

Lecture 13 review

Free vibration response via modal superposition:

$$\mathbf{x} = C_1 \mathbf{a}_1 \cos(\omega_1 t + \varphi_1) + C_2 \mathbf{a}_2 \cos(\omega_2 t + \varphi_2) + \dots$$

Initial conditions used to determine the unknown free response constants:

$$t = 0 : \mathbf{x}(0) = \mathbf{x}_0, \ \dot{\mathbf{x}}(0) = \dot{\mathbf{x}}_0$$

Free harmonic vibration:

$$t = 0 : \mathbf{x}(0) = \alpha \mathbf{a}_i, \ \dot{\mathbf{x}}(0) = 0$$

University of BRISTOL

L14

2

DEPARTMENT OF

Lecture 14

- · Harmonic excitation or forcing
- Steady-state harmonic vibration response
- · Amplitude-frequency characteristics



L14

3

DEPARTMENT OF aerospace engineering

Harmonic excitation

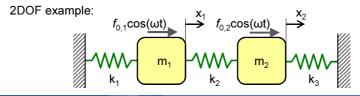
Consider a forced MDOF system:

$$\mathbf{M}\ddot{\mathbf{x}} + \mathbf{K}\mathbf{x} = \mathbf{f}(\mathbf{t})$$

and assume that the harmonic load is defined as follows:

$$\mathbf{f}(\mathbf{t}) = \begin{bmatrix} f_{0,1} \cos(\omega \, \mathbf{t}) \\ \dots \\ f_{0,M} \cos(\omega \, \mathbf{t}) \end{bmatrix} = \begin{bmatrix} f_{0,1} \\ \dots \\ f_{0,M} \end{bmatrix} \cos(\omega \, \mathbf{t}) = \mathbf{f}_0 \cos(\omega \, \mathbf{t})$$

where \boldsymbol{f}_0 is the vector of excitation amplitudes, $\boldsymbol{\omega}$ is the excitation frequency



University of BRISTOI

L14

EPARTMENT OF

Steady-state harmonic response

We study the steady-state response of MDOF system with harmonic excitation:

$$\mathbf{M}\ddot{\mathbf{x}} + \mathbf{K}\mathbf{x} = \mathbf{f}_0 \cos(\omega t)$$

The response is assumed in the following form:

$$\mathbf{x} = \mathbf{x}_0 \cos(\omega t) \Rightarrow \ddot{\mathbf{x}} = -\omega^2 \mathbf{x}_0 \cos(\omega t)$$

 \mathbf{x}_0 is the vector of (*unknown*) response amplitudes, ω is the (*known*) excitation frequency. The phase angle is 0 or 90 degrees (in-phase or out-of phase). This information is be captured by the signs of the components of \mathbf{x}_0 .

The vector of the response amplitudes is found after the following substitutions:

$$-\omega^{2}\mathbf{M} \ \mathbf{x}_{0} \cos(\omega t) + \mathbf{K} \ \mathbf{x}_{0} \cos(\omega t) = \mathbf{f}_{0} \cos(\omega t)$$
$$(\mathbf{K} - \omega^{2}\mathbf{M}) \ \mathbf{x}_{0} = \mathbf{f}_{0}$$
$$\mathbf{x}_{0} = (\mathbf{K} - \omega^{2}\mathbf{M})^{-1} \mathbf{f}_{0}$$

where (...)-1 denotes inverse matrix.



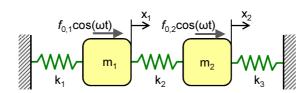
L14

5

aerospace engineerin

2DOF example

Consider the following 2DOF system. Determine its harmonic response:



Mass matrix, stiffness matrix and excitation vector:

$$\mathbf{M} = \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \quad \mathbf{K} = \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 + k_3 \end{bmatrix} \quad \mathbf{f} = \begin{bmatrix} f_{0,1} \\ f_{0,2} \end{bmatrix} \cos(\omega t)$$

