

Example 2.1.1

- a) A plastic rod of solid circular cross-section with diameter 30 mm and length 0.5 m is subjected to a tensile load of 12 kN as shown in Figure 1. The rod is made of PMMA (polymethyl methacrylate, or 'acrylic') with a Young's modulus of 3.1 GPa. Calculate the elongation  $e_a$  of the rod.

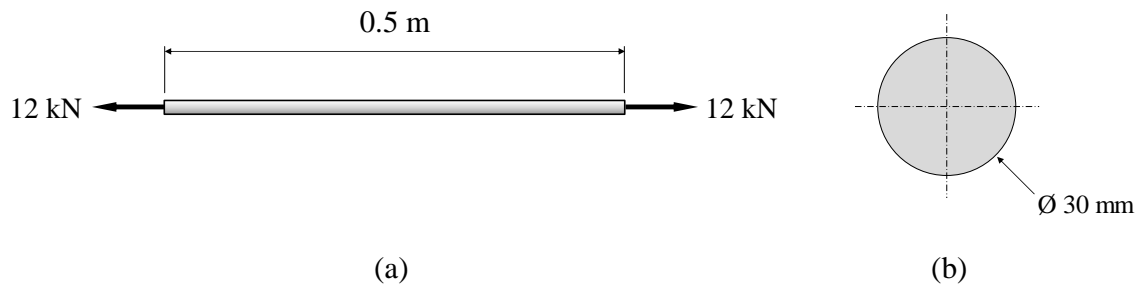


Figure 1: A plastic rod loaded in tension.

- b) In order to increase the axial stiffness, engineers decided to adhesively-bond a sleeve on to the rod as shown in Figure 2. The sleeve has an outer diameter of 45 mm, length of 0.3 m and is made of polyamide (or 'Nylon') with a Young's modulus of 2.5 GPa. Calculate the total elongation  $e_b$  of the assembly when subjected to the same tensile load of 12 kN. Assume that no slippage can occur between the rod and sleeve.

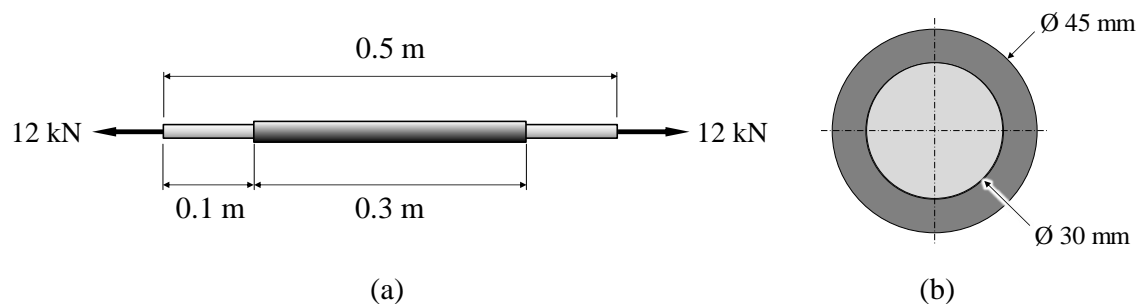
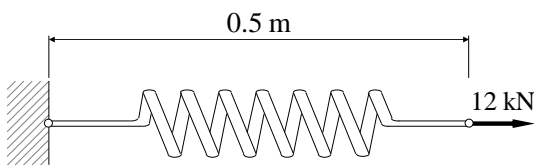


Figure 2: The plastic rod with a bonded sleeve.

- a) This axial member behaves as a single spring of stiffness  $\lambda$  :

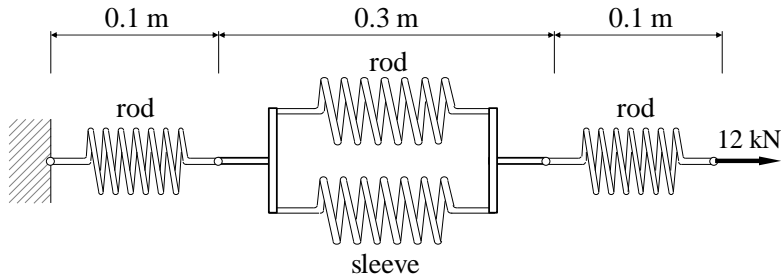


$$F = \lambda e \quad \therefore \quad e = \frac{F}{\lambda}$$

The stiffness  $\lambda$  is given by:  $\lambda_a = \frac{EA}{L} = \frac{E(\pi r^2)}{L} = \left(\frac{1}{500 \text{ mm}}\right) \left(3100 \frac{\text{N}}{\text{mm}^2}\right) \pi (15 \text{ mm})^2 \quad \therefore \quad \lambda_a = 4382.5 \frac{\text{N}}{\text{mm}}$

The elongation is therefore:  $e_a = \frac{F}{\lambda_a} = \frac{12000 \text{ N}}{4382.5 \text{ N/mm}} \quad \therefore \quad e_a = 2.738 \text{ mm}$

b) As the member is now made of two different cross-sections (with or without the sleeve), we can treat it as an assembly of springs:



(Remember the rules for springs in **series** and in **parallel** discussed in lectures.)

Both 'unsleeved' ends behave as springs of length 100 mm:

$$\lambda_1 = \frac{E (\pi r^2)}{L} = \left( \frac{1}{100 \text{ mm}} \right) \left( 3100 \frac{\text{N}}{\text{mm}^2} \right) \pi (15 \text{ mm})^2 \quad \therefore \quad \lambda_1 = 21912.6 \frac{\text{N}}{\text{mm}}$$

The sleeved section behaves as two springs in **parallel**:

$$\begin{aligned} \lambda_2 &= \lambda_{\text{rod}} + \lambda_{\text{sleeve}} \\ &= \frac{E_{\text{sleeve}} \left[ \pi (r_{\text{outer}}^2 - r_{\text{inner}}^2) \right]}{L} + \frac{E_{\text{rod}} (\pi r^2)}{L} \\ &= \left( \frac{\pi}{300 \text{ mm}} \right) \left( 2500 \frac{\text{N}}{\text{mm}^2} \right) [(22.5 \text{ mm})^2 - (15 \text{ mm})^2] + \left( \frac{\pi}{300 \text{ mm}} \right) \left( 3100 \frac{\text{N}}{\text{mm}^2} \right) \pi (15 \text{ mm})^2 \\ &= \left( 7363.1 \frac{\text{N}}{\text{mm}} \right) + \left( 7304.3 \frac{\text{N}}{\text{mm}} \right) \\ \lambda_2 &= 14667.3 \frac{\text{N}}{\text{mm}} \end{aligned}$$

The sleeved and the two unsleeved sections behave as three springs in **series**, therefore:

$$\begin{aligned} e_b &= 2e_1 + e_2 \\ &= 2 \frac{F}{\lambda_1} + \frac{F}{\lambda_2} \\ &= 2 \frac{12000 \text{ N}}{21912.6 \text{ N/mm}} + \frac{12000 \text{ N}}{14667.3 \text{ N/mm}} \\ &= 2(0.547 \text{ mm}) + (0.818 \text{ mm}) \\ e_b &= 1.913 \text{ mm} \end{aligned}$$