3-ANNEX D (informative)

PSYCHOACOUSTIC MODELS

3-D.1. Psychoacoustic Model I

The calculation of the psychoacoustic model has to be adapted to the corresponding layer. This example is valid for Layers I and II. The model can be adapted to LayerIII.

There is no principal difference in the application of psychoacoustic model 1 to Layer I or II.

Layer I: A new bit allocation is calculated for each block of 12 subband or 384 input PCM samples.

Layer II: A new bit allocation is calculated for three blocks totaling 36 subband samples corresponding to 3*384 (1152) input PCM samples.

The bit allocation of the 32 subbands is calculated on the basis of the signal-to-mask ratios of all the subbands. Therefore it is necessary to determine, for each subband the maximum signal level and the minimum masking threshold. The minimum masking threshold is derived from an FFT of the input PCM signal, followed by a psychoacoustic model calculation.

The FFT in parallel with the subband filter compensates for the lack of spectral selectivity obtained at low frequencies by the subband filterbank. This technique provides both a sufficient time resolution for the coded audio signal (Polyphase filter with optimized window for minimal pre-echoes) and a sufficient spectral resolution for the calculation of the masking thresholds.

The frequencies and levels of aliasing distortions can be calculated. This is necessary for calculating a minimum bit rate for those subbands which need some bits to cancel the aliasing components in the decoder. The additional complexity to calculate the better frequency resolution is necessary only in the encoder, and introduces no additional delay or complexity in the decoder.

The calculation of the signal-to-mask-ratio is based on the following steps:

Step 1

- Calculation of the FFT for time to frequency conversion.

Step 2

- Determination of the sound pressure level in each subband.

Step 3

- Determination of the threshold in quiet (absolute threshold).

Step 4

- Finding of the tonal (more sinusoid-like) and non-tonal (more noise-like) components of the audio signal.

Step 5

- Decimation of the maskers, to obtain only the relevant maskers.

Step 6

- Calculation of the individual masking thresholds.

Step 7

- Determination of the global masking threshold.

Step 8

- Determination of the minimum masking threshold in each subband.

Step 9

- Calculation of the signal-to-mask ratio in each subband.

These steps will be further discussed. A sampling frequency of 48kHz is assumed. For the other two sampling frequencies all frequencies mentioned should be scaled accordingly.

Step 1: FFT Analysis

The masking threshold is derived from an estimate of the power density spectrum that is calculated by a 512-point FFT for Layer I, or by a 1024-point FFT for Layers II and III. The FFT is calculated directly from the input PCM signal, windowed by a Hann window.

For a coincidence in time between the bit-allocation and the corresponding subband samples, the PCM-samples entering the FFT have to be delayed:

- 1. The delay of the analysis subband filter is 256 samples, corresponding to 5.3ms at the 48kHz sampling rate. This corresponds to a window shift of 256 samples.
- 2. The Hann window must coincide with the subband samples of the frame. For Layer I this amounts to an additional window shift of 64 samples, for Layer II an additional window shift of minus 64 samples.

Technical data of the FFT:

| | | Layer I | Layer II |
|---|--|-------------------|--------------|
| - | transform length | 512 samples | 1024 samples |
| | Window size if $fs = 48 \text{ kHz}$ | 10.67 ms | 21.3 ms |
| | Window size if $fs = 44.1 \text{ kHz}$ | 11.6 ms | 23.2 ms |
| | Window size if $fs = 32 \text{ kHz}$ | 16 ms | 32 ms |
| - | Frequency resolution | fs/512 | fs/1024 |
| - | Hann window, h(i): | | |
| | $h(i) = *0.5 * \{1 - \cos[2 * p * (i)/(N-1)]\}$ | $0 \le i \le N-1$ | |
| - | power density spectrum X(k): | | |
| | X(k) = 10 * log 1/Nh(l) * s(l) * e(-j*k*l*2*p/N | k = 0N/2 | |

A normalization to the reference level of 96 dB SPL (Sound Pressure Level) has to be done in such a way that the maximum value corresponds to 96dB.

Step 2: Determination of the sound pressure level

The sound pressure level Lsb in subband n is computed by:

Lsb(n) = MAX[
$$X(k)$$
, 20*log(scfmax(n)*32768)-10] dB
 $X(k)$ in subband n

where X(k) is the sound pressure level of the spectral line with index k of the FFT with the maximum amplitude in the frequency range corresponding to subband n. The expression scfmax(n) is in Layer I the scalefactor, and in Layer II the maximum of the three scalefactors of subband n within a frame. The "-10 dB" term corrects for the difference between peak and RMS level. The sound pressure level Lsb(n) is computed for every subband n.

Step 3: Considering the threshold in quiet

The threshold in quiet LTq(k), also called absolute threshold, is available in the tables "Frequencies, Critical Band Rates and Absolute Threshold" (Tables 3-D.1a, 3-D.1b, 3-D.1c for LayerI; Tables 3-D.1d, 3-D.1e, 3-D.1f for LayerII). These tables depend on the sampling rate of the input PCM signal. Values are available for each sample in the frequency domain where the masking threshold is calculated.

An offset depending on the overall bit rate is used for the absolute threshold. This offset is -12 dB for bit rates >= 96 kbit/s and 0 dB for bit rates < 96 kbit/s per channel.

Step 4: Finding of tonal and non-tonal components

The tonality of a masking component has an influence on the masking threshold. For this reason, it is worthwhile to discriminate between tonal and non-tonal components. For calculating the global masking threshold it is necessary to derive the tonal and the non-tonal components from the FFT spectrum.

This step starts with the determination of local maxima, then extracts tonal components (sinusoids) and calculates the intensity of the non-tonal components within a bandwidth of a critical band. The boundaries of the critical bands are given in the tables "CRITICAL BAND BOUNDARIES" (Tables 3-D.2a, 3-D.2b, 3-D.2c for LayerI; Tables 3-D.2d, 3-D.2e, 3-D.2f for LayerII).

The bandwidth of the critical bands varies with the center frequency with a bandwidth of about only 0.1 kHz at low frequencies and with a bandwidth of about 4 kHz at high frequencies. It is known from psychoacoustic experiments that the ear has a better frequency resolution in the lower than in the higher frequency region. To determine if a local maximum may be a tonal component a frequency range df around the local maximum is examined. The frequency range df is given by:

| Sampling | Sampling rate: 32 kHz | | | | | | |
|-----------|-----------------------|------------|--------|------------|--|--|--|
| Layer I: | df = 125 Hz | 0 kHz | < f <= | 4.0kHz | | | |
| | df = 187.5 Hz | 4.0 kHz | < f <= | 8.0 kHz | | | |
| | df = 375 Hz | 8.0 kHz | < f <= | 15.0kHz | | | |
| | | | | | | | |
| Layer II: | df = 62.5 Hz | 0 kHz | < f <= | 3.0 kHz | | | |
| | df = 93.75 Hz | 3.0 kHz | < f <= | 6.0 kHz | | | |
| | df = 187.5 Hz | 6.0 kHz | < f <= | 12.0 kHz | | | |
| | df = 375 Hz | 12.0 kHz | < f <= | 24.0 kHz | | | |
| | | | | | | | |
| | rate: 44.1kHz | | | | | | |
| Layer I: | df = 172.266 Hz | 0 kHz | < f <= | 5.512kHz | | | |
| | df = 281.25 Hz | 5.512 kHz | < f <= | 11.024 kHz | | | |
| | df = 562.50 Hz | 11.024 kHz | < f <= | 19.982kHz | | | |
| | | | | | | | |
| Layer II: | df = 86.133 Hz | 0 kHz | < f <= | 2.756 kHz | | | |
| | df = 129.199 Hz | 2.756 kHz | < f <= | 5.512kHz | | | |
| | df = 258.398 Hz | 5.512 kHz | < f <= | 11.024 kHz | | | |
| | df = 516.797 Hz | 11.024 kHz | < f <= | 19.982kHz | | | |
| G 1: | 40111 | | | | | | |
| | rate: 48 kHz | 0.1.11 | | 60177 | | | |
| Layer I: | df = 187.5 Hz | 0 kHz | < f <= | 6.0 kHz | | | |
| | df = 281.25 Hz | 6.0 kHz | < f <= | 12.0 kHz | | | |
| | df = 562.50 Hz | 12.0 kHz | < f <= | 24.0 kHz | | | |
| T IT. | 10 - 02 750 H- | 0.1-11- | - C | 2.0.1-11- | | | |
| Layer II: | | 0 kHz | < f <= | 3.0 kHz | | | |
| | df = 140.63 Hz | 3.0 kHz | < f <= | 6.0 kHz | | | |
| | df = 281.25 Hz | 6.0 kHz | < f <= | 12.0 kHz | | | |

$$df = 562.50 \text{ Hz}$$
 12.0 kHz < f <= 24.0 kHz

To make lists of the spectral lines X(k) that are tonal or non-tonal, the following three operations are performed:

(i) Labelling of local maxima

A spectral line X(k) is labelled as a local maximum if

$$X(k) > X(k-1)$$
 and $X(k) >= X(k+1)$

(ii) Listing of tonal components and calculation of the sound pressure level

A local maximum is put in the list of tonal components if

$$X(k) - X(k+j) >= 7 dB,$$

where j is chosen according to

$$\begin{array}{lll} j=-2,+2 & \text{for} & 2 < k < 63 \\ j=-3,-2,+2,+3 & \text{for} & 63 <= k < 127 \\ j=-6,...,-2,+2,...,+6 & \text{for} & 127 <= k <= 250 \end{array}$$

Layer II:

$$\begin{array}{lll} j=-2,+2 & \text{for} & 2 < k < 63 \\ j=-3,-2,+2,+3 & \text{for} & 63 <= k < 127 \\ j=-6,...,-2,+2,...,+6 & \text{for} & 127 <= k < 255 \\ j=-12,...,-2,+2,...,+12 & \text{for} & 255 <= k <= 500 \end{array}$$

If X(k) is found to be a tonal component, then the following parameters are listed:

- Index number k of the spectral line.
- Sound pressure level Xtm(k)=X(k-1)+X(k)+X(k+1), in dB
- Tonal flag.

Next, all spectral lines within the examined frequency range are set to -8 dB.

(iii) Listing of non-tonal components and calculation of the power

The non-tonal (noise) components are calculated from the remaining spectral lines. To calculate the non-tonal components from these spectral lines X(k), the critical bands z(k) are determined using the tables, "Critical Band Boundaries" (Tables 3-D.2a, 3-D.2b, 3-D.2c for LayerI; Tables 3-D.2d, 3-D.2e, 3-D.2f for LayerII). In LayerI, 23 critical bands are used for the sampling rate of 32kHz, 24 critical bands for 44.1kHz and 25 critical bands are used for 48kHz. In LayerII, 24 critical bands are used for 32kHz sampling rate, and 26 critical bands are used for 44.1kHz and 48kHz sampling rate. Within each critical band, the power of the spectral lines are summed to form the sound pressure level of the new non-tonal component corresponding to that critical band.

The following parameters are listed:

- Index number k of the spectral line nearest to the geometric mean of the critical band.
- Sound pressure level Xnm(k) in dB.
- Non-tonal flag.

Step 5: Decimation of tonal and non-tonal masking components

Decimation is a procedure that is used to reduce the number of maskers which are considered for the calculation of the global masking threshold.

(i) Tonal Xtm(k) or non-tonal components Xnm(k) are considered for the calculation of the masking threshold only if:

```
Xtm(k) \ge LTq(k) or Xnm(k) \ge LTq(k)
```

In this expression, LTq(k) is the absolute threshold (or threshold in quiet) at the frequency of index k. These values are given in the Tables 3-D.1a, 3-D.1b, 3-D.1c for LayerI; Tables 3-D.1d, 3-D.1e, 3-D.1f for LayerII.

(ii) Decimation of two or more tonal components within a distance of less then 0.5 Bark: Keep the component with the highest power, and remove the smaller component(s) from the list of tonal components. For this operation, a sliding window in the critical band domain is used with a width of 0.5 Bark.

In the following, the index j is used to indicate the relevant tonal or non-tonal masking components from the combined decimated list.

Step 6: Calculation of individual masking thresholds

Of the original N/2 frequency domain samples, indexed by k, only a subset of the samples, indexed by i, are considered for the global masking threshold calculation. The samples used are shown in Tables 3-D.1a, 3-D.1b, 3-D.1c for LayerI; Tables 3-D.1d, 3-D.1e, 3-D.1f for LayerII.

Layer I:

For the frequency lines corresponding to the frequency region which is covered by the first six subbands no subsampling is used. For the frequency region corresponding to the next six subbands every second spectral line is considered. Finally, in the case of 44.1 and 48 kHz sampling rates, in the frequency region corresponding to the remaining subbands, every fourth spectral line is considered up to 20 kHz. In the case of 32 kHz sampling rate, in the frequency region corresponding to the remaining subbands, every fourth spectral line is considered up to 15 kHz (See also Tables 3-D.1a, 3-D.1b, 3-D.1c "Frequencies, Critical Band Rates and Absolute Threshold" for LayerI.)

