

Advanced Bending and Torsion

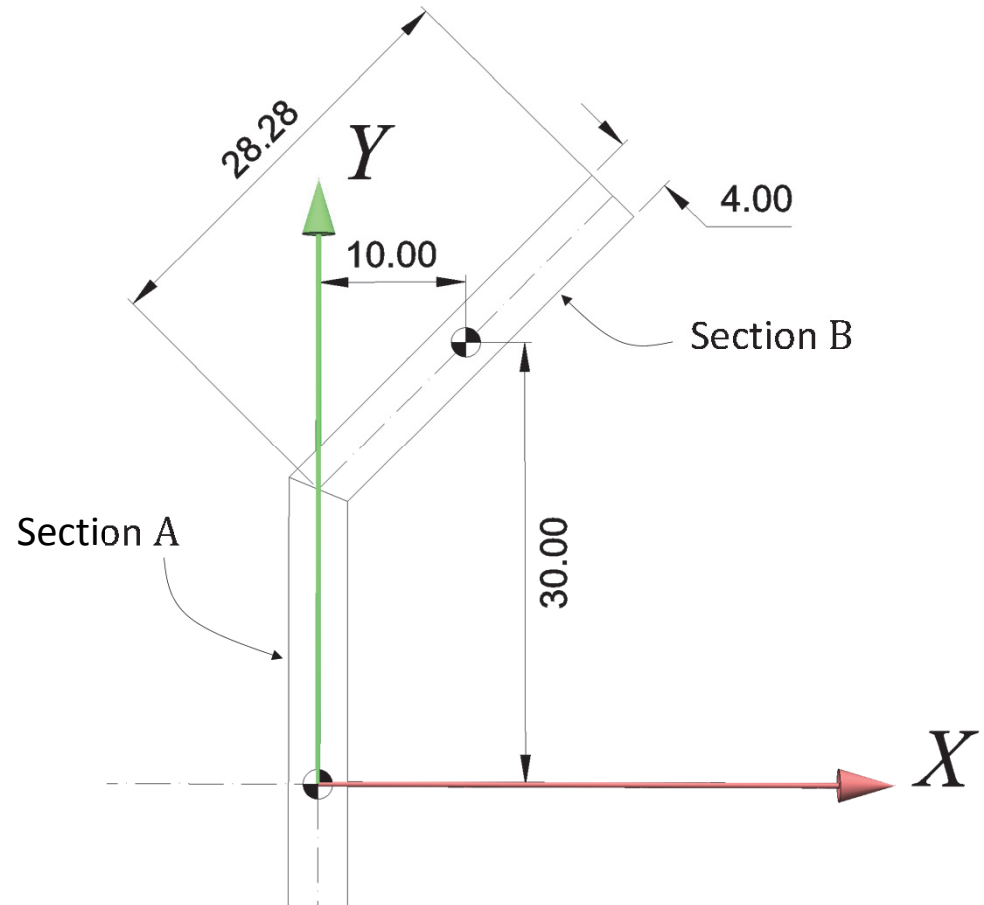
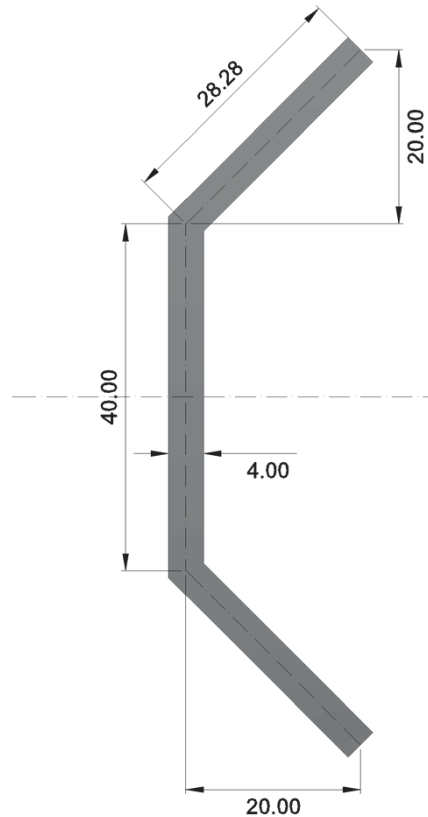
Shear Centre Example – Angled Flanges

