

# Advanced Bending and Torsion

## Shear Centre of Thin-Walled Sections

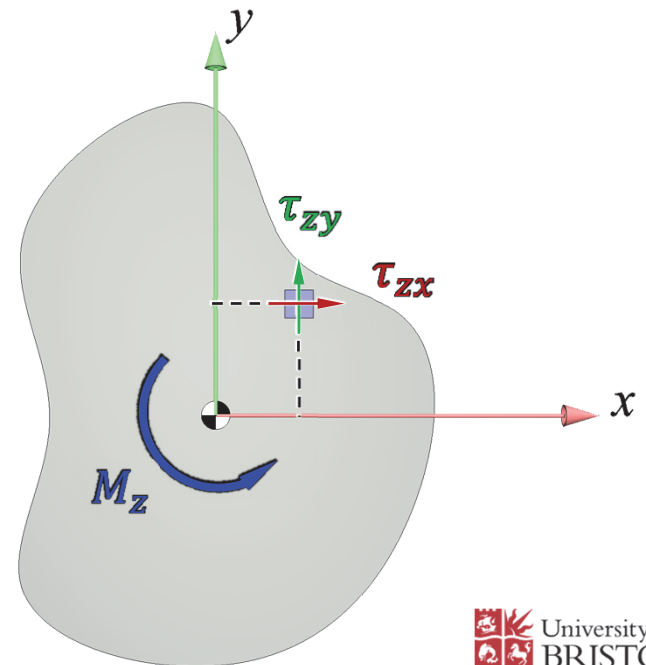
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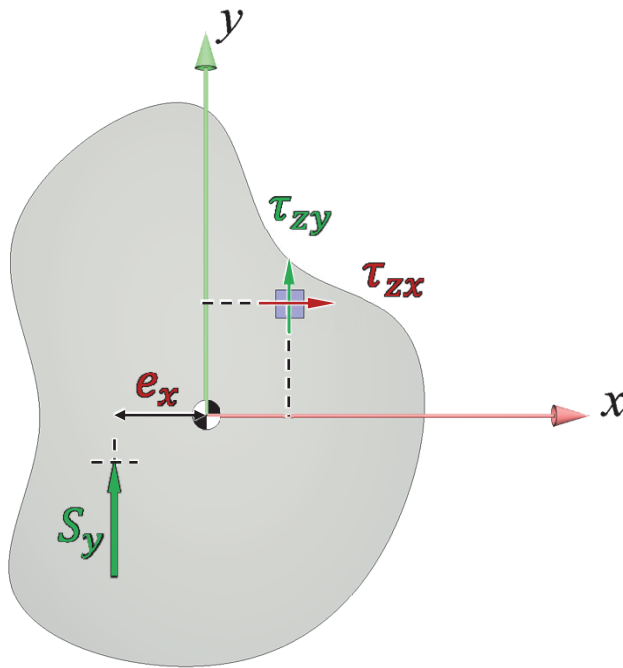
01 November 2018

- Is a point somewhere on the  $x$ - $y$  plane where transverse shear forces can be applied without causing torsion about the  $z$  axis
- A shear centre exists for any cross section, but we will focus only on **convex solid cross-sections** and **thin-walled cross sections**
- As a shear force is applied, shear stresses are generated along the cross-section which can be decomposed into  $\tau_{zx}$  and  $\tau_{zy}$
- These may generate a moment **about a reference point**
  - Important to choose a convenient one
- For a generic cross-section, taking the centroid as reference:

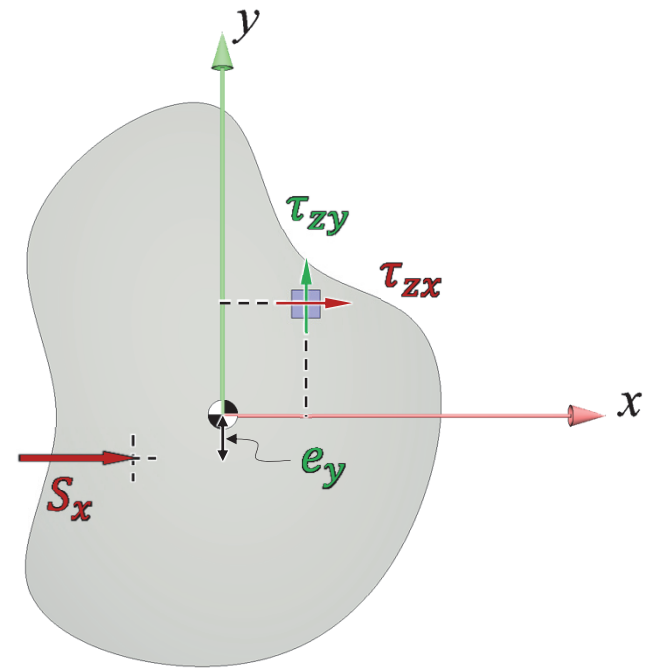
$$M_z = \int (x \tau_{zy} - y \tau_{zx}) dA$$



