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# **Sound control in windy weather**

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Master Thesis  
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Aalborg University  
Electronic Engineering and IT

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# Preface

This report is composed by Jonas Buchholdt during the 10th semester of Electronic Engineering and IT at Aalborg University. The general purpose of the report is *Signal Processing and Acoustics*.

For citations, the report employs the Harvard method. If citations are not present by figures or tables, these have been made by the authors of the report. Units are indicated according to the SI standard.

Aalborg University, May 21, 2019

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# Glossary

**DLL** Dynamic Link library. 157

**DSP** Digital Signal Processor. 82

**FDTD** Finite-Difference Time-Domain. 16

**FIFO** First In First Out. 63

**FOH** Front Of House. 9, 27

**IP** Internet Protocol. 157

**PA** Public Address System. 7, 8

**SPL** Sound Pressure Level. 7, 8, 9, 10, 11, 12, 13, 17, 18, 21, 24, 25, 26, 27, 29, 30, 31, 37, 38, 39, 41, 42, 43, 45, 46, 47, 48, 49, 50, 54, 56, 57, 60, 61, 64, 67, 69, 70, 72, 73, 74, 75, 77, 84, 93, 111, 112, 113, 131, 162, 181, 182, 183, 184, 187, 192, 194

**TTL** Transistor–Transistor Logic. 157

**UDP** User Datagram Protocol. 157



# **Chapter 1**

## **Introduction**

Coming later



# **Part I**

## **Problem Analysis and Requirements**



## Chapter 2

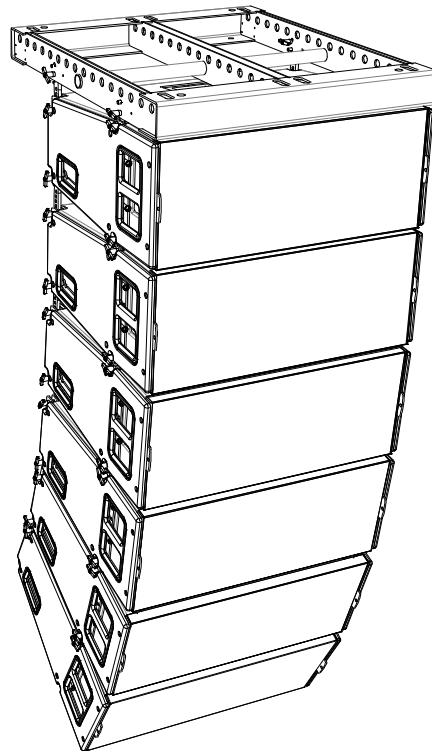
# Analysis of sound propagation in outdoor venue

### 2.1 Live venue sound challenges

This section explores the challenges of producing sound in an outdoor environment. The challenge of producing a good sound experience for the audience highly depend on the calibration method and the atmosphere condition. It is well known that acoustically wave propagation is strongly affected by the inhomogeneous atmosphere doing the outdoor sound propagation. This inhomogeneous atmosphere shifts the calibration of the sound system which affects the intelligibility. In section 2.1.1 an overview of high Sound Pressure Level (SPL) Public Address System (PA) system is discussed.

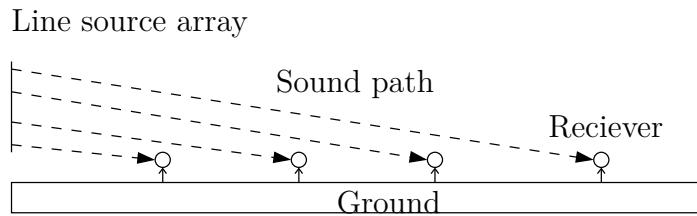
#### 2.1.1 Acoustics as live venue

An outdoor PA system is an essential sound reinforcement concept today. It is used to address information, music or just entertainment where the number of audiences is large, sometimes more than 10.000 audiences. The number of the audience makes it difficult to address the information to a large number of the audience without the reinforcement of the information. The reinforcement is nearly always done from a stage with a sizeable PA system and sometimes delay unit in the middle of the audience area. The stage lifts the artist while the PA system is designed to cover the audience area with sound. The optimal PA system covers the area with a linear frequency spectrum in the audible frequency range with a homogeneous SPL. Today, the used speaker is a line source array flown in both side of the stage and is therefore only close to the audience in front of the stage. The line source array is an array of small identically wide speakers attached to each other, to form a vertical line of speakers. An example of a line source array is shown in Figure 2.1



**Figure 2.1:** The figure shows an illustration of a KUDO line source array from L-Acoustics [L-Acoustics, b]

Every speaker or a small group of the line source array can be controlled individually, both in sound coverage area angle and SPL. The benefit of using the line source array design is that the coupling between the speaker makes a line acting source. With an optimised control system of the line source array, the audience area is covered with sound such that all audience can hear the information without damage the ear of the frontal audience. An optimised line source array has, for example, an optimised main lobe such that the lower part of the main lobe lays flat along the audience area. The following Figure 2.2 shows a graphical illustration of the outdoor PA venue concept.



**Figure 2.2:** The figure illustrate the concept of outdoor PA venue

As shown in Figure 2.2, the distances from one element in the line source array to the receiving audience dependent on the audience position. The distance indicates that the signal to every line source element has to be set individually to cover the audience area with homogeneous SPL. The individual control of the source is necessary because of the wave amplitude decay with distances. This phenomena is addressed in section 2.2. The adjustment is not as simple as just supply the upper speaker with more power. A sound wave is a mechanical movement of the particle in the air, which condense and compress the air molecule, then low pressure and high pressure respectively. The movement of the molecule depends on the medium, and in this thesis, the medium is limited to air. The SPL is the pressure divination of the instantiates atmospheric pressure. The atmospheric pressure, therefore, set a lower bound on the condensation while very high pressure changes the speed of sound and distort the wave as it propagates. To ensure that the information is communicated to the audience without distortion, the limitation is addressed in section 2.3.3. The medium in the air is not constant and varies over time regarding pressure, wind, humidity and temperature. The analysis starts with the experience for live concert of the author in section 2.1.2, next section 2.3 address the impact of homogeneous atmospheric effect on sound propagation. Then section 2.3 address the impact of inhomogeneous atmospheric effect on sound propagation.

### 2.1.2 Author experience of live concert

The Author of the thesis has experience with live concert both as an audience and as a sound engineer. The aspect of being the sound engineer and an audience to a live concert is very different. As a sound engineer, the area for controlling the sound is a secured area with a tent as protection. The tent roof often shadows for the high frequency, and the walls make standing waves of the low frequency because the distance between parallel tent walls fits with the wavelength for the low frequency. The sound engineer control area is defined as the Front Of House (FOH). The FOH is often equipped with an additional speaker, and the sound engineer does not fully know how it sounds outside the FOH, but base there mixes on experience ???. The aspect of being an audience depends on where the audience is regarding the stage. In close hand to the stage the SPL is high and often too high especially in the low frequency. The low frequency is often made as a vertical array at the ground or two end-fire arrays and shall be able to exhibit all audience by an audible low frequency spectrum typically from 25 Hz but one company extends down to 13 Hz. Therefore the SPL just in front of the subwoofer has a very high SPL. This position is not comfortable to be at in longer period, and the high SPL mask the higher frequency. The optimal audience position is in the centre of the stage and not as long from the stage as the delay towers. The average SPL is often less than 102 dB SPL since the sound engineer try to keep a maximum average SPL at 102 dB SPL just in front of the FOH. Moreover, it is the stereo sweet spot. This position is the only position where the stereo image is optimal. The stereo perspective problem is a hot topic nowadays, both L-Acoustics [L-Acoustics, 2019] and D&B Audiotechnik [d&b audiotechnik,

2019] have made their own solution to the problem. The idea is to fly many small line source array above the stage and assign every musician to their own line source array. The concept minimises the interference between two line source array playing the same mono signal. Near the delay towers or approximately 50 m from the main stage, the low frequency spectrum is still sharp and audible but something happens to the high frequency. Often the high frequency disappears for a few seconds and gets back. This phenomenon alters through the full concert. Behind the delay towers, the line source array in the delay tower reproduces the sound such that the audience in the back also gets the high frequency spectrum. The question is why does the high frequency disappear for a short period when the low frequency does not? This analysis focus on finding the atmospheric condition which cause the phenomena.

