

# Lecture 11

## Static Stability

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# Lecture Overview

- Stability – Definitions
- Pitching Moment Equation
- Neutral Point
- Static Margin

# Static Stability

## Definitions

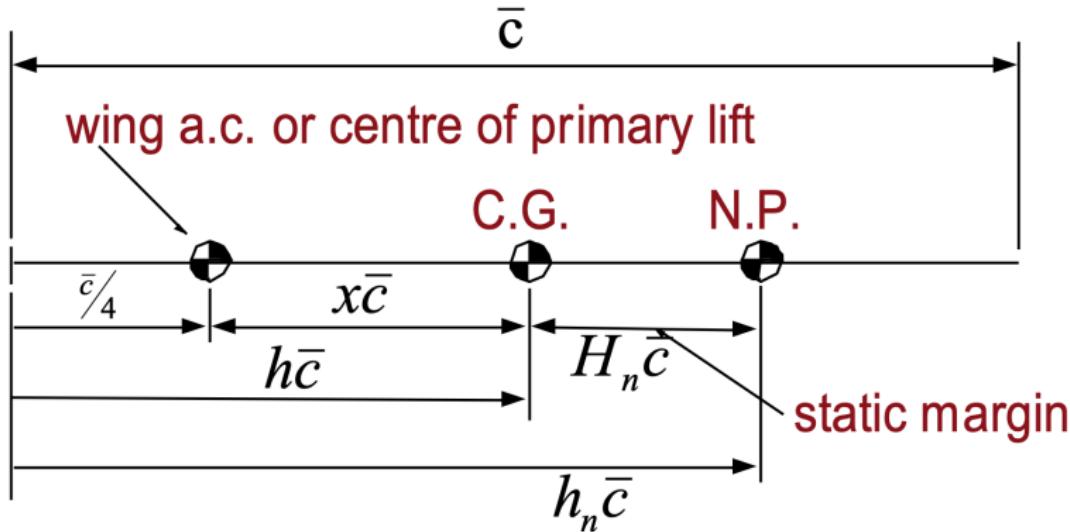
The previous calculations for elevator angle to trim do not guarantee:

- that the necessary angle for  $\eta$  is available
- that the trim condition is *stable*

# The Neutral Point and Static Margin

The **neutral point** is the rearmost position of the c.g. before an unstable condition occurs.

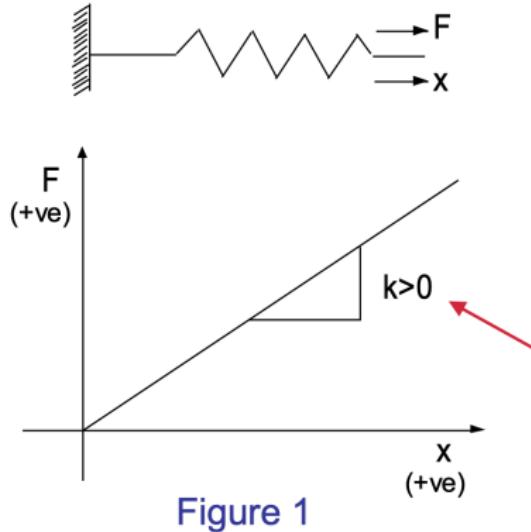
# The Neutral Point and Static Margin



- Note that our earlier use of c.g. position  $x$  (relative to the lift) is replaced here by an alternative measure  $h$  from the MAC i.e. or  $x=h-\frac{1}{4}$  (MAC - Mean Aerodynamic Chord)

# Static Stability

## The Influence of Aerodynamic Stiffness on Stability



- Consider the simple spring shown in Figure 1
- Relationship between force and displacement?
- Applying force  $+F$  results in displacement  $+x$
- Hence positive slope  $k$

# Static Stability

- The force  $F$  is associated with extension  $x$  and results in a positive slope  $k$ . An alternative approach gives:

