FEM Simulation of 3D Deformable Solids

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Outline

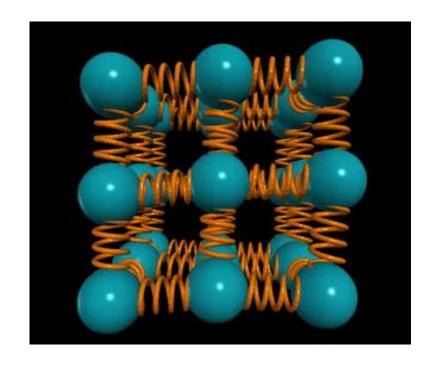
- Elasticity in 3D
- Discretization
- Constitutive models of materials
 - Linear elasticity
 - Corotated linear elasticity
 - Other materials (StVK, Neohookean)
- Modal analysis and model reduction

https://viterbi-web.usc.edu/~jbarbic/femdefo/

Eftychios Sifakis and Jernej Barbic. 2012. *FEM simulation of 3D deformable solids: a practitioner's guide to theory, discretization and model reduction*. In *ACM SIGGRAPH 2012 Courses* (SIGGRAPH '12),

Mass Spring Systems for Solids

- Simple and faster
- Hard to simulate real materials



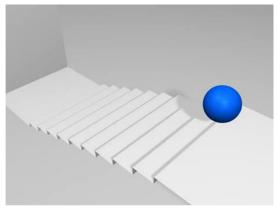
Deformable Solids



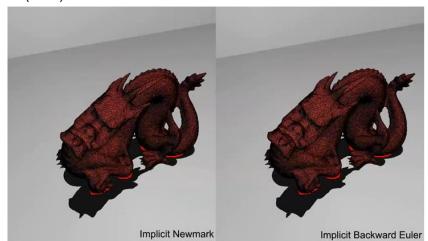
Tan, Jie, Greg Turk, and C. Karen Liu. "Soft body locomotion." *ACM Transactions on Graphics (TOG)* 31.4 (2012): 1-11.



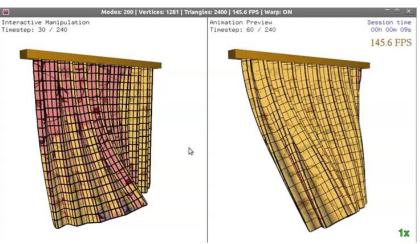
Barbič, Jernej, and Yili Zhao. "Real-time large-deformation substructuring." *ACM transactions on graphics (TOG)* 30.4 (2011): 1-8.



Coros, Stelian, et al. "Deformable objects alive!." *ACM Transactions on Graphics* (*TOG*) 31.4 (2012): 1-9.

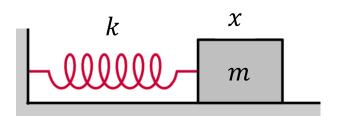


Sin, Fun Shing, Daniel Schroeder, and Jernej Barbič. "Vega: non-linear FEM deformable object simulator." *Computer Graphics Forum*. Vol. 32. No. 1.

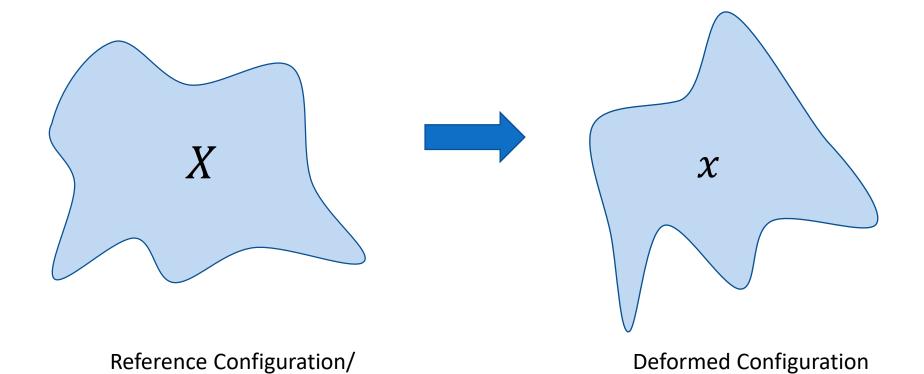


Barbič, Jernej, Funshing Sin, and Eitan Grinspun. "Interactive editing of deformable simulations." *ACM Transactions on Graphics (TOG)* 31.4 (2012): 1-8.

