

BASICS

• DOT PRODUCT

$$\bar{A} \cdot \bar{B} = |\bar{A}| |\bar{B}| \cos \theta$$

$$(\text{SCALAR}) = A_x B_x + A_y B_y + A_z B_z$$

• CROSS PRODUCT

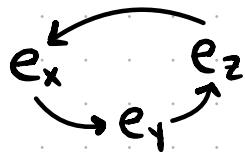
$$\bar{A} \times \bar{B} = |\bar{A}| |\bar{B}| \sin \theta =$$

(VECTOR)

\hat{e}_x	\hat{e}_y	\hat{e}_z
A_x	A_y	A_z
B_x	B_y	B_z

CARTESIAN COORDINATE SYSTEM

$$(x, y, z)$$



DIFFERENTIAL LENGTH:

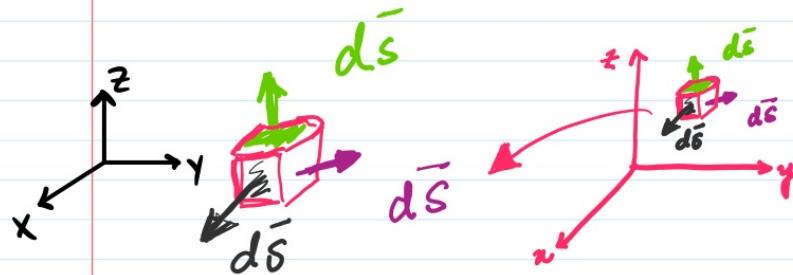
$$d\bar{l} = dx \hat{e}_x + dy \hat{e}_y + dz \hat{e}_z$$

DISTANCE BETWEEN P₁ AND P₂:

$$d = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$$

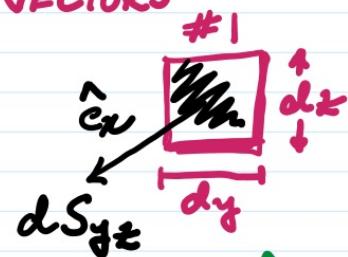
Surfaces and Volume in Cartesian Coordinate System

Tuesday, June 6, 2023 4:51 PM

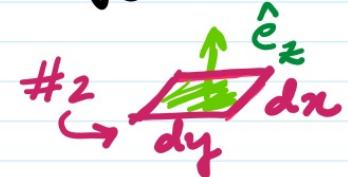


DIFFERENTIAL AREA VECTORS

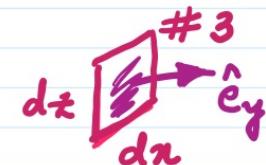
#1 $d\bar{s}_x = dy dz \hat{e}_x$



#2 $d\bar{s}_y = dx dz \hat{e}_y$



#3 $d\bar{s}_z = dx dy \hat{e}_z$



DIFFERENTIAL VOLUME

(SCALAR) $dV = dx dy dz$

• There is NO VECTOR FOR VOLUME

CYLINDRICAL COORDINATE SYSTEM (ρ, ϕ, z)

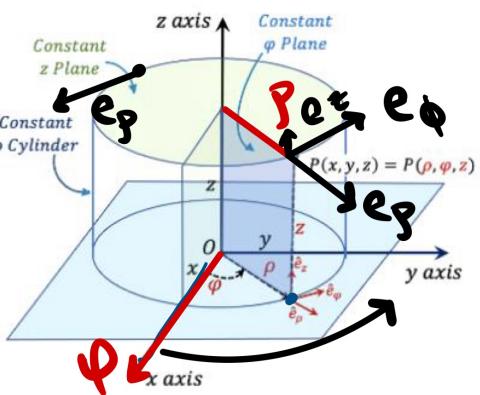


Figure 2: Cylindrical Coordinate System

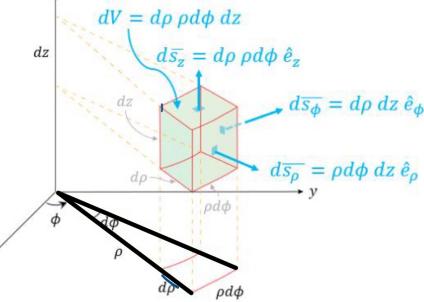
$$\begin{aligned} e_\rho \times e_\rho &= 0 \\ e_\rho \cdot e_\rho &= 1 \end{aligned}$$