## 2.2 Ideal geometric spreading loss

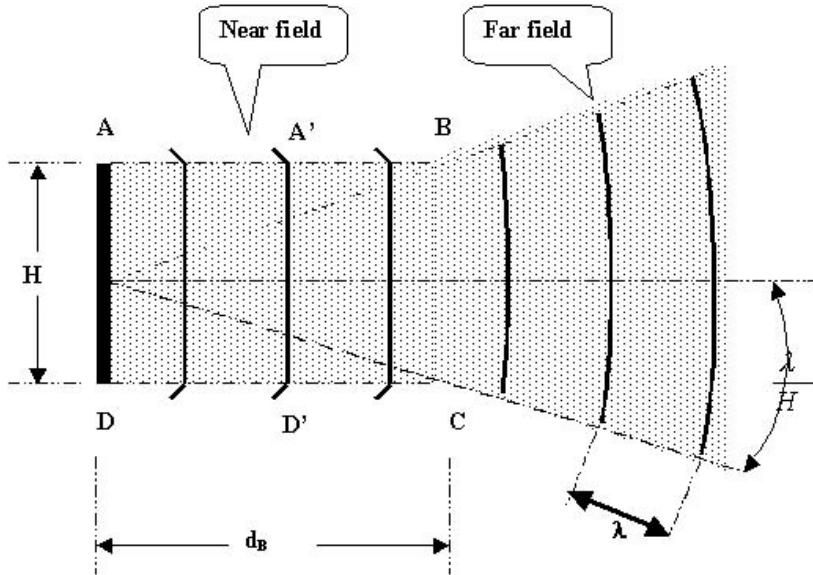
When a line source generates a sound wave, the wave field exhibits two fundamental difference spatially directive regions, near-field and far-field. In near-field, the wave propagates as a cylindrical wave wherein the far-field the wave propagates as a spherical wave. When the wave propagates as a cylindrical wave, the wave propagates only in the horizontal plane, and therefore the attenuation is 3 dB SPL per doubling of distance. For a spherical wave propagation, the wave propagates in all direction. Therefore the attenuation is 6 dB SPL per doubling of distance. The near-field and far-field attenuation are based on non-absorption homogeneous atmospheric conditions. The border between the near-field and far-field depends on the height of the array and the frequency. The distance can be calculated with Fresnel formula Equation 2.1, where the wavelength  $\lambda$  is approximated to  $\frac{1}{3f}$  [Bauman et al., 2001]

$$d_B = \frac{3}{2} f \cdot H^2 \sqrt{1 - \frac{1}{(3f \cdot H)}} \quad (2.1)$$

Where:

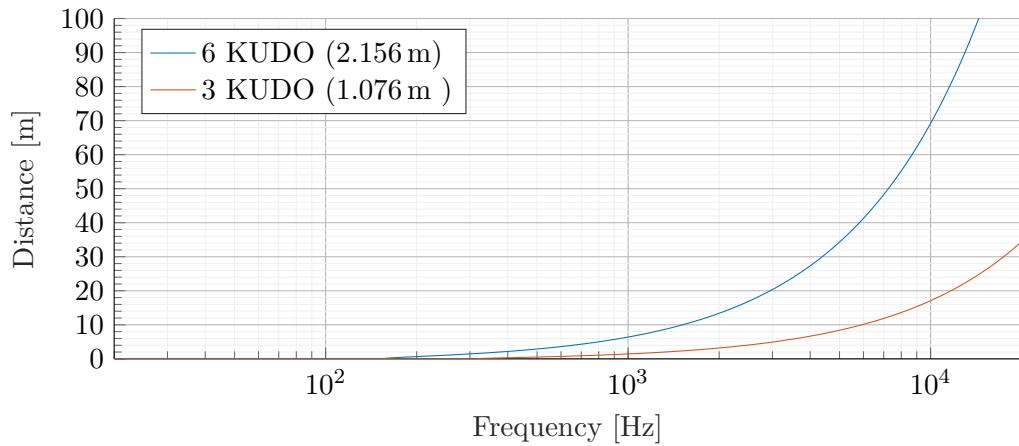
$d_B$	is the distance from the array to the end of near field	[m]
$f$	is the frequency	[kHz]
$H$	is the height of the array	[m]

In equation Equation 2.1 it can be calculated that less than 80 Hz radiate directly into spherical wave on the exit of the speaker no matter the height of the line source array. The following Figure 2.3 shows a horizontal cut of the near-field, far-field from a line source array.



**Figure 2.3:** The figure shows horizontal cut of a SPL radiation pattern of a line source array [Bauman et al., 2001].

As seen in Figure 2.3, the wave propagating as a plane cylindrical wave in the near-field, where the coverage area for every double of distance is twice as big. Since the coverage area is twice as big, the SPL is the half for the doubled distance. When the wave excites distance  $d_B$ , the wave propagates into far-field where the coverage area is four times higher while travelling the double of distance and therefore the SPL is four times less. In far-field, the wave propagates as a spherical sound source. The following Figure 2.4 gives two examples with different height.



**Figure 2.4:** The figure shows two height example calculated from Equation 2.1.

As seen in Figure 2.4, while the height is the double, the far-field is moved four times as far back.

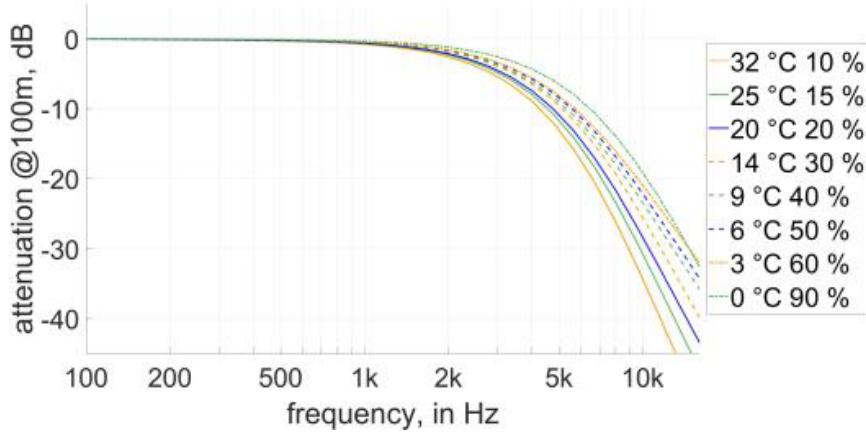
## 2.3 Homogeneous atmospheric conditions

This section aims to analyse the sound wave propagation in homogeneous atmospheric conditions. It is well known that the sound wave propagation is highly depending on the atmospheric conditions. The propagation depends on the atmospheric pressure, wind, temperature and humidity, where the two latter moreover is frequency dependent. The attenuation difference in frequency for temperature and humidity can be above 80 dB SPL [Corteel et al., 2017]. The following sections introduce a brief discussion of homogeneous atmospheric conditions effect on sound propagation.

### 2.3.1 Humidity and temperature impact

The temperature and humidity have three impacts on wave propagation from a line source array, directionality of the speaker, the speed of sound and a lowpass effect. The following description starts with the latter.