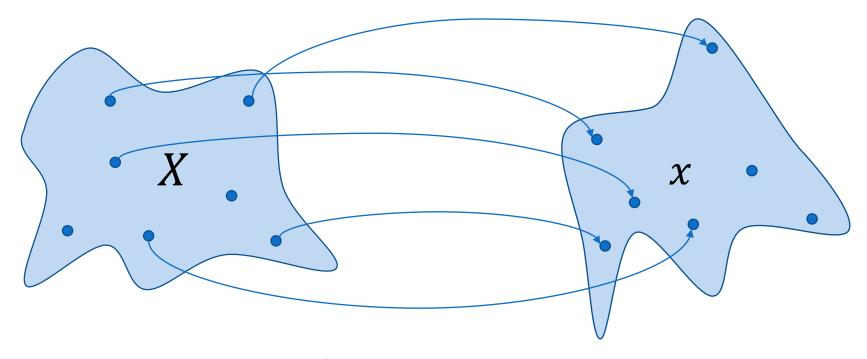
Hooke's Law



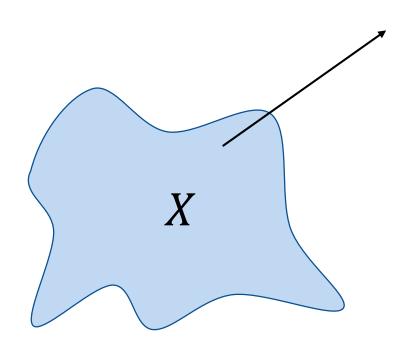
Material Space



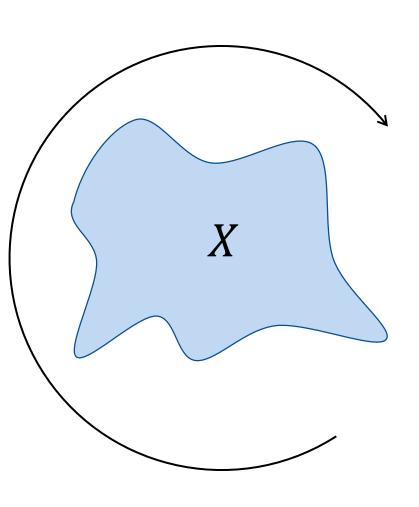
$$x = \varphi(X)$$



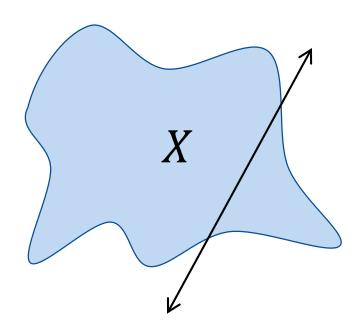
Reference Configuration/ Material Space **Deformed Configuration**



