

LECTURE 5: Undamped Free Vibration & Intro to Forced Vibration

→ Systems w/ Viscous Damping ⇒ $c \neq 0$

$$m\ddot{u} + c\dot{u} + ku = 0 \quad (\text{EOM})$$

$$\ddot{u} + \left(\frac{c}{m}\right)\dot{u} + (\omega_n)^2 u = 0$$

↑ natural frequency (undamped)

$$\text{define } \frac{c}{m} = 2\zeta\omega_n$$

↑ damping ratio

$\zeta < 1.0$ under-damped (oscillation)

$\zeta = 1.0$ critically damped

$\zeta > 1.0$ over damped

$$\ddot{u} + 2\zeta\omega_n\dot{u} + \omega_n^2 u = 0$$

$$\Rightarrow \text{Assume } u = e^{rt}$$

⇒ substituting in

$$(r^2 + 2\zeta\omega_n r + \omega_n^2) e^{rt} = 0$$

↑ this can't be zero.

$$r^2 + 2\zeta\omega_n r + \omega_n^2 = 0 \Leftarrow \text{characteristic equation}$$

$$r_{1,2} = \omega_n \left[-\zeta \pm \sqrt{\zeta^2 - 1} \right]$$

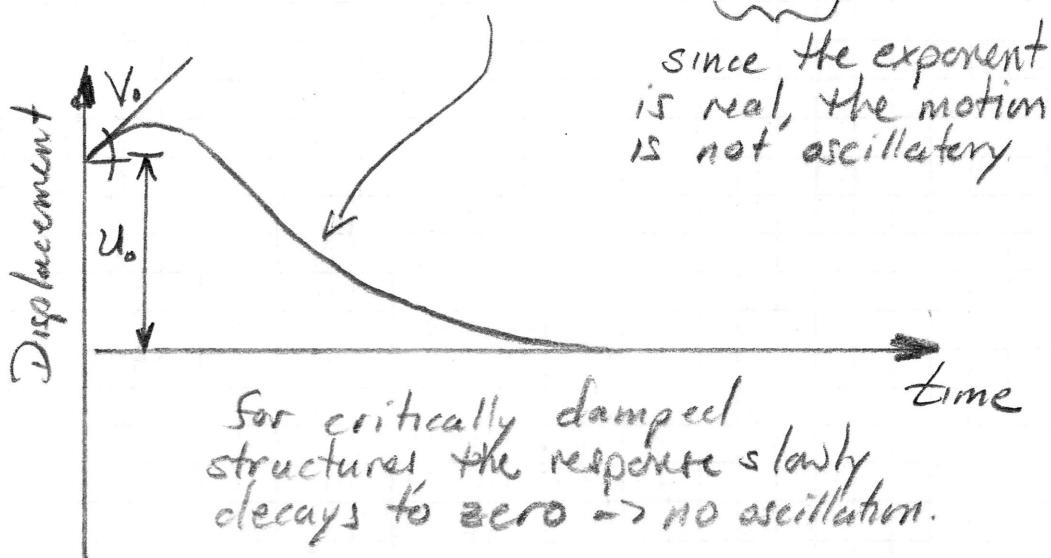
\Rightarrow Critically Damped Systems ($\zeta = 1.0$)

$$r_{1,2} = -\omega_n \quad (\text{repeated real roots})$$

$$u = (G_1 + G_2 t) e^{-\omega n t} \quad \begin{matrix} \downarrow \\ \text{solution} \end{matrix}$$

$\uparrow \quad \uparrow$
constants determined
by initial conditions

$$u = [u_0 + (v_0 + \omega_n u_0)t] e^{-\omega n t}$$



$$\text{recall } \frac{C}{m} = 2\zeta\omega_n$$

$$\text{for } \zeta = 1 \rightarrow C = C_{cr}$$

\uparrow critical damping

$$\Rightarrow C_{cr} = 2m\omega_n$$

\Rightarrow Underdamped Systems ($\zeta < 1.0$)

$$\tau_{1,2} = \omega_n \left[-\zeta \pm \sqrt{\zeta^2 - 1} \right]$$

this is negative for $\zeta < 1.0$

$$\tau_{1,2} = -\omega_n \zeta \pm i \omega_n \sqrt{1 - \zeta^2}$$

↑ imaginary number $= \sqrt{-1}$

\Rightarrow imaginary roots \Rightarrow oscillations

$$u = e^{-\omega_n \zeta t} (G_1 e^{i \omega_d t} + G_2 e^{-i \omega_d t})$$

$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$

Alternative
(and more intuitive)
form \Rightarrow de Moivre's theorem gives

$$\rightarrow u = e^{-\omega_n \zeta t} (A \cos(\omega_d t) + B \sin(\omega_d t))$$

\Rightarrow solve for A & B using initial cond
gives...

