model major advantages. Results are organized into three subsections. In the first subsection, the characteristics of a deciduous and a coniferous canopy and the associated ground truth are described. The second subsection shows comparisons between the calculated and measured values of the backscattering coefficients for walnut canopy at  $L$  and  $X$  bands and for cypress trees at  $S$  and  $X$  bands. Furthermore, illustrations are given showing the contribution of each canopy component to the total backscattering coefficient. The third subsection presents some numerical results to indicate how frequency, second-order interaction, and surface roughness affect the backscattering coefficients.

##### A. Deciduous and Coniferous Canopy Characteristics

In this study the walnut canopy and the cypress trees are taken to represent a deciduous and a coniferous canopy respectively. We shall begin by describing the walnut canopy

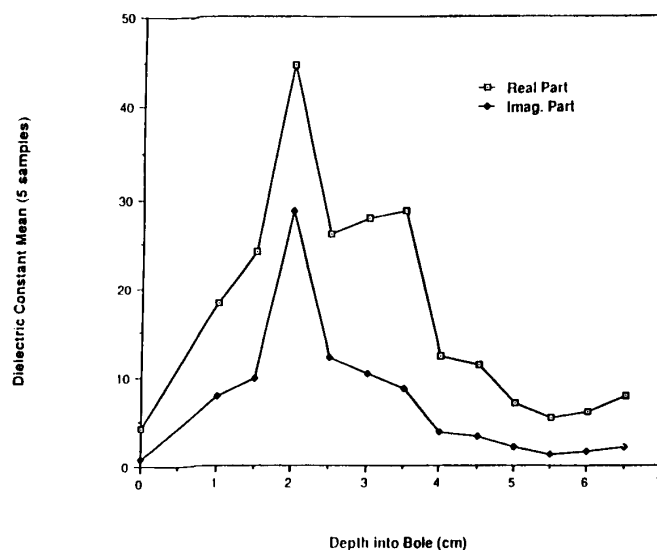


Fig. 6. The relative dielectric constant as a function of depth into walnut bole.

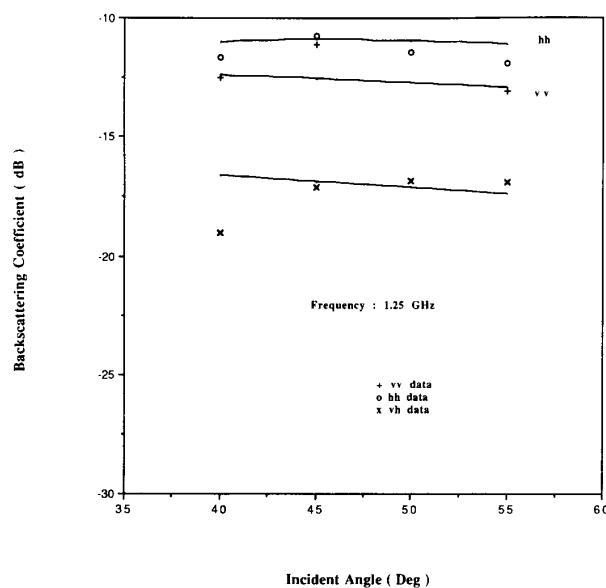


Fig. 7. Comparisons of theoretical and experimental backscattering coefficients for a walnut canopy at L band as a function of the incident angle.

TABLE II  
DIELECTRIC CONSTANT VALUES

Frequency Band	$L$	$X$
Leaves	19.58-j 5.54	14.9-j 4.9
branch/stems	27.3-j 8.4	20.0-j 9.7
soil	5.00-j 0.7	5.00-j 0.7

and its parameters and then the cypress trees.

#### 1) The Walnut Canopy Characteristics:

The canopy consists of 6-year-old black walnut trees [26, Sec. V, Vol I]. The trees have an average height of 4.8 m.

Their geometry data was collected in two parts. Measurements involving branches with diameter greater than 4 cm were termed skeleton geometry measurements and the rest higher order measurements. A group of 16 walnut trees was chosen for the canopy geometry and ground truth measurements. Their heights, width across the row, and the length down the row were measured. The skeleton branches which terminated into a successively smaller diameter branch were physically sampled for their length, diameter, and inclination angle for all 16 trees. Small branches that grew along the skeleton tend to fill the interior of the canopy. Such branches with diameter less than 4 cm were sampled only for a couple of trees. The thinnest branches with diameter less than 1 cm and length less than 30 cm, were not sampled for their inclination orientations. The branches were grouped into four different groups according to their radius, and for each group an average length of the branch was computed. Beside these four branch groups, there are green stems which have an external covering of green bark and are located just below the juncture with the petioles. For modeling purposes we will consider the stems as a group of branches. The stem group will be labeled as group #1 among the other branch groups. Table I sums up the relevant parameters for each branch group type.

From the inclination angle measurements of the branches, the inclination angle probabilities for all branch groups are calculated. Fig. 5 presents the histograms of the inclination angle probabilities for different radius groups. The data show that as the diameter of the branch increases, it tends to become vertical. The thin branches do not show any preferred inclination.

The leaves were found to be growing only on the branches in groups 1 and 2. The leaves on group 2 branches were determined from the routine sampling of higher order canopy geometry measurements. However, due to the large number of branches in group 1, an exclusive sampling was done to