$$x = \varphi(X) = X + t$$



$$x = \varphi(X) = RX$$



$$x = \varphi(X) = SX$$

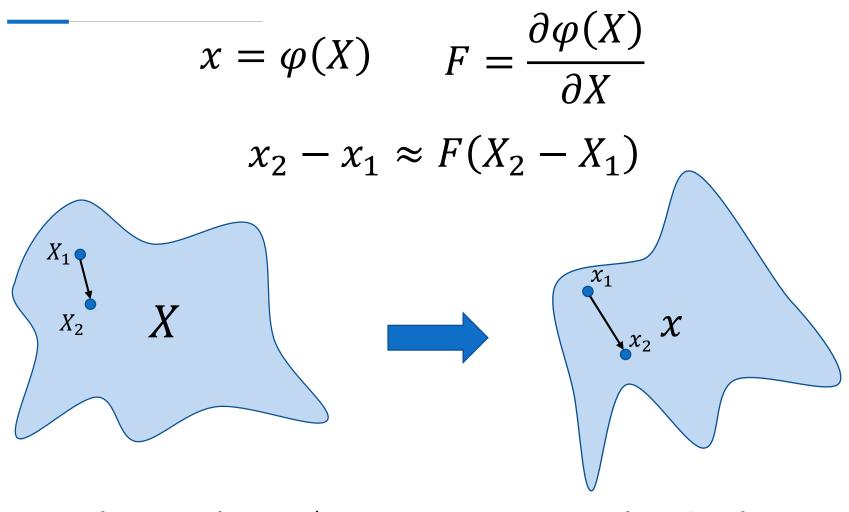
Deformation Gradient

$$x = \varphi(X) \qquad F = \frac{\partial \varphi(X)}{\partial X}$$

Reference Configuration/ Material Space

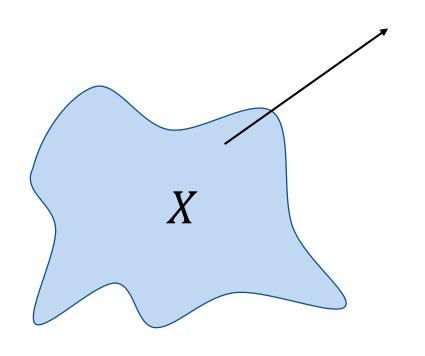
Deformed Configuration

Deformation Gradient



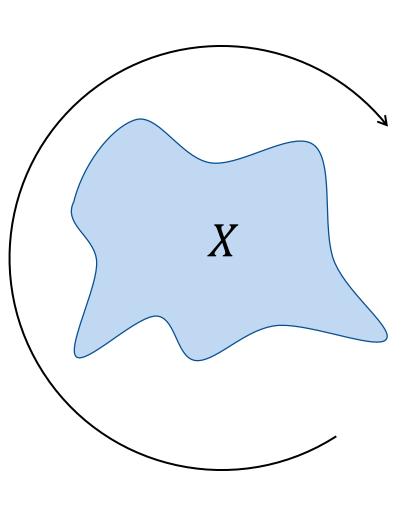
Reference Configuration/ Material Space