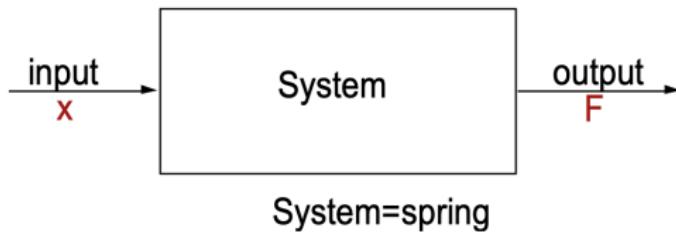
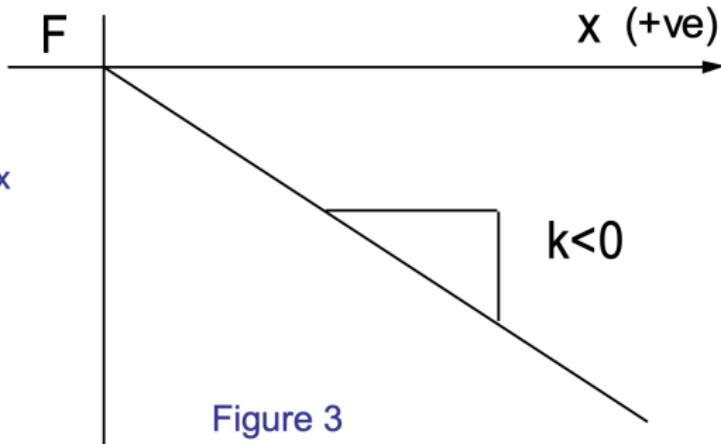


Figure 2

- Using the generalised system-approach of Fig. 2 the force caused by deflection  $x$  is actually *negative*.

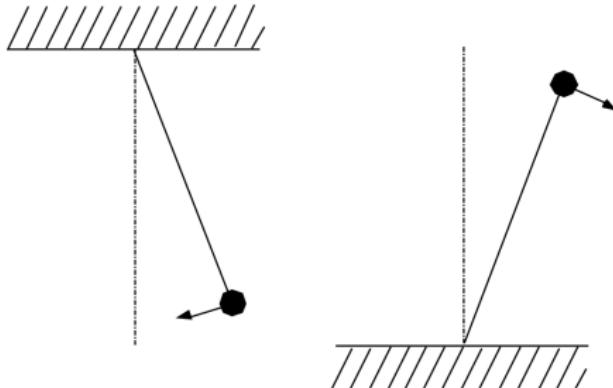
# Static Stability

- This is a restoring force which tries to restore  $x$  to zero and the force which we normally plot (Fig. 1) is actually the force required for equilibrium and which counteracts the force produced by the "system".



- Applied displacement  $x$
- results in  $-ve$  force
- therefore  $-ve$  slope  $k$

# Static Stability



- We normally associate a **positive stiffness** with a restoring force (the pendulum supported at its top)
- *but* when the **displacement** and the **force** caused by it are defined as positive in the same direction a **restoring force** will be one which displays **negative stiffness**.

# Static Stability

- So for the system shown in Figure 2, for which the input is the displacement  $x$  and the output the resulting force  $F$ , we should plot the graph as shown in Figure 3.
- Hence, we need to consider more closely the sign of  $k$  expected for a stable system.

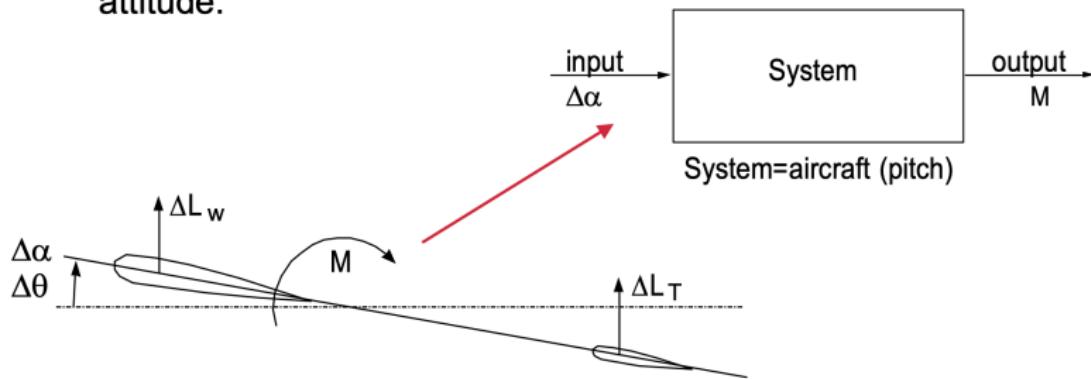
Remember the pendulum example:

