

Properties of Materials

Theme: Polymers and Composites

Lecture 3: Composites

Dr Chenchen Zhu

chenchen.zhu@bristol.ac.uk

Frank LT PHYS BLDG

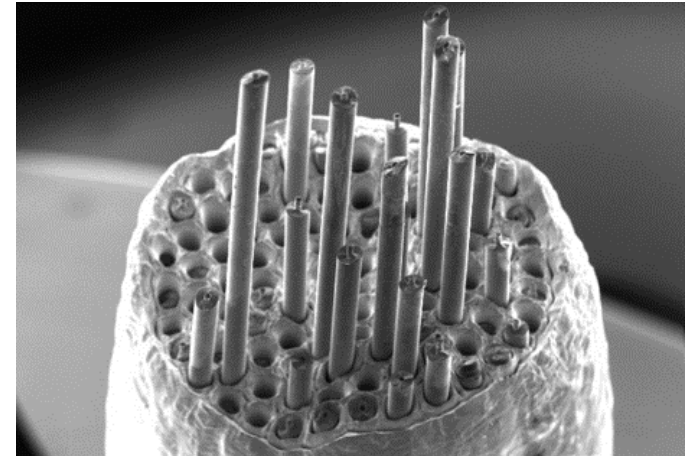
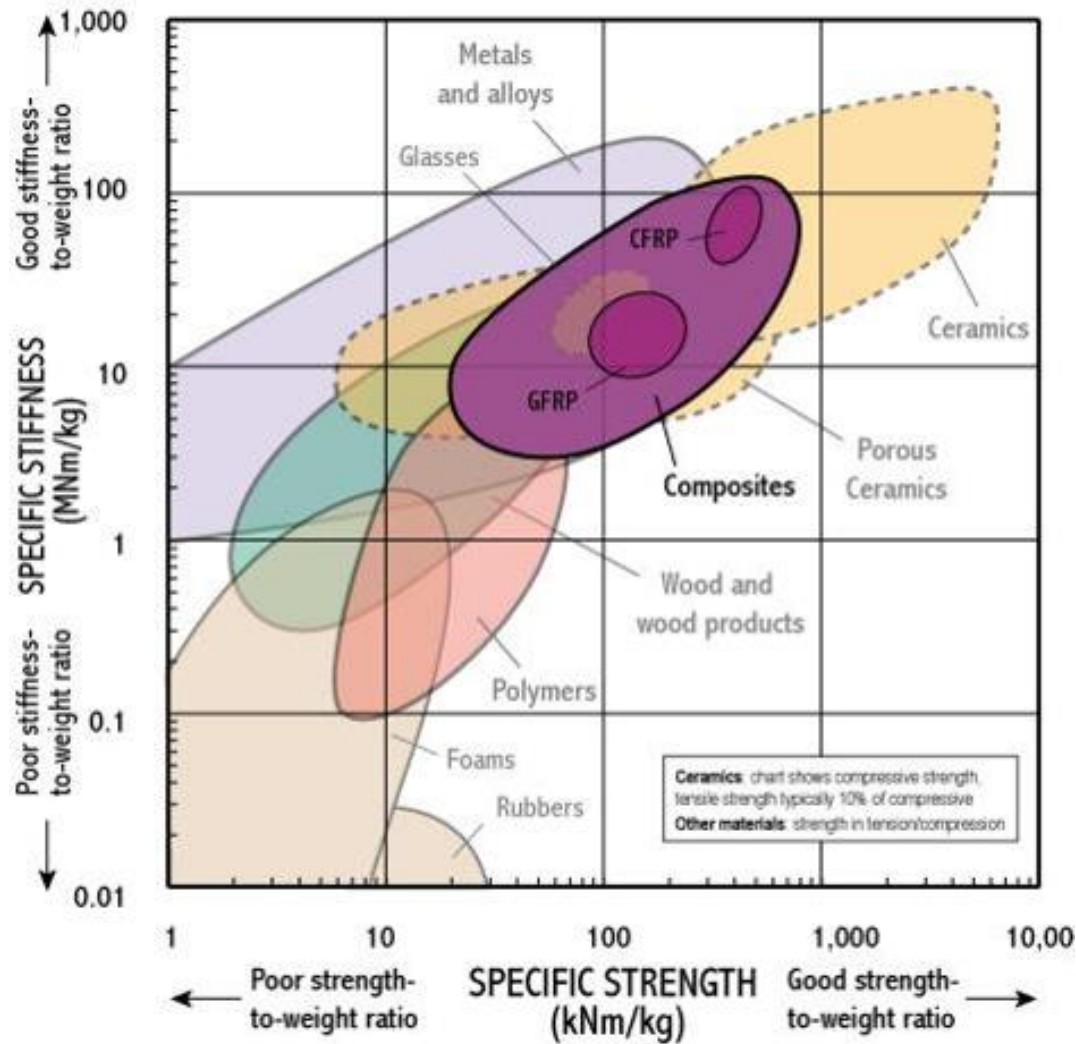
Lecture Contents

- Lecture 1
 - Introduction
 - Basic structure of polymers
- Lecture 2
 - Deformation
 - Chain alignment and viscoelasticity
- Lecture 3
 - Composites
 - Modulus and strength

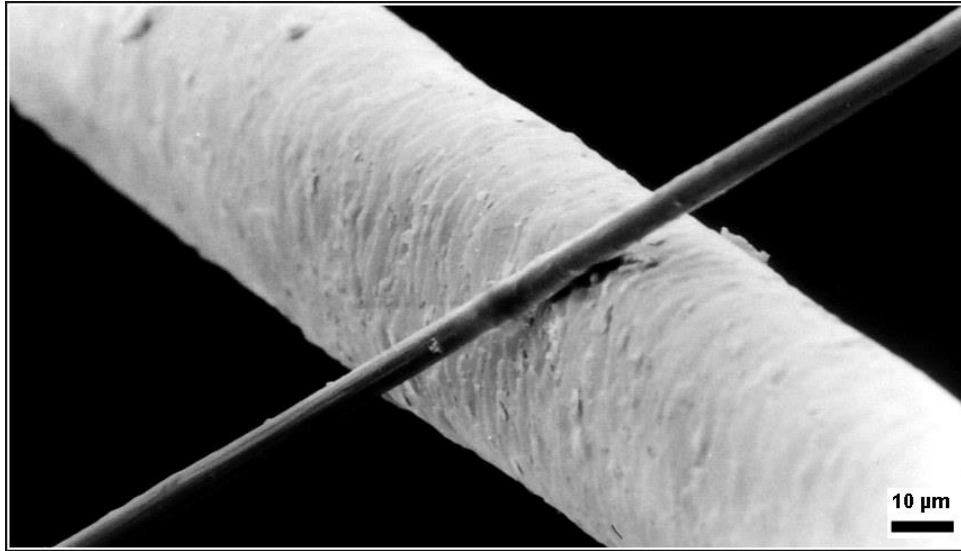
Lecture 3 Composites

1. Composites
2. Carbon fibre
3. Unidirectional carbon fibre/matrix (resin) composites
 - Properties
 - Modulus
 - Strength
 - Anisotropy
 - Toughness

Composites



Carbon fibre



- Hard to make bulk strong carbon
- Easy to make high quality fibre

- Fibre strong in tension
- Weave fibre into fabric for mass use



Unidirectional carbon fibre/matrix (resin) composites

- Fibre provides strength and stiffness
- Resin provides protection (wear, chemical) and holds shape