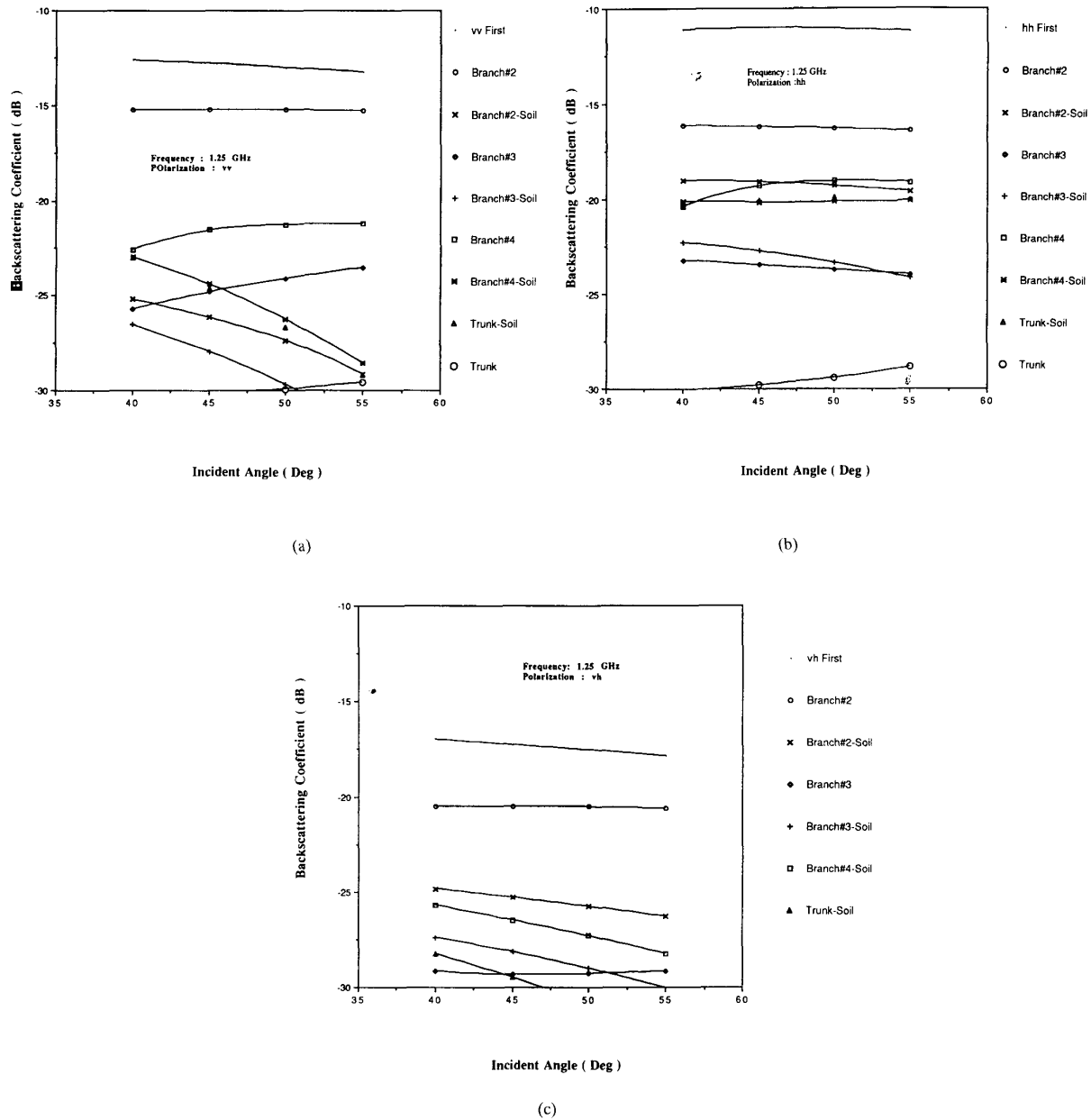


Fig. 8. Illustrations of the contributions by the walnut canopy components in first-order backscattering for (a) VV, (b) HH, and (c) VH polarizations at  $L$  band.

estimate the number of leaves per branch in the group 1 category. This leaf data was extrapolated to cover the whole canopy. The average density of the leaves was  $250 \text{ m}^{-3}$  [15]. Each leaf had an average leaf area of 254 square cm and on the average there were five leaflets on one leaf. Assuming the leaves to be circular, the leaf area results gave the average disc radius of approximately 3.6 cm and a thickness equal to 0.1 mm. The leaf inclination angle has a probability distribution function equal to  $\sin \beta (0^\circ < \beta < 90^\circ)$ .

*In situ* measurements of dielectric constant of stems, branches, and leaves were made by a team from the University of Michigan at  $L$  band ( $f = 1.2 \text{ GHz}$ ). An electric probe

was inserted into a hole drilled into a branch to find the dielectric constant [26, Sec. XIII, Vol. II]. The leaves were stacked in layers upon a flat piece of wood. For each stack, the probe reading was noted at three separate locations on the stack. The behavior of the dielectric constant with depth inside a branch or on a stack of leaves was found from probe readings. Fig. 6 shows the relative dielectric constant as a function of depth into walnut bole. It is clear the dielectric constant real part has values between 4 and 45. The imaginary part varies between 1 and 30. For stem dielectric constant a representative value at the  $L$  band is found to be  $27.3 - j 8.4$ . As this value for the dielectric constant is a mean value for

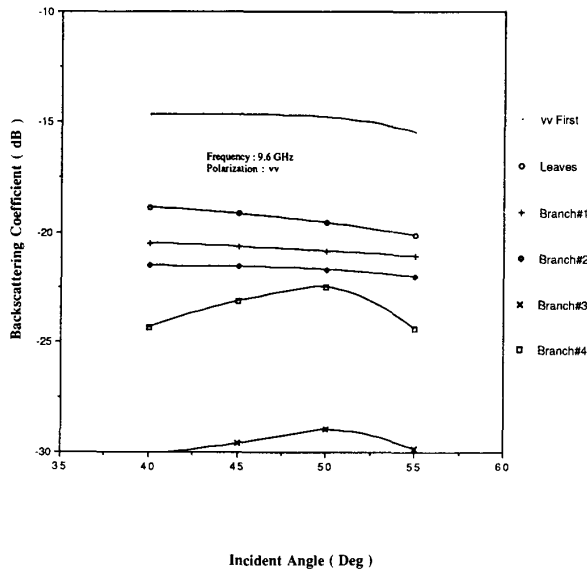


Fig. 9. Comparisons of theoretical and experimental backscattering coefficients for a walnut canopy at X band as a function of the incident angle.

TABLE III  
GROUND TRUTH FOR CYPRESS TREE SCATTERER

	Leaves	Branch#1	Branch#2	Branch#3
Length (cm)	1	13	18	20
Radius (cm)	0.1	0.12	0.3	1
Number	$0.796 \times 10^5$	400	64	10
Density ( $\text{m}^{-3}$ )				
$B_m$ ( $^\circ$ )	90	90	90	0.0
$B_0$ ( $^\circ$ )	0.0	0.0	0.0	10
$B_1$ ( $^\circ$ )	0.0	0.0	0.0	0.0
$B_2$ ( $^\circ$ )	90	90	90	60
$n$	2	1	1	6

the bole dielectric constant, it will be taken as representative value for branch dielectric constant. The leaf dielectric value varies from  $8.77 - j 2.88$  to  $19.58 - j 5.54$  according to the number of the leaves stacked in layers upon a flat piece of wood to measure the dielectric constant. Consequently, an average value  $19.58 - j 5.54$  will be used to represent the leaf dielectric constant. There is no independent confirmation of the leaf and branch dielectric constant values as high as used in [14].

The soil relative dielectric constant measurements were repeated on hourly basis. Each observation sequence consisted of three types of data designated: wet, dry, and mix. The wet and dry consisted of separate samples of the soil surface regions which were always wet or always dry, respectively. A transect sampling was used to evaluate the spatial average of the dielectric constant over the three moisture regions. The dielectric transect data consisted of 22 samples spaced 0.3 m apart and extending from center of one row to the center of the next. The location of the transect along a row with respect to the tree and sprinkler location was randomized. The sprinklers were placed along the rows of the trees to irrigate the trees. The water from sprinklers was sprayed in an approximately 3-ft wide strip along the rows of the trees. There was no

sprinkler in between the tree rows. Thus approximately 70% of the area was not irrigated and thus can be classified as "dry soil." It was found that inter-row dielectric constant has values between  $18.48 - j 1.6$  and  $2.79 - j 0.16$ . Furthermore, ten soil samples taken from area partially covered by organic leaf litter showed an average dielectric constant value of  $2.96 - j 0.49$ . In addition, the spatial averaging for backscatter as seen by the radar was done by rotating the boom across the rows in an arc and it was not done along the tree rows. Accordingly, we believe that the ground dielectric constant should have a small average value which is taken to be  $5.0 - j 0.7$ .

