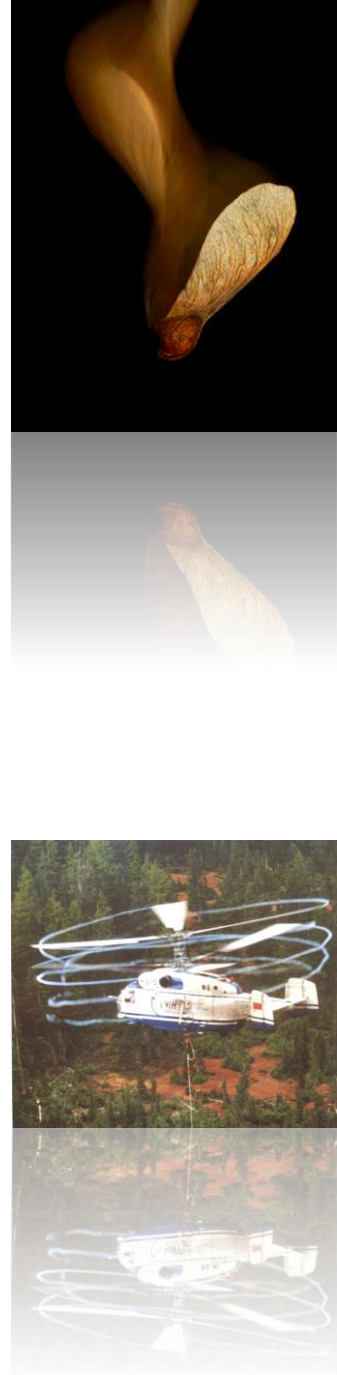


Fundamentals of Vertical Flight (straight up and down) Lecture 3

Dr Djamel Rezgui

djamel.rezgui@bristol.ac.uk



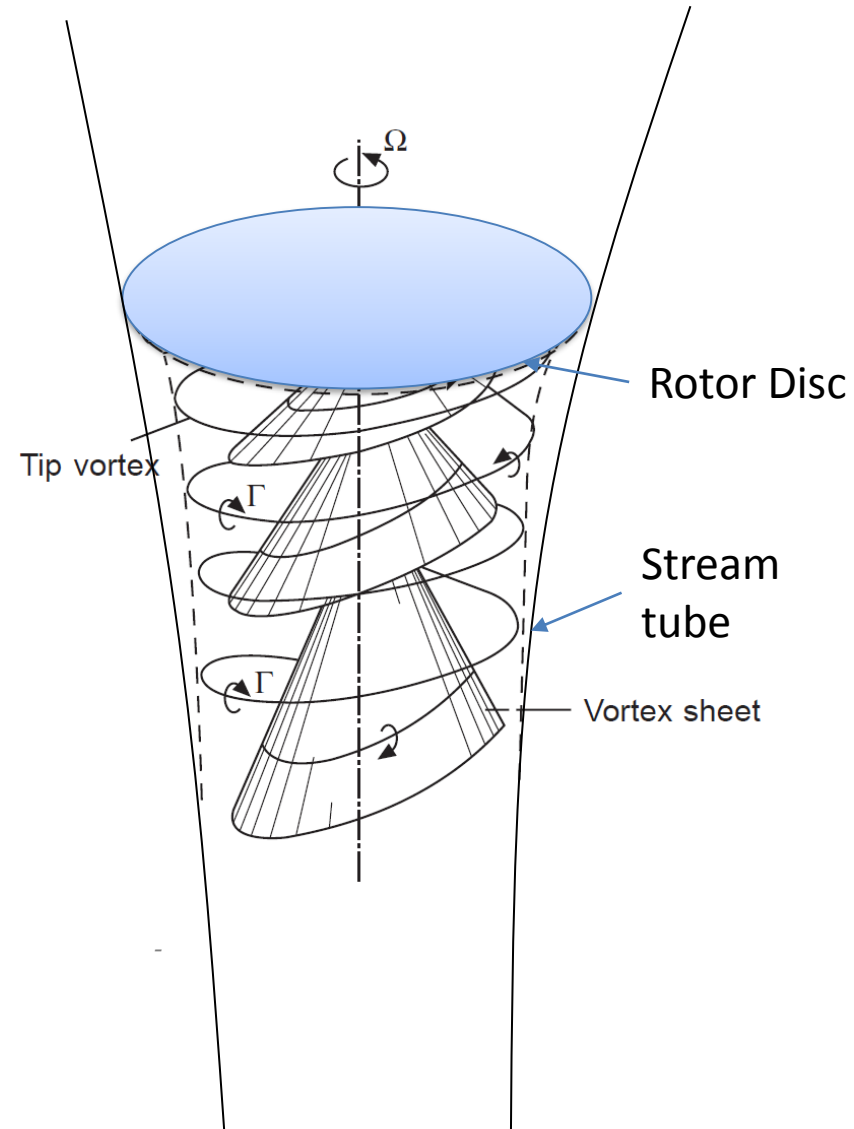
Axial Flight

Hover ... Climb ... Descent

- momentum analysis
- Axial flow states
- Universal Induced
Velocity diagram



Helicopter Aerodynamics in Axial Flight



Actuator Disc (Momentum) Theory

The Lifting Rotor in its most simplistic form is a Propeller.

Mechanical energy (in the form of rotating blades) is used to accelerate **(a)** a mass **(m)** of air.

Newton's law (every action has a reaction), states $F=ma$, where F , is the rotor thrust **(T)**.

Applying Bernoulli's equation:

$$H_0 = P_0 + \frac{1}{2} \rho V^2 = P_1 + \frac{1}{2} \rho (V + v)^2$$

$$H_1 = P_0 + \frac{1}{2} \rho (V + v_1)^2 = P_1 + P' + \frac{1}{2} \rho (V + v)^2$$

Subtracting H_0 from H_1 results in

$$H_1 - H_0 = \frac{1}{2} \rho (2Vv_1 + v_1^2) = P'$$

However, the Thrust=change of axial momentum per unit time

$$\frac{T}{A} = P' = \rho (V + v)v_1$$

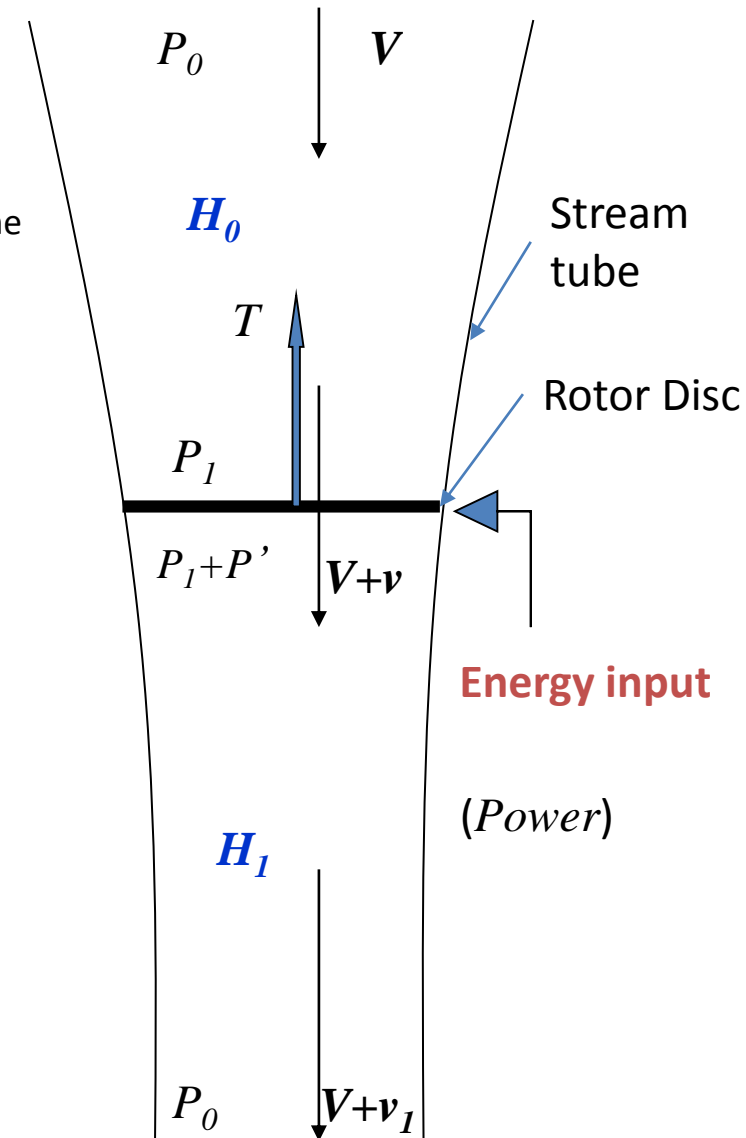
Where ρ is the air density and A is the rotor disc area

