

# VMC

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**Abstract**

*Author's comments:* .

# 1 Introduction

Want to evaluate ground-state energy of a Bose gas. The system is described by a Hamiltonian  $H$ . If we knew the wave function which corresponds to the ground-state energy, this would be a straight forward matter of simply applying the Hamiltonian to said wave function. However, since the exact wave function is not known, I use a trial wave function with adjustable parameters together with the so called Variational Monte Carlo method in order to zero in on the right ground-state energy. Alternatively, one could solve the Schrödinger equation for the system,

For et system av  $N$  partikler beskrevet av  $H$ , ønsker vi å finne den laveste energien systemet kan ha. Den mest direkte måten å gjøre dette på er å Schrödinger-ligningen for systemet. (Dette krever vel en bølgefunksjon, og det har vi ikke ?) - altså sannsynlighetsfordelingen til partiklene i Bose-gassen. Since we do not

Single particle-funksjon som er laveste tilstanden for en harmonisk oscillator.

For flere partikler om det er boson. Alle partiklene er i laveste singelpartikkel tilstand. Bytter vi rekkefølge på et system av Bosoner endres ikke bølgefunksjonen. Bytter vi partikler for ferminioer endres fortegnet.

Skal finne laveste egenpar. Tilhørende en hamilton for en type partikkeltype. Ikke mulig å løse for Schrödinger ligner for flere partikler og interaksjon. Bruker VMC.

finner ikke varians = 0, kan få lav med ulik alfa, men det betyr at bølgefunksjone ikke er fullstendig fysisk. Den er nære.

Spinn lik 0-system. Total bølgefunksjon symmetrisk. Identical particles. fermionivå zlater lese hamonisk oscillator

Pull fra Morten. Kan skru på O3 når jeg veit at koden kjører slik den skal.

In order to write this project paper and the code required to produce the results, I used a variety of tools, including: Python 3.7.5, NumPy [5], , as well as a number of books, web-pages and articles - of which most are listed under [references](#). All the code required to reproduce the results may be found on my [github page](#) .

Hard sphere Bose gas for various number of particles. Bose gas is a quantum mechanical phase of matter composed of bosons, which means that multiple particles may occupy the quantum state, in this case the ground state.

*The mean square vibrational amplitude of a single boson at  $T = 0K$  in the trap (1) is  $\langle x^2 \rangle = (\hbar/2m\omega_{ho})$  so that  $a_{ho} \equiv (\hbar/m\omega_{ho})^{\frac{1}{2}}$  defines the characteristic length of the trap.*

The aim is to evaluate the ground-state of the system;

$$E_0\Psi_o = H\Psi_o$$

However, for complex very hard blabla. first outline system, then lblab

## 2 Material and methods

### 2.1 System and physical quantities

The system consists of  $N$  bosons in an harmonic spherical (S) ( $\omega_{ho}^2 = \omega_z^2$ ) or elliptical (E) ( $\omega_{ho}^2 \neq \omega_z^2$ ) trap (1);

$$V_{ext}(\mathbf{r}) = \begin{cases} \frac{1}{2}m\omega_{ho}^2 r^2 & (S) \\ \frac{1}{2}m[\omega_{ho}^2(x^2 + y^2) + \omega_z^2 z^2] & (E) \end{cases} \quad (1)$$

, where  $\omega_{ho}$  and  $\omega_z$  are trap frequencies in the xy plane and z direction respectively. The Hamiltonian of the system is given by

$$H = \sum_i^N \left( \frac{-\hbar^2}{2m} \nabla_i^2 + V_{ext}(\mathbf{r}_i) \right) + \sum_{i < j}^N V_{int}(\mathbf{r}_i, \mathbf{r}_j), \quad (2)$$

where inter-boson interaction is given by the repulsive force prohibiting particles to come within a distance  $a$  of other particles;

$$V_{int}(|\mathbf{r}_i - \mathbf{r}_j|) = \begin{cases} \infty & |\mathbf{r}_i - \mathbf{r}_j| \leq a \\ 0 & |\mathbf{r}_i - \mathbf{r}_j| > a \end{cases} \quad (3)$$

In order to evaluate the ground-state energy trial wave function (TWF) is used (4), where  $\alpha$  and  $\beta$  are variational parameters used to tune the wave function towards ground-state (more under a the [section on VMC](#)).

$$\Psi_T(\mathbf{r}) = \Psi_T(\mathbf{r}_1, \mathbf{r}_2, \dots, \mathbf{r}_N, \alpha, \beta) = \left[ \prod_i g(\alpha, \beta, \mathbf{r}_i) \right] \left[ \prod_{j < k} f(a, |\mathbf{r}_j - \mathbf{r}_k|) \right], \quad (4)$$

Where

$$g(\alpha, \beta, \mathbf{r}_i) = \exp[-\alpha(x_i^2 + y_i^2 + \beta z_i^2)]. \quad (5)$$

is the non-interactive part of the wave function, and

$$f(a, |\mathbf{r}_i - \mathbf{r}_j|) = \begin{cases} 0 & |\mathbf{r}_i - \mathbf{r}_j| \leq a \\ (1 - \frac{a}{|\mathbf{r}_i - \mathbf{r}_j|}) & |\mathbf{r}_i - \mathbf{r}_j| > a. \end{cases} \quad (6)$$

the interactive part, which by definition renders the repulsive force unnecessary in modeling the system as any breach of the particle spacing  $a$  results in a wave function evaluation of zero.