To obtain the values of the leaf and branch dielectric constant at X band ( $f = 9.6$  GHz), the corresponding values at L band are incorporated in Ulaby and El Rayes' dielectric constant formula [31] to obtain the leaf and branch gravimetric moisture contents (0.55 for leaves and 0.65 for branches). By substituting these values for the moisture contents along with the X band frequency into Ulaby and El Rayes formula, we obtain the values of the dielectric constant at X band ( $14.9 - j 4.9$  for leaves and  $20. - j 9.7$  for branches). Since the soil effect at X band is unimportant in the backscattering calculation, its dielectric constant is not estimated at X band. Table II sums up the dielectric constant values used for the leaves and stems and branches.

For the purpose of modeling we divide the canopy into two layers above a rough interface. The upper layer with a depth of 3 m is the crown layer and the lower layer with a depth of 1.7 m is for the trunk layer. The crown layer contains leaves and the first four branch groups. The fifth branch group is included in the trunk layer. The soil-canopy interface roughness is represented by a Gaussian correlation function with  $\sigma$  and  $L$  given by 0.021 m and 0.25 m, respectively. In calculating the crown- and trunk-soil interaction terms (13), (22) the soil scattering coefficient  $\sigma_{pu}^s(\theta_s, \phi_s; \theta_t, \phi_t)$  is obtained by summing up the coherent (Eq. 12.52 of [2]) and the noncoherent (Eq. 12.55 of [2]) scattering terms.

2) *The Cypress Tree Characteristics:* The cypress trees with the same height and nearly the same density are considered [4]. They are 3–4 years old. Their trunks are thin, having a diameter of 1–2 cm. The average height of the canopy was about 70 cm. The canopy without leaves is composed of a large number of randomly oriented thin branches and a small number of thin vertical trunks. The leaflets of cypress form a thin rod shape, with length of 1 cm and a diameter of 2 mm, and the whole assembly comprises a relatively flat planer structure. The ground plane is covered with microwave absorbers so that canopy ground interaction effect is unimportant. In this study a one layer model (crown) is used since the trunk height is small. The canopy constituents are grouped into four groups, one group for the leaves; three other groups for the branches. The scatterer inclination angle distribution ( $\beta$ ) is governed by the following probability distribution function

$$P(\beta) = A \cos^n \left[ \frac{\pi}{2} \left( \frac{\beta - \beta_m}{\beta_0 - \beta_m} \right) \right], \quad \beta_1 \leq \beta \leq \beta_2$$

$$= 0 \quad \text{otherwise} \quad (29)$$

where  $A$  is the normalization factor, and  $n$  is the shape factor. The probability density function  $P(\beta)$  has its maximum value at  $\beta_m$ , and is equal to zero at  $\beta$  equal to  $\beta_0$ . By adjusting the values of  $\beta_0, \beta_1, \beta_2, \beta_m$ , and  $n$ , the probability density function  $P(\beta)$  in (29) can include a variety of probability density functions reported in the literature [32].

The dielectric constants of the coniferous scatterers (needle leaves, and branches) are obtained by employing Ulaby and El-Rayes' formula [31] which gives the dielectric constant in terms of the gravimetric moisture content. For cypress trees under consideration, the reported values for the leaf and branch gravimetric moisture contents are around 58.

#### B. Comparisons with Backscatter Measurements from Walnut Orchard Canopy

Several sets of microwave data were collected from the walnut canopy [26]. In this study we shall consider two sets of multi-angle data in which the same set of trees were observed at incident angles ranging from  $40^\circ$  to  $55^\circ$  at two different frequencies, 1.25 GHz ( $L$  band) and 9.6 GHz ( $X$  band). The data were collected over a time span of about 2 hours during mid-afternoon, so the variation in the dielectric constant due to the change of environment can be neglected. The model was evaluated as a function of look angle for frequencies 1.25 and 9.6 GHz using the ground truth reported in Tables I and II and Fig. 5. The model output is given in Figs. 7–10. Figs. 7 and 9 show comparisons of measured and calculated scattering coefficients for three different polarizations at  $L$  band and  $X$  band, respectively. Figs. 8 and 10 show the contributions of the individual tree components to the total backscattering coefficients, excluding those more than 15 dB below the total.

At  $L$  band (Fig. 7) there is a good agreement between theory and measurements. The like polarized backscattering coefficients  $\sigma_{vv}$  and  $\sigma_{hh}$  have the same angular trends with  $\sigma_{vv} < \sigma_{hh}$ . The cross polarization  $\sigma_{vh}$  is below the like by about 6 dB. Fig. 8 indicates that the main contribution to the like and cross backscattering coefficients is due to branch group #2. The branches within this group have no preferred orientation and their dimensions are such that their contributions to  $\sigma_{vv}$  and  $\sigma_{hh}$  are approximately the same. Other canopy constituents may be small compared to the wavelength (leaves and branch group #1), or comparable to the wavelength and they are nearly vertically oriented (branch #4 and branch #5). For the small scatterers, their contribution to the like and cross polarization is lower than the noise level. The larger scatterers have radiation pattern with maximum field values confined to the forward direction. Consequently, the scattered field is propagating toward the canopy floor, leading to the soil–canopy interaction terms. Since within the angular range considered in this section, the soil reflectivity is higher for horizontally incident wave than for vertically incident wave, the contribution of the interaction terms are higher for  $\sigma_{hh}$  than  $\sigma_{vv}$ . This is the reason, why  $\sigma_{hh} > \sigma_{vv}$ . Unlike reference [14] we assume the surface to be moderately wet instead of very wet so that this interaction term is not of major importance in  $\sigma_{hh}$ . We made this choice because the surface truth reported in [26] indicates that the very wet condition is a special situation. Also, the  $\sigma_{vv}$  and  $\sigma_{hh}$  returns

are very close to each other. This can be explained if scattering for  $\sigma_{vv}$  and  $\sigma_{hh}$  is dominated by the same branch group as we have found. However, if  $\sigma_{vv}$  is dominated by one branch group and  $\sigma_{hh}$  is dominated by trunk–ground interaction as indicated in [14], then similar level for  $\sigma_{vv}$  and  $\sigma_{hh}$  must be a coincidence.

At  $X$  band, the levels of the backscattering coefficients and the relative levels between polarization components are in agreement with measurements (Fig. 9). An earlier publication [15] did not obtain an agreement at this frequency for cross polarization even though model parameters were readjusted between  $L$  band and  $X$  band. We believe this is due to several factors: (1) enough groups of branches, i.e., an adequate representation of branch size distribution, (2) second-order effects, and (3) validity of model over a wide enough range of frequencies. At  $X$  band the polarized backscattering coefficients have similar angular trends. The cross polarized backscattering coefficient level is below the like polarization by nearly 8 dB. Illustrations of the individual contributors are given in Fig. 10. Here, for like-polarized scattering the leaves and the branch groups #1 and #2 are the most important contributors. At  $X$  band, the dimensions of those scatterers (leaves, branch #1, branch #2) are sensitive to the incident wavelength, and they have no preferred orientation. At this frequency, the interactions with the ground surface are negligible. For cross polarized scattering the major contribution comes from branch group #1 which is the smallest branch group (stems). The cause of depolarization appears to be the small cylindrically shaped stem and its orientation distribution. The leaf area is large at  $X$  band and hence its depolarization is weak. The  $\sin \beta$  function for the leaf orientation distribution also leads to a very small contribution to cross polarization [16], [17], [29].