Hence

$$\frac{v_1}{2} = v \quad \text{or} \quad v_1 = 2v$$

$$\text{Thrust: } T = 2\rho A(V + v)v$$

$$\text{Power: } P = T(V + v)$$



Momentum Theory in Hover

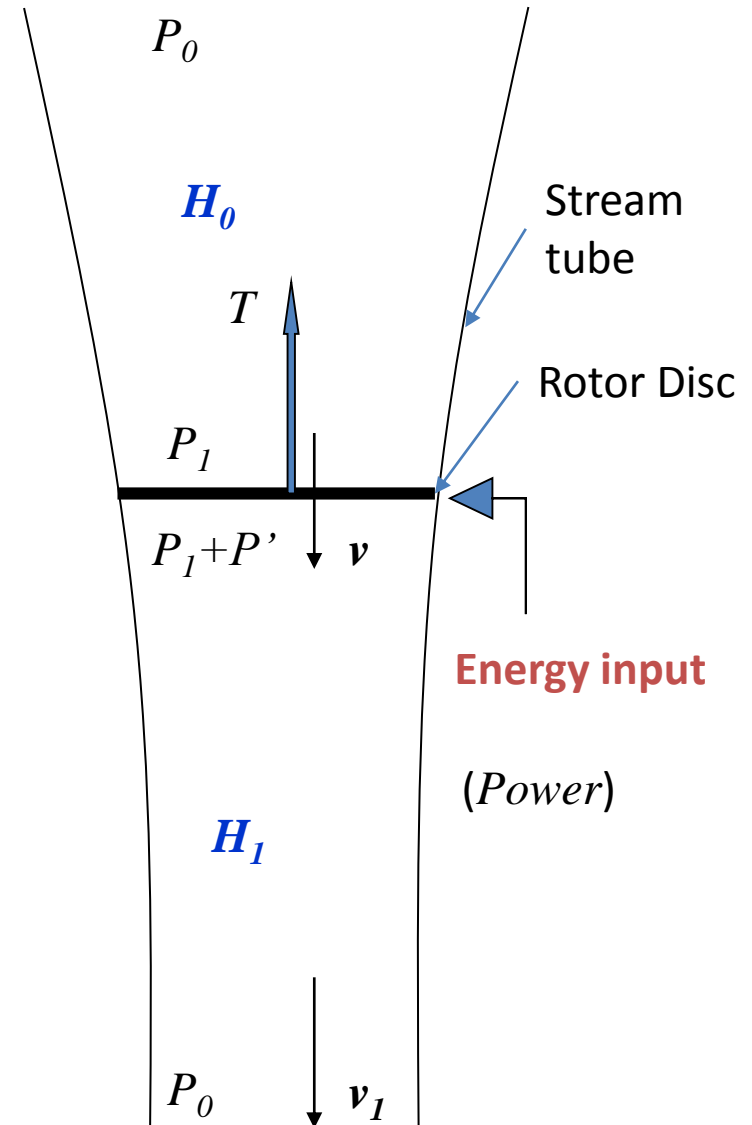
Or a lifting rotor
in **hover**, when
the onset velocity

$$V = 0$$

$$v_h = \sqrt{\frac{T}{2\rho A}}$$

$$P_h = T v_h \quad \text{Hence}$$

$$P_h = \frac{T^{3/2}}{\sqrt{2\rho A}}$$

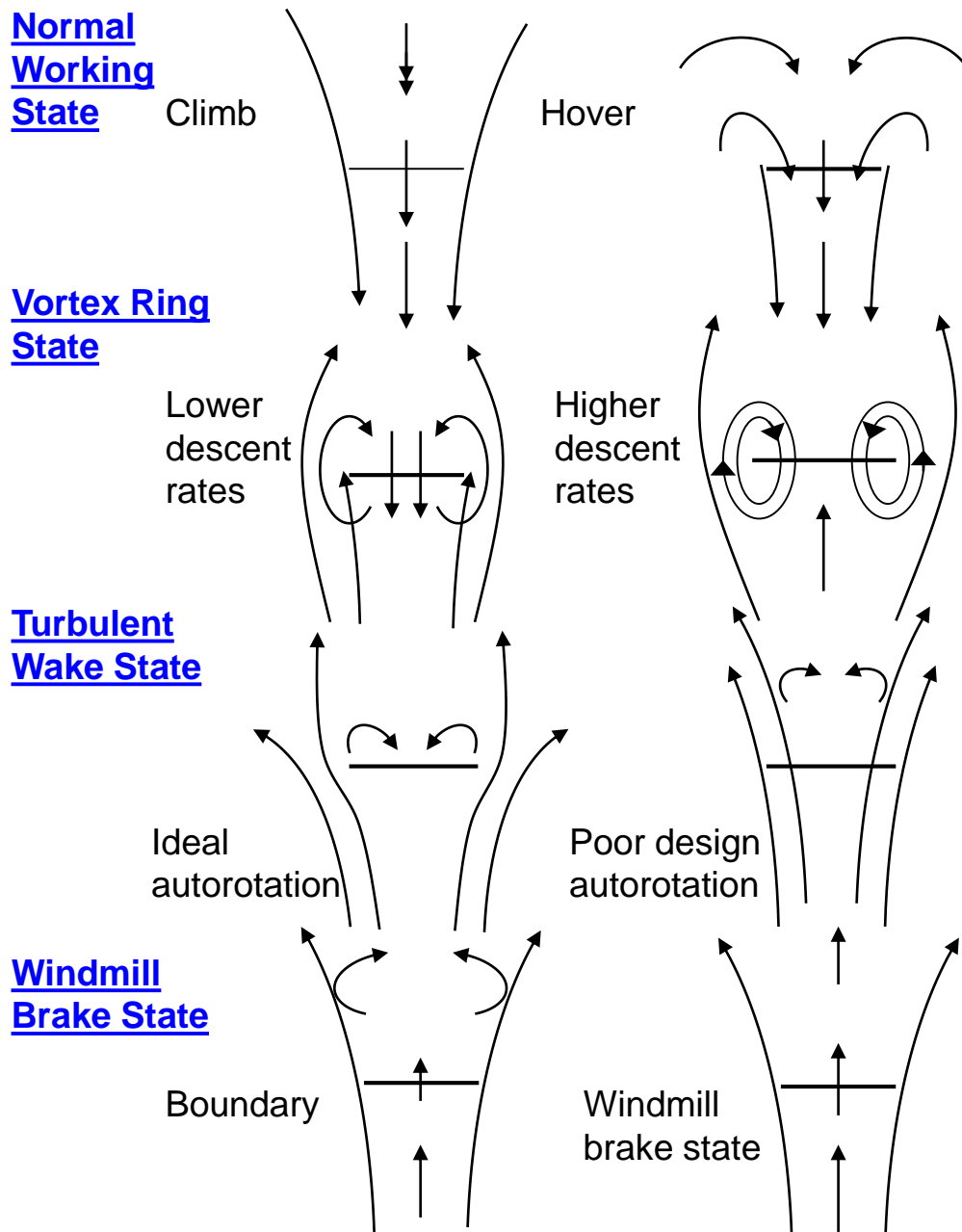


AXIAL FLOW STATES

The vertical climb and hover states (and to a certain extent the slow decent) are easily analysed by momentum considerations, as already discussed.

