

Vibrations 2, Lecture 17

Lagrange's equations

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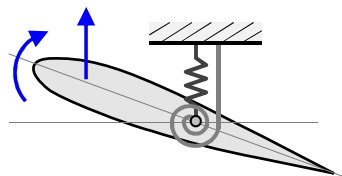
Lecture 16 review

Forced linear *damped* MDOF system: $\mathbf{M} \ddot{\mathbf{x}} + \mathbf{C} \dot{\mathbf{x}} + \mathbf{K} \mathbf{x} = \mathbf{f}(t)$

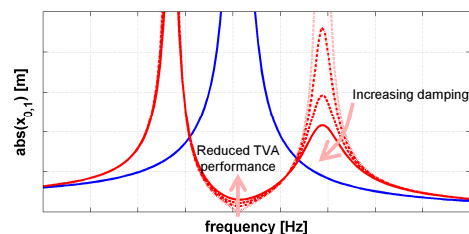
Steady-state harmonic response: $\mathbf{M} \ddot{\mathbf{x}} + \mathbf{C} \dot{\mathbf{x}} + \mathbf{K} \mathbf{x} = \mathbf{f}_0 e^{i\omega t}$
 $\mathbf{x}(t) = \left((-\omega^2 \mathbf{M} + i\omega \mathbf{C} + \mathbf{K})^{-1} \mathbf{f}_0 \right) e^{i\omega t}$

Aero examples/applications:

Elastically suspended rigid wing
with aero loads:



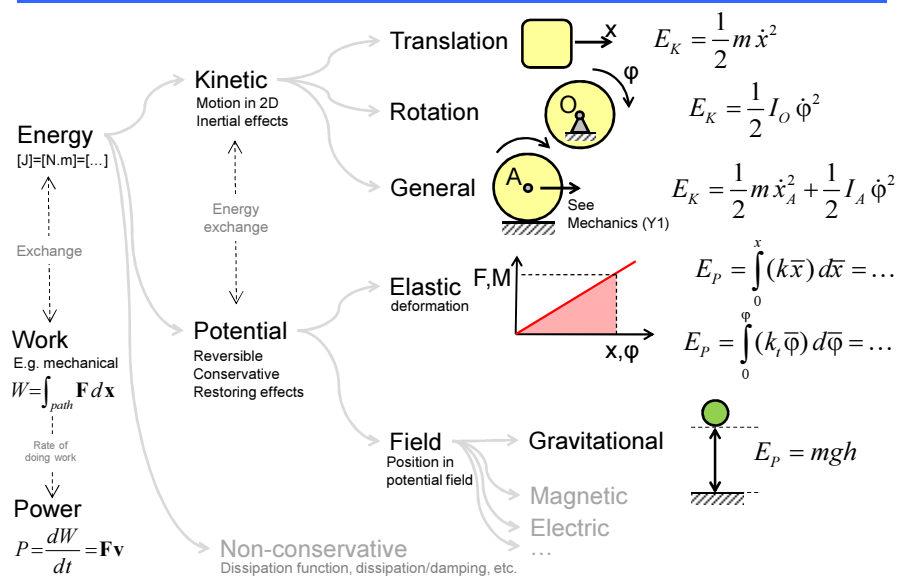
Damped TVA:



Lecture 17

- Overview of energy related concepts
- Lagrange's equations
- Example: 2DOF wing example
- Example: 2 coupled pendulums

Energy and work revision



Lagrange's equations

Lagrange's equations for NDOF system:

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{q}_j} \right) - \frac{\partial \mathcal{L}}{\partial q_j} = Q_j \quad j=1,2,\dots,N$$

where:

$$\mathcal{L} = E_K - E_P$$

\mathcal{L} is the Lagrangian function

E_K is the total kinetic energy (energy stored in motion)

E_P is the total potential energy (energy stored in deformation, position, ...)

q_j are the generalized coordinates (angle, deformation, deflection, ...)

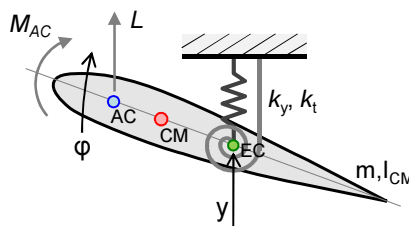
Q_j are the generalized loads (forces or moments)

Properties and advantages:

- Using scalar (energy) functions instead of vectors = "safer" derivations
- Consistent approach when working with rectilinear and angular DOFs and loads
- Minimum number of equations (EOMs) for multi-body and multi-DOF systems
- Programmable

2DOF wing example (Lagrange)

Consider a simplified 2DOF model of a rigid wing suspended on the linear and torsional *springs* (these springs represent elasticity of real wings). Derive the matrix EOM for this system using Lagrange's equations.