- To avoid twisting the beam about  $z$ , the shear force must generate a counterbalancing moment about  $z$
- This is done by offsetting the loading point perpendicularly to the loading direction:

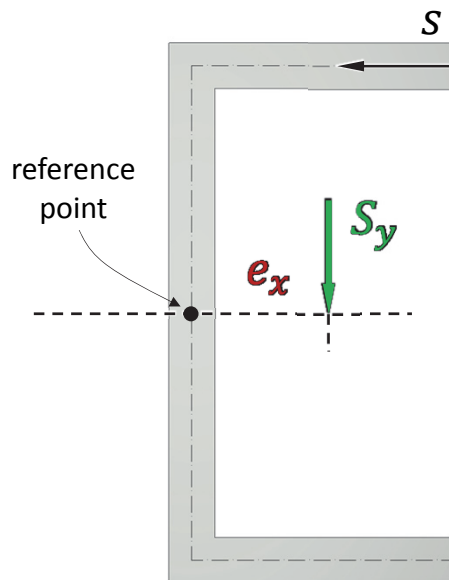


$$S_y e_x = \int (y \tau_{zx} - x \tau_{zy}) dA$$



$$S_x e_y = \int (y \tau_{zx} - x \tau_{zy}) dA$$

- For **convex solid sections** the shear centre **is the centroid**
  - Concave solid sections are outside of the scope of StM2
- For thin walled structures the shear centre can easily be found by ‘inspection’ or by equilibrium of moments
- Thin wall assumptions mean that shear stresses always follow the centreline
- Taking a channel section as example, an picking the origin of  $X, Y$  as reference:

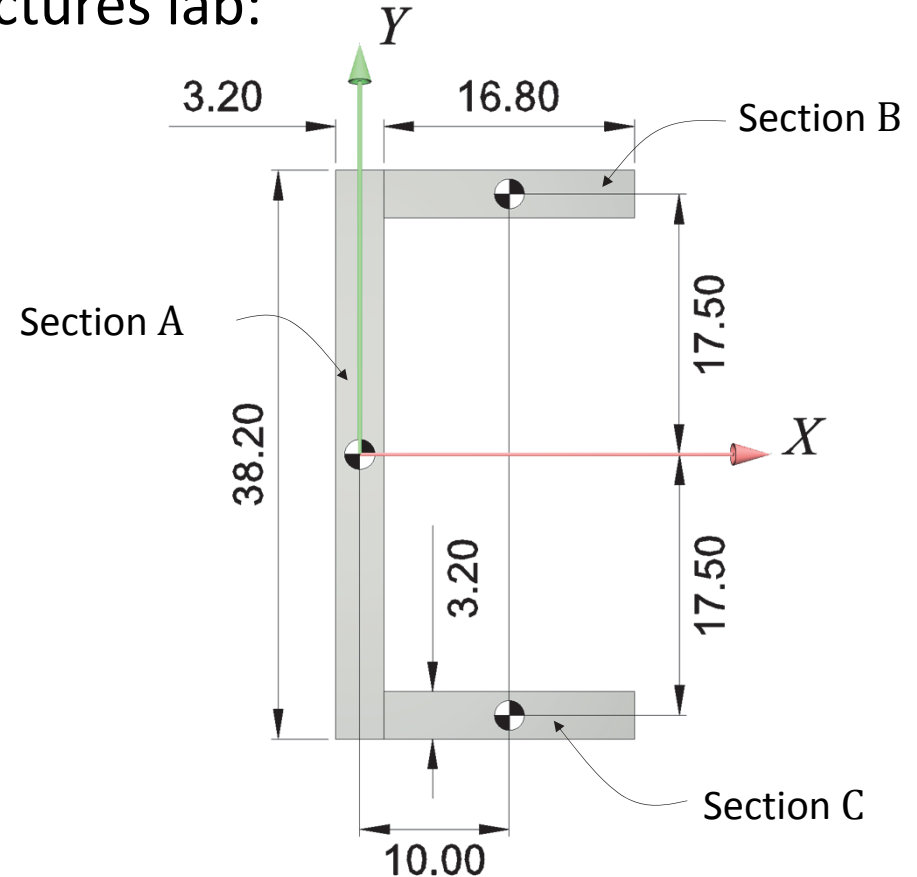
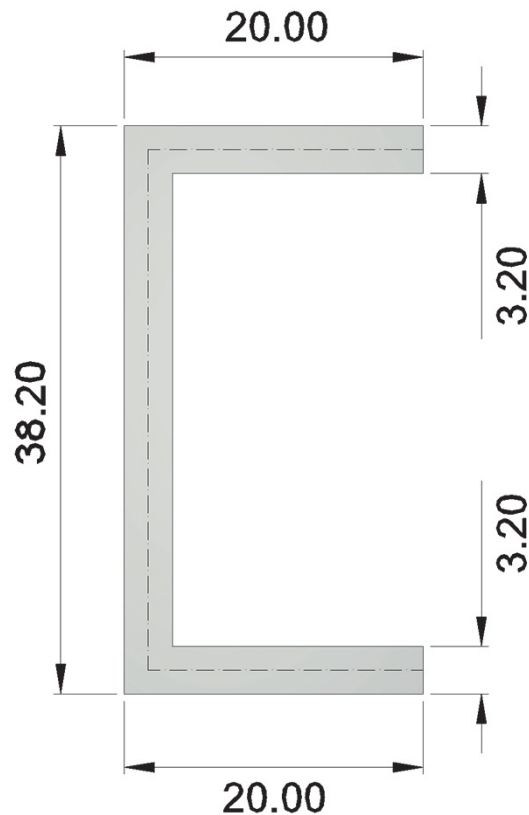