## 2.2 Local energy and drift force

As previously mentioned, the aim is to evaluate the ground-state of the system. A crucial part of this is to evaluate the local energy (more on the application later), which is defined as

$$E_L(\mathbf{r}) = \frac{1}{\Psi_T(\mathbf{r})} H \Psi_T(\mathbf{r}). \quad (7)$$

The variational method which will be used to find the ground-state of the system involves calculating this quantity repeatedly. This means that every reduction of floating point operation (FLOP) involved in doing so leads to a significant speed up - which is why an analytical expression for the local energy is desirable. As will be discussed more under [importance sampling](#), the drift force of the particles are also needed;

$$F_i = \frac{2 \nabla \Psi_T}{\Psi_T} \quad (8)$$

### 2.2.1 Local energy and drift force: Non-interacting boson sphere

For a spherical harmonic oscillator with no interaction between particles,  $a = 0$  and  $\beta = 1$ , the TWF (4) reduces to;

$$\Psi_T(\mathbf{r}) = \left[ \prod_i g(\alpha, \beta, \mathbf{r}_i) \right] \quad (9)$$

Thus simplifying the expression for the calculation for the local energy (7) to;

$$E_L(\mathbf{r}) = \frac{1}{\prod_i g(\alpha, \beta, \mathbf{r}_i)} \sum_i^N \left( \frac{-\hbar^2}{2m} \nabla_i^2 + \frac{1}{2} m \omega_{ho}^2 r^2 \right) \left[ \prod_i g(\alpha, \beta, \mathbf{r}_i) \right]$$

which leads to (see [Appendix 1: Analytic local energy, non-interacting spherical](#)) the following expression when using natural units,  $\hbar = c = 1$ , and unity mass,  $m = 1$ ;

$$E_L(\mathbf{r}) = \alpha d N + \left( -2\alpha + \frac{1}{2} \omega_{ho}^2 \right) \sum_i^N r_i^2. \quad (10)$$

With drift force;

$$F_i = \frac{2\nabla \Psi_T}{\Psi_T} = -4\alpha \mathbf{r}_i \quad (11)$$

### 2.2.2 Local energy and drift force: interacting boson sphere

Concerning a general boson sphere, an analytic expression for the local energy of an elliptical trap with particle interaction,  $\beta \neq 1$  and  $a \neq 0$ , is required. In order to derive it, the TWF (4) is re-written. First, the non-interactive part;

$$g(\alpha, \beta, \mathbf{r}_i) = \exp \left[ -\alpha(x_i^2 + y_i^2 + \beta z_i^2) \right] = \phi(\mathbf{r}_i) = \phi_i.$$

Secondly, the interactive part;

$$\prod_{i < j} f(r_{ij}) = \exp \left( \sum_{i < j} u_{jk} \right) \quad (12)$$

Where  $u_{jk} = \ln f(r_{ij})$ , using the shorthand notation  $r_{ij} = |\mathbf{r}_i - \mathbf{r}_j|$ . Thus, the WTF (4) is expressed as;

$$\Psi_T(\mathbf{r}) = \left[ \prod_i \phi_i \right] \exp \left( \sum_{j < k} u_{jk} \right)$$

Which means that the local energy, using natural units and unity mass as before, (7) can be written as

$$E_L(\mathbf{r}) = \frac{1}{\left[ \prod_i \phi_i \right] \exp \left( \sum_{j < k} u_{jk} \right)} \sum_i^N \left( \frac{1}{2} \nabla_i^2 + \frac{1}{2} \omega_{ho}^2 r^2 \right) \left[ \prod_i \phi_i \right] \exp \left( \sum_{j < k} u_{jk} \right) \quad (13)$$

where (see Appendix 1: Analytic local energy, interacting elliptical)

$$\begin{aligned} \frac{1}{\Psi_T(\mathbf{r})} \nabla_k^2 \Psi_T(\mathbf{r}) &= \frac{\nabla_k^2 \phi_k}{\phi_k} + 2 \frac{\nabla_k \phi_k}{\phi_k} \sum_{l \neq k} \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} u'_{kl} \\ &+ \sum_{j \neq k} \sum_{l \neq k} \frac{(\mathbf{r}_k - \mathbf{r}_l)(\mathbf{r}_k - \mathbf{r}_j)}{r_{kl} r_{kj}} u'_{kl} u'_{kj} \\ &+ \sum_{l \neq k} \left( u''_{kl} + \frac{2}{r_{kl}} u'_{kl} \right) \end{aligned} \quad (14)$$