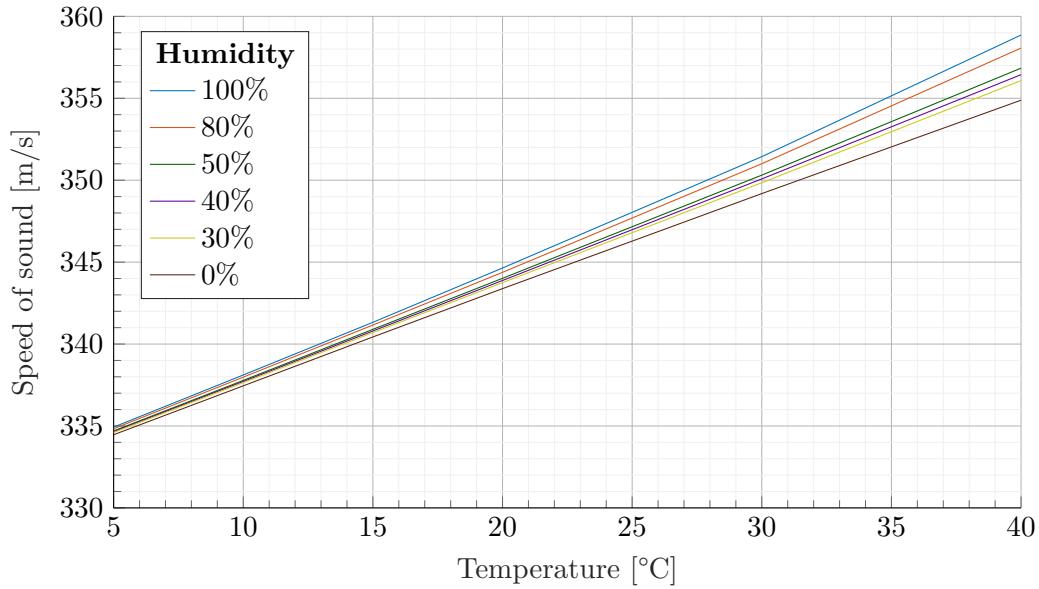
**Lowpass effect** The effect of humidity and temperature on wave propagation act as a lowpass filter while the wave propagates. The low frequency remains without any additional attenuation where the high frequency highly depends on the atmospheric condition. In other words, attenuation in the high frequency range does not only depends on the spreading loss but also temperature and humidity. Therefore, for long distance, the atmospheric conditions have a high influence on the frequency spectrum delivered to the audience. Humanity and temperature attenuation are already well studied and standardised. Standard [ISO 9613-1:1993] gives an overview of calculating the SPL attenuation concerning the frequency, distance, temperature and humanity. The article [Corteel et al., 2017] gives some examples of attenuation at a distance of 100 m. The article shows that if humanity increases proportionally to the temperature, the lowpass effect is small. If the change in temperature and humanity is the opposite of each other, for example, high temperature but dry, the attenuation in high frequency is significant. The following Figure 2.5 shows the worst-case scenario from [Corteel et al., 2017].



**Figure 2.5:** The graph shows the attenuation in dB with respect to frequency, humanity and temperature [Corteel et al., 2017].

As shown in Figure 2.5 the attenuation in the high frequency is significant and exceed 30 dB SPL within the audible frequency range. The attenuation is such markedly that applying more power does not cover the attenuation without an extreme high-pressure driver. That driver might be possible to design in theory but not in practice. Extreme high-pressure drivers introduce high distortion as is explained in section 2.3.3

**Speed of sound** The second consequence is the speed of sound. At temperature range from 0 °C to 40 °C the speed of sound with respect to humanity change is sparse and mostly only depend on temperature change. At 0 % humidity, the speed of sound increases with 0.6 m/s for every increasing degree °C. At humanity higher than 0 % the speed of sound increase with respect to humanity, depends on temperature. At 0 °C the speed of sound increases with approximately 0.8 m/s when the humidity raises from 0 % to 100 %. At 30 °C the speed of sound increases with approximately 2.7 m/s when the humidity raises from 0 % to 100 % [Wong and Embleton, 1985] [Bohn, 1987]. The wave propagation speed start at 331.5 m/s at 0 °C and 0 % humanity. The following Figure 2.6 shows the speed of sound with respect to humanity and temperature.



**Figure 2.6:** The figure shows the increase of sound speed with respect to humanity and temperature [Bohn, 1987]

As seen in Figure 2.6, the effect of humidity is negligible compared to the effect of temperature changes, but as the temperature increases the humidity gets significant. At a temperature of 40 °C the speed of sound is changed 4 m/s from 0 % humidity to 100 %

**Directivity** The directivity of a line source array in the mid and high frequency is always controlled mechanically by a horn because the wavelength is short compared to the size of the speaker. At low frequency, the wavelength is too long to be controlled mechanically by a horn. Therefore the directional pattern is controlled via cancellation from a backwards pointing speaker. The directivity of both the low frequency and the high frequency driver suffers from temperature increased. At the high frequency, the main lobe gets narrower when the mechanical horn gets warmer, and the effect is notable when the sun directly heats up the horn. When the surface of the horn heats up by the sun, the temperature can get much warmer in the horn than the air temperature. Therefore the surface of the horn affect the directivity of the high frequency by radiate warm air from the surface. The reason that main lobe gets narrower is that the wavelength gets shorter at higher temperature [Levine et al., 2018]. The directivity of the low frequency is affected as in the high frequency with the temperature increase. The difference is not as significant as in the high frequency since there is no surface heat. The directivity is then not affected due to the sunlight, but only the temperature increasing and decreasing. As in the high frequency temperature differences change the wavelength, and then the length be-

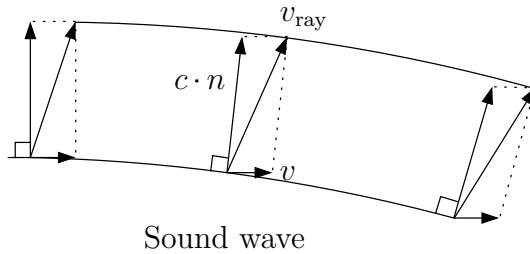
tween the speaker in a cardioid low frequency does not match the optimised distance between the speaker more.

### 2.3.2 Wind impact

The wind influence is depending on the angle of the wind direction with respect to the direction of sound propagation. A homogeneous wind is a laminar wind flown with the same homogeneous speed. The following analysis assumes homogeneous laminar wind flow from one direction. The analysis is of both oblique wind and parallel wind with respect to the frontal direction of the line source array. The analysis starts with the latter.

**Parallel to sound propagation** When the wind flows in the same direction as the sound wave propagation, the wind flow in m/s is an addition to the speed of sound. When the wind flows in the opposite direction, it is a negative addition. In other cases, the influence is complicated since the wind deflects the sound waves.

**oblique- and crosswind** The effect of homogeneous oblique- and crosswind on sound propagation from a speaker is rarely studied, and the effect on high frequency seems to be unclear. One author has addressed the problem in a simulation of a low frequency source [Ostashev et al., 2005] where the author of [Ballou, 2008] have practical experience with high power sound system and indicate that crosswind effect might be frequency dependent. The author indicates that the frequency dependency might be due to the directionality of the high frequency drivers. The author of [Ostashev et al., 2005] has simulated a homogeneous crosswind effect on an omnidirectional source at 100 Hz. The author of [Prospalopoulos and Voutsinas, 2007] implemented a ray tracing method with a vector based interpolation as shown in Figure 2.7.