Higher rates of decent can be problematic, both analytically (as the stream tube no longer exists) and in piloting the craft.

Following a total engine failure the helicopter pilot will descend the aircraft into the upper region of the turbulent wake state.



THE OPERATING STATES

The Rotor in BLUE

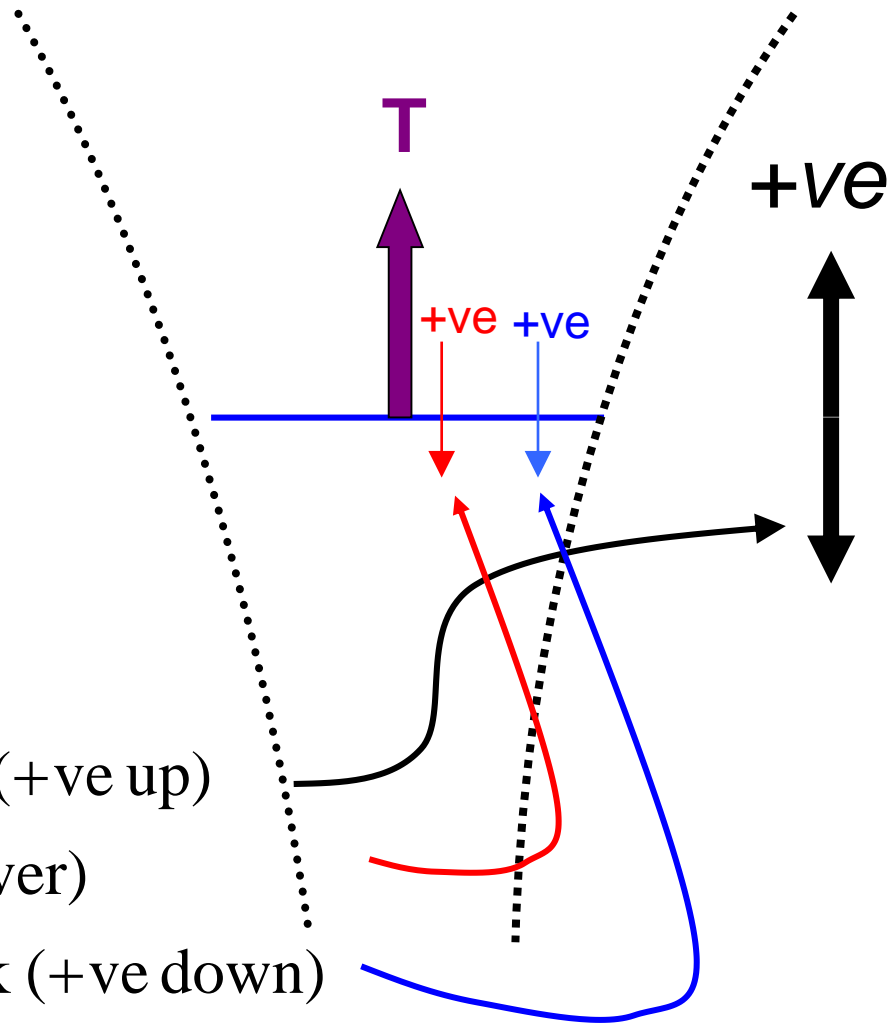
A Constant and always **POSITIVE**
THRUST is produced in each state.

V_V is the Aircraft Vertical Velocity (+ve up)

v is the induced velocity, v_h (in hover)

U is the flow through the rotor disk (+ve down)

Note : V_C is the air flow velocity due to Aircraft Vertical motion ($= -V_V$)



NORMAL WORKING STATE

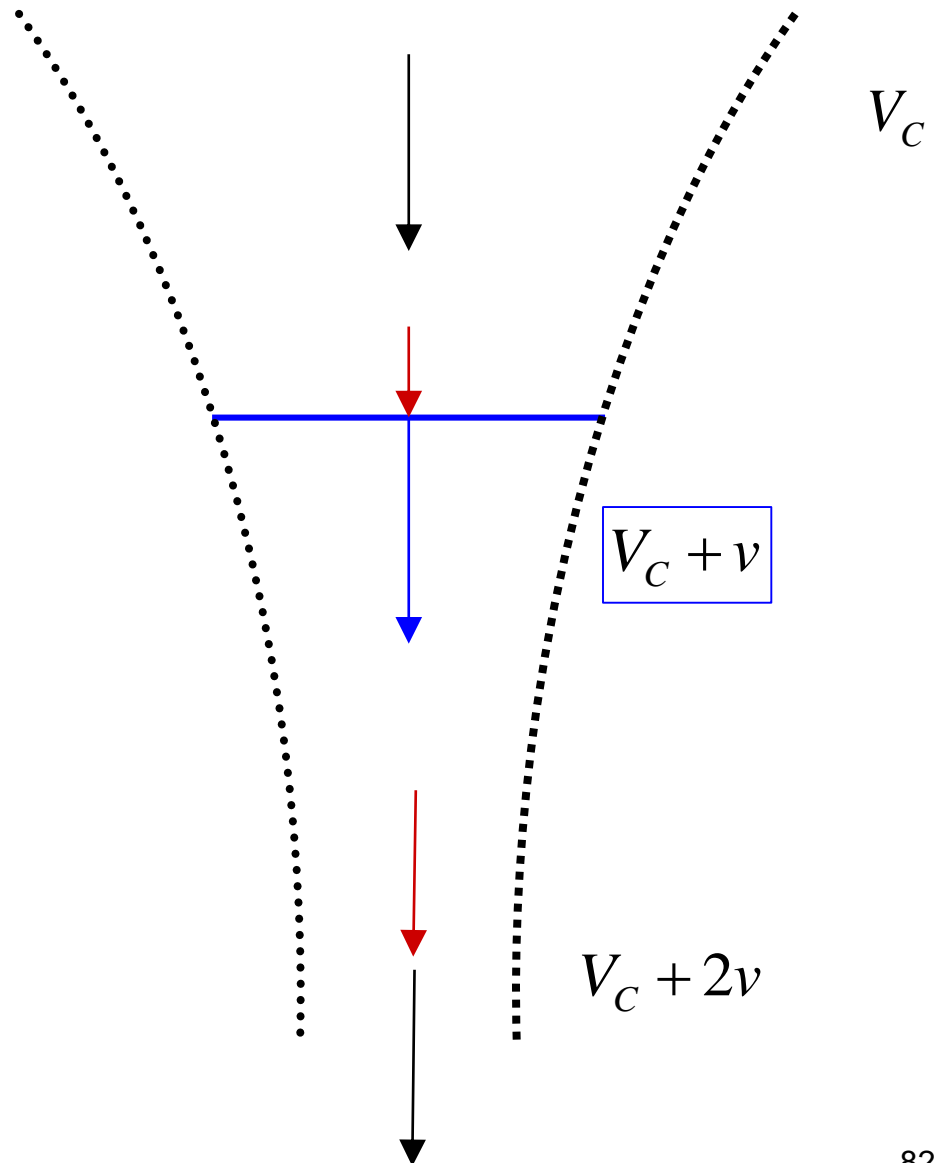
The Rotor in CLIMB

Momentum Theory applies as
an effective stream tube exists.