Volume fraction of composites $V_c = 1$

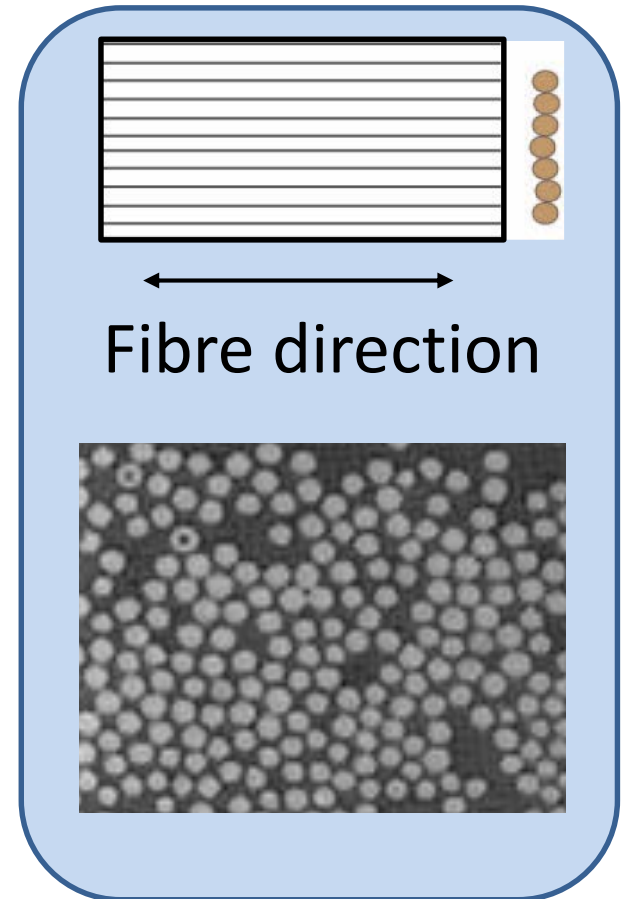
Volume fraction of fibres $V_f = v_f / v_c$

Volume fraction of matrix $V_m = 1 - V_f$



volume of
composites

c = composite
 f = fibre
 m = matrix



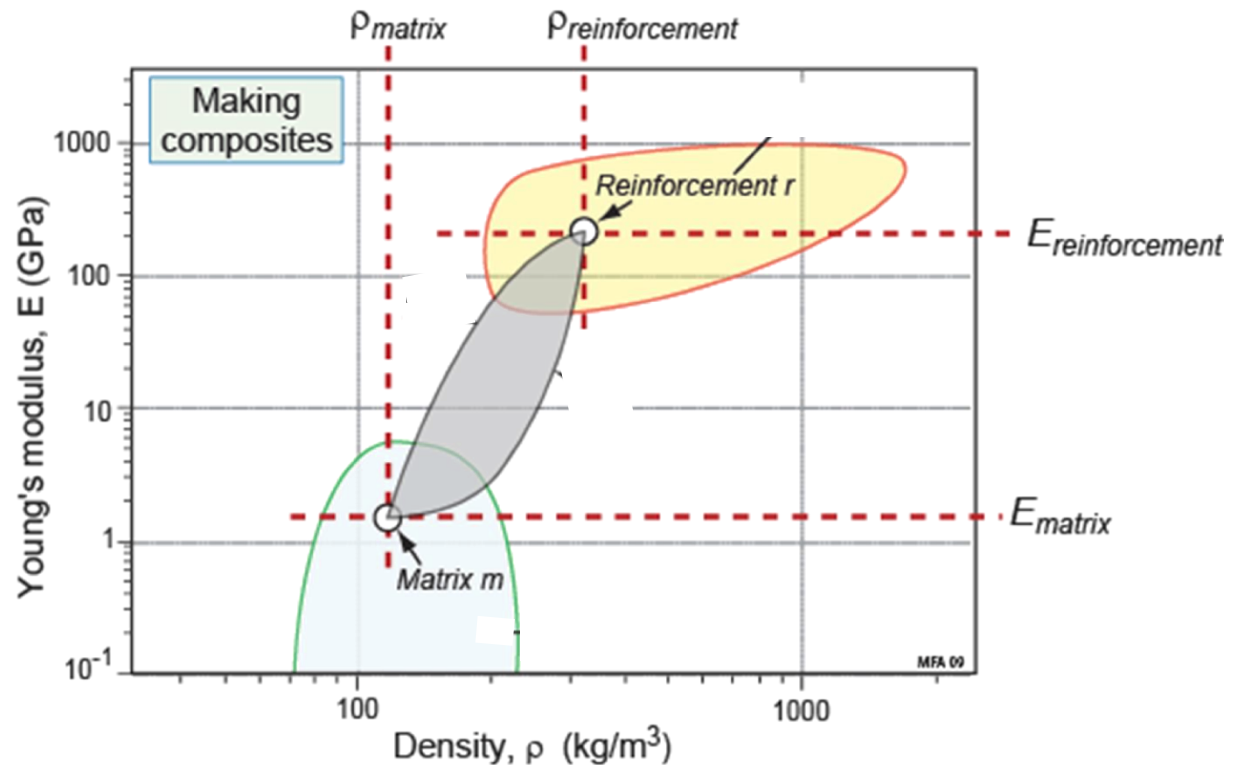
Properties

Expect to see volume fraction dependent properties

E.g. Carbon fibre-epoxy

$$\rho_c = V_f \rho_f + (1 - V_f) \rho_m$$

volume fraction of fibres



$$\sigma_f = E_f \epsilon_f$$

2.2 GPa

390 GPa

0.0056

$$\sigma_m = E_m \epsilon_m$$

0.06 GPa

3.5 GPa

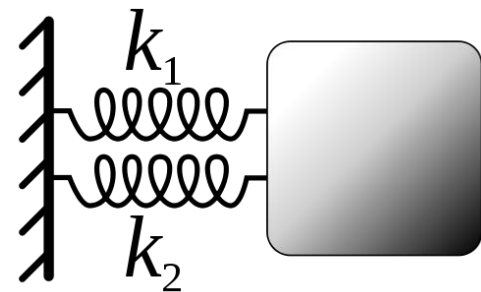
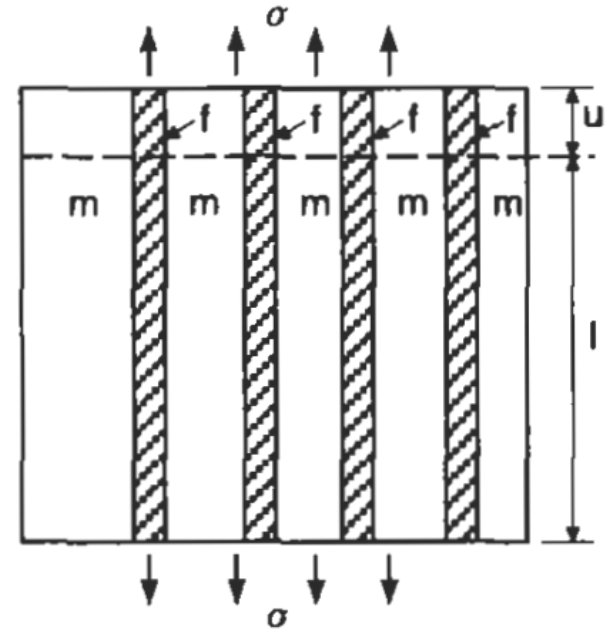
0.017

c = composite
f = fibre
m = matrix

Modulus- parallel with fibres

- Same **strain** in both components
 - $\epsilon_c = \epsilon_f = \epsilon_m$
 - Otherwise continuity breaks
- Fibre higher modulus
 - Same strain, high E = high fibre stress