$$\Rightarrow u = e^{-\omega_n \zeta t} \left(u_0 \cos(\omega_d t) + \left(\frac{v_0 + \omega_n \zeta u_0}{\omega_d} \right) \sin(\omega_d t) \right)$$

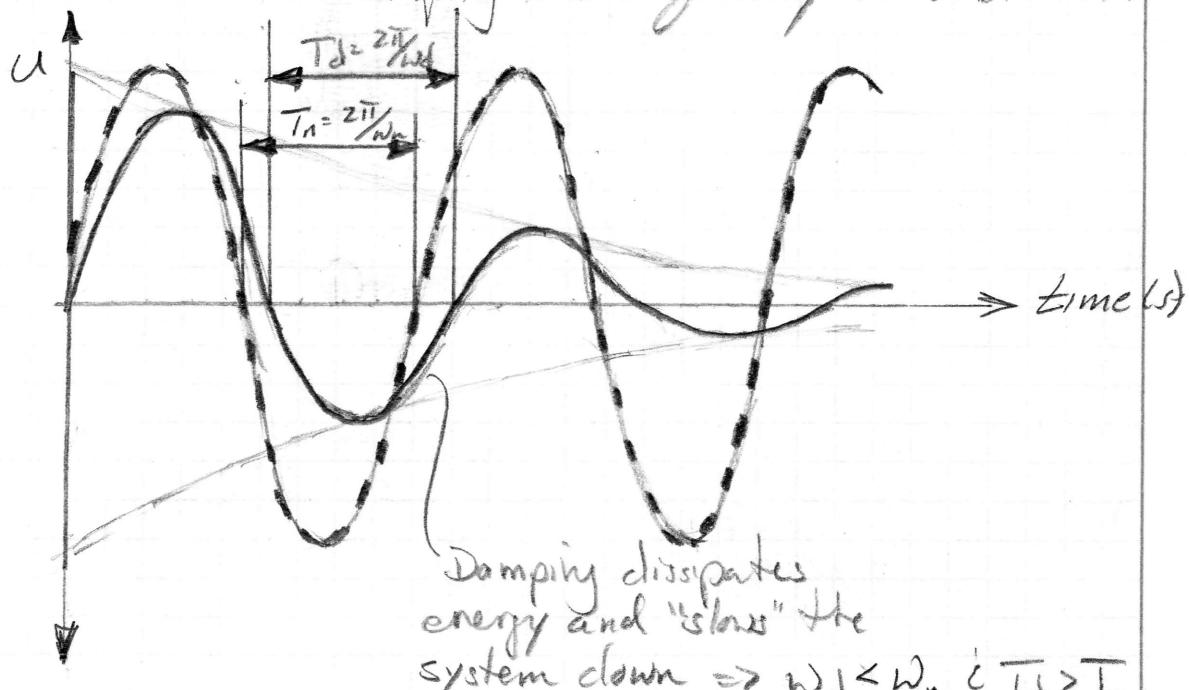
or

$$\Rightarrow u = g e^{-\omega_n \zeta t} \sin(\omega_d t + \phi)$$

$$g = \sqrt{u_0^2 + \left(\frac{v_0 + \omega_n \zeta u_0}{\omega_d} \right)^2}$$

$$\phi = \tan^{-1} \left(\frac{u_0 \omega_d}{v_0 + u_0 \omega_n \zeta} \right)$$

→ Effect of Damping on Frequency of Vibration



$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$

ζ	ω_n (rad/s)	ω_d (rad/s)	% diff
0.01	50	49.998	0.005
0.02	50	49.990	0.020
Most common assumption	0.05	49.937	0.125
0.10	50	49.749	0.504
Upper bound	0.15	49.434	1.144

↳ structure → rubble.

→ Phase - Plane Diagram for Damped System

$$u = g e^{-\omega_n \zeta t} \sin(\omega_d t + \phi)$$

$$\dot{u} = \frac{du}{dt} = \underbrace{-\omega_n \zeta g e^{-\omega_n \zeta t} \sin(\omega_d t + \phi)}_{\text{velocity has two terms}} + \omega_d g e^{-\omega_n \zeta t} \cos(\omega_d t + \phi)$$

- Problem #1 since the amplitude is a function of ζ , the velocity has two terms.

- Simplification #1 ⇒ For small ζ ($\sim 5\%$), neglect the first term.

$$\dot{u} \approx \omega_d g e^{-\omega_n \zeta t} \cos(\omega_d t + \phi)$$

- Problem #2 ⇒ this expression doesn't satisfy the initial velocity.

$$\left. \dot{u} \right|_{t=0} \neq v_0$$

- Simplification #2 ⇒ for small ζ ($\sim 5\%$), define g, ζ, ϕ as if the system is undamped.

$$g = \sqrt{(u_0)^2 + \left(\frac{v_0}{\omega_d}\right)^2}$$

$$\phi = \tan^{-1}\left(\frac{u_0 \omega_d}{v_0}\right)$$

- Simplification #3 ⇒ for small ζ

$\omega_d \approx \omega_n$ ← just for convenience.