LENGTH VECTORS:

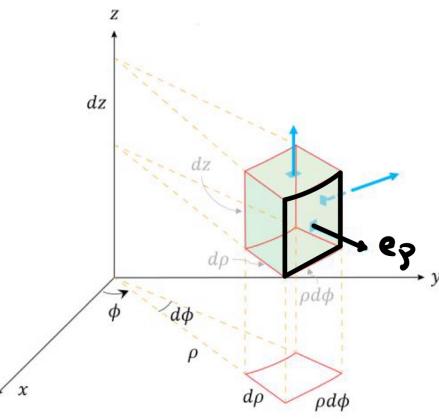
$$d\bar{l}_z = d_z \hat{e}_z$$

$$d\bar{l}_\rho = d\rho \hat{e}_\rho$$

$$d\bar{l}_\phi = \rho d\phi \hat{e}_\phi$$



$$d\bar{l} = d\rho \hat{e}_\rho + \rho d\phi \hat{e}_\phi + d_z \hat{e}_z$$



AREA VECTORS:

$$d\bar{s}_\rho = \rho d\phi d_z \hat{e}_\rho$$

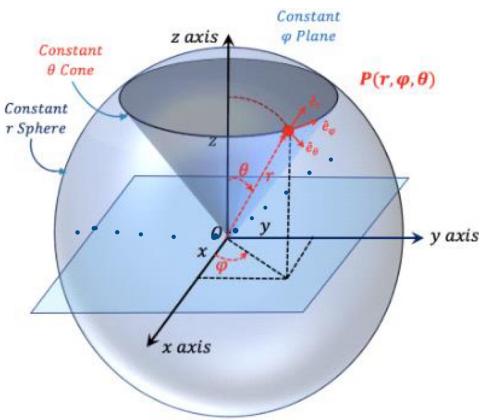
$$d\bar{s}_z = \rho d\phi d_\rho \hat{e}_z$$

$$d\bar{s}_\phi = d_z d_\rho \hat{e}_\phi$$

DIFFERENTIAL VOLUME:

$$dV = d\rho \rho d\phi dz$$

SPHERICAL COORDINATE SYSTEM (r, θ, ϕ)



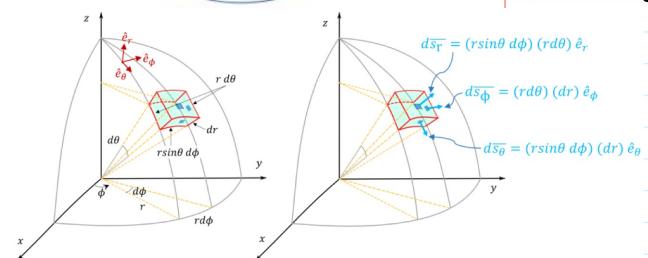
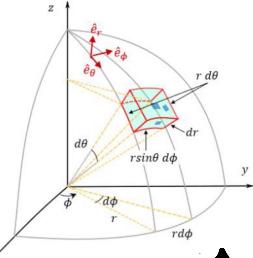
DIFFERENTIAL LENGTHS IN SPHERICAL COORDINATES:

$$d\bar{l}_r = dr \hat{e}_r$$

$$d\bar{l}_\theta = r d\theta \hat{e}_\theta$$

$$d\bar{l}_\phi = r d\phi \sin\theta \hat{e}_\phi$$

$$d\bar{l} = dr \hat{e}_r + r d\theta \hat{e}_\theta + r d\phi \sin\theta \hat{e}_\phi$$

