

Advanced Bending and Torsion

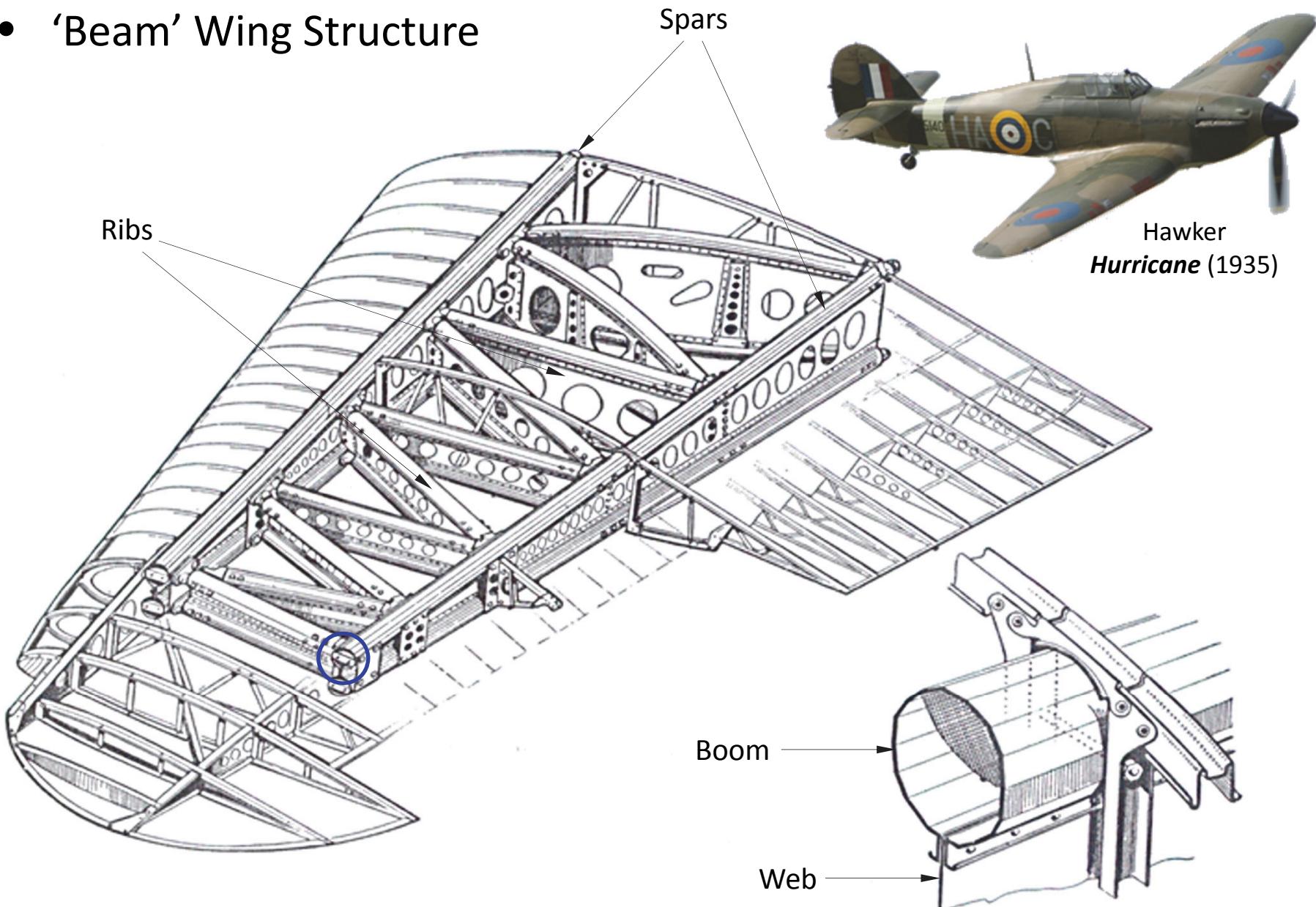
Unsymmetric Bending of Beams

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- ‘Beam’ Wing Structure



Hawker
Hurricane (1935)

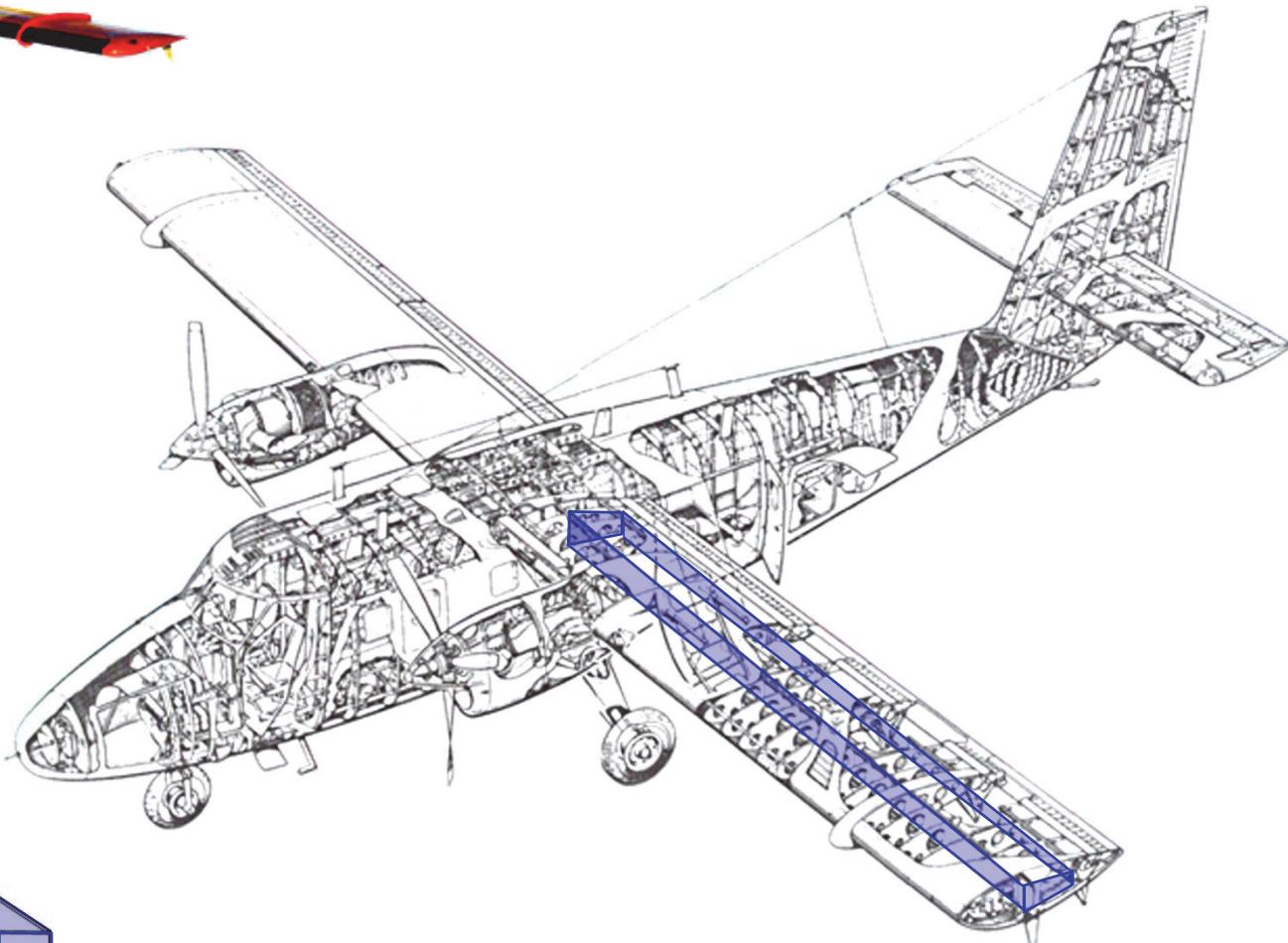
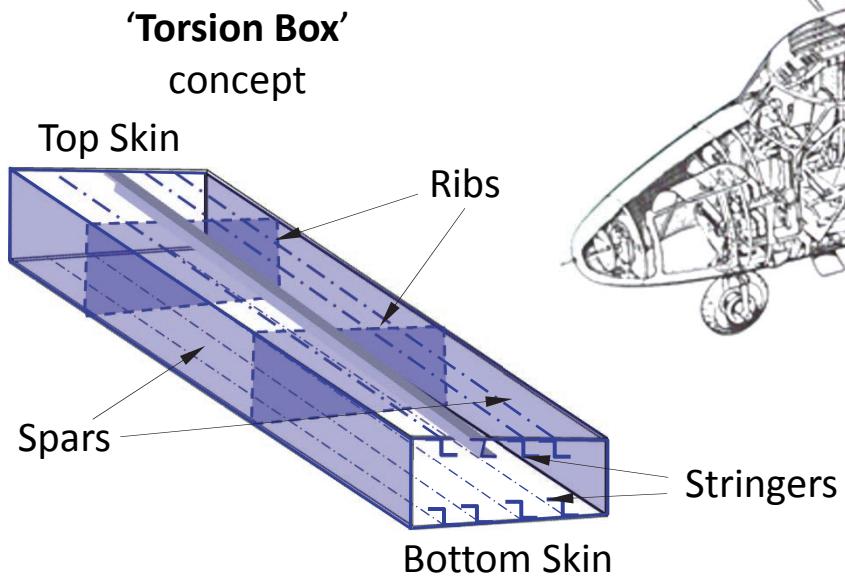
Advanced Bending & Torsion