Thus

$$E_L(\mathbf{r}) = \frac{1}{2} \sum_{k=1}^N \left( \frac{\nabla_k^2 \phi_k}{\phi_k} + 2 \frac{\nabla_k \phi_k}{\phi_k} \sum_{l \neq k} \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} u'_{kl} + \left( \sum_{j \neq k} \frac{(\mathbf{r}_k - \mathbf{r}_j)}{r_{kj}} u'_{kj} \right)^2 + \sum_{l \neq k} \left( u''_{kl} + \frac{2}{r_{kl}} u'_{kl} \right) + \omega_{ho}^2 r_k^2 \right) \quad (15)$$

This expression is calculated piecemeal in the implementation, using that

$$\begin{aligned} \frac{\nabla_k \phi_k}{\phi_k} &= -2\alpha(x_k \vec{e}_1 + y_k \vec{e}_2 + \beta z_k \vec{e}_3), \\ \frac{\nabla_k^2 \phi_k}{\phi_k} &= -2\alpha(d - 1 + \beta) + 4\alpha^2(x_k^2 + y_k^2 + \beta^2 z_k^2), \\ \frac{\partial u_{kl}}{\partial r_{kl}} &= \frac{a}{r_{kl}(r_{kl} - a)}, \\ \frac{\partial^2 u_{kl}}{\partial r_{kl}^2} &= \frac{a^2 - 2ar_{kl}}{r_{kl}^2(r_{kl} - a)^2} \end{aligned}$$

And drift force;

$$F_k = \frac{2\nabla \Psi_T}{\Psi_T} = 2 \left( \frac{\nabla_k \phi_k}{\phi_k} + \sum_{l \neq k} \nabla_k u_{kl} \right)$$

Where  $\nabla_k u_{kl} = \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} \frac{\partial u_{kl}}{\partial r_{kl}}$

## 2.3 variational principle and VMC

There are a multitude of methods available to circumnavigate having to directly solve the Schrödinger equation in order to find the eigenpair of the system we are looking for (CITE!). An important underlying principle for the methods employed in this project is the variational principle [2][p.256.];

$$E_0 \leq E[H] = \langle H \rangle = \langle \Psi | H | \Psi \rangle \quad (16)$$

This principle states that given a Hamiltonian,  $H$ , the ground-state energy,  $E_0$ , is upper bound by the expectation value  $\langle H \rangle$ , and holds for any normalized function  $\Psi$ . Thus, by using the Hamiltonian of the Bose gas, and trial wave function described earlier with variational parameters  $\alpha$ , it possible to hone in on the minimal value of  $\langle H \rangle$  and the desired ground-state energy,  $E_0$ , by solving the integral <sup>1</sup>;

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<sup>1</sup>Since  $\Psi_T$  is not normalized, but normalizable, the favefunction  $\frac{\Psi_T(\mathbf{r})}{\sqrt{\int d\mathbf{r} \Psi_T^*(\mathbf{r}) \Psi_T(\mathbf{r})}}$ , is normalized

$$E[H, \alpha] = \langle H \rangle = \frac{\int d\mathbf{r} \Psi_T^*(\mathbf{r}, \alpha) H(\mathbf{r}) \Psi_T(\mathbf{r}, \alpha)}{\int d\mathbf{r} \Psi_T^*(\mathbf{r}, \alpha) \Psi_T(\mathbf{r}, \alpha)}. \quad (17)$$

*Direct dependence on  $\alpha$  is omitted from the rest of this paper, but is included here to show that the energy also depends on the variational parameters.*

Instead of solving this multi-dimensional integral analytically, which for anything than a single particle becomes complicated, if not impossible, I've used Monte Carlo integration. Monte Carlo integration [3][Ch. 3] is a stochastic method aimed at evaluating a deterministic, high dimensional, integral  $I_M$ . This involves drawing a sequence of  $i = 1, \dots, M$  random events with a probability  $P_i$ , multiplying each event by its probability, and taking the average - which will converge to  $I_M$ . The following shows this method applied to evaluating the ground-state in question;

$$E[H] = \int P(\mathbf{r}) E_L(\mathbf{r}) \approx \frac{1}{M} \sum_{i=1}^M P(\mathbf{r}_i) E_L(\mathbf{r}_i) \quad (18)$$

, where  $E_L(\mathbf{r}_i)$  (7) is the local energy of the system in configuration  $\mathbf{r}_i$ , and  $P(\mathbf{r}_i)$  the probability of that local energy.

$$P(\mathbf{r}) = \frac{|\Psi_T(\mathbf{r})|^2}{\int |\Psi_T(\mathbf{r})|^2 d\mathbf{r}} \quad (19)$$

