


Lecture # 14

# ECEN 438/738 Power Electronics

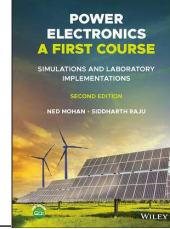
Spring 2025 Semester



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## ECEN 438/738 Power Electronics



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## Chapter 7

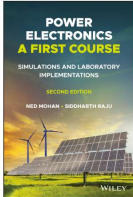
### Magnetic Circuit Concepts

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**POWER ELECTRONICS, A First Course, 2nd Edition**  
WILEY  
by Ned Mohan, Siddharth Bala



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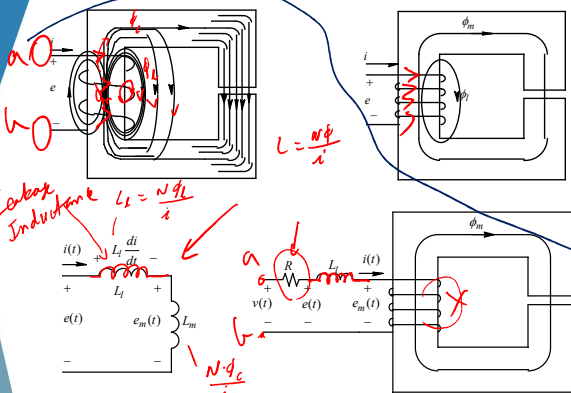
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## Magnetizing Inductance & Leakage



$$e(t) = L_m \frac{di}{dt} + L_\ell \frac{di}{dt}$$

$$\Phi = \frac{L I}{R}$$

Where  $R$  is the resistance of the coil &  $R_c$  is the core loss representation for hysteresis and eddy current losses

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## Transformers – Basics

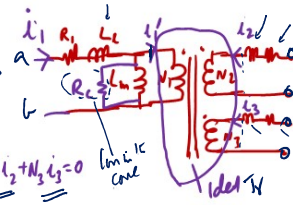
Faraday's Law - a rate of change in flux results in induced voltage

$$\begin{aligned} e_1 &= N_1 \frac{d\phi_m}{dt} \\ e_2 &= N_2 \frac{d\phi_m}{dt} \\ e_3 &= N_3 \frac{d\phi_m}{dt} \end{aligned}$$

Therefore:  $\frac{d\phi_m}{dt} = \frac{e_1}{N_1} = \frac{e_2}{N_2} = \frac{e_3}{N_3} \Rightarrow \frac{e_1}{e_2} = \frac{N_1}{N_2}$

$$\Rightarrow \phi_m = \frac{1}{N_1} \int e_1 dt = \frac{1}{N_2} \int e_2 dt = \frac{1}{N_3} \int e_3 dt$$

The equivalent circuit considering the Leakage flux is:



Transformer with three windings  
Understand the dot convention

In many instances we neglect leakage inductance  
- assuming the coil is tightly wound - i.e. tightly coupled - hence no leakage

Choosing a core with high  $\mu_r$  will result in high  $L_m$  therefore can be neglected.

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## Transformers – Continued

A three-winding transformer with  $N_1=10$  turns,  $N_2=5$  turns, and  $N_3=5$  turns uses a magnetic core that has the following properties:  $A_m=0.639$  cm<sup>2</sup>, the magnetic path length  $l_m = 5.12$  cm, and the relative permeability of the material  $\mu_r=5000$

A square-wave voltage of  $\pm 30$ V amplitude at a frequency of 100kHz is applied to winding 1. Windings 2 and 3 are open. Ignore the leakage inductance. Calculate and draw the magnetizing current waveforms and the voltages induced in the open windings 2 and 3

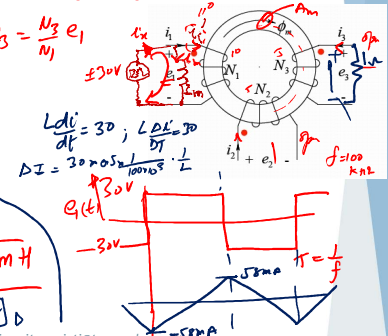
$$\frac{e_1}{N_1} = \frac{e_2}{N_2} = \frac{e_3}{N_3} ; e_2 = \frac{N_2}{N_1} e_1 ; e_3 = \frac{N_3}{N_1} e_1$$

$$e_2 = \pm 15V ; e_3 = \pm 15V$$

$$L_m = \frac{N^2}{R_e} = \frac{N^2}{\left( \frac{l}{\mu_r \mu_0 A} \right)}$$

$$= \frac{100}{\left( \frac{5.12 \times 10^{-2}}{5000 \times 4\pi \times 10^{-7} \times 0.639 \times 10^{-4}} \right)} = 1.29 \text{ mH}$$