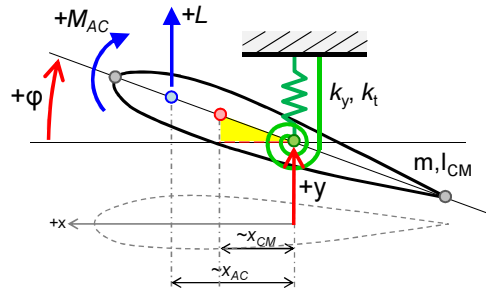
AC ... aerodynamic centre
CM ... centre of mass
EC ... elastic centre

DOFs: 2 (y, ϕ)
Small angle ϕ : $\cos \phi = 1$, $\sin \phi = \phi$

m ... wing mass
 I_{CM} ... moment of inertia about CM

2DOF wing example (Lagrange)

DOFs, generalized coordinates and motion (kinematics):



Number of DOFs: 2 = heaving (up-down) + pitching (rotation about EC)

Generalized coordinates: $q_1 = y$, $q_2 = \phi$; use positive orientations / deflections

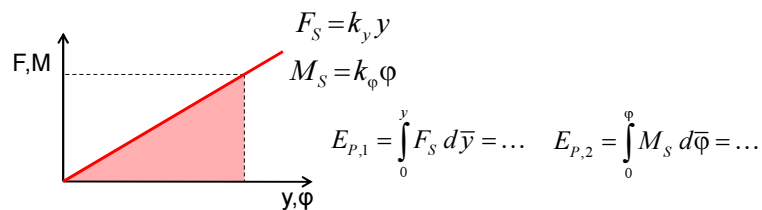
Motion (important points): EC, CM, AC

$$\begin{aligned} x_{EC} &\approx 0 & x_{CM} &\approx 0 & x_{AC} &\approx 0 \\ y_{EC} &\approx y & y_{CM} &\approx y + \phi x_{CM} \Rightarrow \dot{y}_{CM} \approx \dot{y} + \dot{\phi} x_{CM} & y_{AC} &\approx y + \phi x_{AC} \Rightarrow \dot{y}_{AC} = \dots \end{aligned}$$

2DOF wing example (Lagrange)

Energies: kinetic and potential (no damping)

Potential energy:



The potential energy stored in any deformed elastic member is equal to the area under the curve (line) in the load-deflection characteristics of this member.

Potential energy in our case is equal to the area enclosed by the triangle:

$$E_{P,1} = \frac{1}{2}(k_y y)y = \frac{1}{2}k_y y^2 \quad E_{P,2} = \frac{1}{2}(k_\phi \phi)\phi = \frac{1}{2}k_\phi \phi^2$$

The total potential energy: $E_P = \frac{1}{2}k_y y^2 + \frac{1}{2}k_\phi \phi^2$

2DOF wing example (Lagrange)

Kinetic energy:

- General motion in 2D

- vertical CM motion characterized by y_{CM} $E_{K,1} = \frac{1}{2}m(\dot{y} + \dot{\phi}x_{CM})^2$

- rotation about CM characterized by ϕ $E_{K,2} = \frac{1}{2}I_{CM}\dot{\phi}^2$

The total potential energy: $E_K = \frac{1}{2}m(\dot{y}^2 + 2\dot{y}\dot{\phi}x_{CM} + \dot{\phi}^2x_{CM}^2) + \frac{1}{2}I_{CM}\dot{\phi}^2$

Lagrangian using generalized coordinates: $\mathcal{L} = E_K - E_p$

$$\mathcal{L} = E_K - E_p = \frac{1}{2}m(\dot{q}_1^2 + 2\dot{q}_1\dot{q}_2x_{CM} + \dot{q}_2^2x_{CM}^2) + \frac{1}{2}I_{CM}\dot{q}_2^2 - \frac{1}{2}k_yq_1^2 - \frac{1}{2}k_\phi q_2^2$$

\mathcal{L} is the function of the generalized coordinates (displacements), velocities and all system parameters.

$$\mathcal{L} = \mathcal{L}(q_1, q_2, \dot{q}_1, \dot{q}_2; m, I_{CM}, x_{CM}, k_y, k_\phi)$$

2DOF wing example (Lagrange)

Lagrange's equations: $\frac{d}{dt}\left(\frac{\partial \mathcal{L}}{\partial \dot{q}_j}\right) - \frac{\partial \mathcal{L}}{\partial q_j} = Q_j \quad j=1,2$