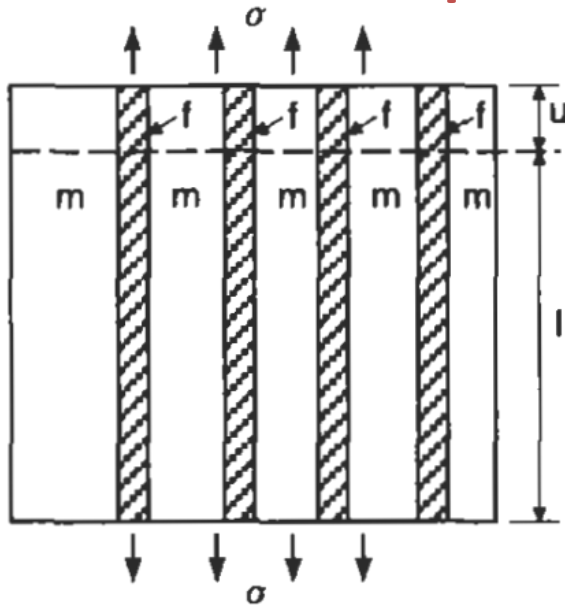
c = composite
 f = fibre
 m = matrix



How to get E_c ?

$$\epsilon_c = \epsilon_f = \epsilon_m$$

Modulus- parallel with fibres



c = composite
f = fibre
m = matrix

$$F_c = F_f + F_m \quad (1)$$

$$\varepsilon_c = \varepsilon_f = \varepsilon_m \quad (2)$$

$$(1) \xrightarrow{F = \sigma A} \sigma_c A_c = \sigma_f A_f + \sigma_m A_m \quad (3)$$

$$(3) \xrightarrow{\sigma = E\varepsilon + (2)} E_c A_c = E_f A_f + E_m A_m \quad (4)$$

$$(5) (4) \xrightarrow{(5)} E_c \mathcal{V}_c = \mathcal{V}_f E_f + \mathcal{V}_m E_m \quad (6)$$

$$(6) \xrightarrow{\substack{V_f = \mathcal{V}_f / \mathcal{V}_c \\ V_m = \mathcal{V}_m / \mathcal{V}_c}} E_c = V_f E_f + V_m E_m$$

volume fraction of fibres

$$V_m = 1 - V_f$$

volume of composites

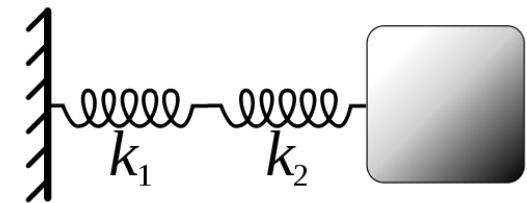
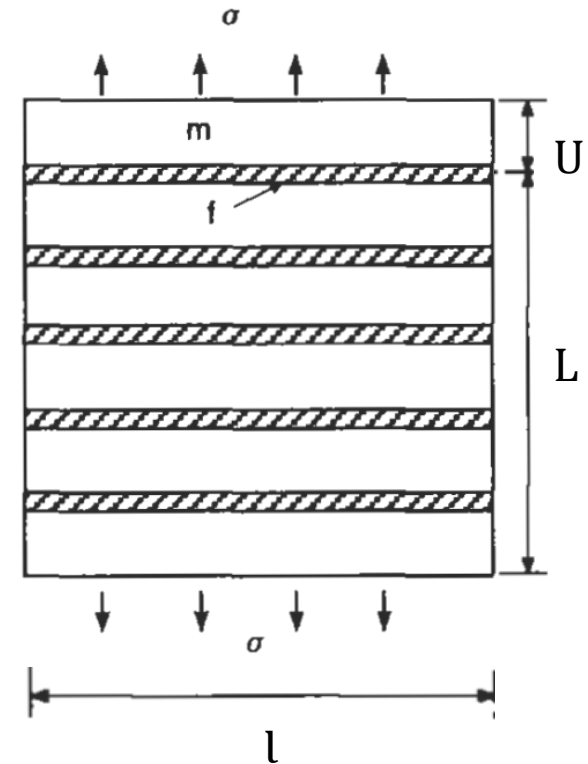
$$\mathcal{V}_c = l A_c$$

$$\mathcal{V}_f = l A_f$$

$$\mathcal{V}_m = l A_m$$

Modulus- perpendicular to fibres

- Same **stress** (σ) in both components
 - $\sigma_c = \sigma_f = \sigma_m$
 - No need for continuity
- Constant length (l) and thickness (t)
- Strain function of E
 - Matrix: low E , high strain
 - Fibre: high E , low strain
- Fibres provide no restraint on matrix strain
 - limited reinforcement

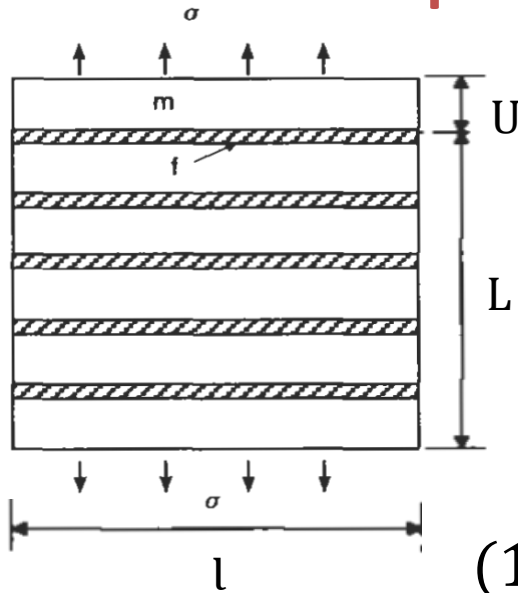


$$\epsilon_c = \epsilon_f + \epsilon_m$$

How to get E_c ?

c = composite
 f = fibre
 m = matrix

Modulus- perpendicular to fibres



Overall displacement of composites

$$U_c = U_f + U_m \quad (1)$$

$$\sigma_c = \sigma_f = \sigma_m \quad (2)$$

$$(1) \xrightarrow{U = L\varepsilon} L_c \varepsilon_c = L_f \varepsilon_f + L_m \varepsilon_m \quad (3)$$

$$(3) \xrightarrow{\varepsilon = \sigma/E} L_c/E_c = L_f/E_f + L_m/E_m \quad (4)$$

$$(4) \xrightarrow{(5)} \mathcal{V}_c/E_c = \mathcal{V}_f/E_f + \mathcal{V}_m/E_m \quad (6)$$

$$(6) \xrightarrow{\substack{V_f = \mathcal{V}_f / \mathcal{V}_c \\ V_m = \mathcal{V}_m / \mathcal{V}_c}} 1/E_c = V_f/E_f + V_m/E_m$$

volume of composites

$$\left. \begin{aligned} \mathcal{V}_c &= tlL_c \\ \mathcal{V}_f &= tlL_f \\ \mathcal{V}_m &= tlL_m \end{aligned} \right\} (5)$$

$$V_m = 1 - V_f$$

Modulus of unidirectional composites

Parallel

$$E_c = V_f E_f + (1 - V_f) E_m$$

Conditions:

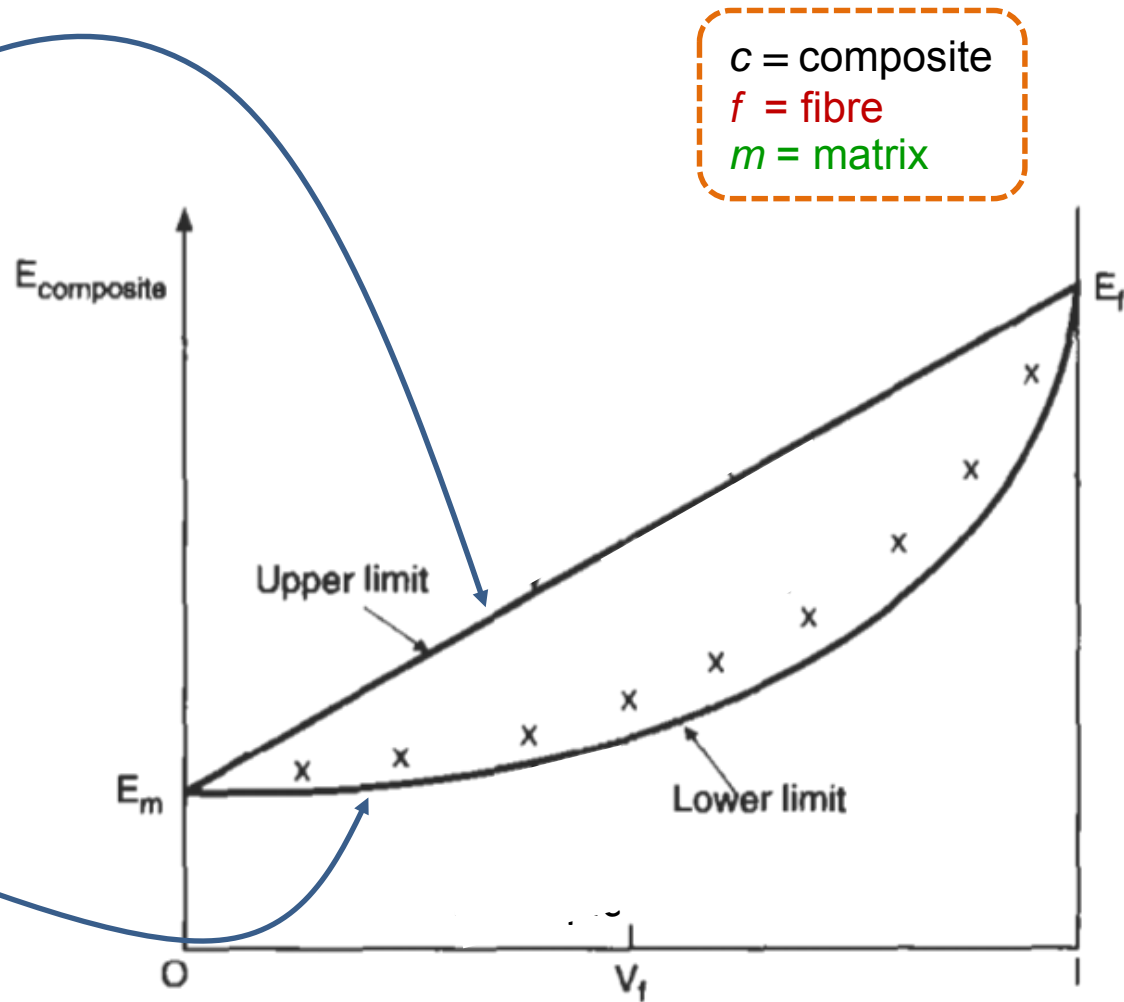
- Same strain ($\epsilon_c = \epsilon_f = \epsilon_m$)

Perpendicular

$$\frac{1}{E_c} = \frac{V_f}{E_f} + \frac{(1 - V_f)}{E_m}$$

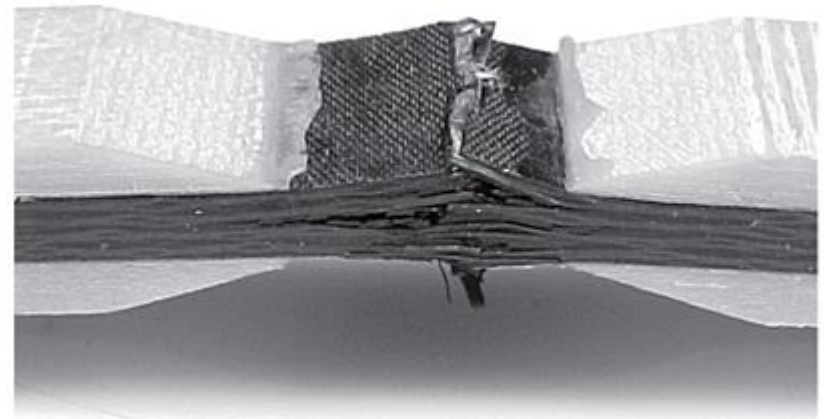
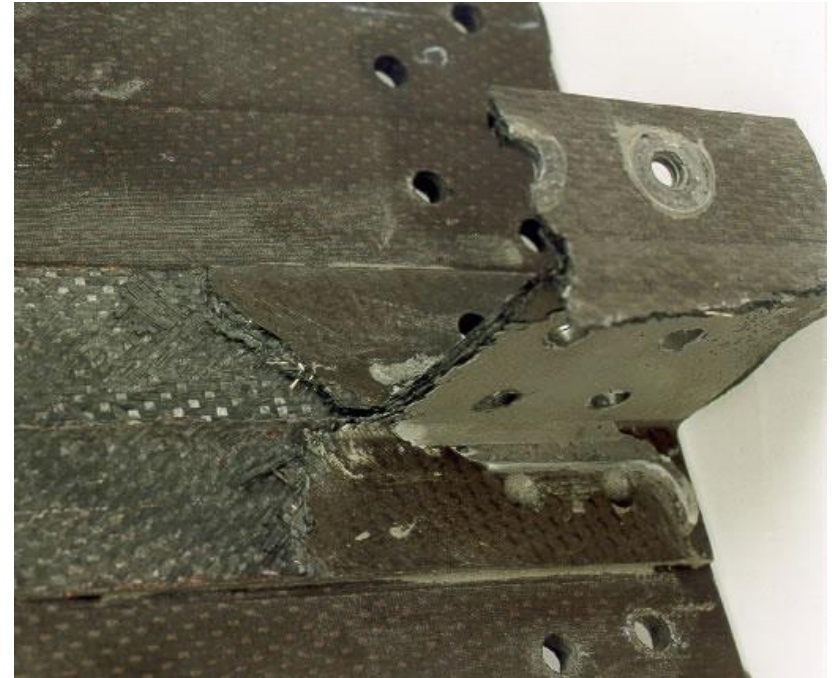
Conditions:

- Same stress ($\sigma_c = \sigma_f = \sigma_m$)