Deformed Configuration



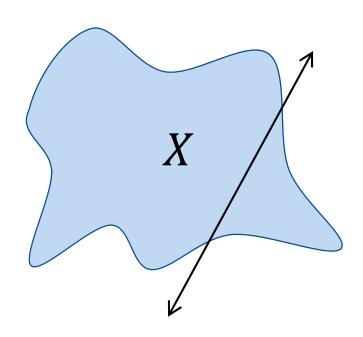
$$x = \varphi(X) = X + t$$

$$F = I$$



$$x = \varphi(X) = RX$$

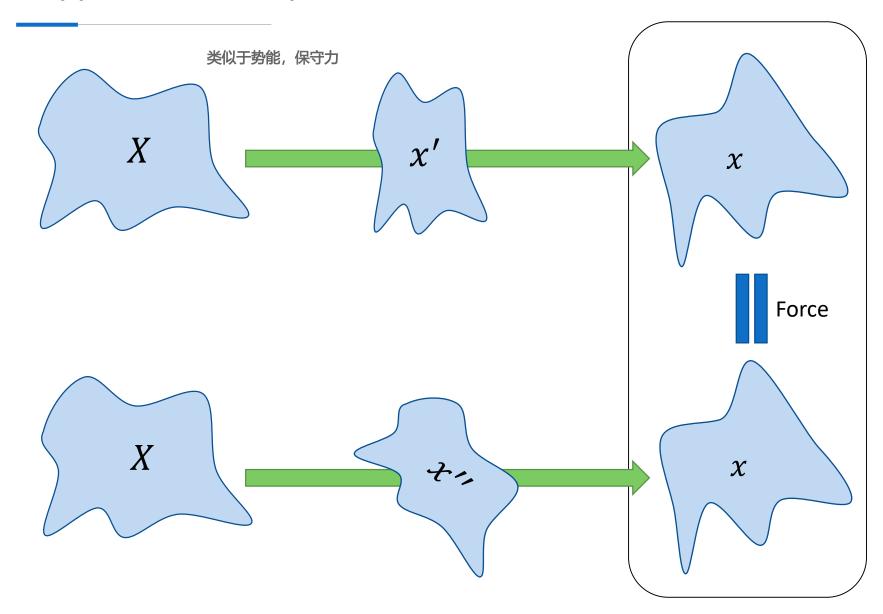
$$F = R$$



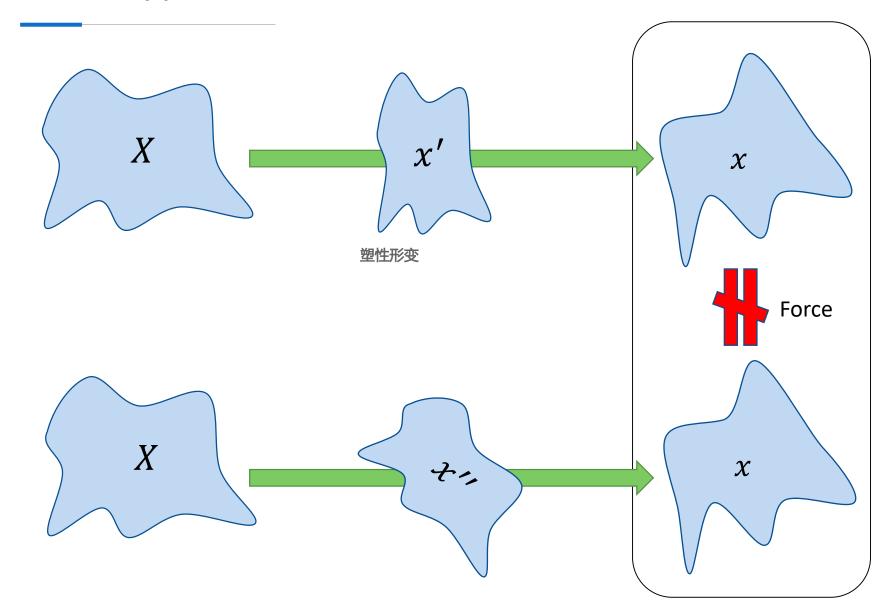
$$x = \varphi(X) = SX$$

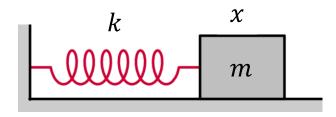
$$F = S$$

Hyperelasticity



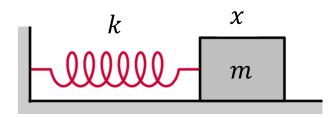
Not Hyperelastic?





