This Documentation revised according to rev 38 source code

Chapter **xx**

SWAT Input Data:

File.cio

File management is performed with the master watershed file (file.cio). The master watershed file contains the file names for the simulation run.

The master watershed file is divided into several sections. A brief description of the variables in the master watershed file follows. They are grouped by section and listed in the order they appear within the file.

**x.1 Title Section**

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| title | The first line of ‘file.cio’ is reserved for a description of the simulation run. The description may take up to 80 spaces. The description is optional, the line is required. |

**x.2 General Information**

**SIMULATION –** The simulation section of file.cio contains filenames for the entire simulation run. The list of the filenames are listed below with a brief description of the inputs within each file.

file.cio

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septic.str

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aqu\_catunit.ele

aqu\_catunit.def

aqu\_reg.def

res\_catunit.ele

res\_catunit.def

res\_reg.def

rec\_catunit.ele

res\_catunit.def

PATH\_PCP

null

PATH\_TMP

null

PATH\_SLR

null

PATH\_HMD

null

PATH\_WND

null

ls\_reg.ele

**time.sim**

The time simulation file includes the number of years to run the simulation and time step

and is space delimited. Below is a sample time.sim file:

time.sim: Simulation period and time step - 2-Stage ditch

IDAF YRC\_START IDAL\_IN YRC\_END STEP

0 2006 0 2007 0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the time.sim file (may be blank) |
| header |  |
| idaf | Beginning Julian day of simulation.  With this variable, SWAT is able to begin a simulation at any time of the year. If the variable is left blank or set to zero, the model starts the simulation on January 1st.  Required. |
| YRC\_start | Beginning year of simulation (for example, 1980).  The value entered for this variable is not important unless measured data (e.g. weather) is used in the run. When measured data is used, the model uses YR\_START to locate the beginning year within the data file.  Required. |
| idaL\_IN | Ending Julian day of simulation.  With this variable, SWAT is able to end a simulation at any time of the year. If the variable is left blank or set to zero, the model ends the simulation on December 31st.  Required. |
| YRC\_END | Ending year of simulation |
| STEP | Timestep of the simulation.  0 = daily; 1=increment (12 hrs); 24=hourly; 96-15 mins; 1440 = minute)  Required. |

**print.prt**

The print file controls the occurrence of the output files and is space delimited. Below is a sample print.prt file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the print.prt file |
| Header | Headings |
| nYSKIP | Number of years to ***not*** print output.  The options are   1. print output for all years of the simulation 2. print output after the first year of simulation 3. print output after the second year of simulation   ⭭  nbyr no output will be printed  Some simulations will need a warm-up or equilibration period. The use of an equilibration period becomes more important as the simulation period of interest shortens. For 30-year simulations, an equilibrium period is optional. For a simulation covering 5 years or less, an equilibrium period is recommended. An equilibration period of one year is usually adequate to get the hydrologic cycle fully operational.  Examples: If NYSKIP =2, the model will skip printing the first two years regardless of the starting year. In other words, if YRC\_START = 2000, we start printing in 2002. If YRC\_START = 2005, printing starts in 2007.  Notes: The daily print start and end time has nothing to do with NYSKIP. If the daily print time is skipped, it simply won't print the daily output.  The start year of printing is max(YRC\_START+NYSKIP). |
| JD\_START | Beginning Julian day of simulation to start printing output files for daily printing only |
| JD\_END | Ending Julian day of simulation to stop printing output files for daily printing only |
| YR\_START | Beginning year of simulation to start printing output files…. |
| YR\_END | Ending year of simulation to stop printing output files…. |
| INTERVAL | Daily print within the period  Specifies the interval within the specified printing time (i.e., INTERVAL =2) will print every other day. |
| header | Headings |
| AA\_NUMINT | Number of print intervals for ave annual output  Example: If AA\_NUMINT == 1955 1965 1975, Average annual results will be printed for the time periods ending in 1955, 1965, 1975.  Leaving the first number zero on this line will print average annual for the entire period (after NYSKIP). |
| aa\_YEARS | End years for aveage annual output |
| Header | Headings |
| csvout | Code to print .csv files n=no print; y = print |
| dbout | Code to print database (db) files n=no print; y = print (not currently active) |
| cdfout | Code to print netcdf (cdf) files n=no print; y = print (not currently active) |
| HEADER | Headers for the output files to follow |
| SOLOUT | Soils output file (print codes apply) (soils.out) |
| MGTOUT | Management output file (print codes apply) (mgt.out) |
| hydcon | Hydrograph connect output file (hydcon.out) |
| FDCOUT | Flow duration curve output file  n=no print; avann=print |
| hEADER | Headers for the output files to follow |
| wb\_bsn | Water balance BASIN output |
| NB\_BSN | Nutrient balance BASIN output |
| LS\_BSN | Losses BASIN output |
| PW\_BSN | Plant weather BASIN output  The print codes for all output files are:  0 = average annual (always prints)  1 = yearly  2 = monthly  3 = daily |
| AQU\_BSN | Aquifer output file (print codes apply) (aquifer.out) |
| RES\_BSN | Reservoir output file (print codes apply) (reservoir.out) |
| ChAN\_BSN | Channel output file (print codes apply) (channel.out) |
| SD\_CHAN\_BSN |  |
| RECALL\_BSN |  |
| WB\_REG | Water balance REGION output |
| NB\_REG | Nutrient balance REGION output |
| LS\_REG | Losses REGION output |
| PW\_REG | Plant weather REGION output |
| AQU\_REG |  |
| RES\_REG |  |
| CHAN\_REG |  |
| SD\_CHAN\_REG |  |
| RECALL\_REG |  |
| wb\_sub | Water balance SUBBASIN output |
| nb\_sub | Nutrient balance SUBBASIN output |
| ls\_sub | Losses SUBBASIN output |
| pw\_sub | Plant weather SUBBASIN output |
| wb\_hru | Water balance hru output |
| nb\_ hru | Nutrient balance hru output |
| ls\_ hru | Losses hru output |
| pw\_ hru | Plant weather hru output |
| wb\_SD | Water balance SWAT-DEG output |
| nb\_ SD | Nutrient balance SWAT-DEG output |
| ls\_ SD | Losses SWAT-DEG output |
| pw\_ SD | Plant weather SWAT-DEG output |
| CHAN | Channel output |
| sd\_chan | SWAT DEG (lte) channel output |
| aqu | Aquifer output |
| res | Reservoir output |
| recall | Recall output |
| hyd | Hydin output and hydout\_output |

**object.prt**

The object print file allows the user to define output and is space delimited. Below is a sample object.prt file:

object.prt: User-defined output files:

NUMB OBTYP OBTYPNO HYDTYP FILENAME

1 cha 64 tot outlet.out

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the object print file |
| header |  |
| WST\_NUMB | The sequential number of the weather station. |
| OB\_TYP | Type of object to print (cha, res, |
| OBTYPNO | Object type number |
| HYDTYP | Hydrograph type to print |
| FILENAME | Filename of output file (user defined). |

**object.cnt**

The object count file contains the total counts for the watershed simulation and is space delimited. Below is a sample object.cnt file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the object count file |
| header |  |
| OBJS | Total number of objects (sum of all following objects) |
| HRU | Total number of HRU’s |
| HRU\_LTE | Total number of HRU LTE (SWAT-DEG) |
| SUB | Total number of subbasins |
| MODFLOW | Total number of modparms |
| AQU | Total number of aquifers |
| CHAN | Total number of channels |
| RES | Total number of reservoirs |
| RECALL | Total number of recdays |
| EXCO | Total number of export coefficients |
| DR | Total number of delivery ratios |
| CANAL | Total number of canals |
| PUMP | Total number of pumps |
| OUTLET | Total number of outlets |
| CHANDEG | Total number of LTE channels (SWAT-DEG) |
| AQU2D | Total number of 2D aquifers |
| HERD | Total number of herds |
| WRO | Total number of water rights |

**CLIMATE –** The CLIMATE section of file.cio contains filenames for the entire simulation run. The list of the filenames are listed below with a brief description of the inputs within each file.

**weather-sta.cli**

The weather station climate file contains the weather stations that will be included in the simulation and is space delimited. Below is a sample weather-sta.cli file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The sequential number of the weather station. |
| header |  |
| WST\_NUMB | The sequential number of the weather station. |
| WST\_NAME | The weather station name |
| WGN | The weather generator station name (from the weather-wgn.cli file) |
| PGAGE | The precipitation station name (from pcp.cli file). If precipitation is generated, ‘sim’ should be input. |
| TGAGE | The temperature station name (from tmp.cli file). If temperature will be generated, ‘sim’ should be input. |
| SGAGE | The solar radiation station name (from slr.cli file). If solar radiation will be generated, ‘sim’ should be input. |
| HGAGE | The relative humidity station name (from hmd.cli file). If relative humidity will be generated, ‘sim’ should be input. |
| WGAGE | The wind station name (from wnd.cli file). If wind will be generated, ‘sim’ should be input. |
| WNDIR | The wind direction name (from wind-dir.cli file). If wind direction will be generated, ‘sim’ should be input. |
| ATMODEP | The atmospheric deposition file name. If no atmospheric deposition file is used, ‘null’ should be input. |

**weather-wgn.cli**

The weather generator climate file contains the weather generator stations that will be included in the simulation and is space delimited. Below is a sample weather-wgn.cli file (partial listing):

WGN\_DAT Generated from V:\CEAP\Model\_Constructor\_Command\_Line\HUC8\_Models\07100001.accdb Time: 6/19/2017 1:30:00 PM

MN214453 43.7 -95.15 466.3 51

TMPMX TMPMN TMPSTDMX TMPSTDMN PCPMM PCPSTD PCPSKW PR\_WD PR\_WW PCPD RAINHMX SOLARAV DEWPT WINDAV

-5.38 -15.72 7.2 7.61 13.16 3.8 3.9 0.09 0.33 3.69 2.62005 7.16 -11.14 4.64

-2.23 -12.64 7.08 7.54 15.58 4.29 2.61 0.1 0.35 3.84 4.300541 10.89 -11.39 4.69

4.18 -6.3 7.27 6.64 41.85 7.13 2.55 0.14 0.43 6.14 5.76011 15.21 -5.57 4.54

13.55 1.13 7.1 4.88 71.18 8.62 2.55 0.22 0.5 9.16 19.09196 18.27 -0.09 4.96

20.99 7.85 5.81 4.64 88.45 9.12 2.84 0.26 0.53 11 25.50741 20.99 3.3 4.96

26.26 13.6 4.46 3.66 105.33 10.24 2.43 0.29 0.51 11.1 37.92709 23.09 13.46 4.12

28.38 15.95 3.55 3.21 93.55 12.14 3.29 0.24 0.45 9.48 27.89453 23.42 16.73 3.51

26.88 14.43 3.7 3.45 96 13.85 2.64 0.24 0.42 8.92 38.13729 20.74 16.14 3.38

22.42 9.28 5.21 4.77 79.96 12.68 4.58 0.2 0.48 8.5 16.00481 16.26 5.14 4.16

15.61 2.62 6.42 5.02 50.81 9.17 2.28 0.14 0.48 6.46 13.91441 11.48 1.27 4.39

5.49 -4.72 7.02 5.66 33.31 7.76 2.72 0.12 0.41 5.16 5.813965 7.37 -3.89 4.66

-2.71 -12.26 6.93 7.04 17.02 4.36 2.32 0.1 0.28 3.86 3.63817 5.78 -10.2 4.75

MN214534 44 -95.95 502.9 51

TMPMX TMPMN TMPSTDMX TMPSTDMN PCPMM PCPSTD PCPSKW PR\_WD PR\_WW PCPD RAINHMX SOLARAV DEWPT WINDAV

-5.36 -15.72 7.51 7.85 14.67 4.05 2.5 0.09 0.31 3.59 1.964559 7.12 -11.14 4.64

-2.2 -12.67 7.34 7.79 17.42 5.03 2.12 0.1 0.3 3.45 4.563535 10.89 -11.39 4.69

4.3 -6.39 7.49 6.86 43.65 8.7 2.29 0.14 0.35 5.48 5.353518 15.34 -5.57 4.54

13.61 0.9 7.26 5.06 72.2 9.98 2.69 0.21 0.41 7.92 18.37086 18.35 -0.09 4.96

21.03 7.71 5.8 4.87 82.66 9.97 3.19 0.23 0.45 9.3 24.11257 20.99 3.3 4.96

26.21 13.31 4.5 3.93 98.65 12.08 2.5 0.26 0.45 9.68 34.52444 23.09 13.46 4.12

28.52 15.84 3.69 3.55 85.56 11.65 2 0.22 0.37 8 25.5597 23.46 16.73 3.51

26.88 14.43 3.7 3.45 96 13.85 2.64 0.24 0.42 8.92 38.13729 20.74 16.14 3.38

22.51 9.23 5.45 5.1 76.83 12.24 2.82 0.19 0.39 7.28 14.49095 16.26 5.14 4.16

15.53 2.57 6.49 5.23 51.89 12.58 2.9 0.12 0.4 5.08 13.51547 11.35 1.27 4.39

5.2 -5.02 7.1 5.88 34.33 8.33 1.92 0.1 0.4 4.35 5.631958 7.25 -3.89 4.66

-2.8 -12.39 7.02 7.22 17.63 4.84 2.09 0.1 0.28 3.63 2.648281 5.74 -10.2 4.75

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the weather-wgn.cli file |
| WGN\_NAME | The weather station name (to be referenced in weather-sta.cli file. |
| LATITUDE | Latitude of weather station used to create statistical parameters (degrees).  The latitude is expressed as a real number with minutes and seconds converted to fractions of a degree. |
| LONGITUDE | Longitude of weather station (degrees). |
| ELEV | Elevation of weather station (m).  Required if elevation bands are modeled in watershed. |
| RAIN\_YRS | The number of years of maximum monthly 0.5 h rainfall data used to define values for RAIN\_HHMX(1) - RAIN\_HHMX(12).  If no value is input for RAIN\_YRS, SWAT will set RAIN\_YRS = 10.  Required. |
| TMPMX(mon) | Average or mean daily maximum air temperature for month (ºC).  This value is calculated by summing the maximum air temperature for every day in the month for all years of record and dividing by the number of days summed:    where μmxmon is the mean daily maximum temperature for the month (°C), Tmx,mon is the daily maximum temperature on record d in month mon (°C), and N is the total number of daily maximum temperature records for month mon.  Required. |
| TMPMN(mon) | Average or mean daily minimum air temperature for month (ºC).  This value is calculated by summing the minimum air temperature for every day in the month for all years of record and dividing by the number of days summed:    where *μmnmon* is the mean daily minimum temperature for the month (°C), *Tmn,mon* is the daily minimum temperature on record *d* in month *mon* (°C), and *N* is the total number of daily minimum temperature records for month *mon*.  Required. |
| TMPstDmx(mon) | Standard deviation for daily maximum air temperature in month (ºC).  This parameter quantifies the variability in maximum temperature for each month. The standard deviation is calculated:    where *σmxmon* is the standard deviation for daily maximum temperature in month *mon* (ºC), *Tmx,mon* is the daily maximum temperature on record *d* in month *mon* (°C), *μmxmon* is the average daily maximum temperature for the month (°C), and *N* is the total number of daily maximum temperature records for month *mon*.  Required. |
| TMPStDmn(mon) | Standard deviation for daily minimum air temperature in month (ºC).  This parameter quantifies the variability in minimum temperature for each month. The standard deviation is calculated:    where *σmnmon* is the standard deviation for daily minimum temperature in month *mon* (ºC), *Tmn,mon* is the daily minimum temperature on record *d* in month *mon* (°C), *μmnmon* is the average daily minimum temperature for the month (°C), and *N* is the total number of daily minimum temperature records for month *mon*.  Required. |
| PCPmm(mon) | Average or mean total monthly precipitation (mm H2O).    where  is the mean monthly precipitation (mm H2O), *Rday,mon* is the daily precipiation for record *d* in month *mon* (mm H2O), *N* is the total number of records in month *mon* used to calculate the average, and *yrs* is the number of years of daily precipitation records used in calculation.  Required. |
| PCPstd(mon) | Standard deviation for daily precipitation in month (mm H2O/day ).  This parameter quantifies the variability in precipitation for each month. The standard deviation is calculated:    where *σmon* is the standard deviation for daily precipitation in month *mon* (mm H2O), *Rday,mon* is the amount of precipitation for record *d* in month *mon* (mm H2O), is the average precipitation for the month (mm H2O), and *N* is the total number of daily precipitation records for month *mon*. (Note: daily precipitation values of 0 mm are included in the standard deviation calculation).  Required. |
| PCPsKW(mon) | Skew coefficient for daily precipitation in month.  This parameter quantifies the symmetry of the precipitation distribution about the monthly mean. The skew coefficient is calculated:    where *gmon* is the skew coefficient for precipitation in the month, *N* is the total number of daily precipitation records for month *mon*, *Rday,mon* is the amount of precipitation for record *d* in month *mon* (mm H2O), is the average precipitation for the month (mm H2O), and *σmon* is the standard deviation for daily precipitation in month *mon* (mm H2O). (Note: daily precipitation values of 0 mm are included in the skew coefficient calculation).  Required. |
| PR\_wd(mon) | Probability of a wet day following a dry day in the month.  This probability is calculated:    where *Pi(W/D)* is the probability of a wet day following a dry day in month *i*, *daysW/D,i* is the number of times a wet day followed a dry day in month *i* for the entire period of record, and *daysdry,i* is the number of dry days in month *i* during the entire period of record. A dry day is a day with 0 mm of precipitation. A wet day is a day with > 0 mm precipitation.  Required. |
| pr\_ww(mon) | Probability of a wet day following a wet day in the month.  This probability is calculated:    where *Pi(W/W)* is the probability of a wet day following a wet day in month *i*, *daysW/W,i* is the number of times a wet day followed a wet day in month *i* for the entire period of record, and *dayswet,i* is the number of wet days in month *i* during the entire period of record. A dry day is a day with 0 mm of precipitation. A wet day is a day with > 0 mm precipitation.  Required. |
| PCPD(mon) | Average number of days of precipitation in month.  This parameter is calculated:    where  is the average number of days of precipitation in month *i*, *dayswet,i* is the number of wet days in month *i* during the entire period of record, and *yrs* is the number of years of record.  Required. |
| rainHmx(mon) | Maximum 0.5 hour rainfall in entire period of record for month (mm H2O).  This value represents the most extreme 30-minute rainfall intensity recorded in the entire period of record.  Required. |
| SoLaRAV(mon) | Average daily solar radiation for month (MJ/m2/day).  This value is calculated by summing the total solar radiation for every day in the month for all years of record and dividing by the number of days summed:    where *μradmon* is the mean daily solar radiation for the month (MJ/m2/day), *Hday,mon* is the total solar radiation reaching the earth’s surface for day *d* in month *mon* (MJ/m2/day), and *N* is the total number of daily solar radiation records for month *mon*.  Required. |
| DeWpt(mon) | Average daily dew point temperature for each month (ºC) or relative humidity (fraction) can be input.  If all twelve months are less than one, the model assumes relative humidity is input. Relative humidity is defined in equation 1:3.5.1 in the SWAT Theoretical documentation as the amount of water vapor in the air as a fraction of saturation humidity. If any month has a value greater than 1.0, the model assumes dewpoint temperature is input.  Dew point temperature is the temperature at which the actual vapor pressure present in the atmosphere is equal to the saturation vapor pressure. This value is calculated by summing the dew point temperature for every day in the month for all years of record and dividing by the number of days summed:    where *μdewmon* is the mean daily dew point temperature for the month (ºC), *Tdew,mon* is the dew point temperature for day *d* in month *mon* (ºC), and *N* is the total number of daily dew point records for month *mon*. Dew point is converted to relative humidity using equations 1:3.5.1 and  1:3.5.2 in the Theoretical Documentation.  Required for Penman-Monteith potential evaporation equation. |
| WiNDAV(mon) | Average daily wind speed in month (m/s).  This value is calculated by summing the average or mean wind speed values for every day in the month for all years of record and dividing by the number of days summed:    where *μwndmon* is the mean daily wind speed for the month (m/s), *μwnd,mon* is the average wind speed for day *d* in month *mon* (m/s), and *N* is the total number of daily wind speed records for month *mon*.  Required. |

**wind-dir.cli**

This file contains the wind direction values that will be included in the simulation and is space delimited. Below is a sample wind-dir.cli file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the wind direction file (may be blank) |
| MWND\_DIR | The maximum number of wind direction stations in the file. |
| SKIP | Next 2 lines are not read in by the model |
| WND\_DIR | The monthly wind directions input data (16 lines/directions) |

**pcp.cli**

This file contains the information on the precipitation gages included in the simulation and is space delimited. A path has been added to file.cio to enable the daily files to be present in another folder; if path is null daily is in same project folder as other data. Below is a sample pcp.cli file:

pcp.cli: Precipitation files

FILENAME

lrew01.pcp

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the precipitation climate file (may be blank) |
| HEADER | The header information for the pcp.cli file |
| PCP\_FILENAME | The name of the precipitation file containing daily precipitation input data (description of the pcp\_filename data follows) |

**pcp\_filename**

The pcp\_filename is input in the pcp.cli file. The description of the ‘pcp\_filename’ contains the daily precipitation amounts for the simulation and is space delimited. A path has been added to file.cio to enable the daily files to be present in another folder; if path is null daily is in same project folder as other data. Below is a sample of the file (partial listing):

LREW01.pcp

NBYR TSTEP LAT LONG ELEV

25 0 31.45 -83.48 115.8

1988 1 0.0

1988 2 10.2

1988 3 12.7

1988 4 9.1

1988 5 0.0

1988 6 0.0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the precipitation file (may be blank) |
| header |  |
| NBYR | The header information for the file |
| TSTEP | Timestep of the simulation |
| LAT | Latitude of the precipitation gage |
| LONG | Longitude of the precipitation gage |
| ELEV | Elevation of the precipitation gage |
| IYR | The year of the precipitation amount |
| ISTEP | The step (day, sub-daily) of the precipitation amount |
| pcp | The amount of precipitation amount (mm) for istep (enter -99.0 for missing days) |

**tmp.cli**

This file contains information on the maximum and minimum temperatures included in the simulation and is space delimited. A path has been added to file.cio to enable the daily files to be present in another folder; if path is null daily is in same project folder as other data. Below is a sample tmp.cli file:

tmp.cli: Temperature file names

FILENAME

lrew01.tmp

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the maximum and minimum temperature file (may be blank) |
| HEADER | The header information for the tmp.cli file |
| TMP\_FILENAME | The name of the temperature file containing daily maximum and minimum temperatures. |

**tmp\_filename**

The tmp\_filename is input in the tmp.cli file. The description of the ‘tmp\_filename’ contains the daily maximum and minimum temperatures for the simulation and is space delimited. Below is a sample of the file (partial listing):

LREW01.tmp: Temperature data gage

NBYR LAT LONG ELEV

25 31.45 -83.48 115.80

1988 1 18.30 5.00

1988 2 20.60 9.40

1988 3 11.70 5.00

1988 4 6.70 3.30

1988 5 12.20 -0.60

1988 6 9.40 -3.30

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the temperature file (may be blank) |
| header | Headings |
| NBYR | The header information for the file |
| LAT | Latitude of the temperature gage |
| LONG | Longitude of the temperature gage |
| ELEV | Elevation of the temperature gage |
| IYR | The year of the temperature data |
| ISTEP | Timestep |
| tmp\_max | The maximum temperatures for istep (enter -99.0 for missing days) |
| TMP\_MIN | The minimum temperatures for istep (enter -99.0 for missing days) |

**slr.cli**

This file contains the information on the solar radiation daily data included in the simulation and is space delimited. A path has been added to file.cio to enable the daily files to be present in another folder; if path is null daily is in same project folder as other data. Below is a sample slr.cli file:

slr.cli

NUMB FILENAME

1 gage1.slr

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the solar radiation file (may be blank) |
| HEADER | The header information for the slr.cli file |
| slr\_FILENAME | The name of the solar radiation file containing values of solar radiation |

**slr\_filename**

The slr\_filename is input in the slr.cli file. The description of the ‘slr\_filename’ contains the daily solar radiation values for the simulation and is space delimited. Below is a sample of the file (partial listing):

gage1.slr

NBYR LAT LONG ELEV

25 0.0 0.0 0.0

1988 1 12.9

1988 2 27.4

1988 3 22.7

1988 4 28.0

1988 5 9.4

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the solar radiation file (may be blank) |
| Header | Headings |
| NBYR | The header information for the file |
| LAT | Latitude of the solar radiation gage |
| LONG | Longitude of the solar radiation gage |
| ELEV | Elevation of the solar radiation gage |
| IYR | The year of the solar radiation data |
| ISTEP | Timestep |
| SLR | The solar radiation value for istep (MJ/m^2; -99.0 to generate missing days) |

**hmd.cli**

This file contains the information on the relative humidity stations included in the simulation and is space delimited. A path has been added to file.cio to enable the daily files to be present in another folder; if path is null daily is in same project folder as other data. Below is a sample hmd.cli file:

hmd.cli

NUMB FILENAME

1. gage1.hmd

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the relative humidity file (may be blank) |
| HEADER | The header information for the hmd.cli file |
| HMD\_FILENAME | The name of the relative humidity file containing daily relative humidity input data |

**hmd\_filename**

The hmd\_filename is input in the hmd.cli file. The description of the ‘hmd\_filename’ contains the daily relative humidity values for the simulation and is space delimited. Below is a sample of the file (partial listing):

gage1.hmd

NBYR LAT LONG ELEV

25 0.0 0.0 0.0

1988 1 1.0

1988 2 0.8

1988 3 0.7

1988 4 1.0

1988 5 0.5

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the relative humidity file (may be blank) |
| Header | Headings |
| NBYR | The header information for the file |
| LAT | Latitude of the relative humidity gage |
| LONG | Longitude of the relative humidity gage |
| ELEV | Elevation of the relative humidity gage |
| IYR | The year of the relative humidity data |
| ISTEP | Timestep |
| RELHUM | The relative humidity value for istep (-99.0 to generate missing days) |

**wnd.cli**

This file contains the information on the windspeed input data included in the simulation and is space delimited. A path has been added to file.cio to enable the daily files to be present in another folder; if path is null daily is in same project folder as other data. Below is a sample wnd.cli file (partial listing):

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the wnd.cli file (may be blank) |
| HEADER | The header information for the wnd.cli file |
| WND\_FILENAME | The name of the precipitation file containing daily windspeed input data |

**wnd\_filename**

The wnd\_filename is input in the wnd.cli file. The description of the ‘wnd\_filename’ contains the daily wind values for the simulation and is space delimited. Below is a sample of the file (partial listing):

gage1.wnd - Little River Watershed

NBYR LAT LONG ELEV

25 0.0 0.0 0.0

1988 1 3.8

1988 2 4.4

1988 3 2.8

1988 4 2.0

1988 5 3.1

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the windspeed file (may be blank) |
| Header | Headings |
| NBYR | The header information for the file |
| LAT | Latitude of the windspeed gage |
| LONG | Longitude of the windspeed gage |
| ELEV | Elevation of the windspeed gage |
| IYR | The year of the windspeed data |
| ISTEP | Timestep |
| WNDSPD | The windspeed value for istep (-99.0 to generate missing days) |

**atmo.cli**

The atmo.cli file contains the input variables for atmospheric deposition. The atmospheric deposition input file contains annual average atmospheric nitrogen deposition values including ammonium, nitrate, dry ammonium and dry nitrate and can be read in as average annual or monthly. This file is optional. Partial Sample atmo.cli (average annual) and atmo\_mon.cli (monthly) files are listed below. not sure about this example data set should line 7 be there?

Atmodep\_file

line2

line3

line4

line5

2 36

1 2000

0.375 2.2 0.02 1.6 0.5 1.1 0.2 1.2 0.3 1.1 0.01 1.5 0.45 1.204 0.224 1.66 0.459 1.178 0.254

|  |  |  |
| --- | --- | --- |
| **Variable name** | | **Definition** |
| TITLE | The first five lines of the atom.dat file are reserved for user comments. The title line is not processed by the model and may be left blank. | |
| MATMODEP |  | |
| MOMAX |  | |
| NO3\_RF | Atmospheric deposition of nitrate (mg/l) for entire watershed. | |
| NH4\_RF | Atmospheric deposition of ammonium (mg/l) values for entire watershed. | |
| NO3\_DRY | Atmospheric dry deposition of nitrates (kg/ha/yr) for entire watershed. | |
| NH4\_DRY | Atmospheric dry deposition of ammonium (kg/ha/yr) for entire watershed. | |

**CONNECT –** The connect section of file.cio contains the filenames for the object connectivity for the simulation run. **All** connect (.con) files read in the same input variables, only differing in the connect units (HRU, HRU-LTE, ROUT\_UNIT, modflow, aquifer, aquifer2d, channel, reservoir, recall, exco, delivery ratio, outlet and chandeg).

**Explanation of SPATIAL OBJECTS**

**SUBBASIN**

The subbasin is defined by the DEM in the GIS interface as it always has been. All flow within the subbasin drains to the subbasin outlet.

**LANDSCAPE UNIT**

A landscape unit is defined as a collection of HRU’s and can be defined as a subbasin, or it could be a flood plain or upland unit, or it could be a grid cell with multiple HRU’s. The landscape unit is not routed, it only used for output. The landscape unit output files (waterbal, nutbal, losses, and plant weather) are output for HRU’s, landscape units, and for the basin. Two input files are required: 1) landscape elements and, 2) landscape define. The elements file includes HRU’s and their corresponding LSU fraction and basin fractions. The define file specifies which HRU’s are contained in each LSU.

**ROUTING UNIT**

A routing unit is a collection of hydrographs that can be routed to any spatial object. The routing unit can be configured as a subbasin, then total flow (surface, lateral and tile flow) from the routing unit can be sent to a channel and all recharge from the routing unit sent to an aquifer. This is analogous to the current approach in SWAT. However, SWAT+ gives us much more flexibility in configuring a routing unit. For example, in CEAP, we are routing each HRU (field) through a small channel (gully or grass waterway) before it reaches the main channel. In this case, the routing unit is a collection of flow from the small channels. We also envision simulating multiple representative hillslopes to define a routing unit. Also, we are setting up scenarios that define a routing unit using tile flow from multiple fields and sending that flow to a wetland.

The routing unit is the spatial unit SWAT+ that allows us to lump outputs and route the outputs to any other spatial object. It gives us considerably more flexibility than the old subbasin lumping approach in SWAT, and will continue to be a convenient way of spatial lumping until we can simulate individual fields or cells in each basin.

**hru.con**

The hru.con file contains the connectivity for the HRU spatial objects within the watershed that will be included in the simulation and is space delimited. Below is a sample hru.con file:

hru.con: HRU spatial units - Little River Experimental Watershed

NUMB NAME AREA\_HA LAT LONG ELEV HRU WST CONSTIT OVERFLOW RULESET OUT\_TOT OBTYP\_OUT OBTYPNO\_OUT HTYP\_OUT FRAC\_OUT

1 bench 0.4800 0.0 0.0 0.00 1 1 0 0 0 0 0

2 field 495.27 0.0 0.0 0.00 2 1 0 0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the connect file |
| HEADER | The header information for the HRU connect file |
| numb | Number of object unit |
| name | Name of the object connect |
| area\_ha | Area of the object (ha) |
| lat | Latitude of the object |
| long | Longitude of the object |
| ELEV |  |
| PROPS(HRU) | Object properties number |
| wst | Weather station number (‘weather-sta.cli’ file) |
| constit | Constituent data pointer (pesticides, pathogens, metals, salts) |
| PROPs2(overflow) | Overbank connectivity pointer to landscape units |
| RULESET | Ruleset pointer for flow fraction of hydrograph |
| SRC\_TOT | Total number of incoming (source) objects |
| oBTYP\_OUT | Outflow object type(’hru’;’hlt’,’ru’;’mfl’; aqu’; ’cha’; ’res’; ’exc’; ’del’; ‘out’;’sdc’) (default == ‘null’)  |  |  | | --- | --- | | **SPATIAL OBJECTS** |  | | HRU | HYDROLOGIC RESPONSE UNIT | | HLT | HRU LITE | | RU | ROUTING UNIT | | MFL | MODFLOW | | AQU | AQUIFER | | CHA | CHANNEL | | RES | RESERVOIR | | REC | RECALL | | EXC | EXPORT COEFFICIENTS | | DR | DELIVERY RATIO | | CAN | CANAL | | PUM | PUMP | | OUT | OUTLET | | SDC | SWAT DEG CHANNEL | |
| obtyp\_NOout | Outflow object type name |
| Htyp\_out | Outflow hydrograph (1=’tot’; 2=’rhg’;3=’sur’;4=’lat’;5=’til’;  (default = ‘null’)   |  |  | | --- | --- | | **OUTFLOW HYDROGRAPHS** | | | TOT | TOTAL | | RHG | RECHARGE | | SUR | SURFACE | | LAT | LATERAL | | TIL | TILLAGE | |
| FRAC\_OUT | Fraction of hydrograph |

**CHANNEL –** The channel section of file.cio contains the filenames for simulation of a channel in the model. In order to simulate the physical processes affecting the flow of water and transport of sediment in the channel network of the watershed, SWAT requires information on the physical characteristics of the main channel within each subbasin. The channel input files summarizes the physical characteristics of the channel which affect water flow and transport of sediment, nutrients and pesticides.