$$S_y e_x = \int (Y \tau_{zx} - X \tau_{zy}) dA$$

$$S_y e_x = \int (Y q_{s,x} - X q_{s,y}) ds$$

Where  $q_{s,x}$  and  $q_{s,y}$  are the components of  $q_s$  along the  $x$  and  $y$  coordinates, respectively, arising from the application of a shear force  $S_y$

- Channel section see in the Structures lab:



$$A_A = (3.2)(38.2) = 122.24 \text{ mm}^2$$

$$\bar{X}_A = 0$$

$$\bar{Y}_A = 0$$

$$A_B = (16.8)(3.2) = 53.76 \text{ mm}^2$$

$$\bar{X}_B = 10.0 \text{ mm}$$

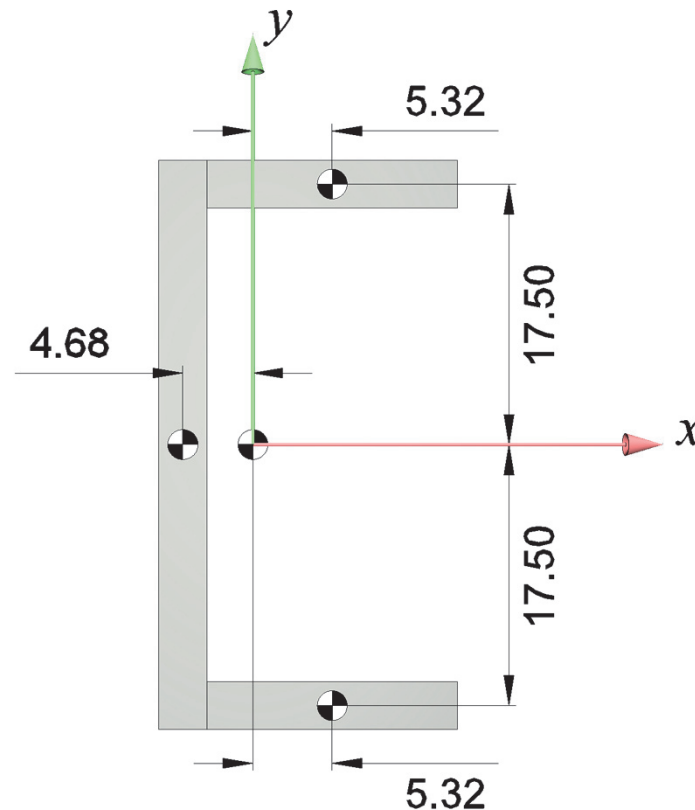
$$\bar{Y}_B = 17.5 \text{ mm}$$

- We can now find the centroid of the compound section:

