# ECEN 325 - 512

**Operational Amplifiers - Part 3** 

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# **Measurements**

# **Lossy Integrator**

# 2a. Low Frequency Gain



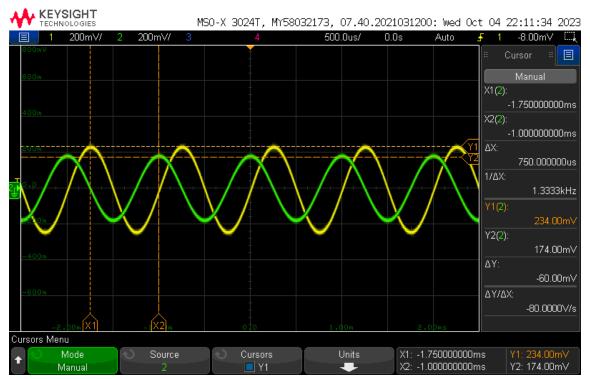
#### 2b. 3-dB Frequency



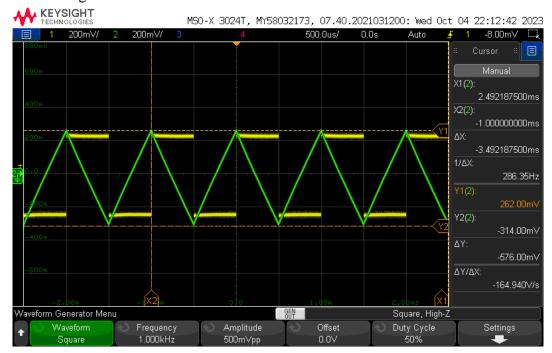
# 2c. Magnitude and Phase of Transfer Function at 1kHz



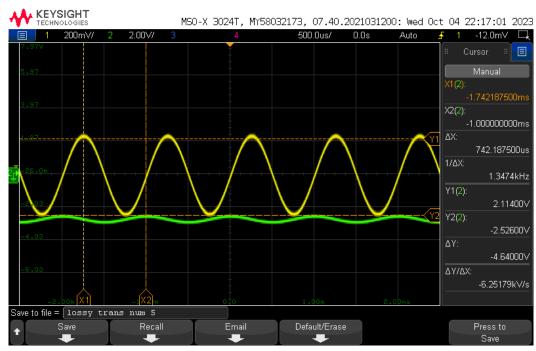
#### 3. Time-domain waveforms



4. Square wave signal time-domain waveform



5. Remove the resistor  $R_2$  and observe what happens to the output signal. Comment on the result.



When  $R_2$  is removed, you can see the capacitor charging and discharging with respect to time.

The sine wave is much smaller than the input signal, it only becomes an integrator circuit, since there is no resistor to alter the circuit.