**initial.cha**

The initial.cha file contains the input variables for the initialization of a channel. Below is a partial sample initial.cha file:

initial.cha: Channel initialization - LREW Subbasin March 2016

CHA\_INI\_NAME VOL SED PARTN NO3N NO2N NH3N PARTP SOLP SECI SAND SILT

null 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | Title of the initial channel file |
| HEADER | The header information for the initial channel file |
| NAME | Name of the channel |
| VOL | Reservoir volume (m^3) |
| SED | Amount of sediment in reservoir (kg/L) |
| ORGN | Amount of organic nitrogen in reservoir (kg N) |
| NO3 | Amount of nitrate in reservoir (kg N) |
| NO2 | Amount of nitrite in reservoir (kg N) |
| NH3 | Amount of ammonia in reservoir (kg) |
| orgp | Amount of organic phosphorous in reservoir (kg P) |
| SOLP | Amount of soluble phosphorous in reservoir (kg P) |
| SECI | Secci-disk depth (m) |
| SAN | Amount of sand in reservoir (kg/L) |
| SIL | Amount of silt in reservoir (kg/L) |
| CLA | Amount of clay in reservoir (kg/L) |
| SAG | Amount of small aggregates in reservoir (kg/L) |
| LAG | Amount of large aggregates in reservoir (kg/L) |
| GRA | Amount of gravel in reservoir (kg/L) |
| CHLA | Amount of chlorophyll-a in reservoir (kg chl-a) |
| PSOL | Amount of soluble phosphorous in reservoir (kg/L) |
| PSOR | Amount of sorbed phosphorous in reservoir (kg/L) |
| BACTLP | Less persistent bacteria stored in reservoir (# cfu/100ml) |
| BACTP | Persistent bacteria stored in reservoir (# cfu/100ml) |

**channel.cha**

The channel.cha file contains the input variables for the initialization of a channel. Below is a sample channel.cha file:

channel.cha

NUMB NAME INI HYD SED NUT PST LS\_LNK AQU\_LNK

1 cha1 null cha1 null null null 0 0

2 cha2 null cha2 null null null 0 0

3 cha3 null cha3 null null null 0 0

4 cha4 null cha4 null null null 0 0

5 cha5 null cha5 null null null 0 0

6 cha6 null cha6 null null null 0 0

7 cha7 null cha7 null null null 0 0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the channel file |
| HEADER | The header information for the channel file |
| NUMB | Number of the channel |
| NAME | Name of the channel |
| INIt | Initial data (points to initial.cha) |
| HYD | Channel hydrology inputs (points to hydrology.cha) |
| SED | Channel sediment inputs (points to sediment.cha) |
| NUT | Channel nutrient inputs (points to nutrients.cha) |
| PST | Channel pesticide inputs (points to pesticide.cha) |
| LS\_LNK | Landscape linkage (points to chan-surf.lin) |
| AQU\_LNK | Aquifer linkage (points to chan-aqu.lin) |

**hydrology.cha**

The hydrology.cha file contains the input variables for the hydrology inputs of a channel. Below is a sample hydrology.cha file:

hydrology.cha: Channel properties

NAME W D S L N K WDR ALPHA\_BNK SIDE

CHA1 3.45 0.3556 0.0090 0.1116 0.014 0.01 9.7 0.1 2.0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the channel hydrology file |
| HEADER | The header information for the channel hydrology file |
| NAME | Name of the channel hydrology |
| W | Average width of the main channel (m) |
| D | Average depth of the main channel (m) |
| S | Average slope of the main channel (m/m) |
| L | Main channel length (km) |
| N | Manning’s “n” value for the main channel |
| K | Effective hydraulic conductivity of main channel alluvium (mm/hr) |
| WDR | Channel width to depth ratio (m/m) |
| ALPHA\_BNK | Alpha factor for bank storage recession curve (days) |
| SIDE | Change in horizontal distance per unit |

**sediment.cha**

The sediment.cha file contains the input variables for the sediment inputs of a channel. Below is a sample sediment.cha file:

sediment.cha: Channel properties

NAME EQN COV1 COV2 BNK\_BD BED\_BD BNK\_KD BED\_KD BNK\_D50 BED\_D50 TC\_BNK TC\_BED EROD(mon)

CHA1 0 0.5 0.5 1.5 1.5 0.5 0.5 1.5 1.5 0.05 0.05 1. 1. 1. 1. 1. 1. 1. 1.1.1.1.1.

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the sediment channel file |
| HEADER | The header information for the sediment channel file |
| NAME | Name of the sediment channel |
| EQN | Sediment routine methods:   1. = original SWAT method; 2. Bagnold’s 3. Kodatie 4. Molinas WU 5. Yang |
| COV1 | Channel erodibility factor (0.0-1.0) |
| COV2 | Channel cover factor (0.0-1.0) |
| BNK\_BD | Bulk density of channel bank sediment (g/cc) |
| BED\_BD | Bulk density of channel bed sediment (g/cc) |
| BNK\_KD | Erodibility of channel bank sediment by jet test |
| BED\_kD | Erodibility of channel bed by jet test |
| BNK\_D50 | D50 (median) particle size diameter of channel bank |
| BED\_D50 | D50 (median) particle size diameter of channel bed |
| TC\_BNK | Critical shear stress of channel bank (N/m^2) |
| TC\_BED | Critical shear stress of channel bed (N/m^2) |
| EROD1-12 | Value of 0.0 indicates a non-erosive channel while a value of 1.0 indicates no resistance to erosion |

**nutrients.cha**

The nutrients.cha file contains the input variables for the nutrients of a channel. Below is a sample partial nutrients.cha file:

nutrients.cha: Nutrients channel properties - LREW Subbasin March 2016

CHA\_NUT\_NAME BNK\_ORGN BNK\_ORGP ALG\_STL BEN\_DISP BEN\_NH3N ORGN\_STL ORGP\_STL CONST\_STL

null 0.000 0.000 1.000 0.050 0.500 0.050 0.050 2.500

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the nutrients.cha file. |
| Name | Name of the nutrients channel |
| ONCO | Channel organic N concentration (ppm) |
| OPCO | Channel organic P concentration (ppm) |
| rs1 | Local algal settling rate in the reach at 20º C (m/day).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of RS1 are converted to m/hr by the model. Values for RS1 should fall in the range 0.15 to 1.82 m/day. If no value for RS1 is entered, the model sets RS1 = 1.0 m/day.  Required if in-stream nutrient cycling is being modeled. |
| rs2 | Benthic (sediment) source rate for dissolved phosphorus in the reach at 20º C (mg dissolved P/(m2·day)).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of RS2 are converted to mg dissolved P/(m2·hr) by the model. If no value for RS2 is entered, the model sets RS2 = 0.05 mg dissolved P/(m2·day).  Required if in-stream nutrient cycling is being modeled. |
| rs3 | Benthic source rate for NH4-N in the reach at 20º C (mg NH4-N/(m2·day)).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of RS3 are converted to mg NH4-N/(m2·hr) by the model. If no value for RS3 is entered, the model sets RS3 = 0.5 mg NH4-N/(m2·day).  Required if in-stream nutrient cycling is being modeled. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| rs4 | Rate coefficient for organic N settling in the reach at 20º C (day-1).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of RS4 are converted to hr-1 by the model. Values for RS4 should fall in the range 0.001 to 0.10 day-1. If no value for RS4 is entered, the model sets RS4 = 0.05 day-1.  Required if in-stream nutrient cycling is being modeled. |
| rs5 | Organic phosphorus settling rate in the reach at 20º C (day-1).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of RS5 are converted to hr-1 by the model. Values for RS5 should fall in the range 0.001 to 0.1 day-1. If no value for RS5 is entered, the model sets RS5 = 0.05 day-1.  Required if in-stream nutrient cycling is being modeled. |
| rs6 | Rate coefficient for settling of arbitrary non-conservative constituent in the reach at 20º C (day-1).  If no value for RS6 is entered, the model sets RS6 = 2.5.  *Not currently used by the model*. |
| rs7 | Benthic source rate for arbitrary non-conservative constituent in the reach at 20º C (mg ANC/(m2·day)).  If no value for RS7 is entered, the model sets RS7 = 2.5.  *Not currently used by the model*. |
| rk1 | Carbonaceous biological oxygen demand deoxygenation rate coefficient in the reach at 20º C (day-1).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of RK1 are converted to hr-1 by the model. Values for RK1 should fall in the range 0.02 to 3.4 day-1. If no value for RK1 is entered, the model sets RK1 = 1.71 day-1.  Required if in-stream nutrient cycling is being modeled. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| rk2 | Oxygen reaeration rate in accordance with Fickian diffusion in the reach at 20º C (day-1).  Numerous methods have been developed to calculate the reaeration rate at 20°C, κ2,20. A few of the methods are listed below. Brown and Barnwell (1987) provide additional methods.  Using field measurements, Churchill, Elmore and Buckingham (1962) derived the relationship:    where κ2,20 is the reaeration rate at 20°C (day-1),  is the average stream velocity (m/s), and depth is the average stream depth (m).  O’Connor and Dobbins (1958) incorporated stream turbulence characteristics into the equations they developed. For streams with low velocities and isotropic conditions,    where *κ*2,20 is the reaeration rate at 20°C (day-1), *Dm* is the molecular diffusion coefficient (m2/day),  is the average stream velocity (m/s), and *depth* is the average stream depth (m). For streams with high velocities and nonisotropic conditions,    where *κ*2,20 is the reaeration rate at 20°C (day-1), *Dm* is the molecular diffusion coefficient (m2/day), *slp* is the slope of the streambed (m/m), and *depth* is the average stream depth (m). The molecular diffusion coefficient is calculated    where *Dm* is the molecular diffusion coefficient (m2/day), and  is the average water temperature (°C). |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| rk2, cont. | Owens et al. (1964) developed an equation to determine the reaeration rate for shallow, fast moving streams where the stream depth is 0.1 to 3.4 m and the velocity is 0.03 to 1.5 m/s.    where *κ*2,20 is the reaeration rate at 20°C (day-1),  is the average stream velocity (m/s), and *depth* is the average stream depth (m).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of RK2 are converted to hr-1 by the model. Values for RK2 should fall in the range 0.01 to 100.0 day-1. If no value for RK2 is entered, the model sets RK2 = 50.0 day-1.  Required if in-stream nutrient cycling is being modeled. |
| rk3 | Rate of loss of carbonaceous biological oxygen demand due to settling in the reach at 20º C (day-1).  Values for RK3 should fall in the range -0.36 to 0.36 day-1. The recommended default for RK3 is 0.36 day-1 (not set by model).  Required if in-stream nutrient cycling is being modeled. |
| rk4 | Benthic oxygen demand rate in the reach at 20º C (mg O2/(m2·day)).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of RK4 are converted to (mg O2/(m2·hr)) by the model. If no value for RK4 is entered, the model sets RK4 = 2.0 mg O2/(m2·day).  Required if in-stream nutrient cycling is being modeled. |
| rk5 | Coliform die-off rate in the reach at 20º C (day-1).  Values for RK5 should fall in the range 0.05 to 4.0. If no value for RK5 is entered, the model sets RK5 = 2.0.  *Not currently used by the model*. |
| rk6 | Decay rate for arbitrary non-conservative constituent in the reach at 20º C (day-1).  If no value for RK6 is entered, the model sets RK6 = 1.71.  *Not currently used by the model*. |

|  |  |  |  |
| --- | --- | --- | --- |
| **Variable name** | | **Definition** | |
| bc1 | | Rate constant for biological oxidation of NH4 to NO2 in the reach at 20º C in well-aerated conditions (day-1).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of BC1 are converted to hr-1 by the model. Values for BC1 should fall in the range 0.1 to 1.0 day-1. If no value for BC1 is entered, the model sets BC1 = 0.55 day-1.  Required if in-stream nutrient cycling is being modeled. | |
| bc2 | | Rate constant for biological oxidation of NO2 to NO3 in the reach at 20º C in well-aerated conditions (day-1).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of BC2 are converted to hr-1 by the model. Values for BC2 should fall in the range 0.2 to 2.0 day-1. If no value for BC2 is entered, the model sets BC2 = 1.1 day-1.  Required if in-stream nutrient cycling is being modeled. | |
| bc3 | | Rate constant for hydrolysis of organic N to NH4 in the reach at 20º C (day-1).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of BC3 are converted to hr-1 by the model. Values for BC3 should fall in the range 0.2 to 0.4 day-1. If no value for BC3 is entered, the model sets BC3 = 0.21 day-1.  Required if in-stream nutrient cycling is being modeled. | |
| bc4 | | Rate constant for mineralization of organic P to dissolved P in the reach at 20º C (day-1).  If routing is performed on an hourly time step (see IEVENT in .bsn file), the units of BC4 are converted to hr-1 by the model. Values for BC4 should fall in the range 0.01 to 0.70 day-1. If no value for BC4 is entered, the model sets BC4 = 0.35 day-1.  Required if in-stream nutrient cycling is being modeled. | |
| LAO | | Qual2E light averaging option. Qual2E defines four light averaging options.Depth-averaged algal growth attenuation factor for light (FL) is computed from one daylight average solar radiation value calculated in the steady state temperature heat balance.FL is computed from one daylight average solar radiation value supplied by the user.FL is obtained by averaging the hourly daylight values of FL computed from the hourly daylight values of solar radiation calculated in the steady state temperature heat balance.FL is obtained by averaging the hourly daylight values of FL computed from the hourly daylight values of solar radiation calculated from a single value of total daily, photosynthetically active, solar radiation and an assumed cosine function.The only option currently active in SWAT is 2.Required if in-stream nutrient cycling is being modeled. | |
| IGROPT | | Qual2E algal specific growth rate option. Qual2E provides three different options for computing the algal growth rate.  1. Multiplicative: the effects of nitrogen, phosphorus and light are multiplied together to calculate the net effect on the local algal growth rate 2. Limiting nutrient: the local algal growth rate is limited by light and one of the nutrients (nitrogen or phosphorus) 3. Harmonic mean: the local algal growth rate is limited by light and the harmonic mean of the nutrient interactions | |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| IGROPT, cont. | The multiplicative option multiplies the growth factors for light, nitrogen and phosphorus together to determine their net effect on the local algal growth rate. This option has its biological basis in the mutiplicative effects of enzymatic processes involved in photosynthesis. The limiting nutrient option calculates the local algal growth rate as limited by light and either nitrogen or phosphorus. The nutrient/light effects are multiplicative, but the nutrient/nutrient effects are alternate. The algal growth rate is controlled by the nutrient with the smaller growth limitation factor. This approach mimics Liebig’s law of the minimum.  The harmonic mean is mathematically analogous to the total resistance of two resistors in parallel and can be considered a compromise between the multiplicative and limiting nutrient options. The algal growth rate is controlled by a multiplicative relation between light and nutrients, while the nutrient/nutrient interactions are represented by a harmonic mean. The default option is the limiting nutrient option (2).Required if in-stream nutrient cycling is being modeled. |
| ai0 | Ratio of chlorophyll-a to algal biomass (μg-chla/mg algae).Values for AI0 should fall in the range 10-100. If no value for AI0 is entered, the model will set AI0 = 50.0.Required if in-stream nutrient cycling is being modeled. |
| ai1 | Fraction of algal biomass that is nitrogen (mg N/mg alg).Values for AI1 should fall in the range 0.07-0.09. If no value for AI1 is entered, the model will set AI1 = 0.08.Required if in-stream nutrient cycling is being modeled. |
| ai2 | Fraction of algal biomass that is phosphorus (mg P/mg alg).Values for AI2 should fall in the range 0.01-0.02. If no value for AI2 is entered, the model will set AI2 = 0.015.Required if in-stream nutrient cycling is being modeled. |
| ai3 | The rate of oxygen production per unit of algal photosynthesis (mg O2/mg alg).Values for AI3 should fall in the range 1.4-1.8. If no value for AI3 is entered, the model will set AI3 = 1.6.Required if in-stream nutrient cycling is being modeled. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| ai4 | The rate of oxygen uptake per unit of algal respiration (mg O2/mg alg).Values for AI4 should fall in the range 1.6-2.3. If no value for AI4 is entered, the model will set AI4 = 2.0.Required if in-stream nutrient cycling is being modeled. |
| ai5 | The rate of oxygen uptake per unit of NH3-N oxidation (mg O2/mg NH3-N).Values for AI5 should fall in the range 3.0-4.0. If no value for AI5 is entered, the model will set AI5 = 3.5.Required if in-stream nutrient cycling is being modeled. |
| ai6 | The rate of oxygen uptake per unit of NO2-N oxidation (mg O2/mg NO2-N).Values for AI6 should fall in the range 1.00-1.14. If no value for AI6 is entered, the model will set AI6 = 1.07.Required if in-stream nutrient cycling is being modeled. |
| mumax | Maximum specific algal growth rate at 20º C (day-1).If routing is performed on an hourly time step (see IEVENT in .bsn file), MUMAX is converted to (hr-1) by the model. Values for MUMAX should fall in the range 1.0-3.0. If no value for MUMAX is entered, the model will set MUMAX = 2.0.Required if in-stream nutrient cycling is being modeled. |
| rhoq | Algal respiration rate at 20º C (day-1).If routing is performed on an hourly time step (see IEVENT in .bsn file), RHOQ is converted to (hr-1) by the model. Values for RHOQ should fall in the range 0.05-0.50. If no value for RHOQ is entered, the model will set RHOQ = 0.30.Required if in-stream nutrient cycling is being modeled. |
| tfact | Fraction of solar radiation computed in the temperature heat balance that is photosynthetically active.Values for TFACT should fall in the range 0.01-1.0. If no value for TFACT is entered, the model will set TFACT = 0.3.Required if in-stream nutrient cycling is being modeled. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| k\_l | Half-saturation coefficient for light (kJ/(m2·min)). Values for K\_L should fall in the range 0.2227-1.135. If no value for K\_L is entered, the model will set K\_L = 0.75.  Required if in-stream nutrient cycling is being modeled. |
| k\_n | Michaelis-Menton half-saturation constant for nitrogen (mg N/L).The Michaelis-Menton half-saturation constant for nitrogen and phosphorus define the concentration of N or P at which algal growth is limited to 50% of the maximum growth rate.Typical values for *KN* range from 0.01 to 0.30 mg N/L. Values for K\_N should fall in the range 0.01-0.30. If no value for K\_N is entered, the model will set K\_N = 0.02.Required if in-stream nutrient cycling is being modeled. |
| k\_p | Michaelis-Menton half-saturation constant for phosphorus (mg P/L).The Michaelis-Menton half-saturation constant for nitrogen and phosphorus define the concentration of N or P at which algal growth is limited to 50% of the maximum growth rate.Typical values for *KP* will range from 0.001 to 0.05 mg P/L. If no value for K\_P is entered, the model will set K\_P = 0.025.Required if in-stream nutrient cycling is being modeled. |
| lambda0 | Non-algal portion of the light extinction coefficient (m-1).The light extinction coefficient, , is calculated as a function of the algal density using the nonlinear equation:   where  is the non-algal portion of the light extinction coefficient (m-1),  is the linear algal self shading coefficient (m-1 (μg-chla/L)-1),  is the nonlinear algal self shading coefficient (m-1 (μg-chla/L)-2/3), *α*0 is the ratio of chlorophyll *a* to algal biomass (μg chla/mg alg), and *algae* is the algal biomass concentration (mg alg/L). |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| lambda0, cont. | This equation allows a variety of algal, self-shading, light extinction relationships to be modeled. When , no algal self-shading is simulated. When  and , linear algal self-shading is modeled. When  and  are set to a value other than 0, non-linear algal self-shading is modeled. The Riley equation (Bowie et al., 1985) defines  and .  If no value for LAMBDA0 is entered, the model will set LAMBDA0 = 1.0.  Required if in-stream nutrient cycling is being modeled. |
| lambda1 | Linear algal self-shading coefficient (m-1·(μg chla/L)-1).See explanation for LAMBDA0 for more information on this variable.Values for LAMBDA1 should fall in the range 0.0065-0.065. If no value for LAMBDA1 is entered, the model will set LAMBDA1 = 0.03.Required if in-stream nutrient cycling is being modeled. |
| lambda2 | Nonlinear algal self-shading coefficient (m-1·(μg chla/L)-2/3). See explanation for LAMBDA0 for more information on this variable. The recommended value for LAMBDA2 is 0.0541. If no value for LAMBDA2 is entered, the model will set LAMBDA2 = 0.054.Required if in-stream nutrient cycling is being modeled. |
| p\_n | Algal preference factor for ammonia.Values for P\_N should fall in the range 0.01-1.0. If no value for P\_N is entered, the model will set P\_N = 0.5.Required if in-stream nutrient cycling is being modeled. |

**pesticide.cha**

The pesticide.cha file contains the input variables for the nutrients of a channel. Below is a sample partial pesticide.cha file:

pesticide.cha: Pesticide channel properties - LREW Subbasin March 2016

CHA\_PST\_NAME PST\_REAC PST\_VOLAT PST\_KOC PST\_MIX PST\_RSP PST\_STL SEDPST\_ACT SEDPST\_BUR

null 0.007 0.010 0.000 0.001 0.000 1.000 0.030 0.002

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | This line is reserved for the pesticide section title. This line is not processed by the model and may be left blank. |
| Header | Headings |
| name | Name of the pesticide channel |
| PST\_REA | Pesticide reaction coefficient in reach (day-1).  The rate constant is related to the aqueous half-life:    where *kp,aq* is the rate constant for degradation or removal of pesticide in the water (1/day), and *t*1/2,*aq* is the aqueous half-life for the pesticide (days).  If no value for CHPST\_REA is entered, the model will set CHPST\_REA = 0.007 day-1.  Required if in-stream pesticide cycling is being modeled. |
| PST\_VOL | Pesticide volatilization coefficient in reach (m/day).  The volatilization mass-transfer coefficient can be calculated based on Whitman’s two-film or two-resistance theory (Whitman, 1923; Lewis and Whitman, 1924 as described in Chapra, 1997). While the main body of the gas and liquid phases are assumed to be well-mixed and homogenous, the two-film theory assumes that a substance moving between the two phases encounters maximum resistance in two laminar boundary layers where transfer is a function of molecular diffusion. In this type of system the transfer coefficient or velocity is:    where *vv* is the volatilization mass-transfer coefficient (m/day), *Kl* is the mass-transfer velocity in the liquid laminar layer (m/day), *Kg* is the mass-transfer velocity in the gaseous laminar layer (m/day), *He* is Henry’s constant (atm m3 mole-1), *R* is the universal gas constant (8.206 × 10-5 atm m3 (K mole)-1), and *TK* is the temperature (K).  For rivers where liquid flow is turbulent, the transfer coefficients are estimated using the surface renewal theory (Higbie, 1935; Danckwerts, 1951; as described by Chapra, 1997). The surface renewal model visualizes the system as |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| pst\_VOL, cont. | consisting of parcels of water that are brought to the surface for a period of time. The fluid elements are assumed to reach and leave the air/water interface randomly, i.e. the exposure of the fluid elements to air is described by a statistical distribution. The transfer velocities for the liquid and gaseous phases are calculated:    where *Kl* is the mass-transfer velocity in the liquid laminar layer (m/day), *Kg* is the mass-transfer velocity in the gaseous laminar layer (m/day), *Dl* is the liquid molecular diffusion coefficient (m2/day), *Dg* is the gas molecular diffusion coefficient (m2/day), *rl* is the liquid surface renewal rate (1/day), and *rg* is the gaseous surface renewal rate (1/day).  O’Connor and Dobbins (1956) defined the surface renewal rate as the ratio of the average stream velocity to depth.    where *rl* is the liquid surface renewal rate (1/day), *vc* is the average stream velocity (m/s) and *depth* is the depth of flow (m).  If no value for CHPST\_VOL is entered, the model will set CHPST\_VOL = 0.01.  Required if in-stream pesticide cycling is being modeled. |
| pst\_koc | Pesticide partition coefficient between water and sediment in reach (m3/g).  The pesticide partition coefficient can be estimated from the octanol-water partition coefficient (Chapra, 1997):    where *Kd* is the pesticide partition coefficient (m3/g) and *Kow* is the pesticide’s octanol-water partition coefficient (). |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| pst\_koc | Values for the octanol-water partition coefficient have been published for many chemicals. If a published value cannot be found, it can be estimated from solubility (Chapra, 1997):    where  is the pesticide solubility (μmoles/L). The solubility in these units is calculated:    where  is the pesticide solubility (μmoles/L), *pstsol* is the pesticide solubility (mg/L) and *MW* is the molecular weight (g/mole).  If no value for CHPST\_KOC is entered, the model will set CHPST\_KOC = 0.  Required if in-stream pesticide cycling is being modeled. |
| PST\_MIX | Mixing velocity (diffusion/dispersion) for pesticide in reach (m/day).  The diffusive mixing velocity, vd, can be estimated from the empirically derived formula (Chapra, 1997):    where vd is the rate of diffusion or mixing velocity (m/day), φ is the sediment porosity, and MW is the molecular weight of the pesticide compound.  If no value for CHPST\_MIX is entered, the model will set CHPST\_MIX = 0.001.  Required if in-stream pesticide cycling is being modeled. |
| pst\_RSP | Resuspension velocity for pesticide sorbed to sediment (m/day).  If no value for CHPST\_RSP is entered, the model will set CHPST\_RSP = 0.002.  Required if in-stream pesticide cycling is being modeled. |
| pst\_stl | Settling velocity for pesticide sorbed to sediment (m/day).  If no value for CHPST\_STL is entered, the model will set CHPST\_STL = 1.0.  Required if in-stream pesticide cycling is being modeled. |
| sedpst\_ACT | Depth of active sediment layer for pesticide (m).  If no value for SEDPST\_ACT is entered, the model will set SEDPST\_ACT = 0.03.  Required if in-stream pesticide cycling is being modeled. |
| sedpst\_bry | Pesticide burial velocity in reach bed sediment (m/day).  If no value for SEDPST\_BRY is entered, the model will set SEDPST\_BRY = 0.002.  Required if in-stream pesticide cycling is being modeled. |
| SEDPST\_CONC | Initial pesticide concentration in reach bed sediment (mg/m3 sediment).  We recommend using a 1 year equilibration period for the model where the watershed simulation is set to start 1 year prior to the period of interest. This allows the model to get the water cycling properly before any comparisons between measured and simulated data are made. When an equilibration period is incorporated, the value for SEDPST\_CONC is not going to be important if a pesticide with a short half-life is being modeled. For pesticides with a long half-life, this variable is important.  Required if in-stream pesticide cycling is being modeled. |
| sedpst\_rea | Pesticide reaction coefficient in reach bed sediment  (day-1).  The rate constant is related to the sediment half-life:    where *kp,sed* is the rate constant for degradation or removal of pesticide in the sediment (1/day), and *t*1/2,*sed* is the sediment half-life for the pesticide (days).  If no value for SEDPST\_REA is entered, the model will set SEDPST\_REA = 0.05.  Required if in-stream pesticide cycling is being modeled. |

**channel-lte.cha**

The channel-lte.cha file contains the input variables for the nutrients of a channel. Below is a sample channel-lte.cha file:

Channel-lte.cha

NAME ORDER RTE\_DB CHW CHD CHS CHL CHN CHK CHEROD COV HC\_COV CHSEQ D50 CLAY BD

1st\_stage ditch 1 4.0 0.50 0.005 0.6 0.10 1 0.01 0.005 6 0.001 12 30.0 1.5 Gully\_hru2 gully 1 5.5 0.71 0.007 8 0.05 1 0.01 0.005 6 0.001 12 30.0 1.5

|  |  |  |
| --- | --- | --- |
| **Variable name** | **Definition** | |
| TITLE | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. | |
| header | Headers for the channel-lte file. | |
| NAME | Name of the nutrients channel | |
| ORDER |  | |
| ROUTE\_DB | Pointer to routing\_nut\_data (nutrients.cha) | |
| CHw | | Average width of main channel at top of bank (m).  Required. |
| CHD | | Depth of main channel from top of bank to bottom (m).  Required. |
| CHS | | Average slope of main channel along the channel length (m/m).  Required. |
| CHL | | Length of main channel (km).  Required. |
| CHN | | Manning’s “n” value for the main channel.  Required. |

Table 25-1: Values of Manning’s roughness coefficient, *n*, for channel flow (Chow, 1959).1

|  |  |  |
| --- | --- | --- |
| **Characteristics of Channel** | **Median** | **Range** |
| Excavated or dredged |  |  |
| Earth, straight and uniform | 0.025 | 0.016-0.033 |
| Earth, winding and sluggish | 0.035 | 0.023-0.050 |
| Not maintained, weeds and brush | 0.075 | 0.040-0.140 |
| Natural streams |  |  |
| Few trees, stones or brush | 0.050 | 0.025-0.065 |
| Heavy timber and brush | 0.100 | 0.050-0.150 |

1 Chow (1959) has a very extensive list of Manning’s roughness coefficients. These values represent only a small portion of those he lists in his book.

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| CHK | Effective hydraulic conductivity in main channel alluvium (mm/hr).  Required.  Streams may be categorized by their relationship to the groundwater system. A stream located in a discharge area that receives groundwater flow is a gaining or effluent stream (Figure 25-1a). This type of stream is characterized by an increase in discharge downstream. A stream located in a recharge area is a losing or influent stream. This type of stream is characterized by a decrease in discharge downstream. A losing stream may be connected to (Figure 25-1b) or perched above (Figure 25-1c) the groundwater flow area. A stream that simultaneously receives and loses groundwater is a flow-through stream (Figure 25-1d). |

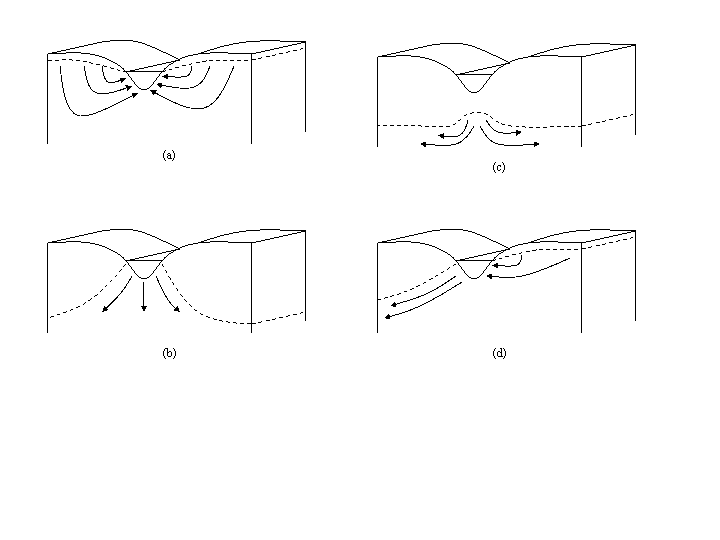


Figure 25-1: Stream-groundwater relationships: a) gaining stream receiving water from groundwater flow; b) losing stream connected to groundwater system; c) losing stream perched above groundwater system; and d) flow-through stream (After Dingman, 1994).

Typical values for *Kch* for various alluvium materials are given in Table 25-2. For perennial streams with continuous groundwater contribution, the effective conductivity will be zero.

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| CHK cont. |  |

Table 25-2: Example hydraulic conductivity values for various bed materials (from Lane, 1983).

|  |  |  |
| --- | --- | --- |
| **Bed material group** | **Bed material characteristics** | **Hydraulic conductivity** |
| 1  Very high loss rate | Very clean gravel and large sand | > 127 mm/hr |
| 2  High loss rate | Clean sand and gravel, field conditions | 51-127 mm/hr |
| 3  Moderately high loss rate | Sand and gravel mixture with low silt-clay content | 25-76 mm/hr |
| 4  Moderate loss rate | Sand and gravel mixture with high silt-clay content | 6-25 mm/hr |
| 5  Insignificant to low loss rate | Consolidated bed material; high silt-clay content | 0.025-2.5 mm/hr |
| CHEROD | CHEROD is set to a value between 0.0 and 1.0. A value of 0.0 indicates a non-erosive channel while a value of 1.0 indicates no resistance to erosion. | | |
| COV | If CH\_EQ is 0 the  CH\_COV1 – Channel erodibility factor.  0 = non-erosive channel  1 = no resistance to erosion  The channel erodibility factor is conceptually similar to the soil erodibility factor used in the USLE equation. Channel erodibility is a function of properties of the bed or bank materials.  If CH\_EQN ≠ 0:  Channel bank vegetation coefficient for critical shear stress (Julian and Torres, 2006)   |  |  | | --- | --- | | Bank Vegetation | CH\_cov1 | | None | 1.00 | | Grassy | 1.97 | | Sparse trees | 5.40 | | Dense trees | 19.20 |   Required. | | |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| hc\_cov | Head cut cover factor |
| CHseq | Equilibrium channel slope (m/m) |
| D50 | Channel median sediment size (%) |
| CLAY | Clay percent of bank and bed (%) |
| BD | Dry bulk density (t/m3) |
| CHsS | Channel side slope |
| BEDLDCOEF | Percent of sediment entering the channel that is bed material |
| TC | Time of concentration |
| SHEAR\_BNK | Bank shear coefficient – fraction of bottom shear |
| HC\_KH | Headcut erodibility |
| HC\_hgt | Headcut height (m) |
| HC\_INI | Initial channel length for gullies (km) |

**RESERVOIR –** The reservoir section of file.cio contains the filenames for simulation of a reservoirs in the model. Reservoirs are impoundments located on the main channel network of the watershed. Reservoirs receive loadings from all upstream subbasins. The reservoir input file (.res) contains input data to simulate water and sediment processes.