Layer II:

For the frequency lines corresponding to the frequency region which is covered by the first three subbands no subsampling is used. For the frequency region which is covered by next three subbands every second spectral line is considered. For the frequency region corresponding to the next six subbands every fourth spectral line is considered. Finally, in the case of 44.1 and 48 kHz sampling rates, in the remaining subbands every eighth spectral line is considered up to 20 kHz. In the case of 32 kHz sampling rate, in the frequency region corresponding to the remaining subbands, every eighth spectral line is considered up to 15 kHz. (See also Tables 3-D.1d, 3-D.1e, 3-D.1f "Frequencies, Critical Band Rates and Absolute Threshold" for LayerII.)

The number of samples, i, in the subsampled frequency domain is different depending on the sampling rates and layers.

```
32 kHz sampling rate: i = 108 for Layer I and i = 132 for Layer II 44.1 kHz sampling rate: i = 106 for Layer I and i = 130 for Layer II i = 102 for Layer II and i = 126 for Layer II
```

To every tonal and non-tonal component the index i in the subsampled frequency domain is assigned, which is closest in frequency to the original spectral line X(k). This index i is given in Tables 3-D.1a, 3-D.1b, 3-D.1c for LayerI; Tables 3-D.1d, 3-D.1e, 3-D.1f for LayerII, "Frequencies, Critical Band Rates and Absolute Threshold".

The individual masking thresholds of both tonal and non-tonal components are given by the following expression:

```
 \begin{array}{lll} LTtm[z(j),z(i)] & = & Xtm[z(j)] + avtm[z(j)] + vf[z(j),z(i)] & dB \\ LTnm[z(j),z(i)] & = & Xnm[z(j)] + avnm[z(j)] + vf[z(j),z(i)] & dB \end{array}
```

In this formula LTtm and LTnm are the individual masking thresholds at critical band ratez in Bark of the masking component at the critical band rate zm in Bark. The values in dB can be either positive or negative. The term Xtm[z(j)] is the sound pressure level of the masking component with the index number j at the corresponding critical band rate z(j). The term av is called the masking index and vf the masking function of the masking component Xtm[z(j)]. The masking index av is different for tonal and non-tonal masker (avtm and avnm).

For tonal maskers it is given by

$$avtm = -1.525 - 0.275 * z(j) - 4.5 dB$$

and for non-tonal maskers

$$avnm = -1.525 - 0.175 * z(j) - 0.5 dB.$$

The masking function vf of a masker is characterized by different lower and upper slopes, which depend on the distance in Bark dz = z(i)- z(j) to the masker. In this expression i is the index of the spectral line at which the masking function is calculated and j that of the masker. The critical band rates z(j) and z(i) can be found in Tables 3-D.1a, 3-D.1b, 3-D.1c for LayerI; Tables 3-D.1d, 3-D.1e, 3-D.1f for LayerII, "Frequencies, Critical Band Rates and Absolute Threshold". The masking function, which is the same for tonal and non-tonal maskers, is given by:

$$vf = 17 * (dz + 1) - (0.4 * X[z(j)] + 6) dB$$
 for $-3 \le dz \le -1$ Bark $vf = (0.4 * X[z(j)] + 6) * dz dB$ for $-1 \le dz \le 0$ Bark $vf = -17 * dz dB$ for $0 \le dz \le 1$ Bark $vf = -(dz - 1) * (17 - 0.15 * X[z(j)]) - 17 dB$ for $1 \le dz \le 8$ Bark

In these expressions X[z(j)] is the sound pressure level of the j'th masking component in dB. If dz < -3 Bark, or $dz \ge 8$ Bark, the masking is no longer considered (LTtm and LTnm are set to -8dB outside this range).

Step 7: Calculation of the global masking threshold LTg

The global masking threshold LTg(i) at the i'th frequency sample is derived from the upper and lower slopes of the individual masking threshold of each of the j tonal and non-tonal maskers, and in addition from the threshold in quiet LTq(i). This is also given in Tables 3-D.1a, 3-D.1b, 3-D.1c for LayerI; Tables 3-D.1d, 3-D.1e, 3-D.1f for LayerII "Frequencies, Critical Band Rates and Absolute Threshold". The global masking threshold is found by summing the powers corresponding to the individual masking thresholds and the threshold in quiet.

$$LTg(i) = 10 log (10LTg(i)/10 + +)$$

The total number of tonal maskers is given by m, and the total number of non-tonal maskers is given by n. For a given i, the range of j can be reduced to just encompass those masking components that are within -8 to +3 Bark from i. Outside of this range LTtm and LTnm are -8 dB.

Step 8: Determination of the minimum masking threshold

The minimum masking level LTmin(n) in subband n is determined by the following expression:

$$\begin{array}{ccc} LTmin(n) = & MIN[\ LTg(i)\] \ dB \\ f(i) \ in \ subband \ n \end{array}$$

where f(i) is the frequency of the i'th frequency sample. The f(i) are tabulated in the Tables 3-D.1a, 3-D.1b, 3-D.1c for LayerI; Tables 3-D.1d, 3-D.1e, 3-D.1f for LayerII of "Frequencies, Critical Band Rates and Absolute Threshold". A minimum masking level LTmin(n) is computed for every subband.

Step 9: Calculation of the signal-to-mask-ratio

The signal-to-mask ratio

SMRsb(n) = Lsb(n)-LTmin(n) dB

is computed for every subband n.

Table 3-D.1a.: Frequencies, Critical Band Rates and Absolute ThresholdTable is valid for Layer I at a sampling rate of 32.0 kHz.

Index Number Frequency i [Hz] [dB] [z]1 62.50 33.44 .617 2 125.00 1.232 19.20 3 187.50 1.842 13.87 4 250.00 2.445 11.01 5 312.50 3.037 9.20 6 375.00 3.618 7.94 7 437.50 4.185 7.00 8 500.00 4.736 6.28 562.50 5.272 9 5.70 625.00 5.789 10 5.21 11 687.50 6.289 4.80 12 750.00 6.770 4.45 812.50 7.233 13 4.14 14 875.00 7.677 3.86 15 937.50 8.103 3.61 16 1000.00 8.511 3.37 17 1062.50 8.901 3.15 18 1125.00 9.275 2.93 19 1187.50 9.632 2.73 20 1250.00 9.974 2.53 21 1312.50 10.301 2.32 22 1375.00 10.614 2.12 23 1437.50 10.913 1.92 24 1500.00 11.199 1.71 25 1562.50 11.474 1.49 26 1625.00 11.736 1.27 27 1687.50 11.988 1.04 28 1750.00 12.230 .80 29 1812.50 12.461 .55 .29 30 1875.00 12.684 31 1937.50 12.898 .02 32 2000.00 13.104 -.25 33 2062.50 13.302 -.54 34 2125.00 13.493 -.83 35 2187.50 13.678 -1.12 36 2250.00 13.855 -1.43 37 2312.50 14.027 -1.73

```
38
       2375.00 14.193 -2.04
39
       2437.50 14.354 -2.34
40
       2500.00 14.509 -2.64
41
       2562.50 14.660 -2.93
42
       2625.00 14.807 -3.22
43
       2687.50 14.949 -3.49
44
       2750.00 15.087 -3.74
45
       2812.50 15.221 -3.98
46
       2875.00 15.351 -4.20
47
       2937.50 15.478 -4.40
48
       3000.00 15.602 -4.57
49
       3125.00 15.841 -4.82
50
       3250.00 16.069 -4.96
51
       3375.00 16.287 -4.97
52
       3500.00 16.496 -4.86
53
       3625.00 16.697 -4.63
54
       3750.00 16.891 -4.29
55
       3875.00 17.078 -3.87
56
       4000.00 17.259 -3.39
57
       4125.00 17.434 -2.86
58
       4250.00 17.605 -2.31
59
       4375.00 17.770 -1.77
60
       4500.00 17.932 -1.24
61
       4625.00 18.089 -.74
62
       4750.00 18.242 -.29
63
       4875.00 18.392 .12
64
       5000.00 18.539 .48
65
       5125.00 18.682
                       .79
       5250.00 18.823 1.06
66
67
       5375.00 18.960 1.29
68
       5500.00 19.095 1.49
69
       5625.00 19.226 1.66
70
       5750.00 19.356 1.81
71
       5875.00 19.482 1.95
72
       6000.00 19.606 2.08
73
       6250.00 19.847
                       2.33
74
       6500.00 20.079
                       2.59
75
       6750.00 20.300 2.86
76
       7000.00 20.513 3.17
77
       7250.00 20.717 3.51
78
       7500.00 20.912 3.89
79
       7750.00 21.098 4.31
80
       8000.00 21.275 4.79
81
       8250.00 21.445 5.31
82
       8500.00 21.606 5.88
83
       8750.00 21.760 6.50
84
       9000.00 21.906
                       7.19
                       7.93
85
       9250.00 22.046
       9500.00 22.178
86
                       8.75
87
       9750.00 22.304 9.63
88
       10000.00
                       22.424 10.58
89
        10250.00
                       22.538 11.60
90
       10500.00
                       22.646 12.71
91
                       22.749 13.90
        10750.00
92
        11000.00
                       22.847 15.18
```

| 93 | 11250.00 | 22.941 | 16.54 |
|-----|----------|--------|-------|
| 94 | 11500.00 | 23.030 | 18.01 |
| 95 | 11750.00 | 23.114 | 19.57 |
| 96 | 12000.00 | 23.195 | 21.23 |
| 97 | 12250.00 | 23.272 | 23.01 |
| 98 | 12500.00 | 23.345 | 24.90 |
| 99 | 12750.00 | 23.415 | 26.90 |
| 100 | 13000.00 | 23.482 | 29.03 |
| 101 | 13250.00 | 23.546 | 31.28 |
| 102 | 13500.00 | 23.607 | 33.67 |
| 103 | 13750.00 | 23.666 | 36.19 |
| 104 | 14000.00 | 23.722 | 38.86 |
| 105 | 14250.00 | 23.775 | 41.67 |
| 106 | 14500.00 | 23.827 | 44.63 |
| 107 | 14750.00 | 23.876 | 47.76 |
| 108 | 15000.00 | 23.923 | 51.04 |

Table 3-D.1b.: Frequencies, Critical Band Rates and Absolute ThresholdTable is valid for Layer I at a sampling rate of 44.1 kHz.

| Index N | Index Number Frequency | | |
|---------|------------------------|--------|-------|
| i | [Hz] | [z] | [dB] |
| 1 | 86.13 | .850 | 25.87 |
| 2 | 172.27 | 1.694 | 14.85 |
| 3 | 258.40 | 2.525 | 10.72 |
| 4 | 344.53 | 3.337 | 8.50 |
| 5 | 430.66 | 4.124 | 7.10 |
| 6 | 516.80 | 4.882 | 6.11 |
| 7 | 602.93 | 5.608 | 5.37 |
| 8 | 689.06 | 6.301 | 4.79 |
| 9 | 775.20 | 6.959 | 4.32 |
| 10 | 861.33 | 7.581 | 3.92 |
| 11 | 947.46 | 8.169 | 3.57 |
| 12 | 1033.59 | 8.723 | 3.25 |
| 13 | 1119.73 | 9.244 | 2.95 |
| 14 | 1205.86 | 9.734 | 2.67 |
| 15 | 1291.99 | 10.195 | 2.39 |
| 16 | 1378.13 | | 2.11 |
| 17 | 1464.26 | 11.037 | 1.83 |
| 18 | 1550.39 | | 1.53 |
| 19 | 1636.52 | | 1.23 |
| 20 | 1722.66 | 12.125 | .90 |
| 21 | 1808.79 | | .56 |
| 22 | 1894.92 | | .21 |
| 23 | 1981.05 | | 17 |
| 24 | 2067.19 | | 56 |
| 25 | 2153.32 | 13.578 | 96 |
| 26 | 2239.45 | 13.826 | -1.38 |
| 27 | 2325.59 | 14.062 | -1.79 |
| 28 | 2411.72 | 14.288 | -2.21 |
| 29 | 2497.85 | | -2.63 |
| 30 | 2583.98 | | -3.03 |
| 31 | 2670.12 | | -3.41 |
| 32 | 2756.25 | | -3.77 |
| 33 | 2842.38 | 15.284 | -4.09 |

```
34
       2928.52 15.460 -4.37
35
       3014.65 15.631 -4.60
36
       3100.78 15.796 -4.78
37
       3186.91 15.955 -4.91
38
       3273.05 16.110 -4.97
39
       3359.18 16.260 -4.98
40
       3445.31 16.406 -4.92
41
       3531.45 16.547 -4.81
42
       3617.58 16.685 -4.65
43
       3703.71 16.820 -4.43
44
       3789.84 16.951 -4.17
45
       3875.98 17.079 -3.87
46
       3962.11 17.205 -3.54
47
       4048.24 17.327 -3.19
48
       4134.38 17.447 -2.82
49
       4306.64 17.680 -2.06
50
       4478.91 17.905 -1.32
51
       4651.17 18.121
                       -.64
52
       4823.44 18.331 -.04
53
       4995.70 18.534 .47
54
       5167.97 18.731 .89
55
       5340.23 18.922 1.23
56
       5512.50 19.108 1.51
57
       5684.77 19.289 1.74
58
       5857.03 19.464 1.93
59
       6029.30 19.635 2.11
60
       6201.56 19.801
                       2.28
61
       6373.83 19.963 2.46
62
       6546.09 20.120 2.63
63
       6718.36 20.273 2.82
       6890.63 20.421 3.03
64
65
       7062.89 20.565 3.25
66
       7235.16 20.705 3.49
67
       7407.42 20.840 3.74
68
       7579.69 20.972 4.02
69
       7751.95 21.099 4.32
70
       7924.22 21.222 4.64
71
       8096.48 21.342 4.98
72
       8268.75 21.457 5.35
73
       8613.28 21.677 6.15
74
       8957.81 21.882 7.07
75
       9302.34 22.074 8.10
76
       9646.88 22.253 9.25
77
       9991.41 22.420 10.54
78
       10335.94
                       22.576 11.97
79
       10680.47
                       22.721 13.56
80
                       22.857 15.31
       11025.00
81
       11369.53
                       22.984 17.23
82
                       23.102 19.34
       11714.06
83
       12058.59
                       23.213 21.64
84
       12403.13
                       23.317 24.15
85
       12747.66
                       23.415 26.88
86
       13092.19
                       23.506 29.84
87
       13436.72
                       23.592 33.05
88
       13781.25
                       23.673 36.52
```