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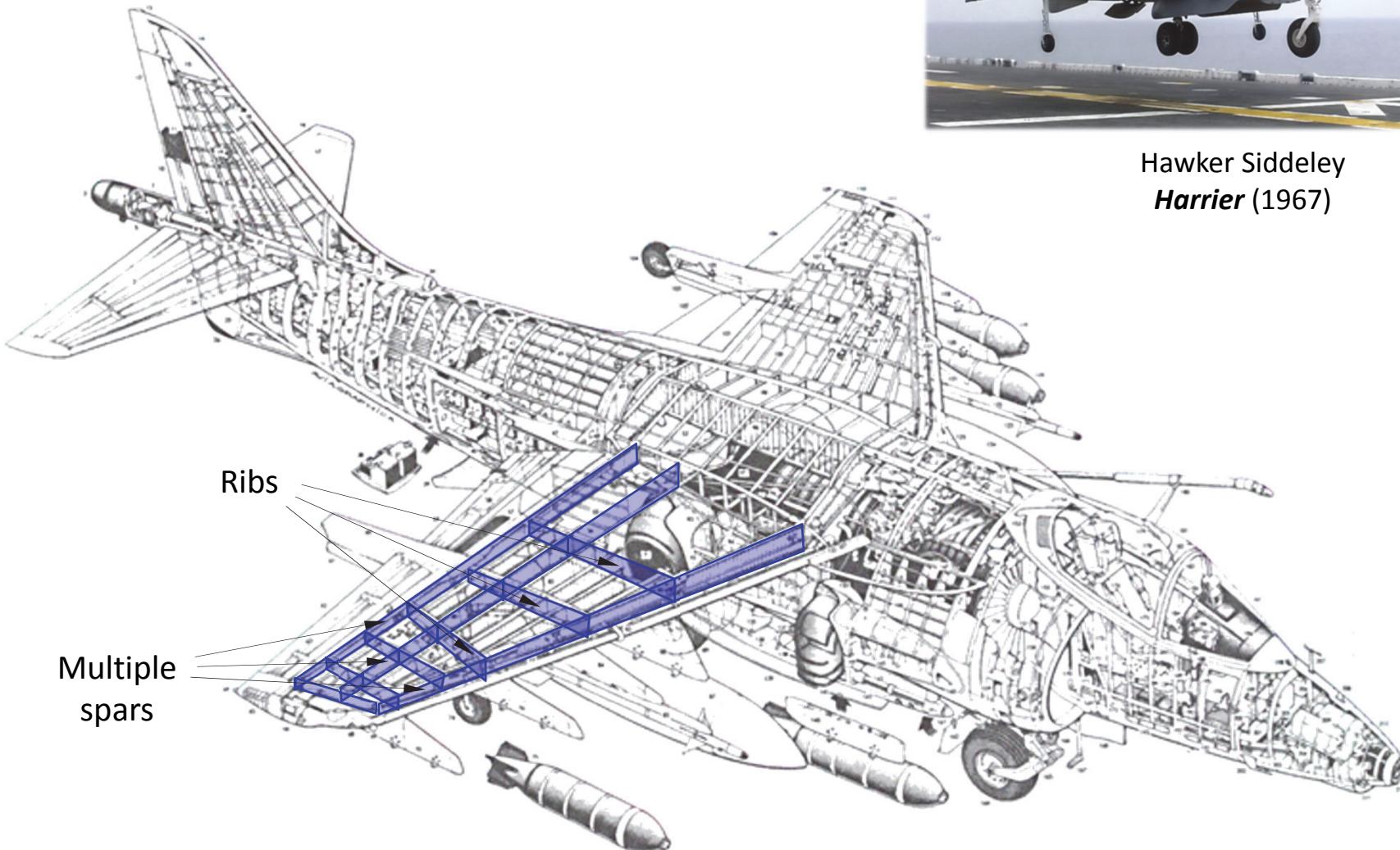
- 2-Spar Wing Box Structure



de Havilland
Canada Twin Otter (1966)



- Multi-Spar Wing Box Structure

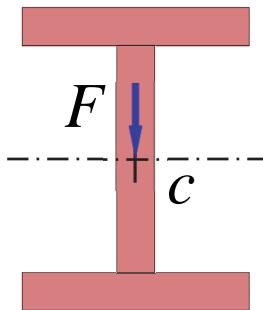


Hawker Siddeley
Harrier (1967)

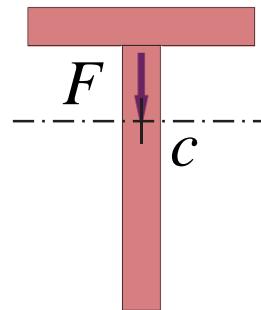
- Cross-sections of more complex shape, seen as an assembly of simpler sections – most often rectangular sections
- All ‘parts’ are perfectly bonded together – *i.e.* via welding or adhesive bonding