### 2.3.1 Metropolis algorithm

The Metropolis algorithm [3][p.86-88] is a highly adaptable method which generates a sequence of random samples from a probability distribution. The method makes iterative changes to a single degree of freedom and either accepts or rejects each change. By using the relative probability between samples, the method does not rely on directly sampling from a probability distribution, making the methods well suited for problems which involve complex probability distributions. The probability of the system being in state  $i$  at time  $t + \epsilon$  can be expressed through the probabilities of all states at time  $t$ ;  $P_i(t + \epsilon) = \sum_j w(j \rightarrow i) P_j(t)$ , where  $w(j \rightarrow i)$  is the transition probability from  $j$  to  $i$ . (19) can be used to find the probability density, but the transition probabilities are unknown. These probabilities can be expressed as  $w(j \rightarrow i) = A(j \rightarrow i) T(j \rightarrow i)$ , where  $T$  is the likelihood of making a transition, and  $A$  the likelihood of that transition being accepted. The Metropolis algorithm works by initializing the system in a certain state, then using a random walker to suggest new states. By assuming  $T(j \rightarrow i) = T(i \rightarrow j)$ , or what is known as detailed balance [3][p.86], one obtains;

$$\frac{P_i}{P_j} = \frac{W(j \rightarrow i)}{W(i \rightarrow j)} = \frac{A(j \rightarrow i) T(j \rightarrow i)}{A(i \rightarrow j) T(i \rightarrow j)} = \frac{A(j \rightarrow i)}{A(i \rightarrow j)}.$$

Using the probability ratio means that normalization is unnecessary, but more importantly this ratio also tells whether or not the random walker is moving into a region of high probability. Since the acceptance probability is unknown, brute force Metropolis uses  $A(j \rightarrow i) = \min(1, \frac{P_i}{P_j})$ . The adaptation of the algorithm used in this project reads as;

**Algorithm: Brute Force Metropolis**

1. Initialize algorithm
  - Set the number of Monte Carlo cycles,  $M$ , and step length,  $l$
  - Set variational parameters  $\alpha$
  - Set particle positions,  $\vec{r}$
  - Set energy  $E = E_L(\vec{r})$
2. Propose new configuration
  - Select random particle
  - Randomly move particle up to a threshold  $l$ . Store proposed particle position  $\vec{r}^*$
3. Evaluate proposal
  - Calculate  $w = \frac{P(\vec{r}^*)}{P(\vec{r})} = \frac{|\Psi_T(\vec{r}^*)|^2}{|\Psi_T(\vec{r})|^2}$
  - Generate a random number  $q$  between 0 and 1.
  - If  $w \geq q$ , accept proposal, calculate  $E_L$  and set  $E = E + E_L$ . Else, reject proposal.
4. If the number of cycles from step 2 to 4 is less than  $M$ , go to step 2. Else calculate  $\langle H \rangle = \frac{E}{M}$  and end simulation.

## 2.4 importance sampling

A problem with the brute force methodology described above is that one may end up with a lot of proposed configurations from regions of relatively lower probability, or in other words, wasted cycles. A strategy to combat this is

In order to not waste cycles on drawing too many samples that are not accepted, Don't want to draw samples from regions where the wave function is zero - these are wasted cycles. That means modeling transition probability,  $T$ , and not assuming  $T(i \rightarrow j) = T(j \rightarrow i)$ .  $T(i \rightarrow j)$  can be modeled in many ways. Instead of picking a step size and take random steps, we let the random walker propose states after a specific distribution. Has longer CPU time per cycle, but a lot high acceptance rate.

Fokker-Planck equation, which comes from fluid mechanics, which gives analytical solution for  $T$ , since numerical slows down program.  $T$  has time and spacial dependence. Standard diffusion equation

$$\frac{\partial T}{\partial t} = D\left(\frac{\partial^2}{\partial x^2} - F\right)T(x, t) \quad (20)$$

Fokker Planck comes from diffusion eq. (CITE derivation) The convergence to a stationary state, or equilibrium state, or most likely state at  $dT/dt = 0$ . So

$$\frac{\partial^2}{\partial x_i^2}T(x, t) = T\frac{\partial}{\partial x_i}F_i + F_i\frac{\partial}{\partial x_i}T \quad (21)$$

if we take  $\bar{a}ll F = g(x)\partial T/\partial x$  we get So

$$\frac{\partial^2}{\partial x_i^2}T(x, t) = T\frac{\partial g}{\partial x_i}\left(\frac{\partial T}{\partial x_i}\right)^2 + Tg\frac{\partial^2 T}{\partial x_i^2} + g\left(\frac{\partial T}{\partial x_i}\right)^2 \quad (22)$$



Which means that

$$g = \frac{1}{T} \quad (23)$$

So,  $F = \frac{1}{\Psi} \vec{\nabla} \Psi$

The solution to the Fokker-Planck equation using this  $F$  can be approximated by the Green's function;

$$T(x, y, t) = \frac{1}{4\pi D \Delta t} \exp\left(-\frac{(y - x - D \Delta t F(x))^2}{4 D \Delta t}\right) \quad (24)$$

) where  $\Delta t$  is a parameter

$$\text{Metropolis hastings } A(x \rightarrow y) = T(x \rightarrow y) = \frac{T(x \rightarrow y) \Psi_T(y)^2}{T(y \rightarrow x) |\Psi_T(x)|^2}$$