restoring force  $\longleftrightarrow$  stability

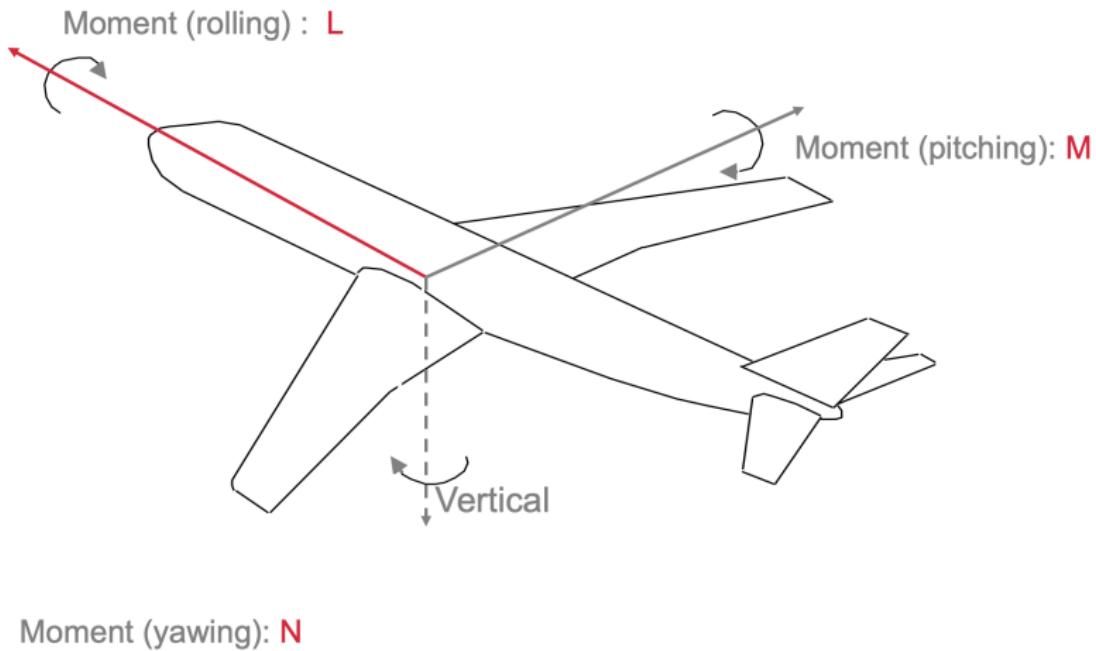
diverging force  $\longleftrightarrow$  instability

# Static Stability

- The flight mechanics case follows this sign convention and displays the displacement/force characteristics given in Figs. 2 & 3.
- Our study of stability will be directed toward an investigation of the pitching moment  $\Delta M$  produced when there is a departure ( $\Delta\alpha$  or  $\Delta\theta$ ) away from the equilibrium flight attitude.



# Body Axes Notation and Sign Conventions



# Static Stability

- The "system" is the pitch response of an aircraft; the "input" is a pitch displacement  $\Delta\alpha$  and the "output" is the consequent pitching moment  $\Delta M$ .
- For stable flight we need  $\Delta M < 0$  for  $\Delta\alpha > 0$  so that there will be a restoring action. This can be seen graphically in Fig. 6.