Classic compound cross-sections:

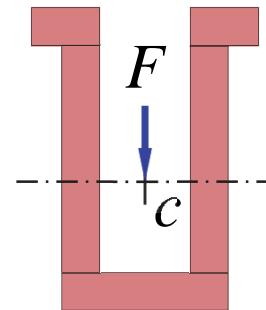
I-section beam



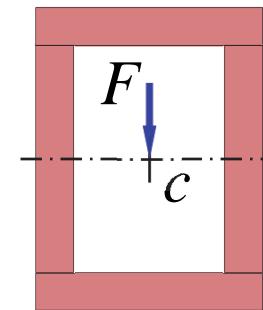
T-section beam



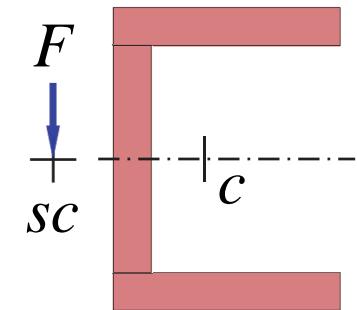
U-section beam



Box beam



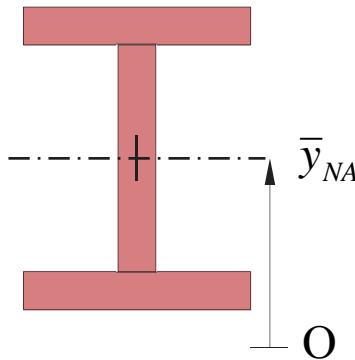
C-section beam



- **Webs** are elements **parallel** with main transverse loading
- **Flanges** are elements **normal** to main transverse loading

- The **centroid of the compound section** is found by considering individual centroids w.r.t a ‘vertical’ coordinate \bar{y} of arbitrary origin:

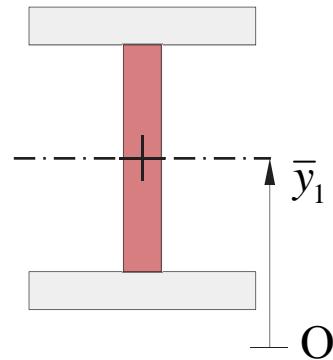
Compound section



Total area A

Centroid at \bar{y}_{NA}

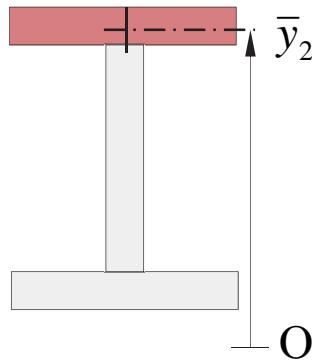
Part 1



Area A_1

Centroid at $\bar{y}_1 (= \bar{y}_{NA})$

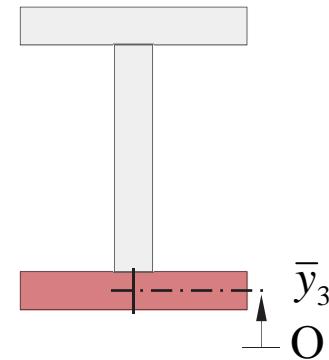
Part 2



Area A_2

Centroid at \bar{y}_2

Part 3



Area A_3

Centroid at \bar{y}_3

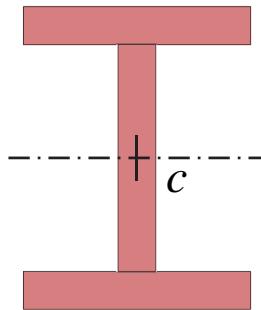
- The first moment of area gives:

$$A \bar{y}_{NA} = \sum_i (A_i \bar{y}_i) \quad \therefore$$

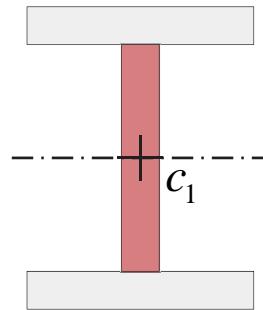
$$\bar{y}_{NA} = \frac{\sum_i (A_i \bar{y}_i)}{\sum_i (A_i)}$$

- We decompose the compound cross section into simple sections identified by an index i :

Compound section

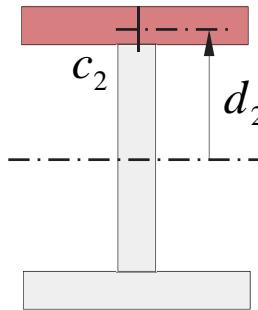


Part 1



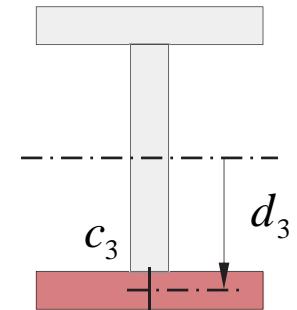
Area A_1
Centroid c_1
SMA I_1
Distance $d_1 (= 0)$

Part 2



Area A_2
Centroid c_2
SMA I_2
Distance d_2

Part 3



Area A_3
Centroid c_3
SMA I_3
Distance d_3

- The contribution of each ‘section’ i to the compound I_{NA} is:

$$I_{i,ZZ} = I_i + A_i (d_i)^2$$

- And the final compound I_{NA} is:

$$I_{NA} = \sum_i (I_{i,ZZ}) = \sum_i [I_i + A_i (d_i)^2]$$

- The theorem is derived directly from the **2nd moment of area**:

$$I_i = \int_{y_1}^{y_2} y^2 b_{(y)} dy$$

(2nd moment of area of a 'part' w.r.t. its own centroid)

$$I_{zz} = \int_{y_1}^{y_2} (y + \bar{y})^2 b_{(y)} dy$$

(2nd moment of area of a 'part' w.r.t. the compound centroid)

$$I_{zz} = \int_{y_1}^{y_2} (y^2 + 2 y \bar{y} + \bar{y}^2) b_{(y)} dy$$

(Origin of \bar{y} , for convenience)

$$I_{zz} = \int_{y_1}^{y_2} y^2 b_{(y)} dy + 2 \bar{y} \int_{y_1}^{y_2} y b_{(y)} dy + \bar{y}^2 \int_{y_1}^{y_2} b_{(y)} dy$$

I_i

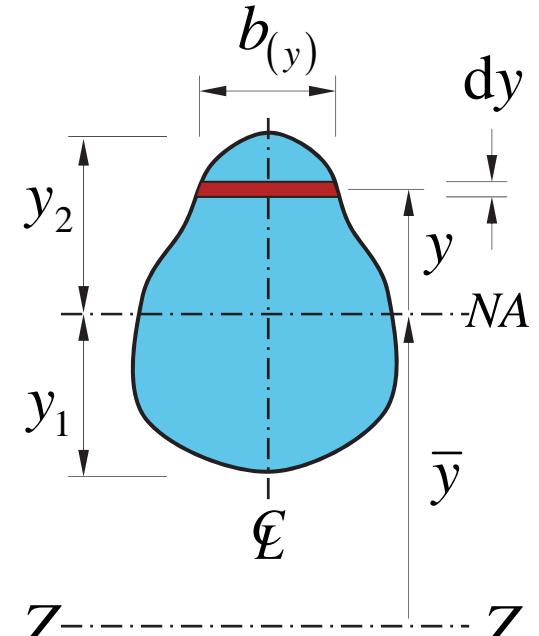
y_1 y_2

1^{st} moment of area

d_i^2

A_i

(Imagine that this shape is now only one 'part' i of a compound section)

