## Insurance Institute for Highway Safety Crashworthiness Evaluation

## Crash Test Report 2001 Ford Taurus (CF09009B)

**Vehicle identification number:** 1FAFP55U41A250759 **Body style:** Large 4-door sedan

**Engine/transmission:** Transverse 3.0-liter V6, 4-speed automatic, front-wheel drive

#### Standard crashworthiness features:

Frontal airbags, dual-stage depending on crash severity, belt use, and driver seat position Frontal airbags also have separate deployment thresholds for belted and unbelted occupants

Dual-locking shoulder belts (front outboard and all rear seating positions)
Shoulder belt height adjusters (front outboard seating positions only)
Seat belt crash tensioners in buckle (front outboard seating positions only)
Seat belt force-limiting mechanisms (front outboard seating positions only)

Lap/shoulder belt, center rear seating position

Shoulder belt retractors (right front and all rear) are convertible from emergency to automatic locking

LATCH system for child restraints (outboard rear seating positions)

#### **Optional safety features:**

Seat-mounted combination head and thorax side airbags (front seating positions) (test vehicle not equipped)

Adjustable brake and accelerator pedals (test vehicle equipped)

Antilock brakes, 4-wheel (test vehicle equipped)

Daytime running lights (test vehicle not equipped)

#### Vehicle specifications (provided by manufacturer):

Wheelbase: 276 cm
Overall length: 502 cm
Overall width: 185 cm
Curb weight: 1,522 kg

#### Vehicle specifications (measured):

Curb weight: 1,468 kg

Test weight: 1,545 kg (62% front, 38% rear)

Overall width: 185 cm

#### Nominal test parameters:

56.3 km/h and 28% overlap into 2005 Ford Taurus

#### **Dummy Seating Protocol:**

IIHS Guidelines for Using the UMTRI ATD Positioning Procedure for ATD and Seat Positioning (Version V)

Crash test date: June 23, 2009

Figure 1
Precrash and Postcrash Side Views — 2001 Ford Taurus





#### Summary

A 2001 Ford Taurus was crashed into a 2005 Ford Taurus in a collinear frontal offset configuration on June 23, 2009. The 2001 Ford Taurus was traveling at 56.1 km/h and the 2005 Ford Taurus was traveling at 55.9 km/h with a 28 percent overlap on the driver side for both vehicles. A Hybrid III 50th percentile male dummy was positioned in the driver seat with the lap/shoulder belt fastened. Figure 2 shows the dummy's postcrash overall position in the vehicle.

The pretest setup followed the IIHS Crashworthiness Evaluation Offset Barrier Crash Test Protocol (version XIII); however, the collinear car-to-car crash configuration for this test required some deviations from the protocol, which include:

- Removal of the fuel tank (resulting in a somewhat reduced test weight);
- A targeted 28 percent overlap with its crash partner (Figure 3); and
- The test was conducted at a nominal speed of 56.3 km/h; and
- The normal Hybrid III dummy ankles were replaced with a prototype design developed by First Technology Safety Systems and Denton ATD for the Society of Automotive Engineers Hybrid III Dummy Family Task Force. The updated design is intended to eliminate signal noise that can result from metal-to-metal contact between the ankle joint ball shaft and the ankle bumper retainer.

Measures of intrusion taken after the crash indicated the lower instrument panel in front of the dummy moved rearward 5-7 cm. Resultant intrusion in the driver footwell measured 13 cm at the footrest and 11-13 cm at other places on the toepan (Table 1). All doors remained closed during the crash. The driver door aperture shortened 6 cm, as measured at the lower edge of the window. After the crash, the driver door required tools to open; all other doors opened with ease.

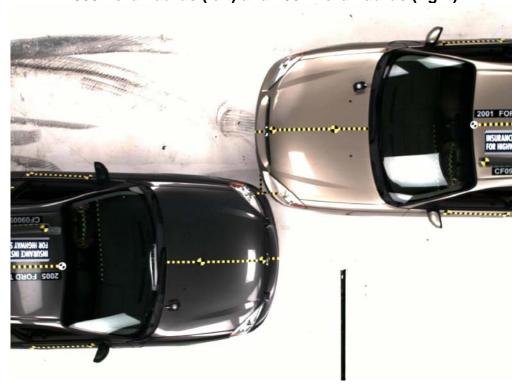
The driver dummy was restrained by a three-point lap/shoulder belt and an airbag. During the crash, the dummy's head loaded the fully inflated airbag. During rebound, the top of the head contacted the roof rail and window frame at about the same time the rear of the head contacted the B-pillar. Late in the crash, after data collection had ended, the rear of the head contacted the driver head restraint. After the crash, the upper end of the steering column had moved upward 5 cm and rearward 3 cm. Table 2 summarizes the timing of airbag deployment and dummy kinematic events.