**initial.res**

The initial.res file contains the input variables for the initialization of a channel. Below is a sample partial initial.res file:

initial.res: Reservoir data file - asdf;lj

NAME VOL SED ORGN NO3 NO2 NH3 ORGP SOLP SECI SAN SIL CLA SAG LAG

reservoir001 0.90 200.00 10.00 2.00 0.20 0.10 1.00 0.10 1.00 0.00 1.00 9.00 0.00 0.00

|  |  |  |
| --- | --- | --- |
| **Variable name** | | **Definition** |
| Title | | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | | Headers for the initial\_res file. |
| name | | Initial name of the reservoir |
| VOL | | Initial reservoir volume.  If the reservoir is in existence at the beginning of the simulation period, the initial reservoir volume is the volume on the first day of simulation. If the reservoir begins operation in the midst of a SWAT simulation, the initial reservoir volume is the volume of the reservoir the day the reservoir becomes operational (104 m3). |
| SED | | Initial sediment concentration in the reservoir (mg/L).  If the reservoir is in existence at the beginning of the simulation period, the initial sediment concentration is the concentration on the first day of simulation. If the reservoir begins operation in the midst of a SWAT simulation, the initial sediment concentration is the concentration the day the reservoir becomes operational (mg/L). | |
| ORGN | | Amount of organic N in reservoir | |
| NO3 | | Initial concentration of NO3-N in reservoir (mg N/L). | |
| NO2 | | Initial concentration of NO2-N in reservoir (mg N/L). | |
| NH3 | | Initial concentration of NH3-N (ammonia) in reservoir (mg N/L). | |
| ORGP | | Initial concentration of organic P in reservoir (mg P/L).  We recommend using a 1 year equilibration period for the model where the watershed simulation is set to start 1 year prior to the period of interest. This allows the model to get the water cycling properly before any comparisons between measured and simulated data are made. When an equilibration period is incorporated, the value for ORGP is not going to be important if the reservoir is in operation at the beginning of the simulation. However, if the reservoir starts operation in the middle of a simulation, this value needs to be reasonably accurate. | |
| SOLP | | Amount of soluble phosphorus in the reservoir  (read in as mg/L and converted to kg/L)  See comment for ORGP. | |
| SECI | | Secchi-disk depth(m) | |
| SAN | | Amount of sand in the reservoir  (read in as mg/L and converted to kg/L) | |
| SIL | | Amount of silt in the reservoir  (read in as mg/L and converted to kg/L) | |
| CLA | | Amount of clay in the reservoir  (read in as mg/L and converted to kg/L) | |
| SAG | | Amount of small aggregates in the reservoir  (read in as mg/L and converted to kg/L) | |
| LAG | | Amount of large aggregates in the reservoir  (read in as mg/L and converted to kg/L) | |
| GRA | | Amount of gravel in the reservoir  (read in as mg/L and converted to kg/L) | |
| CHLA | | Amount of chlorophyll-s in the reservoir  (read in as mg/L and converted to kg/L) | |
| PSOL | | Amount of pest in res (read inas mg/L and converted to kg/L) | |
| PSOR | | Amount of pest in res (read inas mg/L and converted to kg/L) | |
| BACTLP | | Less persistent bacteria stored in the reservoir  (# cfu/100ml) | |
| BACTP | | Persistent bacteria stored in the reservoir  (# cfu/100ml) | |

**reservoir.res**

The reservoir input file (.res) contains input data to simulate water and sediment processes while the lake water quality file (.lwq) contains input data to simulate nutrient and pesticide cycling in the water body.

Below is a sample RESERVOIR.res file:

reservoir.res: Reservoir properties - Water\_LS2\_Take2

NUMB NAME INI HYD RELEASE \_SED NUT PST

1 pnd1 res001 pnd1 corps\_med\_res res001 res001 res001

2 pnd2 res001 pnd2 corps\_med\_res res001 res001 res001

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| HEADER | Headers for the reservoir.res file. |
| Numb | The number of the reservoir |
| NAME | The name of the reservoir |
| variable name | The initial data points to ‘initial.res’ file. |
| INIT | The initial data points to ‘initial.res’ file. |
| HYD | Hydraulic conductivity of the reservoir bottom (mm/hr).  If seepage occurs in the water body, the hydraulic conductivity must be set to a value other than 0.  Required. |
| RELEASE | Average daily principal spillway release rate (m3/s).  The name for this variable is slightly misleading. SWAT uses this variable when the volume of water in the reservoir is between the principal and emergency spillway volumes. If the amount of water exceeding the principal spillway volume can be released at a rate ≤ REL, than all of the water volume in excess of the principal spillway volume is released. Otherwise the release rate, REL is used. |

|  |  |
| --- | --- |
| SED | Initial sediment concentration in the reservoir (mg/L).  If the reservoir is in existence at the beginning of the simulation period, the initial sediment concentration is the concentration on the first day of simulation. If the reservoir begins operation in the midst of a SWAT simulation, the initial sediment concentration is the concentration the day the reservoir becomes operational (mg/L).  Required. |
| NUT | Nutrient inputs points to ‘nutrients.res’ file |
| PST | Pesticide inputs points to ‘pesticide.res’ file |

**hydrology.res**

Reservoirs are impoundments located on the main channel network of the watershed. Reservoirs receive loadings from all upstream subbasins. The reservoir input file (.res) contains input data to simulate water and sediment processes while the lake water quality file (.lwq) contains input data to simulate nutrient and pesticide cycling in the water body.

Below is a sample HYDROLOGY.res file:

hydrology.res: Reservoir properties - asdf;lj

NAME IYRES MORES PSA PVOL ESA EVOL K ENRSV BR1 BR2

reservoir001 0 0 120.00 60.00 400.00 150.00 0.50 0.80 0.00 0.00

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| HEADER | Headers for the hydrology.res file. |
| nAME | The name of the reservoir |
| iYRES | Year the reservoir became operational (eg 1980).  If 0 is input for MORES and IYRES, the model assumes the reservoir is in operation at the beginning of the simulation.  Required. |
| MORES | Month the reservoir became operational (0-12).  If 0 is input for MORES and IYRES, the model assumes the reservoir is in operation at the beginning of the simulation.  Required. |
| PSA | Reservoir surface area when the reservoir is filled to the principal spillway (ha).  See comment for ESA.  Required. |

|  |  |
| --- | --- |
| PVOL | Volume of water needed to fill the reservoir to the principal spillway (104 m3).See comment for RES\_ESA.Required. |
| ESA | Reservoir surface area when the reservoir is filled to the emergency spillway (ha).  For SWAT to calculate the reservoir surface area each day the surface area at two different water volumes must to be defined. Variables referring to the principal spillway can be thought of as variables referring to the normal reservoir storage volume while variables referring to the emergency spillway can be thought of as variables referring to maximum reservoir storage volume.  Required. |
| EVOL | Volume of water needed to fill the reservoir to the emergency spillway (104 m3).  See comment for RES\_ESA.  Required. |
| k | Hydraulic conductivity of the reservoir bottom (mm/hr).  If seepage occurs in the water body, the hydraulic conductivity must be set to a value other than 0.  Required. |
| EvRSV | Lake evaporation coefficient.  Default = 0.6 Required. |
| BR1 | Vol\_surface area coefficient for reservoirs (model estimates if zero) |
| BR2 | Vol\_surface area coefficient for reservoirs (model estimates if zero) |

**nutrients.res**

While water quality is a broad subject, the primary areas of concern are nutrients, organic chemicals—both agricultural (pesticide) and industrial, heavy metals, bacteria and sediment levels in streams and large water bodies. SWAT is able to model processes affecting nutrient, pesticide and sediment levels in the main channels and reservoirs.

Below is a sample partial NUTRIENTS.res file:

nutrients.res: Reservoir nutrient inputs

NAME IRES1 IRES2 NSETLR1 NSETLR2 PSETLR1 PSETLR2 CHLAR SECCIR THETA\_N THETA\_P CONC\_NMIN

reservoir001 4 10 0.50 2.00 1.00 0.50 1.00 1.00 1.00 1.00 0.10

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the nutrients.res file. |
| name | The name of the reservoir |
| IRES1 | Beginning month of mid-year nutrient settling period.  The model allows the user to define two settling rates for each nutrient and the time of the year during which each settling rate is used. A variation in settling rates is allowed so that impact of temperature and other seasonal factors may be accounted for in the modeling of nutrient settling. To use only one settling rate for the entire year, both variables for the nutrient may be set to the same value. Setting all variables to zero will cause the model to ignore settling of nutrients in the water body.  Required. |

|  |  |
| --- | --- |
| Ires2 | Ending month of mid-year nutrient settling period.  See comment for IRES1.  Required. |
| NSETLR1 | Nitrogen settling rate in reservoir for months IRES1 through IRES2 (m/year).  See explanation for PSETLR1 for more information about this parameter.  Required if nutrient cycling is being modeled. |
| Nsetlr2. | Nitrogen settling rate in reservoir for months other than IRES1-IRES2 (m/year).  See explanation for PSETLR1 for more information about this parameter.  Required if nutrient cycling is being modeled. |
| pSETLr1 | Phosphorus settling rate in reservoir for months IRES1 through IRES2 (m/year).  The apparent settling velocity is most commonly reported in units of m/year and this is how the values are input to the model. For natural lakes, measured phosphorus settling velocities most frequently fall in the range of 5 to 20 m/year although values less than 1 m/year to over 200 m/year have been reported (Chapra, 1997). Panuska and Robertson (1999) noted that the range in apparent settling velocity values for man-made reservoirs tends to be significantly greater than for natural lakes. Higgins and Kim (1981) reported phosphorus apparent settling velocity values from –90 to 269 m/year for 18 reservoirs in Tennessee with a median value of 42.2 m/year. For 27 Midwestern reservoirs, Walker and Kiihner (1978) reported phosphorus apparent settling velocities ranging  from –1 to 125 m/year with an average value of 12.7 m/year. A negative settling rate indicates that the reservoir sediments are a source of N or P; a positive settling rate indicates that the reservoir sediments are a sink for N or P.  Table 30-1 summarizes typical ranges in phosphorus settling velocity for different systems.  Required if nutrient cycling is being modeled. |
|  | Table 30-1: Recommended apparent settling velocity values for phosphorus (Panuska and Robertson, 1999)   |  |  | | --- | --- | | **Nutrient Dynamics** | Range in settling velocity values (m/year) | | Shallow water bodies with high net internal phosphorus flux | ν ≤ 0 | | Water bodies with moderate net internal phosphorus flux | 1 < ν < 5 | | Water bodies with minimal net internal phosphorus flux | 5 < ν < 16 | | Water bodies with high net internal phosphorus removal | ν > 16 | |
| PSETLr2 | Phosphorus settling rate in reservoir for months other than IRES1-IRES2 (m/year).  See explanation for PSETLR1 for more information about this parameter.  Required if nutrient cycling is being modeled. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Chlar | Chlorophyll *a* production coefficient for reservoir.  Chlorophyll *a* concentration in the reservoir is calculated from the total phosphorus concentration. The equation assumes the system is phosphorus limited. The chlorophyll *a* coefficient was added to the equation to allow the user to adjust results to account for other factors not taken into account by the basic equation such as nitrogen limitations.  The default value for CHLAR is 1.00, which uses the original equation.  Required if nutrient cycling is being modeled. |
| seccir | Water clarity coefficient for the reservoir.  The clarity of the reservoir is expressed by the secci-disk depth (m) which is calculated as a function of chlorophyll *a*. Because suspended sediment also can affect water clarity, the water clarity coefficient has been added to the equation to allow users to adjust for the impact of factors other than chlorophyll *a* on water clarity.  The default value for SECCIR is 1.00, which uses the original equation.  Required if nutrient cycling is being modeled. |
| THETA\_N | Temperature adjustment for nitrogen loss (settling) |
| THETA\_P | Temperature adjustment for phosphorus loss (settling) |
| cONC\_NMIN | Minimum nitrogen concentration for settling (ppm) |
| CONC\_PMIN | Minimum phosphorus concentration for settling (ppm) |

**pesticide.res**

Reservoirs are impoundments located on the main channel network of the watershed. Reservoirs receive loadings from all upstream subbasins. The reservoir input file (.res) contains input data to simulate water and sediment processes while the lake water quality file (.lwq) contains input data to simulate nutrient and pesticide cycling in the water body.

Below is a sample partial PESTICIDE.res file:

pesticide.res: Reservoir pesticide inputs - asdf;lj

NAME PST\_CONC PST\_KOC PST\_MIX PST\_REA PST\_RSP PST\_STL PST\_VOL SPST\_ACT SPST\_BRY SPST\_CONC

reservoir001 0.00 0.50 0.01 0.02 0.01 0.20 0.010 0.20 0.05 0.01

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the nutrients.res file. |
| name | Reservoir pesticide Name |
| pst\_conC | Initial pesticide concentration in the Lake water for the pesticide defined by IRTPEST (mg/m3).  We recommend using a 1 year equilibration period for the model where the watershed simulation is set to start 1 year prior to the period of interest. This allows the model to get the water cycling properly before any comparisons between measured and simulated data are made. When an equilibration period is incorporated, the value for ORGP is not going to be important if the reservoir is in operation at the beginning of the simulation. However, if the reservoir starts operation in the middle of a simulation, this value needs to be reasonably accurate.  Required if pesticide cycling is being modeled. |
| pst\_koc | Pesticide partition coefficient between water and sediment (m3/g). The pesticide partition coefficient can be estimated from the octanol-water partition coefficient (Chapra, 1997):   where *Kd* is the pesticide partition coefficient (m3/g) and *Kow* is the pesticide’s octanol-water partition coefficient (). Values for the octanol-water partition coefficient have been published for many chemicals. If a published value cannot be found, it can be estimated from solubility (Chapra, 1997):   where  is the pesticide solubility (μmoles/L). The solubility in these units is calculated:    where  is the pesticide solubility (μmoles/L), *pstsol* is the pesticide solubility (mg/L) and *MW* is the molecular weight (g/mole).  PST\_KOC ranges between 10-4 to 10 m3/g. Required if pesticide cycling is being modeled. |
| PST\_MIX | Pesticide diffusion or mixing velocity (m/day) The diffusive mixing velocity, *vd*, can be estimated from the empirically derived formula (Chapra, 1997):    where *vd* is the rate of diffusion or mixing velocity (m/day), *φ* is the sediment porosity, and *MW* is the molecular weight of the pesticide compound. Required if pesticide cycling is being modeled. |
| PST\_REA | Reaction coefficient of the pesticide in lake water (day-1) The rate constant is related to the aqueous half-life:    where *kp,aq* is the rate constant for degradation or removal of pesticide in the water (1/day), and *t*1/2,*aq* is the aqueous half-life for the pesticide (days).  Required if pesticide cycling is being modeled. |
| PST\_RSP | Resuspension velocity of pesticide sorbed to sediment (m/day). Pesticide in the sediment layer is available for resuspension which transfers it back into the water. Required if pesticide cycling is being modeled. |
| pst\_stl | Settling velocity of pesticide sorbed to sediment (m/day). Pesticide in the particulate phase may be removed from the water layer by settling. Settling transfers pesticide from the water to the sediment layer. Required if pesticide cycling is being modeled. |
| pst\_vol | Volatilization coefficient of the pesticide from the lake water (m/day). The volatilization mass-transfer coefficient can be calculated based on Whitman’s two-film or two-resistance theory (Whitman, 1923; Lewis and Whitman, 1924 as described in Chapra, 1997). While the main body of the gas and liquid phases are assumed to be well-mixed and homogenous, the two-film theory assumes that a substance moving between the two phases encounters maximum resistance in two laminar boundary layers where transfer is a function of molecular diffusion. In this type of system the transfer coefficient or velocity is:   where *vv* is the volatilization mass-transfer coefficient (m/day), *Kl* is the mass-transfer velocity in the liquid laminar layer (m/day), *Kg* is the mass-transfer velocity in the gaseous laminar layer (m/day), *He* is Henry’s constant (atm m3 mole-1), *R* is the universal gas constant (8.206 × 10-5 atm m3 (K mole)-1), and *TK* is the temperature (K). For lakes, the transfer coefficients are estimated using a stagnant film approach:    where *Kl* is the mass-transfer velocity in the liquid laminar layer (m/day), *Kg* is the mass-transfer velocity in the gaseous laminar layer (m/day), *Dl* is the liquid molecular diffusion coefficient (m2/day), *Dg* is the gas molecular diffusion coefficient (m2/day), *zl* is the thickness of the liquid film (m), and *zg* is the thickness of the gas film (m).  Alternatively, the transfer coefficients can be estimated with the equations:   where *Kl* is the mass-transfer velocity in the liquid laminar layer (m/day), *Kg* is the mass-transfer velocity in the gaseous laminar layer (m/day),  is the oxygen transfer coefficient (m/day), *MW* is the molecular weight of the compound, and *μw* is the wind speed (m/s). Chapra (1997) lists several different equations that can be used to calculate .  Required if pesticide cycling is being modeled. |
| spst\_act | Depth of active sediment layer in reservoir (m).Required if pesticide cycling is being modeled. |
| spst\_bry | Burial velocity of pesticide in lake bed sediment (m/day).Pesticide in the sediment layer may be lost by burial.Required if pesticide cycling is being modeled. |
| spst\_conc | Initial pesticide concentration in the lake bed sediments. (mg/m3).We recommend using a 1 year equilibration period for the model where the watershed simulation is set to start 1 year prior to the period of interest. This allows the model to get the water cycling properly before any comparisons between measured and simulated data are made. When an equilibration period is incorporated, the value for SPST\_CONC is not going to be important if a pesticide with a short half-life is being modeled. For pesticides with a long half-life, this variable is important. Required if pesticide cycling is being modeled. |
| spst\_rea | Reaction coefficient of pesticide in reservoir bottom sediment (day-1) The rate constant is related to the sediment half-life:    where *kp,sed* is the rate constant for degradation or removal of pesticide in the sediment (1/day), and *t*1/2,*sed* is the sediment half-life for the pesticide (days). Required if pesticide cycling is being modeled. |

**sediment.res**

Reservoirs are impoundments located on the main channel network of the watershed. Reservoirs receive loadings from all upstream subbasins. The reservoir input file (.res) contains input data to simulate water and sediment processes while the lake water quality file (.lwq) contains input data to simulate nutrient and pesticide cycling in the water body. Below is a sample SEDIMENT.res file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the sediment.res file. |
| numb | The number of the reservoir |
| name | The name of the reservoir |
| nsed | Equilibrium sediment concentration in the reservoir (mg/L).The amount of suspended solid settling that occurs in the water body on a given day is calculated as a function of concentration. Settling occurs only when the sediment concentration in the water body exceeds the equilibrium sediment concentration specified by the user. Required. |
| d50 | Median particle diameter of sediment (μm).   |  |  |  | | --- | --- | --- | | **Sediment Class** | **Size (µm)** | **Approx. Size** | | Boulders | > 256,000 | > Volley ball | | Cobbles | > 64,000 | > Tennis ball | | Pebbles | > 2,000 | > Match Head | | Sand |  |  | | V. Course | 1,500 |  | | Medim | 375 |  | | V. Fine | 94 |  | | Silt |  |  | | V. Coarse | 47 |  | | Medium | 11.7 | No longer visible to the human eye | | V. Fine | 4.9 |  | | Clay | 1.95 |  |   SWAT calculates the median sediment particle diameter for impoundments located within a subbasin using the equation:    where *d*50 is the median particle size of the sediment (µm), *mc* is percent clay in the surface soil layer, *msilt* is the percent silt in the surface soil layer, *ms* is the percent sand in the surface soil layer.  Because reservoirs are located on the main channel network and receive sediment from the entire area upstream, defaulting the sand, silt, and clay fractions to those of a single subbasin or HRU in the upstream area is not appropriate. Instead the user is allowed to set the median particle size diameter to a representative value.  If no value is defined for the median particle diameter, the model will set RES\_D50 = 10 μm.  Required. |
| sed\_stlr | Sediment settling rate |
| velsetlr |  |

**weir.res**

Need this info

Below is a sample WEIR.res file:

weir.res: Reservoir weir inputs

NAME STEPS C K WID BCOEF CCOEF

shape001 24 1.00 15000.00 2.00 1.75 1.00

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the weir.res file. |
| name | The name of the reservoir |
| num\_STEPS | The number of time steps in day for weir routing |
| C | Weir discharge coefficient |
| K | Energy coefficient (broad\_crested-147,000’ sharp crested=153,000) |
| W | The width of the weir (m) |
| BCOEF | Velocity exponent coefficient for bedding material |
| CCOEF | Depth exponent coefficient for bedding material |

**wetland.wet**

Need this info

Below is a sample Wetland.wet file:

Wetland properties

NAME INI HYD RELEASE SED NUT PST

wet1 res001 pnd1 corps\_ med\_res res001 res001 res001

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the wetland.wet file. |
| name | The name of the wetland |
| init | Initial data-points to initial.res |
| hyd | Points to hydrology.res for hydrology inputs |
| release | 0 = simulated; 1 = measured outflow |
| sed | Sediment inputs-points to sediment.res |
| nut | Nutrient inputs-points to nutrient.res |
| pst | Pesticide inputs-points to pesticide.res |

**hydrology.wet**

Need this info

Below is a sample Hydrology.wet file:

hydrology.wet

NUMB NAME PSA PVOL ESA EVOL K EVRSV ACOEF BCOEF CCOEF FRAC

1 pnd1 4.95 12.25125 5.445 14.8240125 0 0.6 0 0 1 0.5

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the hydrology.wet file. |
| num | The number of the hydrology |
| nAME | The name of the hydrology |
| PSA | Fraction of hru area at principal spillway (ie: when surface inlet riser flow starts) (frac) |
| PVOL | Average depth of water at principal spillway (mm) |
| ESA | Fraction of hru area at emergency spillway (ie: when starts to spill into ditch) |
| evol | Average depth of water at emergency spillway (mm) |
| k | Hydraulic conductivity of the res bottom (mm/hr) |
| evrsv | Lake evap coeff |
| acoef | Vol-surface area coefficient for hru impoundment |
| bcoef | Vol-depth coefficient for hru impoundment |
| ccoef | Vol-depth coefficient for hru impoundment |
| frac | Fraction of hru that drains into impoundment |

**ROUTING UNIT**

**Not sure how much of this needs to remain???**

The subbasin general input file contains information related to a diversity of features within the subbasin. Data contained in the subbasin input file can be grouped into the following categories: subbasin size and location, specification of climatic data used within the subbasin, the amount of topographic relief within the subbasin and its impact on the climate, properties of tributary channels within the subbasin, variables related to climate change, the number of HRUs in the subbasin and the names of HRU input files.

**rout\_unit.def**

The rout\_unit.def file contains data that defines HRU’s in the subbasin.

Below is a sample rout\_unit.def file:

rout\_unit.def Routing definition file

NUMB NAME NSPU ELEM1 ELEM2

1 Subbasin1 2 1 -34

2 Subbasin2 2 35 -47

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The title of the rout\_unit.def file |
| header | Headers for the rout\_unit.def file. |
| name | The name of the subbasin |
| npsu | Total number of elements to follow |
| Elem1 |  |
| elem2 |  |

**rout\_unit.ele**

NEED THIS INFO

Below is a sample rout\_unit.ele file:

Rout\_unit.ele

NUMB

NAME

OBTYP

OBTYPNO

HTYP

FRAC

IDR

1

hru1

hru

1

tot

0.082

0

2

hru2

hru

2

tot

0.005

0

3

hru3

hru

3

tot

0.478

0

4

hru4

hru

4

tot

0.003

0

5

hru5

hru

5

tot

0.016

0

6

hru6

hru

6

tot

0.011

0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The title of the rout\_unit.ele file |
| header | Headers for the rout\_unit.ele file. |
| num | The number of the connect (routing) unit |
| name | The name of the connect (routing) unit |
| obtyp | Outflow object type (1=hru;2=hru\_lte,3=subbasin;5=aquifer;6=channel; 11=export coefficients; 12=delivery ratios; outlet=15) |
| obtypno | Number of HRU\_LTE’s or 1st HRU lte command. Points to the exco\_connect.dat object. |
| htyp | Hydrograph type (1=tot, 2-surface). Points to del\_ratio.dat file. |
| frac | Fraction of element in the subbasin (expansion factor -1.0 = 100%) |
| Idr | Delivery ratio through the aquifer. The subsurface flow that is delivered through the aquifer. Points to del\_ratio.dat file. |

**ROUT\_UNIT.RTU**

NEED THIS INFO

Below is a sample ROUT\_UNIT.RTU file:

rout\_unit.rtu: routing properties - LREW Subbasin March 2016

NUMB NAME ELEM\_DEF ELEM\_DR TOPOSUB\_DB FIELD\_DB

1 sub1 1 0 1 0

2 sub2 2 0 2 0

3 sub3 3 0 3 0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The title of the rout\_unit.rtu file |
| header | Headers for the rout\_unit.rtu file. |
| numB | Number of the subbasin |
| name | The name of the parm unit |
| elem\_def | Points to define.sub |
| Elem\_dr | Delivery ratio definition |
| toposub\_db | Topography link |
| field\_db | Field database definition |

**rout\_unit.dr**

NEED THIS INFO

Below is a partial sample rout\_unit.dr file:

Rout\_unit.dr

temp

flo

sed

orgn

sedp

no3

solp

psol

psor

chla

nh3

no2

cbod

0.9

0.8

0.7

0.6

0.5

0.4

3

0.2

0.1

0

0.1

0.2

0.3

0.2

0.8

0.7

0.6

0.5

0.4

3

0.2

0.1

0

0.1

0.2

0.3

0.9

0.8

0.7

0.6

0.5

0.4

3

0.2

0.1

0

0.1

0.2

0.3

0.1

0.8

0.7

0.6

0.5

0.4

3

0.2

0.1

0

0.1

0.2

0.3

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The title of the rout\_unit.dr file |
| header | Headers for the rout\_unit.dr file. |
| flo | Volume of water (m^3) |
| sed | sediment (metric tons) |
| orgn | Organic N (kg N) |
| sedp | Organic P (kg P) |
| no3 | NO3-N (kg N) |
| solp | Mineral (soluble P) (kg P) |
| psol | Pesticide in solution (mg pst) |
| psor | Pesticide sorbed to sediment (mg pst) |
| chla | Chlorophyll-a (kg) |
| nh3 | NH3 (kg N) |
| no2 | NO2 (kg N) |
| cbod | Carbonaceous biological oxygen demand (kg) |
| dox | Dissolved oxygen (kg) |
| bacp | Persistent bacteria (# cfu/100ml) |
| baclp | Less persistent bacteria (# cfu/100ml) |
| met1 | Conservative metal #1 (kg) |
| met2 | Conservative metal #2 (kg) |
| met3 | Conservative metal #3 (kg) |
| san | Detached sand (tons) |
| sil | Detached silt (tons) |
| cla | Detached clay (tons) |
| sag | Detached small ag (tons) |
| lag | Detached large ag (tons) |
| grv | gravel (tons) |
| temp | Temperature (deg c) |

**HRU –** HRU’s are now defined by weather, topography, soil, landuse, operational management, potholes, subsurface drainage, structural operations, septic systems, plant community, initial soil chemistry, pesticides, bacteria, impoundments, snow and atmospheric deposition. Each HRU points to objects in each of the associated data files. HRU’s consist of plants and soils on the landscape and now are not associated with aquifers and ponds and wetlands. HRUs are defined as contiguous areas (ie fields or grid cells) and a delivery from edge-of-field to subbasin outlet is computed in the subbasin module. This is not necessary when landscape units or grid cells are used. Several inputs for each HRU are required in addition to pointing to data files, including drainage area. These variables may be moved to a calibration file.

**HRU-DATA.HRU**

NEED THIS INFO

Below is a sample hru-data.hru file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the hru-data.hru file. |
| numb | HRU Number |
| name | Name of the HRU |
| TOPO | Topographic data (topo.dat) |
| HYD | Hydrologic data (hydrol.dat) |
| SOIL | Soil name |
| LAND\_USE\_MGT | Landuse database sequential number within landuse.dat |
| SOIL\_NUTR\_INIT | Initial soil chemical properties sequence number within soil\_nutrients\_initial.dat |
| sURF\_STOR | Pothole database sequential number within pothole.dat file |
| SNOW | Snow database sequential in the snow.dat file. |
| FIELD | Field |

