The Turbojet Cycle (Lecture 4/4)

Thrust from gas cycles.

Contents

- The Turbojet Cycle "modified Brayton (Joule)"- worked example to estimate thrust
- 10. The Turbofan Cycle (Brief notes)

Objectives

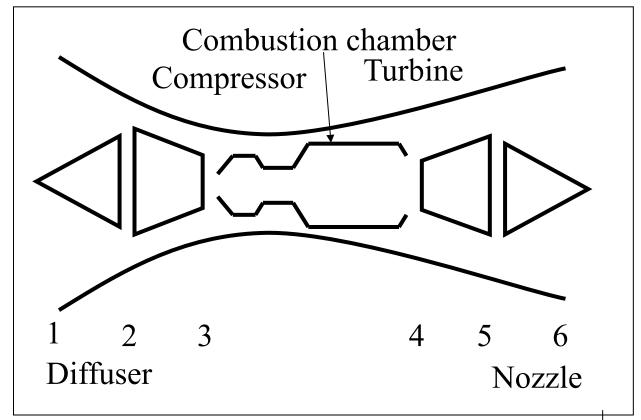
Identify specific processes that are in addition to Brayton – diffuser, nozzle, thrust.

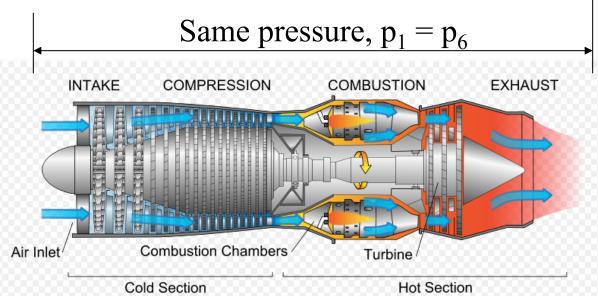
<u>Application</u>

Turbojet – oldest type of jet engine (Whittle). Messerschmidt ME262, De Havilland Comet, Concord

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Sketch and graphic (from Wikipedia!)



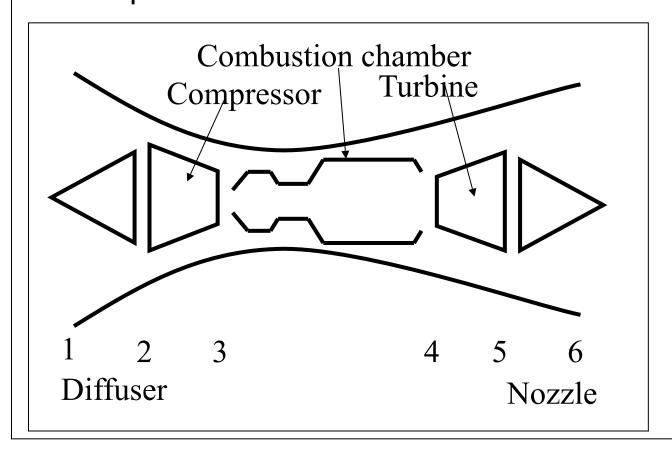


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Resembles Brayton (Joule).

Produces thrust (vs work)

- Diffuser (1-to-2) decellerates incoming air,
 v₂ ~ 0 m s⁻¹
- Nozzle (5-to-6) accelerates exit air until p₆
 = p₁ Assume v₅ ~ 0 m s⁻¹.
- Turbine produces sufficient work to drive compressor – no more.



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Thrust = rate of change of momentum (Newton #2), so

$$F = m v_6 - m v_1 = m (v_6 - v_1) (25)$$

Momentum flow, owing to air leaving the system boundary

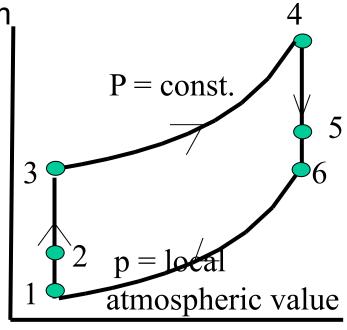
Momentum flow, owing to air entering the system boundary

Quote all velocities relative to airframe. Term $v_1 \approx airframe \ velocity$