*Comparisons with Backscattering Measurements from Cypress Trees:* The measurements from a cypress canopy with and without leaves were reported by Hirose *et al.* [4] at  $S$ ,  $C$ , and  $X$  bands for incident angles between  $10^\circ$  and  $40^\circ$ . In this study the  $S$  and  $X$  band data are selected for comparison. The ground truth given in Table III are used in the model to calculate the backscattering coefficients. Figs. 11(a) and (b) show the comparisons with  $S$  band measurements with and without leaves. Results indicate that negligible change takes place due to the presence or absence of leaves at this frequency. The agreement between model and measurements is very good for like and cross polarizations except at  $10^\circ$  incidence in like polarization in Fig. 11(b). This may be due to scattering from the ground which is not well covered with microwave absorber. Similar comparisons at  $X$  band are shown in Figs. 12(a) and (b). Here again the agreement between model and measurements is very good. The presence of leaves leads to a 4-dB and a 2-dB increase in like and cross-polarized scattering, respectively. Thus, leaves are important scatterers at  $X$  band for cypress as well as the walnut trees discussed in the previous section.

#### C. Surface Roughness, Frequency and Second-Order Effects

In this section we want to illustrate the effects of soil surface roughness, frequency, and the second-order terms in backscattering.

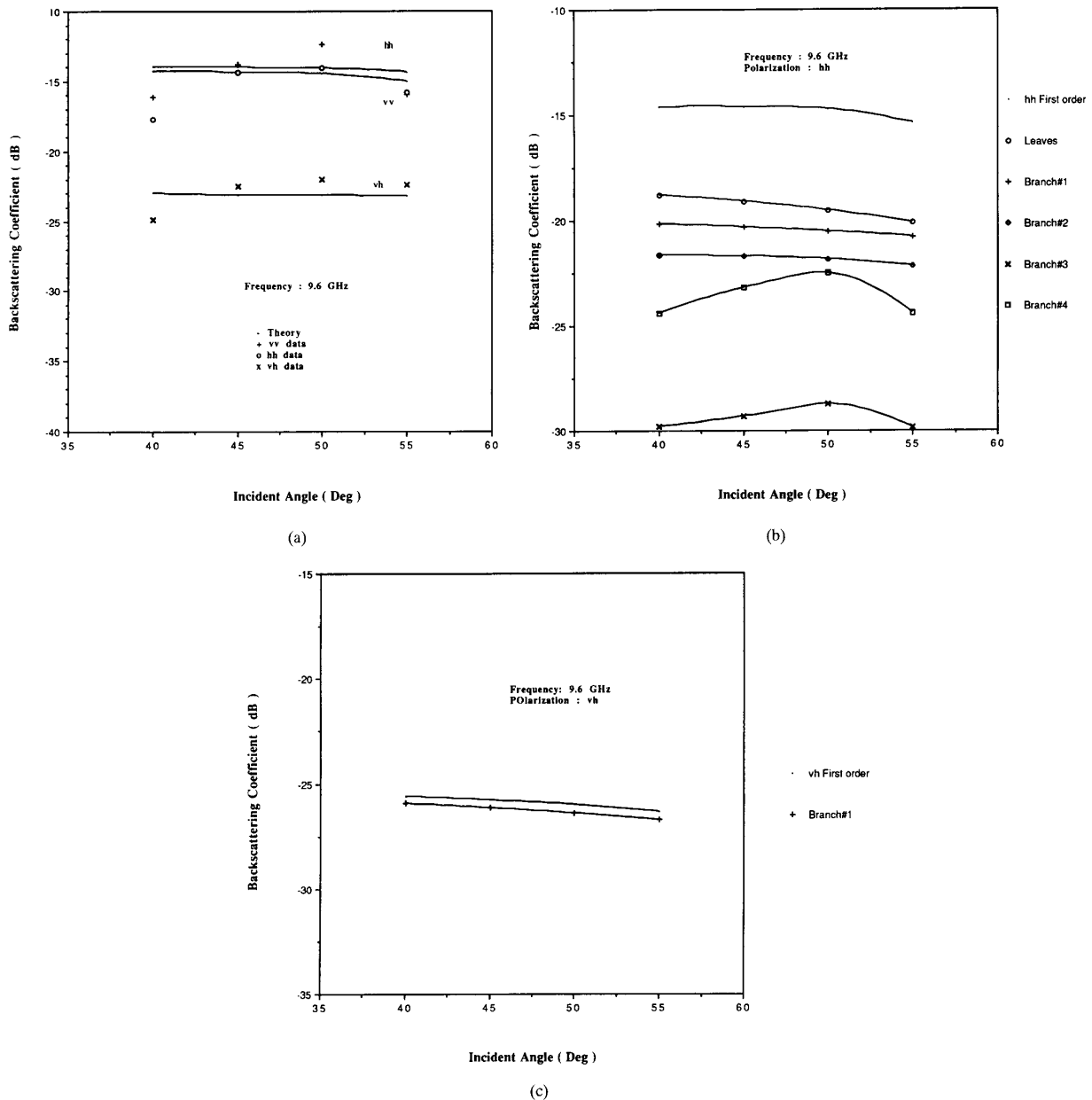


Fig. 10. Illustrations of the contributions by the walnut canopy components in first-order backscattering for (a) VV, (b) HH, and (c) VH polarizations at X band.

*1) The Role of Surface Roughness on the Interaction Terms:* Scattering due to a rough surface is well known and can be computed easily. Less obvious is how canopy interacts with a plane versus a rough ground surface. More specifically the inclusion of the ground-canopy interaction term is not fully accounted for in the available models [10]–[13] because only a flat ground is considered. To see the difference between the use of a flat versus a rough ground surface we show in Figs. 13(a)–(c) the surface roughness effects on the soil-canopy interaction terms for like and cross polarizations. These figures are generated by using the ground truth reported for walnut

canopy in Tables I and II at L band. For the rough surface the correlation function is taken to be Gaussian and the scattering matrix is obtained by employing the Kirchhoff model along with the scalar approximation [2, Chapter 12].