| 89 | 14125.78 | 23.749 | 40.25 |
|-----|----------|--------|-------|
| 90 | 14470.31 | 23.821 | 44.27 |
| 91 | 14814.84 | 23.888 | 48.59 |
| 92 | 15159.38 | 23.952 | 53.22 |
| 93 | 15503.91 | 24.013 | 58.18 |
| 94 | 15848.44 | 24.070 | 63.49 |
| 95 | 16192.97 | 24.125 | 68.00 |
| 96 | 16537.50 | 24.176 | 68.00 |
| 97 | 16882.03 | 24.225 | 68.00 |
| 98 | 17226.56 | 24.271 | 68.00 |
| 99 | 17571.09 | 24.316 | 68.00 |
| 100 | 17915.63 | 24.358 | 68.00 |
| 101 | 18260.16 | 24.398 | 68.00 |
| 102 | 18604.69 | 24.436 | 68.00 |
| 103 | 18949.22 | 24.473 | 68.00 |
| 104 | 19293.75 | 24.508 | 68.00 |
| 105 | 19638.28 | 24.542 | 68.00 |
| 106 | 19982.81 | 24.574 | 68.00 |

Table 3-D.1c. Frequencies, Critical Band Rates and Absolute ThresholdTable is valid for Layer I at a sampling rate of 48 kHz.

| Index Number Frequency | | ncy | |
|------------------------|---------|--------|-------|
| i | [Hz] | [z] | [dB] |
| 1 | 93.75 | .925 | 24.17 |
| 2 | 187.50 | 1.842 | 13.87 |
| 3 | 281.25 | 2.742 | 10.01 |
| 4 | 375.00 | 3.618 | 7.94 |
| 5 | 468.75 | 4.463 | 6.62 |
| 6 | 562.50 | 5.272 | 5.70 |
| 7 | 656.25 | 6.041 | 5.00 |
| 8 | 750.00 | 6.770 | 4.45 |
| 9 | 843.75 | 7.457 | 4.00 |
| 10 | 937.50 | 8.103 | 3.61 |
| 11 | 1031.25 | 8.708 | 3.26 |
| 12 | 1125.00 | 9.275 | 2.93 |
| 13 | 1218.75 | 9.805 | 2.63 |
| 14 | 1312.50 | 10.301 | 2.32 |
| 15 | 1406.25 | 10.765 | 2.02 |
| 16 | 1500.00 | 11.199 | 1.71 |
| 17 | 1593.75 | 11.606 | 1.38 |
| 18 | 1687.50 | 11.988 | 1.04 |
| 19 | 1781.25 | 12.347 | .67 |
| 20 | 1875.00 | 12.684 | .29 |
| 21 | 1968.75 | 13.002 | 11 |
| 22 | 2062.50 | 13.302 | 54 |
| 23 | 2156.25 | 13.586 | 97 |
| 24 | 2250.00 | 13.855 | -1.43 |
| 25 | 2343.75 | 14.111 | -1.88 |
| 26 | 2437.50 | 14.354 | -2.34 |
| 27 | 2531.25 | 14.585 | -2.79 |
| 28 | 2625.00 | 14.807 | -3.22 |
| 29 | 2718.75 | 15.018 | -3.62 |
| 30 | 2812.50 | 15.221 | -3.98 |
| 31 | 2906.25 | 15.415 | -4.30 |

```
32
       3000.00 15.602 -4.57
33
       3093.75 15.783 -4.77
34
       3187.50 15.956 -4.91
35
       3281.25 16.124 -4.98
36
       3375.00 16.287 -4.97
37
       3468.75 16.445 -4.90
38
       3562.50 16.598 -4.76
39
       3656.25 16.746 -4.55
40
       3750.00 16.891 -4.29
41
       3843.75 17.032 -3.99
42
       3937.50 17.169 -3.64
43
       4031.25 17.303 -3.26
44
       4125.00 17.434 -2.86
45
       4218.75 17.563 -2.45
46
       4312.50 17.688 -2.04
47
       4406.25 17.811 -1.63
48
       4500.00 17.932 -1.24
49
       4687.50 18.166 -.51
50
       4875.00 18.392 .12
51
       5062.50 18.611 .64
52
       5250.00 18.823 1.06
53
       5437.50 19.028 1.39
54
       5625.00 19.226 1.66
55
       5812.50 19.419 1.88
56
       6000.00 19.606 2.08
57
       6187.50 19.788 2.27
58
       6375.00 19.964
                       2.46
59
       6562.50 20.135
                       2.65
60
       6750.00 20.300 2.86
61
       6937.50 20.461 3.09
62
       7125.00 20.616 3.33
63
       7312.50 20.766 3.60
64
       7500.00 20.912 3.89
65
       7687.50 21.052 4.20
66
       7875.00 21.188 4.54
67
       8062.50 21.318 4.91
       8250.00 21.445
68
                       5.31
69
       8437.50 21.567
                       5.73
70
       8625.00 21.684 6.18
71
       8812.50 21.797 6.67
72
       9000.00 21.906 7.19
73
       9375.00 22.113
                       8.33
74
       9750.00 22.304 9.63
75
       10125.00
                       22.482 11.08
76
       10500.00
                       22.646 12.71
77
       10875.00
                       22.799 14.53
78
                       22.941 16.54
       11250.00
79
       11625.00
                       23.072 18.77
80
                       23.195 21.23
       12000.00
81
                       23.309 23.94
       12375.00
82
       12750.00
                       23.415 26.90
83
       13125.00
                       23.515 30.14
84
       13500.00
                       23.607 33.67
85
       13875.00
                       23.694 37.51
86
        14250.00
                       23.775 41.67
```

| 87 | 14625.00 | 23.852 | 46.17 |
|-----|----------|--------|-------|
| 88 | 15000.00 | 23.923 | 51.04 |
| 89 | 15375.00 | 23.991 | 56.29 |
| 90 | 15750.00 | 24.054 | 61.94 |
| 91 | 16125.00 | 24.114 | 68.00 |
| 92 | 16500.00 | 24.171 | 68.00 |
| 93 | 16875.00 | 24.224 | 68.00 |
| 94 | 17250.00 | 24.275 | 68.00 |
| 95 | 17625.00 | 24.322 | 68.00 |
| 96 | 18000.00 | 24.368 | 68.00 |
| 97 | 18375.00 | 24.411 | 68.00 |
| 98 | 18750.00 | 24.452 | 68.00 |
| 99 | 19125.00 | 24.491 | 68.00 |
| 100 | 19500.00 | 24.528 | 68.00 |
| 101 | 19875.00 | 24.564 | 68.00 |
| 102 | 20250.00 | 24.597 | 68.00 |
| | | | |

Table 3-D.1d.: Frequencies, Critical Band Rates and Absolute ThresholdTable is valid for Layer II at a sampling rate of 32.0 kHz.

| Index Number | | Frequency | | |
|---------------------|---------|--------------|-------|--|
| i | [Hz] | [z] | [dB] | |
| 1 | 31.25 | .309 | 58.23 | |
| 2 | 62.50 | .617 | 33.44 | |
| 3 | 93.75 | .925 | 24.17 | |
| 4 | 125.00 | 1.232 | 19.20 | |
| 5 | 156.25 | 1.538 | 16.05 | |
| 6 | 187.50 | 1.842 | 13.87 | |
| 7 | 218.75 | 2.145 | 12.26 | |
| 8 | 250.00 | 2.445 | 11.01 | |
| 9 | 281.25 | 2.742 | 10.01 | |
| 10 | 312.50 | 3.037 | 9.20 | |
| 11 | 343.75 | 3.329 | 8.52 | |
| 12 | 375.00 | 3.618 | 7.94 | |
| 13 | 406.25 | 3.903 | 7.44 | |
| 14 | 437.50 | 4.185 | 7.00 | |
| 15 | 468.75 | 4.463 | 6.62 | |
| 16 | 500.00 | 4.736 | 6.28 | |
| 17 | 531.25 | 5.006 | 5.97 | |
| 18 | 562.50 | 5.272 | 5.70 | |
| 19 | 593.75 | 5.533 | 5.44 | |
| 20 | 625.00 | 5.789 | 5.21 | |
| 21 | 656.25 | 6.041 | 5.00 | |
| 22 | 687.50 | 6.289 | 4.80 | |
| 23 | 718.75 | 6.532 | 4.62 | |
| 24 | 750.00 | 6.770 | 4.45 | |
| 25 | 781.25 | 7.004 | 4.29 | |
| 26 | 812.50 | 7.233 | 4.14 | |
| 27 | 843.75 | 7.457 | 4.00 | |
| 28 | 875.00 | 7.677 | 3.86 | |
| 29 | 906.25 | 7.892 | 3.73 | |
| 30 | 937.50 | 8.103 | 3.61 | |
| 31 | 968.75 | 8.309 | 3.49 | |
| 32 | 1000.00 | 8.511 | 3.37 | |
| 33 | 1031.25 | 8.708 | 3.26 | |

```
34
       1062.50 8.901
                       3.15
35
       1093.75 9.090
                       3.04
36
       1125.00 9.275
                       2.93
37
       1156.25 9.456
                       2.83
38
       1187.50 9.632
                       2.73
39
       1218.75 9.805
                       2.63
40
       1250.00 9.974
                       2.53
41
       1281.25 10.139 2.42
42
       1312.50 10.301 2.32
43
       1343.75 10.459 2.22
       1375.00 10.614 2.12
44
45
        1406.25 10.765 2.02
46
       1437.50 10.913 1.92
47
       1468.75 11.058 1.81
48
       1500.00 11.199 1.71
49
       1562.50 11.474 1.49
50
       1625.00 11.736
                       1.27
51
       1687.50 11.988
                       1.04
52
       1750.00 12.230 .80
53
        1812.50 12.461 .55
54
       1875.00 12.684 .29
55
        1937.50 12.898 .02
56
       2000.00 13.104 -.25
57
       2062.50 13.302 -.54
58
       2125.00 13.493 -.83
59
       2187.50 13.678 -1.12
60
       2250.00 13.855 -1.43
61
       2312.50 14.027 -1.73
62
       2375.00 14.193 -2.04
63
       2437.50 14.354 -2.34
64
       2500.00 14.509 -2.64
       2562.50 14.660 -2.93
65
66
       2625.00 14.807 -3.22
67
       2687.50 14.949 -3.49
68
       2750.00 15.087 -3.74
       2812.50 15.221 -3.98
69
70
       2875.00 15.351 -4.20
71
       2937.50 15.478 -4.40
72
       3000.00 15.602 -4.57
73
       3125.00 15.841 -4.82
74
       3250.00 16.069 -4.96
75
       3375.00 16.287 -4.97
76
       3500.00 16.496 -4.86
77
       3625.00 16.697 -4.63
78
       3750.00 16.891 -4.29
79
       3875.00 17.078 -3.87
80
       4000.00 17.259 -3.39
81
       4125.00 17.434 -2.86
82
       4250.00 17.605 -2.31
83
       4375.00 17.770 -1.77
       4500.00 17.932 -1.24
84
85
       4625.00 18.089 -.74
86
       4750.00 18.242 -.29
87
       4875.00 18.392 .12
88
       5000.00 18.539 .48
```

```
89
       5125.00 18.682 .79
90
       5250.00 18.823 1.06
91
       5375.00 18.960 1.29
92
       5500.00 19.095
                       1.49
93
        5625.00 19.226
                       1.66
94
       5750.00 19.356
                        1.81
95
       5875.00 19.482
                       1.95
96
       6000.00 19.606
                       2.08
97
       6250.00 19.847
                       2.33
98
       6500.00 20.079 2.59
99
       6750.00 20.300 2.86
100
       7000.00 20.513
                       3.17
101
       7250.00 20.717
                       3.51
102
       7500.00 20.912 3.89
103
       7750.00 21.098
                       4.31
104
       8000.00 21.275
                       4.79
105
       8250.00 21.445
                       5.31
106
       8500.00 21.606
                       5.88
107
       8750.00 21.760
                       6.50
108
       9000.00 21.906
                       7.19
109
       9250.00 22.046
                       7.93
110
       9500.00 22.178
                       8.75
111
       9750.00 22.304
                       9.63
112
        10000.00
                        22.424 10.58
113
        10250.00
                        22.538 11.60
114
        10500.00
                        22.646 12.71
115
                        22.749 13.90
        10750.00
116
        11000.00
                        22.847 15.18
                        22.941 16.54
117
        11250.00
118
                        23.030 18.01
        11500.00
119
        11750.00
                       23.114 19.57
120
                        23.195 21.23
        12000.00
121
        12250.00
                        23.272 23.01
122
        12500.00
                        23.345 24.90
123
        12750.00
                        23.415 26.90
124
        13000.00
                        23.482 29.03
125
                        23.546 31.28
        13250.00
126
        13500.00
                        23.607
                               33.67
127
        13750.00
                        23.666 36.19
128
        14000.00
                        23.722 38.86
129
        14250.00
                        23.775 41.67
130
                        23.827
        14500.00
                               44.63
131
        14750.00
                        23.876 47.76
132
                        23.923 51.04
        15000.00
```

