# Advanced Bending and Torsion **Shear Centre of Complex Thin-Walled Sections**

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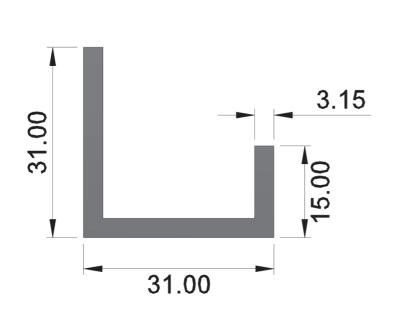
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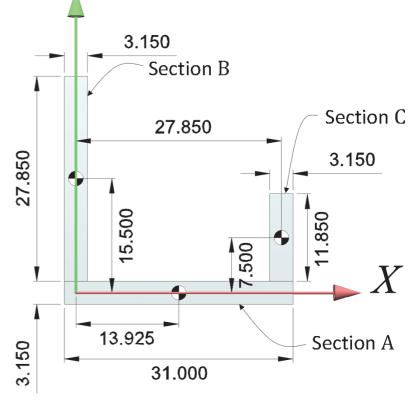
06 November 2018



## **Lipped Section Example**

Lipped section seen in the Structures lab:





$$A_{\rm A} = (31.00)(3.15) \, \rm mm^2$$

$$A_{\rm B} = (3.15)(27.85) \, \rm mm^2$$

$$A_{\rm C} = (3.15)(11.85) \, \rm mm^2$$

$$A_{\rm A} = 97.65 \, \rm mm^2$$

$$A_{\rm B} = 87.73 \; {\rm mm}^2$$

$$A_{\rm C} = 37.33 \, \rm mm^2$$

$$\bar{X}_{A} = 13.925 \text{ mm}$$

$$\bar{X}_{\rm B} = 0$$

$$\bar{X}_{\rm C} = 27.85 \, {\rm mm}$$

$$\bar{Y}_{A}=0$$

$$\bar{Y}_{\rm B} = 15.50 \text{ mm}$$

$$\bar{Y}_{\rm C} = 7.50 \, \rm mm$$



## **Lipped Section Example**

Centroid of the compound section:

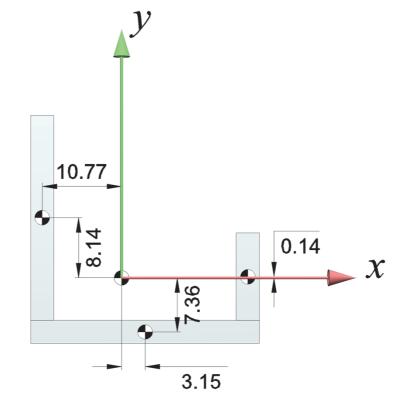
$$\bar{X} = \frac{\sum \bar{X}_i A_i}{\sum A_i} = \frac{\bar{X}_A A_A + \bar{X}_B A_B + \bar{X}_C A_C}{A_A + A_B + A_C} = \frac{(13.925)(97.65) + (0)(87.73) + (27.85)(37.33)}{(97.65) + (87.73) + (37.33)}$$

 $\bar{X} = 10.77 \text{ mm}$ 

$$\bar{Y} = \frac{\sum \bar{Y}_i A_i}{\sum A_i} = \frac{\bar{Y}_A A_A + \bar{Y}_B A_B + \bar{Y}_C A_C}{A_A + A_B + A_C} = \frac{(0)(97.65) + (15.50)(87.73) + (7.50)(37.33)}{(97.65) + (87.73) + (37.33)}$$

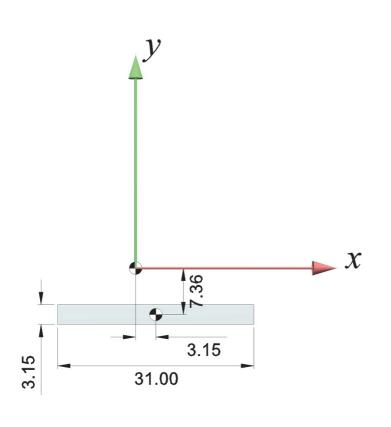
 $\bar{Y} = 7.36 \text{ mm}$ 

New coordinates:





Parallel axis theorem for section A:



$$I_{x_A x_A} = \frac{b h^3}{12} = \frac{(31.00)(3.15)^3}{12} = 80.74 \text{ mm}^4$$

$$\bar{y}_A = \bar{Y}_A - \bar{Y} = 0 - 7.36 = -7.36 \text{ mm}$$

$$I_{xx}^A = I_{x_A x_A} + A_A (\bar{y}_A)^2$$

$$I_{xx}^A = 5,374.43 \text{ mm}^4$$

$$I_{y_A y_A} = \frac{b h^3}{12} = \frac{(3.15)(31.00)^3}{12} = 7,820.14 \text{ mm}^4$$

$$\bar{x}_A = \bar{X}_A - \bar{X} = 13.925 - 10.77 = 3.15 \text{ mm}$$

$$I_{yy}^A = I_{y_A y_A} + A_A (\bar{x}_A)^2$$

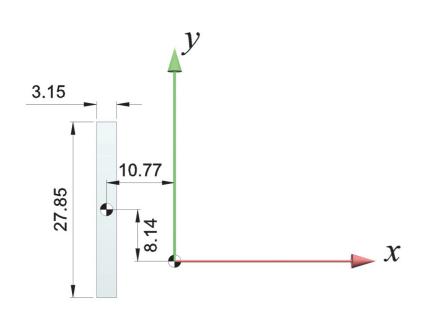
$$I_{yy}^A = 8,789.90 \text{ mm}^4$$

$$I_{x_A y_A} = 0$$
 (symmetric cross-section)  
 $I_{xy}^A = I_{x_A y_A} + A_A (\bar{x}_A \bar{y}_A)$   
 $I_{xy}^A = 0 + (97.65)(3.15)(-7.36)$   
 $I_{xy}^A = -2,265.75 \text{ mm}^4$ 



### **Lipped Section Example**

Parallel axis theorem for section B:



$$I_{x_B x_B} = \frac{b h^3}{12} = \frac{(3.15)(27.85)^3}{12} = 5,670.29 \text{ mm}^4$$

$$\bar{y}_B = \bar{Y}_B - \bar{Y} = 15.50 - 7.36 = 8.14 \text{ mm}$$

$$I_{xx}^B = I_{x_B x_B} + A_B(\bar{y}_B)^2$$

$$I_{xx}^B = 11,479.08 \text{ mm}^4$$

$$I_{y_B y_B} = \frac{b h^3}{12} = \frac{(27.85)(3.15)^3}{12} = 72.54 \text{ mm}^4$$

$$\bar{x}_B = \bar{X}_B - \bar{X} = 0 - 10.77 = -10.77 \text{ mm}$$

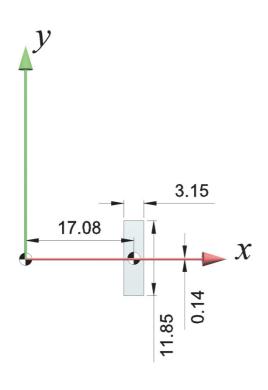
$$I_{yy}^B = I_{y_B y_B} + A_B(\bar{x}_B)^2$$

$$I_{yy}^B = 10,255.22 \text{ mm}^4$$

$$I_{x_{\rm B}\,y_{\rm B}}=0$$
 (symmetric cross-section)   
 $I_{xy}^{\rm B}=I_{x_{\rm B}\,y_{\rm B}}+A_{\rm B}(\bar{x}_{\rm B}\bar{y}_{\rm B})$    
 $I_{xy}^{\rm B}=0+(87.73)(-10.77)(8.14)$    
 $I_{xy}^{\rm B}=-7,690.84~{\rm mm}^4$ 