From these figures we see that the inclusion of surface roughness leads to a reduction in the interaction terms for like polarizations (VV, HH) near nadir incidence but an increase in the like and cross polarization terms at higher incidence angles. The angular range within which the interaction terms are higher for the rough than the plane surface varies from one polarization to another and is expected to vary also with

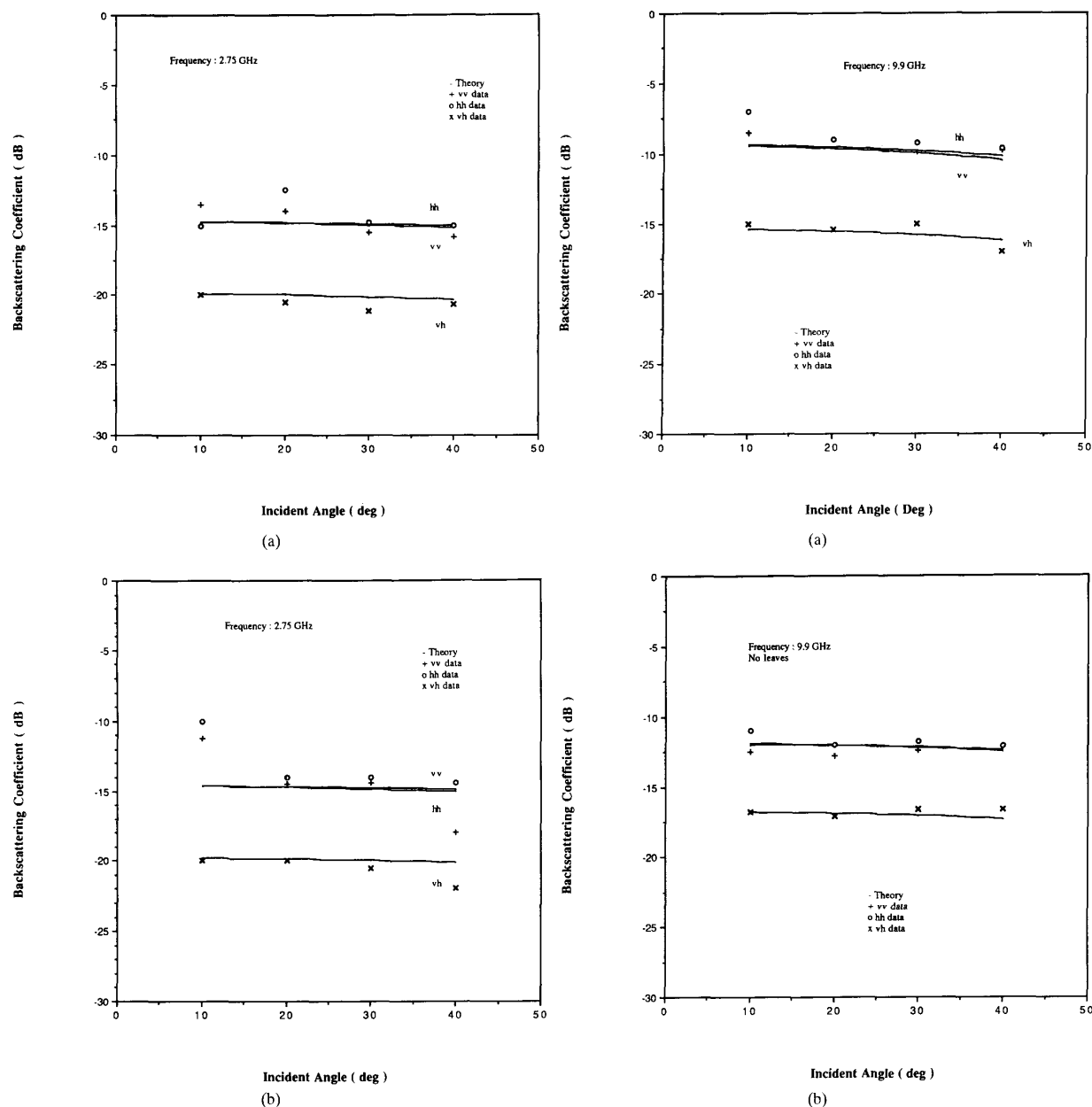


Fig. 11. Comparisons of theoretical and experimental backscattering coefficients for a cypress canopy at *S* band as a function of the incident angle: (a) With leaves. (b) Without leaves.

Fig. 12. Comparisons of theoretical and experimental backscattering coefficients for a cypress canopy at *X* band as a function of the incident angle. (a) With leaves. (b) Without leaves.

a change in the roughness property. While soil roughness is found to be unimportant in the comparisons shown in Section IV.B.1, it is expected to be important when the soil surface is wet.

2) *Second-Order Terms in the Backscattering Coefficients:* The effect of the second-order scattering terms due to branches was not considered in the previous models [11]–[15]. The introduction of the second-order terms in this study is a way to account for the multiple scattering effects within a forested canopy. From the numerical calculations we found that the

second-order terms had little effect on the level and trend of the like polarized signals. Hence, illustrations are limited to cross polarized calculations.

Fig. 14 presents the angular variation of the first- and second-order cross polarized signals ( $\sigma_{vh}$ ) at *L* and *X* bands using model parameters for the walnut orchard. It is seen that the second-order term is not important at *L* band but is significant at *X* band. Fig. 15 shows the variation of the cross polarized signal from cypress trees as a function of frequency at 40° angle of incidence. From these figures we see that