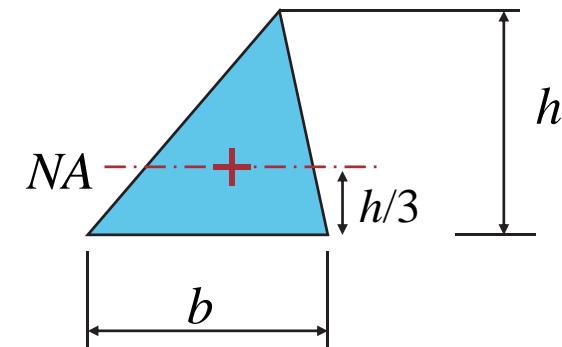
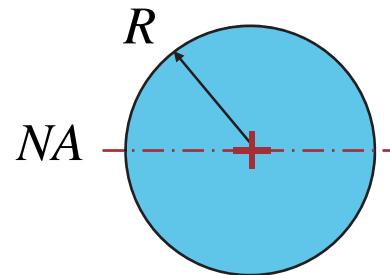
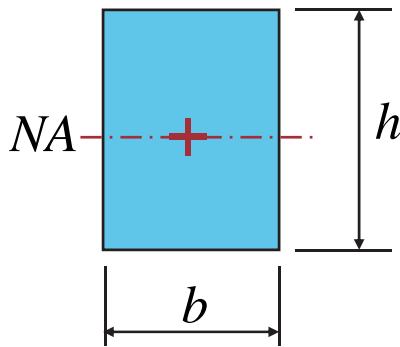


$$I_{i,zz} = I_i + A_i (d_i)^2$$

Engineer's theory of bending

$$-\frac{\sigma}{y} = \frac{M}{I} = \frac{E}{R}$$

Basic 2nd moments
of area



$$I_{NA} = \frac{b h^3}{12}$$

$$I_{NA} = \frac{\pi R^4}{4}$$

$$I_{NA} = \frac{b h^3}{36}$$

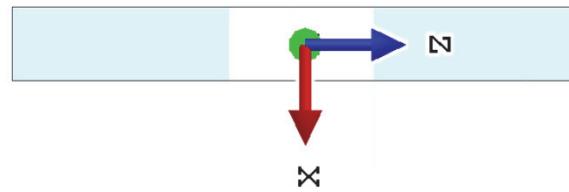
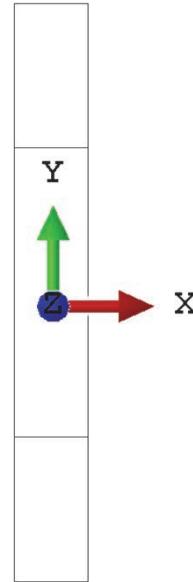
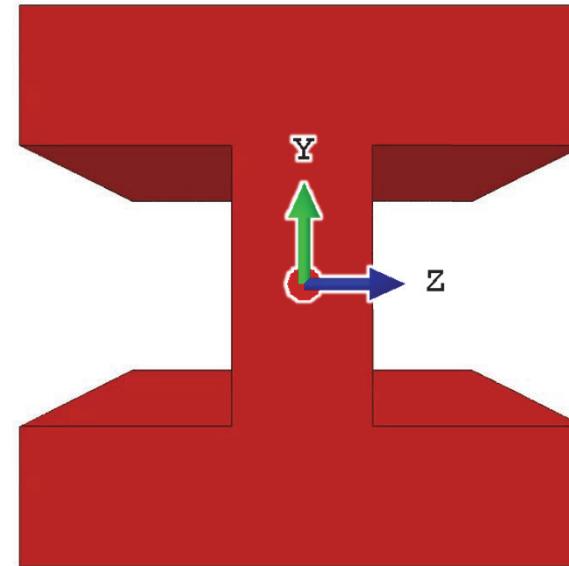
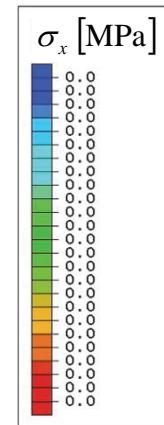
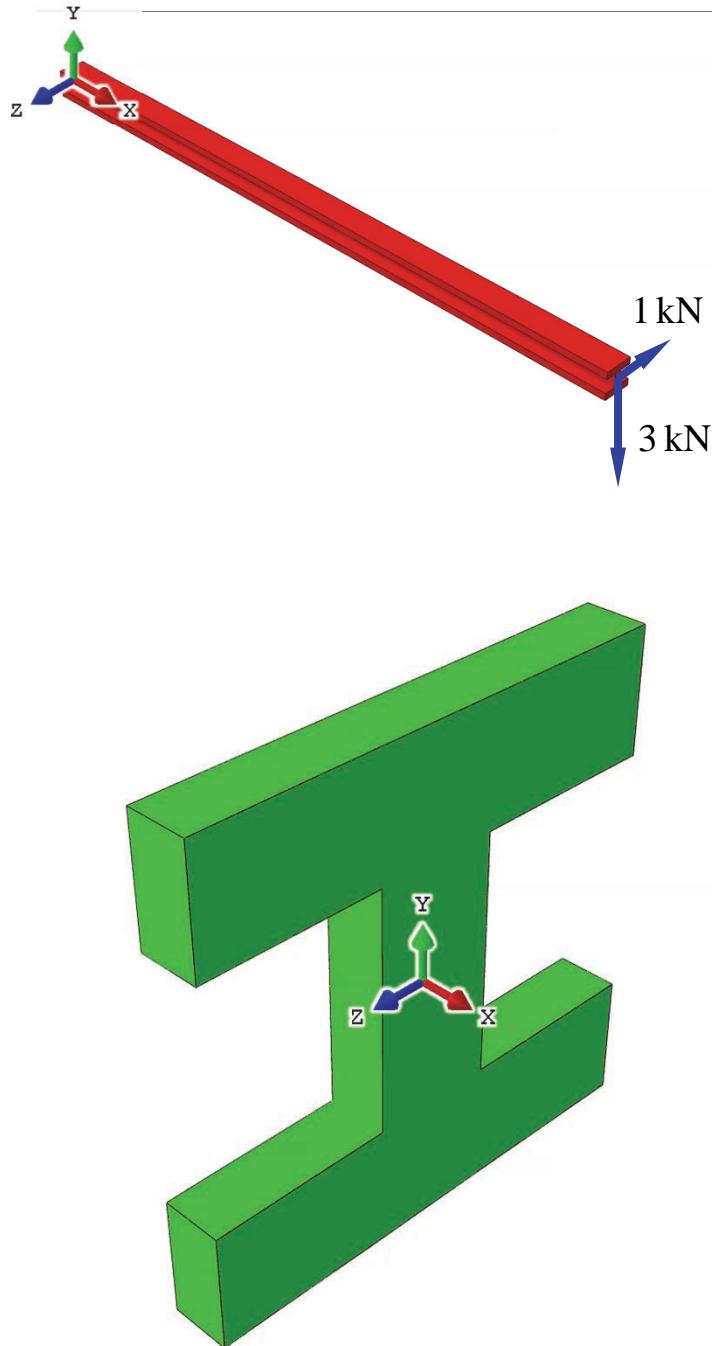
Parallel axis theorem