Table 3-D.1e.: Frequencies, Critical Band Rates and Absolute ThresholdTable is valid for Layer II at a sampling rate of 44.1 kHz.

| Index | Number | Freque | ency | Crit.Band Rate | Absolute Thresh. |
|-------|--------|--------------|-------|-----------------------|------------------|
| i | [Hz] | [z] | [dB] | | |
| 1 | 43.07 | .425 | 45.05 | | |
| 2 | 86.13 | .850 | 25.87 | | |
| 3 | 129.20 | 1.273 | 18.70 | | |
| 4 | 172.27 | 1.694 | 14.85 | | |

```
5
        215.33 2.112
                        12.41
        258.40 2.525
6
                        10.72
7
        301.46 2.934
                        9.47
        344.53 3.337
8
                        8.50
9
        387.60 3.733
                       7.73
10
        430.66 4.124
                       7.10
        473.73 4.507
11
                       6.56
12
        516.80 4.882
                        6.11
13
        559.86 5.249
                       5.72
        602.93 5.608
14
                        5.37
15
        646.00 5.959
                       5.07
        689.06 6.301
                       4.79
16
17
        732.13 6.634
                       4.55
        775.20 6.959
18
                       4.32
19
        818.26 7.274
                       4.11
20
        861.33 7.581
                        3.92
21
        904.39 7.879
                       3.74
        947.46 8.169
22
                       3.57
        990.53 8.450
23
                       3.40
24
        1033.59 8.723
                       3.25
25
        1076.66 8.987
                       3.10
26
        1119.73 9.244
                       2.95
27
        1162.79 9.493
                       2.81
28
        1205.86 9.734
                       2.67
29
        1248.93 9.968
                       2.53
        1291.99 10.195 2.39
30
31
        1335.06 10.416 2.25
32
        1378.13 10.629
                       2.11
33
        1421.19 10.836 1.97
34
        1464.26 11.037 1.83
35
        1507.32 11.232 1.68
36
        1550.39 11.421 1.53
37
        1593.46 11.605 1.38
38
        1636.52 11.783 1.23
39
        1679.59 11.957 1.07
40
        1722.66 12.125
                       .90
41
        1765.72 12.289
                       .74
42
        1808.79 12.448 .56
43
        1851.86 12.603 .39
44
        1894.92 12.753 .21
        1937.99 12.900 .02
45
46
        1981.05 13.042 -.17
47
        2024.12 13.181 -.36
48
        2067.19 13.317 -.56
49
        2153.32 13.578 -.96
50
        2239.45 13.826 -1.38
51
        2325.59 14.062 -1.79
52
        2411.72 14.288 -2.21
53
        2497.85 14.504 -2.63
54
        2583.98 14.711 -3.03
        2670.12 14.909 -3.41
55
56
        2756.25 15.100 -3.77
57
        2842.38 15.284 -4.09
        2928.52 15.460 -4.37
58
59
        3014.65 15.631 -4.60
```

```
60
       3100.78 15.796 -4.78
       3186.91 15.955 -4.91
61
62
       3273.05 16.110 -4.97
63
       3359.18 16.260 -4.98
64
       3445.31 16.406 -4.92
65
       3531.45 16.547 -4.81
66
       3617.58 16.685 -4.65
67
       3703.71 16.820 -4.43
68
       3789.84 16.951 -4.17
69
       3875.98 17.079 -3.87
70
       3962.11 17.205 -3.54
71
       4048.24 17.327 -3.19
       4134.38 17.447 -2.82
72
73
       4306.64 17.680 -2.06
74
       4478.91 17.905 -1.32
75
       4651.17 18.121 -.64
76
       4823.44 18.331 -.04
77
       4995.70 18.534 .47
78
       5167.97 18.731 .89
79
       5340.23 18.922 1.23
80
       5512.50 19.108 1.51
81
       5684.77 19.289 1.74
82
       5857.03 19.464 1.93
83
       6029.30 19.635 2.11
84
       6201.56 19.801 2.28
85
       6373.83 19.963 2.46
86
       6546.09 20.120 2.63
87
       6718.36 20.273
                       2.82
88
       6890.63 20.421 3.03
89
       7062.89 20.565 3.25
90
       7235.16 20.705 3.49
91
       7407.42 20.840 3.74
92
       7579.69 20.972 4.02
93
       7751.95 21.099 4.32
94
       7924.22 21.222 4.64
95
       8096.48 21.342 4.98
96
       8268.75 21.457
                       5.35
97
       8613.28 21.677
                       6.15
98
       8957.81 21.882 7.07
99
       9302.34 22.074 8.10
       9646.88 22.253 9.25
100
101
       9991.41 22.420 10.54
102
       10335.94
                       22.576 11.97
103
       10680.47
                       22.721 13.56
104
       11025.00
                       22.857 15.31
105
       11369.53
                       22.984 17.23
106
                       23.102 19.34
       11714.06
107
       12058.59
                       23.213 21.64
108
                       23.317 24.15
       12403.13
109
       12747.66
                       23.415 26.88
                       23.506 29.84
110
       13092.19
111
       13436.72
                       23.592 33.05
112
       13781.25
                       23.673 36.52
                       23.749 40.25
113
       14125.78
114
        14470.31
                       23.821 44.27
```

| 115 | 14814.84 | 23.888 | 48.59 |
|-----|----------|--------|-------|
| 116 | 15159.38 | 23.952 | 53.22 |
| 117 | 15503.91 | 24.013 | 58.18 |
| 118 | 15848.44 | 24.070 | 63.49 |
| 119 | 16192.97 | 24.125 | 68.00 |
| 120 | 16537.50 | 24.176 | 68.00 |
| 121 | 16882.03 | 24.225 | 68.00 |
| 122 | 17226.56 | 24.271 | 68.00 |
| 123 | 17571.09 | 24.316 | 68.00 |
| 124 | 17915.63 | 24.358 | 68.00 |
| 125 | 18260.16 | 24.398 | 68.00 |
| 126 | 18604.69 | 24.436 | 68.00 |
| 127 | 18949.22 | 24.473 | 68.00 |
| 128 | 19293.75 | 24.508 | 68.00 |
| 129 | 19638.28 | 24.542 | 68.00 |
| 130 | 19982.81 | 24.574 | 68.00 |

Table 3-D.1f.: Frequencies, Critical Band Rates and Absolute ThresholdTable is valid for Layer II at a sampling rate of 48.0 kHz

| Index Number | | Frequency | | |
|---------------------|---------|--------------|-------|--|
| i | [Hz] | [z] | [dB] | |
| 1 | 46.88 | .463 | 42.10 | |
| 2 | 93.75 | .925 | 24.17 | |
| 3 | 140.63 | 1.385 | 17.47 | |
| 4 | 187.50 | 1.842 | 13.87 | |
| 5 | 234.38 | 2.295 | 11.60 | |
| 6 | 281.25 | 2.742 | 10.01 | |
| 7 | 328.13 | 3.184 | 8.84 | |
| 8 | 375.00 | 3.618 | 7.94 | |
| 9 | 421.88 | 4.045 | 7.22 | |
| 10 | 468.75 | 4.463 | 6.62 | |
| 11 | 515.63 | 4.872 | 6.12 | |
| 12 | 562.50 | 5.272 | 5.70 | |
| 13 | 609.38 | 5.661 | 5.33 | |
| 14 | 656.25 | 6.041 | 5.00 | |
| 15 | 703.13 | 6.411 | 4.71 | |
| 16 | 750.00 | 6.770 | 4.45 | |
| 17 | 796.88 | 7.119 | 4.21 | |
| 18 | 843.75 | 7.457 | 4.00 | |
| 19 | 890.63 | 7.785 | 3.79 | |
| 20 | 937.50 | 8.103 | 3.61 | |
| 21 | 984.38 | 8.410 | 3.43 | |
| 22 | 1031.25 | 8.708 | 3.26 | |
| 23 | 1078.13 | 8.996 | 3.09 | |
| 24 | 1125.00 | 9.275 | 2.93 | |
| 25 | 1171.88 | 9.544 | 2.78 | |
| 26 | 1218.75 | 9.805 | 2.63 | |
| 27 | 1265.63 | 10.057 | 2.47 | |
| 28 | 1312.50 | 10.301 | 2.32 | |
| 29 | 1359.38 | 10.537 | 2.17 | |
| 30 | 1406.25 | 10.765 | 2.02 | |
| 31 | 1453.13 | | 1.86 | |
| 32 | 1500.00 | | 1.71 | |
| 33 | 1546.88 | 11.406 | 1.55 | |
| 34 | 1593.75 | 11.606 | 1.38 | |

```
35
       1640.63 11.800 1.21
36
       1687.50 11.988 1.04
37
       1734.38 12.170 .86
38
       1781.25 12.347 .67
39
       1828.13 12.518 .49
40
       1875.00 12.684
                       .29
41
       1921.88 12.845 .09
42
       1968.75 13.002
                       -.11
43
       2015.63 13.154 -.32
44
       2062.50 13.302 -.54
45
       2109.38 13.446 -.75
46
       2156.25 13.586 -.97
47
       2203.13 13.723 -1.20
48
       2250.00 13.855 -1.43
49
       2343.75 14.111 -1.88
50
       2437.50 14.354 -2.34
51
       2531.25 14.585 -2.79
52
       2625.00 14.807 -3.22
53
       2718.75 15.018 -3.62
54
       2812.50 15.221 -3.98
55
       2906.25 15.415 -4.30
56
       3000.00 15.602 -4.57
57
       3093.75 15.783 -4.77
58
       3187.50 15.956 -4.91
59
       3281.25 16.124 -4.98
60
       3375.00 16.287 -4.97
61
       3468.75 16.445 -4.90
62
       3562.50 16.598 -4.76
63
       3656.25 16.746 -4.55
64
       3750.00 16.891 -4.29
65
       3843.75 17.032 -3.99
       3937.50 17.169 -3.64
66
67
       4031.25 17.303 -3.26
68
       4125.00 17.434 -2.86
69
       4218.75 17.563 -2.45
70
       4312.50 17.688 -2.04
71
       4406.25 17.811 -1.63
72
       4500.00 17.932 -1.24
73
       4687.50 18.166 -.51
74
       4875.00 18.392 .12
       5062.50 18.611 .64
75
76
       5250.00 18.823 1.06
77
       5437.50 19.028 1.39
78
       5625.00 19.226 1.66
79
       5812.50 19.419 1.88
80
       6000.00 19.606
                       2.08
81
       6187.50 19.788
                       2.27
82
       6375.00 19.964 2.46
83
       6562.50 20.135 2.65
84
       6750.00 20.300 2.86
85
       6937.50 20.461 3.09
86
       7125.00 20.616 3.33
87
       7312.50 20.766 3.60
88
       7500.00 20.912 3.89
89
       7687.50 21.052 4.20
```

| 90 | 7875.00 21.188 | 4.54 | |
|-----|----------------|--------|-------|
| 91 | 8062.50 21.318 | 4.91 | |
| 92 | 8250.00 21.445 | 5.31 | |
| 93 | 8437.50 21.567 | 5.73 | |
| 94 | 8625.00 21.684 | 6.18 | |
| 95 | 8812.50 21.797 | 6.67 | |
| 96 | 9000.00 21.906 | 7.19 | |
| 97 | 9375.00 22.113 | 8.33 | |
| 98 | 9750.00 22.304 | 9.63 | |
| 99 | 10125.00 | 22.482 | 11.08 |
| 100 | 10500.00 | 22.646 | 12.71 |
| 101 | 10875.00 | 22.799 | 14.53 |
| 102 | 11250.00 | 22.941 | 16.54 |
| 103 | 11625.00 | 23.072 | 18.77 |
| 104 | 12000.00 | 23.195 | 21.23 |
| 105 | 12375.00 | 23.309 | 23.94 |
| 106 | 12750.00 | 23.415 | 26.90 |
| 107 | 13125.00 | 23.515 | 30.14 |
| 108 | 13500.00 | 23.607 | 33.67 |
| 109 | 13875.00 | 23.694 | 37.51 |
| 110 | 14250.00 | 23.775 | |
| 111 | 14625.00 | 23.852 | 46.17 |
| 112 | 15000.00 | 23.923 | 51.04 |
| 113 | 15375.00 | 23.991 | 56.29 |
| 114 | 15750.00 | 24.054 | 61.94 |
| 115 | 16125.00 | 24.114 | 68.00 |
| 116 | 16500.00 | 24.171 | 68.00 |
| 117 | 16875.00 | 24.224 | 68.00 |
| 118 | 17250.00 | 24.275 | 68.00 |
| 119 | 17625.00 | 24.322 | 68.00 |
| 120 | 18000.00 | 24.368 | 68.00 |
| 121 | 18375.00 | 24.411 | 68.00 |
| 122 | 18750.00 | 24.452 | 68.00 |
| 123 | 19125.00 | 24.491 | 68.00 |
| 124 | 19500.00 | 24.528 | 68.00 |
| 125 | 19875.00 | 24.564 | |
| 126 | 20250.00 | 24.597 | 68.00 |
| | | | |