Parallel axis theorem for section C:



$$I_{x_{C}x_{C}} = \frac{b h^{3}}{12} = \frac{(3.15)(11.85)^{3}}{12} = 436.80 \text{ mm}^{4}$$

$$\bar{y}_{C} = \bar{Y}_{C} - \bar{Y} = 7.50 - 7.36 = 0.14 \text{ mm}$$

$$I_{xx}^{C} = I_{x_{B}x_{B}} + A_{C}(\bar{y}_{C})^{2}$$

$$I_{xx}^{C} = 437.50 \text{ mm}^{4}$$

$$I_{y_{C}y_{C}} = \frac{b h^{3}}{12} = \frac{(11.85)(3.15)^{3}}{12} = 30.87 \text{ mm}^{4}$$

$$\bar{x}_{C} = \bar{X}_{C} - \bar{X} = 27.85 - 10.77 = 17.08 \text{ mm}$$

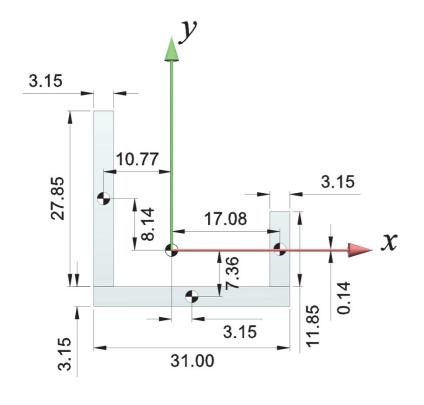
$$I_{yy}^{C} = I_{y_{C}y_{C}} + A_{C}(\bar{x}_{C})^{2}$$

$$I_{yy}^{C} = 10.915.62 \text{ mm}^{4}$$

$$I_{x_{\rm C}\,y_{\rm C}}=0$$
 (symmetric cross-section)   
 $I_{xy}^{\rm C}=I_{x_{\rm C}\,y_{\rm C}}+A_{\rm C}(\bar{x}_{\rm C}\bar{y}_{\rm C})$    
 $I_{xy}^{\rm C}=0+(37.33)(17.08)(0.14)$    
 $I_{xy}^{\rm C}=87.45~{\rm mm}^4$ 



• Finally, for the compound section:



$$I_{xx} = I_{xx}^{A} + I_{xx}^{B} + I_{xx}^{C}$$
  
 $I_{xx} = 17,291.01 \text{ mm}^{4}$ 

$$I_{yy} = I_{yy}^{A} + I_{yy}^{B} + I_{yy}^{C}$$
  
 $I_{yy} = 29,960.73 \text{ mm}^{4}$ 

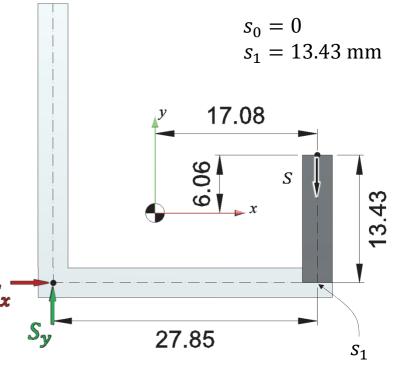
$$I_{xy} = I_{xy}^{A} + I_{xy}^{B} + I_{xy}^{C}$$
  
 $I_{xy} = -9,869.13 \text{ mm}^{4}$ 



#### **Shear centre:**

- Most convenient reference point is the bottom left corner (origin of X, Y)
- Only stresses along section C will generate moments about this reference point (!)
- We integrate shear flow from s = 0 to  $s = s_1 = 13.425 \text{ mm}$
- Important: shear stresses and shear flow are defined in terms of x, y while the **shear centre** is defined in terms of *X*, *Y*

$$(X_0, Y_0) = (27.85 \text{ mm}, 13.425 \text{ mm})$$
  
 $(x_0, y_0) = (17.08 \text{ mm}, 6.06 \text{ mm})$ 



#### **Equations:**

$$S_y e_x = \int (Y q_{s,x} - X q_{s,y}) ds$$

$$S_y e_x = \int (Y q_{s,x} - X q_{s,y}) ds$$
  $S_x e_y = \int (Y q_{s,x} - X q_{s,y}) ds$ 

$$-q_{s} = \left(\frac{S_{x} I_{xx} + S_{y} I_{xy}}{I_{xy}^{2} - I_{xx} I_{yy}}\right) \int_{0}^{s} x t ds + \left(\frac{S_{y} I_{yy} + S_{x} I_{xy}}{I_{xx} I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} y t ds$$