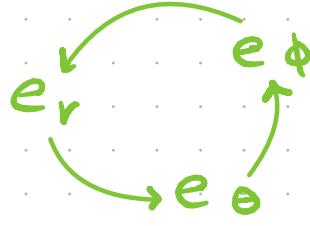


$$d\bar{s}_r = r^2 \sin\theta d\theta d\phi \hat{e}_r$$

$$d\bar{s}_\phi = r d\theta d\phi \hat{e}_\phi$$

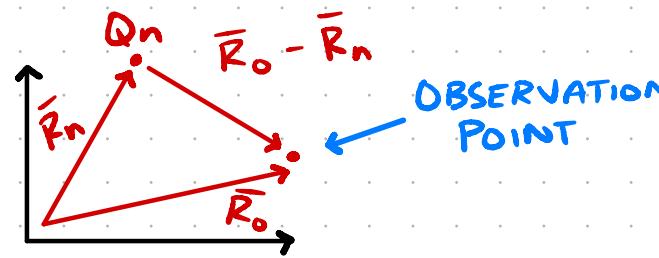
$$d\bar{s}_\theta = r \sin\theta d\phi dr \hat{e}_\theta$$

DIFFERENTIAL VOLUME (SCALAR) $dV = r^2 \sin\theta d\theta d\phi dr$



OPERATORS:

OPERATOR	NAME	INPUT	OUTPUT
$\bar{\nabla} \Psi$	GRADIENT	SCALAR	VECTOR
$\bar{\nabla} \cdot \bar{A}$	DIVERGENCE	VECTOR	SCALAR
$\bar{\nabla} \times \bar{A}$	CURL	VECTOR	VECTOR
$\bar{\nabla}^2 \Psi$	LAPLACIAN	SCALAR	SCALAR



VECTOR ADDITION

$$\bar{R}_1 + \bar{R}_{12} - \bar{R}_2 = 0$$

$$= \bar{R}_{12} = \bar{R}_2 - \bar{R}_1$$

↑
OBSERVATION

GRADIENT : GIVES MAX RATE OF CHANGE AND POINTS IN THE DIRECTION OF MAX INCREASE

Table 2: The gradient $\bar{\nabla} \Psi$ in different coordinate systems

Cartesian Coordinates	Cylindrical Coordinates	Spherical Coordinates
$\Psi(x, y, z)$	$\Psi(\rho, \varphi, z)$	$\Psi(r, \varphi, \theta)$

$$\bar{\nabla} \Psi = e_x \frac{\partial \Psi}{\partial x} + e_y \frac{\partial \Psi}{\partial y} + e_z \frac{\partial \Psi}{\partial z}$$

$$\bar{\nabla} \Psi = e_\rho \frac{\partial \Psi}{\partial \rho} + e_\varphi \frac{1}{\rho} \frac{\partial \Psi}{\partial \varphi} + e_z \frac{\partial \Psi}{\partial z}$$

$$\bar{\nabla} \Psi = e_r \frac{\partial \Psi}{\partial r} + e_\theta \frac{1}{r} \frac{\partial \Psi}{\partial \theta} + e_\varphi \frac{1}{r \sin \theta} \frac{\partial \Psi}{\partial \varphi}$$

DIVERGENCE: $\bar{\nabla} \cdot \bar{A} > 0 \rightarrow$ SOURCE $\bar{\nabla} \cdot \bar{A} = 0 \rightarrow$ PARALLEL FIELD LINES
 $\bar{\nabla} \cdot \bar{A} < 0 \rightarrow$ SINK

Table 3: $\bar{\nabla} \cdot \bar{A}$

Cartesian Coordinates	Cylindrical Coordinates	Spherical Coordinates
$\bar{A}(x, y, z) = e_x A_x + e_y A_y + e_z A_z$	$\bar{A}(\rho, \varphi, z) = e_\rho A_\rho + e_\varphi A_\varphi + e_z A_z$	$\bar{A}(r, \varphi, \theta) = e_r A_r + e_\theta A_\theta + e_\varphi A_\varphi$

$$\frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$$

$$\frac{1}{\rho} \frac{\partial (A_\rho)}{\partial \rho} + \frac{1}{\rho} \frac{\partial A_\varphi}{\partial \varphi} + \frac{\partial A_z}{\partial z}$$

$$\frac{1}{r^2} \frac{\partial (r^2 A_r)}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial (A_\theta \sin \theta)}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial A_\varphi}{\partial \varphi}$$

CURL: INDICATES WHETHER A VECTOR FIELD HAS MICROSCOPIC ROTATION.