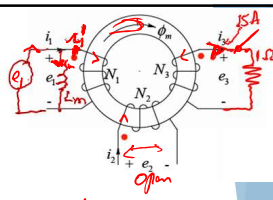
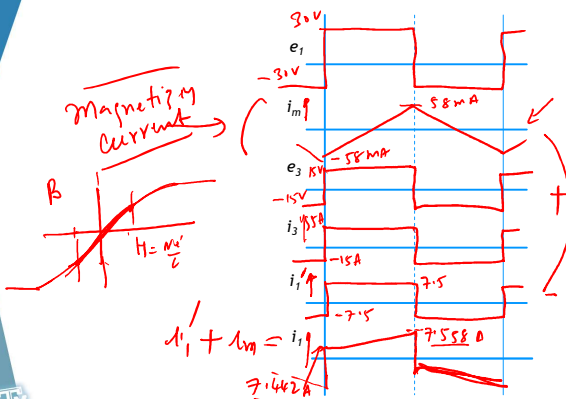
$$\Delta I = 116 \mu A$$



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## Transformers – Continued

Now a 1-Ω resistance is connected to  $e_3$



$$N_1 i_1' + N_3 (i_3) = 0$$

$$N_1 i_1' = -N_3 i_3$$

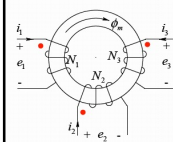
$$i_1' = \frac{N_3}{N_1} i_3$$

$$= \frac{5}{10} (15A)$$

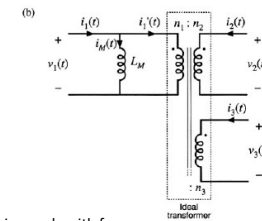
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## Transformers – Continued

### TRANSFORMERS



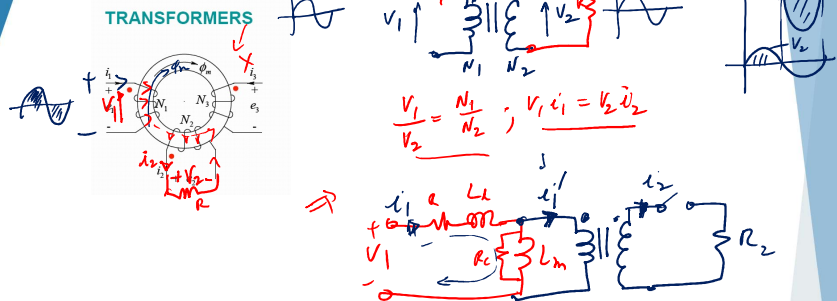
Approximate  
Equivalent Circuit



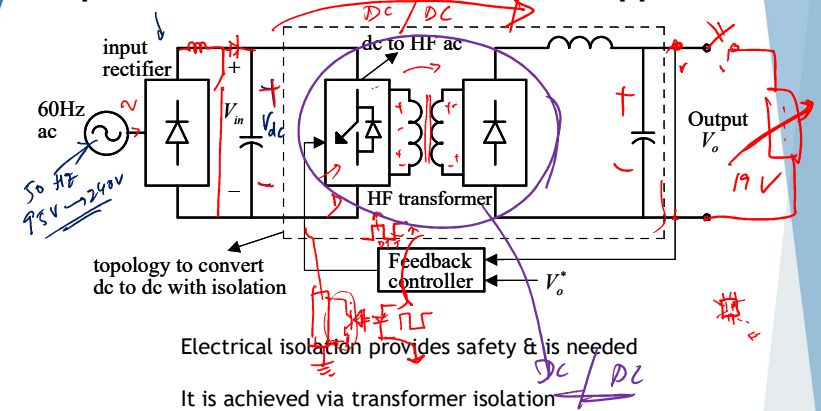
- Transformer provides isolation, its size & weight vary inversely with frequency
- When a large step-up or step-down conversion ratio is required, the use of a transformer can allow better converter optimization.
- By proper choice of transformer turns ratio, the voltage or current stresses imposed on the transistors and diodes can be minimized, leading to improved efficiency and lower cost
- Multiple dc outputs can also be obtained in an inexpensive manner, by adding multiple secondary windings and converter secondary side circuits.