$$f = -k(x - x_0)$$

$$E = \frac{1}{2}k(x - x_0)^2$$



$$f = -k(x - x_0)$$

$$E = \frac{1}{2}k(x - x_0)^2$$

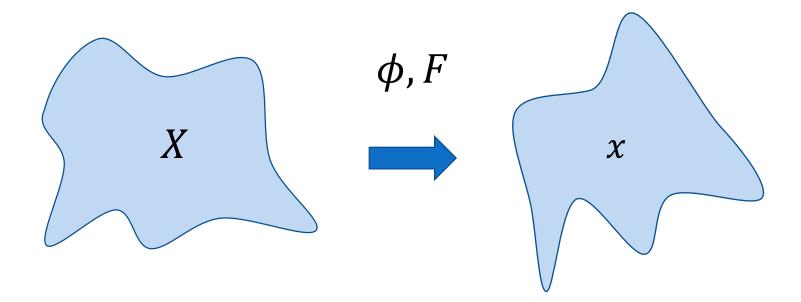
$$f = -\frac{aE}{dx}$$

$$f(x) = -\nabla_{\mathbf{X}} E(x)$$

$$E(x) = \int_{\Omega} \Psi(\phi; X) dX$$

拉格朗日视角, 在material视角做

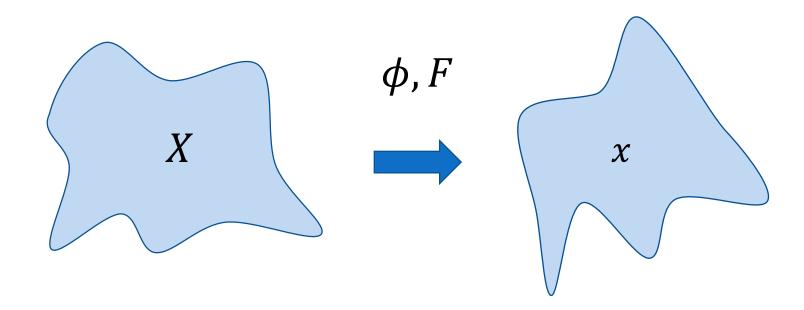
Energy Density



$$f(x) = -\nabla_{\mathbf{X}} E(x)$$

$$E(x) = \int_{\Omega} \Psi(F) dX$$

Energy Density

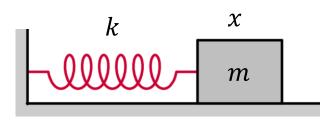


Energy Density

• What would a formula for $\Psi(F)$ look like?

$$\bullet \Psi(F) = \frac{k}{2} ||F||_F^2 ?$$

$$\bullet \Psi(F) = \frac{k}{2} ||F - I||_F^2$$



$$f = -k(x - x_0)$$
$$E = \frac{1}{2}k(x - x_0)^2$$

Stress

• A fundamental descriptor of force

- 1st Piola-Kirchhoff stress tensor
 - One of the variety of "stress" descriptors
 - Commonly used in graphics
 - For hyperelastic materials

$$P(F) = \frac{\partial \Psi(F)}{\partial F}$$

Strain

- $\epsilon(F)$: A measurement of severity of deformation
 - $\epsilon(I) = 0$ $\frac{\partial f}{\partial f} \frac{\partial f}{\partial g} \frac{\partial f}{\partial g}$
 - $\epsilon(RF) = \epsilon(F)$ for $\forall R \in SO(n)$
- Example strain tensors:
 - Green strain tensors:

$$\epsilon(F) = \frac{1}{2} (F^T F - I)$$

$$\epsilon(F) = \frac{1}{2} (\Sigma^2 V - I), \qquad F = U \Sigma V^T$$

• Small (infinitesimal) strain tensors:

$$\epsilon(F) = \frac{1}{2}(F + F^T) - I$$

Constitutive Model of Material

Relationship between

Force-quantities: Ψ, P, E

Kinematic-quantities F, ϵ, ϕ

Linear Elasticity

- Constitutive model:
 - Small (infinitesimal) strain tensors

$$\epsilon(F) = \frac{1}{2}(F + F^T) - I$$

Strain energy density

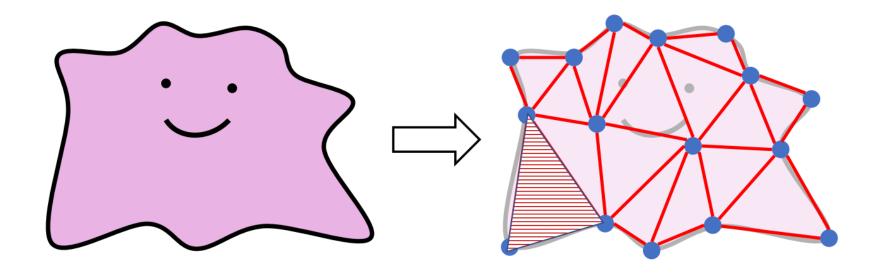
$$A:B=\operatorname{tr}(AB)$$

$$\Psi(F) = \mu \, \epsilon : \epsilon + \frac{\lambda}{2} \, \operatorname{tr}^{2}(\epsilon)$$