**Figure 2.7:** The figure shows a geometrical ray tracing calculation scheme of calculate the resulting wave direction at crosswind [Prospalopoulos and Voutsinas, 2007], [Ostashev et al., 2005]

Where:

$c$	is the speed of sound	[m/s]
$n$	is the normal unit vector	[m]
$v$	is the speed of wind	[m s]
$v_{\text{ray}}$	is the resulting sound ray	[m]

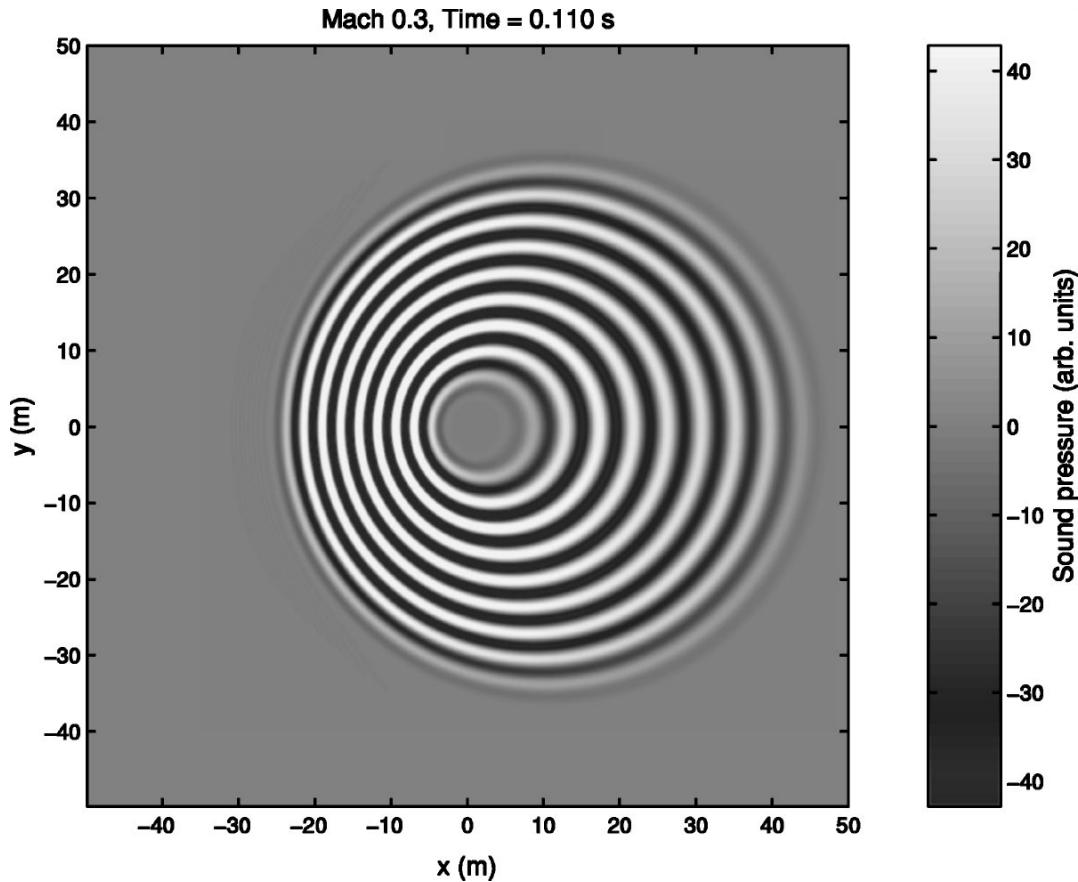
As seen in Figure 2.7, the ray vector  $v_{\text{ray}}$  is an addition of the sound speed vector  $c \cdot n$  and the speed of wind  $v$ . The wave speed and wavelength, therefore, depend on the speed of the wind and the angle between the wind and the sound propagation. The following Equation 2.2 calculate the speed of sound in the  $v_{\text{ray}}$  direction with respect to the wind speed and angle.

$$c_r = c + \|v\|_2 \cdot \sin(\theta) = \|c \cdot n + v\|_2 = \|v_{\text{ray}}\|_2 \quad (2.2)$$

Where:

$\theta$	is the angle of the wave with respect to the wind	[°]
$c_r$	is the resulting speed of sound	[m/s]

As the wave propagating, the resulting  $v_{\text{ray}}$  increases in the direction of the wind. The article [Ostashev et al., 2005] simulates the effect of crosswind in a Finite-Difference Time-Domain (FDTD) simulation with a wind speed of 102.9 m/s. For the acceptable condition to a concert, the wind speed is less than 20 m/s. Otherwise, the audience is escorted from the stage to the exit, and the speaker system is taken down to ensure safety. The following Figure 2.8 shows a simulation result from [Ostashev et al., 2005], where the source is an omnidirectional 100 Hz spherical source while the wind has a constant uniform wind speed from left. The simulation is done in two dimensions.



**Figure 2.8:** The figure shows a simulation of a 100 Hz omnidirectional source with a uniform constant wind speed from left with speed of 102.9 m/s [Ostashev et al., 2005].

As seen in Figure 2.8, the homogeneous crosswind does not affect the direction of the wave from a low frequency spherical source. It only affects the time of arrival to the audience.

### 2.3.3 Pressure impact

The influence of atmospheric pressure change is low compared to the effect of wind, humanity and temperature. The average atmospherical absorption from 4.0 kHz to 16.0 kHz with fixed temperature and variable humanity, increases with 2 dB SPL while going from 101.33 kPa to 54.02 kPa. The atmospheric pressure then only have a negligibility influence on sound propagation and is generally not frequency dependent.

Beside the small impact of pressure difference in the atmosphere, the high pressure generated by the speaker does have a tremendous influence on the sound propagation. There are three states in the propagation way that can produce distortion concerning the pressure. The design of the high frequency horn [Czerwinski et al., 1999], the

port design of the low frequency driver [Vanderkooy, 1998] and the influence of the sound path. The following description starts with the latte.

**Sound path** In the sound path, two factors distort the wave doing propagating in air. As described in section 2.1.1 a sound wave is condensation and compresses of the air particle. The air medium, therefore, has a lower limit that cannot be less than vacuum. The higher bound of SPL is then depending on the atmospheric pressure. As an example, at 54.02 kPa the highest SPL before distortion caused by vacuum is 188.6 dB SPL and at 101.33 kPa the highest SPL before distortion caused by vacuum is 194.1 dB SPL.

There is, therefore, a higher limit determined by the atmospheric pressure to vacuum, but distortion occurs much before the limit of vacuum. High pressure in the compression also distorts the sound because of the lack of linear dependency between the particle velocity and stiffness in the sound wave. The stiffness or density increases while the air particle is closer to each other. Therefore SPL increases more than the density of the sound wave which causing the compression of the sound wave to be stiffer and therefore propagate faster than in the condensation of the wave. This speed differences, therefore, produce harmonic distortion, and is even present in SPL less than 120 dB SPL [Czerwinski et al., 1999]. The speed differences transform the sinusoid into a sawtooth as it propagates which transfer energy to the harmonic of the propagation frequency. The distortion is not only SPL dependent, but also depend on the frequency. The higher the frequency is, the faster the sinusoid transforms into a sawtooth, therefore, the distortion increases with frequency for constant SPL. The harmonic frequency is higher than the fundamental frequency and therefore, as explained in section 2.3.1, the harmonic has higher attenuation with respect to the distance and viscosity. In most cases, the attention is not as high as the increase of the harmonic distortion, and therefore the distortion of the wave propagation is not fully compensated by the viscous losses in the air. [Czerwinski et al., 1999]. The distortion made by air propagation is much less than the distortion in the mouth of the speaker which leads to the next distortion problem produced by high-pressure [Czerwinski et al., 1999].