**hru-lte.hru**

NEED THIS INFO

Below is a sample hru-lte.hru file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the hru-lte.hru file. |
| numb | Number |
| name | Name of the SWAT-DEG hru file |
| dakm2 | Drainage area (km^2) |
| cn2 | Condition II curve number |
| cn3\_swf | Soil water factor for cn3 (used in calibration) 0 =fc; 1=saturation (porosity) |
| tc | Time of concentration (min) |
| soildep | Soil profile depth (mm) |
| slope | Land surface slope (m/m) |
| slopelen | Land surface slope length (m) |
| sy | Specific yld of the shallow aquifer |
| abf | Alpha factor groundwater |
| revapc | Revap coefficient-amt of et from shallow aquifer |
| percc | Percolation coeff from shallow to deep |
| sw | Initial soil water (frac of awc) (fraction) |
| gw | Initial shallow aquifer storage (mm) |
| gwflow | Initial shallow aquifer flow (mm) |
| gwdeep | Initial deep aquifer flow (mm) |
| snow | Initial snow water equivalent (mm) |
| xlat | Latitude |
| itext | Soil texture |
| tropical | 0 = non-tropical  1 = tropical |
| igrow1 | Start of growing season |
| igrow2 | End of growing season |
| plant | Plant type (as listed in plant.dat) |
| stress | Plant stress – pest, root restriction, soil quality, nutrient, (non water, temp) |
| ipet | Potential evapotranspiration (PET) method.   1. Hargreaves method 2. Priestley-Taylor method   Numerous methods exist to calculate potential evapotranspiration. Three of the most popular or widely-used are included in SWAT. However, if a method other than Priestley-Taylor, Penman/Monteith, or Hargreaves is recommended for the area in which the watershed is located, the user can calculate daily PET values with the recommended method and import them into SWAT. A discussion of Priestley-Taylor, Penman-Monteith and Hargreaves PET methods is found in Chapter 2:2 of the theoretical documentation.  Required. |
| irr | Irrigation code.  Water applied to an HRU is obtained from one of five types of water sources: a reach, a reservoir, a shallow aquifer, a deep aquifer, or a source outside the watershed. In addition to the type of water source, the model must know the location of the water source (unless the source is outside the watershed). For the reach, shallow aquifer or deep aquifer, SWAT needs to know the subbasin number in which the source is located. If a reservoir is used to supply water, SWAT must know the reservoir number.  This variable, along with IRRNO, specifies the source of irrigation water applied in the HRU. Irrigation water may be diverted from anywhere in the watershed or outside the watershed. IRRSC tells the model what type of water body the irrigation water is being diverted from.  The options are:  0 no irrigation   1. divert water from reach 2. divert water from reservoir 3. divert water from shallow aquifer 4. divert water from deep aquifer   divert water from unlimited source outside watershed |
| irrsrc | Irrigation source 0=outside basin 1=shall aquifer 2= deep aquifer  Irrigation source location.  Water applied to an HRU is obtained from one of five types of water sources: a reach, a reservoir, a shallow aquifer, a deep aquifer, or a source outside the watershed. In addition to the type of water source, the model must know the location of the water source (unless the source is outside the watershed). For the reach, shallow aquifer or deep aquifer, SWAT needs to know the subbasin number in which the source is located. If a reservoir is used to supply water, SWAT must know the reservoir number |
|  | The definition of this variable depends on the setting of IRR.  IRR = 1: IRRSRC is the number of the reach that water is removed from.  IRR = 2: IRRSRC is the number of the reservoir that water is removed from.  IRR = 3 or 4: IRRSRC is the number of the subbasin that water is removed from.  IRR = 0 or 5: this variable is not used.  Required if 1 ≤ IRR ≤ 4 |
| tdrain | Design subsurface tile drain time (hr) |
| USLEK | USLE equation soil erodibility (K) factor (units: 0.013 (metric ton m2 hr)/(m3-metric ton cm)). Some soils erode more easily than others even when all other factors are the same. This difference is termed soil erodibility and is caused by the properties of the soil itself. Wischmeier and Smith (1978) define the soil erodibility factor as the soil loss rate per erosion index unit for a specified soil as measured on a unit plot. A unit plot is 22.1-m (72.6-ft) long, with a uniform length-wise slope of |
| USLEK, cont. | 9-percent, in continuous fallow, tilled up and down the slope. Continuous fallow is defined as land that has been tilled and kept free of vegetation for more than 2 years. The units for the USLE soil erodibility factor in MUSLE are numerically equivalent to the traditional English units of 0.01 (ton acre hr)/(acre ft-ton inch).Wischmeier and Smith (1978) noted that a soil type usually becomes less erodible with decrease in silt fraction, regardless of whether the corresponding increase is in the sand fraction or clay fraction.Direct measurement of the erodibility factor is time consuming and costly. Wischmeier et al. (1971) developed a general equation to calculate the soil erodibility factor when the silt and very fine sand content makes up less than 70% of the soil particle size distribution. |
| USLEK, cont. |  |
| USLEK, cont. | where KUSLE is the soil erodibility factor, M is the particle-size parameter, OM is the percent organic matter (%), csoilstr is the soil structure code used in soil classification, and cperm is the profile permeability class.The particle-size parameter, M, is calculatedwhere msilt is the percent silt content (0.002-0.05 mm diameter particles), mvfs is the percent very fine sand content (0.05-0.10 mm diameter particles), and mc is the percent clay content (< 0.002 mm diameter particles).The percent organic matter content, OM, of a layer can be calculated:where orgC is the percent organic carbon content of the layer (%). |
| USLEK, cont. | Soil structure refers to the aggregation of primary soil particles into compound particles which are separated from adjoining aggregates by surfaces of weakness. An individual natural soil aggregate is called a ped. Field description of soil structure notes the shape and arrangement of peds, the size of peds, and the distinctness and durability of visible peds. USDA Soil Survey terminology for structure consists of separate sets of terms defining each of these three qualities. Shape and arrangement of peds are designated as type of soil structure; size of peds as class; and degree of distinctness as grade.  Angular Blocky: bounded by planes intersecting at relatively sharp angles  Subangular Blocky: having mixed rounded and plane faces with vertices mostly rounded  The soil-structure codes for the equation are defined by the type and class of soil structure present in the layer. There are four primary types of structure, several of which are further broken down into subtypes:  -Platy, with particles arranged around a plane, generally horizontal  -Prismlike, with particles arranged around a verticle line and bounded by relatively flat vertical surfaces  Prismatic: without rounded upper ends  Columnar: with rounded caps  -Blocklike or polyhedral, with particles arranged around a point and bounded by flat or rounded surfaces which are casts of the molds formed by the faces of surrounding peds -Spheroidal or polyhedral, with particles arranged around a point and bounded by curved or very irregular surfaces that are not accomodated to the adjoining aggregates Granular: relatively non-porous  Crumb: very porous The size criteria for the class will vary by type of structure and are summarized in Table 22-2. |
| USLEK, cont. | **Definition** |
|  | Table 22-2: Size classes of soil structure   |  |  |  |  |  | | --- | --- | --- | --- | --- | |  | **Shape of structure** | | | | | **Size Classes** | **Platy** | **Prismatic and Columnar** | **Blocky** | **Granular** | | Very fine | < 1 mm | < 10 mm | < 5 mm | < 1 mm | | Fine | 1-2 mm | 10-20 mm | 5-10 mm | 1-2 mm | | Medium | 2-5 mm | 20-50 mm | 10-20 mm | 2-5 mm | | Coarse | 5-10 mm | 50-100 mm | 20-50 mm | 5-10 mm | | Very coarse | > 10 mm | > 100 mm | > 50 mm | > 10 mm | |
| USLEK, cont. | The codes assigned to *csoilstr* are:   1. very fine granular 2. fine granular 3. medium or coarse granular 4. blocky, platy, prismlike or massive   Permeability is defined as the capacity of the soil to transmit water and air through the most restricted horizon (layer) when moist. The profile permeability classes are based on the lowest saturated hydraulic conductivity in the profile. The codes assigned to *cperm* are:   1. rapid (> 150 mm/hr) 2. moderate to rapid (50-150 mm/hr) 3. moderate (15-50 mm/hr) 4. slow to moderate (5-15 mm/hr) 5. slow (1-5 mm/hr) 6. very slow (< 1 mm/hr)   Williams (1995) proposed an alternative equation:    where *fcsand* is a factor that gives low soil erodibility factors for soils with high coarse-sand contents and high values for soils with little sand, *fcl-si* is a factor that gives low soil erodibility factors for soils with high clay to silt ratios, *forgc* is a factor that reduces soil erodibility for soils with high organic carbon content, and *fhisand* is a factor that reduces soil erodibility for soils with extremely high sand contents. The factors are calculated: |
| USLEK, cont. |  |
| USLEK, cont. | where *ms* is the percent sand content (0.05-2.00 mm diameter particles), *msilt* is the percent silt content (0.002-0.05 mm diameter particles), *mc* is the percent clay content (< 0.002 mm diameter particles), and *orgC* is the percent organic carbon content of the layer (%).  Required. |
| USLEC | USLE cover factor |
| uslep | USLE equation support practice factor.  The support practice factor, *PUSLE*, is defined as the ratio of soil loss with a specific support practice to the corresponding loss with up-and-down slope culture. Support practices include contour tillage, stripcropping on the contour, and terrace systems. Stabilized waterways for the disposal of excess rainfall are a necessary part of each of these practices.  Contour tillage and planting provides almost complete protection against erosion from storms of low to moderate intensity, but little or no protection against occasional severe storms that cause extensive breakovers of contoured rows. Contouring is most effective on slopes of 3 to 8 percent. Values for *PUSLE* and slope-length limits for contour support practices are given in Table 20-4. |
| USLEP, cont. | Table 20-4: P factor values and slope-length limits for contouring (Wischmeier and Smith, 1978).   |  |  |  | | --- | --- | --- | | **Land slope (%)** | ***PUSLE*** | **Maximum length (m)** | | 1 to 2 | 0.60 | 122 | | 3 to 5 | 0.50 | 91 | | 6 to 8 | 0.50 | 61 | | 9 to 12 | 0.60 | 37 | | 13 to 16 | 0.70 | 24 | | 17 to 20 | 0.80 | 18 | | 21 to 25 | 0.90 | 15 |   Stripcropping is a practice in which contoured strips of sod are alternated with equal-width strips of row crop or small grain. Recommended values for contour stripcropping are given in Table 20-5. |
| USLEP, cont. | Table 20-5: P factor values, maximum strip width and slope-length limits for contour stripcropping (Wischmeier and Smith, 1978).   |  |  |  |  |  |  | | --- | --- | --- | --- | --- | --- | | **Land slope (%)** | ***PUSLE* values**1 | | | **Strip width (m)** | **Maximum length (m)** | | **A** | **B** | **C** | | 1 to 2 | 0.30 | 0.45 | 0.60 | 40 | 244 | | 3 to 5 | 0.25 | 0.38 | 0.50 | 30 | 183 | | 6 to 8 | 0.25 | 0.38 | 0.50 | 30 | 122 | | 9 to 12 | 0.30 | 0.45 | 0.60 | 24 | 73 | | 13 to 16 | 0.35 | 0.52 | 0.70 | 24 | 49 | | 17 to 20 | 0.40 | 0.60 | 0.80 | 18 | 37 | | 21 to 25 | 0.45 | 0.68 | 0.90 | 15 | 30 |   1P values:  A: For 4-year rotation of row crop, small grain with meadow seeding, and 2 years of meadow. A second row crop can replace the small grain if meadow is established in it.  B: For 4-year rotation of 2 years row crop, winter grain with meadow seeding, and 1-year meadow.  C: For alternate strips of row crop and winter grain |
| USLEP, cont. | Terraces are a series of horizontal ridges made in a hillside. There are several types of terraces. Broadbase terraces are constructed on gently sloping land and the channel and ridge are cropped the same as the interterrace area. The steep backslope terrace, where the backslope is in sod, is most common on steeper land. Impoundment terraces are terraces with underground outlets. |
| USLEP, cont. | Terraces divide the slope of the hill into segments equal to the horizontal terrace interval. With terracing, the slope length is the terrace interval. For broadbase terraces, the horizontal terrace interval is the distance from the center of the ridge to the center of the channel for the terrace below. The horizontal terrace interval for steep backslope terraces is the distance from the point where cultivation begins at the base of the ridge to the base of the frontslope of the terrace below.  Values for *PUSLE* for contour farming terraced fields are listed in Table 20-6. These values apply to broadbase, steep backslope and level terraces. Keep in mind that the values given in Table 20-6 do not account for all erosion control benefits of terraces. The shorter slope-length used in the calculation of the length-slope factor will produce additional reduction.  Required. |
| USLEP, cont. | Table 20-6: P factor values for contour-farmed terraced fields1   |  |  |  |  |  | | --- | --- | --- | --- | --- | | **Land slope (%)** | **Farm planning** | | **Computing sediment yield**3 | | | **Contour P factor**2 | **Stripcrop P factor** | **Graded channels**  **sod outlets** | **Steep backslope underground outlets** | | 1 to 2 | 0.60 | 0.30 | 0.12 | 0.05 | | 3 to 8 | 0.50 | 0.25 | 0.10 | 0.05 | | 9 to 12 | 0.60 | 0.30 | 0.12 | 0.05 | | 13 to 16 | 0.70 | 0.35 | 0.14 | 0.05 | | 17 to 20 | 0.80 | 0.40 | 0.16 | 0.06 | | 21 to 25 | 0.90 | 0.45 | 0.18 | 0.06 |   1Slope length is the horizontal terrace interval. The listed values are for contour farming. No additional contouring factor is used in the computation.  2 Use these values for control of interterrace erosion within specified soil loss tolerances.  3 These values include entrapment efficiency and are used for control of offsite sediment within limits and for estimating the field’s contribution to watershed sediment yield. |
| uslels | USLE equation length slope (LS) factor |

**DR –**

**DELRATIO.DEL**

NEED THIS INFO

Below is a sample DELRATIO.DEL FILE:

NEED EXAMPLE

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| mdr\_sp |  |
| header | Headers for the delration.del file. |
| flo | Volume of water (m^3) |
| sed | Sediment (metric tons) |
| org | Organic mass |
| min | Mineral mass |
| chla | Chlorophyll-a (kg) |
| cbod | Carbonaceous biological oxygen demand (kg) |
| dox | Dissolved oxygen (kg) |
| temp | Temperature (deg C) |
| san | detached sand (tons) |
| sil | detached silt (tons) |
| cla | detached clay (tons) |
| sag | detached small ag (tons) |
| lag | detached large ag(tons) |
| grv | Gravel (tons) |

**AQUIFER –**

**AQUIFER.AQU**

NEED THIS INFO

Below is a sample AQUIFER.AQU file:

aquifer.aqu:

NUMB

AQUNM

FLO

STOR

HGT

NO3

MINP

ORGN

ORGP

DELAY

ALPHA

REVAP

SEEP

SPYLD

HLIFE\_N

FLO\_MIN

REVAP\_MIN

1

aqu1

2500

1000

1

0

0

0

0

31

0.048

0.02

0.05

0.003

0

1000

750

2

aqu2

2500

1000

1

0

0

0

0

31

0.048

0.02

0.05

0.003

0

1000

750

3

aqu3

2500

1000

1

0

0

0

0

31

0.048

0.02

0.05

0.003

0

1000

750

4

aqu4

2500

1000

1

0

0

0

0

31

0.048

0.02

0.05

0.003

0

1000

750

5

aqu5

2500

1000

1

0

0

0

0

31

0.048

0.02

0.05

0.003

0

1000

750

6

aqu6

2500

1000

1

0

0

0

0

31

0.048

0.02

0.05

0.003

0

1000

750

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headings for the aquifer.aqu file. |
| numb | **Number** |
| aqunm | Name |
| flo | Initial depth of water in the shallow aquifer (mm H2O).  We recommend using a 1 year equilibration period for the model where the watershed simulation is set to start 1 year prior to the period of interest. This allows the model to get the water cycling properly before any comparisons between measured and simulated data are made. When an equilibration period is incorporated, the value for FLO is not that important. |
| stor | Initial depth of water in the deep aquifer (mm H2O).  We recommend using a 1 year equilibration period for the model where the watershed simulation is set to start 1 year prior to the period of interest. This allows the model to get the water cycling properly before any comparisons between measured and simulated data are made. When an equilibration period is incorporated, the value for STOR is not that important. In watersheds where there is no irrigation with water from the deep aquifer, this variable has no impact at all.  If no value for STOR is entered, the model sets STOR = 1000.0 mm. |
| hgt | Initial groundwater height (m).  Steady-state groundwater flow and the height of the water table are linearly proportional. The equations used to calculate the change in groundwater height with change in flow are included in SWAT. However, the groundwater height is not currently printed out in any of the output files.  *This variable is not active*. |
| no3 | Initial concentration of nitrate in shallow aquifer. (mg N/L or ppm).  Nitrate levels in the shallow aquifer are modeled, allowing for variation in nitrate concentration and groundwater loadings of nitrate contributed to streamflow in the subbasin.  Optional. |
| minp | Concentration of soluble phosphorus in groundwater contribution to streamflow from subbasin (mg P/L or ppm).  This is a fixed concentration used throughout the entire period of simulation.  Optional. |
| orgn | Organic N in the base flow (mg/L) (range 0.0 – 200.0)  default = 0.0  Optional. |
| orgp | Organic P in the base flow (mg/L) (range 0.0 – 200.0) default = 0.0  Optional. |
| delay | The delay time, *δgw*, cannot be directly measured. It can be estimated by simulating aquifer recharge using different values for *δgw* and comparing the simulated variations in water table level with observed values. Johnson (1977) developed a simple program to iteratively test and statistically evaluate different delay times for a watershed. Sangrey et al. (1984) noted that monitoring wells in the same area had similar values for *δgw*, so once a delay time value for a geomorphic area is defined, similar delay times can be used in adjoining watersheds within the same geomorphic province.  Required. |
| alpha | Baseflow alpha factor (1/days).  The baseflow recession constant, *αgw*, is a direct index of groundwater flow response to changes in recharge (Smedema and Rycroft, 1983). Values vary from 0.1-0.3 for land with slow response to recharge to 0.9-1.0 for land with a rapid response. Although the baseflow recession constant may be calculated, the best estimates are obtained by analyzing measured streamflow during periods of no recharge in the watershed.  It is common to find the baseflow days reported for a stream gage or watershed. This is the number of days for base flow recession to decline through one log cycle. When baseflow days are known, the alpha factor can be calculated:    where *αgw* is the baseflow recession constant, and *BFD* is the number of baseflow days for the watershed.  Required. |
| revap | Groundwater "revap" coefficient.  Water may move from the shallow aquifer into the overlying unsaturated zone. In periods when the material overlying the aquifer is dry, water in the capillary fringe that separates the saturated and unsaturated zones will evaporate and diffuse upward. As water is removed from the capillary fringe by evaporation, it is replaced by water from the underlying aquifer. Water may also be removed from the aquifer by deep-rooted plants which are able to uptake water directly from the aquifer.  This process is significant in watersheds where the saturated zone is not very far below the surface or where deep-rooted plants are growing. Because the type of plant cover will affect the importance of revap in the water balance, the parameters governing revap can be varied by land use.  As REVAP approaches 0, movement of water from the shallow aquifer to the root zone is restricted. As REVAP approaches 1, the rate of transfer from the shallow aquifer to the root zone approaches the rate of potential evapotranspiration. The value for REVAP should be between 0.02 and 0.20.  This variable, along with REVAPMN, is the reason a different groundwater file is created for each HRU rather than each subbasin.  Required. |
| seep | Deep aquifer percolation fraction.  The fraction of percolation from the root zone which recharges the deep aquifer. The value for RCHRG\_DP should be between 0.0 and 1.0.  Required. |
| spyld | Specific yield of the shallow aquifer (m3/m3).  Specific yield is defined as the ratio of the volume of water that drains by gravity to the total volume of rock.  Specific yield is required to calculate groundwater height fluctuations.  *This variable is not active* |
| hlife\_n | Half-life of nitrate in the shallow aquifer (days).  Nitrate in the shallow aquifer may be removed by uptake by bacteria present in the aquifer or by chemical conversion to other compounds in regions of the aquifer that are depleted in oxygen (reduced environment). The half-life, as for half-life values reported for pesticides, is the time period required for the concentration of nitrate to drop to one-half its original value. The reduction is a net reduction by all processes occurring in the shallow aquifer.  Optional. |
| flo\_min |  |
| revap\_min | Threshold depth of water in the shallow aquifer for “revap” or percolation to the deep aquifer to occur (mm H2O).  Movement of water from the shallow aquifer to the unsaturated zone is allowed only if the volume of water in the shallow aquifer is equal to or greater than REVAPMN.  This variable, along with GW\_REVAP, is the reason a different groundwater file is created for each HRU rather than each subbasin.  Required. |

**HERD –**

**animal.hrd**

NEED THIS INFO

Below is a sample animal.hrd FILE:

Need this

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| name | Animal (cattle, sheep, goats, etc) |
| phyp | Description |
| pthd |  |
| pthu |  |
| gzlm |  |
| gzin |  |
| gzwi |  |
| gzwm |  |
| pmlk |  |
| antq |  |
| igzd |  |
| impl |  |
| icvb |  |
| icvf |  |
| icwd |  |

**herd.hrd**

NEED THIS INFO

Below is a sample herd.hrd FILE:

Need this

**ranch.hrd**

NEED THIS INFO

Below is a sample ranch.hrd FILE:

Need this

**WATER\_RIGHTS –**

**DEFINE.WRO** : Is this ??? type water\_rights\_objects

NEED THIS INFO

Below is a sample DEFINE.WRO FILE:

Need this

**ELEMENT.WRO**

NEED THIS INFO

Below is a sample ELEMENT.WRO FILE: Is this ??? type water\_rights\_elements

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| name |  |
| OB\_TYP | Object type – hru, channel, reservoir, etc. |
| OB\_NUM | Object Number |
| RIGHTS\_TYP | Ie. jr, sr |
| rights | Ie. Irr demand, minimum flow, flow fraction, etc. |

**water\_rights.wro**

NEED THIS INFO

Below is a sample water\_rights.wro FILE: Is this ??? type water\_rights\_data

Need this

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| name |  |
| num | Number of objects |
| constit | Points to constituent data |
| cond | Points to ruleset to allocate water within the water rights object |

**LINK –**Need description on .lin file(s)

**chan-surf.lin**

Below is a sample chan\_surf.lin FILE:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The title line for the chan-surf.lin file (optional) |
| MCHA | Total number of channel links in file |
| Header | Headings for the chan-surf.lin file |
| numb | The sequential number of the channel links |
| name | The unique name of the channel link |
| nspu | The total objects following |
| obtyp | The object type (1=hru; 2=hru\_lte; 11=export coeff; |
| obtypno | Number of hru\_lte’s or 1st hru\_lte command |

**chan-aqu.lin**

Below is a sample chan-aqu.lin FILE:

chan-aqu.lin: Channel Aquifer Linkage 2-D - Little River Experimental Watershed

4

NUMB NAME NSPU AQU1 AQU2 AQU3

1 chan1 3 1 2 3

2 chan2 1 4

8 chan3 2 5 6

9 chan4 2 8 9

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The title line for the chan-aqu.lin file (may be blank) |
| MCHA\_SP | Total number of channel aquifer links in file |
| numb | The sequential number of the channel aquifer links |
| name | The unique name of the channel link |
| num | The total objects following |
| aqu\_no | The aquifer number |

**BASIN –** General watershed attributes are defined in the basin input file. These attributes control a diversity of physical processes at the watershed level. The interfaces will automatically set these parameters to the “default” or recommended values listed in the variable documentation. Users can use the default values or change them to better reflect what is happening in a given watershed. Variables governing bacteria or pesticide transport need to be initialized only if these processes are being modeled in the watershed. Even if nutrients are not being studied in a watershed, some attention must be paid to these variables because nutrient cycling impacts plant growth which in turn affects the hydrologic cycle.

**CODES.BSN**

Below is a partial sample CODES.BSN FILE:

codes.bsn: Basin control codes - Little River Experimental Watershed

PETFILE WWQFILE PET EVENT CRK SUBWQ SED\_DET RTE DEG WQ NOSTRESS CN CFAC 1 0 0 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the codes.bsn file. |
| petfile | Potential ET filename |
| wwqfile | Watershed stream water quality filename |
| pet | Potential evapotranspiration (PET) method.  There are four options for potential ET calculations:   1. Priestley-Taylor method 2. Penman/Monteith method 3. Hargreaves method 4. read in potential ET values   Numerous methods exist to calculate potential evapotranspiration. Three of the most popular or widely-used are included in SWAT. However, if a method other than Priestley-Taylor, Penman/Monteith, or Hargreaves is recommended for the area in which the watershed is located, the user can calculate daily PET values with the recommended method and import them into SWAT. A discussion of Priestley-Taylor, Penman-Monteith and Hargreaves PET methods is found in Chapter 2:2 of the theoretical documentation.  Required. |
| event | Rainfall/runoff/routing option:   1. daily rainfall/curve number runoff/daily routing 2. sub-daily rainfall/Green & Ampt infiltration/sub-daily routing  Option 0 is the default option. Required. |
| crk | Crack flow code.  There are two options:   1. do not model crack flow in soil 2. model crack flow in soil   Crack, or bypass, flow is a newer feature in SWAT and has been tested on a limited basis in simulations of some areas in Texas. This type of flow should be modeled only on soils classified as Vertisols.  The default option is to model the watershed without crack flow.  Required. |
| subwq | Subbasin water quality code.  The algorithms used to calculate loadings of algae, organic carbonaceous biological oxygen demand and dissolved oxygen to the stream network (see Chapter 4:4 in Theoretical Documentation) were derived from results of limited studies and are still in the testing phase. ISUBWQ allows the user to choose to apply or not apply the algorithms.   1. do not calculate algae/CBOD loadings and set dissolved oxygen to saturated oxygen concentration 2. calculate algae/CBOD/dissolved oxygen loadings using algorithms documented in Theoretical Documentation   The default option is ISUBWQ=0.  Required. |
| sed\_det | Code governing calculation of daily maximum half-hour rainfall value:   1. generate daily value using triangular distribution 2. use monthly maximum half-hour rainfall value for all days in month   The user has the option of using the monthly maximum half-hour rainfall for all days in the month. The randomness of the triangular distribution used to generated daily values causes the maximum half-hour rainfall value to jump around. For small plots or microwatersheds in particular, the variability of the triangular distribution is unrealistic.  Required. |
| rte | Channel water routing method:   1. variable storage method 2. Muskingum method   The user must be careful to define MSK\_CO1, MSK\_CO2 and MSK\_X when the Muskingum method is chosen.  The default option is IRTE=0.  Required. |
| deg | Channel degradation code.  There are two options:   1. channel dimensions are not updated as a result of degradation (the dimensions remain constant for the entire simulation) 2. channel dimensions are updated as a result of degradation   Traditionally, channel dimensions remain fixed, or constant, throughout the simulation. The change in channel dimensions with time is a new feature in SWAT that is still in the testing phase. The recommended option is to keep the channel dimensions constant.  Required. |
| wq | In-stream water quality code.  The variable identifies whether in-stream transformation of nutrients using the QUAL2E algorithms and in-stream transformation of pesticides is allowed to occur.   1. do not model in-stream nutrient and pesticide transformations 2. model in-stream nutrient and pesticide transformations   The default option is IWQ=0.  Required. |
| nostress | Redefined to the sequence number -- changed to no nutrient stress of pest in NPNO( : )to be routed through the watershed |
| cn | Daily curve number calculation method:   1. calculate daily CN value as a function of soil moisture 2. calculate daily CN value as a function of plant evapotranspiration 3. use traditional SWAT method which bases CN on soil   moisture but retention is adjusted for mildly-sloped tiled-drained watersheds  Option 0 was the only method used to calculate the daily CN value in versions of SWAT prior to SWAT2012. Calculation of the daily CN value as a function of plant evapotranspiration was added because the soil moisture method was predicting too much runoff in shallow soils. By calculating daily CN as a function of plant evapotranspiration, the value is less dependent on soil storage and more dependent on antecedent climate.  Required. |
| cfac | CFAC = 0 for C-factor calculation using Cmin.  = 1 for new C-factor calculation. (0-1) |
| cswat | Code for new carbon routines:  0 = original routines  1 = new carbon routines |
| bf\_flg | Baseflow distribution factor during the day for subdaily runs.  0 = baseflow evenly distributed to each time step during the day  0.5 = even weights between even distribution and rainfall pattern  1= profile of baseflow in a day follows rainfall pattern |
| uhyd | Unit hydrograph method:  1 = triangular UH  2 = gamma function UH |
| sed\_ch | Instream sediment model, 0=Bagnold model, 1=Brownlie model, 2=Yang model |
| tdrn | Tile drainage equations flag/code  Tile drainage routines flag/code: 1 = DRAINMOD tile equations (Subroutine DRAINS)  1 simulate tile flow using subroutine drains(wt\_shall)  0 simulate tile flow using subroutine origtile(wt\_shall,d) |
| wtdn | water table depth algorithms flag/code  1 simulate wt\_shall using subroutine new water table depth routine  0 simulate wt\_shall using subroutine original water table depth routine |
| sol\_P\_Model | Soil phosphorus model  0 = original soil phosphorus model  1 = new soil phosphorus model |
| abstr | Initial abstraction on impervious cover (mm) |
| atmo | Atmospheric deposition values  0=read in average annual values  1=read in monthly values |
| smax | Maximum depressional storage code; 1=dynamic stmaxd computed as a function of random roughness and rain intensity by depstor.f; 0 = static stmaxd from .bsn for global value or .sdr for specific HRU’s |
| i\_subhw | Code for routing headwaters |

**PARAMETERS.BSN**

NEED THIS INFO

Below is a sample PARAMETERS.BSN FILE:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the parameters.bsn file. |
| name | Name |
| evlai | Leaf area index at which no evaporation occurs from water surface.  EVLAI is used in HRUs where a plant is growing in a ponded environment (e.g. rice). Currently, this is simulated only in HRUs defined as depressional areas/potholes.  Evaporation from the water surface is allowed until the leaf area of the plant reaches the value specified for EVLAI. Chapter 8:1 in the Theoretical Documentation provides more detail on the use of this parameter.  EVLAI should be set between 0.0 and 10.0. If no value for EVLAI is entered, the model will set EVLAI = 3.0.  Required if depressional areas/potholes are modeled in the watershed. |
| ffcb | Initial soil water storage expressed as a fraction of field capacity water content.  All soils in the watershed will be initialized to the same fraction.  FFCB should be between 0.0 and 1.0. If FFCB is not set to a value, the model will calculate it as a function of average annual precipitation. The default method is to allow the model to calculate FFCB (set FFCB = 0.0).  We recommend using a 1 year equilibration period for the model where the watershed simulation is set to start 1 year prior to the period of interest. This allows the model to get the water cycling properly before any comparisons between measured and simulated data are made. When an equilibration period is incorporated, the value for FFCB is not going to impact model results.  Required. |
| surlag | Surface runoff lag coefficient.  In large subbasins with a time of concentration greater than 1 day, only a portion of the surface runoff will reach the main channel on the day it is generated. SWAT incorporates a surface runoff storage feature to lag a portion of the surface runoff release to the main channel.  SURLAG controls the fraction of the total available water that will be allowed to enter the reach on any one day. Figure 4-7 plots the fraction of total available water entering the reach at different values for *surlag* and *tconc*.  Note that for a given time of concentration, as *surlag* decreases in value more water is held in storage. The delay in release of surface runoff will smooth the streamflow hydrograph simulated in the reach.  If no value for SURLAG is entered, the model will set SURLAG = 4.0.  Required. |
| adj\_pkr | Peak rate adjustment factor for sediment routing in the *subbasin (tributary channels)*.  Sediment routing is a function of peak flow rate and mean daily flow. Because SWAT originally could not directly calculate the sub-daily hydrograph due to the use of precipitation summarized on a daily basis, this variable was incorporated to allow adjustment for the effect of the peak flow rate on sediment routing. This factor is used in the MUSLE equation and impacts the amount of erosion generated in the HRUs.  If no value for ADJ\_PKR is entered, the model will set ADJ\_PKR=1.0.  Required. |
| prf | Peak rate adjustment factor for sediment routing in the main channel.  Sediment routing is a function of peak flow rate and mean daily flow. Because SWAT originally could not directly calculate the sub-daily hydrograph, this variable was incorporated to allow adjustment for the effect of the peak flow rate on sediment routing. This variable impacts channel degradation.  If no value for PRF is entered, the model will set PRF = 1.0.  Required. |
| spcon | Linear parameter for calculating the maximum amount of sediment that can be reentrained during channel sediment routing.  The maximum amount of sediment that can be transported from a reach segment is calculated  where concsed,ch,mx is the maximum concentration of sediment that can be transported by the water (ton/m3 or kg/L), csp is a coefficient defined by the user, vch,pk is the peak channel velocity (m/s), and spexp is an exponent defined by the user.  SPCON should be between 0.0001 and 0.01. If no value for SPCON is entered, the model will set SPCON = 0.0001.  Required. |
| spexp | Exponent parameter for calculating sediment reentrained in channel sediment routing  The maximum amount of sediment that can be transported from a reach segment is calculated  where concsed,ch,mx is the maximum concentration of sediment that can be transported by the water (ton/m3 or kg/L), csp is a coefficient defined by the user, vch,pk is the peak channel velocity (m/s), and spexp is an exponent defined by the user.  The exponent, spexp, normally varies between 1.0 and 2.0 and was set at 1.5 in the original Bagnold stream power equation (Arnold et al., 1995). If no value for SPEXP is entered, the model will set SPEXP = 1.0.  Required. |
| cmn | Rate factor for humus mineralization of active organic nutrients (N and P).  Chapters 3:1 and 3:2 of the Theoretical Documentation describe the use of this parameter in the mineralization calculations.  If no value for CMN is specified, the model will set CMN = 0.0003.  Required. |
| n\_updis | Nitrogen uptake distribution parameter.  Root density is greatest near the surface, and plant nitrogen uptake in the upper portion of the soil will be greater than in the lower portion. The depth distribution of nitrogen uptake is controlled by *βn*, the nitrogen uptake distribution parameter.  The importance of the nitrogen uptake distribution parameter lies in its control over the maximum amount of nitrate removed from the upper layers. Because the top 10 mm of the soil profile interacts with surface runoff, the nitrogen uptake distribution parameter will influence the amount of nitrate available for transport in surface runoff. The model allows lower layers in the root zone to fully compensate for lack of nitrate in the upper layers, so there should not be significant changes in nitrogen stress with variation in the value used for *βn*.  If no value for N\_UPDIS is entered, the model will set N\_UPDIS = 20.0.  Figure 4-9 illustrates nitrogen uptake as a function of depth for four different uptake distribution parameter values.  Required. |
| p\_updis | Phosphorus uptake distribution parameter.This parameter controls plant uptake of phosphorus from the different soil horizons in the same way that UBN controls nitrogen uptake. The illustration of nitrogen uptake as a function of depth for four different uptake distribution parameter values in Figure 4-9 is valid for phosphorus uptake as well. Phosphorus removed from the soil by plants is taken from the solution phosphorus pool. The importance of the phosphorus uptake distribution parameter lies in its control over the maximum amount of solution P removed from the upper layers. Because the top 10 mm of the soil profile interacts with surface runoff, the phosphorus uptake distribution parameter will influence the amount of labile phosphorus available for transport in surface runoff. The model allows lower layers in the root zone to fully compensate for lack of solution P in the upper layers, so there should not be significant changes in phosphorus stress with variation in the value used for βp.  If no value for P\_UPDIS is entered, the model will set P\_UPDIS = 20.0.  Required. |
| nperco | Nitrate percolation coefficient.  NPERCO controls the amount of nitrate removed from the surface layer in runoff relative to the amount removed via percolation.  The value of NPERCO can range from 0.01 to 1.0. As NPERCO → 0.0, the concentration of nitrate in the runoff approaches 0. As NPERCO → 1.0, surface runoff has the same concentration of nitrate as the percolate.  If no value for NPERCO is entered, the model will set NPERCO = 0.20.  Required. |
| pperco | Phosphorus percolation coefficient (10 m3/Mg).  The phosphorus percolation coefficient is the ratio of the solution phosphorus concentration in the surface 10 mm of soil to the concentration of phosphorus in percolate.  The value of PPERCO can range from 10.0 to 17.5 If no value for PPERCO is entered, the model will set PPERCO = 10.0.  Required. |
| phoskd | Phosphorus soil partitioning coefficient (m3/Mg).  The phosphorus soil partitioning coefficient is the ratio of the soluble phosphorus concentration in the surface 10 mm of soil to the concentration of soluble phosphorus in surface runoff.  The primary mechanism of phosphorus movement in the soil is by diffusion. Diffusion is the migration of ions over small distances (1-2 mm) in the soil solution in response to a concentration gradient. Due to the low mobility of solution phosphorus, surface runoff will only partially interact with the solution P stored in the top 10 mm of soil.  If no value for PHOSKD is entered, the model will set PHOSKD = 175.0.  Required. |
| psp | Phosphorus availability index.  Many studies have shown that after an application of soluble P fertilizer, solution P concentration decreases rapidly with time due to reaction with the soil. This initial “fast” reaction is followed by a much slower decrease in solution P that may continue for several years (Barrow and Shaw, 1975; Munns and Fox, 1976; Rajan and Fox, 1972; Sharpley, 1982). In order to account for the initial rapid decrease in solution P, SWAT assumes a rapid equilibrium exists between solution P and an “active” mineral pool. The subsequent slow reaction is simulated by the slow equilibrium assumed to exist between the “active” and “stable” mineral pools. The algorithms governing movement of inorganic phosphorus between these three pools are taken from Jones et al. (1984).  Equilibration between the solution and active mineral pool is governed by the phosphorus availability index. This index specifies the fraction of fertilizer P which is in solution after an incubation period, i.e. after the rapid reaction period.  A number of methods have been developed to measure the phosphorus availability index. Jones et al. (1984) recommends a method outlined by Sharpley et al. (1984) in which various amounts of phosphorus are added in solution to the soil as K2HPO4. The soil is wetted to field capacity and then dried slowly at 25°C. When dry, the soil is rewetted with deionized water. The soil is exposed to several wetting and drying cycles over a 6-month incubation period. At the end of the incubation period, solution phosphorus is determined by extraction with anion exchange resin.  The P availability index is then calculated:    where *pai* is the phosphorus availability index, *Psolution,f* is the amount of phosphorus in solution after fertilization and incubation, *Psolution,I* is the amount of phosphorus in solution before fertilization, and *fertminP* is the amount of soluble P fertilizer added to the sample.  If no value for PSP is entered, the model will set PSP = 0.40.  Required. |
| rsdco | Residue decomposition coefficient.  The fraction of residue which will decompose in a day assuming optimal moisture, temperature, C:N ratio and C:P ratio.  If no value for RSDCO is entered, the model will set RSDCO = 0.05.  Required. |
| percop | Pesticide percolation coefficient.  PERCOP controls the amount of pesticide removed from the surface layer in runoff and lateral flow relative to the amount removed via percolation. The value of PERCOP can range from 0.01 to 1.0. As PERCOP → 0.0, the concentration of pesticide in the runoff and lateral flow approaches 0. As PERCOP → 1.0, surface runoff and lateral flow has the same concentration of pesticide as the percolate.  If no value for PERCOP is entered, the model will set PERCOP = 0.50.  Required if pesticide transport is of interest. |
| Msk\_co1 | Calibration coefficient used to control impact of the storage time constant (*Km*) for normal flow (where normal flow is when river is at bankfull depth) upon the *Km* value calculated for the reach.  Required only if IRTE = 1. |
| MSK\_CO2 | Calibration coefficient used to control impact of the storage time constant (*Km*) for low flow (where low flow is when river is at 0.1 bankfull depth) upon the *Km* value calculated for the reach.  Required only if IRTE = 1. |
| MSK\_X | MSK\_X is a weighting factor that controls the relative importance of inflow and outflow in determining the storage in a reach.  The weighting factor has a lower limit of 0.0 and an upper limit of 0.5. This factor is a function of the wedge storage. For reservoir-type storage, there is no wedge and *X* = 0.0. For a full-wedge, *X* = 0.5. For rivers, *X* will fall between 0.0 and 0.3 with a mean value near 0.2.  If no value for MSK\_X is entered, the model will set MSK\_X = 0.2.  Required only if IRTE = 1. |
| TRNSRCH | Fraction of transmission losses from main channel that enter deep aquifer. The remainder if the transmission losses enter bank storage.  In arid watersheds, transmission losses from the main channel network may be permanently lost due to transmission to aquifers that do not contribute flow back to the stream network. This variable allows the user to specify the fraction of transmission losses from the channel network that is permanently lost.  TRNSRCH varies between 0.00 and 1.00. The default value for TRNSRCH is 0.00.  Required. |
| EVRCH | Reach evaporation adjustment factor.  The evaporation coefficient is a calibration parameter for the user and is allowed to vary between 0.0 and 1.0. This coefficient was created to allow reach evaporation to be dampened in arid regions. The original equation tends to overestimate evaporation in these areas.  If no value for EVRCH is entered, the model will set EVRCH = 1.00.  Required. |
| CNCOEF | Plant ET curve number coefficient.  ET weighting coefficient used to calculate the retention coefficient for daily curve number calculations dependent on plant evapotranspiration.  This value can vary between 0.5 and 2.0. If no value is entered for CNCOEF, the model will set CNCOEF = 1.0.  Required if ICN = 1. |
| CDN | Denitrification exponential rate coefficient.  This coefficient allows the user to control the rate of denitrification.  Acceptable values for CDN range from 0.0 to 3.0. If no value for CDN is specified, the model will set CDN = 1.4.  Required. |
| SDNCO | Denitrification threshold water content.  Fraction of field capacity water content above which denitrification takes place.  Denitrification is the bacterial reduction of nitrate, , to N2 or N2O gases under anaerobic (reduced) conditions. Because SWAT does not track the redox status of the soil layers, the presence of anaerobic conditions in a soil layer is defined by this variable. If the soil water content calculated as fraction of field capacity is ≥ SDNCO, then anaerobic conditions are assumed to be present and denitrification is modeled. If the soil water content calculated as a fraction of field capacity is < SDNCO, then aerobic conditions are assumed to be present and denitrification is not modeled.  If no value for SDNCO is specified, the model will set SDNCO = 1.10.  Required. |
| BACT\_SWF | Fraction of manure applied to land areas that has active colony forming units.  If no value for BACT\_SWF is specified, the model will set BACT\_SWF = 0.15.  Required if bacteria processes are of interest. |
| TB\_ADJ | *New variable in testing.*  *Adjustment factor for subdaily unit hydrograph basetime.* |
| cN\_FROZ | Parameter for frozen soil adjustment on infiltration/runoff.  If no value for CNFROZ\_BSN is entered, the model will set CNFROZ\_BSN = 0.000862.  Optional. |
| dorm\_hr | Time threshold used to define dormancy (hours). The maximum day length minus DORM\_HR is equal to when dormancy occurs.  Optional. |
| smxco | Adjustment factor for maximum curve number S factor. Coefficient curve number method that uses antecedent climate.  Optional. |
| FIXCO | Nitrogen fixation coefficient. (0.0 – 1.0)  1.0 = fixes 100% of nitrogen demand. 0.0 = fixes none of nitrogen demand. |
| NFIXMX | Maximum daily-n fixation (kg/ha). (1.0 – 20.0) |
| DECR\_MIN | Minimum daily residue decay (fraction 0.0 – 0.05) |
| RSD\_COVCO | Residue cover factor for computing fraction of cover. (0.1 – 0.5) |
| VCRIT | Critical velocity |
| RES\_STR\_CO | Reservoir sediment settling coefficient (0.09 – 0.27) |
| UHALPHA | Alpha coefficient for gamma function unit hydrograph. Required if iuh = 2 is selected |
| EROS\_SPL | Splash erosion coefficient (0.9 – 3.1) |
| RILL\_MULT | Rill erosion coefficient – multiplier to USLE\_K for soil susceptible to rill erosion (0.5-2.0) |
| EROS\_EXPO | Exponential coefficient for overland flow – (1.5-3.0) |
| C\_FACTOR | Scaling parameter for cover and management factor for overland flow erosion (0.03/0.001/0.45) |
| CH\_D50 | Median particle diameter of main channel (mm) (50/10/100) |
| SIG\_G | Geometric standard deviation of particle size (1.57/1.0/5.0) |
| R2ADJ | Curve number retention parameter adjustment for low gradient, non-draining soils (dimensionless) (0-3) |
|  | Random generator seed code.  A set of random numbers is needed by SWAT to generate weather data. SWAT has a set of default random numbers embedded in the code. To use the default random numbers, the user should set IGN = 0. This is the default value for IGN.  In some situations, a user may wish to vary the weather sequence between runs. One method to do this is to set ign to a different number every time the model is run. This code will activate a random number generator, which will replace the default set of random numbers with a new set. The value to which IGN is set determines the number of times the random number generator is cycled before the simulation begins. The seeds produced by the random number generator are then utilized by the weather generator instead of the default values.  Measured weather data read into the model is not affected by this variable. However, if the measured data contains missing values, the weather generator is activated to produce data to replace the missing values. The data produced to replace missing values will be affected by this variable.  Required. |
| igen | Randon generator code 0 = use default number; 1 = generate new  numbers in every simulation |
| RDIST | Rainfall distribution code 0=skewed; 1=exponential; |
| REXP | Value of exponent for mixed exponential rainfall distribution.  A value for REXP is needed only if IDIST = 1. The model will set REXP = 1.3 if no value is entered. |