Tables 3-6 contain summaries of the peak dummy injury measures. The peak resultant head acceleration from the contact with the roof rail and B-pillar was 40 g. The maximum right lower tibia L-M moment was -180 Nm, significantly contributing to the right lower tibia index of 0.94. The maximum right tibia axial force was -4.8 kN.

Figure 2
Dummy and Vehicle Interior, Postcrash — 2001 Ford Taurus



Figure 3
Video Frame Capture, Precrash —
2005 Ford Taurus (left) and 2001 Ford Taurus (right)



# Table 1 Residual Measurements of Intrusion Relative to Driver Seat — 2001 Ford Taurus

Selected Locations*	Longitudinal	Lateral	Vertical	Resultant
Steering column (cm)	-3	-3	5	7
Left lower instrument panel (cm)	-7	<b>-</b> 5	4	9
Right lower instrument panel (cm)	<b>–</b> 5	-5	4	8
Brake pedal (cm)	-9	-5	4	11
Left toepan (cm)	-9	-9	4	13
Center toepan (cm)	-6	<b>-7</b>	5	11
Right toepan (cm)	-8	-8	4	12
Footrest (cm)	-9	-9	3	13
Average displacement of the four seat attachment bolts relative to reference system (cm)	0	<b>–1</b>	0	n/a

<sup>\*</sup> All measurements taken on driver side. From the driver's position, positive is forward, left, and up.

Table 2
Restraint System Performance and Dummy Kinematics —
2001 Ford Taurus

Event	Time (ms)
Activation of seat belt crash tensioner (at buckle)	34
Deployment of driver and right front passenger frontal airbags	42
Airbag fully inflated	68
Face begins to load airbag	74
Top of head contacts roof rail/window frame and rear of head contacts B-pillar	206

Table 3 Head Injury Measurements — 2001 Ford Taurus					
Measure	Published Tolerance Threshold	Result	Time (ms)		
Vector resultant acceleration (g), during roof rail and B-pillar contact	80	40	218		
Vector resultant acceleration — 3 ms clip (g), during airbag loading	80	36	104-107		
Vector resultant acceleration — 3 ms clip (g), during roof rail and B-pillar contact	80	32	218-221		
Head Injury Criterion (HIC)	1000	159	86-122		
Head Injury Criterion — 15 ms interval (HIC-15)	700	102	100-115		

Table 4 Neck Injury Measurements — 2001 Ford Taurus				
Measure	Published Tolerance Threshold	Result	Time (ms)	
A-P shear force (kN)	±3.1	-0.6	111	
Axial compression force (kN)	4.0	2.9	220	
Axial tension force (kN)	3.3	1.0	102	
N <sub>ij</sub> Tension-Extension	1.00	0.16	84	
N <sub>ij</sub> Tension-Flexion	1.00	0.25	122	
N <sub>ij</sub> Compression-Extension	1.00	0.49	220	
N <sub>ij</sub> Compression-Flexion	1.00	0.47	220	
Flexion bending moment (Nm)		65	122	
Extension bending moment (Nm)		17	235	

Table 5 Chest Injury Measurements — 2001 Ford Taurus					
Published Tolerance Measure Threshold Result Time (ms)					
Vector resultant spine acceleration — 3 ms clip (g)	60	36	98-101		
Rib compression (mm)	-50	-25	99		
Viscous criteria (m/s)	1.0	0.1	97		
Sternum deflection rate (m/s)	-8.2	-0.7	95		

Table 6
Leg and Foot Injury Measurements — 2001 Ford Taurus

Measure	Published Tolerance Threshold	Left	Time (ms)	Right	Time (ms)
Femur axial force (kN)	-9.1*	-0.8	78	-1.9	83
Tibia-femur displacement (mm)	-15	-1	81	0	0
Upper Tibia					
L-M moment (Nm)	±225	<b>-</b> 56	70	-130	65
A-P moment (Nm)	±225	<b>-</b> 52	54	45	64
Vector resultant moment (Nm)	225	58	54	130	65
Index	1.00	0.31	54	0.71	65
Lower Tibia					
L-M moment (Nm)	±225**	-89	58	-180	65
A-P moment (Nm)	±225**	103	71	23	70
Vector resultant moment (Nm)	225**	113	70	181	65
Axial force (kN)	-8.0**	-2.3	53	-4.8	65
Index	1.00	0.51	70	0.94	65
Foot					
A-P acceleration (g)	±150	-137	51	-97	63
I-S acceleration (g)	±150	-86	54	-64	64
Vector resultant acceleration (g)	150	148	51	97	63

<sup>\*</sup> This critical value is for instantaneous loading. Femur loads are also compared with magnitude-duration injury criteria.

<sup>\*\*</sup> These published thresholds are for fractures of the tibia. Ankle and foot injuries have been associated with bending moments as low as 50-100 Nm, and heel fractures have been associated with axial forces as low as –6.0 kN.