Strength

- Much more complex than modulus
- Multiple failure mechanisms
- Hard to predict compared to metals
 - Major limit on uptake



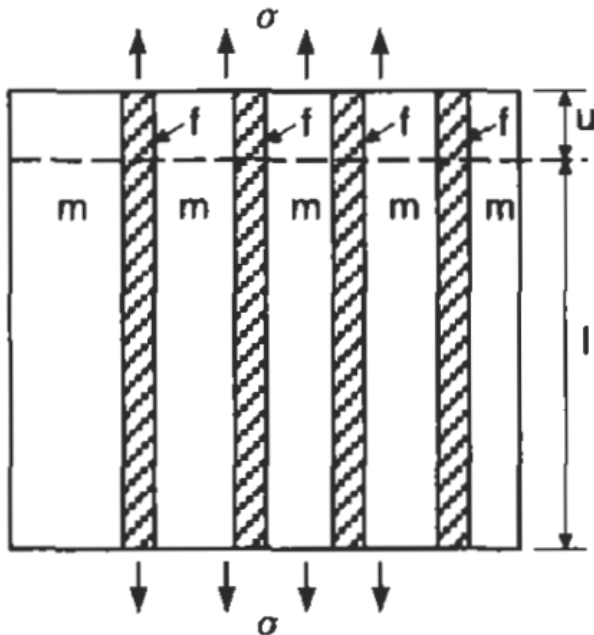
Strength - parallel with fibres

Assume linear elastic fibres and matrix

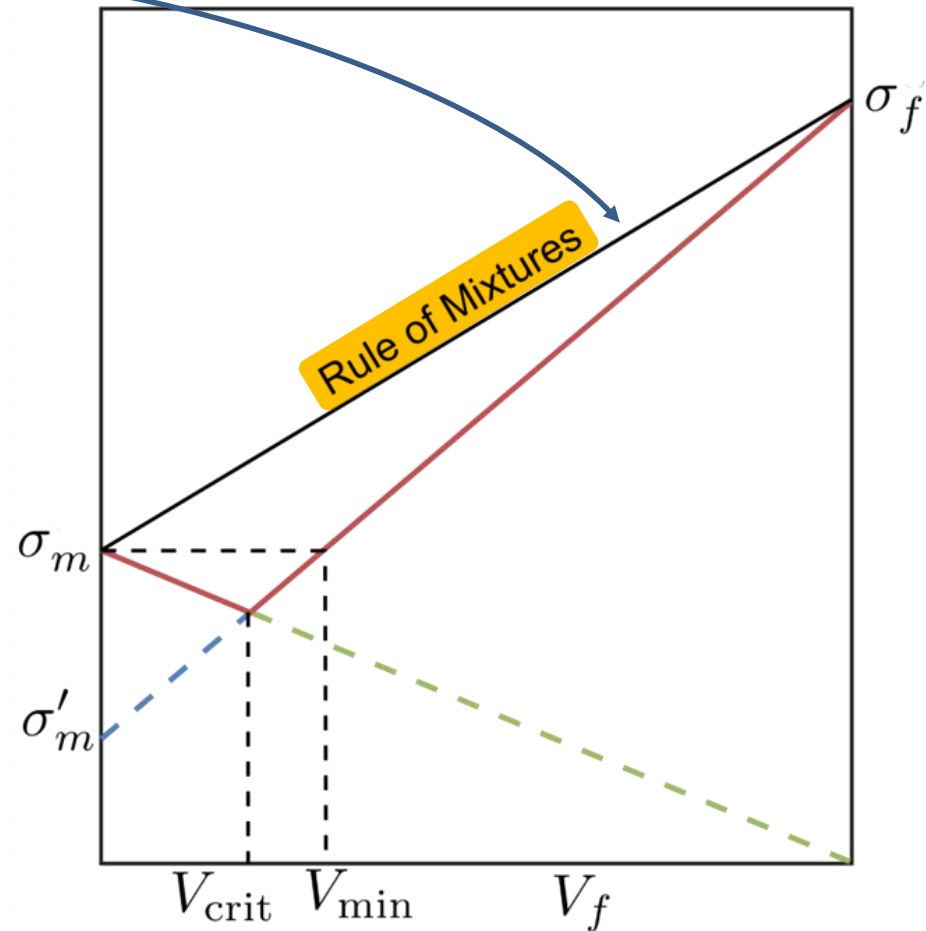
$$\sigma_c = V_f \sigma_f + (1 - V_f) \sigma_m$$

Conditions:

- Loads are parallel with fibres
- Same strain ($\epsilon_c = \epsilon_f = \epsilon_m$)



c = composite
f = fibre
m = matrix



Strength – parallel with fibres

- High fibre fraction
 - Controlled by stiff fibres
 - Fibres fail, matrix fails
 - Reduced matrix contribution

$$\varepsilon'_m = \varepsilon_f \longrightarrow \sigma'_m = E_m \varepsilon_f$$

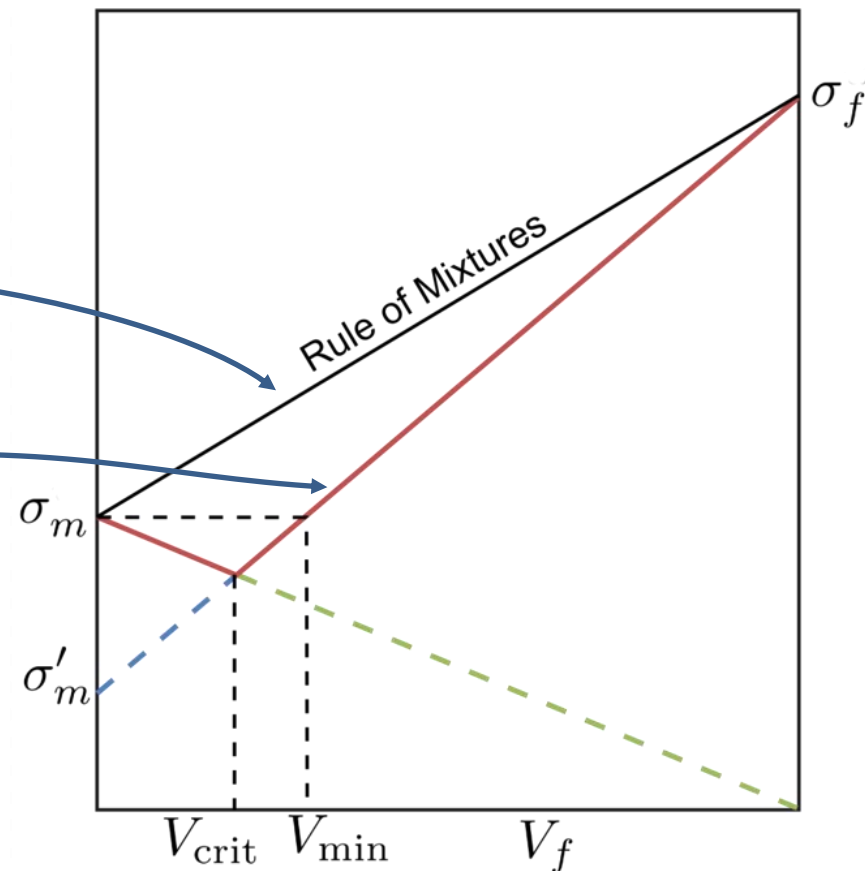
$$\sigma_c = V_f \sigma_f + (1 - V_f) \sigma_m$$



$$\sigma_c = V_f \sigma_f + (1 - V_f) \sigma'_m$$

Conditions:

- Loads are parallel with fibres
- High fibre fraction
- Same strain ($\varepsilon_c = \varepsilon_f = \varepsilon'_m \leq \varepsilon_m$)



Strength - parallel with fibres

- Low fibre fraction
 - Controlled by matrix
 - Fibres already fractured by the time the matrix reaches failure strain

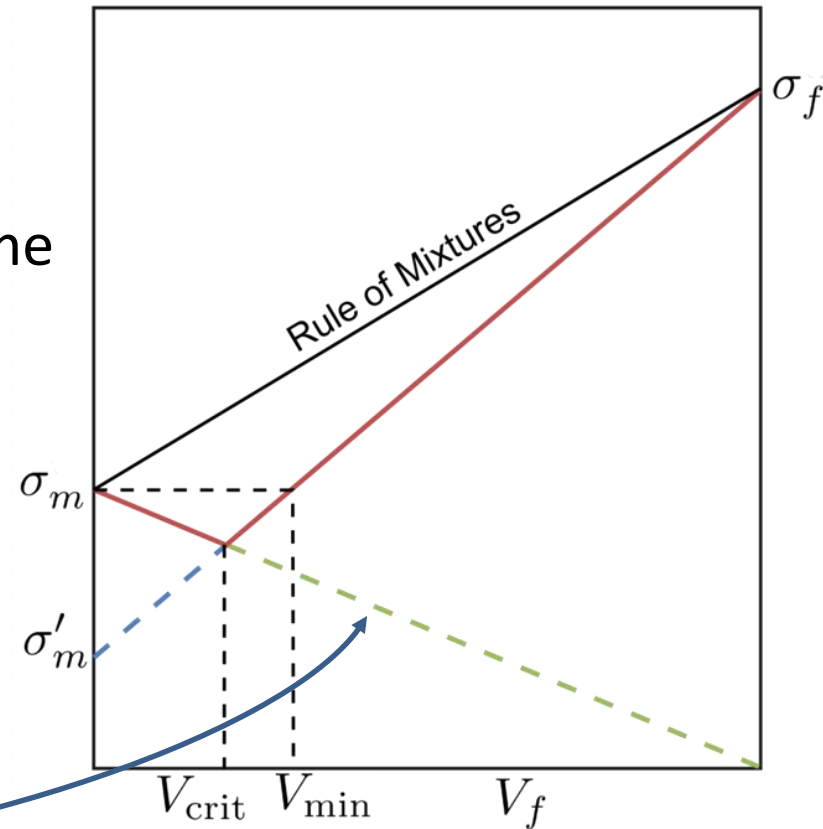
$$\varepsilon_c \approx \varepsilon_m$$

- Fibres don't contribute

$$\sigma_c = V_f \sigma_f + (1 - V_f) \sigma_m$$



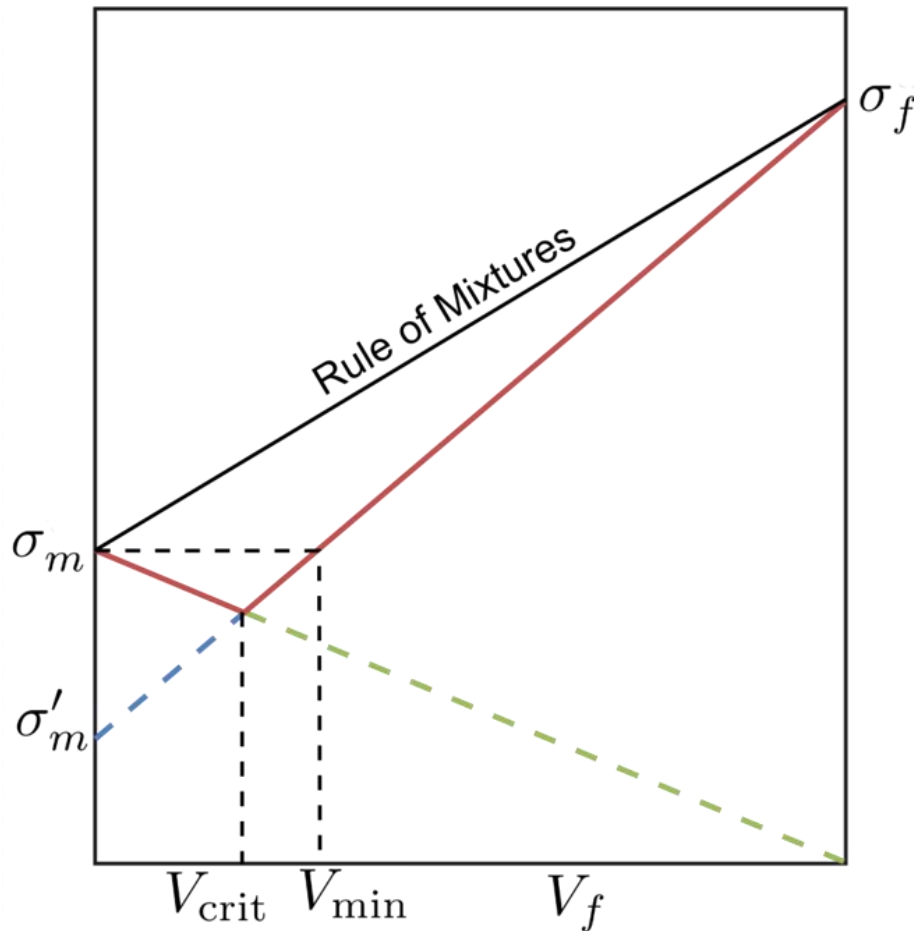
$$\sigma_c = (1 - V_f) \sigma_m$$



Conditions:

- Loads are parallel with fibres
- Low fibre fraction ($V_f \ll 1 - V_f$)
- Same strain ($\varepsilon_c \approx \varepsilon_m \gg \varepsilon_f$)

Strength of composites



- Less benefit than expected
- Need minimum V_f to improve compared to matrix
- Actually compromise strength prior to V_{min}
 - Very low for strong fibres/weak matrix
 - Worst strength at V_{crit}

Example

- Assume in a fibre/matrix composites, $E_f = 350$ GPa, $\varepsilon_f = 0.006$, $E_m = 12$ GPa and $\varepsilon_m = 0.03$. Please use the 'rule of mixtures' to calculate the ratio of matrix stress to composite stress (σ_m / σ_c) for $V_f = 12\%$ and $V_f = 40\%$.