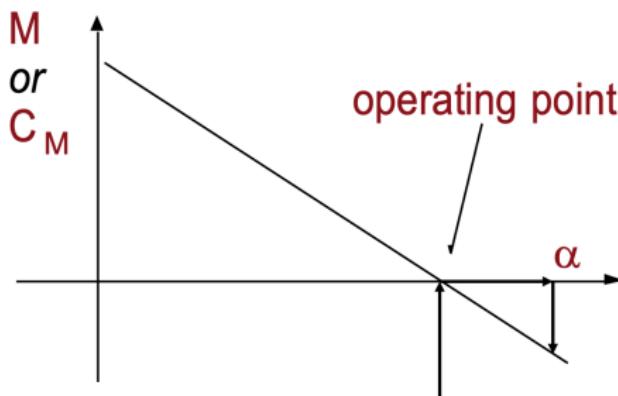


Figure 6

# Static Stability

- The "system" is the **pitch response** of an **aircraft**; the "input" is a pitch displacement  $\Delta\alpha$  and the "output" is the consequent pitching moment  $\Delta M$ .
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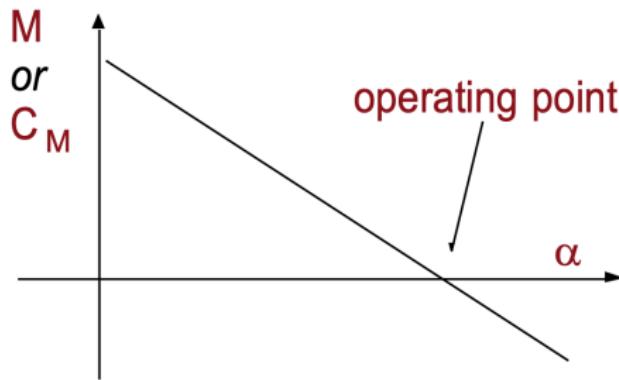


Figure 6

# Static Stability

- Consider a perturbation  $\Delta\alpha$  away from a trimmed, straight and level operating point? +ve or -ve slope desirable?
- This implies that whichever sign there is for  $\Delta\alpha$  away from the equilibrium flight angle  $\alpha$ , the pitching moment caused by  $\Delta\alpha$  will be of such a sign as to counteract  $\Delta\alpha$  and restore the flight to its equilibrium incidence.

**The slope given by  $\partial M / \partial \alpha$  must therefore be negative for stability.**

# Static Stability - Definitions

From Fig 6:

- If the coefficient form  $\partial C_M / \partial \alpha$  is negative the aircraft will be stable
- Remember that  $\alpha$  is  $\alpha_{wing}$  and that we can put  $\alpha_{wing} = C_{L_w} / a_1$
- Hence there is only a constant factor that would distinguish between  $\partial C_M / \partial \alpha$  and  $\partial C_M / \partial C_L$ .
- Hence if  $\partial C_M / \partial C_L$  is negative the aircraft will be stable (restoring moment when in flight)

$$a_1 = \frac{\partial C_L}{\partial \alpha}$$
$$C_L = a_1(\alpha - \alpha_0)$$

zero lift angle  $\alpha_0$

# Previous Exam Question

*Can you think of the directional equivalent?*

- Q2** (a) Explain what is meant by longitudinal static stability when related to a classical aircraft configuration. Provide an appropriate diagram.

(7 marks)

- (b) You have been presented with the plot shown in Figure Q2.1 for an unknown fighter aircraft showing data across a very wide range of  $\alpha$ . Using this plot and with the assumption that the aircraft retains lateral-directional stability throughout the angle of attack range given, describe the likely longitudinal response of the aircraft with  $\alpha$ . Within your answer, provide a sketch of  $\alpha$  vs time for this aircraft as the elevator is ramped in the direction that generates a positive pitching moment.

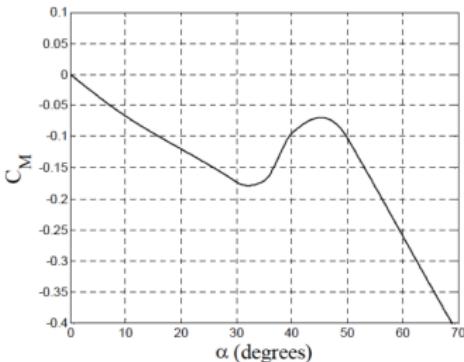


Fig. Q2.1

(13 marks)

- (c) For the aircraft described in part (b) suggest how the longitudinal response might be improved for this aircraft when operating at high angles of attack.

(5 marks)

## Pitching Moment Equation



# Derivatives of the Pitching Moment Equation

- The pitching moment expression which we obtained was:

$$C_M = C_{M_0} - \bar{V} a_{1_T} i_T - C_{L_{WFP}} \left[ \bar{V} \frac{a_{1_T}}{a_1} (1-k) - x \right] - \bar{V} a_{2_T} \eta \quad (1)$$

$$\bar{V} = \frac{S_T l_T}{S \bar{c}}$$

For trimmed flight  $C_M = 0$

- Now consider a disturbance in pitch ( $\Delta\alpha$ ), perhaps caused by an upward gust, and this  $\Delta\alpha$  leads to an associated disturbance  $\Delta C_L > 0$ .