# **Pseudo Differentiator**

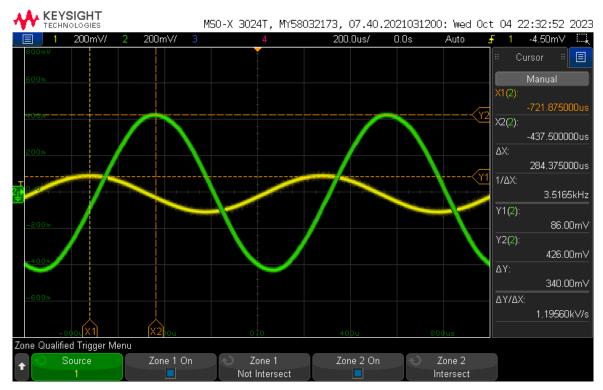
# 2a. Low frequency gain



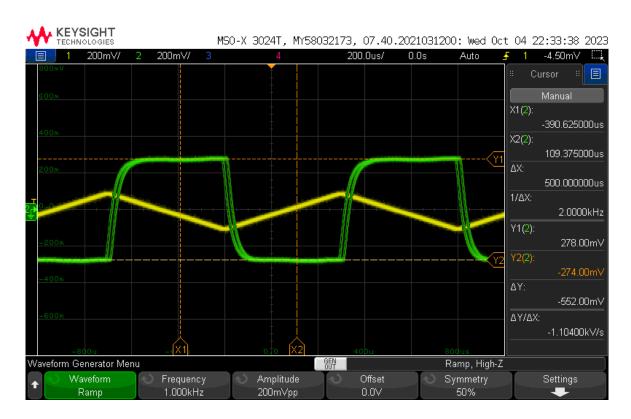
# 2b. 3-dB frequency



# 3. Sine wave signal time-domain waveform



# 4. Triangular wave signal time-domain waveform



# **Finite GBW Limitations**

# 2. Magnitude and phase Bode Plots



#### 3. Low Frequency Gain



# 4a. Parts repeated for 57 gain





# 4b. Parts repeated for 83 gain





# **Slew Rate Limitations**

# 2a. Low-frequency gain



# 2b. 3-dB frequency gain

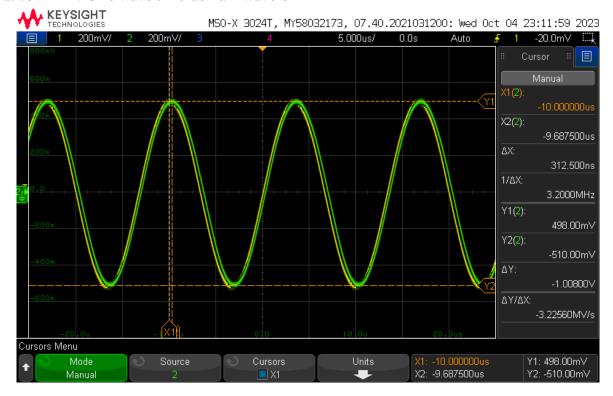


#### 2c. Magnitude of Transfer Function

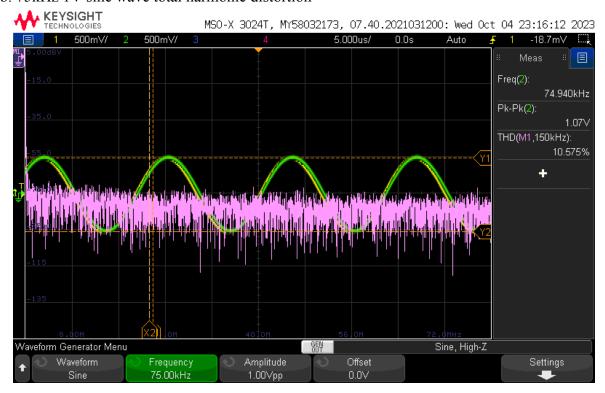




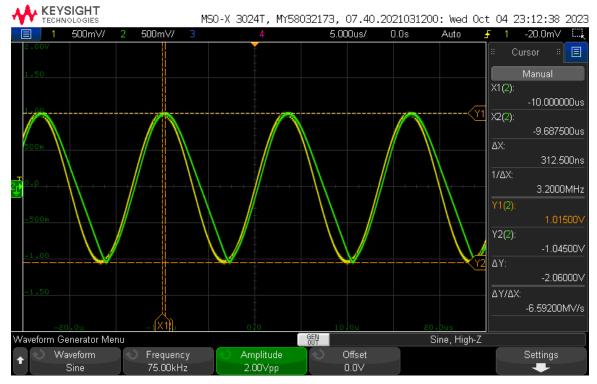
#### 3a. 75kHz 1V sine wave time-domain waveform



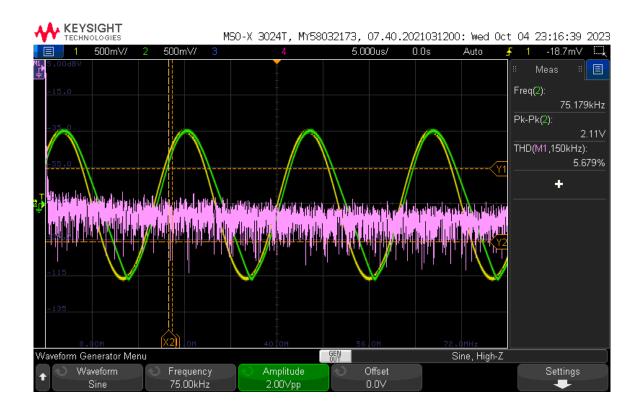
#### 3b. 75kHz 1V sine wave total harmonic distortion



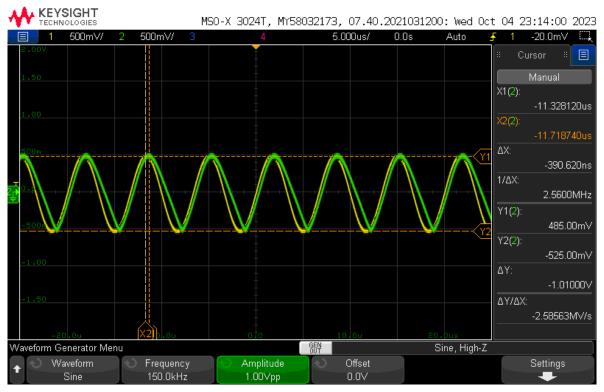
#### 3c. 75kHz 2V sine wave time-domain waveform



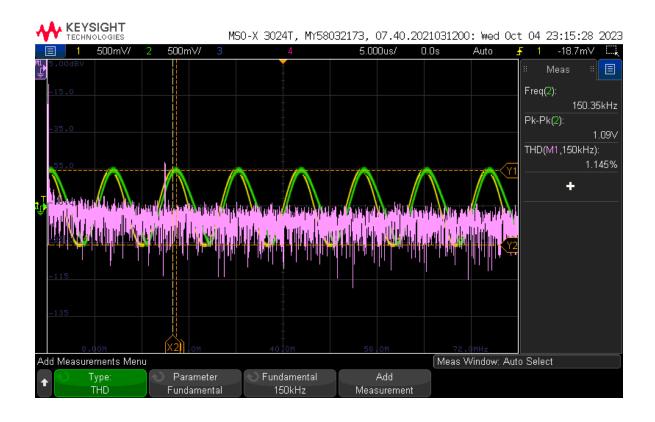
#### 3d. 75kHz 2V total harmonic distortion