Table 4: $\bar{\nabla} \times \bar{A}$

Cartesian Coordinates	Cylindrical Coordinates	Spherical Coordinates
$\bar{A}(x, y, z) = e_x A_x + e_y A_y + e_z A_z$	$\bar{A}(\rho, \varphi, z) = e_\rho A_\rho + e_\varphi A_\varphi + e_z A_z$	$\bar{A}(r, \varphi, \theta) = e_r A_r + e_\theta A_\theta + e_\varphi A_\varphi$

$$\begin{aligned} & (\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z}) e_x \\ & + (\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x}) e_y \\ & + (\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y}) e_z \end{aligned}$$

$$\begin{aligned} & (\frac{1}{\rho} \frac{\partial A_z}{\partial \varphi} - \frac{\partial A_\varphi}{\partial z}) e_\rho \\ & + (\frac{\partial A_\rho}{\partial z} - \frac{\partial A_z}{\partial \rho}) e_\varphi \\ & + \frac{1}{\rho} (\frac{\partial (A_\rho)}{\partial \varphi} - \frac{\partial A_\varphi}{\partial \rho}) e_z \end{aligned}$$

$$\begin{aligned} & \frac{1}{r \sin \theta} (\frac{\partial}{\partial \theta} (A_\varphi \sin \theta) - \frac{\partial A_\theta}{\partial \varphi}) e_r \\ & + \frac{1}{r} (\frac{1}{\sin \theta} \frac{\partial A_r}{\partial \varphi} - \frac{\partial}{\partial r} (r A_\varphi)) e_\theta \\ & + \frac{1}{r} (\frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta}) e_\varphi \end{aligned}$$

CALCULUS.

$$\frac{d}{dx} (\sin x) = \cos x$$

$$\int \sin x = -\cos x$$

$$\frac{d}{dx} \cos x = -\sin x$$

$$\int \cos x = \sin x$$

BIOT-SAVART'S LAW (FINDING \bar{H})

\bar{B} : MAGNETIC FLUX DENSITY

\bar{H} : MAGNETIC FIELD INTENSITY

$$\text{LINE CURRENT: } \bar{H} = \int_L \frac{Id\bar{\lambda} \times \bar{R}}{4\pi |\bar{R}|^3} \left(\frac{A}{m} \right)$$

$$\text{SURFACE CURRENT: } \bar{H} = \iint_S \frac{\bar{J}_s dS \times \bar{R}}{4\pi |\bar{R}|^3} \left(\frac{A}{m} \right) \quad J_s: \text{SURFACE CURRENT DENSITY}$$

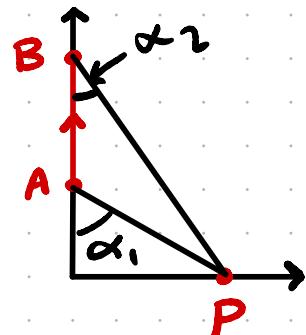
$$\text{VOLUME CURRENT: } \bar{H} = \iiint_V \frac{\bar{J}_v dv \times \bar{R}}{4\pi |\bar{R}|^3} \left(\frac{A}{m} \right) \quad J_v: \text{VOLUME CURRENT DENSITY}$$

MAGNETIC FIELD INTENSITY DUE TO A FINITE CURRENT CARRYING CONDUCTOR.

$$\bar{H} = \frac{I}{4\pi p} [\cos\alpha_2 - \cos\alpha_1] \hat{e}_\phi$$

INFINITE WIRE: p : DISTANCE FROM WIRE

$$\bar{H} = \frac{I}{2\pi p} \hat{e}_\phi \quad \hat{e}_\phi: \text{RIGHT HAND RULE.}$$



MAGNETIC FLUX DENSITY

$\bar{B} = \mu \bar{H}$ ← MAGNETIC FIELD INTENSITY (T).