or

$$P = 2\mu \,\epsilon + \lambda \, \mathrm{tr}(\epsilon)$$

Discretization



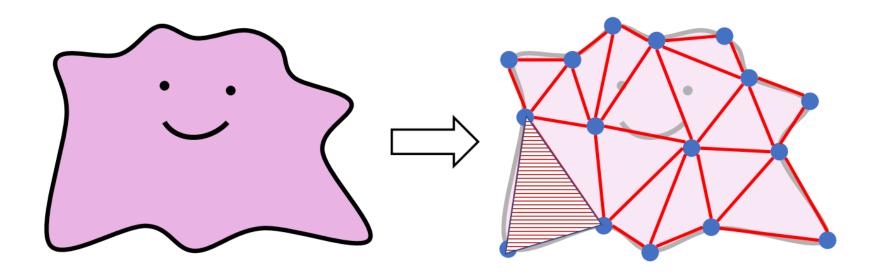
Energy

$$E(x) = \int_{\Omega} \Psi(F) dX$$



$$E(x) = \int_{\Omega} \Psi(F) dX$$

$$E(x) = \sum_{\Omega_i} \int_{\Omega_i} \Psi(F) dX$$

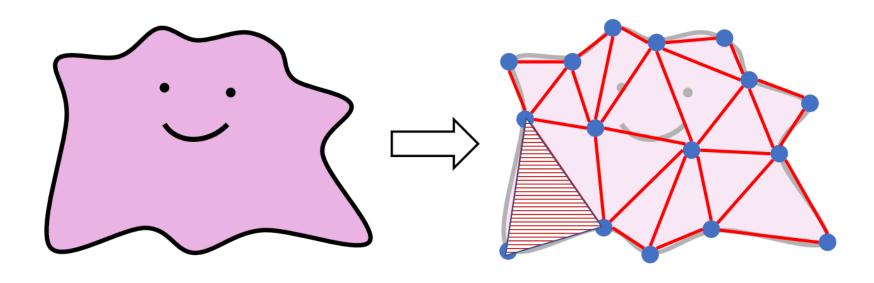


Energy

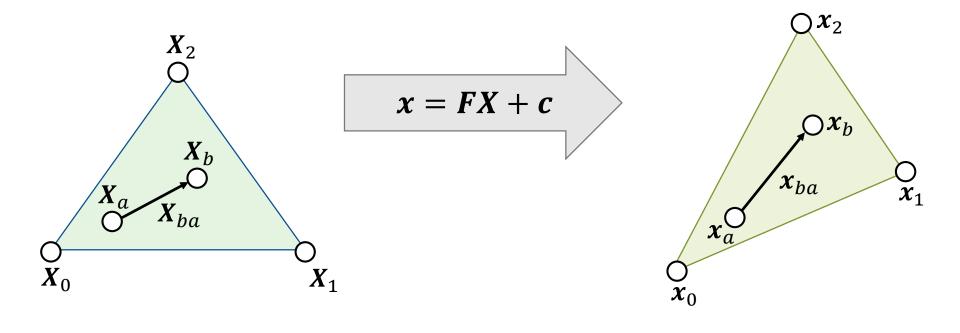
$$E(x) = \int_{\Omega} \Psi(F) dX$$



$$E(x) = \int_{\Omega} \Psi(F) dX \qquad \qquad E(x) = \sum_{\Omega_i} W_i \Psi(F_i)$$

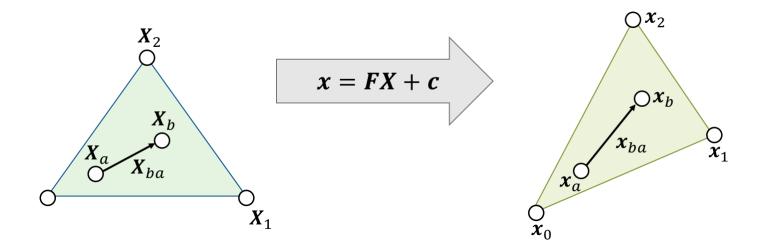


Linear Discretization



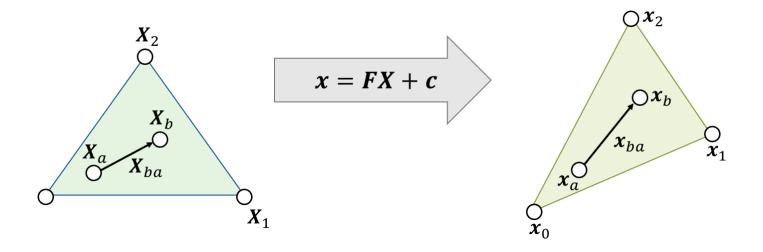
Reference Configuration Material Space **Deformed Configuration**