**Driver throat and mouth design** High pressure in both horn phase plug, sealed enclosures, vented enclosures and reflex enclosures for low frequency driver cabinet produces distortion as they act as nonlinear components. The latter produce distortion because high pressure makes air turbulence in the vent. In the optimal design, the distortion of air turbulent is low but is always present in high-pressure [Roozen et al., 1998]. The air turbulence is not only caused in the vent of the low frequency driver, but it also occurs in the phase plug of the compression driver if the SPL is high [Czerwinski et al., 1999]. The distortion depends on the moving mass, the stiffness and the viscous losses in the air on the diagram displacement and the SPL. As the air in the high frequency driver compress, it becomes heavier, stiffer and thicker which make nonlinear wave propagation. It typically occurs when the compression chamber

exceeds approximately 170 dB SPL. At a higher level, the particle velocity resistance to the air flow increases and the laminar air flow turns into turbulent air flow. The distortion is also depending on the length of the horn and the expansion rate of the horn flare. To keep the distortion as low as possible for the high frequency driver the displacement of the diaphragm should be kept significantly lower than the height of the compression chamber [Voishvillo, 2004]. Therefore, to keep the displacement of the high frequency driver as low as possible, the frequency range should be limited.

### 2.3.4 Ground absorption and reflection

In a concert area, ground absorption and reflection is complicated because there are two very different situations. Before the concert, the area is a local plan area often with mown grass and with ground reflection. An example of a frequency response over mown grass where the measuring height of the microphone is in the height of the ear is given in [Piercy et al., 1977]. The measurement shows that the ground reflection affects the frequency response with high interference. A measurement in Appendix A and ?? is performed where the ground reflection clearly have a big influence on the received frequency response. In this measurement inhomogeneous airflow is present, but the interference is similar in homogenous airflow [Piercy et al., 1977]. Doing the concert the interesting part is not such ground reflection effect but the audience reflection or absorption. The area along the concert is packed by the audience and therefore, the reflection is not easy to calculate. The absorption and reflection in an outside concert area with a group of audience is rarely studied, but absorption for the audience inside a concert hall is highly studied [Beranek, 2006]. The absorption of the audience is founded to be high in all measured concert hall from 1.0 kHz octave band to 4.0 kHz octave band [Beranek, 2006]. The average absorption  $a_{\text{sabine}}$  coefficient is calculated to be above 0.80. The method and result can be founded in [Beranek, 2006]. The reflection in the high frequency in the audience area doing concert is therefore assumed to be low. At low frequency, the article [Beranek, 2006] indicate that the absorption decay with frequency beneath 250 Hz, but The octave band for low frequency driver, which is 31.5 Hz, is not measured by [Beranek, 2006]. The low frequency absorption at 31.5 Hz octave band is therefore assumed to be low. The low frequency driver is mostly located in front of the stage on a line or in end-fire settings, often with a maximum distance of half the wavelength from acoustical centre to acoustical centre. The distance between the low frequency driver is determined by the half wavelength of the highest frequency, such that they radiate a plan wave [Bauman et al., 2001]. A higher distance between the acoustical centre causes interference in the low frequency in the audience area.

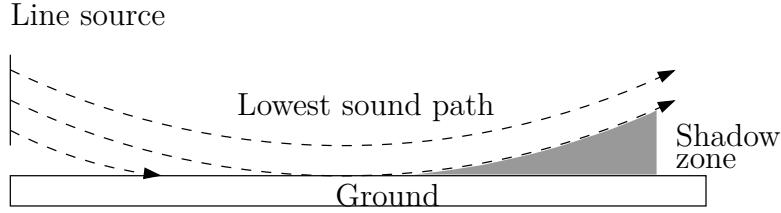
## 2.4 Inhomogeneous atmospheric conditions

This section aims to analyse the sound wave propagation in inhomogeneous atmospheric conditions. In an inhomogeneous atmosphere, the pressure and speed is a

function of position. By this fact, the modelling of a sound wave is very complex and depend on various variables such as temperature and wind speed. The following sections give a short introduction to the effect of inhomogeneous atmospheric conditions.

### 2.4.1 Atmospheric refraction

When the wind speed, the temperature and humanity is assumed to be homogeneous in the sound field, the sound is travelling in a straight plan wave. Often this is not true, the wind speed increases logarithmically with the height from the ground to the geostrophic wind [Yang, 2016] in the free troposphere [Rossing, 2014], and the temperature and humanity are inhomogeneous. The geostrophic wind in the free troposphere is located in a height from approximately 1 km above the ground [Rossing, 2014], [Association, 2003]. The inhomogeneous atmospheric condition makes the speed of sound to depend on the height from the ground. This inhomogeneous atmospheric condition results in a curved sound path and is defined as atmospheric refraction. For small distances, the atmospheric refraction has a sparse effect on the sound travelling path, because the speed of sound is much faster than the speed of the wind and the temperature change. Generally distance up to 50 m is often assumed to have no significant refraction effect [de Oliveira, 2012]. For distances larger than 50 m the refraction is assumed to have a significant influence, especially when the sound source and the receiver are close to the ground. Refraction is frequency and distance dependent and is measured in dB excess attenuation. The means of excess attenuation is that only the effect of wind or temperature is considered, all other atmospherical effect is excluded. A measurement is given in [Piercy et al., 1977] for a point source where the wind speed is 5 m/s. At a distance of 110 m, it is observed that frequency above 400 Hz is refracting while frequency below is rarely effected of refraction. Moreover, at a distance of 615 m the refraction is present in the full measured frequency range from 50 Hz to 3.2 kHz. In the perspective of a live concert the interesting distance is the 110 m from the line source array to the audience rather than the 615 m. Both the downwards and upwards refraction is interesting. In the upwards refraction the audience might be in the shadow zone where for the downwards refraction the high frequency reflection from the ground is assumed to be low when the concert area is full of audience. Therefore the high frequency is refracted down into the frontal audience, and only sparse reflection of the high frequency propagate to the back part of the audience. The following Figure 2.9 display the phenomena of upwards refraction.



**Figure 2.9:** The figure illustrates that the shadow zone occurs from an upwards refraction. A line source speaker array contains of many couplet point sources. Every lowest sound path dashed line indicate the lower directional angle of one point source in the line source array.

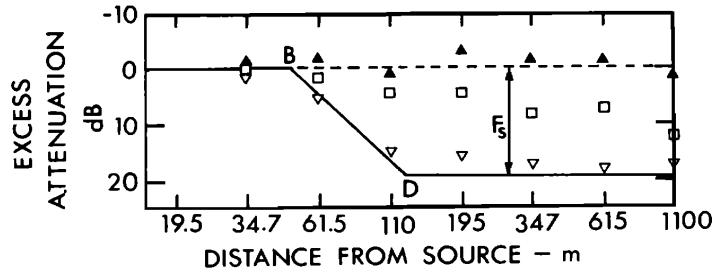
The following description is based on the distance of 110 m and upwards refraction. As explained in [Piercy et al., 1977] the refraction at a distance of 110 m is highly frequency dependent. At a frequency below 400 Hz the effect is sparse but above the effect is high and may result in 20 dB SPL attenuation at the audience. The reason that the refraction is frequency dependent is that the scale of the wind gradient and temperature gradient close to the ground is small compared to the wavelength of the low frequency [Piercy et al., 1977]. This theory does not follow the shell's law of refraction. Shell's law describes the refraction as a layer change in the medium of propagation. Shell's law of refraction is defined as Equation 2.3

$$\frac{\cos(a_1)}{c_1} = \frac{\cos(a_2)}{c_2} \quad (2.3)$$

Where:

$a_1$	is the input angle in the horizontal plan	[°]
$c_1$	is the sound of speed in the medium of arrival	[m/s]
$a_2$	is the output angle in the horizontal plan	[°]
$c_2$	is the sound of speed in the medium of destination	[m/s]

