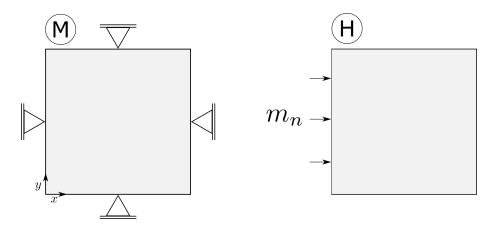
Hydromechanics: flow, no strain



This test uses a square of 1 m x 1 m with a fluid influx from the left edge and no outflow. All displacements are zero. With the mass balance we can derive an analytical solution for the pressure solution.

$$0 = (\varrho_{\rm F})'_{\rm S} + \operatorname{div}(\varrho_{\rm FR} \underline{\tilde{u}}_{\rm FS}) \tag{1}$$

The mass balance in turn can be written in integral form as:

$$0 = \int_{\Omega} \left[(\varrho_{F})'_{S} + \operatorname{div}(\varrho_{FR} \underline{\tilde{w}}_{FS}) \right] d\Omega = \int_{\Omega} (\varrho_{F})'_{S} d\Omega + \int_{\partial\Omega} \varrho_{FR} \underline{\tilde{w}}_{FS} \cdot \underline{n} d\Gamma$$
 (2)

For the homogeneous case considered and the boundary conditions given above this translates into the simple form

$$(\varrho_{\rm F})_{\rm S}' \Omega = m_n \Gamma \tag{3}$$

Furthermore we assume material compressibility of both the solid and fluid

$$(\varrho_{\rm FR})'_{\rm S} = \frac{\partial \varrho_{\rm FR}}{\partial p_{\rm FR}} (p_{\rm FR})'_{\rm S} = \varrho_{\rm FR} \beta_p (p_{\rm FR})'_{\rm S}$$
(4)

the following relation can be obtained

$$(\varrho_{\rm F})'_{\rm S} = \varrho_{\rm FR} \beta_p (p_{\rm FR})'_{\rm S} \phi + \varrho_{\rm FR} (\alpha_{\rm B} - \phi) K_{\rm SR}^{-1} (p_{\rm FR})'_{\rm S}$$

$$(5)$$

$$(\varrho_{\rm F})'_{\rm S} = \varrho_{\rm FR} (p_{\rm FR})'_{\rm S} \left[\beta_p \phi + \frac{\alpha_{\rm B} - \phi}{K_{\rm SR}} \right]$$
 (6)

For ideal gases as the fluid we can further find that

$$\varrho_{\rm FR} = \frac{p_{\rm FR}}{R_s T} \quad \text{and} \quad \beta_p = \frac{1}{p_{\rm FR}}$$
(7)

A combination of the above leads to the pressure solution

$$m_n \frac{\Gamma}{\Omega} R_s T = \left(\phi + \frac{\alpha_{\rm B} - \phi}{K_{\rm SR}} p_{\rm FR} \right) (p_{\rm FR})'_{\rm S}$$
 (8)

$$m_n \frac{\Gamma}{\Omega} R_s T t = \left(p_{\text{FR}}^2 - p_{\text{FR0}}^2 \right) \frac{\alpha_{\text{B}} - \phi}{2K_{\text{SR}}} + \left(p_{\text{FR}} - p_{\text{FR0}} \right) \phi \tag{9}$$

$$p_{\rm FR} = -a \pm \sqrt{(a + p_{\rm FR0})^2 + b}$$
 (10)

with
$$a = K_{\rm SR} \frac{\phi}{\alpha_{\rm B} - \phi}$$
 (11)

and
$$b = p_{FR0}^2 + ap_{FR0} + m_n \frac{\Gamma}{\Omega} R_s T \frac{a}{\phi} t$$
 (12)

Given the following parameters

$$\begin{split} \Gamma &= 1 \, \mathrm{m}^2 & \Omega = 1 \, \mathrm{m}^3 \\ R &= 287.058 \, \mathrm{J/(kgK)} & T = 293.15 \, \mathrm{K} \\ E &= 1000 \, \mathrm{MPa} & \nu = 0.3 \\ p_{\mathrm{FR0}} &= 0.1 \, \mathrm{MPa} & m_n = 10^{-3} \, \mathrm{kg/(m^2s)} \\ \phi &= 0.03 & \alpha_{\mathrm{B}} = 0.6 \\ K_{\mathrm{SR}} &= \frac{K_{\mathrm{S}}}{1 - \alpha_{\mathrm{B}}} & K_{\mathrm{S}} &= \frac{E}{3(1 - 2\nu)} \end{split}$$

we get the following pressure solution for a time of $100\,\mathrm{s}$. The simulation result is reasonable close to the analytical solution with the relative error being below 10^{-6} .

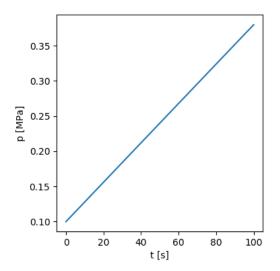


Fig. 1: pressure solution

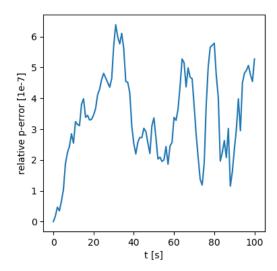


Fig. 2: relative error for pressure