**HYDROLOGY –**

**HYDROLOGY.HYD**

Data contained in the hydrology.dat data file can be grouped into the following categories: topographic characteristics, water flow, erosion, land cover, and depressional storage areas.

Below is a partial sample HYDROLOGY.HYD FILE:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| name | Name |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the nutrients.res file. |
| Name | Name |
| Lat\_Ttime | Lateral flow travel time (days).  Setting LAT\_TTIME = 0.0 will allow the model to calculate the travel time based on soil hydraulic properties. This variable should be set to a specific value only by hydrologists familiar with the base flow characteristics of the watershed.  Required. |
| lat\_sed | Sediment concentration in lateral and groundwater flow (mg/L).  Sediment concentration in lateral and groundwater flow is usually very low and does not contribute significantly to total sediment yields unless return flow is very high.  Optional. |
| canmx | Maximum canopy storage (mm H2O).  The plant canopy can significantly affect infiltration, surface runoff and evapotranspiration. As rain falls, canopy interception reduces the erosive energy of droplets and traps a portion of the rainfall within the canopy. The influence the canopy exerts on these processes is a function of the density of plant cover and the morphology of the plant species.  When calculating surface runoff, the SCS curve number method lumps canopy interception in the term for initial abstractions. This variable also includes surface storage and infiltration prior to runoff and is estimated as 20% of the retention parameter value for a given day (see Chapter 2:1). When the Green and Ampt infiltration equation is used to calculate infiltration, the interception of rainfall by the canopy must be calculated separately.  SWAT allows the maximum amount of water that can be held in canopy storage to vary from day to day as a function of the leaf area index. CANMX is the maximum amount of water that can be trapped in the canopy when the canopy is fully developed (mm H2O).  Required. |
| esco | Soil evaporation compensation factor.  This coefficient has been incorporated to allow the user to modify the depth distribution used to meet the soil evaporative demand to account for the effect of capillary action, crusting and cracks. ESCO must be between 0.01 and 1.0. As the value for ESCO is reduced, the model is able to extract more of the evaporative demand from lower levels.  The change in depth distribution resulting from different values of *esco* are graphed in Figure 19-1.  If no value for ESCO is entered, the model will set ESCO = 0.95. The value for ESCO may be set at the watershed or HRU level (ESCO in .bsn, see Chapter 4).  Required. |
| epco | Plant uptake compensation factor.  The amount of water uptake that occurs on a given day is a function of the amount of water required by the plant for transpiration, *Et*, and the amount of water available in the soil, *SW*. If upper layers in the soil profile do not contain enough water to meet the potential water uptake, users may allow lower layers to compensate. The plant uptake compensation factor can range from 0.01 to 1.00. As *epco* approaches 1.0, the model allows more of the water uptake demand to be met by lower layers in the soil. As *epco* approaches 0.0, the model allows less variation from the original depth distribution to take place.  If no value for EPCO is entered, the model will set EPCO = 1.0. The value for EPCO may be set at the watershed or HRU level (EPCO in .bsn, see Chapter 4).  Required. |
| erorgn | Organic N enrichment ratio for loading with sediment.  As surface runoff flows over the soil surface, part of the water’s energy is used to pick up and transport soil particles. The smaller particles weigh less and are more easily transported than coarser particles. When the particle size distribution of the transported sediment is compared to that of the soil surface layer, the sediment load to the main channel has a greater proportion of clay sized particles. In other words, the sediment load is enriched in clay particles. Organic nitrogen in the soil is attached primarily to colloidal (clay) particles, so the sediment load will also contain a greater proportion or concentration of organic N than that found in the soil surface layer.  The enrichment ratio is defined as the ratio of the concentration of organic nitrogen transported with the sediment to the concentration in the soil surface layer. SWAT will calculate an enrichment ratio for each storm event, or allow the user to define a particular enrichment ratio for organic nitrogen that is used for all storms during the simulation. To calculate the enrichment ratio, the value for ERORGN is set to zero. The default option is to allow the model to calculate the enrichment ratio.  Required. |
| erorgp | Phosphorus enrichment ratio for loading with sediment.  The enrichment ratio is defined as the ratio of the concentration of phosphorus transported with the sediment to the concentration of phosphorus in the soil surface layer. SWAT will calculate an enrichment ratio for each storm event, or allow the user to define a particular enrichment ratio for phosphorus attached to sediment that is used for all storms during the simulation.  If the value for ERORGP is set to zero, the model will calculate an enrichment ratio for every storm event. The default option is to allow the model to calculate the enrichment ratio.  Required. |
| cn3\_swf | Pothole evaporation coefficient |
| biomix | Biological mixing efficiency.  Biological mixing is the redistribution of soil constituents as a result of the activity of biota in the soil (e.g. earthworms, etc.). Studies have shown that biological mixing can be significant in systems where the soil is only infrequently disturbed. In general, as a management system shifts from conventional tillage to conservation tillage to no-till there will be an increase in biological mixing. SWAT allows biological mixing to occur to a depth of 300 mm (or the bottom of the soil profile if it is shallower than 300 mm).  The efficiency of biological mixing is defined by the user and is conceptually the same as the mixing efficiency of a tillage implement. The redistribution of nutrients by biological mixing is calculated using the same methodology as that used for a tillage operation. Biological mixing is performed at the end of every calendar year.  If no value for BIOMIX is entered, the model will set BIOMIX = 0.20.  Optional. |
| dep\_imp | Depth to the bottom of soil profile (mm).  Perched water tables are created when water percolating through the soil profile reaches a layer of low hydraulic conductivity that causes water to pond at the upper boundary of the impervous layer. This variable defines the depth to the impervious layer in the soil profile and is required if perched water tables, depressional storage areas/potholes, or tile drainage is being modeled in the HRU (or subbasin for depressional storage areas).  If perched water tables do not occur in the HRU leave this variable set to 0. If a generic depth is defined using DEPIMP\_BSN (.bsn), set DEP\_IMP = 0 to use the basin-level value. |
| lat\_orgn | If no value for BIOMIX is entered, the model will set BIOMIX = 0.20.  Optional. |
| lat\_orgp | Organic P in the base flow (mg/L) (range 0.0 – 200.0) default = 0.0  Optional. |
| harg\_pet | Coefficient related to radiation used in Hargreaves equation |
| cncoef | Plant ET curve number coefficient.  ET weighting coefficient used to calculate the retention coefficient for daily curve number calculations dependent on plant evapotranspiration.  This value can vary between 0.5 and 2.0. If no value is entered for CNCOEF, the model will set CNCOEF = 1.0.  Required if ICN = 1. |
| perco | Percolation coefficient - adjusts soil moisture for perc to occur (1.0 = fc) |

**topography.hyd**

Data contained in the topo.dat data file can be grouped into the following categories: topographic characteristics, water flow, erosion, land cover, and depressional storage areas.

Below is a sample TOPOGRAPHY.HYD FILE:

topography.hyd

NAME SLOPE SLOPE\_LEN LAT\_LEN DIS\_STREAM DEP\_CO

top1 0.037 50 50 100 1

1

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| HEADER | Headers for the topography.hyd file. |
| Name | Sequential number of topo in file |
| slope | Average slope steepness in HRU (m/m) |
| slope\_len | Average slope length for erosion (m) |
| Lat\_len | Slope length for lateral subsurface flow (m) |
| dis\_stream | Average distance to stream (m) |
| dep\_co | Deposition coefficient |

**FIELD.FLD**

NEED THIS INFO

Below is a sample FIELD.FLD FILE:

field.fld: Field data - LREW Subbasin March 2016

NAME LENGTH WIDTH ANGLE

fld1 600.0 20.0 30.0

fld2 600.0 20.0 30.0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| HEADER | Headers for the field.fld file. |
| name | Name of the field |
| length | Field length for wind erosion (m) |
| wid | Field width for wind erosion (m) |
| ang | Field angle for wind erosion (m) |

**EXCO –**

**EXCO.EXC**

NEED THIS INFO

Below is a sample EXCO.EXC FILE:

Need

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the exco.exc file. |
| NAME | Name |
| FLO | Volume of water (m^3) |
| SED | sediment (metric tons) |
| Orgn | Organic N (kg N) |
| sedp | Organic P (kg P) |
| no3 | NO3-N (kg N) |
| solp | Mineral (soluble P) (kg P) |
| psol | Pesticide in solution (mg pst) |
| psor | Pesticide sorbed to sediment (mg pst) |
| chla | Chlorophyll-a (kg) |
| nh3 | NH3 (kg N) |
| no2 | NO2 (kg N) |
| cbod | Carbonaceous biological oxygen demand (kg) |
| dox | Dissolved oxygen (kg) |
| bacp | Persistent bacteria (# cfu/100ml) |
| BACLP | Less persistent bacteria (# cfu/100ml) |
| MET1 | Conservative metal #1 (kg) |
| met2 | Conservative metal #2 (kg) |
| met3 | Conservative metal #3 (kg) |
| san | Detached sand (tons) |
| sil | Detached clay (tons) |
| cla | Detached clay (tons) |
| sag | Detached small ag (tons) |
| lag | Detached large ag (tons) |
| grv | gravel (tons) |
| TEMP | Temperature (deg c) |

**BACTERIA –**

**INITIAL.BAC**

NEED THIS INFO

Below is a sample INITIAL.BAC FILE:

initial.bac

2

NUM

PLT

SOL

SOR

1

1

100

1000

10

2

1

0

5000

600

2

5000

30000

20000

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| mbac\_db |  |
| header | Headings for the initial.bac file |
| Num | Total number of initial bacteria in file |
| NUM\_DB | Number of bacteria to follow |
| PLt | Bacteria on plants at beginning of simulation (#cfu/m^2) |
| SOL | Soluble bacteria in soil at beginning of simulation (#cfu/m^2) |
| SOr | Sorbed bacteria in soil at beginning of simulation (#cfu/m^2) |

**BACTERIA.BAC**

NEED THIS INFO

Below is a sample partial BACTERIA.BAC FILE:

bacteria.bac: Bacteria properties - LREW Subbasin March 2016

BACT\_NAME DO\_SOLN GR\_SOLN DO\_SORB GR\_SORB KD T\_ADJ WASHOFF DO\_PLNT GR\_PLNT

null 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the bacteria.bac file. |
| bactnm | Name of bacteria |
| do\_soln | Die-off factor for persistent bacteria in soil solution at 20°C. (1/day)  SWAT allows two different bacteria types to be modeled in a given simulation. In the input/output files these two types are referred to as ‘persistent’ and ‘less persistent’. These terms are purely descriptive and are used solely to differentiate between the two types. The bacteria input variables in the .bsn file govern the actual persistence of the two bacteria types. The user may choose to model no, one, or two types of bacteria.  Required if bacteria processes are of interest. |
| gr\_soln | Growth factor for persistent bacteria in soil solution at 20°C. (1/day)  Required if bacteria processes are of interest. |
| do\_sorb | Die-off factor for persistent bacteria adsorbed to soil particles at 20°C. (1/day)  Required if bacteria processes are of interest. |
| gr\_sorb | Growth factor for persistent bacteria adsorbed to soil particles at 20°C. (1/day)  Required if bacteria processes are of interest. |
| kd | Bact part coeff bet sol and sorbed phase in surf runoff |
| t\_adj | Temperature adjustment factor for bacteria die-off/growth.  If no value for THBACT is entered, the model will set THBACT = 1.07.  Required if bacteria processes are of interest. |
| washoff | Wash-off fraction for persistent bacteria.  Fraction of persistent bacteria on foliage that washes off during a rainfall event.  Required if bacteria processes are of interest. |
| do\_plnt | Die-off factor for persistent bacteria on foliage at 20°C. (1/day)  Required if bacteria processes are of interest. |
| gr\_plnt | Growth factor for persistent bacteria on foliage at 20°C. (1/day)  Required if bacteria processes are of interest. |
| fr\_manure | Fraction of manure applied to land areas that has active colony forming units.  If no value for SWF is specified, the model will set SWF = 0.15.  Required if bacteria processes are of interest. |
| perco | Bacteria percolation coefficient (10 m3/Mg).  The bacteria percolation coefficient is the ratio of the solution bacteria concentration in the surface 10 mm of soil to the concentration of bacteria in percolate.  The value of BACTMIX can range from 7.0 to 20.0. If no value for BACTMIX is entered, the model will set BACTMIX = 10.0.  Required if bacteria processes are of interest. |
| det\_thrshd | Threshold detection level for less persistent bac when bacteria levels drop to this amount the model considers bacteria in the soil to be insignificant and sets the levels to zero |
| do\_stream | Die-off factor for persistent bacteria in streams (moving water) at 20°C. (1/day)  Required if bacteria processes are of interest. |
| gr\_stream | growth factor for persistent bacteria in streams |
| do\_res | Die-off factor for less persistent bacteria in streams (moving water) at 20°C. (1/day)  Required if bacteria processes are of interest. |
| gr\_res | growth factor for less persistent bacteria in reservoirs |
| swf | fraction of manure containing active colony forming units |
| conc\_min |  |

**STRUCTURAL –**

**TILEDRAIN.STR**

Need this info

Below is a sample TILEDRAIN.STR FILE:

tiledrain.str: Subsurface drainage properties - Little River Experimental Watershed

NAME DEPTH TIME LAG RADIUS DIST DRAIN\_CO PUMPCAP LATKSAT

Example 1000.0 24.0 96.0 100.0 30.0 10.0 1.0 2.0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| name | Name |
| DEPTH | Depth of drain tube from the soil surface |
| TIME | Time to drain soil to field capacity |
| LAG | Drain tile lag time |
| RADIUS | Effective radius of drains (mm) Range (3.0 – 40.0 mm) |
| DIST | Distance between two drain tubes or tiles (mm) Range (7600 – 30000 mm) |
| DRAIN\_CO | Daily drainage coefficient (mm day-1).  Tile drainage routines flag/code: 1 = DRAINMOD tile equations (Subroutine DRAINS) Range (10-51 mm day-1) |
| PUMPCAP | Pump capacity (mm h-1) Default value = 1.042 mm h-1 or 22 mm day-1 |
| LATKSAT | Multiplication factor to determine lateral ksat (conk(j1,j)) from SWAT ksat input value (sol\_k(j1,j)) for HRU Range (0.01 - 4.00) |

**SEPTIC.STR**

The Onsite Wastewater Systems (OWSs) input file contains information related to a diversity of features of OWSs within the subbasin. Data contained in the septic.dat data file are: type of septic system, geometry of biozone, characteristics of biomass, and bio-physical reaction coefficients occurring in the biozone (Adapted from Siegrist et al., 2005).

Below is a partial sample SEPTIC.STR FILE:

septic.str: Septic system properties - LREW Subbasin March 2016

SEP\_NAME TYP YR OPT CAP AREA TFAIL Z THK STRM\_DIST DENSITY BD BOD\_DC Example 0 0 0 0.000 0.000 0 0.000 0.000 0.000 0.000 0.000 0.

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| NAME | Name |
| TYP | The type of septic system  |  |  | | --- | --- | | Type | Definition | | 1 | Generic type conventional system | | 2 | Generic type advanced system | | 3 | Septic tank with conventional drainfield | | 4 | Septic tank with SASa type 1 | | 5 | Septic tank with SAS type 2 | | 6 | Septic tank with in-tank N removal and SAS | | 7 | Septic tank with effluent N removal recycle | | 8 | Septic tank with corrugated plastic trickling  Filter | | 9 | Septic tank with open-cell form trickling filter | | 10 | Single pass sand filter 1 | | 11 | Single pass sand filter 2 | | 12 | Single pass sand filter 3 | | 13 | Single pass sand filter 4 | | 14 | At grade recirculating sand filter | | 15 | Maryland style RSFb | | 16 | RSF | | 17 | Septic tank w/ constructed wetland  and surface water discharge | | 18 | Municipal wastewater w/ constructed wetland  and surface water discharge 1 | | 19 | Municipal wastewater w/ constructed wetland  and surface water discharge 2 | | 20 | Municipal wastewater w/ constructed wetland | | 21 | Municipal wastewater w/ lagoon and  constructed wetland | | 22 | Waterloo biofilter (plastic media) 1 | | 23 | Waterloo biofilter (plastic media) 2 | | 24 | Peat biofilter | | 25 | Recirculating textile filter | | 26 | Foam or textile filter effluent | | 27 | Septic, recirculating gravel filter,  UV disinfection | | 28 | Untreated Effluent - Texas A&M reference | |
| YR | Year the septic system became operational (eg 1980). If 0 is input for *isep\_iyr*, the model assumes the septic system is in operation at the beginning of the simulation  Required. |
| OPT | Initial septic HRU operational condition. User can define the default condition of a septic HRU as either active (sep\_opt=1), failing (sep\_opt=2), or non-septic (sep\_opt=0). An active system automatically becomes failing as biozone layer gets clogged over time. A failing system turns to an active system after user specified “number of days for rehabilitation” defined by *isep\_tfail*. Required. |
| CAP | Number of permanent residents in the house. SEP\_cap for a typical US residence is 2.5 and ranges 1~10000.  Required. |
| AREA | Average area of drainfield of individual septic systems (m2).  Typically recommended drainfield area per person is about 40 to 70 (m2). This varies from state to state in the United States. For a household with 2.5 people, generally a drainfield area of 100 (m2) is recommended. User can modify the bz\_area based on the number of people in a household. The bz\_area and sep\_cap may be modified appropriately to study the effects of larger population size using septic systems.  Required |
| tFAIL | Time until failing systems gets fixed (days). An active system becomes failing as the biozone gets clogged and hydraulic failure occurs. A failing system automatically turns active during the simulation and septic parameters are re-initialized to default values after the user specified number of days (days assigned for isep\_tfail) for rehabilitation. The default value for *isep\_tfail* is 70 days but it can range between 10~100000 days. For testing long term failure, isep\_tfail can be increased as per the failing duration. isep\_opt should be set at 2 for simulating failing conditions..  Required. |
| z | Depth to the top of biozone layer from the ground surface (mm). The thickness includes top soil layer and septic tank effluent (STE) distribution chamber including perforated pipe. The default is 500mm and the depth typically ranges between 10-10000mm.  Required. |
| thk | Thickness of the biozone layer (mm). The biozone layer is thin soil layer underneath the STE distribution chamber where pollutants are degraded by naturally existing live biomass bacteria. The default thickness is 50mm and ranges 5~100mm.  Required. |
| strm\_dist | Distance to the stream from the septic HRU (km)  Currently not available. |
| density | Number of septic systems per square kilometer.  Currently not available. |
| bd | Density of biomass (kg/m3), typically in the range of 900~1100 kg/m3. The default is 1000 kg/m3.  Required. |
| bod\_dc | BOD decay rate coefficient. Biozone BOD coefficient is normalized by the volume of biomass in the formula. The default value is 0.5 and the value ranges 0.1~ 5.  Required. |
| bod\_cov | A conversion factor representing the proportion of mass bacterial growth and mass BOD degraded in the STE. The default value is 0.32 and the value ranges 0.1~ 0.5.  Required. |
| fc1 | Linear coefficient for calculation of field capacity in the biozone. The default value is 30 and the value ranges 0~ 50.  Required. |
| fc2 | Exponential coefficient for calculation of field capacity in the biozone. The default value is 0.8 and the value ranges 0.5~ 1.  Required. |
| fecal | Fecal coliform bacteria decay rate coefficient. Biozone fecal coliform coefficient is normalized by the volume of biomass in the formula. The default value is 1.3 and the value ranges 0.5~ 2.  Required. |
| plq | Conversion factor for plaque from total dissolved solids. The default value is 0.1 and the value ranges 0.08~ 0.95.  Required. |
| mrt | Mortality rate coefficient. The default value is 0.5 and the value ranges 0.01~ 1.  Required. |
| rsp | Respiration rate coefficient. The default value is 0.16 and the value ranges 0.01~ 1.  Required. |
| slg1 | Linear coefficient for calculating the rate of biomass sloughing. The default value is 0.3 and the value ranges 0.01~ 0.5.  Required. |
| slg2 | Exponential coefficient for calculating the rate of biomass sloughing. The default value is 0.5 and the value ranges 0.1~ 2.5.  Required. |
| nitr | Nitrification rate coefficient. Biozone nitrification rate coefficient is normalized by the volume of biomass in the formula. The default value is 1.5 and the value ranges 0.1~ 300.  Required. |
| denitr | Denitrification rate coefficient. Biozone denitrification rate coefficient is normalized by the volume of biomass in the formula. The default value is 0.32 and the value ranges 0.1~50.  Required. |
| pdistrb | Linear P sorption distribution coefficient (L/kg). The default value is 128 and the value ranges 1.4~478.  Required. |
| psorpmax | Maximum P sorption capacity (mg P/kg Soil). The default value is 850 and the value ranges 0~17600.  Required. |
| solpslp | Slope of the linear effluent soluble P equation. The default value is 0.04 and the value ranges 0~0.3.  Required. |
| solpintc | Intercept of the linear effluent soluble P equation. The default value is 3.1 and the value ranges 0~10.  Required. |

**FILTERSTRIP.STR**

NEED THIS INFO

Below is a sample FILTERSTRIP.STR FILE:

FIlterstrip.str - Little River Experimental Watershed

NAME VFSI VFSRATIO VFSCON VFSCH

filstr1 0.02 0.10 0.003 0.20

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| NAME | Name |
| VFSI | Flag for the simulation of filter strips (VFSI = 1/0 active/inactive). |
| VFSRATIO | Ratio of field area to filter strip area (unitless). Ranges from 0 to 300 with values from 30-60 being most common. Default value is 40 |
| VFSCON | Fraction of the HRU which drains to the most concentrated ten percent of the filters strip area. Runoff generated upslope a filter strip is not uniformly distributed across the entire length of the strip. Ten percent of the filter strip can receive between 0.25 and 0.75 of the runoff from the entire filed. Default value is 0.5. |
| VFSCH | Fraction of the flow within the most concentrated ten percent of the filter strip which is fully channelized (dimensionless). Flow which is fully channelized is not subject to filtering or infiltration effects. Default value is 0.0 |

**GRASSEDWW.STR**

NEED THIS INFO

Below is a sample GRASSEDWW.STR FILE

grassedww.str - Little River Experimental Watershed

NAME GRWAT\_I GRWAT\_N GRWAT\_SPCON GRWAT\_D GRWAT\_W GRWAT\_L GRWAT\_S

grwway1 0.20 0.20 0.20 0.20 0.20 0.20 0.20

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| name | Name |
| GRWAT\_I | On/off Flag for waterway simulation |
| GRWAT\_N | Mannings's n for grassed waterway |
| GRWAT\_SPCON | sediment transport coefficant defined by user |
| GRWAT\_D | depth of Grassed waterway (m) |
| GRWAT\_W | width of grass waterway |
| GRWAT\_L | length of Grass Waterway (km) |
| GRWAT\_S | slope of grass waterway (m/m) |

**BMPUSER.STR**

NEED THIS INFO

Below is a sample BMPUSER.STR FILE:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| name | User BMP Name |
| BMP\_FLAG | Code to turn on/off user BMP (range 0-1)( mgt1i) |
| BMP\_SED | Sediment removal by BMP (%) (range 0-100) |
| BMP\_PP | Particulate (Organic) phosphorous removal by BMP (%) (range 0-100) |
| BMP\_SP | Soluble phosphorous removal by BMP (%) (range 0-100) |
| BMP\_PN | Particulate (Organic) nitrogen removal by BMP (%) (range 0-100) |
| BMP\_SN | Soluble nitrogen removal by BMP (%) (range 0-100) |
| BMP\_BAC | Bacteria removed by BMP (%) (range 0-100) |

**PARM\_DB–** The parameters database files are supplied with the model containing

Input parameters for most of the common plants, fertilizers, pesticides, urban, are included in the database files with the option for the user to add new parameters to each file.