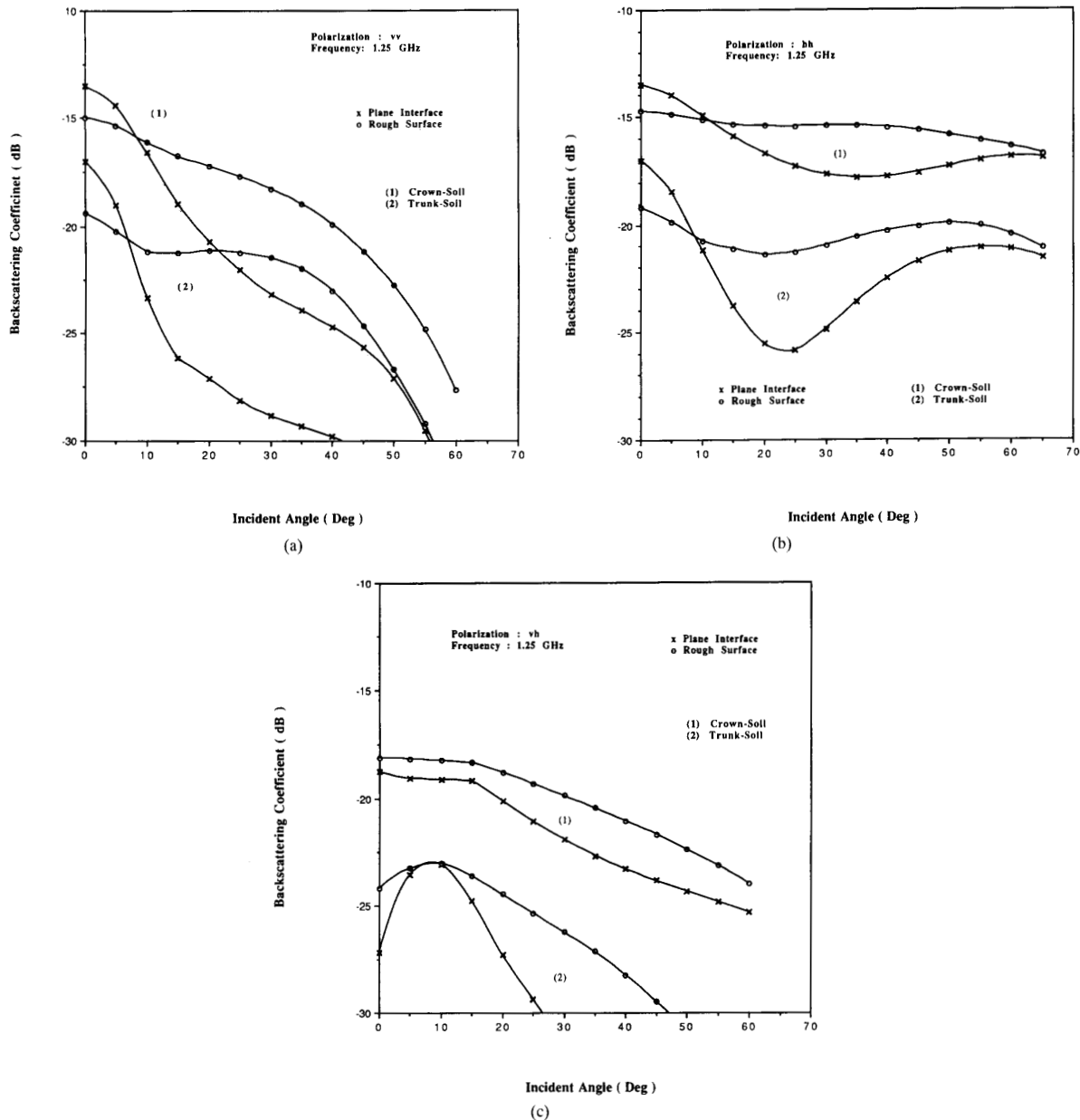


Fig. 13. The effect of including the surface roughness in the canopy-ground interaction on backscattering from a walnut canopy at L band: (a) VV polarization; (b) HH polarization; (c) VH polarization.

the importance of multiple scattering effects are dependent on frequency and canopy parameters.

3) *Frequency Dependence:* One merit of the current model is that it can be applied over a wide frequency band without changing the forest component modeling or adjusting the forest component phase matrices and extinction cross sections. Fig. 16 shows the variation of the backscattering coefficient for cypress trees as a function of the incident frequency at 40° incidence. From this figure we see that for frequency lower than 4 GHz, the backscattering coefficients increase rather quickly with frequency. This increase indicates a Rayleigh

region for the canopy. In the frequency range, 4–8 GHz, the rate of increase of the backscattering coefficients with frequency is much smaller. This corresponds to the resonance region where significant phase interference takes place. For frequencies higher than 8 GHz, the backscattering coefficients have a higher rate of increase with the frequency. This is not necessary true in general but is due to the specific canopy constituents as illustrated in Fig. 17. Here, the needle-shaped leaves happen to have a dimension that is still in the Rayleigh region and hence its contribution increases fast with frequency. In conclusion, the final frequency behavior of a forest canopy

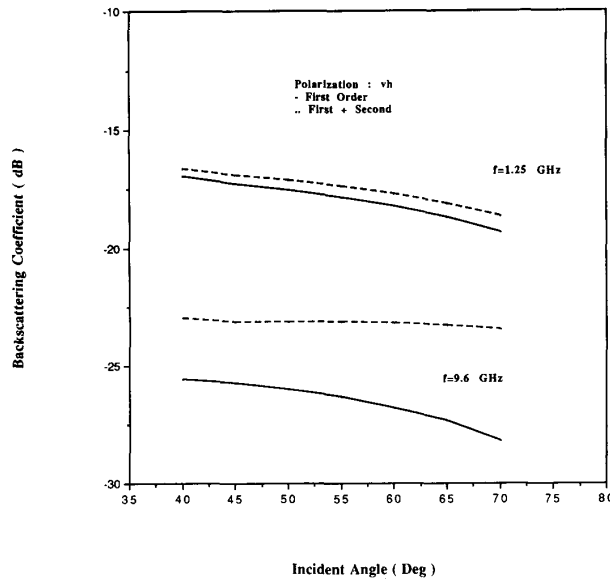


Fig. 14. The angular variation of cross-polarized coefficient for walnut canopy calculated by using the first and second-order solution of the radiative transfer equation at  $L$  and  $X$  band (parameters of Figs. 7 and 9).

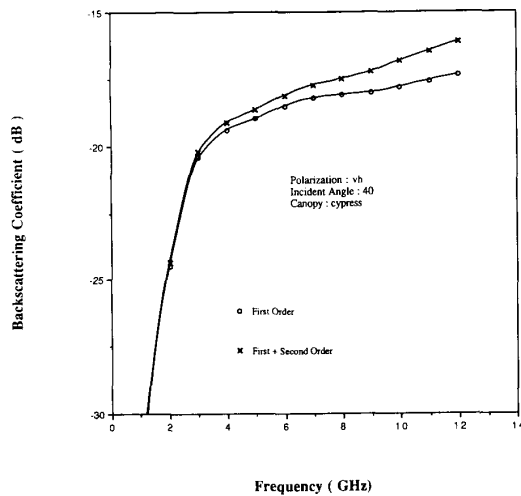


Fig. 15. The variation of the cross-polarized coefficients for cypress trees with the frequency, calculated by using the first and second-order solution of the radiative transfer equation at  $40^\circ$  angle of incidence (parameters as in Figs. 11 and 12).

is dependent on the specific sizes of its components. Hence, it is important to model each canopy component over a wide range of frequency.

## V. DISCUSSION

In this paper a microwave scattering model has been developed for layered vegetation and compared with experimental data from walnut and cypress trees. The major advantages of this model are that, it (1) accounts for first- and second-order scattering within the canopy, (2) fully accounts for the surface

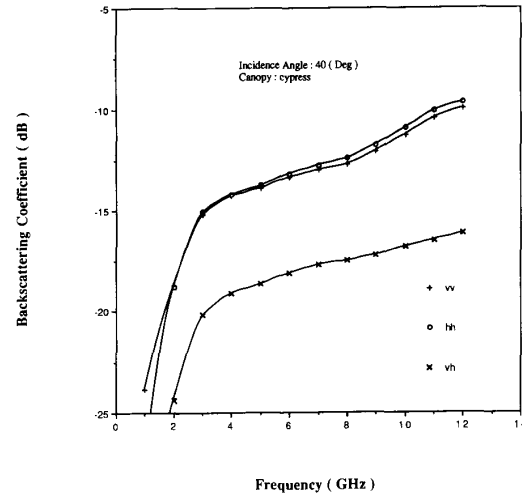


Fig. 16. The variation of the like and cross backscattering coefficients for cypress trees as a function of the incident frequency (parameters as in Figs. 11 and 12).