$$V_v > 0$$

$$v < v_h$$

$$U > v$$



NORMAL WORKING STATE

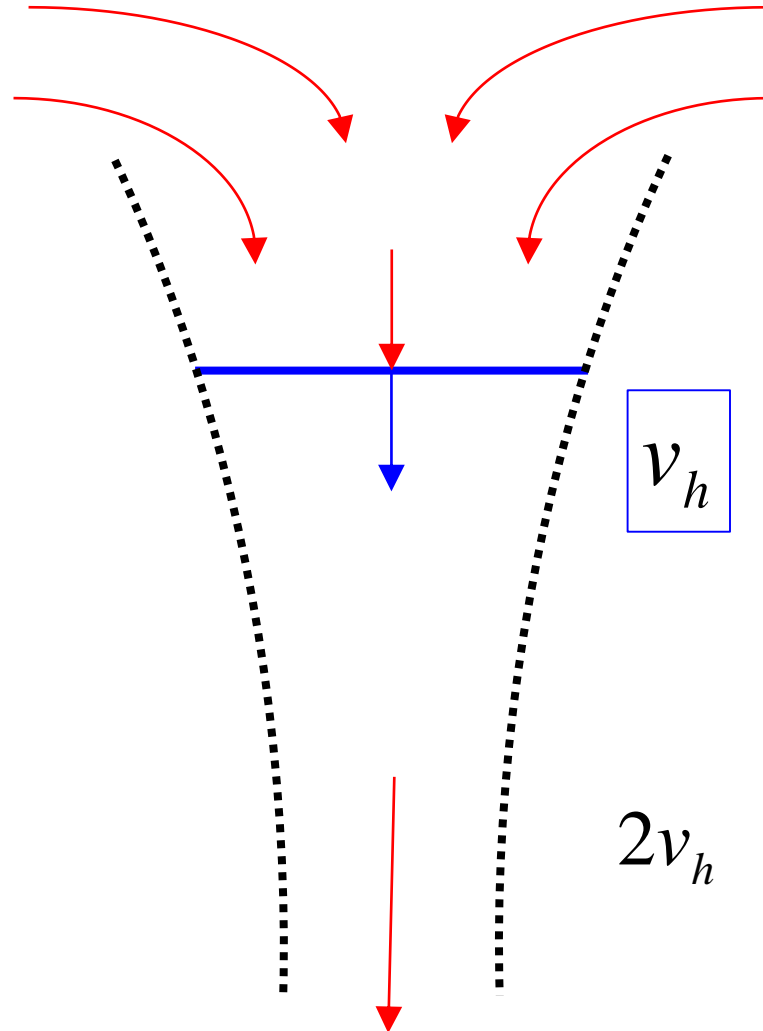
Rotor in HOVER

Momentum Theory applies as
an effective stream tube exists.

$$V_V = 0$$

$$v = v_h$$

$$U = v$$



VORTEX RING STATE

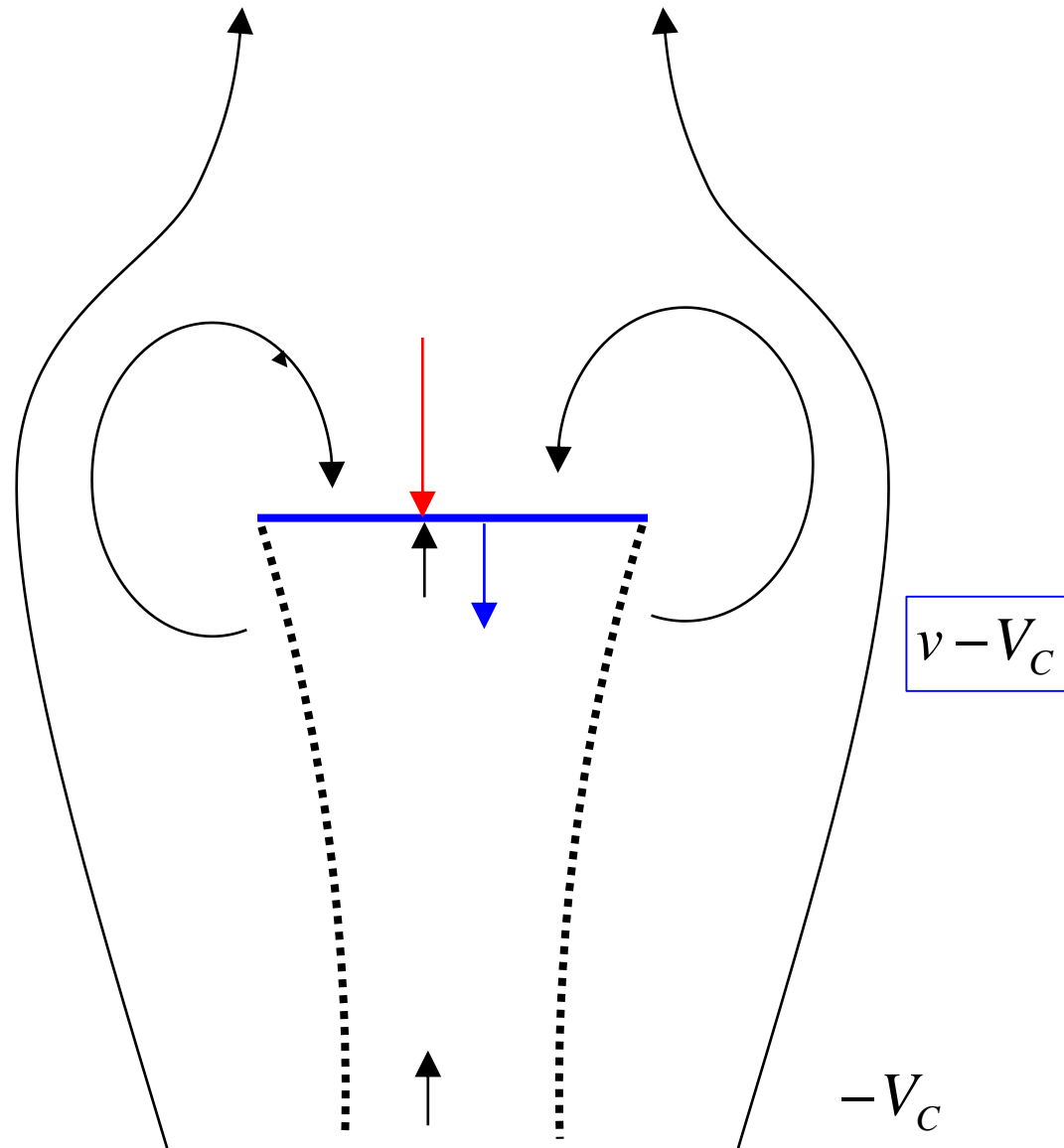
Rotor in VERY SLOW DESCENT

Momentum Theory applies as
an effective stream tube exists.