Dr Luiz Kawashita

Luiz.Kawashita@bristol.ac.uk

07 November 2018

- Section with flanges at 45°:



$$A_A = (4.00)(40.0) \text{ mm}^2$$

$$A_B = (4.00)(28.28) \text{ mm}^2$$

$$A_A = 160.00 \text{ mm}^2$$

$$A_B = 113.14 \text{ mm}^2$$

$$\bar{X}_A = 0$$

$$\bar{X}_B = 10.00 \text{ mm}$$

$$\bar{Y}_A = 0$$

$$\bar{Y}_B = 30.00 \text{ mm}$$

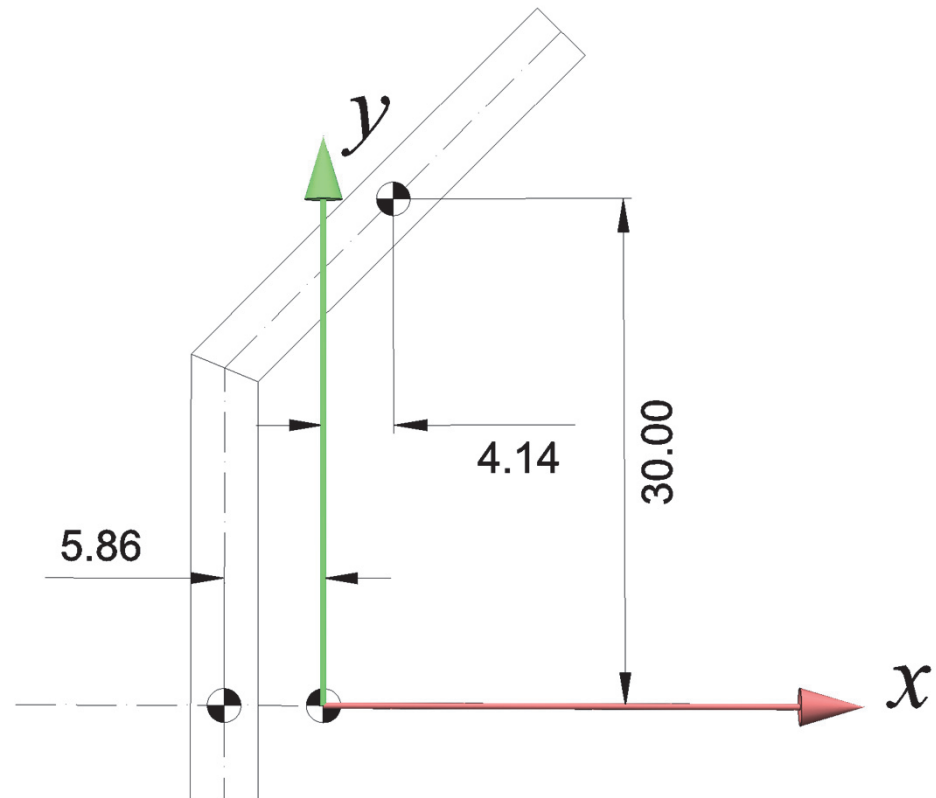
- Centroid of the compound section:

$$\bar{X} = \frac{\sum \bar{X}_i A_i}{\sum A_i} = \frac{\bar{X}_A A_A + 2 \bar{X}_B A_B}{A_A + 2 A_B} = \frac{(0)(160.00) + 2 (10.00)(113.14)}{(160.00) + 2 (113.14)}$$