→ Using Excel, show...

- (1) When the simplifications cause large errors.
- (2) That the proper ξ & ϕ do not satisfy the initial cond. when the sin term is neglected (in $\ddot{\theta}$ eqn).
- (3) The spiral nature of the phase-plane diagram → i.e. a continual loss of energy.

→ If the damping is large, the phase-plane representation is too cumbersome and should not be used.

↳ use the direct θ & $\dot{\theta}$ expressions.

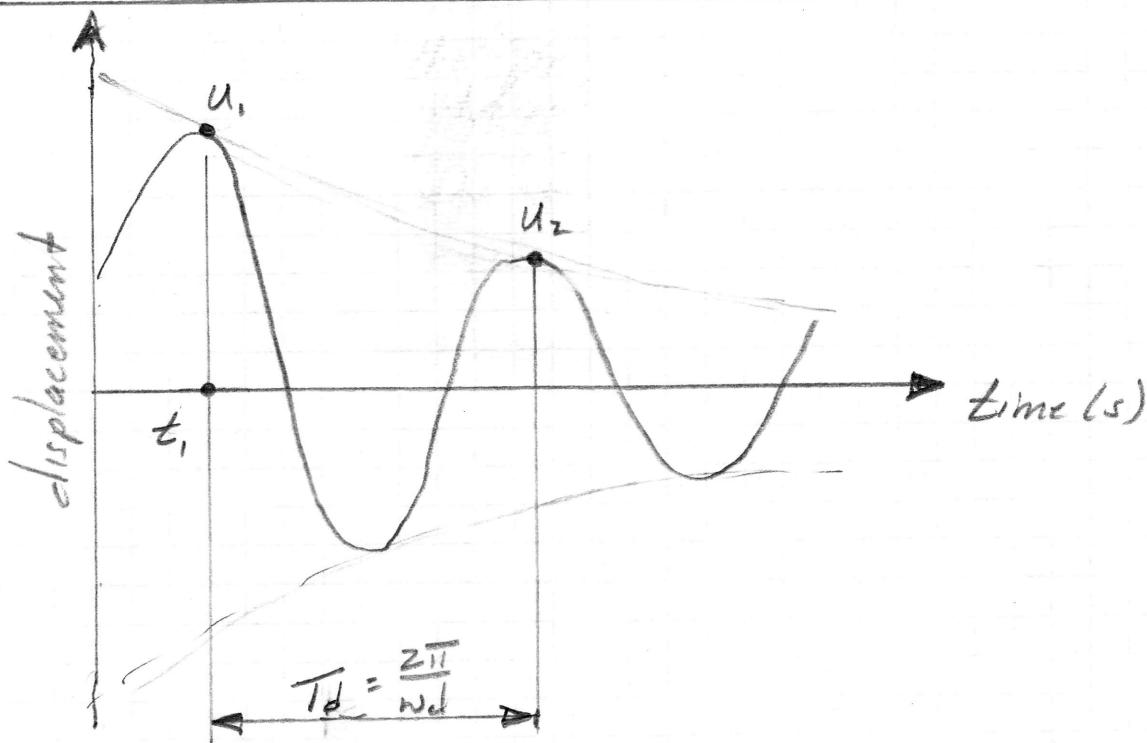
⇒ 'Log' Decrement

(1) Provides a physical understanding of the damp ratio ζ

(2) Provides an easy means to experimentally estimate damping

↳ this is important because it is very difficult to estimate damping 'in an a priori sense.'

→ key question → While it is obvious that an increase in ζ results in a faster 'decay' of vibrations, what is the exact relationships between ζ and vibration decay.



$$u_1 = u(t_1) = g e^{-\zeta \omega_n t_1} \sin(\omega_d t_1 + \phi)$$

causes 1 fm rotation

$$u_2 = u\left(t_1 + \frac{2\pi}{\omega_d}\right) = g e^{-\zeta \omega_n\left(t_1 + \frac{2\pi}{\omega_d}\right)} \sin\left(\omega_d\left(t_1 + \frac{2\pi}{\omega_d}\right) + \phi\right)$$

$$\sin(\omega_d t_1 + \phi)$$

$$\frac{u_1}{u_2} = \frac{g e^{-\zeta \omega_n t_1}}{g e^{-\zeta \omega_n\left(t_1 + \frac{2\pi}{\omega_d}\right)}}$$

$$\text{define log dec: } \delta = \ln \left[\frac{u_1}{u_2} \right] = \ln \left[\frac{e^{-\zeta \omega_n t_1}}{e^{-\zeta \omega_n\left(t_1 + \frac{2\pi}{\omega_d}\right)}} \right]$$

$$\delta = -\zeta \omega_n t_1 - \left(-\zeta \omega_n t_1 - \zeta \omega_n \frac{2\pi}{\omega_d} \right)$$

$$\delta = \frac{\zeta \omega_n 2\pi}{\omega_d} \leftarrow \delta \text{ is a constant!}$$