PERMEABILITY: $\mu = \mu_0 \mu_r$

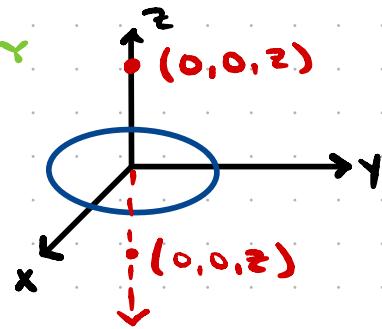
$$\mu_0 = 4\pi \times 10^{-7} (\text{H/m})$$

MAGNETIC FLUX DENSITY DUE TO A LOOP.

$$B(z) = \frac{1}{2} \frac{\mu I a^2}{(a^2 + z^2)^{3/2}} \hat{e}_z$$

AT THE CENTER.

$$B(z=0) = \frac{\mu I}{2a} \hat{e}_z$$



AMPERE'S LAW (1st MAXWELLS EQUATION)

$$\oint \bar{H} \cdot d\bar{l} = I_{enc} \rightarrow \text{INTERGAL FORM}$$

$$\nabla \times \bar{H} = J \rightarrow \text{DIFFERENTIAL FORM}$$

THE LINE INTERGAL OF \bar{H} AROUND A CLOSED PATH IS THE SAME AS THE TOTAL CURRENT ENCLOSED BY THE PATH.

2nd MAXWELLS EQUATION

MAGNETIC MONOPOLES DO NOT EXIST

FIELD LINES GOING IN
= FIELD LINES GOING OUT.

$$\iint \bar{B} \cdot d\bar{s} = \iiint_v (\nabla \cdot \bar{B}) dv = 0$$

$$\rightarrow \nabla \cdot \bar{B} = 0 \quad \begin{matrix} \text{NO SOURCE} \\ \text{OR SINK.} \end{matrix}$$

FORCE ON A CURRENT CARRYING CONDUCTOR.

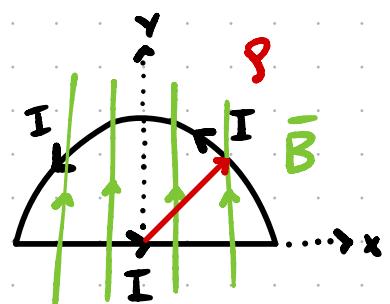
$$\text{EQUATION: } \bar{F}_m = \int_L I d\bar{l} \times \bar{B} \text{ (N)}$$

STRAIGHT CONDUCTOR SECTION:

$$\text{ALONG X AXIS} \rightarrow 2IB_0 \rho \hat{e}_z \text{ (N)}$$

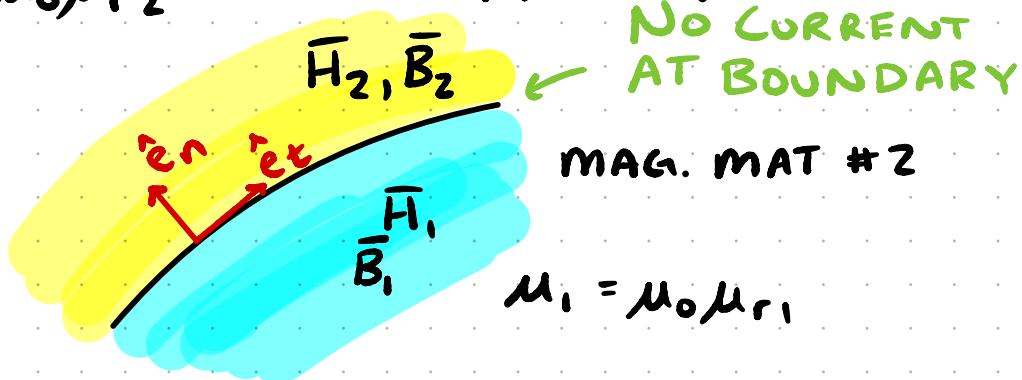
CURVED CONDUCTOR:

$$\bar{F} = -2I\rho B_0 \hat{e}_z \text{ (N)}$$



MAGNETOSTATICS BOUNDARY CONDITION

$$\mu_2 = \mu_0 \mu_{r2}$$



1 NORMAL Component IS CONTINUOUS

$$\bar{B}_{1n} = \bar{B}_{2n} \rightarrow \mu_1 \bar{H}_{1n} = \mu_2 \bar{H}_{2n}$$

2 TANGENTIAL IS CONTINUOUS.

$$\bar{H}_{1t} = \bar{H}_{2t}$$

PERFECT CONDUCTOR. MATERIAL 1 IS CONDUCTOR

$$\bar{B}_{2n} = 0 = \bar{H}_{2t}$$

$$\bar{B}_{1n} = 0, \bar{H}_{1t} = J_s \leftarrow \begin{matrix} \text{SURFACE} \\ \text{CURRENT} \\ \text{DENSITY} \end{matrix}$$

OVERALL:

$$\bar{B}_{1n} = \bar{B}_{2n} \rightarrow \mu_1 \bar{H}_{1n} = \mu_2 \bar{H}_{2n} \text{ (NORMAL)}$$

$$(\bar{H}_1 - \bar{H}_2) \times \hat{e}_n = \bar{J} \text{ (TANGENTIAL)}$$

$$\text{IF } \bar{J} = 0 \rightarrow \bar{H}_{1t} = \bar{H}_{2t}$$

INDUCTANCE

MAGNETIC FLUX THRU A LOOP.

$$\Psi_{\text{MAG}} = \iint \bar{B} \cdot d\bar{s}$$

INDUCTANCE OF A LOOP

$$L = \frac{\Psi_{\text{MAG}}}{I}$$

FOR N LOOPS: $L = \frac{N \Psi_{\text{MAG}}}{I}$

INDUCTANCE OF A LONG SOLENOID: $l \gg a$ [a: RADIUS]

$$L = \frac{\mu N^2 S}{l} \quad (\text{H}) \quad \begin{matrix} N: \text{TURNS} \\ l: \text{LENGTH.} \end{matrix} \quad \begin{matrix} S: \text{AREA} \end{matrix}$$

$$S = \pi a^2 \quad N = nl$$

TIME VARYING FIELDS:

FARADAY'S LAW:

$$V_{\text{emf}} = -N \frac{d}{dt} \Psi_{\text{MAG}} \leftrightarrow V_{\text{emf}} = -N \frac{d}{dt} \left[\iint_S \bar{B} \cdot d\bar{s} \right]$$

STATIONARY LOOP IN TIME VARYING \bar{B} FIELD.
(TRANSFORMER EMF)

$$V_{\text{emf}}^{\text{tr}} = -N \iint \frac{\partial}{\partial t} \bar{B} \cdot d\bar{s}$$

MOTIONAL EMF $\overset{\text{B}}{\curvearrowleft}$ REFERENCE.

$$V_{\text{emf}}^m = \oint_C (\bar{v} \times \bar{B}) \cdot d\bar{l}$$

MAXWELL'S EQUATIONS

GAUSS LAW

$$\bar{\nabla} \cdot \bar{D} = q_0 \quad \text{OR} \quad \iint_S \bar{D} \cdot d\bar{s} = \iiint_V q_v dv$$

FARADAY'S LAW

$$\bar{\nabla} \times \bar{E} = - \frac{\partial \bar{B}}{\partial t} \quad \text{OR} \quad \oint \bar{E} \cdot d\bar{l} = - \frac{\partial}{\partial t} \iint \bar{B} \cdot d\bar{s}$$

CHANGE IN MAGNETIC FIELD WILL GIVE RISE TO INDUCED CURRENT.