$$0 > V_v \geq \left(\frac{-v_h}{2} \right)$$

$$v > v_h$$

$$U < v$$



VORTEX RING STATE

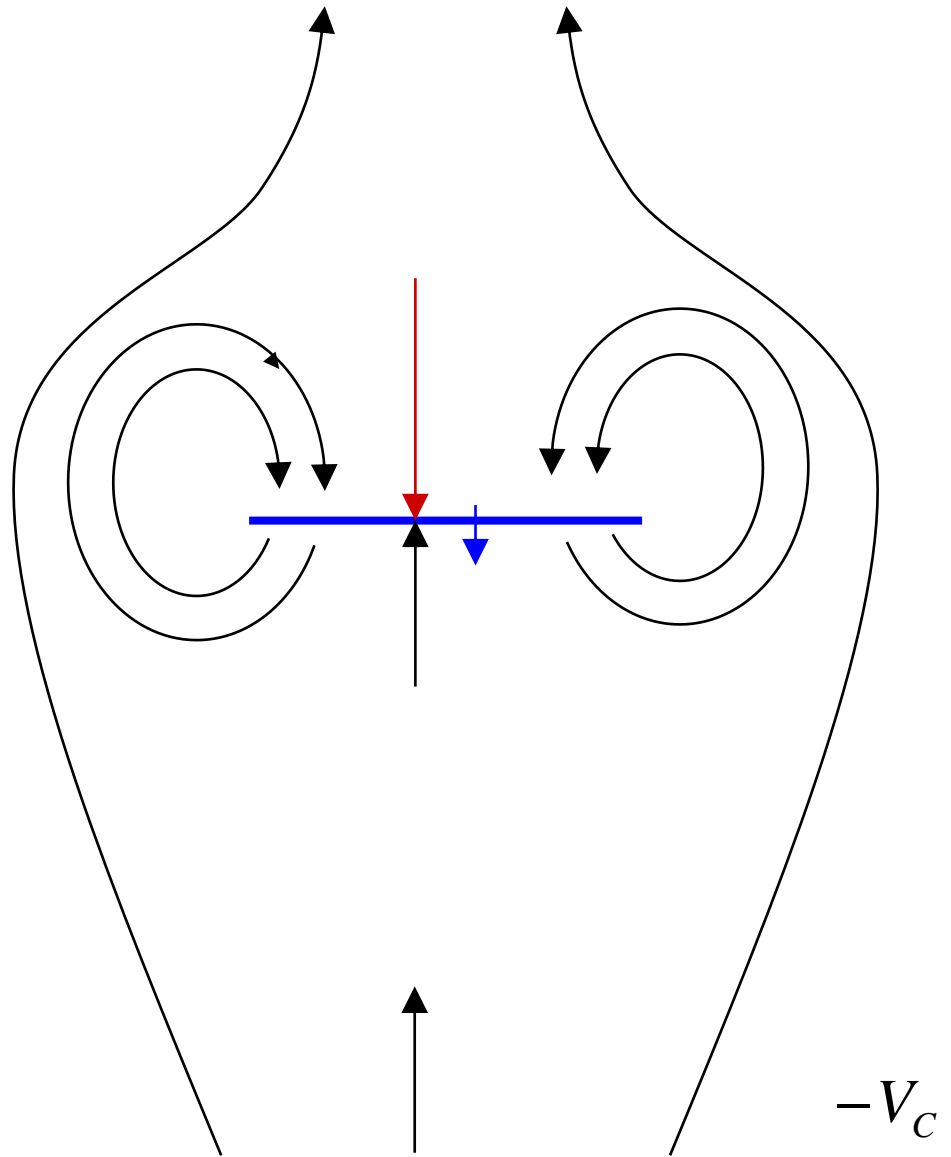
Rotor in SLOW DESCENT

Momentum Theory does not
apply as no effective stream
tube exists.

$$\left(\frac{-v_h}{2} \right) \geq V_V \geq -v_h$$

$$v \gg v_h$$

$$U < v$$



TURBULENT WAKE STATE

Rotor in MODERATE DESCENT

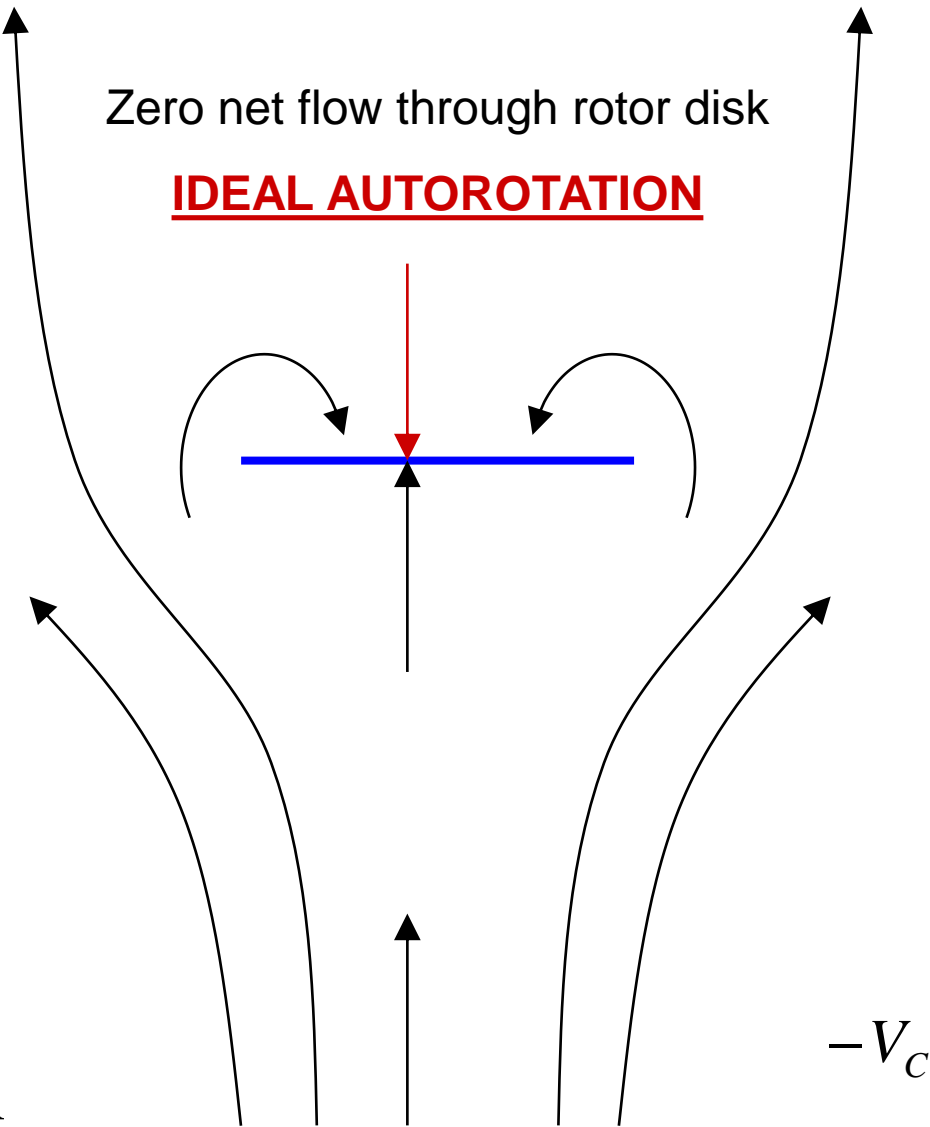
Momentum Theory does not
apply as no effective stream
tube exists.

$$-v_h \geq V_V \geq -\frac{3}{2} v_h$$

$$v > v_h$$

$$U \leq 0,$$

$$U \approx 0 \text{ ideal autorotation}$$



TURBULENT WAKE STATE

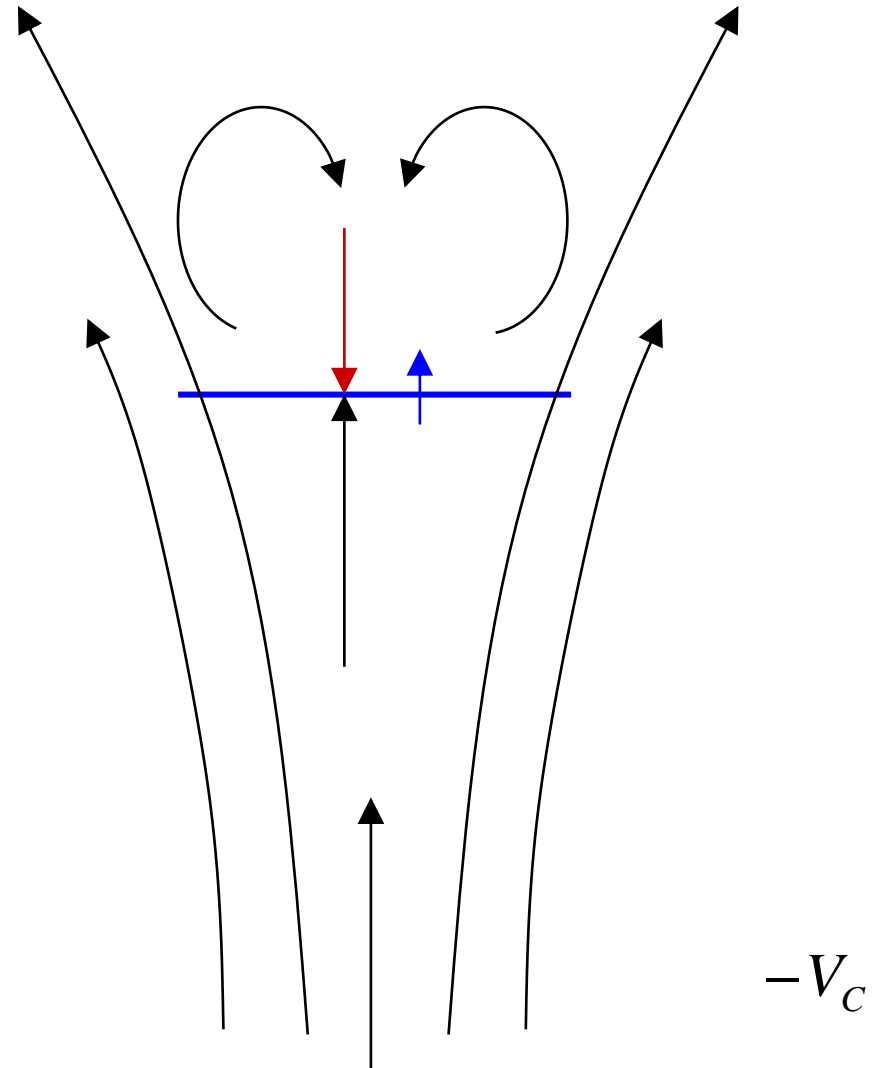
Rotor in HIGH DESCENT RATE

Momentum Theory does not
apply as no effective stream
tube exists.