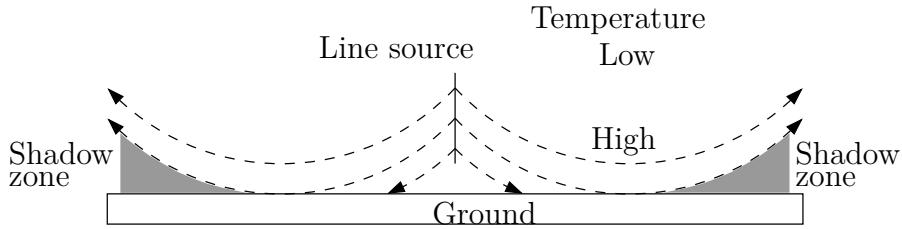
As shown in shell's law Equation 2.3 the frequency dependency is not a factor and are therefore maybe only valid for a laminar wind flow profile. The article [Piercy et al., 1977] only explores frequency up to 3.2 kHz but since the refraction depends on the wavelength, the distance of refraction wave might be smaller for higher frequency. The attenuation with respect to refraction seems to have a saddle attenuation at 20 dB SPL. A measurement in [Piercy et al., 1977] shows the attenuation for the center frequency of 1.2 kHz with  $1/3$  octave band filtered airplane noise over mown grass. The measurement is interesting with respect to a concert area and is therefore shown in Figure 2.10



**Figure 2.10:** Excess attenuation measured for aircraft noise in the 1.2 kHz  $\frac{1}{3}$  octave band for the ground-to-ground configuration. The vector component of the wind velocity in the direction of propagation for  $\blacktriangle$  is 5 m/s,  $\square$  is 0 m/s, and  $\nabla$  is -5 m/s. The temperature profile is neutral.  $F_s$  is the shielding factor, B is the shadow boundary [Piercy et al., 1977]

The following two paragraphs explain the difference between wind refraction and temperature refraction.

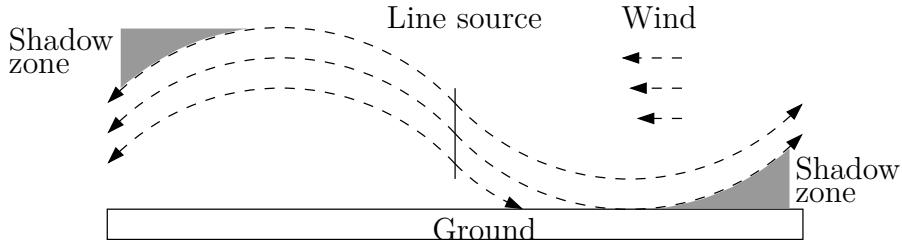
**Temperature** Temperature decreases with respect to the height at day time and increases at the night time. The increase or decrease is usually approximated as a logarithmic function. In the day time, the sun heats the ground even on a cloudy day, and the concert area is full of audience. Therefore, the earth and audience radiate warm air, which makes the temperature at a low height warmer than the temperature at higher height. These phenomena are named lapse where the opposite is defined as inversion. As explained in section 2.3.1, the speed of sound depends on the temperature. Therefore, at day time, the speed of sound in this situation decay with respect to height. The speed change can be modelled as a change of layer for a plane wave. The output angle of the layer change follows the shell's law when the frequency dependency is excluded. Therefore when the temperature profile is logarithmic, the layer change is a function of height and change the wave direction. The wave direction of the descript weather condition results in an upwards refraction. Since the temperature is a scalar quantity uniformly over a large area and a function of height, an identical temperature profile is applicable all around an omnidirectional sound source. Therefore the upwards refraction is uniform all along the speaker in the horizontal plane. The following Figure 2.11 illustrate the phenomena where the temperature decay with respect to the height and the line source array is omnidirectional in the horizontal plane. The omnidirectionality of the line source array is only present in the low frequency typically below 200 Hz.



**Figure 2.11:** Wave refraction of a horizontal omnidirectional line source array in inhomogeneous temperature with lapse profile

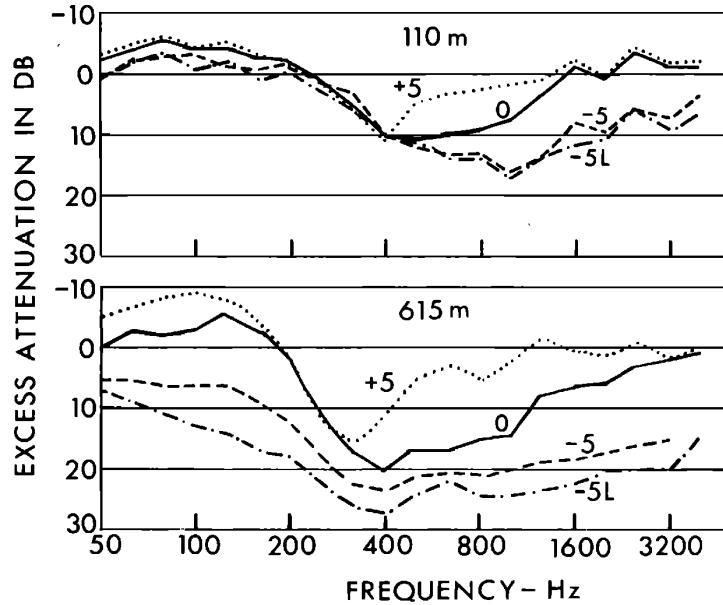
When the temperature profile is reversed, the refraction is downwards.

**Wind** With respect to the wind speed, a concert area is often a protected area with for example barrier, stage and building. This blockage and the ground friction slows down the wind speed near the ground and cause turbulence. Moreover, from nature itself, the wind speed is often logarithmically increased with respect to the height. When the wave is propagation in the same direction as the wind, the atmospheric refraction refracts the sound wave downwards. When the wave propagates against the wind, the atmospheric refraction refracts the sound wave upwards. The following Figure 2.12 illustrate the phenomena with a logarithmic increasing wind from left, and the line source array is omnidirectional in the horizontal plane.



**Figure 2.12:** Wave refraction of a horizontal omnidirectional line source array in inhomogeneous logarithmically increasing wind profile where the wind gradient points towards left

As shown in Figure 2.9 the refraction is upwards when the wind flows in the opposite direction as the wave propagation. Behind the line array source, the refraction is downwards and is therefore different than for temperature refraction. The refraction of wind is the most dominant at a distance of 110 m. The following Figure 2.13 shows an excess attenuation plot of both inhomogeneous wind and lapse temperature profile.

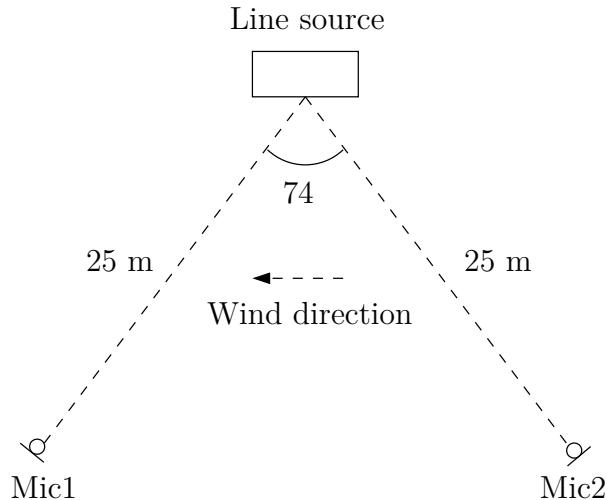


**Figure 2.13:** Observed attenuation of aircraft noise in a ground-to-ground configuration under a variety of weather conditions. Calculated losses from atmospheric absorption and spherical spreading have been subtracted from the attenuation measured in  $1/3$  octave bands for distances of 110 m and 615 m. The numbers on the curves indicate the vector component of the wind velocity in the direction of propagation in m/s. All curves are for neutral conditions of temperature except for those marked L, which are for lapse. [Piercy et al., 1977]