**plants.plt**

Information required to simulate plant growth is stored by plant species in the plant growth database file. This database file is supplied with the model. The plant growth database distributed with SWAT includes parameters for most of the common plant species. If a user needs to model a land use or plant not included in the database, please feel free to contact the SWAT development team for assistance in determining plant parameters. Appendix A documents the source of parameter values in the distributed database file. Below is a partial sample plants.plt file (partial file, please see plants.plt in example input dataset directory for complete file:

plants.plt NAME IDC PHU BIO\_E HVSTI BLAI FRGRW1 LAIMX1 FRGRW2 LAIMX2 DLAI CHTMX agrl 4 2000 33.5 0.45 3 0.15 0.05 0.5 0.95 0.64 1 2 30 11 0.0199 0.0032 0.044 0.0164 0.0128 0.006 0.0022 0.0018 0.25 0.2 0.005 4 0.75 8.5 660 36 0.05 0 0 0 0 0.65 0.1 0 0 0 0 0 0 0.5 0 0 0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| plantNM | A four character code to represent the land cover/plant name.  The 4-letter codes in the plant growth and urban databases are used by the GIS interfaces to link land use/land cover maps to SWAT plant types. This code is printed to the output files.  When adding a new plant species or land cover category, the four letter code for the new plant must be unique.  Required. |
| IDC | Land cover/plant classification:   1. warm season annual legume 2. cold season annual legume 3. perennial legume 4. warm season annual 5. cold season annual 6. perennial 7. trees   Processes modeled differently for the 7 groups are:   1. warm season annual legume  * simulate nitrogen fixation * root depth varies during growing season due to root growth  1. cold season annual legume  * simulate nitrogen fixation * root depth varies during growing season due to root growth   fall-planted land covers will go dormant when daylength is less than the threshold daylength |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| IDC, cont. | 1. perennial legume  * simulate nitrogen fixation * root depth always equal to the maximum allowed for the plant species and soil * plant goes dormant when daylength is less than the threshold daylength  1. warm season annual  * root depth varies during growing season due to root growth  1. cold season annual  * root depth varies during growing season due to root growth * fall-planted land covers will go dormant when daylength is less than the threshold daylength  1. perennial  * root depth always equal to the maximum allowed for the plant species and soil * plant goes dormant when daylength is less than the threshold daylength  1. trees  * root depth always equal to the maximum allowed for the plant species and soil * partitions new growth between leaves/needles (20%) and woody growth (80%). At the end of each growing season, a fraction of the biomass is converted to residue   Required. |
| PHU | Total number of heat units to bring crop to maturity |
| BIO\_E | Radiation-use efficiency or biomass-energy ratio ((kg/ha)/(MJ/m2)).  Radiation-use efficiency (RUE) is the amount of dry biomass produced per unit intercepted solar radiation. The radiation-use efficiency is assumed to be independent of the plant’s growth stage. BIO\_E represents the potential or unstressed growth rate (including roots) per unit of intercepted photosynthetically active radiation. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| BIO\_E, cont. | Determination of RUE is commonly performed and a literature review will provide those setting up experiments with numerous examples. The following overview of the methodology used to measure RUE was summarized from Kiniry et al (1998) and Kiniry et al (1999).  To calculate RUE, the amount of photosynthetically active radiation (PAR) intercepted and the mass of aboveground biomass is measured several times throughout a plant’s growing season. The frequency of the measurements taken will vary but in general 4 to 7 measurements per growing season are considered to be adequate. As with leaf area determinations, the measurements should be performed on non-stressed plants.  Intercepted radiation is measured with a light meter. Whole spectrum and PAR sensors are available and calculations of RUE will be performed differently depending on the sensor used. A brief discussion of the difference between whole spectrum and PAR sensors and the difference in calculations is given in Kiniry (1999). The use of a PAR sensor in RUE studies is strongly encouraged.  When measuring radiation, three to five sets of measurements are taken rapidly for each plant plot. A set of measurements consists of 10 measurements above the leaf canopy, 10 below, and 10 more above. The light measurements should be taken between 10:00 am and 2:00 pm local time.  The measurements above and below the leaf canopy are averaged and the fraction of intercepted PAR is calculated for the day from the two values. Daily estimates of the fraction of intercepted PAR are determined by linearly interpolating the measured values. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| BIO\_E, cont. | The *fraction* of intercepted PAR is converted to an *amount* of intercepted PAR using daily values of incident total solar radiation measured with a standard weather station. To convert total incident radiation to total incident PAR, the daily solar radiation values are multiplied by the percent of total radiation that has a wavelength between 400 and 700 mm. This percent usually falls in the range 45 to 55% and is a function of cloud cover. 50% is considered to be a default value.  Once daily intercepted PAR values are determined, the total amount of PAR intercepted by the plant is calculated for each date on which biomass was harvested. This is calculated by summing daily intercepted PAR values from the date of seedling emergence to the date of biomass harvest.  To determine biomass production, aboveground biomass is harvested from a known area of land within the plot. The plant material should be dried at least 2 days at 65°C and then weighed.  RUE is determined by fitting a linear regression for aboveground biomass as a function of intercepted PAR. The slope of the line is the RUE. Figure 14-1 shows the plots of aboveground biomass and summed intercepted photosynthetically active radiation for Eastern gamagrass. (Note that the units for RUE values in the graph, as well as values typically reported in literature, are different from those used by SWAT. To obtain the value used in SWAT, multiply by 10.)  This parameter can greatly change the rate of growth, incidence of stress during the season and the resultant yield. This parameter should be one of the last to be adjusted. Adjustments should be based on research results. Care should be taken to make adjustments based only on data with no drought, nutrient or temperature stress.  Required. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |



Figure 14-1: Aboveground biomass and summed intercepted photosynthetically active radiation for Eastern gamagrass (after Kiniry et al.,1999).

|  |  |
| --- | --- |
| HVSTI | Harvest index for optimal growing conditions.  The harvest index defines the fraction of the aboveground biomass that is removed in a harvest operation. This value defines the fraction of plant biomass that is “lost” from the system and unavailable for conversion to residue and subsequent decomposition. For crops where the harvested portion of the plant is aboveground, the harvest index is always a fraction less than 1. For crops where the harvested portion is belowground, the harvest index may be greater than 1. Two harvest indices are provided in the database, the harvest index for optimal growing conditions (HVSTI) and the harvest index under highly stressed growing conditions (WSYF). |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| HVSTI, cont. | To determine the harvest index, the plant biomass removed during the harvest operation is dried at least 2 days at 65°C and weighed. The total aboveground plant biomass in the field should also be dried and weighed. The harvest index is then calculated by dividing the weight of the harvested portion of the plant biomass by the weight of the total aboveground plant biomass. Plants will need to be grown in two different plots where optimal climatic conditions and stressed conditions are produced to obtain values for both harvest indices.  Required. |
| BLAI | Maximum potential leaf area index.  BLAI is one of six parameters use to quantify leaf area development of a plant species during the growing season. Figure 14-2 illustrates the relationship of the database parameters to the leaf area development modeled by SWAT. |

Figure 14-2: Leaf area index as a function of fraction of growing season for Alamo switchgrass

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| BLAI, cont. | To identify the leaf area development parameters, record the leaf area index and number of accumulated heat units for the plant species throughout the growing season and then plot the results. For best results, several years worth of field data should be collected. At the very minimum, data for two years is recommended. It is important that the plants undergo no water or nutrient stress during the years in which data is collected.  The leaf area index incorporates information about the plant density, so field experiments should either be set up to reproduce actual plant densities or the maximum LAI value for the plant determined from field experiments should be adjusted to reflect plant densities desired in the simulation. Maximum LAI values in the default database correspond to plant densities associated with rainfed agriculture.  The leaf area index is calculated by dividing the green leaf area by the land area. Because the entire plant must be harvested to determine the leaf area, the field experiment needs to be designed to include enough plants to accommodate all leaf area measurements made during the year.  Although measuring leaf area can be laborious for large samples, there is no intrinsic difficulty in the process. The most common method is to obtain an electronic scanner and feed the harvested green leaves and stems into the scanner. Older methods for estimating leaf area include tracing of the leaves (or weighed subsamples) onto paper, the use of planimeters, the punch disk method of Watson (1958) and the linear dimension method of Duncan and Hesketh (1968).  Chapter 5:1 in the Theoretical Documentation reviews the methodology used to calculate accumulated heat units for a plant at different times of the year as well as determination of the fraction of total, or potential, heat units that is required for the plant database. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| BLAI, cont. | The values for BLAI in the plant growth database are based on average plant densities in dryland (rainfed) agriculture. BLAI may need to be adjusted for drought-prone regions where planting densities are much smaller or irrigated conditions where densities are much greater.  Required. |
| FRGRW1 | Fraction of the plant growing season or fraction of total potential heat units corresponding to the 1st point on the optimal leaf area development curve.  Please see Figure 14-2 and the explanation given for parameter BLAI to obtain additional information about this parameter and methods used to measure it.  Required. |
| LAIMX1 | Fraction of the maximum leaf area index corresponding to the 1st point on the optimal leaf area development curve.  Please see Figure 14-2 and the explanation given for parameter BLAI to obtain additional information about this parameter and methods used to measure it.  Required. |
| FRGRW2 | Fraction of the plant growing season or fraction of total potential heat units corresponding to the 2nd point on the optimal leaf area development curve.  Please see Figure 14-2 and the explanation given for parameter BLAI to obtain additional information about this parameter and methods used to measure it.  Required. |
| LAIMX2 | Fraction of the maximum leaf area index corresponding to the 2nd point on the optimal leaf area development curve.  Please see Figure 14-2 and the explanation given for parameter BLAI to obtain additional information about this parameter and methods used to measure it.  Required. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| DLAI | Fraction of growing season when leaf area begins to decline.  Please see Figure 14-2 and the explanation given for parameter BLAI to obtain additional information about this parameter and methods used to measure it.  Required. |
| CHTMX | Maximum canopy height (m).  Maximum canopy height is a straightforward measurement. The canopy height of non-stressed plants should be recorded at intervals throughout the growing season. The maximum value recorded is used in the database.  Required. |
| RDMX | Maximum root depth (m).  To determine maximum rooting depth, plant samples need to be grown on soils without an impermeable layer. Once the plants have reached maturity, soil cores are taken for the entire depth of the soil. Each 0.25 meter increment is washed and the live plant material collected. Live roots can be differentiated from dead roots by the fact that live roots are whiter and more elastic and have an intact cortex. The deepest increment of the soil core in which live roots are found defines the maximum rooting depth.  Required. |
| T\_OPT | Optimal temperature for plant growth (ºC).  Both optimal and base temperatures are very stable for cultivars within a species.  Optimal temperature for plant growth is difficult to measure directly. Looking at Figure 14-3, one might be tempted to select the temperature corresponding to the peak of the plot as the optimal temperature. This would not be correct. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| T\_OPT, cont. | The peak of the plot defines the optimal temperature for leaf development—not for plant growth.  If an optimal temperature cannot be obtained through a review of literature, use the optimal temperature listed for a plant already in the database with similar growth habits.  Review of temperatures for many different plants have provided generic values for base and optimal temperatures as a function of growing season. In situations, where temperature information is unavailable, these values may be used. For warm season plants, the generic base temperature is ~8ºC and the generic optimal temperature is ~25ºC. For cool season plants, the generic base temperature is ~0ºC and the generic optimal temperature is ~13ºC.  Required. |
| T\_BASE | Minimum (base) temperature for plant growth (ºC).  SWAT uses the base temperature to calculate the number of heat units accrued every day. The minimum or base temperature for plant growth varies with growth stage of the plant. However, this variation is ignored by the model—SWAT uses the same base temperature throughout the growing season.  Base temperature is measured by growing plants in growth chambers at several different temperatures. The rate of leaf tip appearance as a function of temperature is plotted. Extrapolating the line to the leaf tip appearance rate of 0.0 leaves/day gives the base or minimum temperature for plant growth. Figure 14-3 plots data for corn. (Note that the line intersects the x-axis at 8°C.)  Required. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| **T\_BASE, cont.** |  |



Figure 14-3: Rate of leaf tip appearance as a function of temperature for corn (after Kiniry et al, 1991)

|  |  |
| --- | --- |
| CNYLD | Normal fraction of nitrogen in yield (kg N/kg yield).  In addition to the amount of plant biomass removed in the yield, SWAT needs to know the amount of nitrogen and phosphorus removed in the yield. The harvested portion of the plant biomass is sent to a testing laboratory to determine the fraction of nitrogen and phosphorus in the biomass.  This value is estimated on a dry weight basis.  Required. |
| CPYLD | Normal fraction of phosphorus in yield (kg P/kg yield).  In addition to the amount of plant biomass removed in the yield, SWAT needs to know the amount of nitrogen and phosphorus removed in the yield. The harvested portion of the plant biomass is sent to a testing laboratory to determine the fraction of nitrogen and phosphorus in the biomass.  This value is estimated on a dry weight basis.  Required. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| PLTNFR1 | Nitrogen uptake parameter #1: normal fraction of nitrogen in plant biomass at emergence (kg N/kg biomass)  In order to calculate the plant nutrient demand throughout a plant’s growing cycle, SWAT needs to know the fraction of nutrient in the total plant biomass (on a dry weight basis) at different stages of crop growth. Six variables in the plant database provide this information: PLTNFR(1), PLTNFR(2), PLTNFR(3), PLTPFR(1), PLTPFR(2), and PLTPFR(3). Plant samples are analyzed for nitrogen and phosphorus content at three times during the growing season: shortly after emergence, near the middle of the season, and at maturity. The plant samples can be sent to testing laboratories to obtain the fraction of nitrogen and phosphorus in the biomass.  Ideally, the plant samples tested for nutrient content should include the roots as well as the aboveground biomass. Differences in partitioning of nutrients to roots and shoots can cause erroneous conclusions when comparing productivity among species if only the aboveground biomass is measured.  Required. |
| PLTNFR2 | Nitrogen uptake parameter #2: normal fraction of nitrogen in plant biomass at 50% maturity (kg N/kg biomass)  Please read the explanation for parameter PLTNFR(1) to obtain additional information about this parameter and methods used to measure it.  Required. |
| PLTNFR3 | Nitrogen uptake parameter #3: normal fraction of nitrogen in plant biomass at maturity (kg N/kg biomass)  Please read the explanation for parameter PLTNFR(1) to obtain additional information about this parameter and methods used to measure it.  Required. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| PLTPFR1 | Phosphorus uptake parameter #1: normal fraction of phosphorus in plant biomass at emergence (kg P/kg biomass)  Please read the explanation for parameter PLTNFR(1) to obtain additional information about this parameter and methods used to measure it.  Required. |
| PLTPFR2 | Phosphorus uptake parameter #2: normal fraction of phosphorus in plant biomass at 50% maturity (kg P/kg biomass)  Please read the explanation for parameter PLTNFR(1) to obtain additional information about this parameter and methods used to measure it.  Required. |
| PLTPFR3 | Phosphorus uptake parameter #3: normal fraction of phosphorus in plant biomass at maturity (kg P/kg biomass)  Please read the explanation for parameter PLTNFR(1) to obtain additional information about this parameter and methods used to measure it.  Required. |
| WSYF | Lower limit of harvest index ((kg/ha)/(kg/ha)).  The value between 0.0 and HVSTI which represents the lowest harvest index expected due to water stress.  Please read the explanation for parameter HVSTI to obtain additional information about this parameter and methods used to measure it.  Required. |

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| **Variable name** | **Definition** |
| USLE\_C | Minimum value of USLE C factor for water erosion applicable to the land cover/plant.  The minimum C factor can be estimated from a known average annual C factor using the following equation (Arnold and Williams, 1995):    where *CUSLE,mn* is the minimum C factor for the land cover and *CUSLE,aa* is the average annual C factor for the land cover.  Required. |
| GSI | Maximum stomatal conductance at high solar radiation and low vapor pressure deficit (m·s-1).  Stomatal conductance of water vapor is used in the Penman-Monteith calculations of maximum plant evapotranspiration. The plant database contains three variables pertaining to stomatal conductance that are required only if the Penman-Monteith equations are chosen to model evapotranspiration: maximum stomatal conductance (GSI), and two variables that define the impact of vapor pressure deficit on stomatal conductance (FRGMAX, VPDFR).  Körner et al (1979) defines maximum leaf diffusive conductance as the largest value of conductance observed in fully developed leaves of well-watered plants under optimal climatic conditions, natural outdoor CO2 concentrations and sufficient nutrient supply. Leaf diffusive conductance of water vapor cannot be measured directly but can be calculated from measurements of transpiration under known climatic conditions. A number of different methods are used to determine diffusive conductance: transpiration measurements in photosynthesis cuvettes, energy balance measurements or weighing experiments, ventilated diffusion porometers and non-ventilated porometers. Körner (1977) measured diffusive conductance using a ventilated diffusion porometer. |

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| **Variable name** | **Definition** |
| GSI, cont. | To obtain maximum leaf conductance values, leaf conductance is determined between sunrise and late morning until a clear decline or no further increase is observed. Depending on phenology, measurements are taken on at least three bright days in late spring and summer, preferably just after a rainy period. The means of maximum leaf conductance of 5 to 10 samples each day are averaged, yielding the maximum diffusive conductance for the species. Due to the variation of the location of stomata on plant leaves for different plant species, conductance values should be calculated for the total leaf surface area.  Required. |
| VPDFR | Vapor pressure deficit (kPa) corresponding to the second point on the stomatal conductance curve.  (The first point on the stomatal conductance curve is comprised of a vapor pressure deficit of 1 kPa and the fraction of maximum stomatal conductance equal to 1.00.)  As with radiation-use efficiency, stomatal conductance is sensitive to vapor pressure deficit. Stockle et al (1992) compiled a short list of stomatal conductance response to vapor pressure deficit for a few plant species. Due to the paucity of data, default values for the second point on the stomatal conductance vs. vapor pressure deficit curve are used for all plant species in the database. The fraction of maximum stomatal conductance (FRGMAX) is set to 0.75 and the vapor pressure deficit corresponding to the fraction given by FRGMAX (VPDFR) is set to 4.00 kPa. If the user has actual data, they should use those values, otherwise the default values are adequate.  Required. |

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| **Variable name** | **Definition** |
| GMAXFR | Fraction of maximum stomatal conductance corresponding to the second point on the stomatal conductance curve.  (The first point on the stomatal conductance curve is comprised of a vapor pressure deficit of 1 kPa and the fraction of maximum stomatal conductance equal to 1.00.)  Please read the explanation for parameter VPDFR to obtain additional information about this parameter and methods used to measure it.  Required. |
| WAVP | Rate of decline in radiation use efficiency per unit increase in vapor pressure deficit.  Stockle and Kiniry (1990) first noticed a relationship between RUE and vapor pressure deficit and were able to explain a large portion of within-species variability in RUE values for sorghum and corn by plotting RUE values as a function of average daily vapor pressure deficit values. Since this first article, a number of other studies have been conducted that support the dependence of RUE on vapor pressure deficit. However, there is still some debate in the scientific community on the validity of this relationship. If the user does not wish to simulate a change in RUE with vapor pressure deficit, the variable WAVP can be set to 0.0 for the plant.  To define the impact of vapor pressure deficit on RUE, vapor pressure deficit values must be recorded during the growing seasons that RUE determinations are being made. It is important that the plants are exposed to no other stress than vapor pressure deficit, i.e. plant growth should not be limited by lack of soil water and nutrients.  Vapor pressure deficits can be calculated from relative humidity (see Chapter 1:2 in Theoretical Documentation) or from daily maximum and minimum temperatures using the technique of Diaz and Campbell (1988) as described by Stockle and Kiniry (1990). The change in RUE with vapor pressure deficit is determined by fitting a linear regression for RUE as a function of vapor pressure deficit. Figure 14-4 shows a plot of RUE as a function of vapor pressure deficit for grain sorghum. |

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| **Variable name** | **Definition** |
| WAVP, cont. |  |



Figure 14-4: Response of radiation-use efficiency to mean daily vapor pressure deficit for grain sorghum (after Kiniry, 1999).

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|  | From Figure 14-4, the rate of decline in radiation-use efficiency per unit increase in vapor pressure deficit, Δ*ruedcl*, for sorghum is 8.4×10-1 g⋅MJ-1⋅kPa-1. When RUE is adjusted for vapor pressure deficit, the model assumes the RUE value reported for BIO\_E is the radiation-use efficiency at a vapor pressure deficit of 1 kPa.  The value of WAVP varies among species, but a value of 6 to 8 is suggested as an approximation for most plants.  Required. |
| CO2HI | Elevated CO2 atmospheric concentration (μL CO2/L air) corresponding the 2nd point on the radiation use efficiency curve.  (The 1st point on the radiation use efficiency curve is comprised of the ambient CO2 concentration, 330 μL CO2/L air, and the biomass-energy ratio reported for BIO\_E) |

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| **Variable name** | **Definition** |
| CO2HI, cont. | In order to assess the impact of climate change on agricultural productivity, SWAT incorporates equations that adjust RUE for elevated atmospheric CO2 concentrations. Values must be entered for CO2HI and BIOEHI in the plant database whether or not the user plans to simulate climate change.  For simulations in which elevated CO2 levels are not modeled, CO2HI should be set to some number greater than 330 ppmv and BIOEHI should be set to some number greater than BIO\_E.  To obtain radiation-use efficiency values at elevated CO2 levels for plant species not currently in the database, plants should be established in growth chambers set up in the field or laboratory where CO2 levels can be controlled. RUE values are determined using the same methodology described in the explanation of BIO\_E.  Required. |
| BIOEHI | Biomass-energy ratio corresponding to the 2nd point on the radiation use efficiency curve.  (The 1st point on the radiation use efficiency curve is comprised of the ambient CO2 concentration, 330 μL CO2/L air, and the biomass-energy ratio reported for BIO\_E.)  Please read the explanation for parameter CO2HI and BIO\_E to obtain additional information about this parameter and methods used to measure it.  Required. |
| RSDCO\_PL | Plant residue decomposition coefficient.  The plant residue decomposition coefficient is the fraction of residue that will decompose in a day assuming optimal moisture, temperature, C:N ratio, and C:P ratio.  This variable was originally in the basin input file (.bsn), but was added to the crop database so that users could vary decomposition by plant species. A default value of 0.05 is used for all plant species in the database.  Required. |

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| **Variable name** | **Definition** |
| ALAI\_MIN | Minimum leaf area index for plant during dormant period (m2/m2).  This variable pertains to perennials and trees only. (The value is never used for other types of plants.) In versions of SWAT prior to SWAT2012, the minimum leaf area index for plants during the dormant period was always set to 0.75. Because this value was not ideal for all plants (trees in particular), users are now allowed to vary the minimum LAI for dormancy.  Please see the explanation given for parameter BLAI to obtain additional information about this parameter and methods used to measure it.  Required. |
| laixco\_tree | Fraction of tree biomass accumulated each year that is converted to residue during dormancy.  This variable pertains to trees only. (The value is never used for other types of plants.) BIO\_LEAF governs the amount of biomass that falls off the tree and is converted to residue when the plant goes dormant in the winter. In versions of SWAT prior to SWAT2012, the fraction of biomass converted to residue at the beginning of dormancy was always defined as 0.30.  Required if land cover is classified as a tree (see IDC). |
| MAT\_YRS | Number of years required for tree species to reach full development (years).  This variable pertains to trees only. (The value is never used for other types of plants.)  Required if land cover is classified as a tree (see IDC). |
| BMX\_peren | Maximum biomass for a forest (metric tons/ha).  This variable pertains to trees only. (The value is never used for other types of plants.)  The maximum biomass for a mature forest stand generally falls in the range of 30-50 metric tons/ha.  Required if land cover is classified as a tree (see IDC). |
| EXT\_COEF | Light extinction coefficient.  This coefficient is used to calculate the amount of intercepted photosynthetically active radiation. In versions of SWAT prior to SWAT2012, the light extinction coefficient was always defined as 0.65. |
| EXT\_COEF (cont) | Differences in canopy structure for a species are described by the number of leaves present (leaf area index) and the leaf orientation. Leaf orientation has a significant impact on light interception and consequently on radiation-use efficiency. More erect leaf types spread the incoming light over a greater leaf area, decreasing the average light intensity intercepted by individual leaves (Figure 14-5). A reduction in light intensity interception by an individual leaf favors a more complete conversion of total canopy-intercepted light energy into biomass.  horizontally oriented leaf  vertically oriented leaf  Figure 14-5: Light intensity interception as a function of leaf orientation. The vertically oriented leaf intercepts 4 units of light while a horizontally oriented leaf of the same length intercepts 6 units of light.  Using the light extinction coefficient value (*kℓ*) in the Beer-Lambert formula (equation 5:2.1.1) to quantify efficiency of light interception per unit leaf area index, more erect leaf types have a smaller *kℓ*.  To calculate the light extinction coefficient, the amount of photosynthetically active radiation (PAR) intercepted and the mass of aboveground biomass (LAI) is measured several times throughout a plant’s growing season using the methodology described in the previous sections. The light extinction coefficient is then calculated using the Beer-Lambert equation:  or  where *TPAR* is the transmitted photosynthetically active radiation, and *PAR* is the incoming photosynthetically active radiation. |
| BM\_DIEOFF | Biomass dieoff fraction.  This coefficient is the fraction above ground biomass that dies off at dormancy. Default value = 0.10. |
| RSR1 | Initial root to shoot ration at the beginning of the growing season. Default = 0.40. |
| RSR2 | Root to shoot ration at the end of the growing season. Default = 0.20. |
| pop1 | Plant population corresponding to the 1st point on the  population lai curve (plants/m^2) |
| frlai1 | Frac of max leaf area index corresponding to the 1st  point on the leaf area development curve (frac) |
| pop2 | Plant population corresponding to the 2nd point on the  population lai curve (plants/m^2) |
| FRLAI2 | Frac of max leaf area index corresponding to the 2nd  point on the leaf area development curve (frac) |
| frsw\_gro | Frac of field capacity to initiate growth of tropical  plants during monsoon season - pcom()%plcur()%iseason  (frac) |
| Wind\_stl | Wind erosion factor for standing live biomass |
| wind\_std | Wind erosion factor for standing dead residue |
| wind\_flat | Wind erosion factor for flat residue |

**fertilizer.frt**

The fertilizer database summarizes the relative fractions of nitrogen and phosphorus pools in the different fertilizers. Information on levels of bacteria in manure is also stored in this file. Appendix A documents the source of parameter values in the database file provided with the model. Below is a partial listing of the fertilizer.frt file.



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the fertilizer.frt file. |
| FERTNM | Name of fertilizer/manure (up to 8 characters allowed).Required. |
| FMINN | Fraction of mineral N (NO3 and NH4) in fertilizer (kg min-N/kg fertilizer).Value should be between 0.0 and 1.0.Required. |
| FMINP | Fraction of mineral P in fertilizer (kg min-P/kg fertilizer).Value should be between 0.0 and 1.0.Required. |
| FORGN | Fraction of organic N in fertilizer (kg org-N/kg fertilizer).Value should be between 0.0 and 1.0.Required. |
| FORGP | Fraction of organic P in fertilizer (kg org-P/kg fertilizer).Value should be between 0.0 and 1.0.Required. |
| FNH3N | Fraction of mineral N in fertilizer applied as ammonia (kg NH3-N/kg min-N).Value should be between 0.0 and 1.0.Required. |
| BACTpdb | Concentration of persistent bacteria in manure/fertilizer (# cfu/g manure).Optional. |

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| --- | --- |
| **Variable name** | **Definition** |
| BACTlpdb | Concentration of less-persistent bacteria in manure/fertilizer (# cfu/g manure).Optional. |
| BACtkddb | Fraction of bacteria in solution.Value should be between 0.0 and 1.0. As the bacteria partition coefficient approaches 0.0, bacteria is primarily sorbed to soil particles. As the bacteria partition coefficient approaches 1.0, bacteria is primarily in solution.Optional. |

**tillage.til**

Tillage operations redistribute nutrients, pesticide and residue in the soil profile. Appendix A documents the source of parameter values in the database file provided with the model.

Below is a partial listing of the tillage.til file.

tillage.til:

TILLNM

EFFMIX

DEPTIL

RANRNS

RIDGE\_HT

RIDGE\_SP

Description

fallplow

0.95

150

75

0

0

genericfallplowingoperation

sprgplow

0.5

125

50

0

0

genericspringplowingoperation

constill

0.25

100

40

0

0

genericconservationtillage

zerotill

0.05

25

10

0

0

genericno-tillmixing

duckftc

0.55

100

15

0

0

duckfootcultivator

fldcult

0.3

100

20

0

0

fieldcultivator

furowout

0.75

25

15

0

0

furrow-outcultivator

marker

0.45

100

15

0

0

marker(cultivator)

rollcult

0.5

25

15

0

0

rollingcultivator

rowcult

0.25

25

15

0

0

rowcultivator

discovat

0.5

25

15

0

0

discovator

leveler

0.5

25

15

0

0

leveler

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| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the tillage.til.res file. |
| TILLNM | Name of fertilizer/manure (up to 8 characters allowed).Required. |
| effmix | | Mixing efficiency of tillage operation.The mixing efficiency specifies the fraction of materials (residue, nutrients and pesticides) on the soil surface which are mixed uniformly throughout the soil depth specified by DEPTIL. The remaining fraction of residue and nutrients is left in the original location (soil surface or layer).Required. |
| deptil | | Depth of mixing caused by the tillage operation (mm).Required. |
| RANRNS | | Random roughness (mm)Required. |
| RIDGE\_HT | | Ridge height (mm)Required. |
| RIDGE\_SP | | Ridge interval (mm)Required. |

**pesticide.pst**

The pesticide database contains parameters that govern pesticide fate and transport in the HRUs. Appendix A documents the source of parameter values in the database file provided with the model. Below is a partial listing of the pesticide.pst file.



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the pestidide.pst file. |
| PESTNM | Name of pesticide/toxin. (up to 17 characters allowed)  Required. |
| SKOC | Soil adsorption coefficient normalized for soil organic carbon content (mg/kg)/(mg/L).  Pesticide in the soil environment can be transported in solution or attached to sediment. The partitioning of a pesticide between the solution and soil phases is defined by the soil adsorption coefficient for the pesticide. The soil adsorption coefficient is the ratio of the pesticide concentration in the soil or solid phase to the pesticide concentration in the solution or liquid phase:    where *Kp* is the soil adsorption coefficient ((mg/kg)/(mg/L) or m3/ton), *Csolidphase* is the concentration of the pesticide sorbed to the solid phase (mg chemical/kg solid material or g/ton), and *Csolution* is the concentration of the pesticide in solution (mg chemical/L solution or g/ton). The definition of the soil adsorption coefficient in this equation assumes that the pesticide sorption process is linear with concentration and instantaneously reversible.  Because the partitioning of pesticide is dependent upon the amount of organic material in the soil, the soil adsorption coefficient input to the model is normalized for soil organic carbon content. The relationship between the soil adsorption coefficient and the soil adsorption coefficient normalized for soil organic carbon content is: |

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| **Variable name** | **Definition** |
| skoc, cont. | where *Kp* is the soil adsorption coefficient ((mg/kg)/(mg/L)), *Koc* is the soil adsorption coefficient normalized for soil organic carbon content ((mg/kg)/(mg/L) or m3/ton), and *orgC* is the percent organic carbon present in the soil.  Required. |
| PST\_WOF | Wash-off fraction.  The wash-off fraction quantifies the fraction of pesticide on the plant canopy that may be dislodged. The wash-off fraction is a function of the nature of the leaf surface, plant morphology, pesticide solubility, polarity of the pesticide molecule, formulation of the commercial product and timing and volume of the rainfall event.  Required. |
| HLIFE\_F | Degradation half-life of the chemical on the foliage (days).  The half-life for a pesticide defines the number of days required for a given pesticide concentration to be reduced by one-half. The half-life entered for a pesticide is a lumped parameter that includes the net effect of volatilization, photolysis, hydrolysis, biological degradation and chemical reactions.  For most pesticides, the foliar half-life is much less than the soil half-life due to enhanced volatilization and photodecomposition. If the foliar half-life is available for the pesticide this value should be used. If the foliar half-life is not available, the foliar half-life can be estimated using the following rules:   1. Foliar half-life is assumed to be less than the soil half-life by a factor of 0.5 to 0.25, depending on vapor pressure and sensitivity to photodegradation. 2. Foliar half-life is adjusted downward for pesticides with vapor pressures less than 10-5 mm Hg. 3. The maximum foliar half-life assigned is 30 days.   Required. |

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| **Variable name** | **Definition** |
| HLIFE\_S | Degradation half-life of the chemical in the soil (days).  The half-life for a pesticide defines the number of days required for a given pesticide concentration to be reduced by one-half. The soil half-life entered for a pesticide is a lumped parameter that includes the net effect of volatilization, photolysis, hydrolysis, biological degradation and chemical reactions.  Required. |
| ap\_ef | Application efficiency.  The fraction of pesticide applied which is deposited on the foliage and soil surface (0.1-1.0). The remainder is lost.  The application efficiency for all pesticides listed in the database is defaulted to 0.75. This variable is a calibration parameter.  Required. |
| PST\_WSOL | Solubility of the chemical in water (mg/L or ppm)  The water solubility value defines the highest concentration of pesticide that can be reached in the runoff and soil pore water. While this is an important characteristic, researchers have found that the soil adsorption coefficient, *Koc*, tends to limit the amount of pesticide entering solution so that the maximum possible concentration of pesticide in solution is seldom reached.  Reported solubility values are determined under laboratory conditions at a constant temperature, typically between 20°C and 30°C.  Required. |

**urban.urb**

The urban database summarizes parameters used by the model to simulate different types of urban areas. Appendix A documents the source of parameter values in the database file provided with the model. Below is a partial listing of the urban.urb file.

urban.urb: Urban parameters

urbnm fimp fcimp curbden urbcoef dirtmx thalf tnconc tpconc tno3conc urbcn2 Description

residen\_high\_den 0.600 0.440 0.240 0.180 225.000 0.750 550.000 223.000 7.200 98.000 Residential-High Density

residen\_med\_den 0.380 0.300 0.240 0.180 225.000 0.750 550.000 223.000 7.200 98.000 Residential-Medium residen\_ml\_den 0.200 0.170 0.240 0.180 225.000 0.750 460.000 196.000 6.000 98.000 Residential-Med/Low residen\_low\_den 0.120 0.100 0.240 0.180 225.000 0.750 460.000 196.000 6.000 98.000 Residential-Low Density

commercial 0.670 0.620 0.280 0.180 200.000 1.600 420.000 240.000 5.500 98.000 Commercial

industrial 0.840 0.790 0.140 0.180 400.000 2.350 430.000 104.000 5.600 98.000 Industrial

transportation 0.980 0.950 0.120 0.180 340.000 3.900 480.000 212.000 6.300 98.000 Transportation

institutional 0.510 0.470 0.120 0.180 340.000 3.900 480.000 212.000 6.300 98.000 Institutional

residential 0.380 0.300 0.240 0.180 225.000 0.750 550.000 223.000 7.200 98.000 Residential

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| --- | --- |
| **Variable name** | **Definition** |
| title | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| Header | Headings for the variables |
| URBNM | 4-character code for urban land type.  The 4-letter codes in the plant growth and urban databases are used by the GIS interfaces to link land use/land cover maps to SWAT plant types. This code is printed to the output files.  When adding a new urban category, the four letter code for the new urban land type must be unique.  Required. |
| FIMP | Fraction total impervious area in urban land type. This includes directly and indirectly connected impervious areas.  Urban areas differ from rural areas in the fraction of total area that is impervious. Construction of buildings, parking lots and paved roads increases the impervious cover in a watershed and reduces infiltration. With development, the spatial flow pattern of water is altered and the hydraulic efficiency of flow is increased through artificial channels, curbing, and storm drainage and collection systems.  Required. |
| FCIMP | Fraction directly connected impervious area in urban land type. |

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| **Variable name** | **Definition** |
| FCIMP, cont. | Impervious areas can be differentiated into two groups—the area that is hydraulically connected to the drainage system and the area that is not directly connected. As an example, assume there is a house surrounded by a yard where runoff from the roof flows into the yard and is able to infiltrate into the soil. The rooftop is impervious but it is not hydraulically connected to the drainage system. In contrast, a parking lot whose runoff enters a storm water drain is hydraulically connected.  When modeling urban areas the connectedness of the drainage system must be quantified. The best methods for determining the fraction total and directly connected impervious areas is to conduct a field survey or analyze aerial photographs.  Required. |
| CURBDEN | Curb length density in urban land type (km/ha).  Curb length may be measured directly by scaling the total length of streets off of maps and multiplying by two. To calculate the density, the curb length is divided by the area represented by the map.  Required. |
| URBCOEF | Wash-off coefficient for removal of constituents from impervious area (mm-1).  Wash off is the process of erosion or solution of constituents from an impervious surface during a runoff event. The original default value for *urbcoef* was calculated as 0.18 mm-1 by assuming that 13 mm of total runoff in one hour would wash off 90% of the initial surface load (Huber and Heaney, 1982). Using sediment transport theory, Sonnen (1980) estimated values for the wash-off coefficient ranging from 0.002-0.26 mm-1. Huber and Dickinson (1988) noted that values between 0.039 and 0.390 mm-1 for the wash-off coefficient give sediment concentrations in the range of most observed values. This variable is used to calibrate the model to observed data.  Required. |
| DIRTMX | Maximum amount of solids allowed to build up on impervious areas (kg/curb km).  Required. |