# Static Stability

- Now consider a disturbance in pitch ( $\Delta\alpha$ ), perhaps caused by an upward gust, and this  $\Delta\alpha$  leads to an associated disturbance

$$\Delta C_L > 0$$

- On the basis of what we saw above, it should be clear that:

$\Delta C_M > 0$  is adverse → unstable aircraft

$\Delta C_M < 0$  is restoring → stable aircraft,

# Static Stability

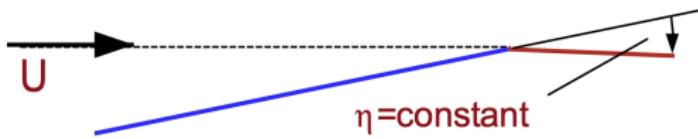
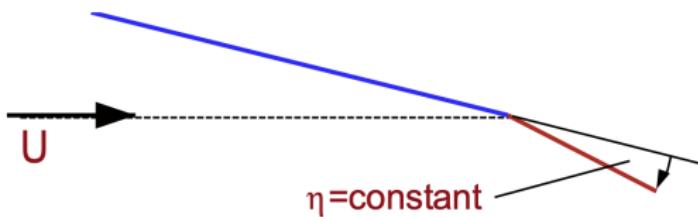
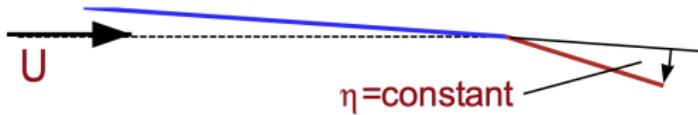
**and thus in general**

$$\frac{1}{a_1} \frac{\partial C_M}{\partial \alpha} \text{ or } \frac{\partial C_M}{\partial C_L} > 0 \quad \text{unstable}$$
$$= 0 \quad \text{neutrally stable} \quad (2)$$
$$< 0 \quad \text{stable}$$

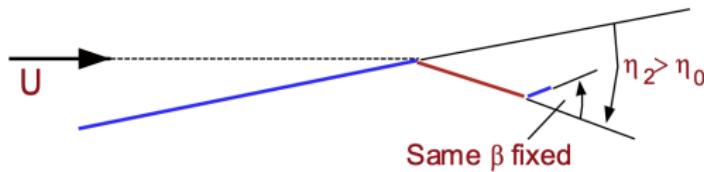
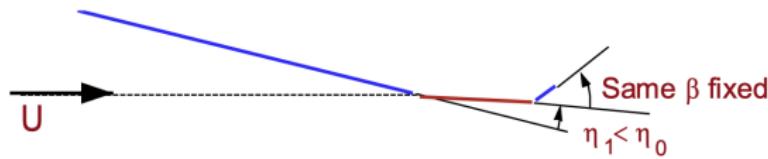
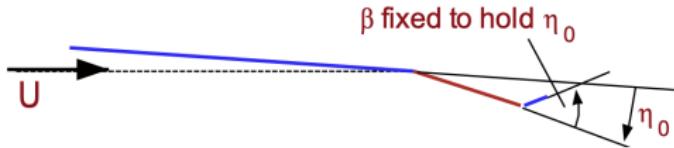
## The case for a Fixed Elevator ("Stick-Fixed")

- We will assume that the **elevator** is held **fixed** by the pilot or that there is a "**control-fixed**" condition imposed by the hydraulics when control demands remain constant.
- With the "**stick-free**" case, there can be a small difference in the **pitch stability** if the elevator position is allowed to drift. Under such conditions, the nominal value  $\eta = \eta_{trim}$  is not retained when the pitch attitude is disturbed.
- We will only consider the "**stick-fixed**" case.

# "Stick-Fixed"



# "Stick-Free"



# Static Stability

- Thus for the case where the elevator is locked and  $\eta = \text{constant}$  (but not necessarily zero), we have from (1) above, for static stability

$$\frac{1}{a_1} \frac{\partial C_M}{\partial \alpha} = \frac{\partial C_M}{\partial C_L} = \left[ \frac{V}{a_1} \frac{a_{1T}}{a_1} (1 - k) - x \right] < 0 \quad (3)$$

and the factor in the square brackets must therefore be positive for a stable aircraft.