Instead of randomly moving the particle. The time evolution of the walker is described by the stochastic differential equation

$$\frac{\partial x(t)}{\partial t} = DF(x(t)) + \eta \quad (25)$$

where  $\eta$  is noise, which has the can be used to find the next position by euler's method;  $y = x + DF(x)\Delta t + \xi\sqrt{\Delta t}$

$$q = \frac{G(y, g, t) |\Psi_T(y)|^2}{G(x, y, t) |\Psi_T(x)|^2}$$

numerically;  $G/G$  can be shortened a lot. Precalc  $\exp(-y)$  etc.

computational aspects  $\Psi_t = \Psi_{OB} \Psi_C$  OB - one body - product of all the single particle wfs  
Jastrow factor - C for correlation /correlated part. For ratio in Metropolis test (without importance sampling): splitt opp ratio,  $|psi|^2/|psi| = psi_{ob}|^2\psi_c|^2..$

Variance used to determine how close (CITE) - if not it's impossible to tell how close we are. rather, need a method to determine how close we are.

By adjusting the parameters of the trial wave function described earlier, the variational principle

In order to evaluate the ground-state energy of the Bose gas without solving the The variational ground-state energy of a system which is described by the Hamiltonian  $H$  i

## 2.5 Error analysis

The ground-state energy of the system is estimated by the sample mean of the local energies over  $M$  cycles (or the fraction left after equilibration);

$$\bar{E} = \frac{1}{M} \sum^M E_L(\vec{r}_i) \quad (26)$$

This means that the error of the sample mean, or sample error (squared) (27), coincides with the estimation error of  $E_0$ ;

$$err_{\bar{E}}^2 = var(\bar{E}) = \frac{1}{M} \sum^M (E_L(\vec{r}_i) - \mu_{\bar{E}_L})^2, \quad (27)$$

where  $\mu_{\bar{E}_L}$  is the true mean of  $E_L$ . Assuming that the samples are independent of one another, then by the law of large numbers<sup>2</sup>, the difference between the sample mean and the true mean will decreases as the number of samples increase. For a sufficiently large number of Monte Carlo cycles, this would reduce the sample error arbitrarily close to zero, as long as  $\mu_{\bar{E}_L} = E_0$ , which depends on having chosen the correct variational parameters. Assuming that  $\bar{E} = \mu_{\bar{E}_L} = E_0$ , the error of the

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<sup>2</sup>  $\lim_{n \rightarrow \infty} \frac{1}{n} \sum_{i=1}^n x_i p(x_i) = \mu_x$

sample mean can be directly compared to the variance of the ground-energy; In general,  $H\Psi = E_0\Psi$  when  $\Psi$  is the exact ground-state (the same holds for any eigenpair) of the system. This means that  $\langle H^n \rangle = \langle \Psi | H^n | \Psi \rangle = E^n$ , which also means that the exact wave function has variance of zero;

$$\text{var}(E) = \langle H^2 \rangle - \langle H \rangle^2 = E^2 - (E)^2 = 0 \quad (28)$$

In other words, the sample error should be (machine precision) equal to the energy variance, which is zero, if the variational parameters are correct and the number of cycles sufficiently large. If the paramters are not correct, then the closer the parameters are to the correct values, the smaller the sample error. The magnitude of this sample error however, will only be correct if the assumption of independent samples holds, which it in this case does not.

### 2.5.1 Error estimate of correlated energy samples; the "blocking" method

An particular system configuration is directly dependent on the previous configuration of the system through the use of a random walker. Because of this, the associated energy samples are correlated. Currently, the error estimate (27) does not reflect this correlation, which means that the error estimate will be less accurate. In order to remedy this, I have chosen to use the "blocking" or "bunching" meothd [1], which benefits from being more accurate the larger the sample size, unlike for example bootstrapping.

As the series of energy samples from the VMC is ordered as a function of time, it is a time series of finite length. In general, a time series of  $n$  samples can be used to form an  $n$ -vector or  $n$ -tuple,  $\vec{X}$ , where  $(X_i)$  denotes the  $i$ 'th sample in the series. In order to estimate the variance of the sample mean,  $\text{var}(\vec{X})$ , by use of the "blocking" method, the time series is divided into blocks of increasing size. By combining these transformations with theorems on strictly stationary time series an automated "blocking" method (explained in detail in [4]) may be applied to the VMC sample series. Pivotal for this method is the distribution of the quantity  $M$  (32), which depends on a small number different statistical quantities from the transformed series. Using this, the automated "blocking" method may be applied to the VMC sample series. Below is a brief outline of the automated "blocking" method.

Starting with one block per sample, followed by two samples per block and so on, the sample variance,  $\hat{\sigma}^2$  is calculated. As these blocks increase in size,  $\hat{\sigma}^2$  of the time series gradually unravels from the sample covariance. From  $\mathbf{X}_0 = \mathbf{X}$ , the subsequent "blocking" transformation,  $\mathbf{X}_0 \rightarrow \mathbf{X}_1$ , produces a new time series  $\mathbf{X}_1$  with length  $n_1 = n/2$ <sup>3</sup>. The subsequent "blocking" number  $k$ , continues in the same fashion, where each transformation is achieved through

$$(X_i)_k = \frac{1}{2}(X_{2i-1})_{k-1} + (X_{2i})_{k-1} \quad (29)$$

for  $i = 1, \dots, n_k$ , where  $n_k$  is the length of the  $\mathbf{X}_k$ . These transformations are carried out until only one block remains.