Lagrangian: $\mathcal{L} = \frac{1}{2}m(\dot{q}_1^2 + 2\dot{q}_1\dot{q}_2x_{CM} + \dot{q}_2^2x_{CM}^2) + \frac{1}{2}I_{CM}\dot{q}_2^2 - \frac{1}{2}k_yq_1^2 - \frac{1}{2}k_\phi q_2^2$

Partial derivatives:

$$\frac{\partial \mathcal{L}}{\partial \dot{q}_1} = m\dot{q}_1 + \dot{q}_2mx_{CM} \quad \frac{\partial \mathcal{L}}{\partial q_1} = -k_yq_1$$

$$\frac{\partial \mathcal{L}}{\partial \dot{q}_2} = \dot{q}_1mx_{CM} + \dot{q}_2mx_{CM}^2 + I_{CM}\dot{q}_2 \quad \frac{\partial \mathcal{L}}{\partial q_2} = -k_\phi q_2$$

Substituting all relationships into Lagrange's equations:

$$\frac{d}{dt}(m\dot{q}_1 + \dot{q}_2mx_{CM}) + k_yq_1 = Q_1 \quad \Rightarrow m\ddot{q}_1 + m\dot{q}_2\ddot{x}_{CM} + k_yq_1 = Q_1$$

$$\frac{d}{dt}(m\dot{q}_1x_{CM} + (I_{CM} + m\dot{q}_1^2x_{CM}^2)\dot{q}_2) + k_\phi q_2 = Q_2 \quad \Rightarrow m\dot{q}_1\ddot{x}_{CM} + (I_{CM} + m\dot{q}_1^2x_{CM}^2)\ddot{q}_2 + k_\phi q_2 = Q_2$$

2DOF wing example (Lagrange)

Generalized loads are determined using the *equivalency* between the total power generated by the applied loads (moments, forces) and the total power produced by the generalized loads and their corresponding generalized velocities.

$$P = Q_1 \dot{q}_1 + Q_2 \dot{q}_2$$

$$P = L \dot{y}_{AC} + M \dot{\phi} = L(\dot{y} + \dot{\phi} x_{AC}) + M \dot{\phi} = L \dot{y} + (M + L x_{AC}) \dot{\phi} = L \dot{q}_1 + (M + L x_{AC}) \dot{q}_2$$

From this: $m \ddot{q}_1 + m x_{CM} \ddot{q}_2 + k_y q_1 = L$

$$m x_{CM} \ddot{q}_1 + (I_{CM} + m x_{CM}^2) \ddot{q}_2 + k_\phi q_2 = M + L x_{AC}$$

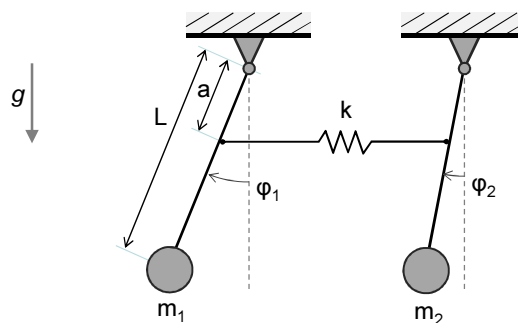
Matrix form of the EOM:

$$\begin{bmatrix} m & m x_{CM} \\ m x_{CM} & I_{CM} + m x_{CM}^2 \end{bmatrix} \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{bmatrix} + \begin{bmatrix} k_y & 0 \\ 0 & k_\phi \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \end{bmatrix} = \begin{bmatrix} L \\ M_{AC} + L x_{AC} \end{bmatrix}$$

After this step (*modelling*), one would typically perform *analysis* of the EOMs, e.g. calculate **M** and **K** and perform eigenvalue or harmonic response analysis (see L12-14), performance and design analyses (see L15,16) etc.

2 coupled pendulums (Lagrange)

Consider the two coupled pendulums. Derive EOMs for this 2DOF system.