$$-\frac{3}{2}v_h \geq V_V \geq -2v_h$$

$$v \geq v_h$$

$$U < v \text{ (and -ve in value)}$$



WINDMILL BRAKE STATE

Rotor in VERY HIGH DESCENT RATE

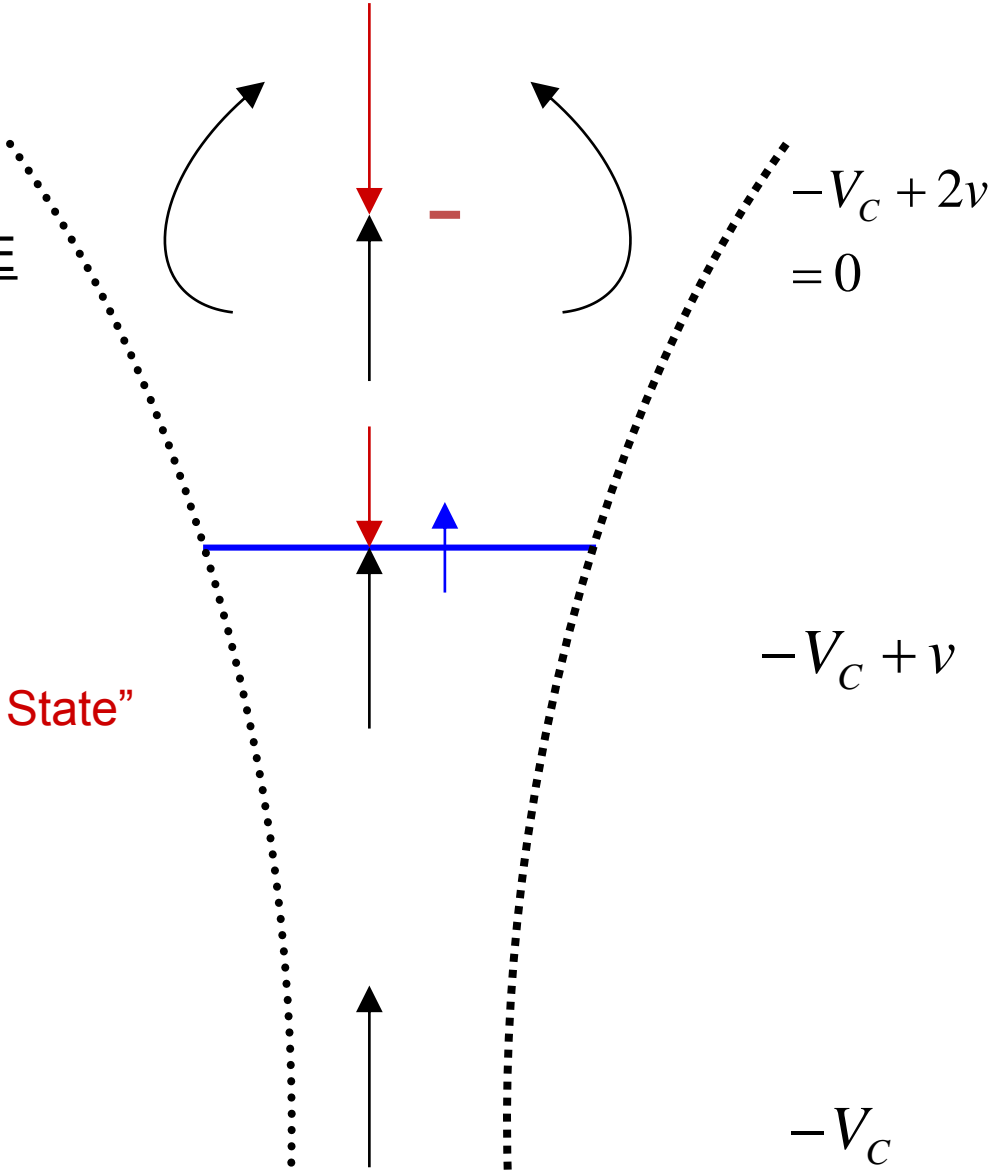
Momentum Theory applies as
an effective stream tube exists.

This is analogous to “Normal Working State”

$$V_v \leq -2v_h$$

$$v \approx v_h$$

$$U \leq v \text{ (and -ve in value)}$$



WINDMILL BRAKE STATE

Rotor in EXTREME DESCENT RATE

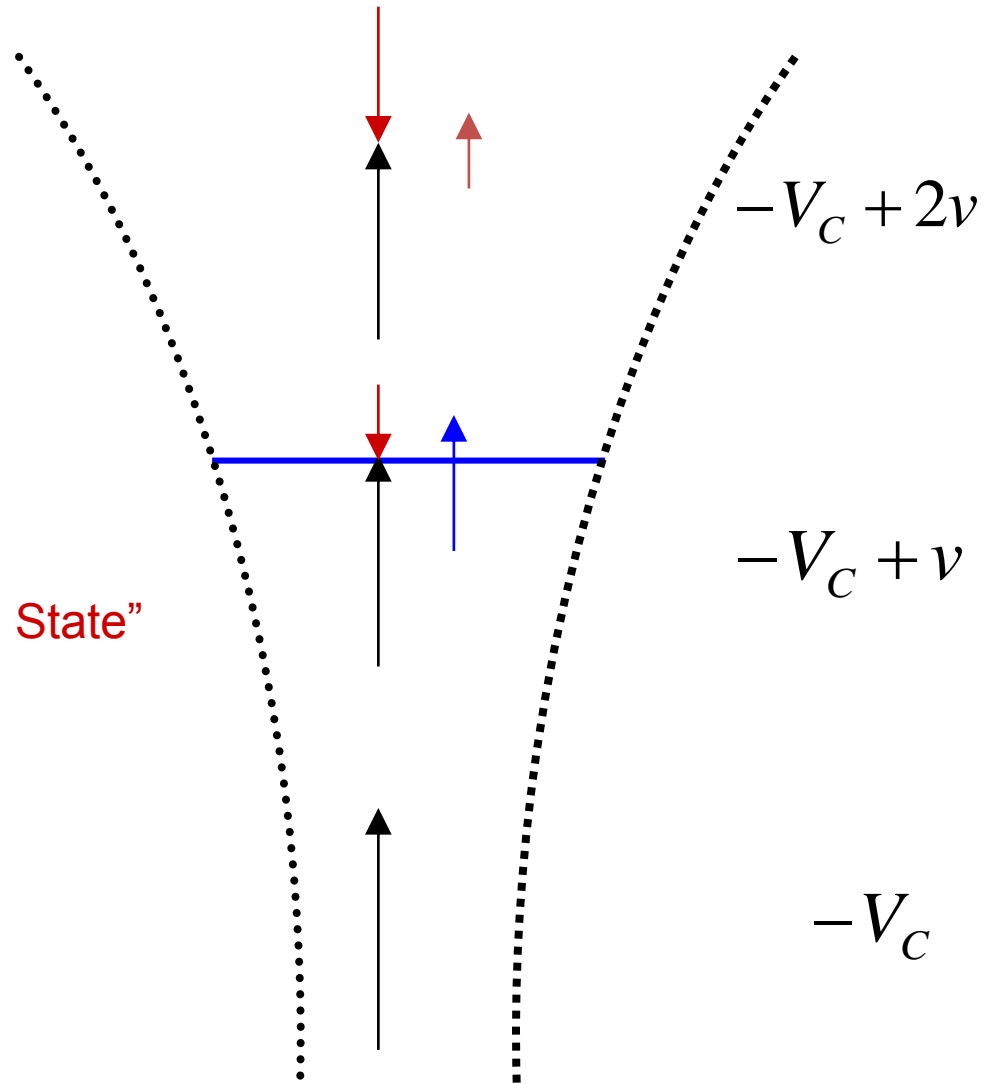
Momentum Theory applies as
an effective stream tube exists.