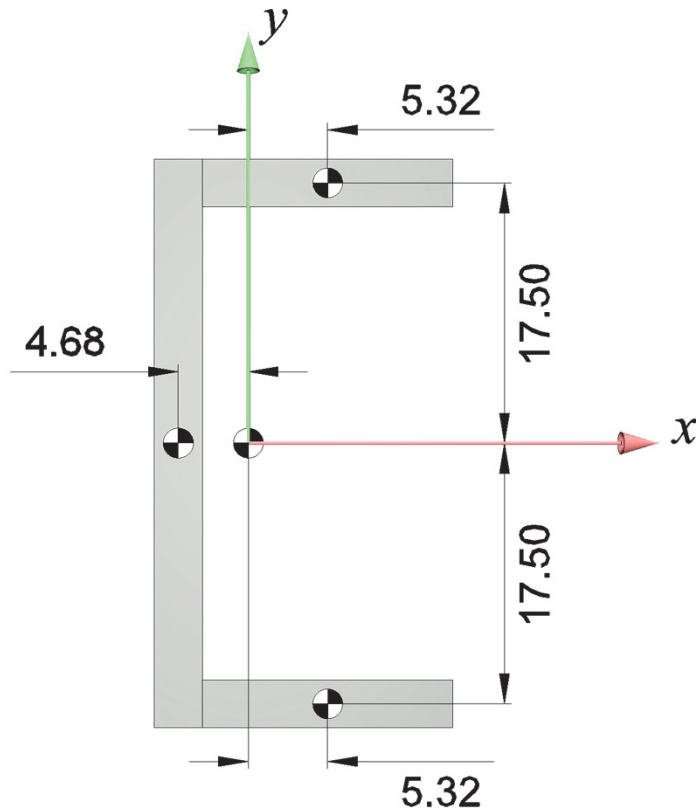
$$\bar{X} = \frac{\sum \bar{X}_i A_i}{\sum A_i} = \frac{\bar{X}_A A_A + \bar{X}_B A_B + \bar{X}_C A_C}{A_A + A_B + A_C} = \frac{2 (10.0)(53.76)}{(122.24) + 2 (53.76)}$$

$$\bar{X} = 4.68 \text{ mm}$$

$$\bar{Y} = 0$$



- Applying the parallel axis theorem for section A:



$$I_{x_A x_A} = \frac{b h^3}{12} = \frac{(3.2)(38.2)^3}{12} = 14,864.79 \text{ mm}^4$$

$$\bar{y}_A = \bar{Y}_A - \bar{Y} = 0$$

$$I_{xx}^A = I_{x_A x_A} + A_A (\bar{y}_A)^2$$

$$I_{xx}^A = 14,864.79 \text{ mm}^4$$

$$I_{y_A y_A} = \frac{b h^3}{12} = \frac{(38.2)(3.2)^3}{12} = 104.31 \text{ mm}^4$$