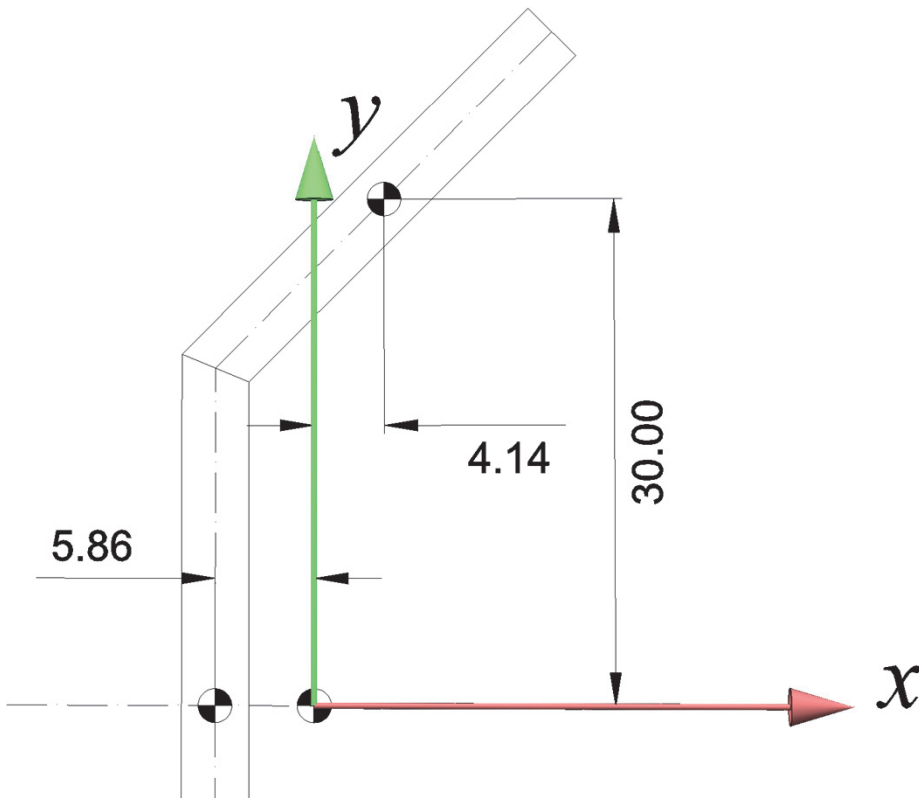
$$\bar{X} = 5.86 \text{ mm}$$

$$\bar{Y} = 0$$

- New coordinates:



- Parallel axis theorem for section A:



$$I_{x_A x_A} = \frac{b h^3}{12} = \frac{(4.00)(40)^3}{12} = 21,333.33 \text{ mm}^4$$

$$\bar{y}_A = \bar{Y}_A - \bar{Y} = 0 \text{ mm}$$

$$I_{xx}^A = I_{x_A x_A} + A_A (\bar{y}_A)^2$$

$$I_{xx}^A = 21,333.33 \text{ mm}^4$$

$$I_{y_A y_A} = \frac{b h^3}{12} = \frac{(40.00)(4.00)^3}{12} = 213.33 \text{ mm}^4$$