NON-EXISTENCE OF MAGNETIC MONOPOLES

$$\bar{\nabla} \cdot \bar{B} = 0 \quad \text{OR} \quad \oint \bar{B} \cdot d\bar{s} = 0$$

DISPLACEMENT CURRENT.

AMPERE'S LAW

$$\bar{\nabla} \times \bar{H} = J + \frac{\partial \bar{D}}{\partial t} \quad \text{OR} \quad \oint \bar{H} \cdot d\bar{l} = I + \iint_S \frac{\partial \bar{D}}{\partial t} \cdot d\bar{s}$$

WAVES

PROPAGATING IN $+x$ DIRECTION

$$y(x,t) = A \cos(\omega t - \beta x + \phi)$$

A : Amplitude

B : PHASE CONSTANT / ANGULAR WAVENUMBER.

w : ANGULAR FREQUENCY

$$\omega = 2\pi f = \frac{2\pi}{T} \left(\frac{\text{rad}}{\text{s}} \right)$$

$$\beta = \frac{2\pi}{\lambda} \left(\frac{\text{rad}}{\text{m}} \right)$$

v_p : PHASE VELOCITY

λ : WAVELENGTH

$$v_p = \frac{\omega}{\beta} = \frac{2\pi f}{\frac{2\pi}{\lambda}} = f\lambda \left(\frac{\text{m}}{\text{s}} \right)$$

$$\lambda = \frac{v_p}{f} = \frac{2\pi}{\beta} \text{ (m)}$$

PHASOR

$$\tilde{Y} = A e^{(-j\beta x + j\phi_0)} \cdot e^{j\omega t}$$

COMPLEX PERMITTIVITY

$$\tilde{D} = (\underbrace{\epsilon' - j\epsilon''}_{\text{COMPLEX PERMITTIVITY}}) \tilde{E} = \overbrace{\epsilon_0 \epsilon_r}^{\text{PERMITTIVITY}} - j \frac{\sigma}{\omega} \tilde{E}$$

CONDUCTIVITY

IN MOST MATERIALS:

$$\epsilon' = \epsilon = \epsilon_0 \epsilon_r \quad [\text{REAL VALUED PERMITTIVITY}]$$

$$\epsilon'' = \frac{\sigma}{\omega} \quad [\text{HIGHER ORDER TERMS}]$$

σ : CONDUCTIVITY

$$\text{LOSS TANGENT} - \tan \delta = \frac{\epsilon''}{\epsilon'} = \frac{\sigma}{\omega \epsilon}$$

IN AN UNBOUNDED HOMOGENEOUS MEDIUM

$$\bar{\nabla}^2 \tilde{E} - \gamma^2 \tilde{E} = 0 \quad \gamma = \sqrt{-\omega^2 \mu \epsilon_c}$$

$$\bar{\nabla}^2 \tilde{H} - \gamma^2 \tilde{H} = 0 \quad \text{IN FORM } \alpha + j\beta$$

α : ATTENUATION CONSTANT $(\frac{Np}{m})$

$$\alpha = \omega \sqrt{\frac{\mu \epsilon}{2} \left[\sqrt{1 + \left[\frac{\sigma}{\omega \epsilon} \right]^2} - 1 \right]}$$

REAL PART

$$\alpha^2 - \beta^2 = -\omega^2 \mu \epsilon'$$

β : PHASE CONSTANT (rad/m)

IMAGINARY PART

$$\beta = \omega \sqrt{\frac{\mu \epsilon}{2} \left[\sqrt{1 + \left[\frac{\sigma}{\omega \epsilon} \right]^2} + 1 \right]}$$

$$2\alpha\beta = \omega^2 \mu \epsilon''$$

LOSSY WAVE

$$\bar{E}(z,t) = E_0^+ e^{-\alpha z} \cos(\omega t - \beta z + \phi_0) \hat{e}_E (\text{V/m})$$

E_0^+ : INITIAL AMPLITUDE (V/m)

α : ATTENUATION CONSTANT (Np/m)

ω : ANGULAR FREQUENCY = $2\pi f$

β : PHASE CONSTANT (rad/m)

$-\beta x$: DIRECTION OF PROPAGATION.