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Shown as T-s diagram

T



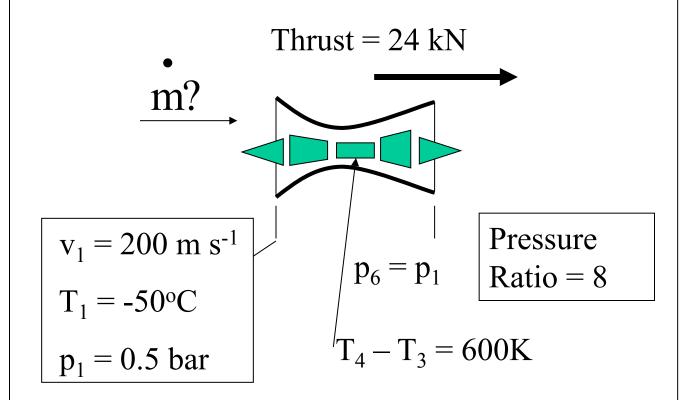
Worked example

S

Statement: Air throughput giving specified thrust.

Schematic: - Ts diagram plus ...

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<u>Assumptions</u>: v_2 , $v_5 \sim 0$. Internally reversible processes throughout. Adiabatic processes (other than "combustor"). Ignore KE and PE changes in turbine and compressor. Turbine transmits work perfectly.

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Properties: $c_p = 1.005 \text{ kJ kg}^{-1} \text{ K}^{-1}$

Physical Laws: isentropic expansion/compression in nozzle, diffuser, compressor, turbine so $p/T^{\gamma/\gamma-1} = constant$. SFEE relates enthalpy change to KE change in nozzle and diffuser

Calculations:

Enthalpy and KE

Diffuser – manipulate SFEE ⇒ T_2 = -30.1°C = 243 K

$$T_2 = T_1 + \frac{v_1^2}{2c_p}$$

$$p_2 = p_1 (T_2/T_1)^{\gamma/\gamma-1} = 1.351 p_1$$

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Given as 8

Compressor –
$$T_3 = (p_3 / p_2)^{(\gamma-1)/\gamma} T_2 = 440 \text{ K}$$

$$p_3 = 8 p_2 = 10.81 p_1$$
 Given

Combustor -
$$T_4 = 440 + 600 = 1040 \text{ K}$$

$$p_4 = p_3 = 10.81 p_1$$

Turbine- same work as comp, const c_p

$$T_3 - T_2 = T_4 - T_5 \Rightarrow \underline{T_5} = 843 \text{ K}$$

$$p_5 = p_4 (T_5/T_4)^{\gamma/\gamma-1} = (843/1040)^{3.5} \times 10.81 p_1$$

= $5.18 p_1$

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Nozzle - if
$$p_1 = p_6$$

$$T_6 = T_5 / (p_5/p_6)^{\gamma-1/\gamma} = 843/5.18^{1/3.5} = 527 \text{ K}$$

Apply SFEE, (assume $v_5 \sim 0$)

$$v_6 = \sqrt{2c_p(T_5 - T_6)} = \sqrt{2 \times 1005 \times (843 - 527)}$$

$$V_6 = 797 \text{ m s}^{-1}$$

Thrust

$$F=m(v_6-v_1) \Rightarrow$$

$$24000=m(797-200) \Rightarrow$$

$$m=40.2 \text{ kg s}^{-1}$$

The Turbojet Cycle (Lecture 4/4)

10. Turbofan

Very simply, the fan drives by-pass air/ Can prove more effective/ economic.

Conclusions

Differences with Brayton (Joule)— nozzle, diffuser, less turbine work.

Analysis – thoughtful application of

SFEE ,e.g.
$$0 = c_p \left(T_{end} - T_{start} \right) + \left(\frac{v_{end}^2}{2} - \frac{v_{start}^2}{2} \right)$$

$$\overset{\bullet}{W}$$
 or $\overset{\bullet}{Q} = \overset{\bullet}{m} c_p \left(T_{end} - T_{start} \right)$

Isentropic

$$T = const. p^{(\gamma-1)/\gamma}$$