DOFs: 2 (ϕ_1, ϕ_2)

Small angle assumption: $\cos\phi=1$, $\sin\phi=\phi$

2 coupled pendulums (Lagrange)

Number of DOFs: 2 = pendulum 1 rotation + pendulum 2 rotation

Generalized coordinates: $q_1 = \varphi_1$, $q_2 = \varphi_2$; use positive orientations

Potential energy due to deformed spring, assume $\varphi_1 > \varphi_2$:

$$E_{p,1} = \frac{1}{2} k \Delta^2 = \frac{1}{2} k (a\varphi_1 - a\varphi_2)^2 = \frac{1}{2} k a^2 (\varphi_1^2 - 2\varphi_1\varphi_2 + \varphi_2^2) = \frac{1}{2} k a^2 (q_1^2 - 2q_1q_2 + q_2^2)$$

Potential energy due to gravity increases with increasing φ and has the form: (mass \times g \times height), where *height* represents the height of the mass from the reference position (e.g. equilibrium position):

$$E_{p,2} = m_1 g \Delta h_1 = m_1 g (L - L \cos \varphi_1) = m_1 g L (1 - \cos q_1)$$

$$E_{p,3} = m_2 g \Delta h_2 = m_2 g (L - L \cos \varphi_2) = m_2 g L (1 - \cos q_2)$$

The total potential energy:

$$E_p = \frac{1}{2} k a^2 (q_1^2 - 2q_1q_2 + q_2^2) + m_1 g L (1 - \cos q_1) + m_2 g L (1 - \cos q_2)$$

2 coupled pendulums (Lagrange)

Kinetic energy due to moving masses m_1 and m_2 :

Magnitude of the velocity = radius of the circular trajectory \times angular speed

$$|\mathbf{v}_1| = L \dot{\varphi}_1, \quad |\mathbf{v}_2| = L \dot{\varphi}_2$$

The total kinetic energy:

$$E_K = E_{K,1} + E_{K,2} = \frac{1}{2} m_1 |\mathbf{v}_1|^2 + \frac{1}{2} m_2 |\mathbf{v}_2|^2 = \frac{1}{2} m_1 L^2 \dot{\varphi}_1^2 + \frac{1}{2} m_2 L^2 \dot{\varphi}_2^2 = \frac{1}{2} m_1 L^2 \dot{q}_1^2 + \frac{1}{2} m_2 L^2 \dot{q}_2^2$$

Lagrangian: $\mathcal{L} = E_K - E_p$

$$\mathcal{L} = \frac{1}{2} m_1 L^2 \dot{q}_1^2 + \frac{1}{2} m_2 L^2 \dot{q}_2^2 - \frac{1}{2} k a^2 (q_1^2 - 2q_1q_2 + q_2^2) - m_1 g L (1 - \cos q_1) - m_2 g L (1 - \cos q_2)$$

Partial derivatives (assume small angles φ_i):

$$\frac{\partial \mathcal{L}}{\partial \dot{q}_1} = m_1 L^2 \dot{q}_1 \quad \frac{\partial \mathcal{L}}{\partial q_1} = -k a^2 (q_1 - q_2) - m_1 g L \sin q_1 \approx -k a^2 (q_1 - q_2) - m_1 g L q_1$$

$$\frac{\partial \mathcal{L}}{\partial \dot{q}_2} = m_2 L^2 \dot{q}_2 \quad \frac{\partial \mathcal{L}}{\partial q_2} = -k a^2 (-q_1 + q_2) - m_2 g L \sin q_2 \approx -k a^2 (-q_1 + q_2) - m_2 g L q_2$$

2 coupled pendulums (Lagrange)

Substituting all relationships into Lagrange's equations:

$$\left. \begin{aligned} \frac{d}{dt}(m_1 L^2 \dot{q}_1) + ka^2(q_1 - q_2) + m_1 g L q_1 &= Q_1 = 0 \\ \frac{d}{dt}(m_2 L^2 \dot{q}_2) + ka^2(-q_1 + q_2) + m_2 g L q_2 &= Q_2 = 0 \end{aligned} \right\} \begin{array}{l} \text{Note zero generalized loads} \\ Q_i, \text{ no external loads are} \\ \text{applied, therefore free} \\ \text{vibrations problem} \end{array}$$

Matrix form of the EOM:

$$\begin{bmatrix} m_1 L^2 & 0 \\ 0 & m_2 L^2 \end{bmatrix} \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{bmatrix} + \begin{bmatrix} ka^2 + m_1 g L & -ka^2 \\ -ka^2 & ka^2 + m_2 g L \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

Usual other problem solving tasks:

- Substitute numerical values and determine **M** and **K**
- Eigenvalue analysis (e.g. via characteristic equation / determinant)
- Eigenvalues / natural frequencies
- Eigenvalue problem, use computed eigenvalues and determine eigenvectors
- ...

Summary

- Modelling using Lagrange's equations and further analysis:
 - DOFs, generalized coordinates
 - kinetic and potential energy, Lagrangian
 - partial and time derivatives, generalized loads
 - EOMs, matrix format (if linear problem), **K** and **M**
 - Eigenvalues, eigenvectors
 - Free, harmonic or general time response
 - Aero-elastic analyses (divergence, reversal, gust, flutter, loads, etc.)