This is analogous to “Normal Working State”

$$V_v \ll -2v_h$$

$$v < v_h$$

$$U \geq v$$

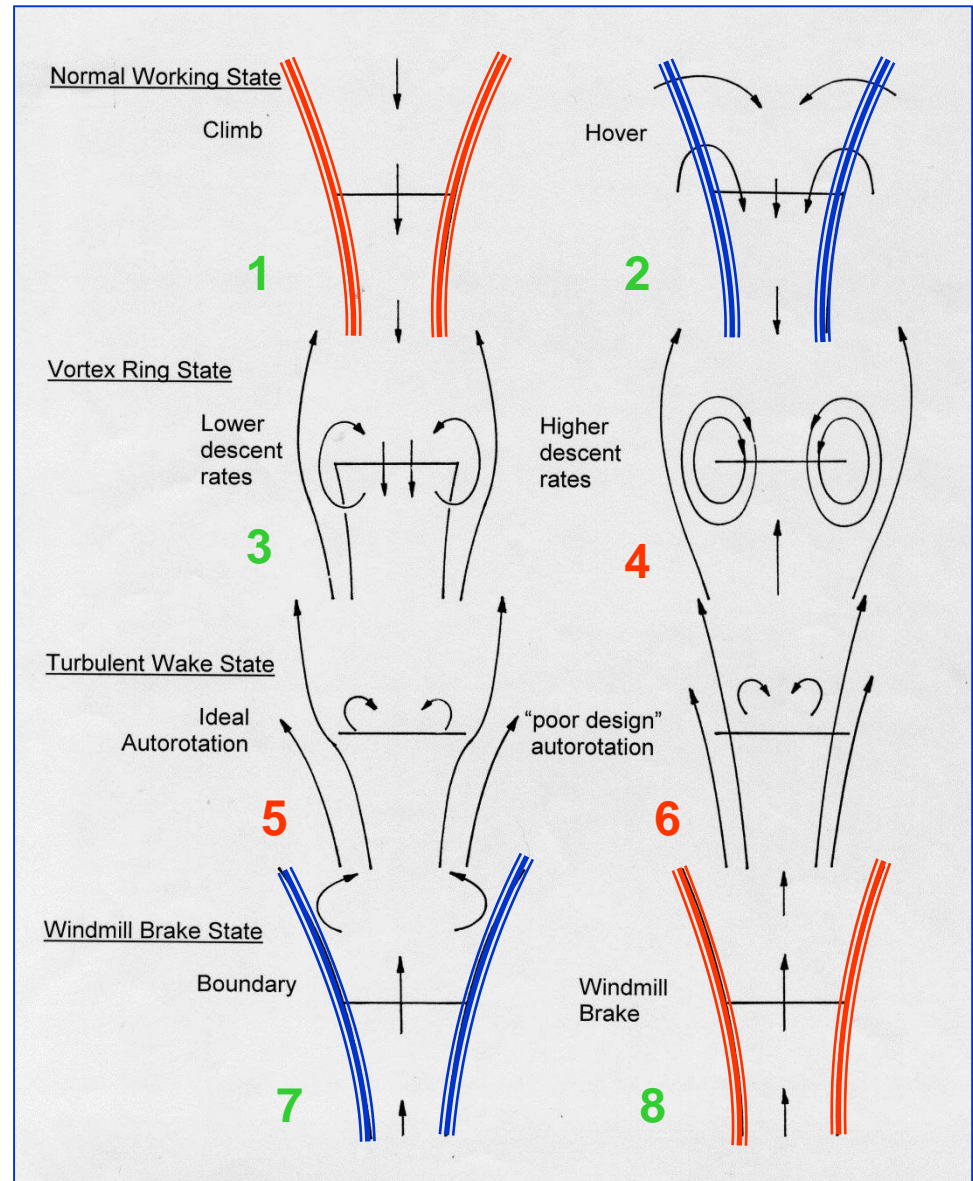


AXIAL FLOW STATES

The vertical climb and hover states are easily analysed by momentum considerations (as already discussed) and to a certain extent the slow decent.

Higher rates of decent can be problematic, both in analysis (as the stream tube no longer exists) and in piloting the craft.

Following a total engine failure the helicopter pilot will descend the aircraft into the upper regions of the turbulent wake state.

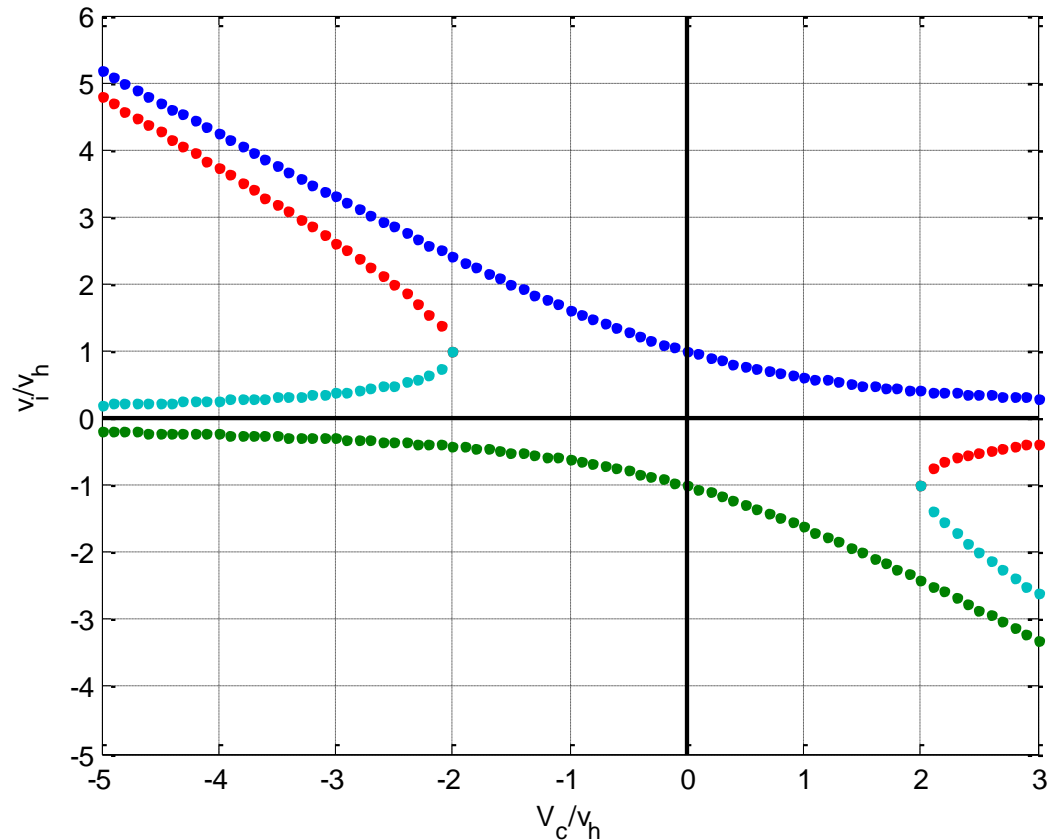


Question

- Starting from $T_{Hover} = T_{AxialFlight} = T$,
- i.e. $2\rho A v_h^2 = 2\rho A(V + v)v$
- Plot the variation of $\frac{v}{v_h}$ as a function of $\frac{V}{v_h}$