Table 3-D.2a. Critical Band Boundaries

This table is valid for Layer I at a sampling rate of 32.0 kHz. The frequencies represent the top end of each critical band.

| no | | index of frequency [Hz] table F&CB | | | | |
|----|----|------------------------------------|--------|--|--|--|
| 0 | 1 | 62.500 .617 | | | | |
| 1 | 3 | 187.500 1.842 | | | | |
| 2 | 5 | 312.500 3.037 | | | | |
| 3 | 7 | 437.500 4.185 | | | | |
| 4 | 9 | 562.500 5.272 | | | | |
| 5 | 11 | 687.500 6.289 | | | | |
| 6 | 13 | 812.500 7.233 | | | | |
| 7 | 15 | 937.500 8.103 | | | | |
| 8 | 18 | 1125.000 | 9.275 | | | |
| 9 | 21 | 1312.500 | 10.301 | | | |
| 10 | 24 | 1500.000 | 11.199 | | | |

| 11 | 27 | 1687.500 | 11.988 |
|----|-----|-----------|--------|
| 12 | 32 | 2000.000 | 13.104 |
| 13 | 37 | 2312.500 | 14.027 |
| 14 | 44 | 2750.000 | 15.087 |
| 15 | 50 | 3250.000 | 16.069 |
| 16 | 55 | 3875.000 | 17.078 |
| 17 | 61 | 4625.000 | 18.089 |
| 18 | 68 | 5500.000 | 19.095 |
| 19 | 74 | 6500.000 | 20.079 |
| 20 | 79 | 7750.000 | 21.098 |
| 21 | 85 | 9250.000 | 22.046 |
| 22 | 94 | 11500.000 | 23.030 |
| 23 | 108 | 15000.000 | 23.923 |

Table 3-D.2b. Critical Band Boundaries

This table is valid for Layer I at a sampling rate of 44.1 kHz. The frequencies represent the top end of each critical band.

| no | index of | f frequency [Hz] &CB | Bark [z] |
|----|----------|-------------------------|----------|
| 0 | 1 | 86.133 .850 | |
| 1 | 2 | 172.266 1.694 | |
| 2 | 3 | 258.398 2.525 | |
| 3 | 5 | 430.664 4.124 | |
| 4 | 6 | 516.797 4.882 | |
| 5 | 8 | 689.063 6.301 | |
| 6 | 9 | 775.195 6.959 | |
| 7 | 11 | 947.461 8.169 | |
| 8 | 13 | 1119.727 | 9.244 |
| 9 | 15 | 1291.992 | 10.195 |
| 10 | 17 | 1464.258 | 11.037 |
| 11 | 20 | 1722.656 | 12.125 |
| 12 | 23 | 1981.055 | 13.042 |
| 13 | 27 | 2325.586 | 14.062 |
| 14 | 32 | 2756.250 | 15.100 |
| 15 | 37 | 3186.914 | 15.955 |
| 16 | 45 | 3875.977 | 17.079 |
| 17 | 50 | 4478.906 | 17.904 |
| 18 | 55 | 5340.234 | 18.922 |
| 19 | 61 | 6373.828 | 19.963 |
| 20 | 68 | 7579.688 | 20.971 |
| 21 | 75 | 9302.344 | 22.074 |
| 22 | 81 | 11369.531 | 22.984 |
| 23 | 93 | 15503.906 | 24.013 |
| 24 | 106 | 19982.813 | 24.573 |
| | | | |

Table 3-D.2c. Critical Band Boundaries

This table is valid for Layer I at a sampling rate of 48.0 kHz. The frequencies represent the top end of each critical band.

| no | indez table | Bark[z] | |
|----|----------------|---------------|--|
| 0 | 1 | 93.750 .925 | |
| 1 | 2 | 187.500 1.842 | |
| 2 | 3 | 281.250 2.742 | |

| 3 | 4 | 375.000 3.618 | |
|----|-----|---------------|--------|
| 4 | 5 | 468.750 4.463 | |
| 5 | 6 | 562.500 5.272 | |
| 6 | 7 | 656.250 6.041 | |
| 7 | 9 | 843.750 7.457 | |
| 8 | 10 | 937.500 8.103 | |
| 9 | 12 | 1125.000 | 9.275 |
| 10 | 14 | 1312.500 | 10.301 |
| 11 | 16 | 1500.000 | 11.199 |
| 12 | 19 | 1781.250 | 12.347 |
| 13 | 21 | 1968.750 | 13.002 |
| 14 | 25 | 2343.750 | 14.111 |
| 15 | 29 | 2718.750 | 15.018 |
| 16 | 35 | 3281.250 | 16.124 |
| 17 | 41 | 3843.750 | 17.032 |
| 18 | 49 | 4687.500 | 18.166 |
| 19 | 53 | 5437.500 | 19.028 |
| 20 | 58 | 6375.000 | 19.964 |
| 21 | 65 | 7687.500 | 21.052 |
| 22 | 73 | 9375.000 | 22.113 |
| 23 | 79 | 11625.000 | 23.072 |
| 24 | 89 | 15375.000 | 23.991 |
| 25 | 102 | 20250.000 | 24.597 |

Table 3-D.2d. Critical Band BoundariesThis table is valid for Layer II at a sampling rate of 32.0 kHz.
The frequencies represent the top end of each critical band.

| no | indexof | frequency[Hz] | Bark[z] |
|----|---------|---------------|---------|
| | tableF& | кCB | |
| 0 | 1 | 31.250 .309 | |
| 1 | 3 | 93.750 .925 | |
| 2 | 6 | 187.500 1.842 | |
| 3 | 10 | 312.500 3.037 | |
| 4 | 13 | 406.250 3.903 | |
| 5 | 17 | 531.250 5.006 | |
| 6 | 21 | 656.250 6.041 | |
| 7 | 25 | 781.250 7.004 | |
| 8 | 30 | 937.500 8.103 | |
| 9 | 35 | 1093.750 | 9.090 |
| 10 | 41 | 1281.250 | 10.139 |
| 11 | 47 | 1468.750 | 11.058 |
| 12 | 51 | 1687.500 | 11.988 |
| 13 | 56 | 2000.000 | 13.104 |
| 14 | 61 | 2312.500 | 14.027 |
| 15 | 68 | 2750.000 | 15.087 |
| 16 | 74 | 3250.000 | 16.069 |
| 17 | 79 | 3875.000 | 17.078 |
| 18 | 85 | 4625.000 | 18.089 |
| 19 | 92 | 5500.000 | 19.095 |
| 20 | 98 | 6500.000 | 20.079 |
| 21 | 103 | 7750.000 | 21.098 |
| 22 | 109 | 9250.000 | 22.046 |
| 23 | 118 | 11500.000 | 23.030 |

Table 3-D.2e. Critical Band Boundaries

This table is valid for Layer II at a sampling rate of 44.1 kHz. The frequencies represent the top end of each critical band.

| no | indexof tableF& | frequency[Hz] | Bark[z] |
|----|--------------------|---------------|---------|
| 0 | 1 | 43.066 .425 | |
| 1 | 2 | 86.133 .850 | |
| 2 | 3 | 129.199 1.273 | |
| 3 | 5 | 215.332 2.112 | |
| 4 | 7 | 301.465 2.934 | |
| 5 | 10 | 430.664 4.124 | |
| 6 | 13 | 559.863 5.249 | |
| 7 | 16 | 689.063 6.301 | |
| 8 | 19 | 818.262 7.274 | |
| 9 | 22 | 947.461 8.169 | |
| 10 | 26 | 1119.727 | 9.244 |
| 11 | 30 | 1291.992 | 10.195 |
| 12 | 35 | 1507.324 | 11.232 |
| 13 | 40 | 1722.656 | 12.125 |
| 14 | 46 | 1981.055 | 13.042 |
| 15 | 51 | 2325.586 | 14.062 |
| 16 | 56 | 2756.250 | 15.100 |
| 17 | 62 | 3273.047 | 16.11 |
| 18 | 69 | 3875.977 | 17.079 |
| 19 | 74 | 4478.906 | 17.904 |
| 20 | 79 | 5340.234 | 18.922 |
| 21 | 85 | 6373.828 | 19.963 |
| 22 | 92 | 7579.688 | 20.971 |
| 23 | 99 | 9302.344 | 22.074 |
| 24 | 105 | 11369.531 | 22.984 |
| 25 | 117 | 15503.906 | 24.013 |
| 26 | 130 | 19982.813 | 24.573 |

Table 3-D.2f. Critical Band Boundaries

This table is valid for Layer II at a sampling rate of 48.0 kHz. The frequencies represent the top end of each critical band.

| no | index | of frequency [Hz] | Bark [z] |
|----|-------|-------------------|----------|
| | table | F&CB | |
| 0 | 1 | 46.875 .463 | |
| 1 | 2 | 93.750 .925 | |
| 2 | 3 | 140.625 1.385 | |
| 3 | 5 | 234.375 2.295 | |
| 4 | 7 | 328.125 3.184 | |
| 5 | 9 | 421.875 4.045 | |
| 6 | 12 | 562.500 5.272 | |
| 7 | 14 | 656.250 6.041 | |
| 8 | 17 | 796.875 7.119 | |
| 9 | 20 | 937.500 8.103 | |
| 10 | 24 | 1125.000 | 9.275 |
| 11 | 27 | 1265.625 | 10.057 |
| 12 | 32 | 1500.000 | 11.199 |
| 13 | 37 | 1734.375 | 12.170 |

| 14 | 42 | 1968.750 | 13.002 |
|----|-----|-----------|--------|
| 15 | 49 | 2343.750 | 14.111 |
| 16 | 53 | 2718.750 | 15.018 |
| 17 | 59 | 3281.250 | 16.124 |
| 18 | 65 | 3843.750 | 17.032 |
| 19 | 73 | 4687.500 | 18.166 |
| 20 | 77 | 5437.500 | 19.028 |
| 21 | 82 | 6375.000 | 19.964 |
| 22 | 89 | 7687.500 | 21.052 |
| 23 | 97 | 9375.000 | 22.113 |
| 24 | 103 | 11625.000 | 23.072 |
| 25 | 113 | 15375.000 | 23.991 |
| 26 | 126 | 20250.000 | 24.597 |

3-D.2 Psychoacoustic Model II

Psychoacoustic Model II is an independent psychoacoustic model that can be adjusted and adapted to any ISO-MPEG-Audio layer. This annex presents the general Psychoacoustic Model II, and provides sufficient information for implementation of Model II with Layers I and II. The Layer III Psychoacoustic Model is based on this implementation, with adaptations as described in the Layer III encoder clause.

The threshold generation process has three inputs. They are:

- 1. The shift length for the threshold calculation process, *iblen*, where 384<*iblen*<640. This *iblen* must remain constant over any particular application of the threshold calculation process. If (as in Layer III), it is necessary to calculate thresholds for two different shift lengths, two processes, each running with a fixed shift length, will be necessary. In the case of *iblen* outside the range of 384 to 640 it may be necessary to calculate the psychoacoustic thresholds with a different window length as well as shift length. There are two ways to do this:
 - Use a different length transform, and recalculate the startup coefficients for the model, or
 - Use the same length transform, but a substantially shorter Hann window, appropriate to the data and problem at hand.

The choice of these is left to the implementation.

- 2. The newest *iblen* samples of the signal, with the samples delayed (either in the filter bank or psychoacoustic calculation) such that the window of the psychoacoustic calculation is centered in the time-window of application.
- 3. The sampling rate. There are sets of tables provided for the standard sampling rates. Sampling rate, like *iblen*, must necessarily remain constant over one implementation of the threshold calculation process.

There is one output from Psychoacoustic Model II, a set of Signal to Masking Ratios, *SMRn*, which are adapted to the layers as described below.

Before running the Model initially, the array used to hold the preceding FFT source data window and the arrays used to hold r and f should be zeroed to provide a known starting point.

In Layer II, the psychoacoustic masking ratios must be calculated twice during each coder frame. The more stringent of each pair of ratios is used for bit allocation as shown in the software simulation model for Layers I and II with Psychoacoustic Model II.

Comments on Notation

Throughout this threshold calculation process, three indices for data values are used. These are:

- w indicates that the calculation is indexed by frequency in the FFT spectral line domain. An index of 1 corresponds to the DC term and an index of 513 corresponds to the spectral line at the Nyquest frequency.
- b indicates that the calculation is indexed in the threshold calculation partition domain. In the case where the calculation includes a convolution or sum in the threshold calculation partition domain, bb will be used as the summation variable. Partition numbering starts at 1.
- *n* indicates that the calculation is indexed in the coder bit (or codebook) allocation domain. An index of 1 corresponds to the lowest band in the subband filter bank.