$$\bar{x}_A = \bar{X}_A - \bar{X} = 0 - 5.86 = -5.86 \text{ mm}$$

$$I_{yy}^A = I_{y_A y_A} + A_A (\bar{x}_A)^2$$

$$I_{yy}^A = 5,703.67 \text{ mm}^4$$

$$I_{x_A y_A} = 0 \text{ (symmetric cross-section)}$$

$$I_{xy}^A = I_{x_A y_A} + A_A (\bar{x}_A \bar{y}_A)$$

$$I_{xy}^A = 0$$

$$x_{(s)} = 10\sqrt{2} - s \frac{\sqrt{2}}{2}$$

$$x_{(s)} = \frac{\sqrt{2}}{2} (20 - s)$$

$$y_{(s)} = 40 - s \frac{\sqrt{2}}{2}$$

$$s_1 = 20\sqrt{2}$$

$$I_{xx}^B = \int_0^{s_1} y^2 t \, ds$$

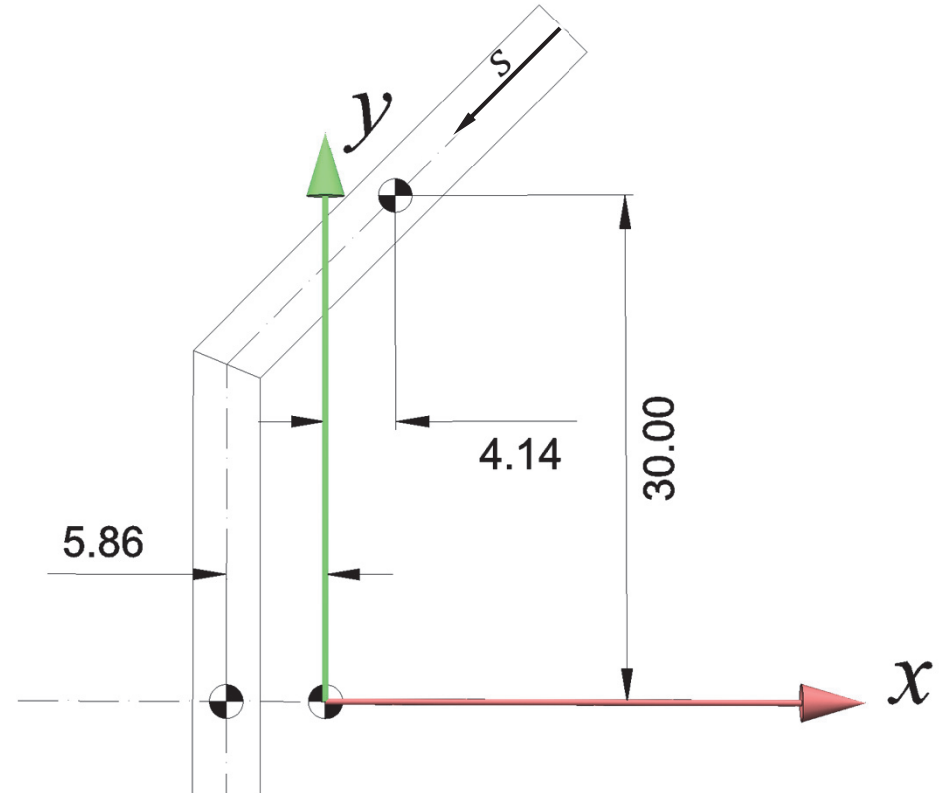
$$I_{xx}^B = \int_0^{s_1} \left(40 - s \frac{\sqrt{2}}{2} \right)^2 t \, ds$$

$$I_{xx}^B = t \int_0^{s_1} \left(40^2 - 40 s \sqrt{2} + \frac{1}{2} s^2 \right) ds$$

$$I_{xx}^B = t \left[40^2 s - 20 s^2 \sqrt{2} + \frac{1}{6} s^3 \right]_0^{s_1}$$

$$I_{xx}^B = t \left[40^2 s_1 - 20 s_1^2 \sqrt{2} + \frac{1}{6} s_1^3 \right]$$

$$I_{xx}^B = 105,595 \text{ mm}^4$$



$$I_{yy}^B = \int_0^{s_1} x^2 t \, ds$$

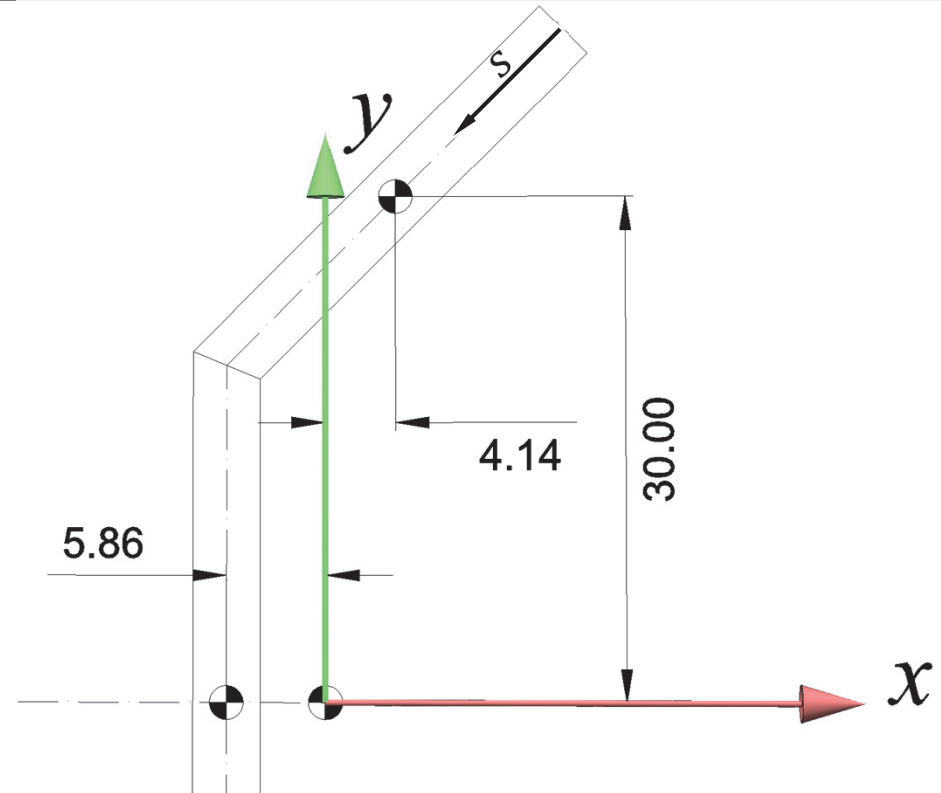
$$I_{yy}^B = \int_0^{s_1} \left[\frac{\sqrt{2}}{2} (20 - s) \right]^2 t \, ds$$