# Static Stability

- For  $k$  of order  $1/2$  and with the c.g. behind the primary lift by a *small* distance (i.e.  $x$  is small and positive), the terms in the [ ] lead to a positive value.
- This will remain so, as the c.g. moves forward and passes the primary lift to make  $x < 0$ .
- However, clearly  $x$  could become sufficiently large and positive for [ ] to become negative and the aircraft would be **unstable**.

# An Alternative Criterion for Pitch Stability?

- Another way of looking at the longitudinal stability is to use a logical argument which relates  $C_L$  and  $\eta_{trim}$  as follows for balanced flight:
  1. If flight is to be at a faster speed, it must also be at a lower  $C_L$ , i.e.  $\Delta C_L < 0$
  2. To obtain a lower  $C_L$  we must push the nose down to obtain lower incidence  $\alpha$ .
  3. This lower incidence is obtained by a larger upward force at the tail, via a more positive  $\eta$ , i.e.  $\Delta \eta > 0$ , even if  $\eta < 0$ .

## *For Reference*

- *and thus the elevator angle required to obtain this trim is:*

$$\eta_{trim} = \frac{1}{\bar{V} a_{2_T}} \left\{ C_{M_0} - \bar{V} a_{1_T} i_T - C_{L_{WFP}} \left[ \bar{V} \frac{a_{1_T}}{a_1} (1-k) - x \right] \right\}$$

# Static Stability

- Thus in flight we should expect to have  $\Delta\eta_{trim}$  positive as speed is increased while  $\Delta C_L$  becomes negative, and thus:

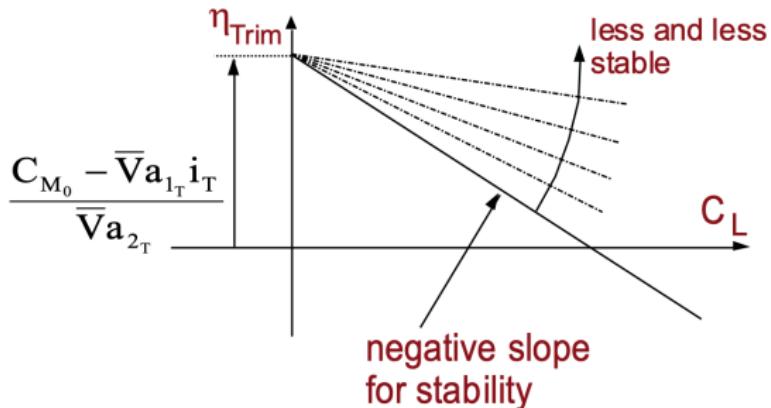
$$\frac{\partial \eta_{trim}}{\partial C_L} < 0$$

- Indeed a differentiation of the expression for  $\eta_{trim}$  will show that this leads to

$$\frac{\partial \eta_{trim}}{\partial C_L} = -\frac{1}{\bar{V} a_{2_T}} [\text{same factor in brackets}] \quad (4)$$

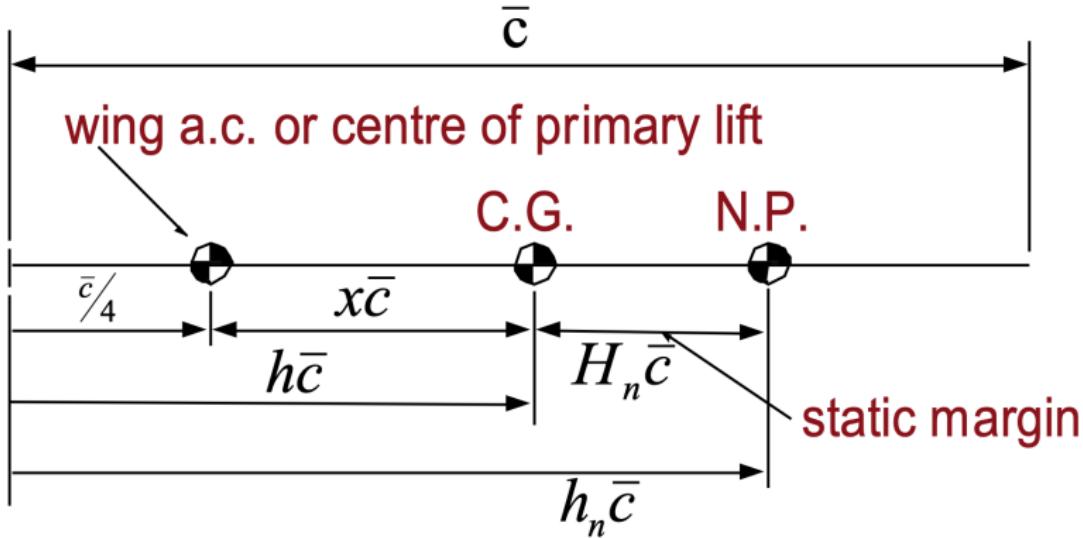
- Clearly, the RHS of Eqn. (4) will be negative if the bracketed expression is again positive; the logical requirement for retaining balanced flight rests on the stability criterion.