$$\bar{y}_{NA} = \frac{\sum_i (A_i \bar{y}_i)}{\sum_i (A_i)}$$

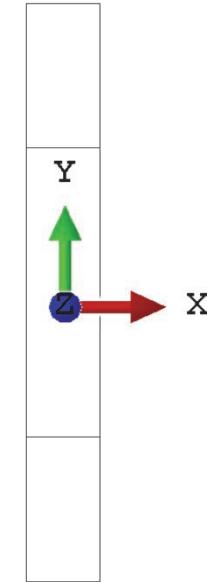
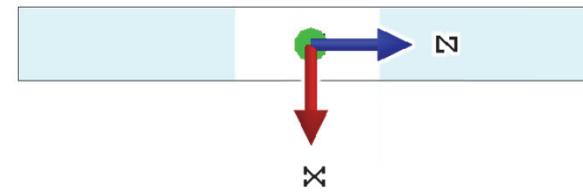
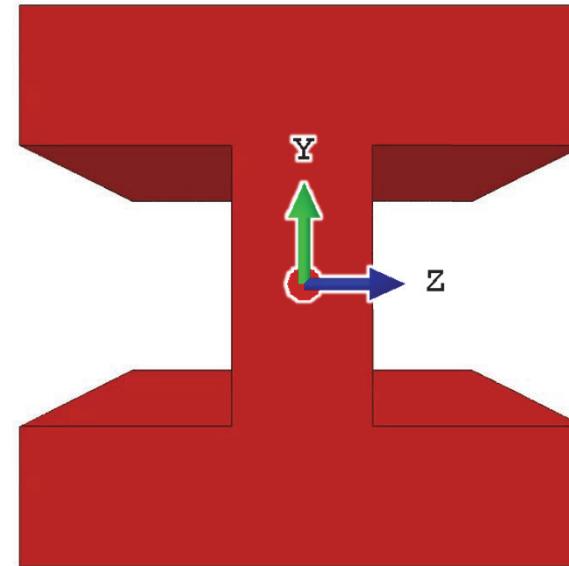
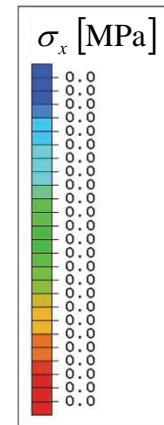
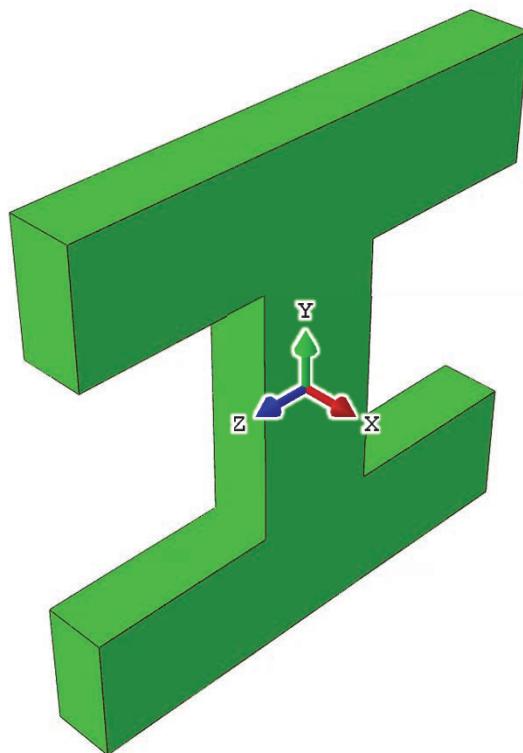
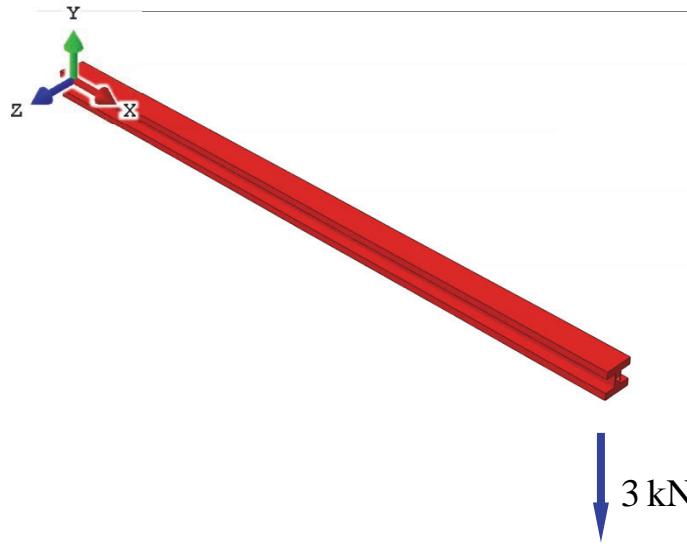
$$d_i = \bar{y}_i - \bar{y}_{NA}$$