$$I_{yy}^B = \frac{t}{2} \int_0^{s_1} (400 - 40s + s^2) \, ds$$

$$I_{yy}^B = \frac{t}{2} \left[400s - 20s^2 + \frac{1}{3}s^3 \right]_0^{s_1}$$

$$I_{yy}^B = \frac{t}{2} \left(400s_1 - 20s_1^2 + \frac{1}{3}s_1^3 \right)$$

$$I_{yy}^B = 5,712 \, \text{mm}^4$$



$$x_{(s)} = \frac{\sqrt{2}}{2} (20 - s)$$

$$y_{(s)} = 40 - s \frac{\sqrt{2}}{2}$$

$$s_1 = 20\sqrt{2}$$

$$I_{xy}^B = \int_0^{s_1} x y t ds$$

$$I_{xy}^B = \int_0^{s_1} \left[\frac{\sqrt{2}}{2} (20 - s) \right] \left[40 - s \frac{\sqrt{2}}{2} \right] t ds$$

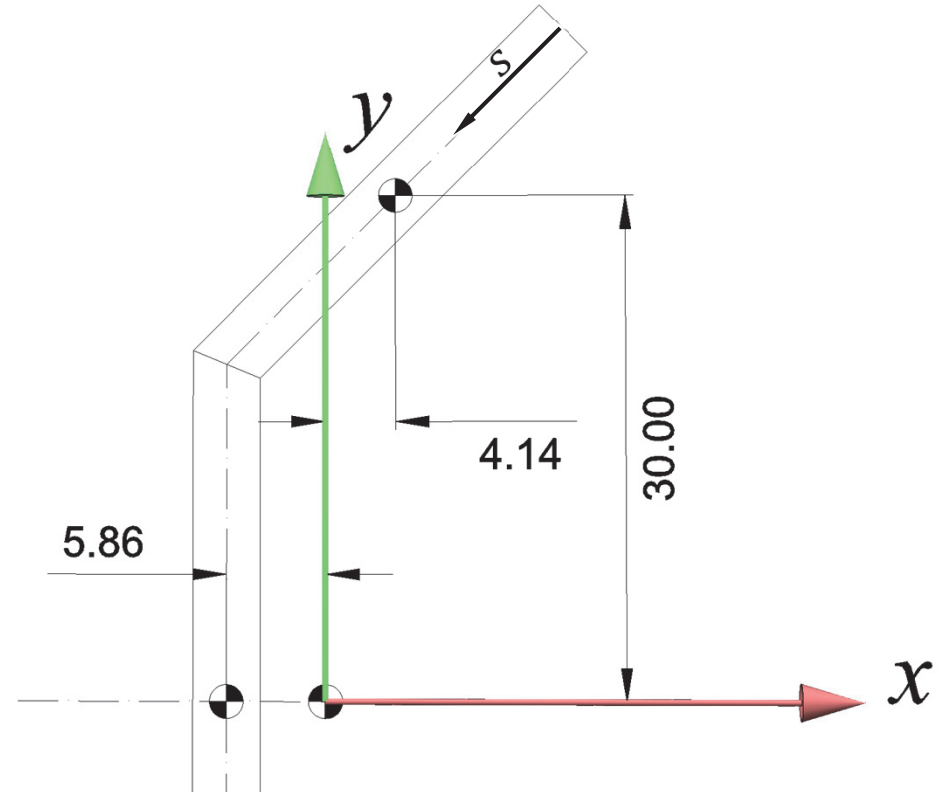
$$I_{xy}^B = \frac{\sqrt{2}}{2} t \int_0^{s_1} \left(800 - 10 \sqrt{2} s - 40 s + \frac{\sqrt{2}}{2} s^2 \right) ds$$