$$\sigma_c = V_f \sigma_f + (1 - V_f) \sigma_m$$

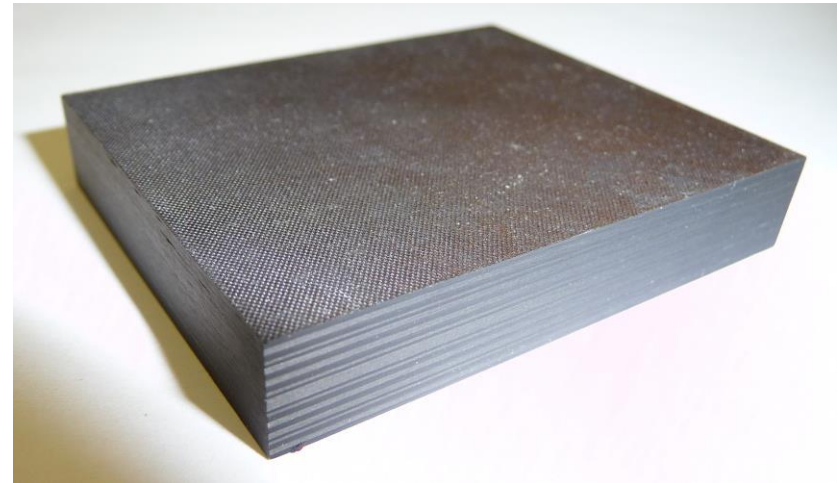
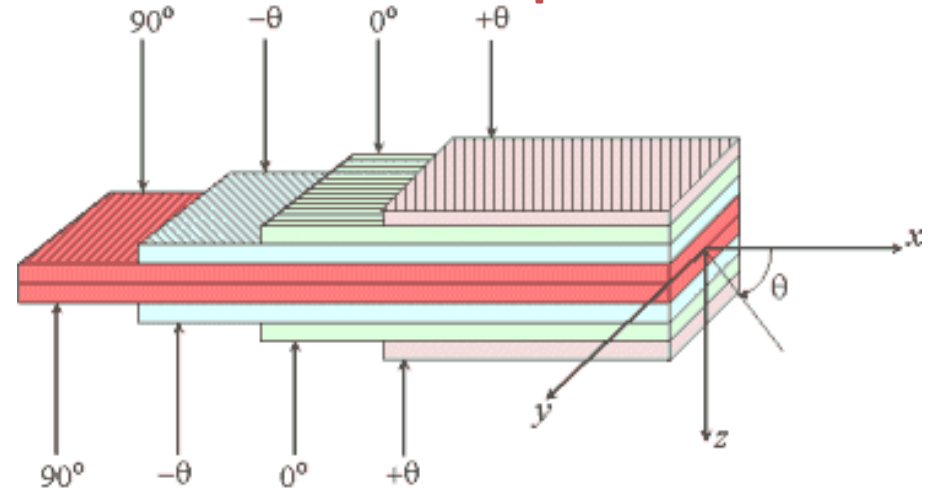
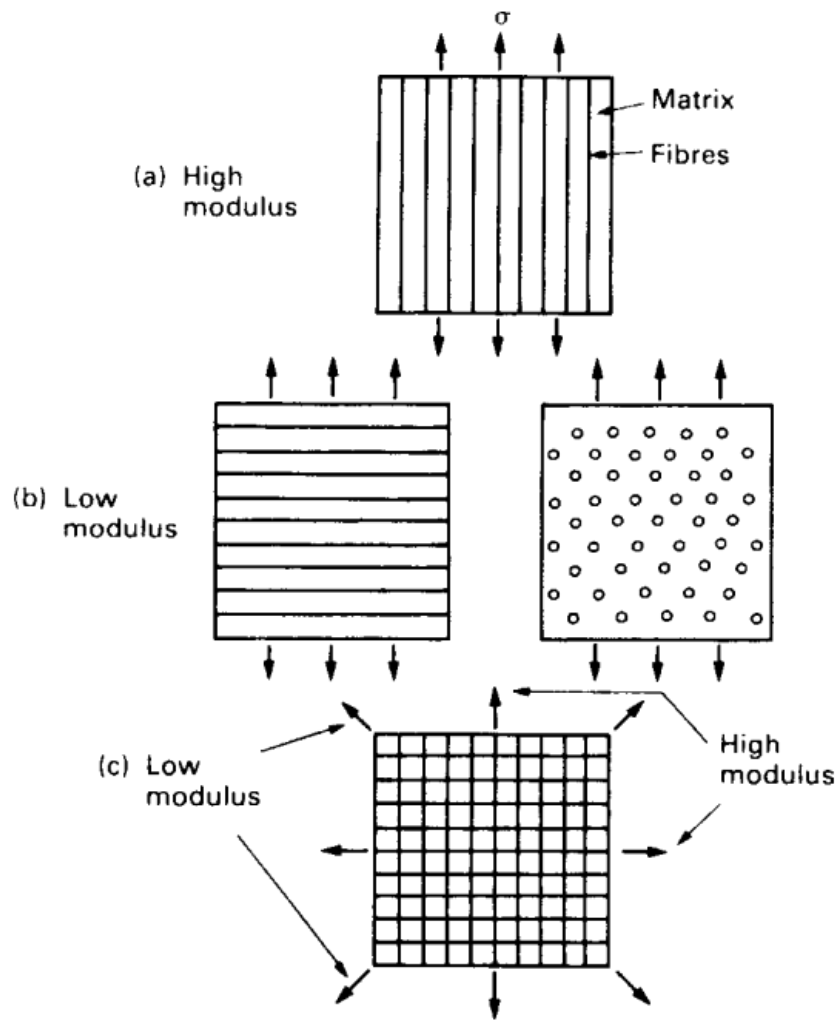


$$\xrightarrow{\sigma = E\varepsilon} \begin{cases} \sigma_c = V_f E_f \varepsilon_f + (1 - V_f) E_m \varepsilon_m & (1) \\ \sigma_m = E_m \varepsilon_m & (2) \end{cases}$$

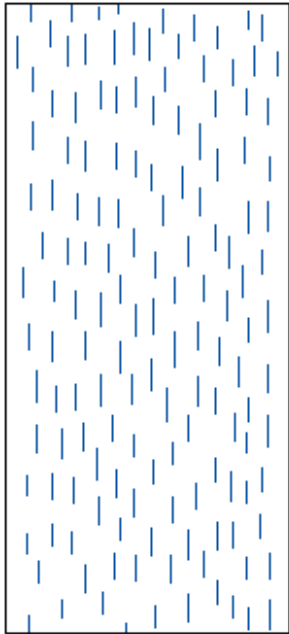
After being used in composites, actually $\varepsilon_c = \varepsilon_m = \varepsilon_f$

$$\xrightarrow[\varepsilon_c = \varepsilon_m = \varepsilon_f]{(2)/(1)} \sigma_m / \sigma_c = \frac{E_m}{V_f E_f + (1 - V_f) E_m} = 0.23 \text{ (12 \%)} \text{ or } 0.08 \text{ (40 \%)}$$

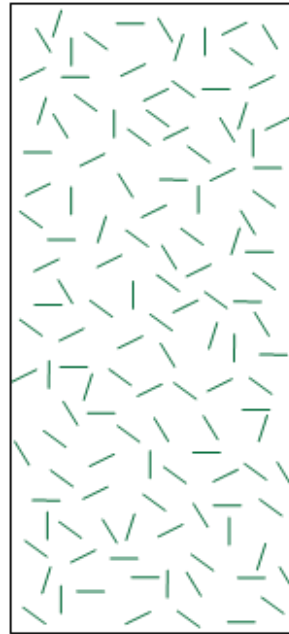
Anisotropy of continuous fibre composites