$$I_{NA} = \sum_i [I_i + A_i (d_i)^2]$$

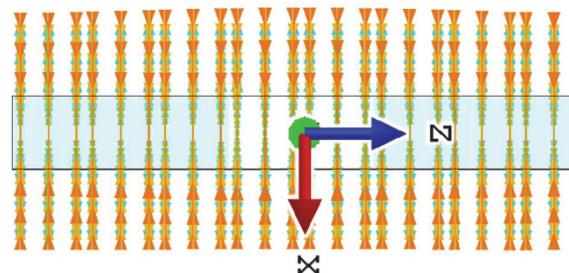
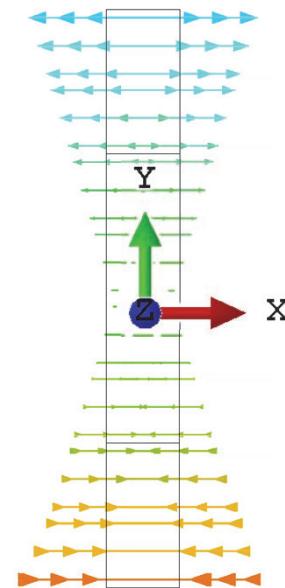
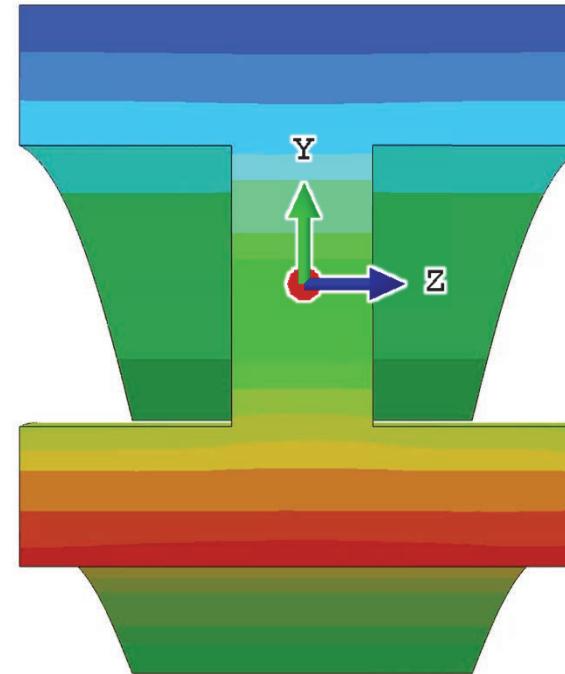
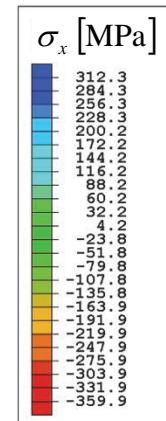
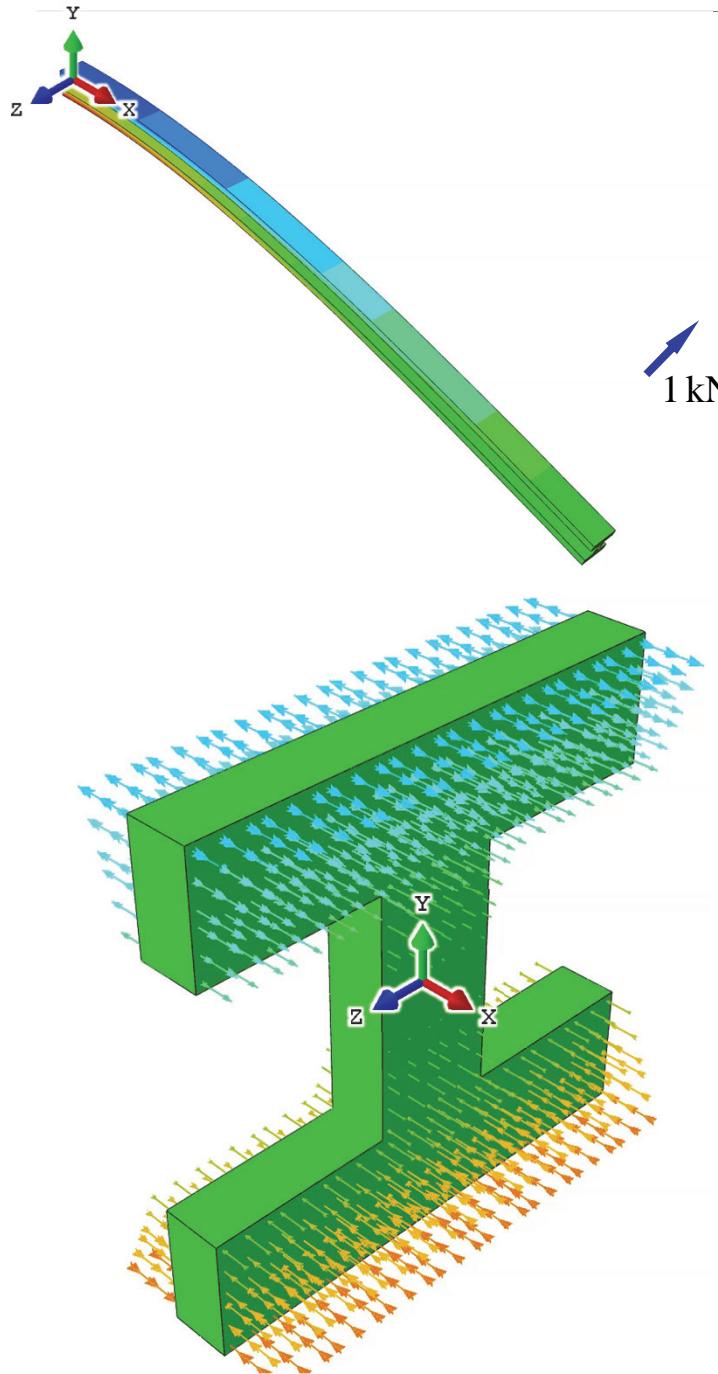
I-section beam in combined bending



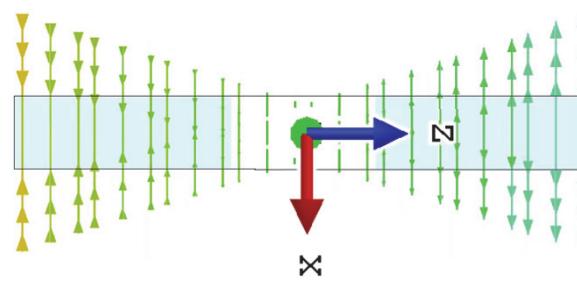
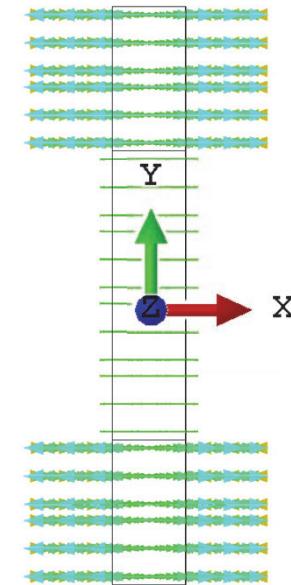
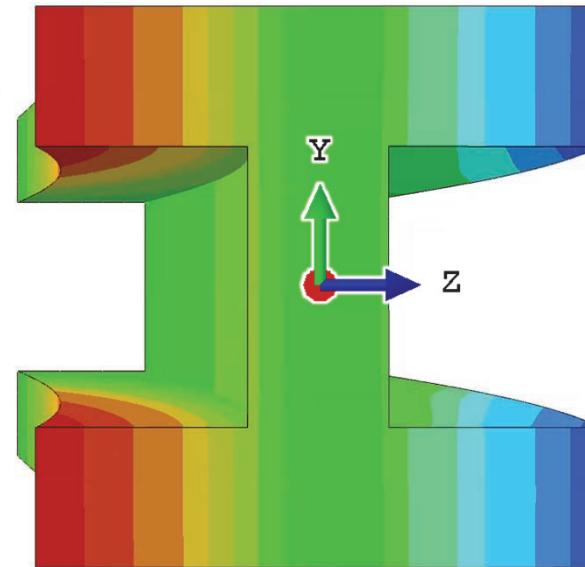
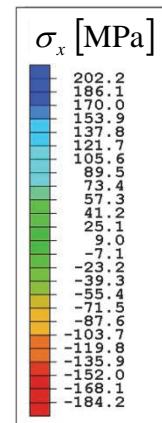
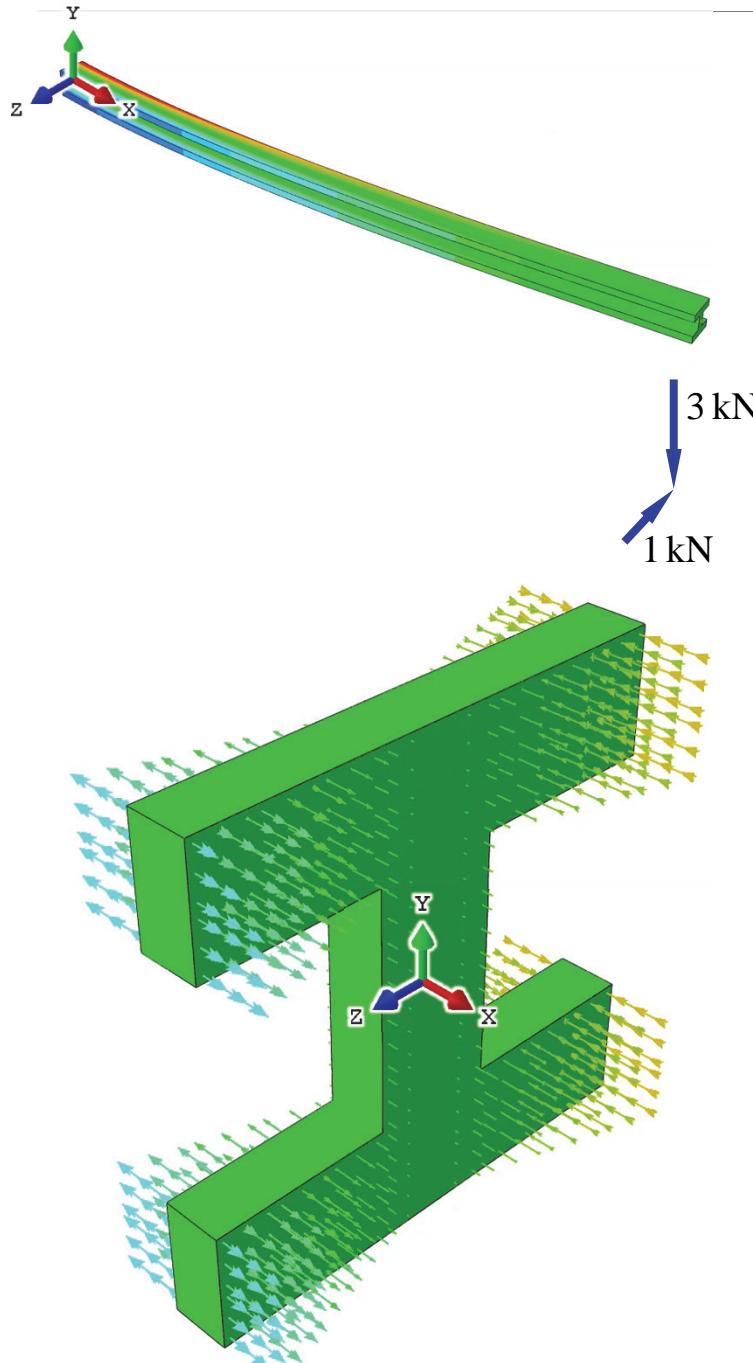
I-section beam in combined bending