University of BRISTOI

L14

6

DEPARTMENT OF

2DOF example

The system of equations for this example is:

$$(\mathbf{K} - \omega^2 \mathbf{M}) \mathbf{x}_0 = \mathbf{f}_0$$

$$\begin{bmatrix} k_1 + k_2 - \omega^2 m_1 & -k_2 \\ -k_2 & k_2 + k_3 - \omega^2 m_2 \end{bmatrix} \begin{bmatrix} x_{0,1} \\ x_{0,2} \end{bmatrix} = \begin{bmatrix} f_{0,1} \\ f_{0,2} \end{bmatrix}$$

Matrix inverse for matrices of size 2×2 is:

$$\mathbf{A}^{-1} = \begin{bmatrix} A & B \\ C & D \end{bmatrix}^{-1} = \frac{1}{\det(\mathbf{A})} \begin{bmatrix} D & -B \\ -C & A \end{bmatrix} = \frac{1}{AD - CB} \begin{bmatrix} D & -B \\ -C & A \end{bmatrix}$$

The steady-state amplitudes of response are:

$$\begin{bmatrix} x_{0,1} \\ x_{0,2} \end{bmatrix} = \frac{1}{\det(\mathbf{K} - \omega^2 \mathbf{M})} \begin{bmatrix} k_2 + k_3 - \omega^2 m_2 & k_2 \\ k_2 & k_1 + k_2 - \omega^2 m_1 \end{bmatrix} \begin{bmatrix} f_{0,1} \\ f_{0,2} \end{bmatrix}$$
$$\det(\mathbf{K} - \omega^2 \mathbf{M}) = (k_1 + k_2 - \omega^2 m_1)(k_2 + k_3 - \omega^2 m_2) - k_2^2$$



L14

7

DEPARTMENT O

2DOF example

From the previous derivations, we can show that $x_{0,1}$ and $x_{0,2}$ are functions of ω

$$x_{0,1}(\omega) = \frac{(k_2 + k_3 - \omega^2 m_2) f_{0,1} + k_2 f_{0,2}}{\det(\mathbf{K} - \omega^2 \mathbf{M})}$$

$$x_{0,2}(\omega) = \frac{k_2 f_{0,1} + (k_1 + k_2 - \omega^2 m_1) f_{0,2}}{\det(\mathbf{K} - \omega^2 \mathbf{M})}$$

In other words, the amplitudes of steady-state vibrations depend on the excitation frequency. These functions have singular values at the points where the excitation frequencies ω are equal to the natural frequencies ω_i . These points are defined as follows (see Eigenvalue Problem section):

$$\det(\mathbf{K} - \omega_i^2 \mathbf{M}) = 0$$

Based on this, the amplitudes of vibration reach infinite values if harmonically excited at one of the natural frequencies, i.e. *resonance/resonant excitation*:

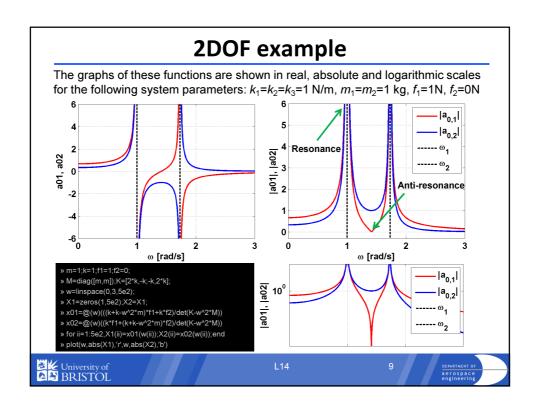
$$x_{0,1}(\omega_i) \to \pm \infty, \ x_{0,2}(\omega_i) \to \pm \infty$$

University of BRISTOI

L14

8

DEPARTMENT OF



Summary

- In linear systems: harmonic excitation causes steady-state harmonic vibration at the same frequency
- Amplitude-frequency response functions have important properties, 2DOF example:
 - 2DOF 2 resonant peaks
 - 2DOF 2 natural frequencies
 - 2DOF 2 mode shapes
 - 2DOF 1 anti-resonance