$$\bar{x}_A = \bar{X}_A - \bar{X} = 0 - 4.68 = -4.68 \text{ mm}$$

$$I_{yy}^A = I_{y_A y_A} + A_A (\bar{x}_A)^2$$

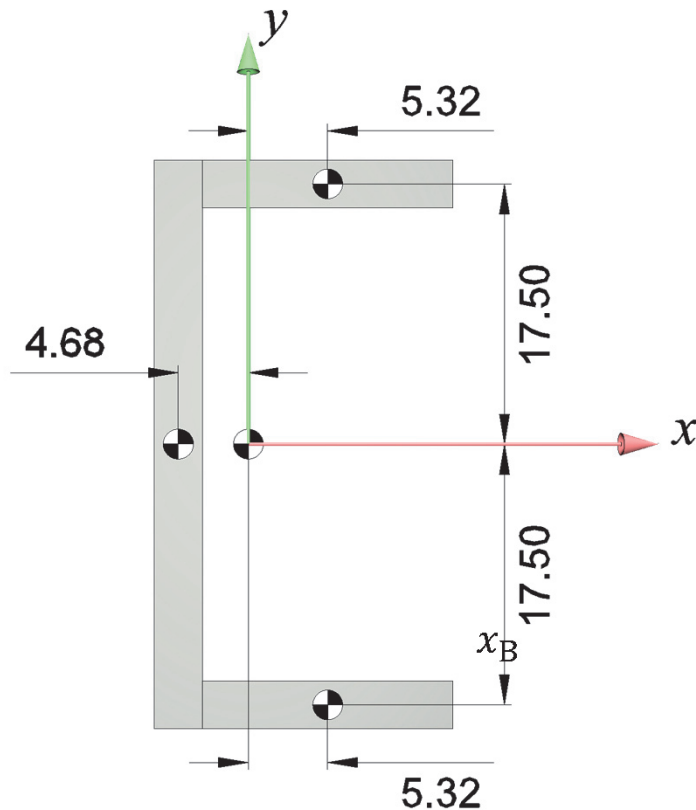
$$I_{yy}^A = 2,781.28 \text{ mm}^4$$

$$I_{x_A y_A} = 0 \text{ (symmetric cross-section)}$$

$$I_{xy}^A = I_{x_A y_A} + A_A (\bar{x}_A \bar{y}_A)$$

$$I_{xy}^A = 0$$

- Applying the parallel axis theorem for sections B and C:



$$I_{x_B x_B} = \frac{b h^3}{12} = \frac{(19.95)(3.26)^3}{12} = 45.88 \text{ mm}^4$$

$$\bar{y}_B = \bar{Y}_B - \bar{Y} = 17.5 - 0 = 17.5 \text{ mm}$$

$$I_{xx}^B = I_{x_B x_B} + A_B (\bar{y}_B)^2$$

$$I_{xx}^B = I_{xx}^C = 2,786.28 \text{ mm}^4$$

$$I_{y_B y_B} = \frac{b h^3}{12} = \frac{(3.26)(19.95)^3}{12} = 1,264.44 \text{ mm}^4$$

$$\bar{x}_B = \bar{X}_B - \bar{X} = 10.0 - 4.68 = 5.32 \text{ mm}$$

$$I_{yy}^B = I_{y_B y_B} + A_B (\bar{x}_B)^2$$

$$I_{yy}^B = I_{yy}^C = 16,509.88 \text{ mm}^4$$

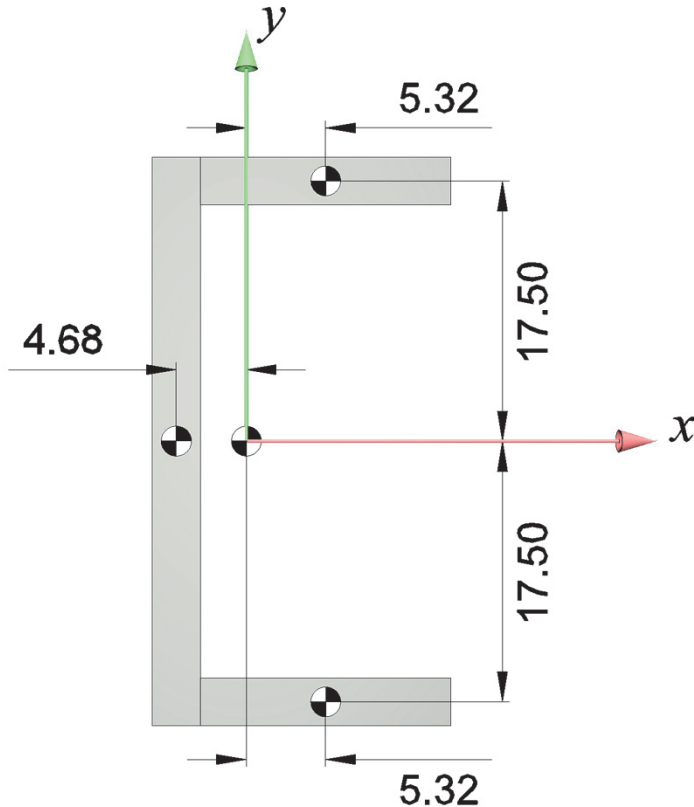
$$I_{x_B y_B} = 0 \text{ (symmetric cross-section)}$$

$$I_{xy}^B = I_{x_B y_B} + A_B (\bar{x}_B \bar{y}_B)$$

$$I_{xy}^B = 5,005.37 \text{ mm}^4 \quad \text{and} \quad I_{xy}^C = -5,005.37 \text{ mm}^4$$