The estimate for the variance of the sample mean can be expressed as  $\text{var}(\vec{X}) = \frac{\sigma_k}{n_k} + \epsilon_k$ , where  $\epsilon_k$  is the truncation error, which after a certain number of transformations is expected to become constant. Finding the lowest  $k$ , such that  $\epsilon_k = \epsilon_{k+1}$  is the goal of the last step. By calculating  $M$  (32), where  $d$  comes from  $n = 2^d$ , the smallest  $k$  such that  $M_k \leq q_{d-k}(1 - \alpha)$  gives which  $k$  to use when calculating  $\hat{v}ar(\vec{x}) = \sigma_k^2/n_k$  to use as an estimate for the sample mean<sup>4</sup>, with confidence interval  $(1 - \alpha)$ . Because  $M$  requires both  $\sigma_k$ , and  $\gamma_k(1)$ , these quantities should be calculated after each transformation.

<sup>3</sup>In the case where a time series is not divisible by two, a random sample is omitted.

<sup>4</sup> $q_{d-k}(1 - \alpha)$  may be found in a table for the  $\chi$  distribution.

$$\hat{\gamma}(h) = \frac{1}{n} \sum_{i=1}^{n-h} (X_i - \bar{X})(X_{i+h} - \bar{X}) \quad (30)$$

which is a measure of the  $h$ -order ( $h = |i - j|$ ) covariance of a time series series with length  $n$ .

$$\hat{\gamma}_k = \frac{1}{4} \quad (31)$$

$$M_j = \sum_{k=j}^{d-1} \frac{n_k [(n_k - 1)\hat{\sigma}_k^2 / (n_k^2) + \hat{\gamma}_k(1)]^2}{\sigma_k^4} \quad (32)$$

When tailored to finding an estimate for the variance of  $\bar{E}_L$ , from the VMC calculations, the automatic "blocking" algorithm reads as;

**Algorithm: The automated "blocking" method**

1. Initialize algorithm
  - Set  $\alpha$
  - Estimate  $var(\bar{E})$
  - Set  $i = 0$
2. Iterative "blocking" while size of  $E_{i+1} \geq 2$ :
  - If  $n_i \% 2 \neq 0$ , remove a random energy sample from  $E_i$
  - Compute  $\hat{\sigma}_i^2, \hat{\gamma}_i(1)$
  - Transform data  $\vec{E}_i \rightarrow \vec{E}_{i+1}$ , and set  $i = i + 1$
3. Calculate final values
  - Compute  $M_j$  from  $\hat{\sigma}_j^2, \hat{\gamma}_j(i)$
  - Find smallest  $k$  such that  $M_k \leq q_{d-k}(1 - \alpha)$
  - Calculate  $\hat{var}(\bar{E}) = \hat{\sigma}_k^2 / n_k$

where  $E_i$  is the time series of energy samples after a number of  $i$  "blocking" transformations.

kalle både estimated energy og energy heter begge E. Problem? sjekk at det ene er bar E!

Linke var med covar -> link med autocorr, juster uttrykk for sigma -> trenger autocorr tid -> estimate av autocorr time med blocking -> mer nøyaktig feil esimat.

kommenter at det kan være smart å regne på deltaer i stdet for fuelle funksjonseval. v tilstand.

blocking is a lot faster than bootstrap

## 2.6 Steepest descent

## 2.7 onebody

Høgberget, Jørgen duo uio

må sample kartesisk

lage bins. løpe over partiklene, tell opp antall i hver

### 3 Results

### 4 Conclusions

Repulsive force trengs ikke pga wavefunc =0, men kan ende opp med å kaste bort en hel haug av mc cycles?

min  $E[H]$  på *alpha* Noe av MC skal være expectation legg til varianse anzatz is  $\exp(\dots)$ . Noramlization not required., as it sdissapears in the metropolis step.

### References

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## Appendices

### Appendix 1.

#### Analytic local energy, non-interacting spherical

Gradient of  $g$ :

$$\nabla_i g(\alpha, \beta, \mathbf{r}_i) = -2\alpha \mathbf{r}_i g(\alpha, \beta, \mathbf{r}_i)$$

Laplacian of  $g$ : From the product rule, derivation of  $\mathbf{r}_i$ , gives a coefficient  $d$  representing the dimensionality of  $r$ .

$$\nabla_i^2 g(\alpha, \beta, \mathbf{r}_i) = (-2d\alpha + 4\alpha \mathbf{r}_i^2) g(\alpha, \beta, \mathbf{r}_i)$$