#### References

Backaitis, S.H. and Mertz, H.J. (eds). 1994. *Hybrid III: The First Human-Like Crash Test Dummy*. Warrendale, PA: Society of Automotive Engineers.

Begeman, P.C. and Prasad, P. 1990. Human ankle impact response in dorsiflexion (SAE 902308). *Thirty-fourth Stapp Car Crash Conference Proceedings*, 39-53. Warrendale, PA: Society of Automotive Engineers.

Begeman, P.; Balakrishnan, P.; Levine, R.; and King, A. 1993. Dynamic human ankle response to inversion and eversion (SAE 933115). *Thirty-seventh Stapp Car Crash Conference Proceedings*, 83-93. Warrendale, PA: Society of Automotive Engineers.

Insurance Institute for Highway Safety. 2004. Crashworthiness evaluation offset barrier crash test protocol (version XIII). Arlington, VA.

Insurance Institute for Highway Safety. 2004. Guidelines for using the UMTRI ATD positioning procedure for ATD and seat positioning (version V). Arlington, VA.

Mertz, H.J. and Patrick, L.M. 1971. Strength and response of the human neck (SAE 710855). *Biomechanics of Impact Injury and Injury Tolerances of the Head-Neck Complex*, 821-46. Warrendale, PA: Society of Automobile Engineers.

Parenteau, C.S. 1995. Foot-ankle injury: epidemiology and method to investigate joint biomechanics. Gothenburg, Sweden: Chalmers University of Technology.

Prasad, P. and Mertz, H.J. 1985. The position of the United States delegation to the ISO Working Group 6 on the use of HIC in the automotive environment (SAE 851246). *Biomechanics of Impact Injury and Injury Tolerances of the Head-Neck Complex*, 373-83. Warrendale, PA: Society of Automotive Engineers.

Transport Canada. 1998. Motor Vehicle Safety Regulations – Canadian Motor Vehicle Safety Standards, Schedule IV Part III Standard 208, Occupant Restraint Systems in Frontal Impact. Ottawa, Ontario.

Welbourne, E.R. 1994. Vehicle performance requirements for head injury protection: a comparison of the head injury criterion with an 80 g limit on resultant acceleration. Technical Memorandum. Ottawa, Ontario: Transport Canada, Vehicle System Division.

Zeidler, F. 1984. The significance of lower limb injuries of belted drivers. *Journal of Orthopedics* [German].

### Appendix

**Dummy Clearance Measurements** 

#### **Dummy Clearance Measurements**

**Test Number:** CF09009B Vehicle: 2001 Ford Taurus

Electrically adjusted bucket seat (fore/aft and height) with Seat Type:

manually adjusted seat back angle

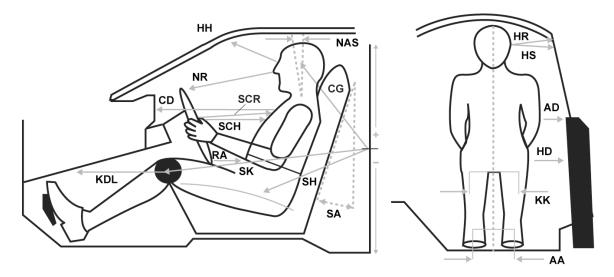
**Upper Belt Anchorage:** 

Set to 3<sup>rd</sup> of 5 positions Set to 3<sup>rd</sup> of 5 tilt adjustment positions **Steering Column Adjustment: Foot Pedal Adjustment** Set to fully forward position of fore/aft range

Location	Code Measure		Location	Code	Measure	
Head to header	НН	395	Striker to CG, horizontal	CGH	-13	
Nose to rim	NR	465	Striker to CG, lateral	CGL	345	
Chest to dash	CD	679	Striker to CG, vertical	CGV	531	
Rim to abdomen	RA	269	Striker to knee**	SK	535	
Knee to dash, left	KDL	303	Striker to knee angle**	SKA	–2.1°	
Knee to dash, right	KDR	255	Striker to H-point, horizontal	SHH	-152	
Steering wheel to chest, horizontal	SCH	347	Striker to H-point, vertical	SHV	-118	
Steering wheel to chest, reference	SCR	425	Ankle to ankle	AA	331	
Hub to chest, minimum	HCM	298	Knee to knee	KK	345	
Pelvic angle	PA	27.3°	Arm to door	AD	111	
Seat back angle*	SA	22.9°	H-point to door	HD	183	
Torso recline angle (H-point to Head CG)	TRA	12.0°	Head to A-pillar	HA	483	
Neck bracket angle	NBA	0°	Head to roof	HR	148	
Neck angle, seated	NAS	4.5°	Head to side window	HS	295	

All distance measurements are in millimeters (mm).

<sup>\*\*</sup> These measurements were made in a vertical plane containing the striker and parallel to the driver door sill.



<sup>\*</sup> Indicated value is from vertical, as measured on the head restraint post.