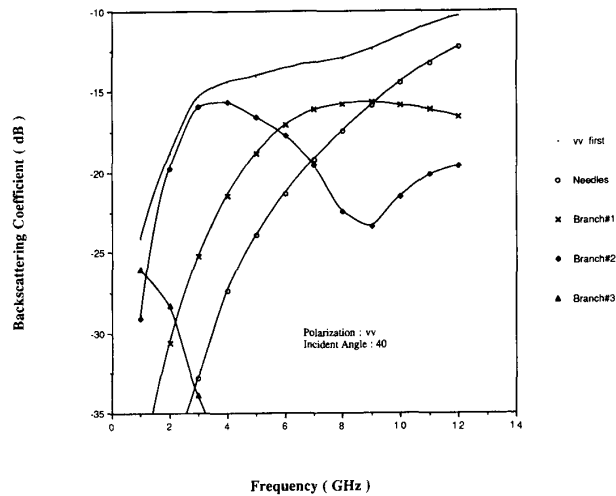


Fig. 17. The components of  $\sigma_{vv}$  for cypress trees as a function of the incident frequency (parameters as in Figs. 11 and 12).

roughness in the canopy-soil interaction terms (3) allows many branch sizes and their orientation distributions and (4) is valid over a wide frequency range for both deciduous and coniferous vegetation.

The application of this model to walnut and cypress trees leads to the following conclusions:

1. To obtain a match between the calculated and measured values of the backscattering coefficients, the branch size distribution is important. In this paper, the branch size distribution has been discretized into four sizes. We expect that the use of only one or two average branch sizes will not be able to explain multifrequency data. This indicates that the structure of a forest is important.
2. Small branches and leaves generally contribute to the backscattering coefficients at  $X$  band. In particular, cross

polarization at X band is dominated by stems and not leaves in deciduous trees.

3. The contribution of the trunk-soil interaction to the backscattering coefficients depends heavily on soil moisture and soil roughness and it is more important for  $\sigma_{hh}$  than  $\sigma_{vv}$  polarization.

#### VI. APPENDIX A THE ITERATIVE SOLUTION OF THE RADIATIVE TRANSFER EQUATIONS

**I**N this appendix the radiative transfer equations governing the intensity (Stokes' parameters) within the canopy is presented and the procedures for obtaining their iterative solution is outlined. For simplicity only the radiative transfer equation within the crown layer is considered.

The radiative transfer equations describing the Stokes parameters within the crown layer are [34]:

$$\begin{aligned} \cos \theta \frac{d\bar{I}(\theta, \phi, z)}{dz} &= -\bar{K}(\theta) \bar{I}(\theta, \phi, z) + \bar{S}(\theta, \phi, z) \\ -\cos \theta \frac{d\bar{I}(\pi - \theta, \phi, z)}{dz} &= -\bar{K}(\pi - \theta) \bar{I}(\pi - \theta, \phi, z) \\ &\quad + \bar{S}(\pi - \theta, \phi, z) \end{aligned} \quad (A1)$$

where  $\bar{I}(\theta, \phi, z)$  and  $\bar{I}(\pi - \theta, \phi, z)$  are the upward and downward Stokes parameters at location  $z$  with

$$\bar{I}(\theta, \phi, z) = \begin{bmatrix} I_v(\theta, \phi, z) \\ I_h(\theta, \phi, z) \\ I_3(\theta, \phi, z) \\ I_4(\theta, \phi, z) \end{bmatrix} = \begin{bmatrix} \langle |E_v|^2 \rangle \\ \langle |E_h|^2 \rangle \\ 2\text{Re}\langle E_v E_h^* \rangle \\ 2\text{Im}\langle E_v E_h^* \rangle \end{bmatrix}. \quad (A2)$$

$E_v$  and  $E_h$  are the vertically and horizontally polarized components for the electric field vectors. In (A1)  $\bar{S}(\theta, \phi)$  and  $\bar{S}(\pi - \theta, \phi)$  are the upward and downward source functions defined as

$$\begin{aligned} \bar{S}(\theta, \phi, z) &= \int_0^{2\pi} d\phi_t \int_0^{\pi/2} \sin \theta_t d\theta_t \\ &\quad \cdot \sum_{m=1}^{N_1} n_m [\langle \bar{P}_m(\theta, \phi; \theta_t, \phi_t) \rangle \bar{I}(\theta_t, \phi_t, z) \\ &\quad + \langle \bar{P}_m(\theta, \phi; \pi - \theta_t, \phi_t) \rangle \bar{I}(\pi - \theta_t, \phi_t, z)]. \end{aligned} \quad (A3)$$

In (A3)  $\bar{P}_m(\theta, \phi; \theta_t, \phi_t)$  is a  $4 \times 4$  phase matrix of the  $m$ th group of scatterers. This matrix describes the scattering properties from direction  $(\theta_t, \phi_t)$  into direction  $(\theta, \phi)$  [2], [25]. A similar expression can be written for  $\bar{S}(\pi - \theta, \phi)$  by replacing  $\theta$  with  $\pi - \theta$ . Furthermore  $\bar{K}(\theta)$  and  $\bar{K}(\pi - \theta)$

are the upward and downward extinction coefficient matrices. For forest constituents with statistical azimuthal symmetry, the averages of the cross-polarized scattering amplitudes,  $F_{mvh, mhv}$ , vanish and the extinction matrix simplifies to (A4) at the bottom of the page. Where scattering amplitude tensor elements  $F_{mpp}$  (with  $p = v, h$ ) are calculated in the forward direction for an exciting wave in direction  $(\theta, \phi)$ .

An approach to solve (A1) is to diagonalize the extinction matrices and then solve the resulting radiative transfer equations. This can be done using a matrix  $\bar{E}$  constructed from the eigenvectors of the extinction matrix [25]. For the matrix given in (A4) the eigenvector matrix is

$$\bar{E} = \frac{1}{2} \begin{bmatrix} 2 & 0 & 0 & 0 \\ 0 & 2 & 0 & 0 \\ 0 & 0 & 1 & j \\ 0 & 0 & 1 & -j \end{bmatrix}. \quad (A5)$$

Then by multiplying (A1) from the left-hand side by the matrix  $\bar{E}$  we can rearrange (A1) as

$$\begin{aligned} \cos \theta \frac{d\bar{I}(\theta, \phi, z)}{dz} &= -\bar{\kappa}(\theta) \bar{I}(\theta, \phi, z) + \bar{S}(\theta, \phi, z) \\ -\cos \theta \frac{d\bar{I}(\pi - \theta, \phi, z)}{dz} &= -\bar{\kappa}(\pi - \theta) \bar{I}(\pi - \theta, \phi, z) \\ &\quad + \bar{S}(\pi - \theta, \phi, z) \end{aligned} \quad (A6)$$

where

$$\begin{aligned} \bar{I}(\theta, \phi, z) &= \bar{E} \bar{I}(\theta, \phi, z) \\ \bar{\kappa}(\theta) &= \bar{E} \bar{K}(\theta) \bar{E}^{-1} \end{aligned} \quad (A7)$$

and

$$\begin{aligned} \bar{S}(\theta, \phi, z) &= \int_0^{2\pi} d\phi_t \int_0^{\pi/2} \sin \theta_t d\theta_t [\bar{Q}(\theta, \phi; \theta_t, \phi_t) \bar{I}(\theta_t, \phi_t, z) \\ &\quad + \bar{Q}(\theta, \phi; \pi - \theta_t, \phi_t) \bar{I}(\pi - \theta_t, \phi_t, z)] \end{aligned} \quad (A8)$$

$$\bar{Q}(\theta, \phi; \theta_t, \phi_t) = \sum_{m=1}^{N_1} n_m \bar{E} \bar{P}_m(\theta, \phi; \theta_t, \phi_t) \bar{E}^{-1}. \quad (A9)$$