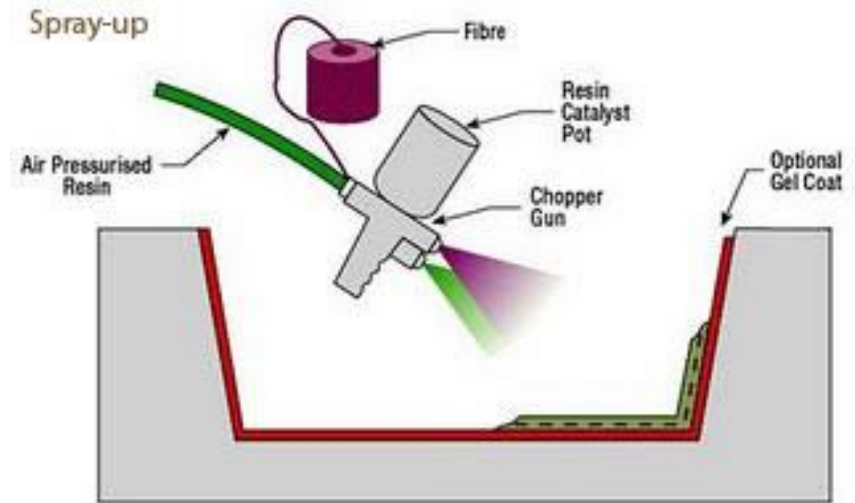
Anisotropy of short fibre composites



Aligned short
fibres
High E
High anisotropy



Random short
fibres
Low E
Low anisotropy



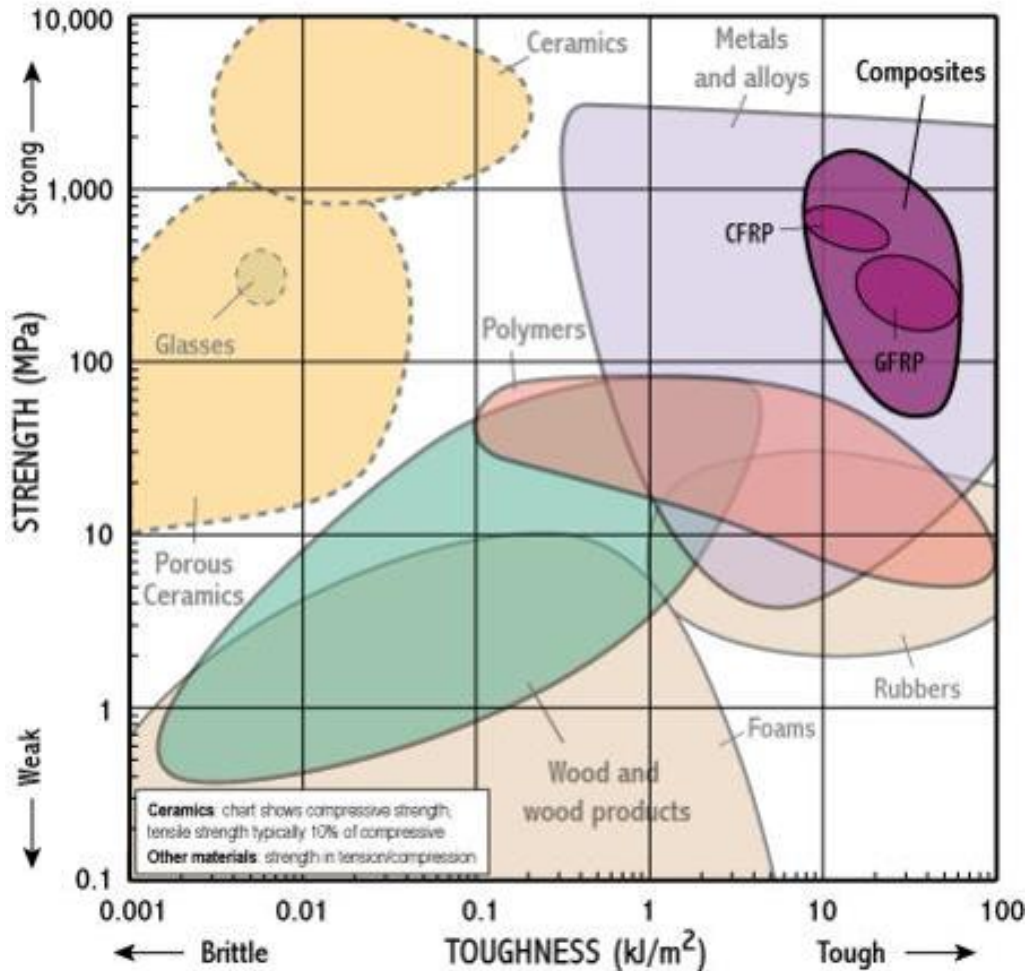
Anisotropy

Opportunity to customise modulus to be high in specified directions



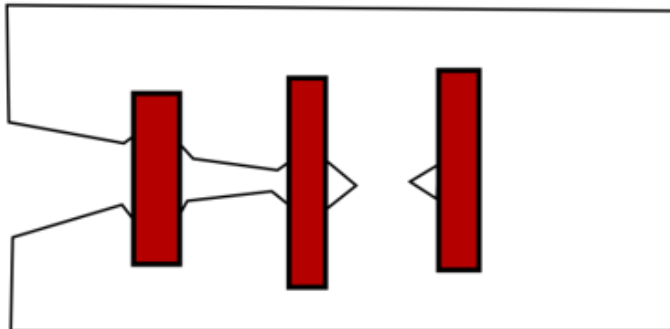
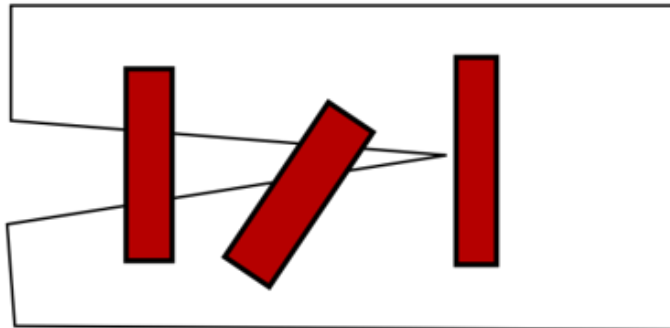
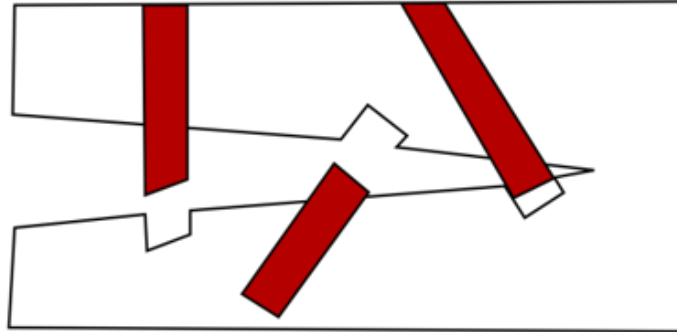
Potential for failure due to unexpected loading!

Toughness



- Composites give E_c and σ_c like ceramic but without the brittleness (not quite)

Toughness of composites



- Fibre pull out
 - Drag fibres from matrix
- Crack bridging
 - Fibres hold crack together and prevent it growing
- Deflection
 - Fibres get in way of crack

Summary

- Composites (and other hybrids) get strengths of both phases and mitigate weaknesses of both
- Potential game changer in design
 - Not properly exploited?
- Introduce new set of complications
 - Either component can fail
 - Multiple failure modes
 - New failure modes
 - Anisotropy in modulus and strength