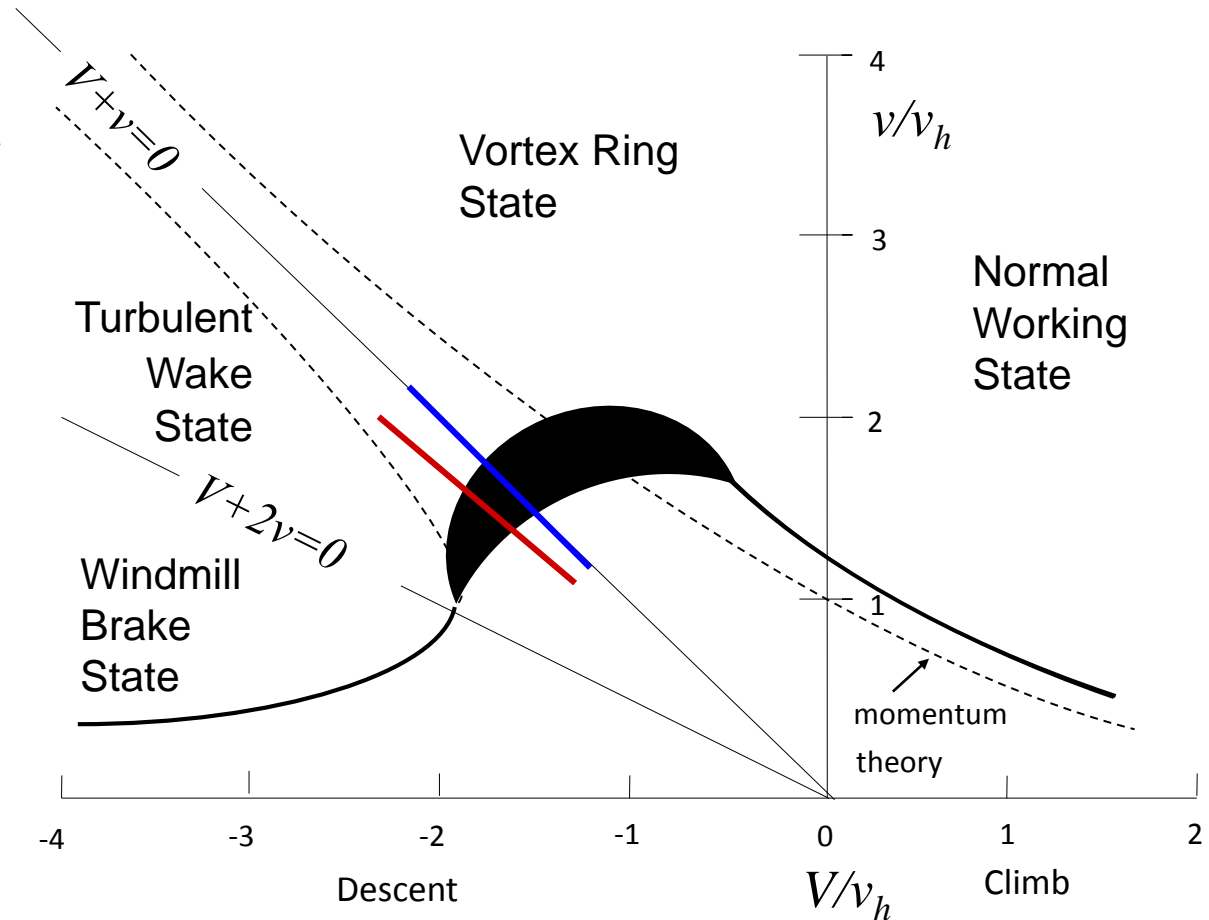
Answer

$$\frac{v_i}{v_h} = -\frac{V_c}{2v_h} \pm \sqrt{\left(\left(\frac{V_c}{2v_h}\right)^2 \pm 1\right)}$$



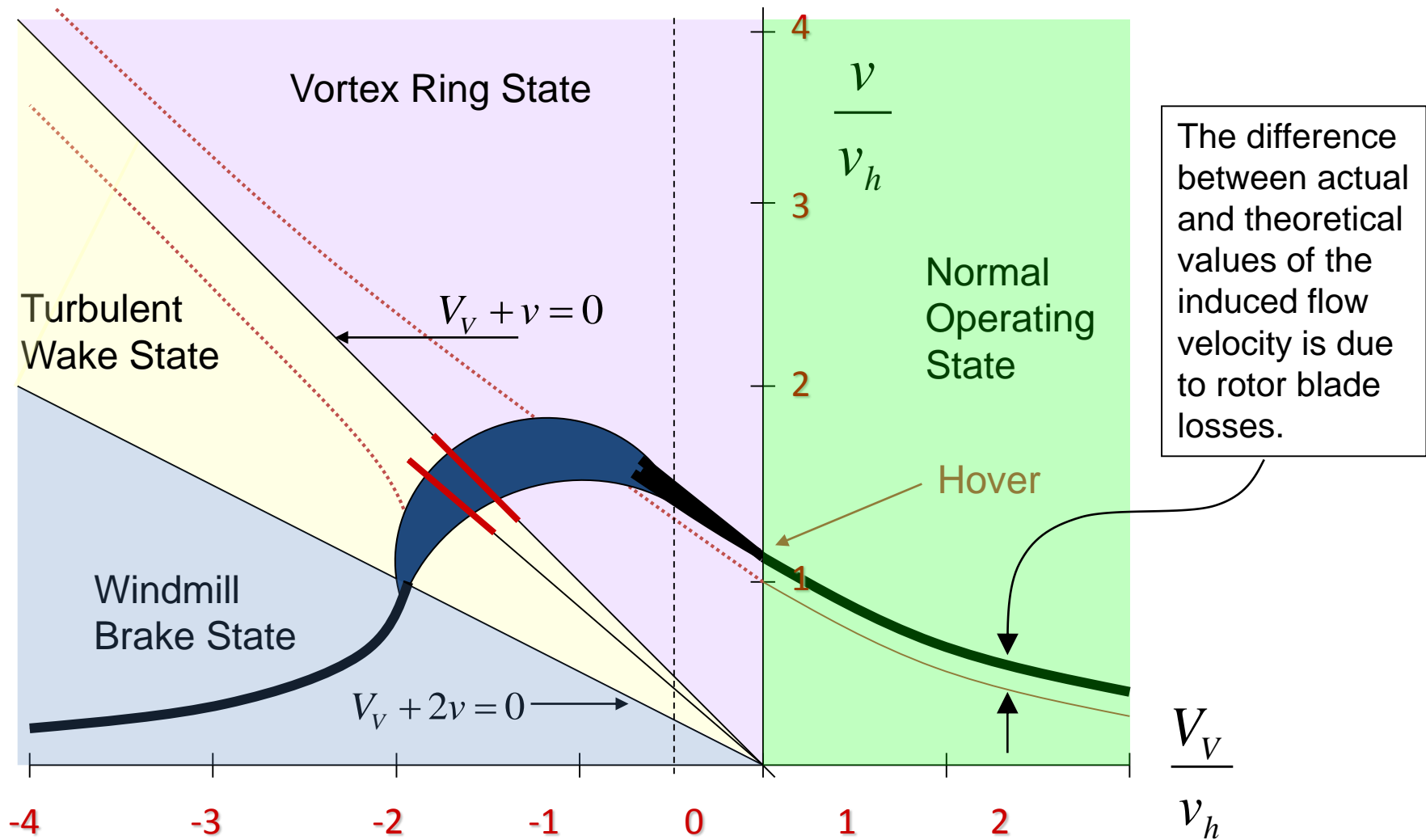
ALL THESE FLOW STATES

can now be summarised on one diagram, the **Universal Induced Velocity Curve**. The **dark area** is literally a “grey area” as it cannot be solved analytically and therefore comprises of empirical obtained by flight test.



The induced velocity (Y-axis) and the helicopter rotor's vertical velocity (X-axis) have been non-dimensionalised by the rotor induced velocity in the hover.

The Universal Induced Velocity Diagram



Remembering that $P = T(V + v)$, then at $(V + v) = 0, T \neq 0, P = 0$

HELICOPTER in Vortex Ring State



It is important to design for low autorotation rates