#### 3e. 150kHz 1V time-domain waveform



#### 3f. 150kHz 1V total harmonic distortion



# **Data Table:**

The provided data table is a good way to organize and present our range of simulated and measured values. It is divided into three distinct sections: Lossy Integrator, Pseudo Differentiator, Finite GBW, and Slew Rate which correspond to different stages and aspects of the experiment or analysis. This format simplifies the detection of inconsistencies, allows for easy comparison of results across different methods or frequency domains, and ensures transparency and data integrity. By structuring data in this manner, we can efficiently manage and reference our findings, enhancing the clarity and reliability of our work.

|   | Simulated       | Measured           |
|---|-----------------|--------------------|
| Lossy Integrator low-frequency gain               | 26.78 dB        | 27 dB              |
| Lossy Integrator 3 dB frequency                   | 36.55 kHz       | 37 kHz             |
| Lossy Integrator magnitude at 1kHz                | -3.11 dB        | -3 dB              |
| Lossy Integrator phase at 1kHz                    | 91.75 degrees   | 92 degrees         |
| Lossy Integrator sine wave input voltage          | 497.598 mV      | 234 mV             |
| Lossy Integrator sine wave output voltage         | 68.40 mV        | 174 mV             |
| Lossy Integrator sine wave phase                  | 91.6 degrees    | <mark>270</mark> ° |
| Lossy Integrator square wave peak to peak voltage | 556.37 mV       | 262 mV             |
| Pseudo Differentiator low-frequency gain          | -60 dB          | -25 dB             |
| Pseudo Differentiator 3 dB frequency              | 58.71 kHz       | 33.77 kHz          |
| Pseudo Differentiator<br>magnitude at 1kHz        | 13.61 dB        | 14 dB              |
| Pseudo Differentiator phase at 1kHz               | -101.96 degrees | -100 degrees       |
| Pseudo Differentiator sine                        | 99.86 mV        | 86 mV              |

|  | T             | 1         |
|--|---------------|-----------|
| wave input voltage   |               |           |
| Pseudo Differentiator sine wave output voltage                   | 449.25 mV     | 426 mV    |
| Pseudo Differentiator sine wave phase                            | 106.5 degrees | 102. 24°  |
| Pseudo Differentiator<br>triangular wave peak to<br>peak voltage | 290.4 mV      | 278 mV    |
| Finite GBW Low frequency<br>R2 = 23                              | 27.21 dB      | 27.34 dB  |
| Finite GBW 3-dB frequency R2 = 23                                | 47.58 kHz     | 29.21 kHz |
| Finite GBW Low frequency<br>R2 = 57                              | 35.08 dB      | 35.2 dB   |
| Finite GBW 3-dB frequency R2 = 57                                | 19.64 kHz     | 10.58 kHz |
| Finite GBW Low frequency<br>R2 = 83                              | 38.31 dB      | 37.77 dB  |
| Finite GBW 3-dB frequency R2 = 83                                | 13.21 kHz     | 7.915 kHz |
| Slew Rate low frequency  | 0 dB          | 0 dB      |
| Slew Rate 3-dB frequency   | 1.55 Mhz      | 0.99 MHz  |
| Slew Rate magnitude<br>75kHz                                     | 36.5 uV       | 498 mV    |
| Slew Rate magnitude<br>150kHz                                    | 447.43 uV     | 485 mV    |
| Slew Rate 75kHz 1V sine wave THD                                 | 0.656%        | 10.575%   |
| Slew Rate 75kHz 2V sine wave THD                                 | 11.66%        | 5.679%    |
| Slew Rate 150kHz 1V sine wave THD                                | 11.15%        | 1.145%    |

$$|H| = \frac{V_{out}}{V_{in}} = \frac{234mV}{174mV} = 1.345$$

$$\Delta t = (-1mS - (-1.75mS) = 750\mu S \Rightarrow T = \frac{1}{f} = \frac{1}{1000} = 0.001S,$$

$$\angle H = \frac{\Delta t}{T} \times 360^{\circ} = \frac{750\mu S}{0.001S} \times 360^{\circ} = 270^{\circ}$$

Pseudo Differentiator sine wave phase

$$|H| = \frac{V_{out}}{V_{in}} = \frac{86mV}{426mV} = 0.202$$

$$\Delta t = (-437.5 \mu S - (-721.9 \mu S) = 284 \mu S \Rightarrow T = \frac{1}{f} = \frac{1}{1000} = 0.001S,$$

$$\angle H = \frac{\Delta t}{T} \times 360^{\circ} = \frac{284 \mu S}{0.001S} \times 360^{\circ} = 102.24^{\circ}$$

# **Results:**

In summary, this lab experiment demonstrated a strong correlation between our theoretical predictions and real-world measurements, affirming our understanding of circuit concepts. There were a few discrepancies found within our data when compared to prelab. While the exact causes remains unclear, the error serves as a reminder of the complexities in practical circuits, influenced by factors like environmental interference and component variations. Future experiments should explore error mitigation strategies. This experience emphasizes the importance of bridging theory and practice in electrical engineering education.