It can be seen in Figure 2.13 that the refraction effect at a distance of 110 m starts at 400 Hz. The reason that sound enters the shadow zone is not fully understood, but one theory is that the shadow boundary wave is diffuse and therefore a significant amount of sound energy enters the shadow zone by turbulent air flow. In a non-turbulent atmosphere condition the SPL inside the shadow zone is attenuated well more than 30 dB SPL. Close to the ground, the atmosphere condition is always turbulent because of ground friction. The turbulence wind diffuses the sound wave and changes the direction of propagation. The wave that enters the shadow zone is considered as a creeping wave while turbulent air flow is present. The creeping wave will by them self also be refracted and therefore parallel to the other refraction waves. [Embleton, 1996]

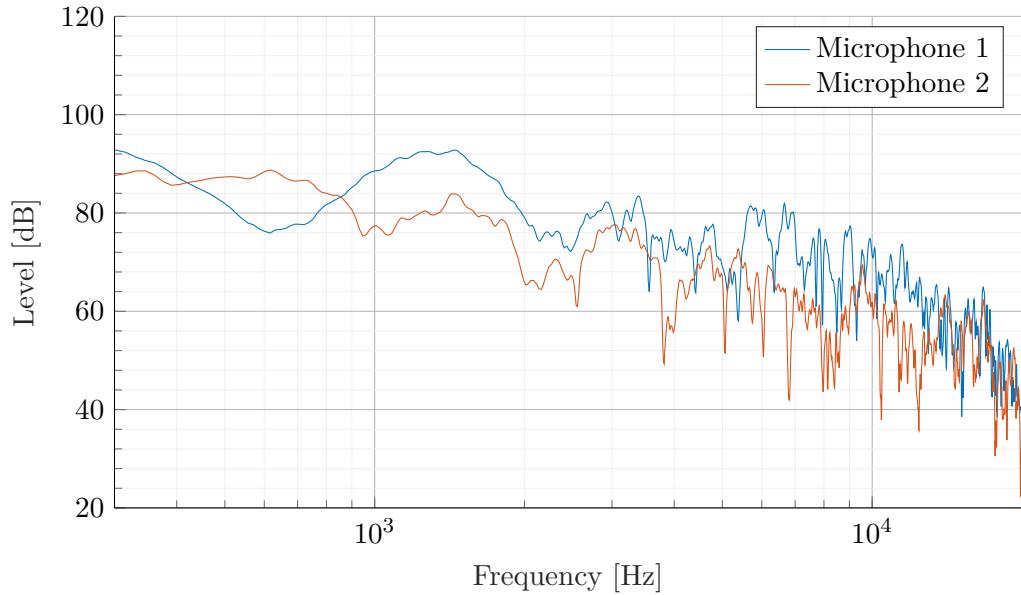
**Oblique- and crosswind** The effect of oblique- and crosswind on acoustical wave propagation in inhomogeneous atmospheric conditions are rarely studied. The author in [Piercy et al., 1977] explain that the refraction is directly zero when only crosswind is present, and increase progressively as the direction of propagation deviate from the angle of crosswind. The author of [Crocker, 1998] support this theory for inhomogeneous atmospheric condition.

Since the effect of oblique wind on a line source array speaker is rarely studied, a measurement in windy condition is performed. The measurement is performed over mown grass in a large open area used for football. The used measurement technique is done according to [Gunness, 2001] where more than one impulse response is measured, and average by alining the impulse response. The wind was considered as healthy for an outdoor concert. The wind speed was measured to 14 m/s doing the full measurement. The measurement was done with a four element line source array 1.1 m above the ground. There were used two microphones, where both were situated 25 m from the speaker in the first measurements and 23 m from the speaker in the last measurements. While changing the distance, the angle to the speaker was changed. The frontal direction of the speaker was placed orthogonal to the wind direction, and the microphone was placed on both side of the speaker as shown in Figure 2.14



**Figure 2.14:** The figure shows the microphone position versus the position of the line source array angle of main lobe

The measurement was done with sine swept and according to the description in Appendix A. The measurement was performed with two microphone positions, two measurements where the microphone are within the speaker high frequency directional angle and three outside the speaker high frequency directional angle. The first measurement is shown in Figure 2.15. The other four measurement result can be seen in Appendix A. They show the same tendency, but the difference between the measurements are more drastically in the measurement where the microphone are situated outside the high frequency directional angle.



**Figure 2.15:** The graph shows the first transfer function measurement within the high frequency directional angle. The  $L_{eq,5}$  SPL difference between the microphones is 4.41 dB SPL (IR\_3)

It can be seen in Figure 2.15 that the general SPL is higher for microphone 1. Furthermore, microphone 1 also shows the typical downwards refraction ground reflection interference in the frequency response which is very similar to the calculated ground reflection interference in [Piercy et al., 1977]. Microphone 2 does not have the same strong interference in the low frequency and the general SPL is lower than microphone 1. This difference indicates upwards refraction in the direction of microphone 2 with only a small amount of ground reflection. The resulting  $L_{eq,5}$  SPL difference for all measurement is shown in Table 2.1.

**Table 2.1:** The table shows the measured  $L_{eq,5}$  SPL for all measurement and the difference between the microphone

Measurement number	Mic 1 $L_{eq,5}$	Mic 2 $L_{eq,5}$	Difference
Measurement 1 Figure A.4	71.82 dB SPL	66.33 dB SPL	5.49 dB SPL
Measurement 2 Figure A.5	69.09 dB SPL	64.69 dB SPL	4.40 dB SPL
Measurement 3 Figure A.6	67.67 dB SPL	63.44 dB SPL	4.23 dB SPL
Measurement 4 Figure A.7	68.10 dB SPL	63.69 dB SPL	4.41 dB SPL
Measurement 5 Figure A.8	68.44 dB SPL	63.62 dB SPL	4.81 dB SPL
Average	69.02 dB SPL	64.35 dB SPL	4.67 dB SPL

As it is shown in Table 2.1, the  $L_{eq,5}$  SPL is higher for microphone 1 in all measurement. Moreover the average  $L_{eq,5}$  SPL difference is 4.67 dB SPL while for A-weighted  $L_{Aeq,5}$  SPL the average difference is 6.17 dB SPL.

With respect to the intelligibility frequency range, a weighting filter is designed to observe the SPL differences in the critical intelligibility frequency range. The filter is based on the founded intelligibility frequency range in [Letowski and Scharine, 2017]. It is shown in [Letowski and Scharine, 2017] that the critical intelligibility frequency range lays between 1.0 kHz and 4.0 kHz. The designed intelligibility weighting filter is an 8<sup>th</sup> order bandpass filter with lower crossover frequency at 1.0 kHz and higher crossover frequency at 4.0 kHz. The resulting average difference is 7.88 dB SPL and the maximum difference is 9.95 dB SPL.

**Turbulent** Turbulence is an atmospheric condition where the wind eddies. It often starts with large eddies and progressively brakes down like a cascade effect to smaller and smaller eddies which only depend on the local region. When the eddies are as small as 1 mm the energy disappears in viscosity and thermal conduction. A statistical distribution of the eddies is defined as turbulence. The turbulence wind flow is, therefore, a chaotic and stochastic process by nature and is present all the time. It can occur because of change in landscape, stage and blockage, but can also be a process of flow speed increase in the wind, which make the wind to refract on itself. Turbulence is often high on a windy afternoon day and low under the inverse of lapse. Turbulence also often occurs near the ground because the ground surface slows down the speed of wind by the friction to the ground. The effect of turbulence on sound is known to make phase and amplitude fluctuation of pure tone. The fluctuation increases with distance until the standard deviation of the phase fluctuation is comparable to 90° [Piercy et al., 1977]. At this point the phase correlation for each sound path is uncorrelated

## 2.5 sound pressure level doing a concert

In Denmark there is no law limiting the SPL doing a concert. The only restriction there might be of SPL is area dependent. In a city the local komunity has limited the total SPL average over 15 min of any event. Out on the countryside, the sound engineer can decide by himself and the often used limit is A-weighted 102 dB SPL average over 15 min.