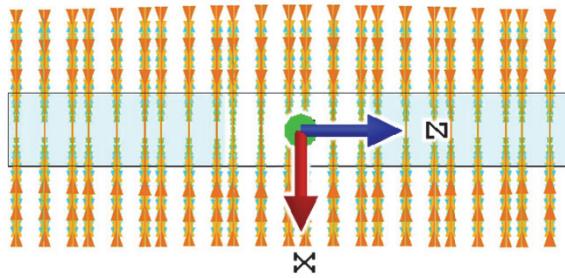
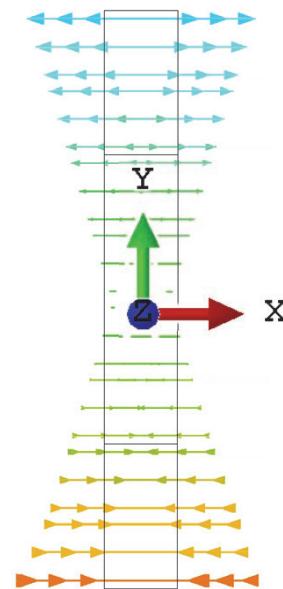
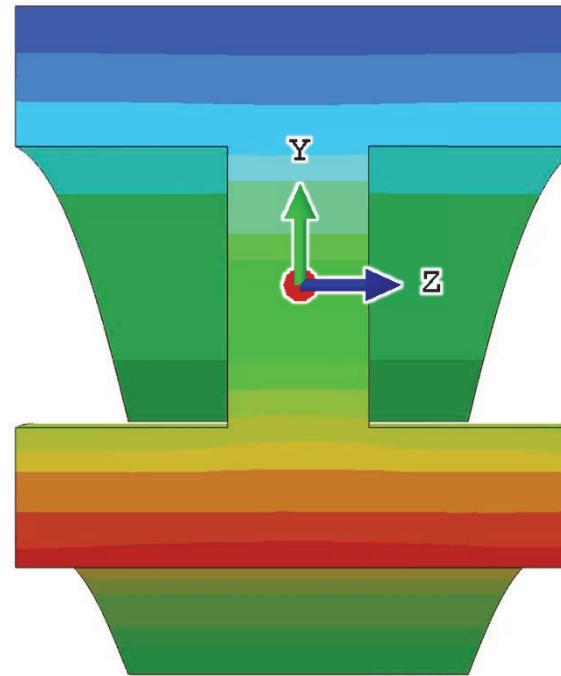
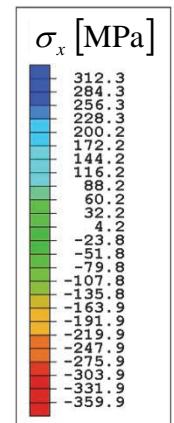
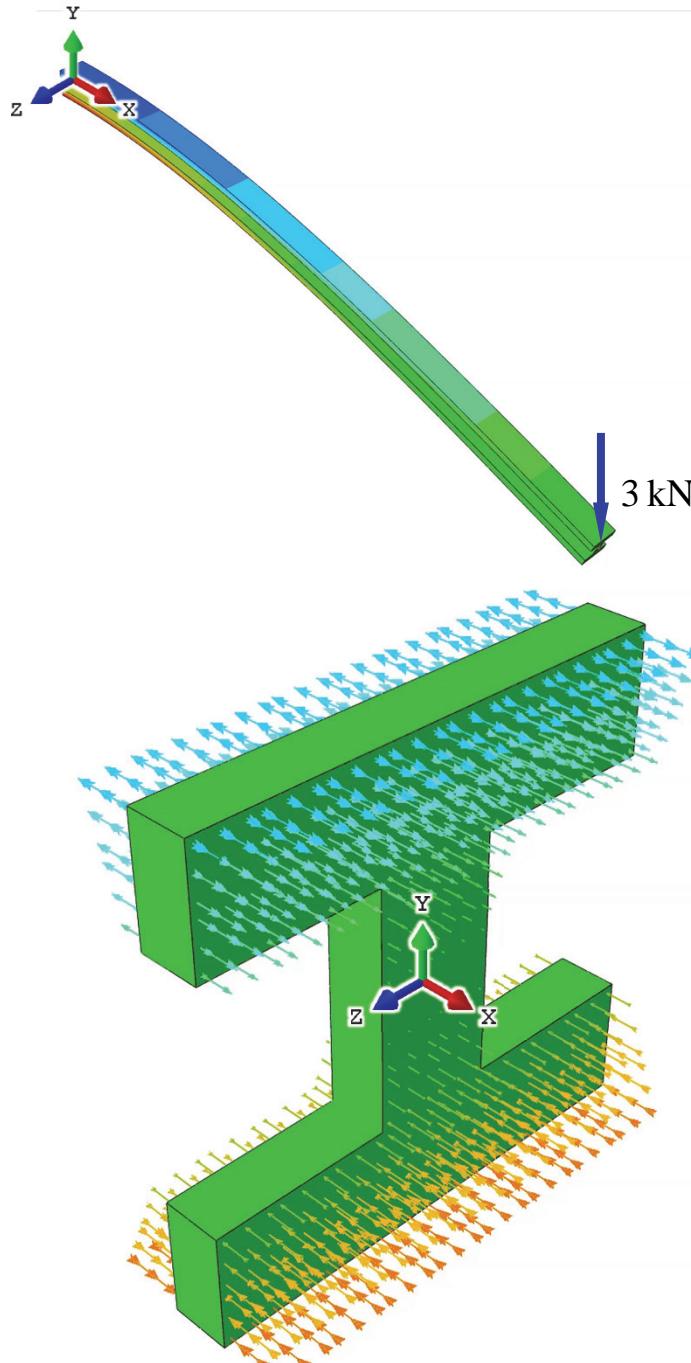
I-section beam in combined bending