\Rightarrow for small $\zeta \Rightarrow \omega_n \approx \omega_d$

$$\delta = \zeta (2\pi) \text{ or } \zeta = \frac{\delta}{2\pi} *$$

⇒ From Excel...

$$u_1 = -8.479 \text{ in}$$

$$u_2 = -6.231 \text{ in}$$

$$\delta = \ln \left[\frac{-8.479}{-6.231} \right] = 0.3081$$

$$\zeta = \frac{0.3081}{2\pi} = 0.0490 \approx 0.05$$

↳ actual?

⇒ Example: Inverse problem

→ You are hired to test a cantilever structure w/ to determine its mass, damping, & stiffness properties.

→ You elect to perform an impact test using a device that imparts a impulse of 20 kips over a 0.01 sec duration.

→ Using disp sensors, you capture the resulting free vibration response.

⇒ Goal: Determine m , c , & k ...

⇒ Method 1: Model Updating.

⇒ Construct a model and modify m , c , k parameters until it matches the measured response.

⇒ Which parameters should we change?
why?

⇒ try to build a physical feel

⇒ Method 2: Analytical.

Step 1: Determine ζ

⇒ log slope

→ from Excel

$$\delta = \ln\left(\frac{U_1}{U_2}\right) = \ln\left(\frac{1.924''}{1.319''}\right) = 0.3775$$

$$\zeta = \frac{\delta}{2\pi} = \frac{0.3775}{2\pi}$$

$$\underline{\zeta = 0.0601 \sim 0.06}$$

Step 2: Determine 'm'

$$\Delta V = \frac{F at}{m} \quad \left. \begin{array}{l} \text{every thing is} \\ \text{known except 'm'} \end{array} \right\}$$

1st two measured points.

$$\Delta V = \frac{(0.2204 - 0)''}{0.005s} = 44.08 \text{ m/s.}$$

← time step.

This assumes no noise or other measurement error.

$$44.08 \text{ m/s} = \frac{(20,000/\text{b})(0.01\text{s})}{m}$$

$$\underline{\underline{m = 4537 \text{ lbm.} \sim 4.5}}$$

Step 3: Determine 'K'

$$\omega_d = \sqrt{1 - \zeta^2} \sqrt{\frac{k}{m}}$$

$$\omega_d = \frac{2\pi}{T_d}$$

from Excel.

from book

$$T_d = -0.15 + 0.44 = 0.29 \text{ sec.}$$

$$\omega_d = 21.67 \text{ rad/s.}$$

$$21.67 = \sqrt{1 - 0.06^2} \sqrt{\frac{k}{4.537}}$$

$$21.70 = \sqrt{\frac{k}{4.537}}$$

$$\underline{k = 2137 \text{ kip/in.} \neq 2000 \text{ kip/in.}}$$

→ Where did the error come from?

$$\Rightarrow \text{using } \zeta = 0.06 \text{ & } m = 4.5$$

$$k = 2102 \text{ kip/in}$$

↳ still 5% error.

⇒ Use more precise T_d estimate.

$$t_1 = 0.145 + 0.1584 \left(\frac{0.005}{0.1584 + 0.02618} \right) = 0.14929 \text{ sec}$$

$$t_2 = 0.445 + 0.07244 \left(\frac{0.005}{0.07244 + 0.05323} \right)$$

$$t_2 = 0.44787 \text{ sec.}$$

$$T_d = 0.44787 - 0.14929 = 0.29858 \text{ sec}$$

$$w_d = 21.044 \text{ rad/sec} \quad (\underline{2.98\%} \text{ diff from before})$$

$$w_n = 21.082 \text{ rad/sec}$$

why??

$$\kappa = 2000.025 \text{ tip/in} \quad (\underline{5.10\%} \text{ diff from before})$$

$\Rightarrow w_d$ is squared to solve for
 $\kappa' \Rightarrow$ all errors are magnified.

\Rightarrow Sample HW Problems.

\rightarrow Code the damped free vibration response of an SDOF in Excel and examine the accuracy of the simplified phase-plane representation.

\rightarrow What is an upper bound for ζ ?

\rightarrow Does any other parameter affect the accuracy?

\rightarrow Using the above coding try to solve the inverse problem using model updating and the analytical approach.

\rightarrow Which is more efficient?

\rightarrow Which is more realistic?

\rightarrow Why?