$$I_{xy}^B = \frac{\sqrt{2}}{2} t \left(800 s - 5 \sqrt{2} s^2 - 20 s^2 + \frac{\sqrt{2}}{6} s^3 \right)_0^{s_1}$$

$$I_{xy}^B = \frac{\sqrt{2}}{2} t \left[800 s_1 - (5 \sqrt{2} + 20) s_1^2 + \frac{\sqrt{2}}{6} s_1^3 \right]$$

$$I_{xy}^B = 17,830 \text{ mm}^4$$

$$I_{xy}^C = -17,830 \text{ mm}^4$$

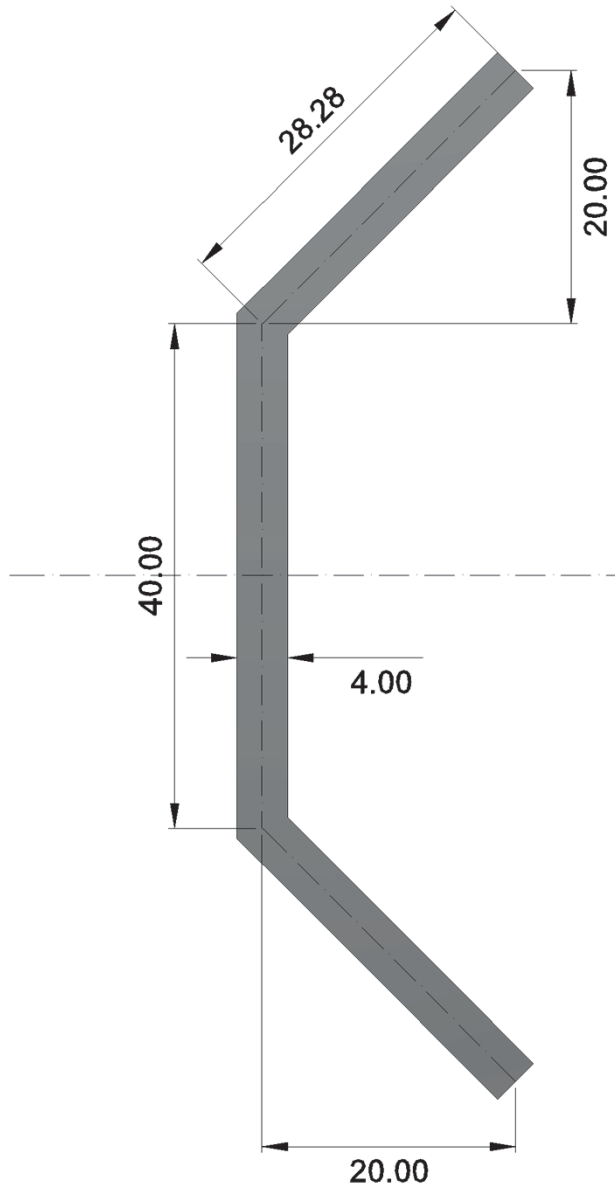


$$x(s) = \frac{\sqrt{2}}{2} (20 - s)$$

$$y(s) = 40 - s \frac{\sqrt{2}}{2}$$

$$s_1 = 20 \sqrt{2}$$

- Finally, for the compound section:



$$I_{xx} = I_{xx}^A + I_{xx}^B + I_{xx}^C$$

$$I_{xx} = 232,523 \text{ mm}^4$$

$$I_{yy} = I_{yy}^A + I_{yy}^B + I_{yy}^C$$

$$I_{yy} = 17,128 \text{ mm}^4$$

$$I_{xy} = I_{xy}^A + I_{xy}^B + I_{xy}^C$$

$$I_{xy} = 0$$

• Shear centre:

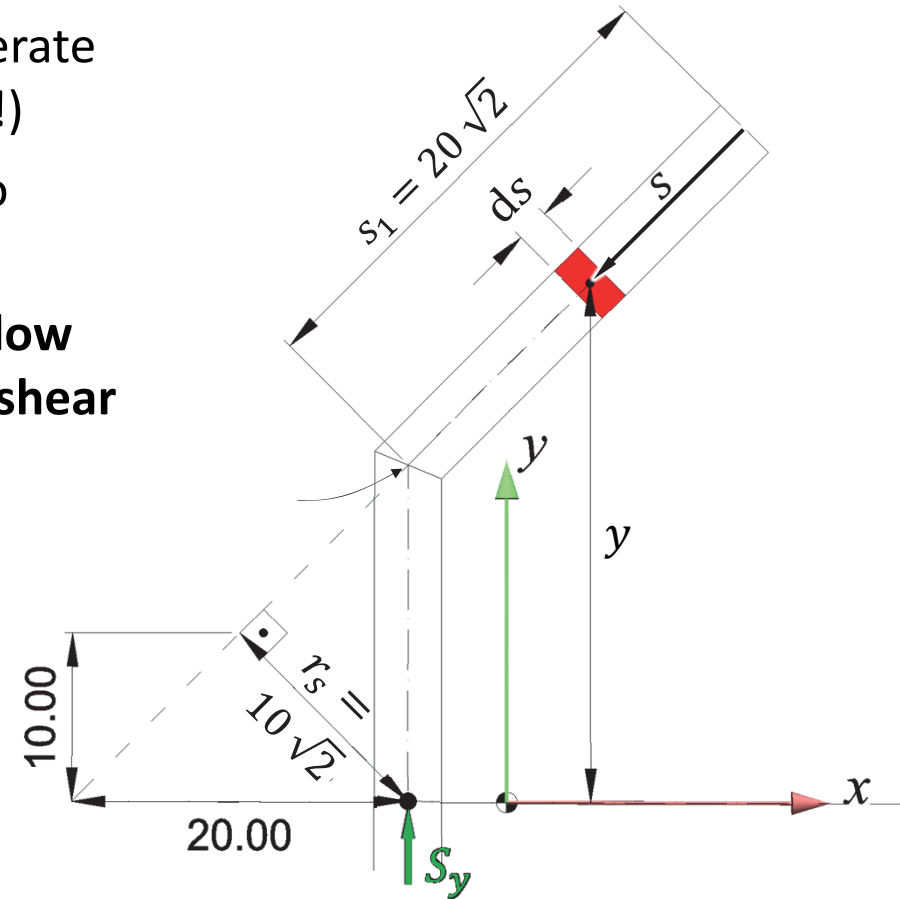
- Most convenient reference point is the bottom left corner (origin of X, Y)
- Only stresses along section C will generate moments about this reference point (!)
- We integrate shear flow from $s = 0$ to $s = s_1 = 13.425 \text{ mm}$
- **Important:** shear stresses and **shear flow** are defined in terms of x, y while the **shear centre** is defined in terms of X, Y

$$(x_0, y_0) = (20 \text{ mm}, 40 \text{ mm})$$

$$r_s = 10 \sqrt{2} \text{ mm}$$

$$s_0 = 0$$

$$s_1 = 20 \sqrt{2} \text{ mm}$$



Equations:

Shear centre:

$$S_y e_x = \int r_s q_s ds$$

Shear flow:

$$-q_s = \left(\frac{S_x I_{xx} + S_y I_{xy}}{I_{xy}^2 - I_{xx} I_{yy}} \right) \int_0^s x t ds + \left(\frac{S_y I_{yy} + S_x I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right) \int_0^s y t ds$$

$$-q_s = \left(\frac{S_x I_{xx} + S_y I_{xy}}{I_{xy}^2 - I_{xx} I_{yy}} \right) \int_0^s x t \, ds + \left(\frac{S_y I_{yy} + S_x I_{xy}}{I_{xx} I_{yy} - I_{xy}^2} \right) \int_0^s y t \, ds$$