I-section beam in combined bending

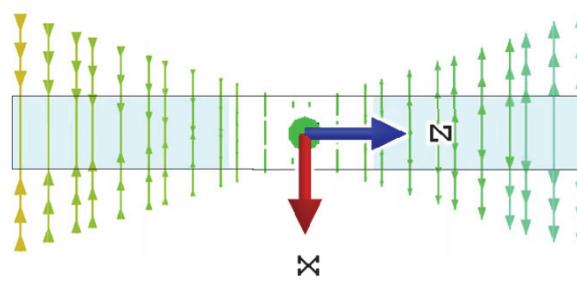
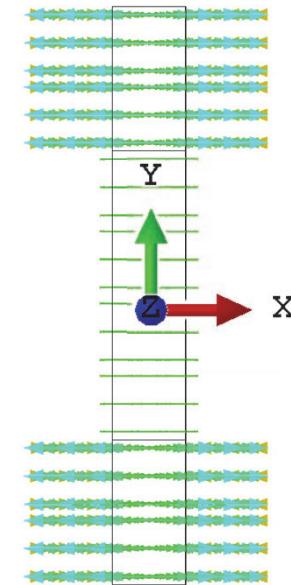
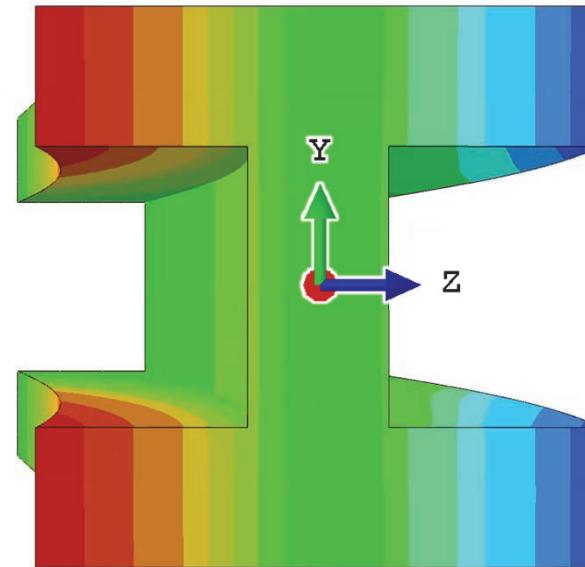
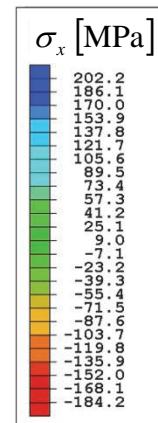
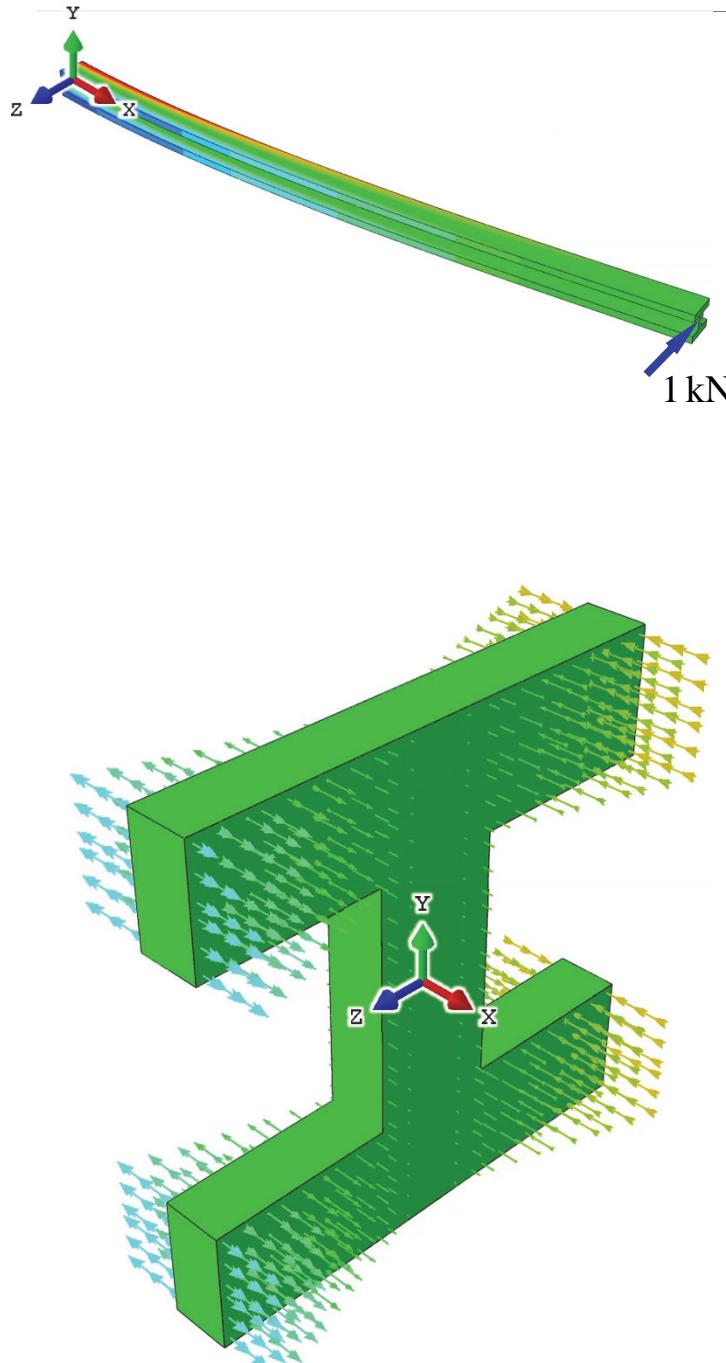


I-section beam in combined bending



I-section beam in combined bending

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I-section beam in combined bending