Linear Triangular Elements



$$[x_1 - x_0 \quad x_2 - x_0] = F[X_1 - X_0 \quad X_2 - X_0]$$

Linear Triangular Elements

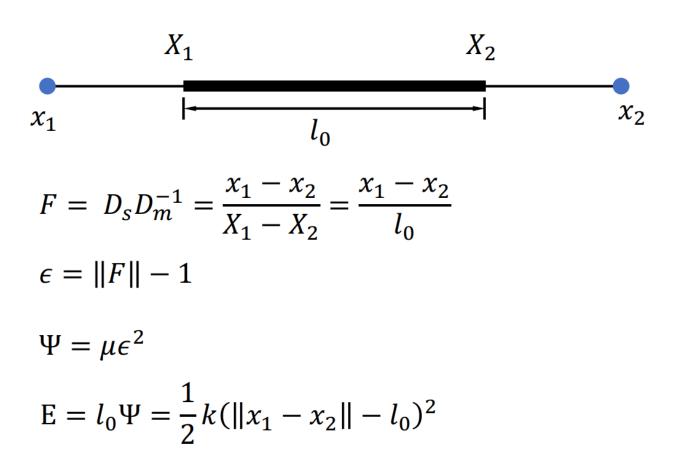


$$[x_1 - x_0 \quad x_2 - x_0] = F[X_1 - X_0 \quad X_2 - X_0]$$

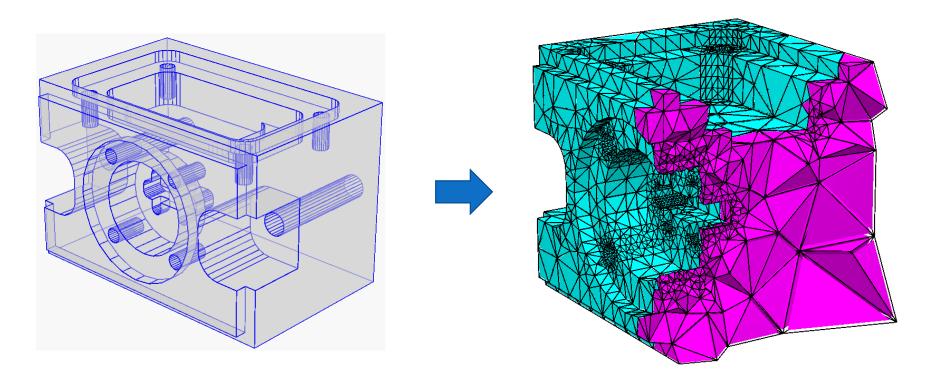


$$F = D_S D_m^{-1}$$

1D Example: spring

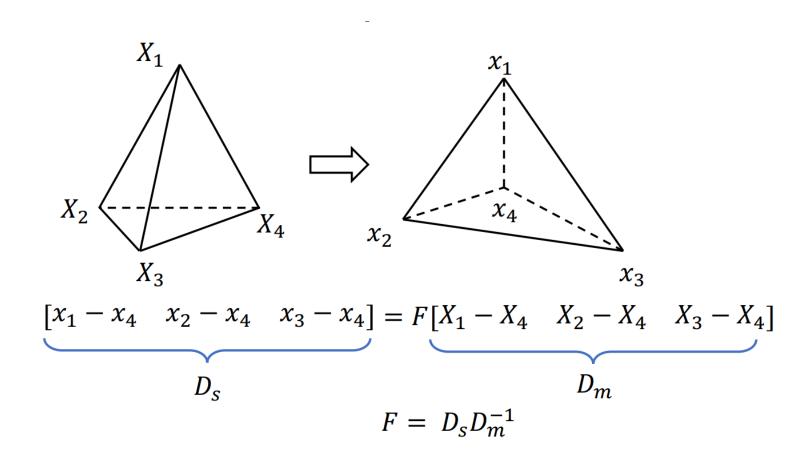


Tetrahedralization

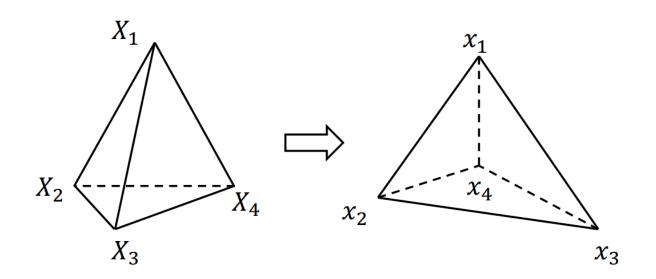


TETGEN: https://wias-berlin.de/software/tetgen/features.html

Linear Tetrahedral Elements



Force Discretization



$$\vec{f_i}(\mathbf{x}) = -\frac{\partial E(\mathbf{x})}{\partial \vec{x_i}}$$

$$\mathbf{H} = \begin{bmatrix} \vec{f}_1 & \vec{f}_2 & \vec{f}_3 \end{bmatrix} = -W\mathbf{P}(\mathbf{F})\mathbf{D}_m^{-T} \text{ and } \vec{f}_4 = -\vec{f}_1 - \vec{f}_2 - \vec{f}_3$$

Simulation of Deformable Solids

 $\vec{f}_1 += (-\vec{h}_1 - \vec{h}_2 - \vec{h}_3)$

16:

17:

end for

18: end procedure

```
Algorithm 1 Batch computation of elastic forces on a tetrahedral mesh
  1: procedure Precomputation(\mathbf{x}, \mathbf{B}_m[1 \dots M], W[1 \dots M])
             for each \mathcal{T}_e = (i, j, k, l) \in \mathcal{M} do \triangleright M is the number of tetrahedra
                                \begin{bmatrix} X_i - X_l & X_i - X_l & X_k - X_l \end{bmatrix}
                  \mathbf{D}_m \leftarrow \left[ egin{array}{cccc} Y_i - Y_l & Y_j - Y_l & Y_k - Y_l \ Z_i - Z_l & Z_j - Z_l & Z_k - Z_l \end{array} 
ight]
 3:
        \mathbf{B}_m[e] \leftarrow \mathbf{D}_m^{-1}