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| **Variable name** | **Definition** |
| THALF | Number of days for amount of solids on impervious areas to build up from 0 kg/curb km to half the maximum allowed, i.e. 1/2 DIRTMX (days).  Required. |
| TNCONC | Concentration of total nitrogen in suspended solid load from impervious areas (mg N/kg sed).  Required. |
| TPCONC | Concentration of total phosphorus in suspended solid load from impervious areas (mg P/kg sed).  Required. |
| TNO3CONC | Concentration of nitrate in suspended solid load from impervious areas (mg NO3-N/kg sed).  Required. |
| URBCN2 | Curve number for moisture condition II in impervious areas of urban land type.  Required. |

**septic.sep**

Information of water quality or effluent characteristics required to simulate different types of Onsite Wastewater Systems (OWSs) is stored in the septic water quality database. The database file distributed with SWAT includes water quality data for most of conventional, advanced, and failing septic systems. Information contained in the septic water quality database is septic tank effluent flow rate for per capita and effluent characteristics of various septic systems. The database is developed based on the field data summarized by Siegrist et al. (2005), McCray et al. (2005) and OWTS 201 (2005). Below is a partial listing of the septic.sep file.

septic\_parms.dat: Septic parameters - General (Septic type 1-conventional,2-advanced,3-failing)

SEPNM QS BODCONCS TSSCONCS NH4CONCS NO3CONCS NO2CONCS ORGNCONCS MINPS ORGPS FCOLIS

GCON 0.227 170.000 75.000 42.400 0.000 0.000 10.000 6.000 1.000 10000000.0

GADV 0.227 22.000 14.000 18.900 9.600 0.000 3.000 5.100 0.900 543.0

COND 0.227 170.000 75.000 58.000 0.200 0.000 14.000 9.000 1.000 10000000.0

SAS1 0.227 170.000 75.000 60.000 0.000 0.000 10.000 8.500 1.500 10000000.0

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| --- | --- | --- |
| **Variable name** | | **Definition** |
| Title | | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | | Headers for the septic.sep file. |
| SEPNM | Abridged name of a septic system   |  |  | | --- | --- | | sptname | Definition | | GCON | Generic type conventional system | | GADV | Generic type advanced system | | COND | Septic tank with conventional drainfield | | SAS1 | Septic tank with SASa type 1 | | SAS2 | Septic tank with SAS type 2 | | SAS3 | Septic tank with in-tank N removal and SAS | | SAS4 | Septic tank with effluent N removal recycle | | SAS5 | Septic tank with corrugated plastic trickling  Filter | | SAS6 | Septic tank with open-cell form trickling filter | | SPF1 | Single pass sand filter 1 | | SPF2 | Single pass sand filter 2 | | SPF3 | Single pass sand filter 3 | | SPF4 | Single pass sand filter 4 | | RCF1 | At grade recirculating sand filter | | RCF2 | Maryland style RSFb | | RCF3 | RSF | | CWT1 | Septic tank w/ constructed wetland  and surface water discharge | | CWT2 | Municipal wastewater w/ constructed wetland  and surface water discharge 1 | | CWT3 | Municipal wastewater w/ constructed wetland  and surface water discharge 2 | | CWT4 | Municipal wastewater w/ constructed wetland | | CWT5 | Municipal wastewater w/ lagoon and  constructed wetland | | BFL1 | Waterloo biofilter (plastic media) 1 | | BFL2 | Waterloo biofilter (plastic media) 2 | | BFL3 | Peat biofilter | | TXF1 | Recirculating textile filter | | TXF2 | Foam or textile filter effluent | | GFL1 | Septic, recirculating gravel filter,  UV disinfection | | USPT | Untreated Effluent - Texas A&M reference |   a: Sand absorption system  b: Recirculating sand filter  Optional. |

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| QS | Septic tank effluent (STE) flow rate (m3/capita/day). McCray et al. (2005) proposed 0.227 m3/capita/day as the median value for USA based on the data collected from various sources.    R2=0.999877  Figure 34.1 Cumulative frequency distribution for residential septic tank effluent flow rate (after McCray et al., 2005) |
| BODCONCS | 7 day Biochemical oxygen demand in STE (mg/L). BOD for a conventional system is typically 170 mg/L. The value varies greatly for different types of septic systems (See Table A-1 of Siegrist et al., 2005).  Required. |
| TSSCONCS | Total suspended solids in STE (mg/L). TSS for a conventional system is typically 75 mg/L. The value varies greatly for different types of septic systems (See Table A-1 of Siegrist et al., 2005).  Required. |

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| --- | --- |
| **Variable name** | **Definition** |
| NH4CONCS | Ammonium nitrogen in STE (mg-N/L). NH4 for a conventional system is typically 60 mg-N/L (ranging 17~78 mg-N/L). The value varies greatly for different types of septic systems (See Table A-1 of Siegrist et al., 2005).    Figure 34.2 Cumulative frequency distribution for ammonium concentration in the septic tank effluent flow rate (after McCray et al., 2005)  Required. |
| NO3CONCS | Nitrate nitrogen in STE (mg-N/L). NO3 for a conventional system ranges 0~1.94 mg-N/L. The value varies for different types of septic systems (See Table A-1 of Siegrist et al., 2005).  Required. |
| NO2CONCS | Nitrite nitrogen in STE (mg-N/L). NO2 for a conventional system is typically very low.  Required. |
| ORGNCONCS | Organic nitrogen in STE (mg-N/L). ORGN for a conventional system ranges 9.4~15 mg-N/L.  Required. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| minps | Concentration of mineral phosphorus in the septic tank effluent (mg/L). Required. |
| ORGPS | Organic phosphorus in STE (mg-P/L). ORGP for a conventional system is typically 1 mg-p/L.  Required. |
| FCOLIS | Total number of fecal coliform in STE (cfu/100mL). FCOLI for a conventional system is typically 1E7 cfu/100mL. The value varies greatly for different types of septic systems (See Table A-1 of Siegrist et al., 2005).  Required. |

**snow.sno**

The snow.sno file contains the input variables for snow. Below is a partial listing of the snow.sno file.

****

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | The first line is reserved for user comments. This line is not processed by the model and may be left blank.  Optional. |
| header | Headers for the snow.sno file. |
| NAME | Name of the snow parameters |
| FALLTMP | Snowfall temperature (ºC).  Mean air temperature at which precipitation is equally likely to be rain as snow/freezing rain. The snowfall temperature should be between –5 ºC and 5 ºC.  A default recommended for this variable is SFTMP = 1.0.  Required in watersheds where snowfall is significant. |
| MELTTMP | Snow melt base temperature (ºC).  The snow pack will not melt until the snow pack temperature exceeds a threshold value, *Tmlt*. The snow melt base temperature should be between –5 ºC and 5 ºC.  A default recommended for this variable is SMTMP = 0.50.  Required in watersheds where snowfall is significant. |
| MELTMX | Melt factor for snow on June 21 (mm H2O/ºC-day).  If the watershed is in the Northern Hemisphere, SMFMX will be the maximum melt factor. If the watershed is in the Southern Hemisphere, SMFMX will be the minimum melt factor. SMFMX and SMFMN allow the rate of snow melt to vary through the year. The variables account for the impact of snow pack density on snow melt.  In rural areas, the melt factor will vary from 1.4 to 6.9 mm H2O/day-°C (Huber and Dickinson, 1988). In urban areas, values will fall in the higher end of the range due to compression of the snow pack by vehicles, pedestrians, etc. Urban snow melt studies in Sweden (Bengston, 1981; Westerstrom, 1981) reported melt factors ranging from 3.0 to 8.0 mm H2O/day-°C. Studies of snow melt on asphalt (Westerstrom, 1984) gave melt factors of 1.7 to 6.5 mm H2O/day-°C.  If no value for SMFMX is entered, the model will set SMFMX = 4.5.  Required in watersheds where snowfall is significant. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| MELTMN | Melt factor for snow on December 21 (mm H2O/ºC-day).  If the watershed is in the Northern Hemisphere, SMFMN will be the minimum melt factor. If the watershed is in the Southern Hemisphere, SMFMN will be the maximum melt factor. SMFMX and SMFMN allow the rate of snow melt to vary through the year. The variables account for the impact of snow pack density on snow melt.  In rural areas, the melt factor will vary from 1.4 to 6.9 mm H2O/day-°C (Huber and Dickinson, 1988). In urban areas, values will fall in the higher end of the range due to compression of the snow pack by vehicles, pedestrians, etc. Urban snow melt studies in Sweden (Bengston, 1981; Westerstrom, 1981) reported melt factors ranging from 3.0 to 8.0 mm H2O/day-°C. Studies of snow melt on asphalt (Westerstrom, 1984) gave melt factors of 1.7 to 6.5 mm H2O/day-°C.  If no value for SMFMN is entered, the model will set SMFMN = 4.5.  Required in watersheds where snowfall is significant. |
| TIMP | Snow pack temperature lag factor.  The influence of the previous day’s snow pack temperature on the current day’s snow pack temperature is controlled by a lagging factor, . The lagging factor inherently accounts for snow pack density, snow pack depth, exposure and other factors affecting snow pack temperature. TIMP can vary between 0.01 and 1.0. As  approaches 1.0, the mean air temperature on the current day exerts an increasingly greater influence on the snow pack temperature and the snow pack temperature from the previous day exerts less and less influence. As TIMP goes to zero, the snow pack's temperature will be less influenced by the current day's air temperature.  If no value for TIMP is entered, the model will set TIMP = 1.0.  Required in watersheds where snowfall is significant. |
| COVMX | Minimum snow water content (mm H20) |
| COv50 | Fraction of COVMX |

**OPS–** The OPS files contain management operations for fertilizer, pesticide, grazing, harvest, irrigation and sweep.

**harv.ops**

The inputs for grazing are found in the harv.ops file. This operation harvests the portion of the plant designated as yield and removes the yield from the HRU, but allows the plant to continue growing. This operation is used for hay cuttings. A sample harv.ops file is listed below.



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| NAME | Name of harvest operation |
| typ | grain;biomass;residue;tree;tuber; |
| HI\_OVR | Harvest index override ((kg/ha)/(kg/ha))This variable will force the ratio of yield to total aboveground biomass to the specified value. For grain harvest, the harvest index in the plant growth database (plant.dat) is used that assumes that only the seed is being harvested (HI\_OVR is not used in grain harvest). If biomass is cut and removed (for example, in hay cuttings), HIOVR must be used to specify the amount of biomass cut.Optional. |
| EFF | Harvest efficiency. For grain harvest, the harvest efficiency defines the fraction of yield biomass removed by the harvesting equipment, with the remaining yield lost. For biomass harvest, if HARVEFF is close to zero, the cutting or clipping are left on the ground and if HARVEFF is 1.0, all cut biomass (yield) is removed. If the harvest efficiency is not set or 0.00 is entered, the model assumes the user wants to ignore harvest efficiency and sets the fraction to 1.00 so that the entire yield is removed from the HRU. Optional. |
| bm\_min | minimum biomass to allow harvest (kg/ha) |

**graze.ops**

The inputs for grazing are found in the graze.ops file. This operation removes plant biomass at a specified rate and allows simultaneous application of manure. A sample graze.ops file is listed below.



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| NAME | Name of grazing operation |
| fertnm | Name of grazing operation from fertilizer database |
| DAYS | Number of consecutive days grazing takes place in the HRU. |
| EAT | Dry weight of biomass consumed daily ((kg/ha)/day |
| TRAMP | Dry weight of biomass trampled daily ((kg/ha)/day)Trampling becomes significant as the number of animals grazing per hectare increases. This is a very subjective value which is typically set equal to BIO\_EAT, i.e. the animals trample as much as they eat. |
| MANURE | Dry weight of manure deposited daily ((kg/ha)/day). |
| BIO\_min | Minimum plant biomass for grazing (kg/ha) |

**irr.ops**

The inputs for irrigation are found in the irr.ops file. This operation applies water to the HRU on the specified day. A sample irr.ops file is listed below.

|  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- |
| Irrigation\_operation\_datafile |  |  |  |  |  |  |
| NAME | EFF\_FRAC | SURQ\_FRAC | DEP\_MM | SALT | NO3 | PO4 |
| sprinkler\_med | 0.8 | 0.1 | 25 | 100 | 20 | 1 |
| sprinkler\_high | 0.8 | 0.1 | 40 | 100 | 20 | 1 |
| drip | 0.8 | 0.1 | 25 | 100 | 20 | 1 |
| furrow | 0.8 | 0.1 | 25 | 100 | 20 | 1 |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| NAME | Name of irrigation operation |
| EFf | Irrigation in-field efficiency (0-1). |
| surq | Surface runoff ratio (0-1). (.1 is 10% surface runoff) (fraction) |
| dep\_mm | Depth of irrigation water applied on HRU (mm).Required. |
| SALT | Concentration of salt in irrigation (mg/kg). Not currently operational. |
| no3 | Concentration of nitrate in irrigation (mg/kg) |
| po4 | Concentration of phosphate in irrigation |

**chem\_app.ops**

The inputs for sweeping operations are found in the chem\_app.ops file. A sample chem\_app.ops file is listed below.

Chem\_app.ops: Fertilzer and Pesticide operations

PEST\_OP\_NAME FORM OPERATION APP\_EFF FOLIAR\_EFF INJECT\_DEP SURF\_FRAC DRIFT\_POT AERIAL\_UNIF

broadcast solid spread 0.9 0.0 0.0 1.0 0.0 1.0

band solid spread 0.9 0.0 0.0 1.0 0.0 0.5

foliar liquid spray 0.8 0.7 0.0 1.0 0.0 1.0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| NAME | Name of chemical application operation |
| form | solid; liquid |
| op\_typ | operation type-spread; spray; inject; direct |
| app\_eff | application efficiency |
| foliar\_eff | foliar efficiency |
| inject\_dep | injection depth (mm) |
| surf\_frac | surface fraction-amount in upper 10 mm |
| Drift\_pot | drift potential |
| aerial\_unif | aerial uniformity |

**fire.ops**

The inputs for sweeping operations are found in the fire.ops file. A sample fire.ops file is listed below.

Fire.ops: fire operations

NAME CN2\_UPD FR\_BURN

example 0.000 0.000

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| NAME | Name of fire operation |
| CN2\_UPD | change in SCS curve number II value |
| FR\_BURN | fraction burned |

**sweep.ops**

The inputs for sweeping operations are found in the sweep.ops file. A sample sweep.ops file is listed below.



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Headings for variables |
| NAME | Name of sweep operation |
| eff | Removal efficiency of sweeping operation |
| fr\_curb | Availability factor, the fraction of the curb length that is sweepable |

**LUM –** A primary goal of environmental modeling is to assess the impact of human activities on a given system. Central to this assessment is the itemization of the land and water management practices taking place within the system. The primary file used to summarize these practices is the HRU management file (.sch). This file contains input data for planting, harvest, irrigation applications, nutrient applications, pesticide applications, and tillage operations. Information regarding tile drains and urban areas is also stored in this file.

**LANDUSE.LUM**

NEED THIS INFO

Below is a sample LANDUSE.LUM FILE:

landuse.lum: General land use properties

name cal\_group plant\_cov mgt\_ops cn\_lu cons\_prac urb\_lu urb\_ro ovn tiledrain septic fstrip grassww bmpuser

forestmixed null frst null wood\_f up\_down\_slope null null fallow\_nores null null null null null

pasture null past null pasth up\_down\_slope null null fallow\_nores null null null null null

agriculture null agrl csoy rc\_strowres\_p up\_down\_slope null null fallow\_nores null null null null null

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| title | The first line of the landuse.lum file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| Header | Headings for landuse.lum variables |
| name | Name of land use treatments/practice/conditions |
| CAL\_GRP | Calibration group |
| plant\_cov | Plant cover from plants.plt |
| mgt\_ops | Management operation |
| cn\_lu | Landuse curve number identifier (from table) |
| cons\_prac | USLE equation support practice (P) factor |
| urb\_lu | Urban land use |
| urb\_ro | Urban simulation runoff code:  USGS\_REG - simulate using USGS regression equations  Build up/wash off – simulate using build up washoff algorithm  Most large watersheds and river basins contain areas of urban land use. Estimates of the quantity and quality of runoff in urban areas are required for comprehensive management analysis. SWAT calculates runoff from urban areas with the SCS curve number method or the Green & Ampt equation. Loadings of sediment and nutrients are determined using one of two options. The first is a set of linear regression equations developed by the USGS (Driver and Tasker, 1988) for estimating storm runoff volumes and constituent loads. The other option is to simulate the buildup and washoff mechanisms, similar to SWMM – Storm Water Management Model (Huber and Dickinson, 1988). |
| ovn | Manning’s “n” value for overland flow |
| tiledrain | Tile drain file name |
| septic | Septic tank file name |
| fstrip | Filter strip file name |
| grassww | Grassed waterways file name |
| bmpuser | Best management practices file name |

**management.sch**

The inputs management operations are found in the management.sch file. A sample management.sch file is listed below:

management.lum: Management schedules – 2-stage ditch

NAME NUM\_OPS OP MON DAY HUSC OP\_TYPE OP\_PLANT OP\_OVER

csoy 7 1

autoirr\_str.8

fert 0 0 0.140 nh-nh3 null 200.0 FERTILIZER

plnt 0 0 0.150 corn null 0.0 plant CORN BEGIN

hvkl 10 30 1.200 grain corn 0.0 HARVKILL

skip 0 0 0.000 null null 0.0 SKIP\_YEAR

plnt 0 0 0.150 soyb null 0.0 PLANT SOYBEANS

hvkl 10 30 1.200 soyb grain 0.0 HARVKILL

skip 0 0 0.000 null null 0.0 SKIP\_YEAR

cana 0 0

SWAT will simulate different types of management operations. The variables for the different operations will be defined in separate sections. The type of operation simulated is identified by the code given for the variable MGT\_OP.

The different codes for MGT\_OP are:

|  |  |
| --- | --- |
| PCO | **plant community:** this operation initializes the plant community in the HRU |
| PLNT | **planting/beginning of growing season:** this operation initializes the growth of a specific land cover/plant type in the HRU |
| HARV | **harvest only operation:** this operation harvests the portion of the plant designated as yield and removes the yield from the HRU, but allows the plant to continue growing. This operation is used for hay cuttings. |
| HVKL | **harvest and kill operation:** this operation harvests the portion of the plant designated as yield, removes the yield from the HRU and converts the remaining plant biomass to residue on the soil surface. |
| TILL | **tillage operation:** this operation mixes the upper soil layers and redistributes the nutrients/chemicals/etc. within those layers |
| IRRM | **irrigation operation:** this operation applies water to the HRU on the specified day. (IRROPS.DAT) |
| FERT | **fertilizer application:** this operation adds nutrients to the soil in the HRU on the specified day (FERTOPS.DAT) |
| PEST | **pesticide application:** this operation applies a pesticide to the plant and/or soil in the HRU on the specified day |
| GRAZ | **grazing operation:** this operation removes plant biomass at a specified rate and allows simultaneous application of manure. |
| BURN | **burn operation:** the burn operation records the biomass, residue and phosphorus that is burned. |
| SWEP | **street sweeping operation:** this operation removes sediment and nutrient build-up on impervious areas in the HRU. This operation can only be used when the urban build up/wash off routines are activated for the HRU (see IURBAN). |
| SKIP | **skip operation:** this operation skips to the end of the year. |

For each year of management operations provided, the operations must be listed in chronological order starting in January.

For simulations where a certain amount of crop yield and biomass is required, the user can force the model to meet this amount by setting a harvest index target and a biomass target. These targets are effective only if a harvest and kill operation is used to harvest the crop. Variables are listed below.

|  |  |  |
| --- | --- | --- |
| **Variable name** | **Definition** | |
| title | Title for the management.sch file. Optional (may be blank) | |
| header | Header for the management.sch variables | |
| name | Name of the operations | |
| nUM\_OPS | Number of operations following | |
| nUM\_AUTOs |  | |
| OP | Management operation name:**pcom** = plant community**plnt** = beginning of growing season**harv** = harvests the portion of the plant designated as yield and removes the yield from the HRU, but allows the plant to continue to grow.**hvkl** = harvests the portion of the plant designated as yield, removes the yield from the HRU and converts the remaining plant biomass to residue on the soil surface.**till** = mixed the upper soil layers and redistributes the nutrients/chemicals, etc within thos layers**irrm** = applies water to the HRU on the specified day**fert** = adds nutrients to the soil in the specified day**pest** = applies a pesticide to the plant and/or soil in the HRU on a specified day**graz** = removes plant biomass at a specified rate and allows simultaneous application of manure**burn** = burning**swep** = removes sediment and nutrient build up on impervious areas in the HRU. This operation can only be used when the urban build up/wash off routines are activated for the HRU (see IURBAN) **skip** | |
| MON | Month operation takes place.Either MONTH/DAY or HUSC is required. |
| DAY | Day operation takes place.Either MONTH/DAY or HUSC is required. |
| HUSC | Fraction of total base zero heat units at which operation takes place. Heat unit scheduling is explained in Chapter 5:1 of the Theoretical Documentation. If MONTH and DAY are not provided, HUSC must be set to a value.  Either MONTH/DAY or HUSC is required. |
| OP\_CHAR | Operation type character |
| op\_PLANT | Plant name in community |
| op3 | Harvest index override |

**CNTABLE.LUM**

NEED THIS INFO

Below is a sample CNTABLE.LUM FILE:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| title | The first line of the cntable.lum file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| Header | Headings for cntable.lum variables |
| name | Name of land use treatments/practice/conditions |
| cnA | Land use curve number A |
| cnb | Land use curve number B |
| cnc | Land use curve number C |
| cnd | Land use curve number D |
|  | Land use description follows (not read by model) |

**CONS\_PRACTICE.LUM**

NEED THIS INFO

Below is a sample CONS\_PRACTICE.LUM FILE:

Table 5. P Factor and Slope Length Data for Conservation Practices From USLE Handbook

NAME P\_FACTOR SLOPE\_LEN\_MAX DESCRIPTION

up\_down\_slope 1.0 121. Up\_and\_down\_slope

cross\_slope 0.75 121. Cross\_slope\_tillage

contour\_farming 0.50 121. Contour\_tillage

strip\_cros\_slope 0.37 121. Strip\_cropping\_cross\_slope

strip\_contour 0.25 121. Strip\_cropping\_contour

contour\_1-2 0.30 121. Contour\_tillage\_1-2%\_slopes

contour\_3-5 0.50 91. Contour\_tillage\_3-5%\_slopes

contour\_6-8 0.50 61. Contour\_tillage\_6-8%\_slopes

contour\_9-12 0.60 36. Contour\_tillage\_9-12%\_slopes

contour\_13-16 0.70 24. Contour\_tillage\_13-16%\_slopes

contour\_17-20 0.80 18. Contour\_tillage\_17-20%\_slopes

contour\_21-25 0.90 15. Contour\_tillage\_21-25%\_slopes

strip\_1-2\_past 0.30 244. Strip\_cropping\_1-2%\_slopes\_with-pasture

strip\_1-2\_row 0.60 244. Strip\_cropping\_1-2$\_slopes\_with-rowcrops

strip\_3-5\_past 0.25 183. Strip\_cropping\_3-5%\_slopes\_with-pasture

strip\_3-5\_row 0.50 183. Strip\_cropping\_3-5%\_slopes\_with-rowcrops

strip\_6-8\_past 0.25 122. Strip\_cropping\_6-8%\_slopes\_with-pasture

strip\_6-8\_row 0.50 122. Strip\_cropping\_6-8%\_slopes\_with-rowcrops

strip\_9-12\_past 0.30 73. Strip\_cropping\_9-12%\_slopes\_with-pasture

strip\_9-12\_row 0.60 73. Strip\_cropping\_9-12%\_slopes\_with-rowcrops

strip\_13-16\_past 0.35 49. Strip\_cropping\_13-16%\_slopes\_with-pasture

strip\_13-16\_row 0.70 49. Strip\_cropping\_13-16%\_slopes\_with-rowcrops

strip17-20\_past 0.40 36. Strip\_cropping\_17-20%\_slopes\_with-pasture

strip\_17-20\_row 0.80 36. Strip\_cropping\_17-20%\_slopes\_with-rowcrops

strip\_21-25\_past 0.45 30. Strip\_cropping\_21-25%\_slopes\_with-pasture

strip\_21-25\_row 0.90 30. Strip\_cropping\_21-25%\_slopes\_with-rowcrops

ter\_1-2\_sodout 0.12 121. terraces\_1-2%\_slopes\_sod-outlet

ter\_1-2\_undout 0.05 121. terraces\_1-2%\_slopes\_underflow-outlet

ter\_3-8\_sodout 0.50 76. terraces\_3-8%\_slopes\_sod-outlet

ter\_3-8\_undout 0.25 76. terraces\_3-8%\_slopes\_underflow--outlet

ter\_9-12\_sodout 0.60 61. terraces\_9-12%\_slopes\_sod-outlet

ter\_9-12\_undout 0.30 61. terraces\_9-12%\_slopes\_underflow--outlet

ter\_13-16\_sodout 0.70 45. terraces\_13-16%\_slopes\_sod-outlet

**ter\_13-16\_undout 0.35 45. terraces\_13-16%\_slopes\_underflow--outlet**

**ter\_17-20\_sodout 0.80 45. terraces\_17-20%\_slopes\_sod-outlet**

**ter\_17-20\_undout 0.40 45. terraces\_17-20%\_slopes\_underflow--outlet**

**ter\_21-25\_sodout 0.90 30. terraces\_21-25%\_slopes\_sod-outlet**

**ter\_21-25\_undout 0.45 30. terraces\_21-25%\_slopes\_underflow--outlet**

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| title | The first line of the cons\_practice.lum file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| Header | Headings for cons\_practice.lum variables |
| name | Name of conservation practice |
| pfac | Usle P factor |
| sl\_len\_mx | Maximum slope length (m) |

**OVN\_TABLE.LUM**

NEED THIS INFO

Below is a sample OVN\_TABLE.LUM FILE:

ovn\_table.lum: Typical Manning's n values - LREW Sub Water

NAME OVN OVN\_MIN OVN\_ MAX DESCRIPTION

fallow\_nores 0.010 0.008 0.012 Fallow\_no\_residue

convtill\_nores 0.090 0.060 0.120 Conventional\_tillage\_no\_residue

convtill\_res 0.190 0.160 0.220 Conventional\_tillage\_residue

chisplow\_nores 0.090 0.060 0.120 Chisel\_plow\_no\_residue

chisplow\_res 0.130 0.100 0.160 Chisel\_plow\_residue

falldisk\_res 0.400 0.300 0.500 Fall\_disking\_residue

notill\_nores 0.070 0.040 0.100 No\_till\_no\_residue

notill\_0.5-1res 0.120 0.070 0.170 No\_till\_0.5-1\_t/ha\_residue

notill\_2-9res 0.300 0.170 0.470 No\_till\_2-9\_t/ha\_residue

range\_sparse 0.130 0.130 0.130 Rangeland\_sparse\_cover

range\_20cover 0.600 0.600 0.600 Rangeland\_20%\_cover

shortgrass 0.150 0.100 0.200 Short\_grass\_prairie

densegrass 0.240 0.170 0.300 Dense\_grass

bermudagrass 0.410 0.300 0.480 Bermudagrass

forest\_light 0.400 0.300 0.500 Forest\_light\_fair

forest\_med 0.600 0.500 0.700 Forest\_medimum\_good

forest\_heavy 0.800 0.700 0.900 Forest\_heavy

urban\_asphalt 0.110 0.110 0.110 Urban\_asphalt

urban\_concrete 0.012 0.012 0.012 Urban\_concrete

urban\_rubble 0.024 0.024 0.024 Urban\_rubble

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| title | The first line of the ovn\_table.lum file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| Header | Headings for ovn\_table.lum variables |
| name | Name of conservation practice |
| ovn | Overland flow mannings n – mean |
| ovn\_min | Overland flow mannings n – min |
| ovn\_max | Overland flow mannings n - max |

**CHG –** The change section includes the files for soft calibration simulation runs in SWAT+.

**codes.cal**

The codes.cal file contains the input variables for the characteristics of the calibration update properties. Below is a sample codes.cal file:

codes.cal

HYD\_HRU HYD\_HRUL PLT SED NUT CHSED CHNUT RES

n n n n n n n n

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| title | The first line of the codes.cal file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| Header | Headings for codes.cal variables |
| hyd\_hru | if y, calibrate hydrologic balance for hru by land use in each region |
| hyd\_hru1 | if y, calibrate hydrologic balance for hru\_lte by land use in each region |
| PLT | if y, calibrate plant growth by land use (by plant) in each region |
| sed | if y, calibrate sediment yield by land use in each region |
| nut | if y, calibrate nutrient balance by land use in each region |
| chsed | if y, calibrate channel widening and bank accretion by stream order |
| chnut | if y, calibrate channel nutrient balance by stream order |
| res | if y, calibrate reservoir budgets by reservoir |

**cal\_parms.cal**

The cal\_parms.cal file contains the input variables for the characteristics of the calibration update properties. Below is a sample cal\_parms.cal file:

cal\_parms.cal

9

NAME OBJ\_TYP ABSMIN ABSMAX UNITS

cn2 hru 25 98 null

usle\_p hru 0 1 null

ovn hru 0.01 30 null

elev hru 0 5000 m

slope hru 0 1 m/m

slope\_len hru 10 150 m

lat\_ttime hru 0 180 days

lat\_sed hru 0 5000 g/L

lat\_len hru 0 150 m

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| title | The first line of the cal\_parms.cal file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| mchg\_par | Maximum number of calibration parm changes |
| Header | Headings for cal\_parms.cal variables |
| name | cn2, esco, awc, etc. |
| ob\_typ | object type the parameter is associated with (hru, chan, res, basin, etc) |
| absmin | minimum range for variable |
| absmax | maximum change for variable |
| units | units used for each parameter |

**calibration.cal**

The calibration.cal file contains the input variables for the characteristics of the calibration update properties. Below is a sample calibration.cal file:

calibratio

8

NAME

CHG\_TYPE

VAL

CONDS

LYR1

LYR2

YEAR1

YEAR2

DAY1

DAY2

NUM\_TOT

k

pctchg

25

0

1

1

0

0

0

0

0

k

pctchg

20

0

1

2

0

0

0

0

0

k

pctchg

20

0

4

6

0

0

0

0

0

k

pctchg

27

0

0

0

0

0

0

0

0

k

pctchg

25

1

1

2

0

0

0

0

0

hsg

=

0

D

k

pctchg

25

1

1

1

0

0

0

0

0

texture

=

0

fsl

k

pctchg

25

2

1

1

0

0

0

0

0

texture

=

0

fsl

landuse

=

0

past

k

pctchg

25

2

1

1

0

0

0

0

6

1 -3 4 -8 12 -18

texture

=

0

FSL

landuse

=

0

past

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the calibration.cal file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| MCAL | Total number of calibration updates in the file |
| NAME | Name of SWAT+ variable (NAME column from cal\_parms.upd file) |
| CHG\_TYPE | Type of change (‘absval’, ‘abschg’, ‘pctchg’) |
| VAL | Value of change |
| CONDS | Number of conditions in following lines |
| LYR1 | First layer in range for soil variables (input == 0 assumes all layers) |
| LYR2 | Last layer in range for soil variables |
| YEAR1 | First year of update (for precip and temp) |
| YEAR2 | Last year of update (for precip and temp) |
| DAY1 | First day in range (for precip and temp) |
| DAY2 | Last day in range (for precip and temp) |
| num\_TOT | Total number of objects to follow |
| elem\_cnt1 | Number of elements modified |

**ls\_parms.cal**

The ls\_parms.cal file contains the input variables for the characteristics of the calibration parameter properties. Below is a sample ls\_parms.cal file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the ls\_parms.cal file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| MLSP | Total number of parameter updates in the file |
| NAME | Name of SWAT+ variable (NAME column from cal\_parms.upd file) |
| CHG\_TYPE | Type of change (‘absval’, ‘abschg’, ‘pctchg’) |
| NEG | Negative limit of change |
| POS | Positive limit of change |
| LO | Lower limit of parameter |
| up | Upper limit of parameter |

**ls\_regions.cal**

The ls\_regions.cal file contains the input variables for the characteristics of land use regions parameter properties for HRUs. Below is a sample ls\_regions.cal file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the ls\_regions.cal file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| mlscal | Total number of regions updates in the file |
| NAME | Regions calibration name |
| LUM\_NUM | Total number of land use regions in following lines |
| num\_reg | The number of elements in following lines |
| reg | Elements count |
| NAME | Name of the land use management regions |
| SRR | Surface runoff ratio – surface runoff/precip |
| LFR | Lateral flow ratio – soil lat flow/precip |
| PCR | Percolation ratio – perc/precip |
| etr | ET ratio – ET/precip |
| tfr | Tile flow ratio – tile flow/total runoff |
| sed | Sediment yield (t/ha or t) |
| orgn | Organic N yield (kg/ha or kg) |
| orgp | Organic P yield (kg/ha or kg) |
| no3 | Nitrate yield (kg/ha or kg) |
| solp | Soluble P yield (kg/ha or kg) |

**ch\_orders.cal**

The ch\_orders.cal file contains the input variables for the characteristics of channel orders parameter properties for

SWAT HRUs. Below is a sample ch\_orders.cal file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the chn\_orders.cal file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| Mreg | Total number of stream order updates in the file |
| NAME | Regions calibration name |
| ORD\_NUM | Total number of stream orders in following lines |
| NSPU | The number of elements in following lines |
| elem\_cnt |  |
| name | Order name |
| chw | Channel widening (mm/yr) |
| chd | Channel down cutting or accretion (mm/yr) |
| HC | Head Cut advance (m/yr) |
| fpd | Flood plain accretion (mm/yr) |

**ch\_parms.cal**

The ch\_parms.cal file contains the input variables for the characteristics of land use parameter properties for

SWAT HRUs. Below is a sample ch\_parms.cal file:

This example is not good (didn’t know what values should be) gsm

cal\_parms.cal

5

NAME CH\_TYP NEG POS LO UP

cn2 hru 25 98 null

usle\_p hru 0 1 null

ovn hru 0.01 30 null

elev hru 0 5000 m

slope hru 0 1 m/m

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the chan\_parms.cal file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| Mchp | Total number of stream order updates in the file |
| HEADER |  |
| NAME | Regions calibration name |
| CH\_TYP |  |
| NEG |  |
| POS |  |
| LO |  |
| UP |  |

**INIT –** The initial files includes initialization data for pesticide and plants.

**initial.pst**

The initial.pst file contains the input variables for the characteristics of the pesticide properties. Below is a sample initial.pst file:

initial.pst

NUMB

NAME

NUM

NAME

PLT

SOIL

ENR

1

Example1

3

atrazine

0.5

0.0

dual

0.2

2.0

aatrex

0.1

2.0

2

Example2

1

atrazine

0

0.0

.