In (A7)  $\bar{\kappa}(\theta)$  is a diagonalized matrix. Its elements are the eigenvalues of the extinction matrix  $\bar{K}$ . For the eigenvector

$$\begin{aligned} \bar{K}(\theta) &= \frac{2\pi}{k} \sum_{m=1}^{N_1} n_m \\ &\quad \begin{bmatrix} 2\text{Im}\langle F_{mvv} \rangle & 0 & 0 & 0 \\ 0 & 2\text{Im}\langle F_{mhh} \rangle & 0 & 0 \\ 0 & 0 & \text{Im}\langle F_{mvv} + F_{mhh} \rangle & \text{Re}\langle F_{mvv} - F_{mhh} \rangle \\ 0 & 0 & \text{Re}\langle F_{mhh} - F_{mvv} \rangle & \text{Im}\langle F_{mvv} + F_{mhh} \rangle \end{bmatrix}. \end{aligned} \quad (A4)$$



matrix given in (A5), see (A10) below. In addition,  $\bar{I}(\theta, \phi, z)$  and  $\bar{Q}(\theta, \phi; \theta_t, \phi_t)$  reduce to

$$\bar{I}(\theta, \phi, z) = \begin{bmatrix} I_v(\theta, \phi, z) \\ I_h(\theta, \phi, z) \\ \frac{1}{2}(I_3(\theta, \phi, z) + jI_4(\theta, \phi, z)) \\ \frac{1}{2}(I_3(\theta, \phi, z) - jI_4(\theta, \phi, z)) \end{bmatrix} \quad (\text{A11})$$

and (A12) at the bottom of the page. It is clear that the first two terms of the Stokes parameter vector (A11) do not change with the transformation.

Equations in (A6) are linear differential equations. For the purpose of iteration they can be written as integral equations in the form [34]

$$\begin{aligned} \bar{I}(\theta, \phi, z) &= e^{-\bar{\kappa}(\theta)(z+H_1)} \sec \theta \bar{I}(\theta, \phi, -H_1) \\ &\quad + \int_{-H_1}^z dz' e^{-\bar{\kappa}(\theta)(z-z')} \sec \theta \bar{S}(\theta, \phi, z') \\ \bar{I}(\pi - \theta, \phi, z) &= e^{\bar{\kappa}(\pi-\theta)z} \sec \theta \bar{I}(\pi - \theta, \phi, 0) \\ &\quad + \int_z^0 dz' e^{\bar{\kappa}(\pi-\theta)(z-z')} \sec \theta \bar{S}(\pi - \theta, \phi, z'). \end{aligned} \quad (\text{A13})$$

The zero-order solution of (A13) is obtained by setting the source function to zero yielding

$$\begin{aligned} \bar{I}^0(\theta, \phi, z) &= e^{-\bar{\kappa}(\theta)(z+H_1)} \sec \theta \bar{I}^0(\theta, \phi, -H_1) \\ \bar{I}^0(\pi - \theta, \phi, z) &= e^{\bar{\kappa}(\pi-\theta)z} \sec \theta \bar{I}^0(\pi - \theta, \phi, 0) \end{aligned} \quad (\text{A14})$$

where  $\bar{I}^0(\theta, \phi, -H_1)$  and  $\bar{I}^0(\pi - \theta, \phi, 0)$  are to be obtained from the boundary conditions. The  $v$ th order solution ( $v > 1$ ) can be written as

$$\begin{aligned} \bar{I}^v(\theta, \phi, z) &= \int_{-H_1}^z e^{-\bar{\kappa}(\theta)(z-z')} \sec \theta \bar{S}^v(\theta, \phi, z') \\ \bar{I}^v(\pi - \theta, \phi, z) &= \int_z^0 e^{\bar{\kappa}(\pi-\theta)(z-z')} \sec \theta \bar{S}^v(\pi - \theta, \phi, z') \end{aligned} \quad (\text{A15})$$

with

$$\begin{aligned} \bar{S}^v(\theta, \phi, z') &= \int_0^{2\pi} d\phi_t \int_0^{\pi/2} \sin \theta_t d\theta_t [\bar{Q}(\theta, \phi; \theta_t, \phi_t) \bar{I}^{v-1}(\theta_t, \phi_t, z') \\ &\quad + \bar{Q}(\theta, \phi; \pi - \theta_t, \phi_t) \bar{I}^{v-1}(\pi - \theta_t, \phi_t, z')]. \end{aligned} \quad (\text{A16})$$

The original Stokes parameters can be recovered from (A14) and (A15) by multiplying them by  $\bar{E}^{-1}$ .

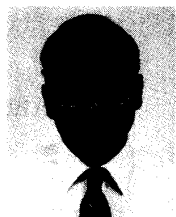
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$$\bar{\kappa}(\theta) = \frac{2\pi}{k} \sum_{m=1}^{N_1} n_m \begin{bmatrix} 2\text{Im}\langle F_{mvv} \rangle & 0 & 0 & 0 \\ 0 & 2\text{Im}\langle F_{mhh} \rangle & 0 & 0 \\ 0 & 0 & \text{Im}\langle F_{mvv} + F_{mhh} \rangle & 0 \\ 0 & 0 & +j\text{Re}\langle F_{mvv} - F_{mhh} \rangle & \text{Im}\langle F_{mvv} + F_{mhh} \rangle \\ & & & -j\text{Re}\langle F_{mvv} - F_{mhh} \rangle \end{bmatrix}. \quad (\text{A10})$$

$$\bar{Q}(\theta, \phi; \theta_s, \phi_s) = \sum_{m=1}^{N_1} n_m \begin{bmatrix} \langle |F_{mvv}|^2 \rangle & \langle |F_{mvh}|^2 \rangle & \langle F_{mvv} F_{mvh}^* \rangle & \langle F_{mvv}^* F_{mvh} \rangle \\ \langle |F_{mhv}|^2 \rangle & \langle |F_{mhh}|^2 \rangle & \langle F_{mhv} F_{mhh}^* \rangle & \langle F_{mhv}^* F_{mhh} \rangle \\ \langle F_{mvv} F_{mhv}^* \rangle & \langle F_{mvh} F_{mhh}^* \rangle & \langle F_{mvv} F_{mhh}^* \rangle & \langle F_{mvh} F_{mhh}^* \rangle \\ \langle F_{mhv}^* F_{mvv} \rangle & \langle F_{mhh}^* F_{mvh} \rangle & \langle F_{mhv}^* F_{mhh} \rangle & \langle F_{mhh}^* F_{mhv} \rangle \end{bmatrix} \quad (\text{A12})$$

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