          W[e] \leftarrow \frac{1}{6} \det(\mathbf{D}_m)
                                                                                      \triangleright W is the undeformed volume of \mathcal{T}_e
             end for
  7: end procedure
  8: procedure ComputeElasticForces(\mathbf{x}, \mathbf{f}, \mathcal{M}, \mathbf{B}_m[], W[])
             \mathbf{f} \leftarrow \mathbf{0}
                                                                                                            \triangleright \mathcal{M} is a tetrahedral mesh
  9:
             for each \mathcal{T}_e = (i, j, k, l) \in \mathcal{M} do
10:
                  \mathbf{D}_{s} \leftarrow \begin{bmatrix} x_{i} - x_{l} & x_{j} - x_{l} & x_{k} - x_{l} \\ y_{i} - y_{l} & y_{j} - y_{l} & y_{k} - y_{l} \\ z_{i} - z_{l} & z_{j} - z_{l} & z_{k} - z_{l} \end{bmatrix}
11:
           \mathbf{F} \leftarrow \mathbf{D}_{s} \mathbf{B}_{m}[e]
12:
        \mathbf{P} \leftarrow \mathbf{P}(\mathbf{F})
                                                                                                          > From the constitutive law
13:
14: \mathbf{H} \leftarrow -W[e]\mathbf{P} \left(\mathbf{B}_m[e]\right)^T
        \vec{f_i} += \vec{h_1}, \ \vec{f_i} += \vec{h_2}, \ \vec{f_k} += \vec{h_3}
                                                                                                                             \triangleright \mathbf{H} = \left[ \vec{h}_1 \ \vec{h}_2 \ \vec{h}_3 \right]
```