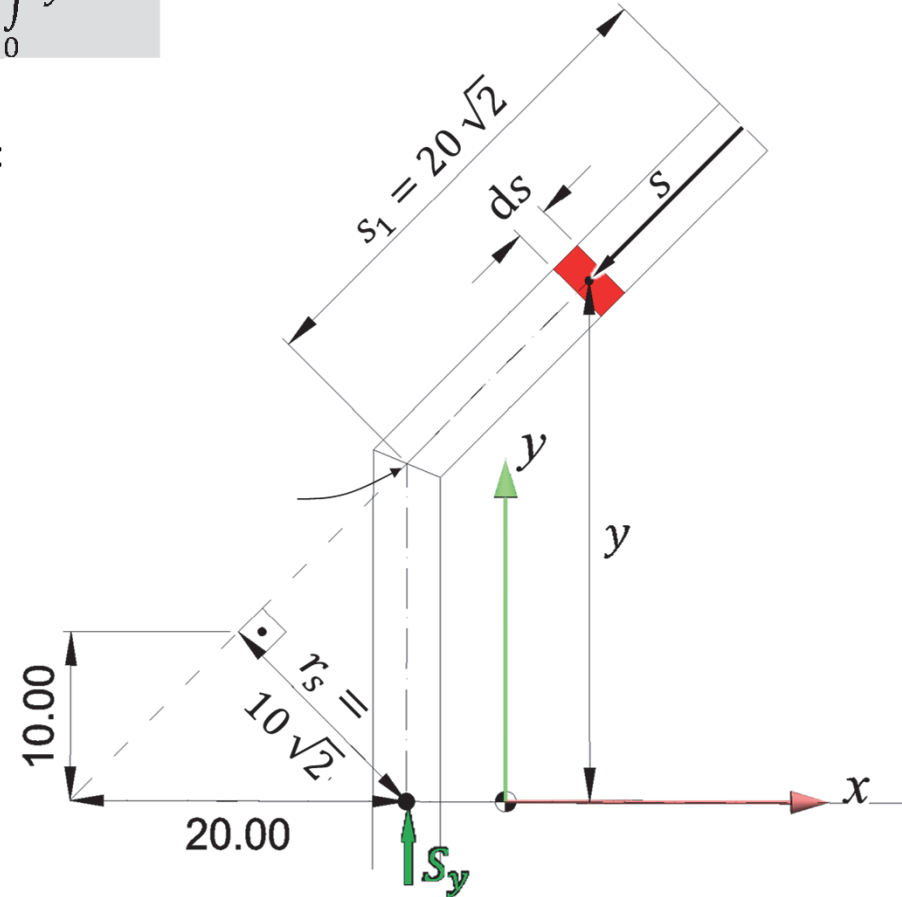
To find e_x we apply S_y , but $S_x = I_{xy} = 0$ and therefore:

$$-q_s = \left(\frac{S_y}{I_{xx}} \right) \int_0^s y t \, ds$$

$$y_{(s)} = 40 - s \frac{\sqrt{2}}{2}$$

$$-q_s = \left(\frac{S_y}{I_{xx}} \right) \int_0^s \left(40 - s \frac{\sqrt{2}}{2} \right) t \, ds$$

$$-q_s = t \left(\frac{S_y}{I_{xx}} \right) \left(40 s - \frac{\sqrt{2}}{4} s^2 \right)$$



$$S_y e_x = \int r_s q_s ds$$

Note that there are **two** angled flanges, therefore:

$$S_y e_x = 2 \int_0^{s_1} (10 \sqrt{2} q_s) ds \quad -q_s = t \left(\frac{S_y}{I_{xx}} \right) \left(40 s - \frac{\sqrt{2}}{4} s^2 \right)$$

$$S_y e_x = 20 \sqrt{2} \int_0^{s_1} - \left[t \left(\frac{S_y}{I_{xx}} \right) \left(40 s - \frac{\sqrt{2}}{4} s^2 \right) \right] ds$$

$$e_x = - \frac{20 t \sqrt{2}}{I_{xx}} \int_0^{s_1} \left(40 s - \frac{\sqrt{2}}{4} s^2 \right) ds$$

$$e_x = - \frac{20 t \sqrt{2}}{I_{xx}} \left(20 s^2 - \frac{\sqrt{2}}{12} s^3 \right)$$

$$e_x = -6.49 \text{ mm}$$