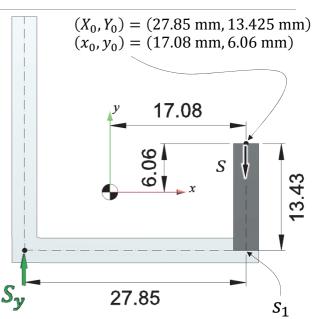


## Lipped Section Example – Shear Centre $e_{\chi}$

$$-q_{s} = \left(\frac{S_{x} I_{xx} + S_{y} I_{xy}}{I_{xy}^{2} - I_{xx} I_{yy}}\right) \int_{0}^{s} x t ds + \left(\frac{S_{y} I_{yy} + S_{x} I_{xy}}{I_{xx} I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} y t ds$$

To find  $e_x$  we apply  $S_y$ , make  $S_x=0$  and therefore:

$$-q_{s} = \left(\frac{S_{y} I_{xy}}{I_{xy}^{2} - I_{xx} I_{yy}}\right) \int_{0}^{s} x t ds + \left(\frac{S_{y} I_{yy}}{I_{xx} I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} y t ds$$



Note that here  $x_{(s)} = x_0 = 17.08$  mm, while  $y_{(s)} = y_0 - s$  and therefore:

$$-q_{s} = \left(\frac{S_{y} I_{xy}}{I_{xy}^{2} - I_{xx} I_{yy}}\right) \int_{0}^{s} x t ds + \left(\frac{S_{y} I_{yy}}{I_{xx} I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} (y_{0} - s) t ds$$

$$-q_{s} = \left(\frac{S_{y} I_{xy}}{I_{xy}^{2} - I_{xx} I_{yy}}\right) x t s + \left(\frac{S_{y} I_{yy}}{I_{xx} I_{yy} - I_{xy}^{2}}\right) \left(y_{0} s - \frac{s^{2}}{2}\right) t$$



## Lipped Section Example – Shear Centre $e_{\chi}$

$$S_y e_x = \int (Y q_{s,x} - X q_{s,y}) ds$$

Note that here we only consider the vertical shear flow  $(q_{s,y})$  while the 'moment arm' is constant and equal to  $X_0$ , therefore:

$$S_y e_x = \int_0^{s_1} (-X_0 q_s) \, \mathrm{d}s$$

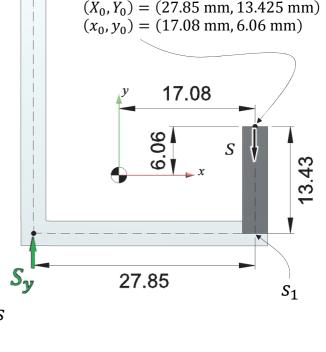
$$S_y e_x = X_0 t \int_0^{s_1} \left[ \left( \frac{S_y I_{xy}}{I_{xy}^2 - I_{xx} I_{yy}} \right) x s + \left( \frac{S_y I_{yy}}{I_{xx} I_{yy} - I_{xy}^2} \right) \left( y_0 s - \frac{s^2}{2} \right) \right] ds$$

$$e_x = X_0 t \left[ \left( \frac{I_{xy}}{I_{xy}^2 - I_{xx} I_{yy}} \right) x \frac{s^2}{2} + \left( \frac{I_{yy}}{I_{xx} I_{yy} - I_{xy}^2} \right) \left( y_0 \frac{s^2}{2} - \frac{s^3}{6} \right) \right]_0^{s_1}$$

$$e_x = X_0 t \left[ \left( \frac{I_{xy}}{I_{xy}^2 - I_{xx} I_{yy}} \right) x \frac{s_1^2}{2} + \left( \frac{I_{yy}}{I_{xx} I_{yy} - I_{xy}^2} \right) \left( y_0 \frac{s_1^2}{2} - \frac{s_1^3}{6} \right) \right]$$

$$e_x = (27.85)(3.15) \left\{ \left( \frac{-9,869.13}{-420,651,624} \right) (17.08) \frac{(13.425)^2}{2} + \left( \frac{29,960.73}{420,651,624} \right) \left[ (6.06) \frac{(13.425)^2}{2} - \frac{(13.425)^3}{6} \right] \right\}$$