The "Spreading Function"

Several points in the following description refer to the "spreading function". It is calculated by the following method:

```
tmpx = 1.05 (j-i),
```

Where i is the bark value of the signal being spread, j is the bark value of the band being spread into, and tmpx is a temporary variable.

```
x=8 minimum ((tmpx-0.5)^2-2(tmpx-0.5),0)
```

Where x is a temporary variable, and minimum (a,b) is a function returning the more negative of a or b.

```
tmpy=15.811389+7.5(tmpx+0.474)-17.5(1.0+(tmpx+0.474)^2)^{0.5}
```

where *tmpy* is another temporary variable.

```
if (tmpy < -100) then \{sprdngf(i,j)=0\} else \{sprdngf(i,j)=10^{(x+tmpy)/10}\}
```

Steps in Threshold Calculation

The following are the necessary steps for calculation of the SMRn used in the coder.

1. Reconstruct 1024 samples of the input signal.

iblen new samples are made available at every call to the threshold generator. The threshold generator must store 1024-*iblen* samples, and concatenate those samples to accurately reconstruct 1024 consecutive samples of the input signal, si, where i represents the index, 1 < i < 1024 of the current input stream.

2. Calculate the complex spectrum of the input signal.

First, si is windowed by a 1024 point Hann window, i.e. swi=si*(0.5-0.5cos()). Note that in Layer III, a shorter window may be used when window switching is active, with appropriate centering of the window, per the Layer III encoder description.

Second, a standard forward FFT of swi is calculated.

Third, the polar representation of the transform is calculated. rw and fw represent the magnitude and phase components of the transformed swi, respectively.

3. Calculate a predicted *r* and *f*.

A predicted magnitude, ^rw, and phase, ^fw are calculated from the preceding two threshold calculation blocks' r and f:

$$^{rw} = 2.0 rw (t-1) - rw (t-2)$$

$$fw = 2.0 fw (t-1) - fw (t-2)$$

where t represents the current block number, t-1 indexes the previous block's data, and t-2 indexes the data from the threshold calculation block before that.

4. Calculate the unpredictability measure cw

cw, the unpredictability measure, is:

$$cw = (((rw \cos fw - ^rw \cos ^fw)^2 + (rw \sin fw - ^rw \sin ^fw)^2)^{0.5}) / (rw + abs (^rw))$$

By sacrificing performance, this measure can be calculated on only a lower portion of the frequency lines. Calculations should be done from DC to at least 3kHz and preferably to7kHz. An upper limit of less than 5.5kHz may considerably reduce performance from that obtained during the subjective testing of the audio algorithm. The *cw* values above this limit should be set to 0.3. Best results will be obtained by calculating cw up to 20kHz.

5. Calculate the energy and unpredictability in the threshold calculation partitions.

The energy in each partition, eb, is:

$$eb = {}_{w=wlowb}{}^{whighb} \sum rw^2$$

and the weighted unpredictability, cb, is:

The threshold calculation partitions provide a resolution of approximately either one FFT line or 1/3 critical band, whichever is wider. At low frequencies, a single line of the FFT will constitute a calculation partition. At high frequencies, many lines will be combined into one calculation partition. A set of partition values is provided for each of the three sampling rates in Table 3-D.3."Calculation Partition Tables". These table elements will be used in the threshold calculation process. There are several elements in each table entry:

- 1. The index of the calculation partition, b.
- 2. The lowest frequency line in the partition, wlowb.
- 3. The highest frequency line in the partition, whighb.
- 4. The median bark value of the partition, *bvalb*.
- 5. A lower limit for the SNR in the partition that controls stereo unmasking effects, *minvalb*.
- 6. The value for tone masking noise (in dB) for the partition, *TMNb*.

A largest value of *b,bmax*, equal to the largest index, exists for each sampling rate.

6. Convolve the partitioned energy and unpredictability with the spreading function.

$$ctb = bb = 1$$
 $bmax \sum cbb * sprdngf(bvalbb, bvalb)$

Because ctb. is weighted by the signal energy, it must be renormalized to cbb.

At the same time, due to the non-normalized nature of the spreading function, *ecbb* should be renormalized and the normalized energy *enb*, calculated.

The normalization coefficient, rnormb. is:

$$rnormb=1/(bb=0)^{bmax} \sum sprdngf(bvalbb,bvalb))$$

7. Convert *cbb* to *tbb* .

$$tbb = -0.299-0.43\log(cbb)$$

Each tbb is limited to the range of 0 < tbb < 1.

8. Calculate the required SNR in each partition.

NMTb = 5.5 dB for all b. NMTb is the value for noise masking tone (in dB) for the partition. The required signal to noise ratio, SNRb, is:

$$SNRb = \max(minvalb, tbb * TMNb + (1-tbb) NMTb)$$

Where maximum (a,b) is a function returning the least negative of a or b.

9. Calculate the power ratio.

The power ratio, bcb, is:

$$bcb = 10^{-SNRb/10}$$

10. Calculation of actual energy threshold, *nbb*.

11. Spread the threshold energy over FFT lines, yielding *nbw*.

$$nbw = nbb / (whighb-wlowb+1)$$

12. Include absolute thresholds, yielding the final energy threshold of audibility, *thrw*

$$thrw = \max(nbw, absthrw)$$

The dB values of *absthr* shown in Tables 3-D.4. "Absolute Threshold Tables" are relative to the level that a sine wave of $\pm \frac{1}{2}$ lsb has in the FFT used for threshold calculation. The dB values must be converted into the energy domain after considering the FFT normalization actually used.

13. Pre-echo control

For Layer III, pre-echo control occurs at this point. The actual control is described as part of the Layer III encoder specification. This step is omitted for Layers I and II.

14. Calculate the signal-to-mask ratios, *SMRn*.

Table 3-D.5. "Layer I and II Coder Partition Table" shows:

- 1. The index, n, of the coder partition.
- 2. The lower index wlown, of the coder partition.
- 3. The upper index, whighn of the coder partition.
- 4. The width index, *widthn*, where *widthn*=1 for a psychoacoustically narrow scalefactor band, and *widthn*=0 for a psychoacoustically wide scalefactor band. A psychoacoustically narrow scalefactor band is one whose width is less than approximately 1/3 critical band.

The energy in the scalefactor band, epartn, is:

$$epartn = w = wlown whighn \sum rw^2$$

Then, if (widthn = 1), the noise level in the scalefactor band, *npartn* is calculated as:

$$npartn = w = wlown$$
 $vhighn$ $\sum thrw$

else,

$$npartn = minimum(thr_{wlown}, ..., thr_{whighn}) * (whighn - wlown + I)$$

Where, in this case, minimum (a,...,z) is a function returning the smallest positive argument of the arguments a...z.

The ratios to be sent to the coder, SMRn, are calculated as:

$$SMRn = 10 \log_{10} (epart_n/npart_n)$$

Table 3-D.3a. Calculation Partition Table

This table is valid at a sampling rate of 32.0 kHz.

| Index | wlow | whigh | bval | minval | TMN |
|-------|------|-------|------|--------|------------|
| 1 | 1 | 1 | 0.00 | 0.0 | 24.5 |
| 2 | 2 | 4 | 0.63 | 0.0 | 24.5 |
| 3 | 5 | 7 | 1.56 | 20.0 | 24.5 |
| 4 | 8 | 10 | 2.50 | 20.0 | 24.5 |
| 5 | 11 | 13 | 3.44 | 20.0 | 24.5 |
| 6 | 14 | 16 | 4.34 | 20.0 | 24.5 |
| 7 | 17 | 19 | 5.17 | 20.0 | 24.5 |
| 8 | 20 | 22 | 5.94 | 20.0 | 24.5 |

| 0 | 22 | 25 | ((2 | 17.0 | 24.5 |
|----------|----------|----------|----------------|--------------|--------------|
| 9 | 23 | 25 | 6.63 7.28 | 17.0 15.0 | 24.5 |
| 10 11 | 26 29 | 28 31 | 7.28 7.90 | 15.0 | 24.5 24.5 |
| 12 | 32 | 34 | 7.90 8.50 | 10.0 | 24.5 |
| 13 | 32 35 | 34 37 | 8.30 9.06 | 7.0 | 24.5 |
| 13 | 38 | 37 41 | 9.06 9.65 | 7.0 | 24.5 |
| 15 | 38 42 | 41 | 10.28 | 7.0 4.4 | 24.3 |
| 16 | 42 46 | 43 49 | 10.28 | 4.4 4.4 | 25.4 |
| 17 | 50 | 53 | 10.87 | 4.4 | 25.4 |
| 18 | 50 54 | 55 57 | 11.41 | 4.5 4.5 | 26.4 |
| | | | 12.39 | 4.5 4.5 | |
| 19 20 | 58 62 | 61 65 | 12.39 | 4.5 4.5 | 26.9 |
| | | | | | 27.3 |
| 21 22 | 66 | 70 75 | 13.29 13.78 | 4.5 4.5 | 27.8 |
| 23 | 71 76 | 75 81 | | | 28.3 |
| | 76 | | 14.27 | 4.5 | 28.8 |
| 24 | 82 | 87 | 14.76 | 4.5 | 29.3 |
| 25 | 88 | 93 | 15.22 | 4.5 | 29.7 |
| 26 | 94 | 99 | 15.63 | 4.5 | 30.1 |
| 27 | 100 | 106 | 16.06 | 4.5 | 30.6 |
| 28 | 107 | 113 | 16.47 | 4.5 | 31.0 |
| 29 | 114 | 120 | 16.86 | 4.5 | 31.4 |
| 30 | 121 | 129 | 17.25 | 4.5 | 31.8 |
| 31 | 130 | 138 | 17.65 | 4.5 | 32.2 |
| 32 | 139 | 148 | 18.05 | 4.5 | 32.5 |
| 33 | 149 | 159 | 18.42 | 4.5 | 32.9 |
| 34 | 160 | 170 | 18.81 | 4.5 | 33.3 |
| 35 | 171 | 183 | 19.18 | 4.5 | 33.7 |
| 36 | 184 | 196 | 19.55 | 4.5 | 34.1 |
| 37 | 197 | 210 | 19.93 | 4.5 | 34.4 |
| 38 | 211 | 225 | 20.29 | 4.5 | 34.8 |
| 39 | 226 | 240 | 20.65 | 4.5 | 35.2 |
| 40 | 241 | 258 | 21.02 | 4.5 | 35.5 |
| 41 | 259 | 279 | 21.38 | 4.5 | 35.9 |
| 42 | 280 | 300 | 21.74 | 4.5 | 36.2 |
| 43 | 301 | 326 | 22.10 | 4.5 | 36.6 |
| 44 | 327 | 354 | 22.44 | 4.5 | 36.9 |
| 45 | 355 | 382 | 22.79 | 4.5 | 37.3 |
| 46 | 383 | 420 | 23.14 | 4.5 | 37.6 |
| 47 | 421 | 458 | 23.49 | 4.5 | 38.0 |
| 48 | 459 | 496 | 23.83 | 4.5 | 38.3 |
| 49 | 497 | 513 | 24.07 | 4.5 | 38.6 |
| | | | | | |

Table 3-D.3b. Calculation Partition Table This table is valid at a sampling rate of 44.1.0 kHz.

| Index | wlow | whigh | bval | minval | TMN |
|-------|------|-------|------|--------|------|
| 1 | 1 | 1 | 0.00 | 0.0 | 24.5 |
| 2 | 2 | 2 | 0.43 | 0.0 | 24.5 |
| 3 | 3 | 3 | 0.86 | 0.0 | 24.5 |
| 4 | 4 | 4 | 1.29 | 20.0 | 24.5 |
| 5 | 5 | 5 | 1.72 | 20.0 | 24.5 |
| 6 | 6 | 6 | 2.15 | 20.0 | 24.5 |
| 7 | 7 | 7 | 2.58 | 20.0 | 24.5 |
| 8 | 8 | 8 | 3.01 | 20.0 | 24.5 |