- Finally, for the compound section:



$$I_{xx} = I_{xx}^A + I_{xx}^B + I_{xx}^C$$

$$I_{xx} = 47,884.54 \text{ mm}^4$$

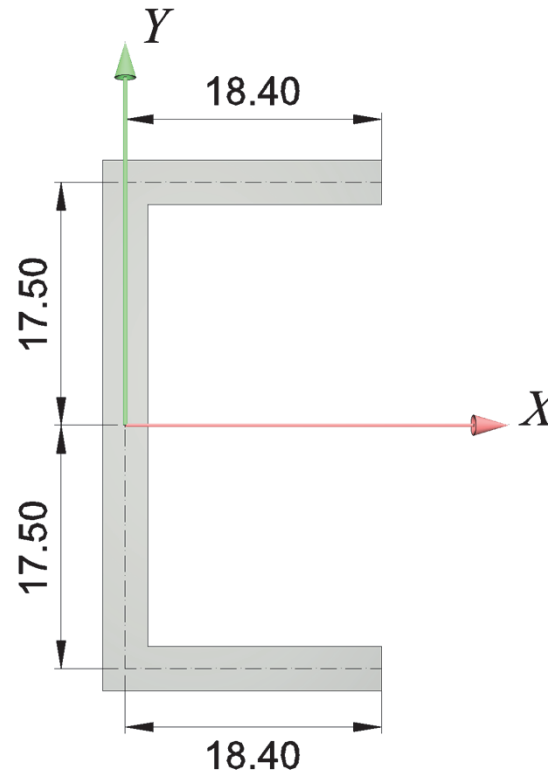
$$I_{yy} = I_{yy}^A + I_{yy}^B + I_{yy}^C$$

$$I_{yy} = 8,353.60 \text{ mm}^4$$

$$I_{xy} = I_{xy}^A + I_{xy}^B + I_{xy}^C$$

$$I_{xy} = 0$$

- To calculate the shear centre we apply thin-wall assumptions and consider the centrelines of the cross-section:



Equations:

Shear centre:

$$S_y e_x = \int (Y q_{s,x} - X q_{s,y}) ds \quad S_x e_y = \int (Y q_{s,x} - X q_{s,y}) ds$$

Shear flow:

$$-q_s = \left( \frac{S_x I_{xx} + S_y I_{xy}}{I_{xy}^2 - I_{xx} I_{yy}} \right) \int_0^s x t ds + \left( \frac{S_y I_{yy} + S_x I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right) \int_0^s y t ds$$

$$-q_s = \left( \frac{S_x I_{xx} + S_y I_{xy}}{I_{xy}^2 - I_{xx} I_{yy}} \right) \int_0^s x t ds + \left( \frac{S_y I_{yy} + S_x I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right) \int_0^s y t ds$$

Since  $I_{xy} = S_x = 0$ :

$$-q_s = \left( \frac{S_y}{I_{xx}} \right) \int_0^s y t ds$$

Integrating:

$$-q_s = \frac{S_y y t}{I_{xx}} s$$

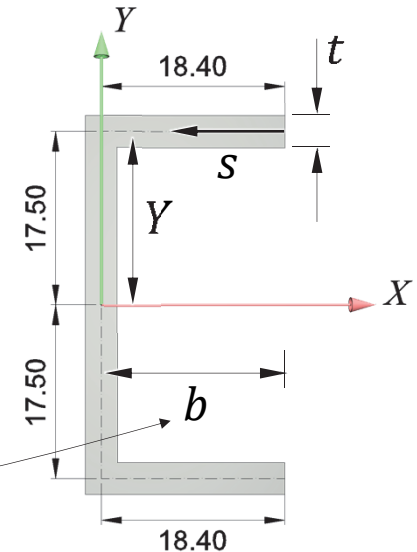
Shear centre formula:  $S_y e_x = \int (Y q_{s,x} - X q_{s,y}) ds$

Combining sections B and C:  $S_y e_x = 2 \int_0^b (Y q_s) ds$

Replacing  $q_s$ :  $S_y e_x = -2 \int_0^b \frac{S_y y^2 t}{I_{xx}} s ds$

Integrating:  $S_y e_x = -\frac{S_y y^2 t b^2}{I_{xx}}$

Cancelling out  $S_y$ :  $e_x = -\frac{y^2 t b^2}{I_{xx}}$



$$e_x = -\frac{(17.5)^2 (3.2) (18.4)^2}{(47,884.54)}$$

$$e_x = -6.93 \text{ mm}$$

(i.e. to the left of the reference point)