# Static Stability



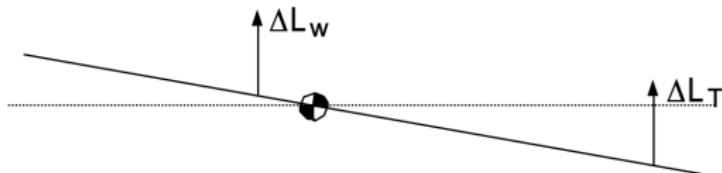
- Because the bracketed terms in Eqn. (3) & (4) are the same, the *boundary* between stable and unstable flight is shown by a zero value for that term and thus a horizontal line for the  $\eta_{\text{trim}}$  vs  $C_L$  graph.
- C.G. change = data for another line (*moving significant masses!*)

# The Neutral Point and Static Margin



Note that our earlier use of **c.g. position  $x$**  (relative to the lift) is replaced here by an alternative measure  **$h$**  from the **MAC** i.e. or  **$x=h-\frac{1}{4}$**  (*MAC - Mean Aerodynamic Chord*)

# The Neutral Point and Static Margin



- When perturbed in pitch the new (additional) forces define its **stability**
  - **wing force** with a small moment arm trying to tip it farther out of alignment
  - while the (smaller) **tail force** with a long moment arm tries to restore the earlier alignment.
- Rearward movement of the c.g. reduces **static stability**

# The Neutral Point

- Stability becomes **neutral** when the c.g. moves just back to the **neutral point (N.P.)**, where:

$$h = h_n \quad x = h_n - \frac{1}{4}$$

- The **stick-fixed neutral point** can be found by setting to zero the derivative that we saw earlier:

$$\frac{1}{a_1} \frac{\partial C_M}{\partial \alpha} = \frac{\partial C_M}{\partial C_L} = - \left[ \bar{V} \frac{a_{1T}}{a_1} (1-k) - x \right] < 0 \quad (5)$$

# The Neutral Point

- Alternatively:  $\bar{V} \frac{a_{1T}}{a_1} (1 - k) - h_n + \frac{1}{4} = 0$  (6)
- or, to define the length  $h_n$ :  $h_n = \frac{1}{4} + \bar{V} \frac{a_{1T}}{a_1} (1 - k)$  (7)
- and this defines the **stick fixed neutral point** relative to the MAC i.e. ...

# Static Margin

- The static margin is a measure of the distance remaining through which the c.g. could be moved rearward before the aircraft displays neutral static stability.
- It is defined as the remaining distance divided by  $\bar{C}$ , so it is a chord-fraction and is given by

$$(h_n - h) = H_n \quad (8)$$

- Static Margin is positive if the aircraft is still stable. Note that if in (5) we insert  $x = h - 1/4$  we have:

$$\frac{\partial C_M}{\partial C_L} = h - \frac{1}{4} - \bar{V} \frac{a_{1T}}{a_1} (1 - k)$$

# The Neutral Point and Static Margin

- but (7) shows that this is just:

$$\frac{\partial C_M}{\partial C_L} = -(h_n - h) = -H_n. \quad (9)$$

- Thus (5) is really just:

$$\frac{\partial C_M}{\partial C_L} = -H_n, \quad (10)$$

- which shows that:

**the static margin must be positive for positive static stability.**