| 9 | 9 | 9 | 3.45 | 20.0 | 24.5 |
|----|-----|-----|-------|------|------|
| 10 | 10 | 10 | 3.88 | 20.0 | 24.5 |
| | | | | | |
| 11 | 11 | 11 | 4.28 | 20.0 | 24.5 |
| 12 | 12 | 12 | 4.67 | 20.0 | 24.5 |
| 13 | 13 | 13 | 5.06 | 20.0 | 24.5 |
| 14 | 14 | 14 | 5.42 | 20.0 | 24.5 |
| 15 | 15 | 15 | 5.77 | 20.0 | 24.5 |
| | | | | | 24.5 |
| 16 | 16 | 16 | 6.11 | 17.0 | |
| 17 | 17 | 19 | 6.73 | 17.0 | 24.5 |
| 18 | 20 | 22 | 7.61 | 15.0 | 24.5 |
| 19 | 23 | 25 | 8.44 | 10.0 | 24.5 |
| 20 | 26 | 28 | 9.21 | 7.0 | 24.5 |
| 21 | 29 | 31 | 9.88 | 7.0 | 24.5 |
| 22 | 32 | 34 | 10.51 | 4.4 | 25.0 |
| 23 | 35 | 37 | 11.11 | 4.5 | 25.6 |
| 24 | 38 | 40 | 11.65 | 4.5 | 26.2 |
| | | | | | |
| 25 | 41 | 44 | 12.24 | 4.5 | 26.7 |
| 26 | 45 | 48 | 12.85 | 4.5 | 27.4 |
| 27 | 49 | 52 | 13.41 | 4.5 | 27.9 |
| 28 | 53 | 56 | 13.94 | 4.5 | 28.4 |
| 29 | 57 | 60 | 14.42 | 4.5 | 28.9 |
| 30 | 61 | 64 | 14.86 | 4.5 | 29.4 |
| 31 | 65 | 69 | 15.32 | 4.5 | 29.8 |
| 32 | 70 | 74 | 15.79 | 4.5 | 30.3 |
| 33 | | | 16.26 | | |
| | 75 | 80 | | 4.5 | 30.8 |
| 34 | 81 | 86 | 16.73 | 4.5 | 31.2 |
| 35 | 87 | 93 | 17.19 | 4.5 | 31.7 |
| 36 | 94 | 100 | 17.62 | 4.5 | 32.1 |
| 37 | 101 | 108 | 18.05 | 4.5 | 32.5 |
| 38 | 109 | 116 | 18.45 | 4.5 | 32.9 |
| 39 | 117 | 124 | 18.83 | 4.5 | 33.3 |
| 40 | 125 | 134 | 19.21 | 4.5 | 33.7 |
| 41 | 135 | 144 | 19.60 | 4.5 | 34.1 |
| 42 | 145 | 155 | 20.00 | 4.5 | 34.5 |
| | | | | | |
| 43 | 156 | 166 | 20.38 | 4.5 | 34.9 |
| 44 | 167 | 177 | 20.74 | 4.5 | 35.2 |
| 45 | 178 | 192 | 21.12 | 4.5 | 35.6 |
| 46 | 193 | 207 | 21.48 | 4.5 | 36.0 |
| 47 | 208 | 222 | 21.84 | 4.5 | 36.3 |
| 48 | 223 | 243 | 22.20 | 4.5 | 36.7 |
| 49 | 244 | 264 | 22.56 | 4.5 | 37.1 |
| 50 | 265 | 286 | 22.91 | 4.5 | 37.4 |
| 51 | 287 | 314 | 23.26 | 4.5 | |
| | | | | | 37.8 |
| 52 | 315 | 342 | 23.60 | 4.5 | 38.1 |
| 53 | 343 | 371 | 23.95 | 4.5 | 38.4 |
| 54 | 372 | 401 | 24.30 | 4.5 | 38.8 |
| 55 | 402 | 431 | 24.65 | 4.5 | 39.1 |
| 56 | 432 | 469 | 25.00 | 4.5 | 39.5 |
| 57 | 470 | 513 | 25.33 | 3.5 | 39.8 |
| | | - | | | |

Table 3-D.3c. Calculation Partition Table This table is valid at a sampling rate of 48.0 kHz.

| Index | wlow | whigh | bval | minval | TMN |
|-------|------|-------|------|--------|------|
| 1 | 1 | 1 | 0.00 | 0.0 | 24.5 |

| 2 3 | 2 3 | 2 3 | 0.47 0.94 | 0.0 0.0 | 24.5 24.5 |
|----------|------------|------------|----------------|--------------|--------------|
| 4 | 4 | 4 | 1.41 | 20.0 | 24.5 |
| 5 | 5 | 5 | 1.88 | 20.0 | 24.5 |
| 6 7 | 6 7 | 6 | 2.34 2.81 | 20.0 20.0 | 24.5 24.5 |
| 8 | 8 | 7 8 | 3.28 | 20.0 | 24.5 |
| 9 | 9 | 9 | 3.75 | 20.0 | 24.5 |
| 10 | 10 | 10 | 4.20 | 20.0 | 24.5 |
| 11 | 11 | 11 | 4.63 | 20.0 | 24.5 |
| 12 | 12 | 12 | 5.05 | 20.0 | 24.5 |
| 13 | 13 | 13 | 5.44 | 20.0 | 24.5 |
| 14 | 14 | 14 | 5.83 | 20.0 | 24.5 |
| 15 | 15 | 15 | 6.19 | 20.0 | 24.5 |
| 16 | 16 | 16 | 6.52 | 17.0 | 24.5 |
| 17 18 | 17 | 17 20 | 6.86 | 17.0 | 24.5 |
| 19 | 18 21 | 23 | 7.49 8.40 | 15.0 10.0 | 24.5 24.5 |
| 20 | 24 | 26 | 9.24 | 7.0 | 24.5 |
| 21 | 27 | 29 | 9.97 | 7.0 | 24.5 |
| 22 | 30 | 32 | 10.65 | 4.4 | 25.1 |
| 23 | 33 | 35 | 11.28 | 4.5 | 25.8 |
| 24 | 36 | 38 | 11.86 | 4.5 | 26.4 |
| 25 | 39 | 41 | 12.39 | 4.5 | 26.9 |
| 26 | 42 | 45 | 12.96 | 4.5 | 27.5 |
| 27 | 46 | 49 53 | 13.56 | 4.5 | 28.1 |
| 28 29 | 50 54 | 53 57 | 14.12 14.62 | 4.5 4.5 | 28.6 29.1 |
| 30 | 58 | 62 | 15.14 | 4.5 | 29.1 |
| 31 | 63 | 67 | 15.67 | 4.5 | 30.2 |
| 32 | 68 | 72 | 16.15 | 4.5 | 30.7 |
| 33 | 73 | 77 | 16.58 | 4.5 | 31.1 |
| 34 | 78 | 83 | 17.02 | 4.5 | 31.5 |
| 35 | 84 | 89 | 17.44 | 4.5 | 31.9 |
| 36 | 90 | 95 | 17.84 | 4.5 | 32.3 |
| 37 | 96 | 103 | 18.24 | 4.5 | 32.7 |
| 38 | 104 | 111 | 18.66 | 4.5 | 33.2 |
| 39 40 | 112 121 | 120 129 | 19.07 19.47 | 4.5 4.5 | 33.6 34.0 |
| 41 | 130 | 138 | 19.47 | 4.5 | 34.3 |
| 42 | 139 | 149 | 20.23 | 4.5 | 34.7 |
| 43 | 150 | 160 | 20.63 | 4.5 | 35.1 |
| 44 | 161 | 173 | 21.02 | 4.5 | 35.5 |
| 45 | 174 | 187 | 21.40 | 4.5 | 35.9 |
| 46 | 188 | 201 | 21.76 | 4.5 | 36.3 |
| 47 | 202 | 219 | 22.12 | 4.5 | 36.6 |
| 48 | 220 | 238 | 22.47 | 4.5 | 37.0 |
| 49 50 | 239 258 | 257 283 | 22.83 23.18 | 4.5 4.5 | 37.3 37.7 |
| 51 | 284 | 309 | 23.18 | 4.5 | 38.0 |
| 52 | 310 | 335 | 23.88 | 4.5 | 38.4 |
| 53 | 336 | 363 | 24.23 | 4.5 | 38.7 |
| 54 | 364 | 391 | 24.58 | 4.5 | 39.1 |
| 55 | 392 | 423 | 24.93 | 4.5 | 39.4 |
| 56 | 424 | 465 | 25.27 | 4.5 | 39.8 |
| | | | | | |

| 57 | 466 | 507 | 25.61 | 3.5 | 40.1 |
|----|-----|-----|-------|-----|------|
| 58 | 508 | 513 | 25.81 | 3.5 | 40.3 |

Table 3-D.4a. Absolute Threshold Table This table is valid at a sampling rate of 32.0 kHz.

A value of 0 dB represents a level in the absolute threshold calculation of 96 dB below the energy of a sine wave of amplitude +-32760.

| | (line) higher | absthr (dB) |
|------------------|------------------|----------------|
| 1 | 1 | 58.23 |
| 2 | 2 | 33.44 |
| 3 | 3 | 24.17 |
| 3 4 5 6 | 4 5 | 19.20 16.05 |
| 6 | 6 | 13.87 |
| 7 | 7 | 12.26 |
| 8 | 8 | 11.01 |
| 9 | 9 | 10.01 |
| 10 | 10 | 9.20 |
| 11 | 11 | 8.52 |
| 12 | 12 | 7.94 |
| 13 | 13 | 7.44 |
| 14 | 14 | 7.00 |
| 15 | 15 | 6.62 |
| 16 | 16 | 6.28 |
| 17 | 17 | 5.97 |
| 18 | 18 | 5.70 |
| 19 | 19 | 5.44 |
| 20 | 20 | 5.21 |
| 21 | 21 | 5.00 |
| 22 | 22 | 4.80 |
| 23 | 23 | 4.62 |
| 24 | 24 | 4.45 |
| 25 | 25 | 4.29 |
| 26 | 26 | 4.14 |
| 27 | 27 | 4.00 |
| 28 | 28 | 3.86 |
| 29 | 29 | 3.73 |
| 30 | 30 | 3.61 |
| 31 | 31 | 3.49 |
| 32 | 32 | 3.37 |
| 33 | 33 | 3.26 |
| 34 | 34 | 3.15 |
| 35 | 35 | 3.04 |
| 36 | 36 | 2.93 |
| 37 | 37 | 2.83 |
| 38 | 38 | 2.73 |

| 39 | 39 | 2.63 |
|------------|------------|----------------|
| 40 | 40 | 2.53 |
| 41 42 | 41 42 | 2.42 2.32 |
| 43 | 43 | 2.22 |
| 44 | 44 | 2.12 |
| 45 46 | 45 46 | 2.02 1.92 |
| 47 | 47 | 1.81 |
| 48 | 48 | 1.71 |
| 49 51 | 50 52 | 1.49 1.27 |
| 53 | 54 | 1.04 |
| 55 | 56 | .80 |
| 57 59 | 57 60 | .55 .29 |
| 61 | 62 | .02 |
| 63 | 64 | 25 |
| 65 67 | 66 | 54 83 |
| 69 | 68 70 | -1.12 |
| 71 | 72 | -1.43 |
| 73 75 | 74 76 | -1.73 |
| 75 77 | 76 78 | -2.04 -2.34 |
| 79 | 80 | -2.64 |
| 81 83 | 82 | -2.93 |
| 85 85 | 84 86 | -3.22 -3.49 |
| 87 | 88 | -3.74 |
| 89 | 90 | -3.98 -4.20 |
| 91 93 | 92 94 | -4.20 -4.40 |
| 95 | 96 | -4.57 |
| 97 | 100 | -4.82 |
| 101 105 | 104 108 | -4.96 -4.97 |
| 109 | 112 | -4.86 |
| 113 | 116 | -4.63 |
| 117 121 | 120 124 | -4.29 -3.87 |
| 125 | 128 | -3.39 |
| 129 | 132 | -2.86 |
| 133 137 | 136 140 | -2.31 -1.77 |
| 141 | 144 | -1.77 -1.24 |
| 145 149 | 148 152 | 74 29 |
| 153 | 156 | .12 |
| 157 | 160 | .48 |
| 161 165 | 164 168 | .79 1.06 |
| 169 | 172 | 1.00 |
| 173 | 176 | 1.49 |
| 177 | 180 | 1.66 |

| 181 | 184 | 1.81 |
|-----|-----|-------|
| 185 | 188 | 1.95 |
| 189 | 192 | 2.08 |
| 193 | 200 | 2.33 |
| 201 | 208 | 2.59 |
| 209 | 216 | 2.86 |
| 217 | 224 | 3.17 |
| 225 | 232 | 3.51 |
| 233 | 240 | 3.89 |
| 241 | 248 | 4.31 |
| 249 | 256 | 4.79 |
| 257 | 264 | 5.31 |
| 265 | 272 | 5.88 |
| 273 | 280 | 6.50 |
| 281 | 288 | 7.19 |
| 289 | 296 | 7.13 |
| 297 | 304 | 8.75 |
| 305 | 312 | 9.63 |
| 313 | 320 | 10.58 |
| 321 | 328 | 11.60 |
| 329 | 336 | 12.71 |
| 337 | 344 | 13.90 |
| 345 | 352 | 15.18 |
| 353 | 360 | 16.54 |
| 361 | 368 | 18.01 |
| 369 | 376 | 19.57 |
| 377 | 384 | 21.23 |
| 385 | 392 | 23.01 |
| 393 | 400 | 24.90 |
| 401 | 408 | 26.90 |
| 409 | 416 | 29.03 |
| 417 | 424 | 31.28 |
| 425 | 432 | 33.67 |
| 433 | 440 | 36.19 |
| 441 | 448 | 38.86 |
| 449 | 456 | 41.67 |
| 457 | 464 | 44.63 |
| 465 | 472 | 47.76 |
| 473 | 480 | 51.03 |
| +/3 | 400 | 31.03 |

Table 3-D.4b. Absolute Threshold Table

This table is valid at a sampling rate of 44.1 kHz.