Meaning that

$$E_L(\mathbf{r}) = \sum_i^N \left( \frac{-\hbar^2}{2m} (-2d\alpha + 4\alpha \mathbf{r}_i^2) + \frac{1}{2} m \omega_{ho}^2 r_i^2 \right)$$

Using natural units,  $\hbar = c = 1$ , and unity mass  $m = 1$ , the equation becomes;

$$E_L(\mathbf{r}) = \alpha d N + \left( -2\alpha + \frac{1}{2} \omega_{ho}^2 \right) \sum_i^N r_i^2$$

And using the gradient of  $g$ , the drift force is

$$F_i = \frac{2\nabla \Psi_T}{\Psi_T} = -4\alpha \mathbf{r}_i$$

## Analytic local energy, interacting elliptical

Starting with

$$E_L(\mathbf{r}) = \frac{1}{[\prod_i \phi_i] \exp\left(\sum_{j<k} u_{jk}\right)} \sum_i^N \left( \frac{-\hbar^2}{2m} \nabla_i^2 + \frac{1}{2} m \omega_{ho}^2 r^2 \right) \left[ \prod_i \phi_i \right] \exp\left(\sum_{j<k} u_{jk}\right)$$

With the first goal being to calculate the term

$$\frac{1}{\Psi_T(\mathbf{r})} \sum_i^N \nabla_i^2 \Psi_T(\mathbf{r}),$$

starting by taking the gradient with respect to the  $k$ 'th particle;

$$\begin{aligned} \nabla_k \Psi_T(\mathbf{r}) &= \nabla_k \left( \left[ \prod_i \phi_i \right] \exp\left(\sum_{j<m} u_{jm}\right) \right) \\ &= \left( \nabla_k \left[ \prod_i \phi_i \right] \right) \exp\left(\sum_{j<m} u_{jm}\right) + \left[ \prod_i \phi_i \right] \left( \nabla_k \exp\left(\sum_{j<m} u_{jm}\right) \right) \end{aligned}$$

The gradient of the non-interacting part of the TW:

$$\nabla_k \left[ \prod_i \phi_i \right] = \nabla_k \phi_k \left[ \prod_{i \neq k} \phi_i \right] = \nabla_k \phi_k \frac{\prod_i g(\alpha, \beta, \mathbf{r}_i)}{\phi_k} \quad (33)$$

And the gradient of the interacting part, remembering that  $r_{kl} = r_{lk}$ ;

$$\nabla_k \exp\left(\sum_{j<m} u_{jm}\right) = \exp\left(\sum_{j<m} u_{jm}\right) \sum_{j \neq k} \nabla_k u_{kj} = \prod_{j<m} f(r_{jm}) \sum_{l \neq k} \nabla_k u_{kl} \quad (34)$$

Thus (39) is

$$\begin{aligned} \nabla_k \Psi_T(\mathbf{r}) &= \nabla_k \phi_k \left[ \prod_{i \neq k} \phi_i \right] \exp\left(\sum_{j<m} u_{jm}\right) \\ &\quad + \left[ \prod_i \phi_i \right] \exp\left(\sum_{j<m} u_{jm}\right) \sum_{l \neq k} \nabla_k u_{kl} \end{aligned} \quad (35)$$

or

$$\begin{aligned} \nabla_k \Psi_T(\mathbf{r}) &= \nabla_k \phi_k \frac{\prod_i g(\alpha, \beta, \mathbf{r}_i)}{\phi_k} \prod_{j<m} f(r_{jm}) \\ &\quad + \prod_i g(\alpha, \beta, \mathbf{r}_i) \prod_{j<m} f(r_{jm}) \sum_{l \neq k} \nabla_k u_{kl} \\ &= \left( \frac{\nabla_k \phi_k}{\phi_k} + \sum_{l \neq k} \nabla_k u_{kl} \right) \Psi_T(\mathbf{r}) \end{aligned} \quad (36)$$

Next, the above expressions are used to find the second derivative;

$$\begin{aligned}
\frac{1}{\Psi_T(\mathbf{r})} \nabla_k^2 \Psi_T(\mathbf{r}) &= \frac{1}{\Psi_T(\mathbf{r})} \nabla_k \left( \left( \frac{\nabla_k \phi_k}{\phi_k} + \sum_{l \neq k} \nabla_k u_{kl} \right) \Psi_T(\mathbf{r}) \right) \\
&= \frac{1}{\Psi_T(\mathbf{r})} \left( \left( \phi_k \nabla_k \frac{1}{\phi_k} + \frac{\nabla_k^2 \phi_k}{\phi_k} + \sum_{l \neq k} \nabla_k^2 u_{kl} \right) \Psi_T(\mathbf{r}) + \left( \frac{\nabla_k \phi_k}{\phi_k} + \sum_{l \neq k} \nabla_k u_{kl} \right)^2 \Psi_T(\mathbf{r}) \right) \\
&= \left( \frac{\nabla_k \phi_k}{\phi_k} \right)^2 + \frac{\nabla_k^2 \phi_k}{\phi_k} + \sum_{l \neq k} \nabla_k^2 u_{kl} + \left( \frac{\nabla_k \phi_k}{\phi_k} + \sum_{l \neq k} \nabla_k u_{kl} \right)^2 \\
&= - \left( \frac{\nabla_k \phi_k}{\phi_k} \right)^2 + \frac{\nabla_k^2 \phi_k}{\phi_k} + \sum_{l \neq k} \nabla_k^2 u_{kl} + \left( \frac{\nabla_k \phi_k}{\phi_k} \right)^2 + 2 \left( \frac{\nabla_k \phi_k}{\phi_k} \sum_{l \neq k} \nabla_k u_{kl} \right) + \left( \sum_{l \neq k} \nabla_k u_{kl} \right)^2 \\
&= \frac{\nabla_k^2 \phi_k}{\phi_k} + 2 \frac{\nabla_k \phi_k}{\phi_k} \sum_{l \neq k} \nabla_k u_{kl} + \sum_{l \neq k} \nabla_k^2 u_{kl} + \left( \sum_{l \neq k} \nabla_k u_{kl} \right)^2
\end{aligned} \tag{37}$$