0.0

0.0

0.0

2.0

|  |  |
| --- | --- |
| TITLE | The first line of the initial.pst file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| Header |  |
| NUMb | Number of pesticides in community |
| Name |  |
| num |  |
| EXCO\_DF | Name of export coefficient file for pesticide community |
| DR\_DF | Name of delivery ratio file for pesticide community |
| NAME | Name in pesticide community |
| PLT | Amount of pesticide on plant at start of simulation (kg/ha) |
| SOIL | Amount of pesticide in soil at start of simulation (kg/ha) |
| ENR | Pesticide enrichment ratio |

**initial.plt**

The initial.plt file contains the input variables for the characteristics of the plant community properties. Below is a sample initial.plt file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| header | Headings for the variables |
| NAME | Name of plant community |
| numb |  |
| PLANTS\_COM | Number of plants in the community |
| CPNM | Plant name (from plants.plt database file) |
| IGRO | Land cover status code.This code informs the model whether or not a land cover is growing at the beginning of the simulation.  1. no land cover growing 2. land cover growing   Required. |

|  |  |
| --- | --- |
| LAI | Initial leaf area index.If a land cover is growing at the beginning of the simulation (IGRO = 1), the leaf area index of the land cover must be defined.Required if IGRO = 1. |
| BIOMS | Initial dry weight biomass (kg/ha).If a land cover is growing at the beginning of the simulation (IGRO = 1), the initial biomass must be defined.Required if IGRO = 1. |
| PHUACC | Total number of heat units or growing degree days needed to bring plant to maturity.  This value is needed only if a land cover is growing at the beginning of the simulation (IGRO = 1). Calculation of PHU\_PLT is reviewed in Chapter 5:1 of the Theoretical Documentation.  Required if IGRO = 1. |
| POP | Plant population |
| YRSMAT | Years to maturity |
| RSDIN | Initial residue cover (kg/ha) |

**SOILS –** The soils data used by SWAT+ can be divided into two groups, physical characteristics and chemical characteristics. The physical properties of the soil govern the movement of water and air through the profile and have a major impact on the cycling of water within the HRU. Inputs for chemical characteristics are used to set initial levels of the different chemicals in the soil. While the physical properties are required, information on chemical properties is optional. The soil input (.sol) file defines the physical properties for all layers in the soil.

**soils.sol**

The soils.sol file contains the input variables for the characteristics of the soil properties. Below is a partial sample soils.sol file (four layer soil):



|  |  |  |
| --- | --- | --- |
| TITLE | The first line of the .sol file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. | |
| header |  | |
| SNAM | Soil name | |
| NLY | Number of layers in the soil | |
| HYDGRP | Soil hydrologic group (A, B, C, or D).  Required only for the SWAT ArcView interface.  The U.S. Natural Resource Conservation Service (NRCS) classifies soils into four hydrologic groups based on infiltration characteristics of the soils. NRCS Soil Survey Staff (1996) defines a hydrologic group as a group of soils having similar runoff potential under similar storm and cover conditions. Soil properties that influence runoff potential are those that impact the minimum rate of infiltration for a bare soil after prolonged wetting and when not frozen. These properties are depth to seasonally high water table, saturated hydraulic conductivity, and depth to a very slowly permeable layer. The definitions for the different classes are: | |
| A  B | Soils having high infiltration rates even when thoroughly wetted, consisting chiefly of sands or gravel that are deep and well to excessively drained. These soils have a high rate of water transmission (low runoff potential).  Soils having moderate infiltration rates when thoroughly wetted, chiefly moderately deep to deep, moderately well to well drained, with moderately fine to moderately coarse textures. These soils have a moderate rate of water transmission. |

|  |  |  |
| --- | --- | --- |
| **Variable name** | **Definition** | |
| HYDGRP, cont. | C  D | Soils having slow infiltration rates when thoroughly wetted, chiefly with a layer that impedes the downward movement of water or of moderately fine to fine texture and a slow infiltration rate. These soils have a slow rate of water transmission (high runoff potential).  Soils having very slow infiltration rates when thoroughly wetted, chiefly clay soils with a high swelling potential; soils with a high permanent water table; soils with a clay pan or clay layer at or near the surface; and shallow soils over nearly impervious materials. These soils have a very slow rate of water transmission. |

Guidelines used by USDA Soil Survey to categorize soils into Hydrologic Groups are summarized in Table 22-1.

Table 22-1: Hydrologic Group Rating Criteria

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
|  | **Hydrologic Soil Groups** | | | |
| **Criteria\*** | **A** | **B** | **C** | **D** |
| Final constant infiltration rate (mm/hr) | 7.6-11.4 | 3.8-7.6 | 1.3-3.8 | 0-1.3 |
| Mean permeability: surface layer (mm/hr) | > 254.0 | 84.0-254.0 | 8.4-84.0 | < 8.4 |
| Mean permeability: most restrictive layer below the surface layer to a depth of 1.0 m (mm/hr) | > 254.0 | 84.0-254.0 | 8.4-84.0 | < 8.4 |
| Shrink-swell potential: most restrictive layer\*\* | Low | Low | Moderate | High,  Very High |
| Depth to bedrock or cemented pan (mm) | > 1016 | > 508 | > 508 | < 508 |
| DUAL HYDROLOGIC GROUPS | **A/D** | **B/D** | **C/D** |  |
| Mean depth to water table (m) | < 0.61 | < 0.61 | < 0.61 |  |

\* These criteria are guidelines only. They are based on the theory that the minimum permeability occurs within the uppermost 50 cm. If the minimum permeability occurs between a depth of 50 to 100 cm, then the Hydrologic Soil Group is increased one group. For example, C to B. If the minimum permeability occurs below a depth of 100 cm, the Hydrologic Soil Group is based on the permeability above 100 cm, using the rules previously given.

\*\* Shrink-swell potential is assigned to a profile using the following guidelines:

Low: All soils with sand, loamy sand, sandy loam, loam or silt loam horizons that are at least 50 cm thick from the surface without a clay horizon within 100 cm of the surface.

Medium: All soils with clay loam horizons within 50 cm of the surface or soils with clay horizons from 50 to 100 cm beneath the surface.

High: All soils with clay horizons within 50 cm of the surface. Lower the shrink-swell potential one class when kaolinite clay is dominant.

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| ZMX | Maximum rooting depth of soil profile (mm).  If no depth is specified, the model assumes the roots can develop throughout the entire depth of the soil profile. |
| Anion\_EXCL | Fraction of porosity (void space) from which anions are excluded.  Most soil minerals are negatively charged at normal pH and the net interaction with anions such as nitrate is a repulsion from particle surfaces. This repulsion is termed negative adsorption or anion exclusion.  Anions are excluded from the area immediately adjacent to mineral surfaces due to preferential attraction of cations to these sites. This process has a direct impact on the transport of anions through the soil for it effectively excludes anions from the slowest moving portion of the soil water volume found closest to the charged particle surfaces (Jury et al, 1991). In effect, the net pathway of the anion through the soil is shorter than it would be if all the soil water had to be used (Thomas and McMahon, 1972).  If no value for ANION\_EXCL is entered, the model will set ANION\_EXCL = 0.50. |
| CRK | Potential or maximum crack volume of the soil profile expressed as a fraction of the total soil volume.  To accurately predict surface runoff and infiltration in areas dominated by Vertisols, the temporal change in soil volume must be quantified. Bronswijk (1989, 1990) outlines methods used to determine the maximum crack volume. |
| Texture | Texture of soil layer.  This data is not processed by the model and the line may be left blank. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Z(layer #) | Depth from soil surface to bottom of layer (mm). |
| BD(layer #) | Moist bulk density (Mg/m3 or g/cm3).  The soil bulk density expresses the ratio of the mass of solid particles to the total volume of the soil, *ρb = MS /VT*. In moist bulk density determinations, the mass of the soil is the oven dry weight and the total volume of the soil is determined when the soil is at or near field capacity. Bulk density values should fall between 1.1 and 1.9 Mg/m3. |
| AWC(layer #) | Available water capacity of the soil layer (mm H2O/mm soil).  The plant available water, also referred to as the available water capacity, is calculated by subtracting the fraction of water present at permanent wilting point from that present at field capacity,  where *AWC* is the plant available water content, *FC* is the water content at field capacity, and *WP* is the water content at permanent wilting point.  Available water capacity is estimated by determining the amount of water released between in situ field capacity (the soil water content at soil matric potential of -0.033 MPa) and the permanent wilting point (the soil water content at soil matric potential of -1.5 MPa). |
| K(layer #) | Saturated hydraulic conductivity (mm/hr).  The saturated hydraulic conductivity, Ksat, relates soil water flow rate (flux density) to the hydraulic gradient and is a measure of the ease of water movement through the soil. Ksat is the reciprocal of the resistance of the soil matrix to water flow. |
| CBN(layer #) | Organic carbon content (% soil weight).  When defining by soil weight, the soil is the portion of the sample that passes through a 2 mm sieve. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| CLAY(layer #) | Clay content (% soil weight).  The percent of soil particles which are < 0.002 mm in equivalent diameter. |
| SILT(layer #) | Silt content (% soil weight).  The percentage of soil particles which have an equivalent diameter between 0.05 and 0.002 mm. |
| SAND(layer #) | Sand content (% soil weight).  The percentage of soil particles which have a diameter between 2.0 and 0.05 mm. |
| ROCK(layer #) | Rock fragment content (% total weight).  The percent of the sample which has a particle diameter > 2 mm, i.e. the percent of the sample which does not pass through a 2 mm sieve. |
| ALB(top layer) | Moist soil albedo.  The ratio of the amount of solar radiation reflected by a body to the amount incident upon it, expressed as a fraction. The value for albedo should be reported when the soil is at or near field capacity. |
| USLE\_K(top layer) | USLE equation soil erodibility (K) factor (units: 0.013 (metric ton m2 hr)/(m3-metric ton cm)).  Some soils erode more easily than others even when all other factors are the same. This difference is termed soil erodibility and is caused by the properties of the soil itself. Wischmeier and Smith (1978) define the soil erodibility factor as the soil loss rate per erosion index unit for a specified soil as measured on a unit plot. A unit plot is 22.1-m (72.6-ft) long, with a uniform length-wise slope of |

|  |  |  |
| --- | --- | --- |
| **Variable name** | | **Definition** |
| USLE\_K, cont. | | 9-percent, in continuous fallow, tilled up and down the slope. Continuous fallow is defined as land that has been tilled and kept free of vegetation for more than 2 years. The units for the USLE soil erodibility factor in MUSLE are numerically equivalent to the traditional English units of 0.01 (ton acre hr)/(acre ft-ton inch).  Wischmeier and Smith (1978) noted that a soil type usually becomes less erodible with decrease in silt fraction, regardless of whether the corresponding increase is in the sand fraction or clay fraction.  Direct measurement of the erodibility factor is time consuming and costly. Wischmeier et al. (1971) developed a general equation to calculate the soil erodibility factor when the silt and very fine sand content makes up less than 70% of the soil particle size distribution. |
|  |  | |
|  | | where KUSLE is the soil erodibility factor, M is the particle-size parameter, OM is the percent organic matter (%), csoilstr is the soil structure code used in soil classification, and cperm is the profile permeability class.  The particle-size parameter, M, is calculated    where msilt is the percent silt content (0.002-0.05 mm diameter particles), mvfs is the percent very fine sand content (0.05-0.10 mm diameter particles), and mc is the percent clay content (< 0.002 mm diameter particles).  The percent organic matter content, OM, of a layer can be calculated:    where orgC is the percent organic carbon content of the layer (%). |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| USLE\_K, cont. | Soil structure refers to the aggregation of primary soil particles into compound particles which are separated from adjoining aggregates by surfaces of weakness. An individual natural soil aggregate is called a ped. Field description of soil structure notes the shape and arrangement of peds, the size of peds, and the distinctness and durability of visible peds. USDA Soil Survey terminology for structure consists of separate sets of terms defining each of these three qualities. Shape and arrangement of peds are designated as type of soil structure; size of peds as class; and degree of distinctness as grade.  Angular Blocky: bounded by planes intersecting at relatively sharp angles  Subangular Blocky: having mixed rounded and plane faces with vertices mostly rounded  The soil-structure codes for the equation are defined by the type and class of soil structure present in the layer. There are four primary types of structure, several of which are further broken down into subtypes:  -Platy, with particles arranged around a plane, generally horizontal  -Prismlike, with particles arranged around a verticle line and bounded by relatively flat vertical surfaces  Prismatic: without rounded upper ends  Columnar: with rounded caps  -Blocklike or polyhedral, with particles arranged around a point and bounded by flat or rounded surfaces which are casts of the molds formed by the faces of surrounding peds  -Spheroidal or polyhedral, with particles arranged around a point and bounded by curved or very irregular surfaces that are not accomodated to the adjoining aggregates  Granular: relatively non-porous  Crumb: very porous  The size criteria for the class will vary by type of structure and are summarized in Table 22-2. |

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| USLE\_K, cont. | Table 22-2: Size classes of soil structure   |  |  |  |  |  | | --- | --- | --- | --- | --- | |  | **Shape of structure** | | | | | **Size Classes** | **Platy** | **Prismatic and Columnar** | **Blocky** | **Granular** | | Very fine | < 1 mm | < 10 mm | < 5 mm | < 1 mm | | Fine | 1-2 mm | 10-20 mm | 5-10 mm | 1-2 mm | | Medium | 2-5 mm | 20-50 mm | 10-20 mm | 2-5 mm | | Coarse | 5-10 mm | 50-100 mm | 20-50 mm | 5-10 mm | | Very coarse | > 10 mm | > 100 mm | > 50 mm | > 10 mm | |

The codes assigned to *csoilstr* are:

1. very fine granular
2. fine granular
3. medium or coarse granular
4. blocky, platy, prismlike or massive

Permeability is defined as the capacity of the soil to transmit water and air through the most restricted horizon (layer) when moist. The profile permeability classes are based on the lowest saturated hydraulic conductivity in the profile. The codes assigned to *cperm* are:

1. rapid (> 150 mm/hr)
2. moderate to rapid (50-150 mm/hr)
3. moderate (15-50 mm/hr)
4. slow to moderate (5-15 mm/hr)
5. slow (1-5 mm/hr)
6. very slow (< 1 mm/hr)

Williams (1995) proposed an alternative equation:



where *fcsand* is a factor that gives low soil erodibility factors for soils with high coarse-sand contents and high values for soils with little sand, *fcl-si* is a factor that gives low soil erodibility factors for soils with high clay to silt ratios, *forgc* is a factor that reduces soil erodibility for soils with high organic carbon content, and *fhisand* is a factor that reduces soil erodibility for soils with extremely high sand contents. The factors are calculated:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| USLE\_K, cont. |  |





where *ms* is the percent sand content (0.05-2.00 mm diameter particles), *msilt* is the percent silt content (0.002-0.05 mm diameter particles), *mc* is the percent clay content (< 0.002 mm diameter particles), and *orgC* is the percent organic carbon content of the layer (%).

|  |  |
| --- | --- |
| EC(layer #) | Electrical conductivity (dS/m). |
| CAL(layer #) | Soil CaCo3 (%). (0 – 50%) |
| PH(layer #) | Soil Ph (3-10) |

**nutrients.sol**

The nutrients.sol file Soil nutrient parameters.

Below is a sample nutrients.sol file (one layer soil):

nutrients.sol Soil nutrient parameter - Water\_LS2\_Take2

NAME EXP\_CO TOTAL\_N MINN ORGN TOTAL\_P MINP ORGP WAT\_SOLP H3A\_P MEHLICH\_P BRAY\_STRONG\_P

soilnut001 0.001 13 6.85 3.34 3.22 3.66 0.39 0.16 0.26 1.22 0.85

|  |  |
| --- | --- |
| TITLE | The first line of the nutrients.sol file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| header |  |
| name | Nutrient name |
| EXP\_CO | Depth coefficient to adjust concentrations for depth |
| TOTALN | Total N in soil (ppm) |
| INORGN | Inorganic N in soil surface (ppm) |
| ORGN | Organic N in soil surface (ppm) |
| TOTALP | Total P in soil surface (ppm) |
| INORGP | Inorganic P in soil surface (ppm) |
| orgp | Organic P in soil surface (ppm) |
| watersol\_p | Water soluble P in soil surface (ppm) |
| H3A\_P | H3a P in soil surface (ppm) |
| MEHLICH\_P | Mehlich P in soil surface (ppm) |
| BRAY\_STRONG\_p | Bray P in soil surface (ppm) |

**CONDITIONAL**

**Not sure about this one**

**D\_TABLE –** Decision tables are a precise yet compact way to model complex rule sets and their corresponding actions.

Decision tables, like flowcharts and if-then-else and switch-case statements, associate conditions with actions to perform, but in many cases do so in a more elegant way (see Wikipedia – ‘Decision table’)

**Structure of Decision Tables**

1. Conditions
2. Condition alternatives
3. Actions
4. Action entries

Each decision corresponds to a variable, relation or predicate whose possible values are listed among the condition alternatives. Each action is a procedure or operation to perform, and the entries specify whether (or in what order) the action is to be performed for the set of condition alternatives the entry corresponds to. Many decision tables include in their condition alternatives the ‘don’t care’ symbol, a hyphen. Using ‘don’t cares’ can simply decision tables, especially when a given condition has little influence on the actions to be performed. In some cases, entire conditions thought to be important initially are found to be irrelevant when none of the conditions influence which actions are performed.

Decision tables, especially when coupled with the use of a domain-specific language, allow developers and policy experts to work from the same information, the decision tables themselves.

Tools to render nested if statements from traditional programming languages into decision tables can also be used as a debugging tool.

Decision tables have proven to be easier to understand and review than code, and have been used extensively and successfully to produce specifications for complex systems.

**Quadrant I.** Number of conditions, alternatives and actions

1. Conditional variables
2. Limit variables (each conditional variable has predefined limit variables

**char name type description units limit var**

soil\_water soil wp, fc, ul

w\_stress plant

month time

jday time

hu plant

n\_stress plant

soil\_n soil

soil\_p soil

n\_applied mgt

plant plant

rot\_yr mgt

biomass plant

cover plant/soil

lai

stir\_tillage mgt

vol res pvol, evol

flow chan

**Quadrant II.** Condition alternatives

1. Condition rules – all alternatives met (<, >, =, -)

**Quadrant III.** Actions

Action Options

irrigate amt, file 🡪 irr.ops

release rate,day,weir

plant name from plants.plt

harvest file🡪 harv.ops

tillage file🡪 till.ops

fire file🡪 fire.ops

(structures)

(herd)

(water-rights)

**Quadrant IV.** Action Entries

1. ‘y’ (yes)
2. ‘n’ (no)

**d\_table.dtl**

The d\_table.dtl file contains the input variables for the nutrient characteristics of the soil properties. Below is a sample d\_table.dtl file:

d\_table.dtl - Little River Watershed

2

NAME CONDS ALTS ACTS

autoirr\_str.8 1 1 1

VAR OBJ OB\_NUM LIM\_VAR LIM\_OP LIM\_CONST ALT1

w\_stress plant 1 null - 0.7 <

ACT\_TYP NAME OPTION CONST FILE\_POINTER OUTCOME

irrigate drip\_high file 0 drip y

NAME CONDS ALTS ACTS

sw\_deficit75 1 1 1

VAR OBJ OB\_NUM LIM\_VAR LIM\_OP LIM\_CONST ALT1

soil\_water hru 0 fcap\_mm - 75. <

ACT\_TYP NAME OPTION CONST FILE\_POINTER OUTCOME

irrigate sprinkler\_high rate 0 sprinkler\_high y

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| MDTBL | Total number of decision tables in the file |
| HEADER | Header |
| name | | Name of decision table |
| CONDS | | Number of conditions |
| ALTS | | Number of alternatives |
| ACTS | | Number of actions |
| VAR | | Condition variable (vol, sw, time, etc) |
| OB | | Object variable (res, hru, canal, etc) |
| OB\_NUM | | Object number |
| LIM\_VAR | | Limit variable (evol, pvol, fc, ul, etc) |
| LIM\_OP | | Limit operator (\*,+,-) |
| LIM\_CONST | | Limit constant |
| ALT | | Condition alternatives |
| ACT\_TYP | | Type of action (reservoir, irrigate, fertilizer, etc) |
| name | | Name of action |
| OPTION | | Action option-specific to type of action (ie for reservoir, option to input rate, days of drawdown, weir equation pointer, etc) |
| CONST | | Constant used for rate, days, etc |
| FILE\_POINTER | | Pointer for option (ie weir equation pointer) |
| ACT\_OUTCOME | | Action outcomes (‘y’ to perform action; ‘n’ to not perform action |

**CONST –** what to say about constituents…..

**constituents.cs**

The constituents.cs file contains the input variables for the pesticide constituents. Below is a sample constituents.cs file:

Need example file

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Header for the constituent.cs file |
| name | The name of the constituent |
| units | 1=mass, 2=mass/area, 3=frac for dr, 4=cms and concentration |
| pest\_com | name of pesticide community (pesticide.com) |
| pest\_dat | name of pesticide data (filename for recall, and object in file for exco/dr) |
| path\_com | name of pathogen community (pathogen.com) |
| path\_dat | name of pathogen data (filename for recall, and object in file for exco/dr) |
| hmet\_com | name of heavy metal community (heavy\_metal\_.com) |
| hmet\_dat | name of heavy metal data (filename for recall, and object in file for exco/dr) |
| salt\_com | name of salt ion community (salt\_ion.com) |
| salt\_dat | name of salt ion data (filename for recall, and object in file for exco/dr) |

**pest.cs**

The pest.cs file contains the input variables for the pesticide constituents. Below is a sample pest.cs file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Header for the pest.cs file |
| name | The name of the pesticide community |
| init\_df | The name of the initialization file for pesticide community |
| recall\_df | The name of the recall file for the pesticide community |
| exco\_df | The name of the export coefficient file for the pesticide community |
| dr\_df | The name of the delivery ratio file for the pesticide community |
| num | The number of pesticides in the pesticide community |
| pests | The name of the pesticides in the community |

**path.cs**

The pest.cs file contains the input variables for the pathogens constituents. Below is a sample path.cs file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Header for the path.cs file |
| name | The name of the pathogens community |
| init\_df | The name of the initialization file for pathogens community |
| recall\_df | The name of the recall file for the pathogens community |
| exco\_df | The name of the export coefficient file for the pathogens community |
| dr\_df | The name of the delivery ratio file for the pathogens community |
| num | The number of pathogens in the pathogens community |
| paths | The name of the pathogens in the community |

**hmet.cs**

The hmet.cs file contains the input variables for the heavy metals constituents. Below is a sample hmet.cs file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Header for the hmet.cs file |
| name | The name of the heavy metals community |
| init\_df | The name of the initialization file for heavy metals community |
| recall\_df | The name of the recall file for the heavy metals community |
| exco\_df | The name of the export coefficient file for the heavy metals community |
| dr\_df | The name of the delivery ratio file for the heavy metals community |
| num | The number of pathogens in the heavy metals community |
| METALS | The name of the heavy metals in the community |

**salt.cs**

The salt.cs file contains the input variables for the heavy metals constituents. Below is a sample salt.cs file:



|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| TITLE | The first line of the file is reserved for user comments. The comments may take up to 80 spaces. The title line is not processed by the model and may be left blank. |
| HEADER | Header for the salt.cs file |
| name | The name of the salt community |
| init\_df | The name of the initialization file for salt community |
| recall\_df | The name of the recall file for the salt community |
| exco\_df | The name of the export coefficient file for the salt community |
| dr\_df | The name of the delivery ratio file for the salt community |
| num | The number of pathogens in the salt community |
| saltS | The name of the salt in the community |

**REGIONS–**

**ls\_unit.ele**

The ls\_unit.ele file contains the input variables

Below is a sample ls\_unit.ele

ls\_unit.ele

NUMB NAME OBTYP OBTYPNO BSN\_FRAC SUB\_FRAC REG\_FRAC

1 hru1 hru 1 0.500 0.5 0

2 hru2 hru 2 0.500 0.5 0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the LS\_UNIT.ELE file |
| HEADER |  |
| NUMB | The sequential number of the LS\_UNIT.ELE |
| NAME |  |
| OB\_TYP | Type of object to print (cha, res, etc) |
| OBTYPNO | Object type number |
| BSN\_FRAC | fraction of element in basin (expansion factor) |
| SUB\_FRAC | fraction of element in sub (expansion factor) |
| REG\_FRAC | fraction of element in calibration region (expansion factor) |

**ls\_unit.def**

The ls\_unit.def file contains the input variables

Below is a sample ls\_unit.def

ls\_unit.def Subbasin

2

NUMB NAME AREA\_HA NPSU ELEM1 ELEM2

1 lcu1 493.38 1 1 2

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the LS\_UNIT.DEF file |
| mreg | Number of regions |
| HEADER |  |
| NUMB | The sequential number of the LS\_UNIT.DEF |
| NAME |  |
| area\_ha | Surface area |
| NPSU |  |
| ELEM\_CNT |  |

**ls\_reg.def**

The ls\_reg.def file contains the input variables

Below is a sample ls\_reg.def

ls\_reg.def Subbasin

2

NUMB NAME AREA\_HA NPSU ELEM1 ELEM2

1 lcu1 493.38 1 1 2

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the LS\_REG.DEF file |
| mreg | Number of regions |
| HEADER |  |
| NUMB | The sequential number of the LS\_REG.DEF |
| NAME |  |
| area\_ha | Surface area |
| NPSU |  |
| ELEM\_CNT |  |

**ch\_catunit.def**

The ch\_catunit.def file contains the input variables

Below is a sample ch\_catunit.def

Ch\_catunit.def Subbasin

2

NUMB NAME AREA\_HA NPSU ELEM1 ELEM2

1 lcu1 493.38 1 1 2

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the CH\_CATUNIT.DEF file |
| mreg | Number of regions |
| HEADER |  |
| NUMB | The sequential number of the CH\_CATUNIT.DEF |
| NAME |  |
| area\_ha | Surface area |
| NPSU |  |
| ELEM\_cnt |  |

**ch\_reg.def**

The ch\_reg.def file contains the input variables

Below is a sample ch\_reg.def

Ch\_reg.def Subbasin

2

NUMB NAME AREA\_HA NPSU ELEM1 ELEM2

1 lcu1 493.38 1 1 2

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the CH\_REG.DEF file |
| mreg | Number of regions |
| HEADER |  |
| NUMB | The sequential number of the CH\_REG.DEF |
| NAME |  |
| area\_ha | Surface area |
| NPSU |  |
| ELEM\_cnt |  |

**aqu\_catunit.ele**

The aqu\_catunit.ele file contains the input variables

Below is a sample aqu\_cattunit.ele

Aqu\_catunit.ele

NUMB NAME OBTYP OBTYPNO BSN\_FRAC SUB\_FRAC REG\_FRAC

1 hru1 hru 1 0.500 0.5 0

2 hru2 hru 2 0.500 0.5 0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the AQU\_CATUNIT.ELE file |
| HEADER |  |
| NUMB | The sequential number of the AQU\_CATUNIT.ELE |
| NAME |  |
| OB\_TYP | Type of object to print (cha, res, etc) |
| OBTYPNO | Object type number |
| BSN\_FRAC | fraction of element in basin (expansion factor) |
| SUB\_FRAC | fraction of element in sub (expansion factor) |
| REG\_FRAC | fraction of element in calibration region (expansion factor) |

**aqu\_catunit.def**

The aqu\_catunit.def file contains the input variables

Below is a sample aqu\_catunit.def

Aqu\_catunit.def Subbasin

2

NUMB NAME AREA\_HA NPSU ELEM1 ELEM2

1 lcu1 493.38 1 1 2

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the AQU\_CATUNIT.DEF file |
| mreg | Number of regions |
| HEADER |  |
| NUMB | The sequential number of the AQU\_CATUNIT.DEF |
| NAME |  |
| area\_ha | Surface area |
| NPSU |  |
| ELEM\_cnt |  |

**aqu\_reg.def**

The aqu\_reg.def file contains the input variables

Below is a sample aqu\_reg.def

aqu\_reg.def Subbasin

2

NUMB NAME AREA\_HA NPSU ELEM1 ELEM2

1 lcu1 493.38 1 1 2

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the AQU\_REG.DEF file |
| mreg | Number of regions |
| HEADER |  |
| NUMB | The sequential number of the AQU\_REG.DEF |
| NAME |  |
| area\_ha | Surface area |
| NPSU |  |
| ELEM\_CNT |  |

**res\_catunit.ele**

The res\_catunit.ele file contains the input variables

Below is a sample res\_cattunit.ele

res\_catunit.ele

NUMB NAME OBTYP OBTYPNO BSN\_FRAC SUB\_FRAC REG\_FRAC

1 hru1 hru 1 0.500 0.5 0

2 hru2 hru 2 0.500 0.5 0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the RES\_CATUNIT.ELE file |
| HEADER |  |
| NUMB | The sequential number of the RES\_CATUNIT.ELE |
| NAME |  |
| OB\_TYP | Type of object to print (cha, res, etc) |
| OBTYPNO | Object type number |
| BSN\_FRAC | fraction of element in basin (expansion factor) |
| SUB\_FRAC | fraction of element in sub (expansion factor) |
| REG\_FRAC | fraction of element in calibration region (expansion factor) |

**res\_reg.def**

The res\_reg.def file contains the input variables

Below is a sample res\_reg.def

res\_reg.def Subbasin

2

NUMB NAME AREA\_HA NPSU ELEM1 ELEM2

1 lcu1 493.38 1 1 2

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the RES\_REG.DEF file |
| mreg | Number of regions |
| HEADER |  |
| NUMB | The sequential number of the RES\_REG.DEF |
| NAME |  |
| area\_ha | Surface area |
| NPSU |  |
| ELEM\_cnt |  |

**res\_reg.def**

The res\_reg.def file contains the input variables

Below is a sample res\_reg.def

res\_reg.def Subbasin

2

NUMB NAME AREA\_HA NPSU ELEM1 ELEM2

1 lcu1 493.38 1 1 2

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the RES\_REG.DEF file |
| mreg | Number of regions |
| HEADER |  |
| NUMB | The sequential number of the RES\_REG.DEF |
| NAME |  |
| area\_ha | Surface area |
| NPSU |  |
| ELEM\_cnt |  |

**rec\_catunit.ele**

The rec\_catunit.ele file contains the input variables

Below is a sample rec\_cattunit.ele

rec\_catunit.ele

NUMB NAME OBTYP OBTYPNO BSN\_FRAC SUB\_FRAC REG\_FRAC

1 hru1 hru 1 0.500 0.5 0

2 hru2 hru 2 0.500 0.5 0

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the REC\_CATUNIT.ELE file |
| HEADER |  |
| NUMB | The sequential number of the REC\_CATUNIT.ELE |
| NAME |  |
| OB\_TYP | Type of object to print (cha, res, etc) |
| OBTYPNO | Object type number |
| BSN\_FRAC | fraction of element in basin (expansion factor) |
| SUB\_FRAC | fraction of element in sub (expansion factor) |
| REG\_FRAC | fraction of element in calibration region (expansion factor) |

**rec\_catunit.def**

The rec\_catunit.def file contains the input variables

Below is a sample rec\_catunit.def

res\_catunit.def Subbasin

2

NUMB NAME AREA\_HA NPSU ELEM1 ELEM2

1 lcu1 493.38 1 1 2

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the REC\_CATUNIT.DEF file |
| mreg | Number of regions |
| HEADER |  |
| NUMB | The sequential number of the REC\_CATUNIT.DEF |
| NAME |  |
| area\_ha | Surface area |
| NPSU |  |
| ELEM\_cnt |  |

**rec\_reg.def**

The rec\_reg.def file contains the input variables

Below is a sample rec\_reg.def

res\_reg.def Subbasin

2

NUMB NAME AREA\_HA NPSU ELEM1 ELEM2

1 lcu1 493.38 1 1 2

|  |  |
| --- | --- |
| **Variable name** | **Definition** |
| Title | Description of the REC\_REG.DEF file |
| mreg | Number of regions |
| HEADER |  |
| NUMB | The sequential number of the REC\_REG.DEF |
| NAME |  |
| area\_ha | Surface area |
| NPSU |  |
| ELEM1 |  |
| ELEM2 |  |