 $e_x = 4.06 \text{ mm}$ 



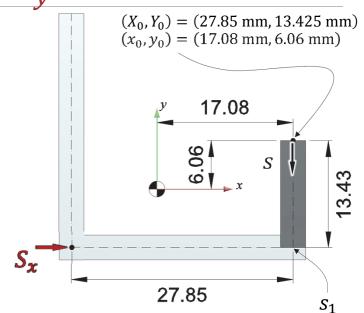


## Lipped Section Example – Shear Centre $e_{\nu}$

$$-q_{s} = \left(\frac{S_{x} I_{xx} + S_{y} I_{xy}}{I_{xy}^{2} - I_{xx} I_{yy}}\right) \int_{0}^{s} x t ds + \left(\frac{S_{y} I_{yy} + S_{x} I_{xy}}{I_{xx} I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} y t ds$$

To find  $e_y$  we apply  $S_x$ , make  $S_y = 0$  and therefore:

$$-q_{s} = \left(\frac{S_{x} I_{xx}}{I_{xy}^{2} - I_{xx} I_{yy}}\right) \int_{0}^{s} x t ds + \left(\frac{S_{x} I_{xy}}{I_{xx} I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} y t ds$$



Note that here  $x_{(s)} = x_0 = 17.08$  mm, while  $y_{(s)} = y_0 - s$  and therefore:

$$-q_{s} = \left(\frac{S_{x} I_{xx}}{I_{xy}^{2} - I_{xx} I_{yy}}\right) \int_{0}^{s} x t ds + \left(\frac{S_{x} I_{xy}}{I_{xx} I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} (y_{0} - s) t ds$$

$$-q_{s} = \left(\frac{S_{x} I_{xx}}{I_{xy}^{2} - I_{xx} I_{yy}}\right) x t s + \left(\frac{S_{x} I_{xy}}{I_{xx} I_{yy} - I_{xy}^{2}}\right) \left(y_{0} s - \frac{s^{2}}{2}\right) t$$



 $(X_0, Y_0) = (27.85 \text{ mm}, 13.425 \text{ mm})$  $(x_0, y_0) = (17.08 \text{ mm}, 6.06 \text{ mm})$ 

17.08

27.85

 $S_{x}$ 

## Lipped Section Example – Shear Centre $e_{\gamma}$

$$S_x e_y = \int (Y q_{s,x} - X q_{s,y}) ds$$

Note that here we only consider the vertical shear flow  $(q_{s,y})$  while the 'moment arm' is constant and equal to  $X_0$ , therefore:

$$S_x e_y = \int_0^{s_1} (-X_0 q_s) \, \mathrm{d}s$$

$$S_x e_y = X_0 t \int_0^{s_1} \left[ \left( \frac{S_x I_{xx}}{I_{xy}^2 - I_{xx} I_{yy}} \right) x s + \left( \frac{S_x I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right) \left( y_0 s - \frac{s^2}{2} \right) \right] ds$$

$$e_y = X_0 t \left[ \left( \frac{I_{xx}}{I_{xy}^2 - I_{xx} I_{yy}} \right) x \frac{s^2}{2} + \left( \frac{I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right) \left( y_0 \frac{s^2}{2} - \frac{s^3}{6} \right) \right]_0^{s_1}$$

$$e_{y} = X_{0} t \left[ \left( \frac{I_{xx}}{I_{xy}^{2} - I_{xx} I_{yy}} \right) x \frac{s_{1}^{2}}{2} + \left( \frac{I_{xy}}{I_{xx} I_{yy} - I_{xy}^{2}} \right) \left( y_{0} \frac{s_{1}^{2}}{2} - \frac{s_{1}^{3}}{6} \right) \right]$$

$$e_y = (27.85)(3.15) \left\{ \left( \frac{17,291.01}{-420,651,624} \right) (17.08) \frac{(13.425)^2}{2} + \left( \frac{-9,869.13}{420,651,624} \right) \left[ (6.06) \frac{(13.425)^2}{2} - \frac{(13.425)^3}{6} \right] \right\}$$



Thin wall (analytical) solution

Full 2D (numerical) solution