In order to simplify applying the  $\nabla_k$ -operator to  $u_{kl}$ , the operator is re-written:

$$\nabla_k = \nabla_k \frac{\partial r_{kl}}{\partial r_{kl}} = \nabla_k \sqrt{(\mathbf{r}_k - \mathbf{r}_l)^2} \frac{\partial}{\partial r_{kl}} = \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} \frac{\partial}{\partial r_{kl}}$$

This re-written operator is then applied to the  $\nabla_k u_{kl}$  terms, such that

$$\nabla_k u_{kl} = \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} \frac{\partial u_{kl}}{\partial r_{kl}} = \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} u'_{kl}$$

And

$$\begin{aligned}
\nabla_k^2 u_{kl} &= \left( \nabla_k \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} \right) \partial u'_{kl} + \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} (\nabla_k u'_{kl}) \\
&= \left( \frac{\nabla_k (\mathbf{r}_k - \mathbf{r}_l)}{r_{kl}} \right) u'_{kl} + (\mathbf{r}_k - \mathbf{r}_l) \left( \nabla_k \frac{1}{r_{kl}} \right) u'_{kl} + \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} (\nabla_k u'_{kl}) \\
&= \frac{d}{r_{kl}} u'_{kl} - (\mathbf{r}_k - \mathbf{r}_l) \frac{(\mathbf{r}_k - \mathbf{r}_l)}{r_{kl}^3} u'_{kl} + \left( \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} \right)^2 u''_{kl} \\
&= \left( \frac{d}{r_{kl}} - \frac{(\mathbf{r}_k - \mathbf{r}_l)^2}{r_{kl}^3} \right) u'_{kl} + \left( \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} \right)^2 u''_{kl}
\end{aligned}$$

Where  $(\mathbf{r}_k - \mathbf{r}_l)^2 = r_{kl}^2$ , thus

$$\nabla_k^2 u_{kl} = \left( \frac{d}{r_{kl}} - \frac{1}{r_{kl}} \right) u'_{kl} + u''_{kl} = \frac{d-1}{r_{kl}} u'_{kl} + u''_{kl}$$

Applied to the Laplacian;

$$\begin{aligned}
\frac{1}{\Psi_T(\mathbf{r})} \nabla_k^2 \Psi_T(\mathbf{r}) &= \frac{\nabla_k^2 \phi_k}{\phi_k} + 2 \frac{\nabla_k \phi_k}{\phi_k} \sum_{l \neq k} \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} u'_{kl} \\
&+ \left( \sum_{l \neq k} \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} \partial u'_{kl} \right)^2 \\
&+ \sum_{l \neq k} \left( \frac{d-1}{r_{kl}} u'_{kl} + u''_{kl} \right)
\end{aligned} \tag{38}$$

Expanding the third term, re-arranging, and inserting  $d = 3$ ;

$$\begin{aligned}
\frac{1}{\Psi_T(\mathbf{r})} \nabla_k^2 \Psi_T(\mathbf{r}) &= \frac{\nabla_k^2 \phi_k}{\phi_k} + 2 \frac{\nabla_k \phi_k}{\phi_k} \sum_{l \neq k} \frac{\mathbf{r}_k - \mathbf{r}_l}{r_{kl}} u'_{kl} \\
&+ \sum_{j \neq k} \sum_{l \neq k} \frac{(\mathbf{r}_k - \mathbf{r}_l)(\mathbf{r}_k - \mathbf{r}_j)}{r_{kl} r_{kj}} u'_{kl} u'_{kj} \\
&+ \sum_{l \neq k} \left( u''_{kl} + \frac{2}{r_{kl}} u'_{kl} \right)
\end{aligned} \tag{39}$$

For the drift Force; Using (42), the drift force of for particle  $k$  in the interacting system

$$F_k = \frac{2 \nabla \Psi_T}{\Psi_T} = 2 \left( \frac{\nabla_k \phi_k}{\phi_k} + \sum_{l \neq k} \nabla_k u_{kl} \right)$$