A value of 0 dB represents a level in the absolute threshold calculation of 96 dB below the energy of a sine wave of amplitude ± 32760 .

| | (line) higher | absthr dB | |
|---|------------------|--------------|--|
| | | | |
| 1 | 1 | 45.05 | |

| 2 | 2 | 25.87 |
|------------|----------|----------------|
| 3 | 3 | 18.70 |
| 4 | 4 | 14.85 |
| 5 | 5 | 12.41 |
| 6 7 | 6 7 | 10.72 9.47 |
| 8 | 8 | 8.50 |
| 9 | 9 | 7.73 |
| 10 | 10 | 7.10 |
| 11 | 11 | 6.56 |
| 12 | 12 | 6.11 |
| 13 | 13 | 5.72 |
| 14 | 14 | 5.37 |
| 15 | 15 | 5.07 |
| 16 | 16 | 4.79 |
| 17 | 17 | 4.55 |
| 18 | 18 | 4.32 |
| 19 | 19 | 4.11 |
| 20 | 20 | 3.92 |
| 21 | 21 | 3.74 |
| 22 | 22 23 | 3.57 |
| 23 24 | 23 24 | 3.40 3.25 |
| 25 | 25 | 3.23 |
| 26 | 26 | 2.95 |
| 27 | 27 | 2.81 |
| 28 | 28 | 2.67 |
| 29 | 29 | 2.53 |
| 30 | 30 | 2.39 |
| 31 | 31 | 2.25 |
| 32 | 32 | 2.11 |
| 33 | 33 | 1.97 |
| 34 | 34 | 1.83 |
| 35 | 35 | 1.68 |
| 36 | 36 | 1.53 1.38 |
| 37 38 | 37 38 | 1.38 |
| 39 | 38 39 | 1.23 |
| 40 | 40 | .90 |
| 41 | 41 | .74 |
| 42 | 42 | .56 |
| 43 | 43 | .39 |
| 44 | 44 | .21 |
| 45 | 45 | .02 |
| 46 | 46 | 17 |
| 47 | 47 | 36 |
| 48 | 48 | 56 |
| 49 | 50 | 96 |
| 51 | 52 54 | -1.37 |
| 53 55 | 54 56 | -1.79 -2.21 |
| 55 57 | 56 58 | -2.21 -2.63 |
| 5 <i>1</i> | 58 60 | -3.03 |
| 61 | 62 | -3.41 |
| 63 | 64 | -3.77 |
| 55 | ٠. | 2.11 |

| 133 136 1.93 137 140 2.11 141 144 2.28 145 148 2.45 149 152 2.63 153 156 2.82 157 160 3.03 161 164 3.25 165 168 3.49 169 172 3.74 173 176 4.02 177 180 4.32 181 184 4.64 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 | 133 136 1.93 137 140 2.11 141 144 2.28 145 148 2.45 149 152 2.63 153 156 2.82 157 160 3.03 161 164 3.25 165 168 3.49 169 172 3.74 173 176 4.02 177 180 4.32 181 184 4.64 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 | 65 67 69 71 73 75 77 79 81 83 85 87 89 91 93 95 97 101 105 109 113 117 121 | 66 68 70 72 74 76 78 80 82 84 86 88 90 92 94 96 100 104 108 112 116 120 124 128 | -4.09 -4.37 -4.60 -4.78 -4.91 -4.97 -4.98 -4.92 -4.81 -4.65 -4.43 -4.17 -3.87 -3.54 -3.19 -2.82 -2.06 -1.33 64 04 .47 .89 1.23 1.51 |
|--|---|--|--|--|
| 129 132 1.74 133 136 1.93 137 140 2.11 141 144 2.28 145 148 2.45 149 152 2.63 153 156 2.82 157 160 3.03 161 164 3.25 165 168 3.49 169 172 3.74 173 176 4.02 177 180 4.32 181 184 4.64 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 | 129 132 1.74 133 136 1.93 137 140 2.11 141 144 2.28 145 148 2.45 149 152 2.63 153 156 2.82 157 160 3.03 161 164 3.25 165 168 3.49 169 172 3.74 173 176 4.02 177 180 4.32 181 184 4.64 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 249 256 15.30 257 264 17.23 265 272 19.33 273 <td>117 121</td> <td>120 124</td> <td>.89 1.23</td> | 117 121 | 120 124 | .89 1.23 |
| 145 148 2.45 149 152 2.63 153 156 2.82 157 160 3.03 161 164 3.25 165 168 3.49 169 172 3.74 173 176 4.02 177 180 4.32 181 184 4.64 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 | 145 148 2.45 149 152 2.63 153 156 2.82 157 160 3.03 161 164 3.25 165 168 3.49 169 172 3.74 173 176 4.02 177 180 4.32 181 184 4.64 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 249 256 15.30 257 264 17.23 265 272 19.33 273 280 21.64 | 129 133 137 | 132 136 140 | 1.74 1.93 2.11 |
| 157 160 3.03 161 164 3.25 165 168 3.49 169 172 3.74 173 176 4.02 177 180 4.32 181 184 4.64 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 | 157 160 3.03 161 164 3.25 165 168 3.49 169 172 3.74 173 176 4.02 177 180 4.32 181 184 4.64 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 249 256 15.30 257 264 17.23 265 272 19.33 273 280 21.64 | 145 149 | 148 152 | 2.45 2.63 |
| 173 176 4.02 177 180 4.32 181 184 4.64 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 | 173 176 4.02 177 180 4.32 181 184 4.64 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 249 256 15.30 257 264 17.23 265 272 19.33 273 280 21.64 | 157 161 | 160 164 | 3.03 3.25 |
| 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 | 185 188 4.98 189 192 5.35 193 200 6.15 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 249 256 15.30 257 264 17.23 265 272 19.33 273 280 21.64 | 173 177 | 176 180 | 4.02 4.32 |
| 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 | 201 208 7.07 209 216 8.10 217 224 9.25 225 232 10.54 233 240 11.97 241 248 13.56 249 256 15.30 257 264 17.23 265 272 19.33 273 280 21.64 | 185 189 | 188 192 | 4.98 5.35 |
| 233 240 11.97 241 248 13.56 | 233 240 11.97 241 248 13.56 249 256 15.30 257 264 17.23 265 272 19.33 273 280 21.64 | 201 209 217 | 208 216 224 | 7.07 8.10 9.25 |
| | 257 264 17.23 265 272 19.33 273 280 21.64 | 233 241 | 240 248 | 11.97 13.56 |

| 313 | 320 | 36.51 |
|-----|-----|-------|
| 321 | 328 | 40.24 |
| 329 | 336 | 44.26 |
| 337 | 344 | 48.58 |
| 345 | 352 | 53.21 |
| 353 | 360 | 58.17 |
| 361 | 368 | 63.48 |
| 369 | 376 | 69.13 |
| 377 | 384 | 69.13 |
| 385 | 392 | 69.13 |
| 393 | 400 | 69.13 |
| 401 | 408 | 69.13 |
| 409 | 416 | 69.13 |
| 417 | 424 | 69.13 |
| 425 | 432 | 69.13 |
| 433 | 440 | 69.13 |
| 441 | 448 | 69.13 |
| 449 | 456 | 69.13 |
| 457 | 464 | 69.13 |

Table 3-D.4c. Absolute Threshold Table

This table is valid at a sampling rate of 48.0 kHz.

A value of 0 dB represents a level in the absolute threshold calculation of 96 dB below the energy of a sine wave of amplitude ± 32760 .

| | (line) highe | absthr. r dB |
|----|-----------------|-----------------|
| | | |
| 1 | 1 | 42.10 |
| 2 | 2 | 24.17 |
| 3 | 3 | 17.47 |
| 4 | 4 | 13.87 |
| 5 | 5 | 11.60 |
| 6 | 6 | 10.01 |
| 7 | 7 | 8.84 |
| 8 | 8 | 7.94 |
| 9 | 9 | 7.22 |
| 10 | 10 | 6.62 |
| 11 | 11 | 6.12 |
| 12 | 12 | 5.70 |
| 13 | 13 | 5.33 |
| 14 | 14 | 5.00 |
| 15 | 15 | 4.71 |
| 16 | 16 | 4.45 |
| 17 | 17 | 4.21 |
| 18 | 18 | 4.00 |
| 19 | 19 | 3.79 |
| 20 | 20 | 3.61 |
| 21 | 21 | 3.43 |
| 22 | 22 | 3.26 |
| 23 | 23 | 3.09 |
| 24 | 24 | 2.93 |

| 25 | 25 | 2.78 |
|-----|-----|-------|
| 26 | 26 | 2.63 |
| 27 | 27 | 2.47 |
| 28 | 28 | 2.32 |
| 29 | 29 | 2.17 |
| 30 | 30 | 2.02 |
| 31 | 31 | 1.86 |
| 32 | 32 | 1.71 |
| | | |
| 33 | 33 | 1.55 |
| 34 | 34 | 1.38 |
| 35 | 35 | 1.21 |
| 36 | 36 | 1.04 |
| 37 | 37 | .86 |
| 38 | 38 | .67 |
| 39 | 39 | .49 |
| 40 | 40 | .29 |
| 41 | 41 | .09 |
| 42 | 42 | 11 |
| 43 | 43 | 32 |
| 44 | 44 | 54 |
| 45 | 45 | 75 |
| 46 | 46 | 97 |
| 47 | 47 | -1.20 |
| 48 | 48 | -1.43 |
| 49 | 50 | |
| | | -1.88 |
| 51 | 52 | -2.34 |
| 53 | 54 | -2.79 |
| 55 | 56 | -3.22 |
| 57 | 58 | -3.62 |
| 59 | 60 | -3.98 |
| 61 | 62 | -4.30 |
| 63 | 64 | -4.57 |
| 65 | 66 | -4.77 |
| 67 | 68 | -4.91 |
| 69 | 70 | -4.98 |
| 71 | 72 | -4.97 |
| 73 | 74 | -4.90 |
| 75 | 76 | -4.76 |
| 77 | 78 | -4.55 |
| 79 | 80 | -4.29 |
| 81 | 82 | -3.99 |
| 83 | 84 | -3.64 |
| 85 | 86 | -3.26 |
| 87 | 88 | -2.86 |
| | 90 | -2.45 |
| 89 | | |
| 91 | 92 | -2.04 |
| 93 | 94 | -1.63 |
| 95 | 96 | -1.24 |
| 97 | 100 | 51 |
| 101 | 104 | .12 |
| 105 | 108 | .64 |
| 109 | 112 | 1.06 |
| 113 | 116 | 1.39 |
| 117 | 120 | 1.66 |
| 121 | 124 | 1.88 |
| | | |

| 105 | 120 | 2.00 |
|-----|-----|--------------|
| 125 | 128 | 2.08 |
| 129 | 132 | 2.27 |
| | | |
| 133 | 136 | 2.46 |
| 137 | 140 | 2.65 |
| 141 | 144 | |
| | | 2.86 |
| 145 | 148 | 3.09 3.33 |
| 149 | 152 | 3 33 |
| 149 | | 3.33 |
| 153 | 156 | 3.60 |
| 157 | 160 | 3.89 |
| | | |
| 161 | 164 | 4.20 |
| 165 | 168 | 4.54 |
| | 172 | 4.91 |
| 169 | | |
| 173 | 176 | 5.31 |
| 177 | 180 | 5.73 |
| | | |
| 181 | 184 | 6.18 |
| 185 | 188 | 6.67 |
| | | |
| 189 | 192 | 7.19 |
| 193 | 200 | 8.33 |
| 201 | 208 | 9.63 |
| | | |
| 209 | 216 | 11.08 |
| 217 | 224 | 12.71 |
| 225 | 232 | 14.52 |
| | | 14.53 |
| 233 | 240 | 16.54 |
| 241 | 248 | 18.77 |
| 249 | 256 | 21.23 |
| | | 21.23 |
| 257 | 264 | 23.94 |
| 265 | 272 | 26.90 |
| | | |
| 273 | 280 | 30.14 |
| 281 | 288 | 33.67 |
| 289 | 296 | 37.51 |
| | | |
| 297 | 304 | 41.67 |
| 305 | 312 | 46.17 |
| 313 | 320 | 51.04 |
| | | |
| 321 | 328 | 56.29 |
| 329 | 332 | 61.94 |
| 333 | | |
| | 340 | 68.00 |
| 341 | 348 | 68.00 |
| 349 | 356 | 68.00 |
| - | | |
| 357 | 364 | 68.00 |
| 365 | 372 | 68.00 |
| 373 | 380 | 68.00 |
| | | |
| 381 | 388 | 68.00 |
| 389 | 396 | 68.00 |
| | | |
| 397 | 404 | 68.00 |
| 405 | 412 | 68.00 |
| 413 | 420 | 68.00 |
| | | |
| 421 | 428 | 68.00 |
| | | |

Table 3-D.5. Layer I and Layer II Coder Partition Table

| Index | ωlown+1 | | widthn |
|-------|---------|----|--------|
| | ωhigl | hn | |
| 0 | 1 | 0 | |
| 1 | 17 | 0 | |
| 2 | 33 | 0 | |
| 3 | 49 | 0 | |

| 4 | 65 | 0 |
|----|-----|---|
| 5 | 81 | 0 |
| 6 | 97 | 0 |
| 7 | 113 | 0 |
| 8 | 129 | 0 |
| 9 | 145 | 0 |
| 10 | 161 | 0 |
| 11 | 177 | 0 |
| 12 | 193 | 0 |
| 13 | 209 | 1 |
| 14 | 225 | 1 |
| 15 | 241 | 1 |
| 16 | 257 | 1 |
| 17 | 273 | 1 |
| 18 | 289 | 1 |
| 19 | 305 | 1 |
| 20 | 321 | 1 |
| 21 | 337 | 1 |
| 22 | 353 | 1 |
| 23 | 369 | 1 |
| 24 | 385 | 1 |
| 25 | 401 | 1 |
| 26 | 417 | 1 |
| 27 | 433 | 1 |
| 28 | 449 | 1 |
| 29 | 465 | 1 |
| 30 | 481 | 1 |
| 31 | 497 | 1 |
| 32 | 513 | 1 |
| | | |