γ : INTRINSIC IMPEDANCE OF MATERIAL (Ω)

COMPLEX NUMBER

$$n = |\gamma| \angle \theta_\gamma$$

↓

$$\tan 2\theta_\gamma = \frac{\sigma}{\omega \epsilon}$$

MAGNITUDE

$$\eta: E_0^+ / H_0^+$$

$$|\gamma| = \sqrt{\frac{\mu/\epsilon}{1 + (\frac{\sigma}{\omega \epsilon})^2}}^{1/4}$$

IMAGINARY PART

$$\theta_\gamma = \frac{\tan^{-1}(\frac{\sigma}{\omega \epsilon})}{2}$$

IN PHASOR FORM

$$\tilde{E} = E_0^+ e^{-\alpha z} e^{j[-\beta z + \phi_0]} \hat{e}_E (\text{V/m})$$

WHEN SOLVING FOR ϵ' AND ϵ'' .

MAGNITUDE $|\gamma| = \sqrt{\frac{\mu/\epsilon}{1 + (\frac{\epsilon''}{\epsilon'})^2}}^{1/4}$

TO FIND ϵ' AND ϵ''

IMAGINARY PART $\theta_\gamma = \frac{\tan^{-1}(\frac{\epsilon''}{\epsilon'})}{2}$

REAL PART

$$\alpha^2 - \beta^2 = -\omega^2 \mu \epsilon'$$

IMAGINARY PART

$$2\alpha\beta = \omega^2 \mu \epsilon''$$

LOSSLESS PERFECT DIELECTRIC [NON-CONDUCTING]

$\sigma = 0$ CONDUCTIVITY

$\alpha = 0$ AND $\beta = \omega\sqrt{\mu\epsilon}$ (rad/m) PHASE CONSTANT

$\eta = \sqrt{\frac{\mu}{\epsilon}}$ [η IS A REAL NUMBER FOR LOSSLESS MATERIALS]

PHASE VELOCITY $v_p = \frac{\omega}{\beta} = \frac{1}{\sqrt{\mu\epsilon}} = 3 \times 10^8 \text{ m/s}$

IN FREE SPACE

$$\epsilon = \epsilon_0 = 8.854 \times 10^{-12} \text{ F/m} \quad \mu = \mu_0 = 4\pi \times 10^{-7} \text{ H/m}$$

$$\eta_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 120\pi (\text{n})$$

FOR ANY LOSSLESS DIELECTRIC.

$$\eta = \sqrt{\frac{\mu_r \mu_0}{\epsilon_r \epsilon_0}} = 120\pi \sqrt{\frac{\mu_r}{\epsilon_r}} (\text{n}) \quad v_p = \frac{c}{\sqrt{\mu_r \epsilon_r}} (\text{m/s})$$

WAVELENGTH

$$\lambda = \frac{c}{f\sqrt{\mu_r \epsilon_r}}$$

IN FREE SPACE

$$\lambda_0 = \frac{c}{f}$$

PHASE CONSTANT

$$\beta = \omega\sqrt{\mu\epsilon} = \frac{2\pi}{\lambda}$$

[IN LOSSLESS MATERIALS]

RELATIONSHIP BETWEEN \vec{E} AND \vec{H} .

$$\eta = \frac{E_0^+}{H_0^+} \quad (\hat{\vec{e}}_E \times \hat{\vec{e}}_H) = \hat{\vec{e}}_K$$

RADIAN TO DEGREE

$$\text{RADIAN} \times \frac{180}{\pi}$$