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## Transformers – Basics - Dot Convention

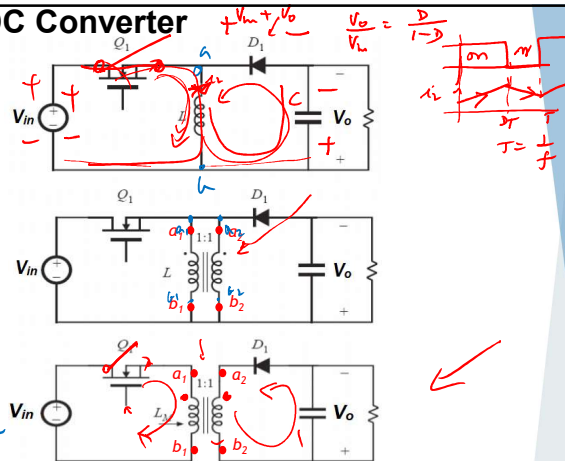


## Chapter # 8 Switch-Mode DC Power Supplies

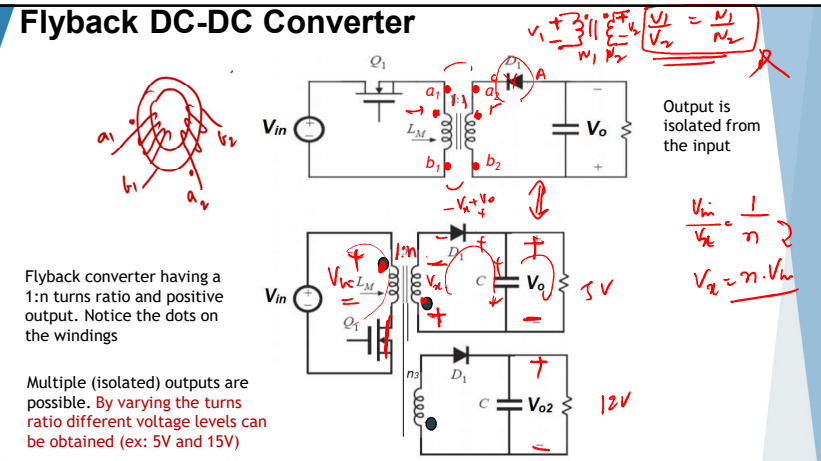


## Flyback DC-DC Converter

### Buck Boost Converter



## Flyback DC-DC Converter



### Flyback DC-DC Converter

Another representation of a buck-boost converter evolving into a flyback converter

(a) (b) (c)

$\frac{V_o}{V_{in}} = f(D, R, f)$

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### Flyback DC-DC Converter

Flyback converter

Flyback converter with simplified transformer model

Transformer

TRANSFORMERS

(a) (b)

$V_1 = V_{in}$   
 $V_2 = \frac{N_2}{N_1} V_1$   
 $V_2 = V_o$   
 $V_{sw} = V_{in} + V_o \frac{N_1}{N_2}$

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### Flyback DC-DC Converter - Analysis

Switch  $Q_1$  is Closed for  $DT$

$\frac{V_1}{V_2} = \frac{N_1}{N_2} \Rightarrow V_2 = V_1 \frac{N_2}{N_1}$

$V_d = V_{in} \frac{N_2}{N_1} + V_o$

$v_1 = V_{in}$   
 $v_2 = -V_o$

$v_1 = V_{in} = L_m \frac{di_{Lm}}{dt}$   
 $\frac{di_{Lm}}{dt} = \frac{V_{in}}{L_m}$   
 $L_m = \frac{V_{in} \cdot DT}{\Delta i_{Lm}}$

Diode voltage rating is:  $V_d = V_{in} \frac{N_2}{N_1} + V_o$

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### Flyback DC-DC Converter - Analysis

Switch  $Q_1$  is Open for  $(1-D)T$

$\frac{V_1}{V_2} = \frac{N_1}{N_2}$

$v_1 = -V_o \frac{N_1}{N_2}$   
 $v_2 = -V_o$

$v_{sw} = V_{in} + V_o \frac{N_1}{N_2}$

Volt-sec balance across the inductor  $L_m$  we have

$V_{in} \cdot DT + \left(-V_o \frac{N_2}{N_1}\right) \cdot (1-D)T = 0$

$\frac{V_o}{V_{in}} = \frac{D}{1-D} \cdot \frac{N_2}{N_1}$

Voltage rating of the switch is:  $V_{sw} = V_{in} + V_o \frac{N_1}{N_2}$

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