The standard ?? for long term exposior of high SPL limits the SPL for A-weighted 94 dB SPL average over maximum of 1 h, then the ear needs to have a brake to ensure no damage the the hering. A concert i often more than 1 h with A-weighted 102 dB SPL average. This is at least 8 dB SPL A-waighed more than the regulation recommend. It shall here be clearly understood that the SPL measurement is done in the FOH and the actian exposed SPL is higher for the audience close the the stage.



## Chapter 3

# Summary of Problem Analysis

The analysis started addressing the generally used method for a live concert. It is founded that live concert today use line source array system to cover the audience area with sound. The line source array is flown above the audience at the main stage, and the delay speaker covers the back audience at a large concert. The line source array is constructed of many identical speakers attached to each other in a vertical line. Moreover, the distance from the speaker to the individual audience depends on the audience position. The analysis founded that a homogeneous SPL among all audience might not possible but the SPL among all audience can be optimised by knowledge of the condition of the atmosphere and gain up for the spreading lose. The author observes that the wind does have a frequency and distance-dependent effect on sound propagation, for example at high frequency the high frequency attenuate audibly in the crosswind. The high frequency blows away for periods and comes back again. The analysis of sound from a line source array started by the ideal geometric spreading loss. Here it is founded that the sound propagation of the line source array highly depends on the hight of the source. The line source array propagates differently with respect to frequency. At a certain hight of the line source array the propagation is a cylindrical propagation until a certain distance from the source where it starts propagating as a spherical source. In the cylindrical propagation, the sound field is defined as near-field while in the spherical propagation the sound field is defined as far-field. In the non-ideal scenario, the line source array propagates in inhomogeneous atmospherical condition. To cover the inhomogeneous atmospherical condition, the local homogeneous atmospherical condition is analysed. In the homogeneous atmospherical condition, it is founded that the temperature, humidity, pressure and wind influence the sound field. The effect of temperature and humidity is close coupled on sound propagation. When the temperature is high, and the humidity is low the air has a significant high frequency absorption whereas when the temperature and humidity follow each other, the absorption is less. The second effect the temperature and humidity have on sound propagation is the speed of sound. The higher the temperature is, the higher the sound of speed. The humidity affects the speed of sound the same way as the temparature, but the increase is negligible

compared to the temperature. The effect of wind seems to have a sparse effect on the sound propagation when and only when the wind is homogeneous. It is founded that the speed of wind affects the speed of sound. If the wind moves in the direction of the sound propagation the wind speed is an addition to the speed of sound. In the opposite wind case, the speed of sound is lowered. In the case of oblique- or crosswind, the effect seems to be unclear for high frequencies. One author has simulated a low frequency spherical source and founded that the only effect is the time of arrival to the audience. The impact of the atmospheric pressure is small, and the pressure close to the ground is so high that other limitations of wave propagation limit the SPL before the negative amplitude riches vacuum in the condensation. When the wave compresses the air, the wave travels faster such that the received wave at the audience is a sawtooth wave. The effect produces harmonic distortion where some of the harmonic energy is attuned by the viscous losses. The harmonic distortion is present in SPL lower than 120 dB SPL but is not as critical as the distortion created by the construction of the speaker enclosure. The audience area is assumed to have high absorption in frequency above 1.0 kHz, while frequency in octave band 31.5 Hz is assumed to have low absorption of the audience.

In the inhomogeneous atmospherical condition, it is founded that refraction of the sound wave is one of the biggest challenges for an outside sound concert. The refraction occurs because of inhomogeneous speed which is present in both inhomogeneous wind and temperature. It is further founded that the refraction is frequency dependent and distance dependent. The effect, however, is low at a distance lower than 50 m with a wind speed of 5 m/s. Depending on the atmospheric condition two kinds of refraction was founded, upwards and downwards. Upwards refraction produces a shadow zone where turbulent atmospheric condition makes creeping wave into the shadow zone. For the case of oblique and crosswind the effect of high frequency, the refraction might be zero at direct crosswind but increases progressively as the direction of propagation deviate from crosswind. One measurement was done to research the effect of crosswind on a line source array. It was founded that the average  $L_{Aeq,5}$  SPL at microphone 1 was 6.17 dB SPL higher than microphone 2. Therefore it can be concluded that the crosswind with respect to the speaker coverage area does affect.

## Chapter 4

# Problem statement

Based on the knowledge founded in chapter 2 and the conclusion drawn in chapter 3 a problem statement can be made. For the rest of this theses, the following will be the focus.

**Is it possible to control the speaker directivity such that the average SPL over the speaker coverage area is more homogeneous in cross- and obliquewind condition**

### 4.1 Delimitation

The following delimitations are made for the rest of the project:

- It is chosen to work with mono line source array since the number of line source array element is limited to six pieces.
- Due to the amount of needed audience to the research, the homogeneous SPL is searched over mown grass without the audience.



## **Part II**

# **Test Design**



## **Chapter 5**

# **Preknowledge of outside measurement**

### **5.1 Measuring in inhomogeneous atmosphere**

The aim of this section is to gain pre knowledge about outdoor measurement, such that effecting condition doing measurement is controlled.

### **5.2 Ground reflection**

### **5.3 Wind noise**

### **5.4 Frequency response**



# **Chapter 6**

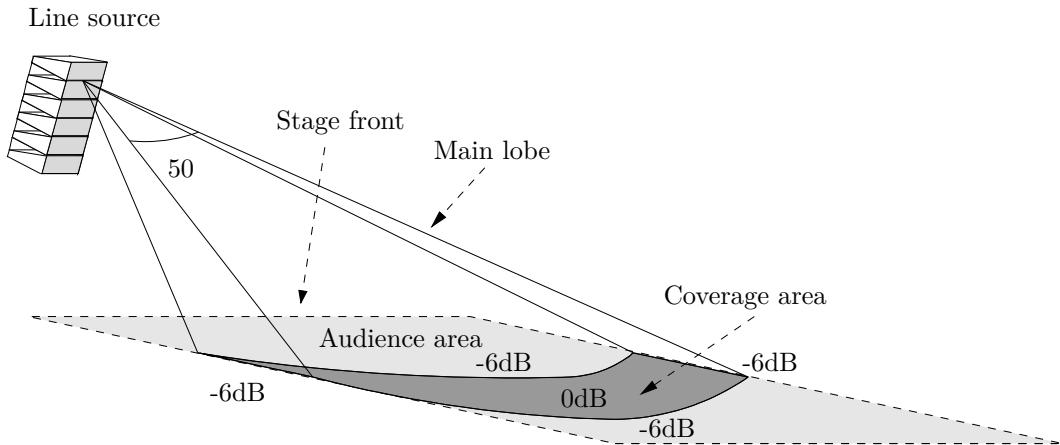
## **Proposal solution**

### **6.1 proposal of solution to the wind problem**

This section aims to propose a solution to the problem founded in the crosswind measurement section 2.4.1 and the problem statement in chapter 4. To be able to find a solution to the problem, the optimal condition is defined in section 6.2. Then a proposed solution to the crosswind is defined in section 6.3 and lastly a proposed solution to the parallel wind is defined in section 6.4

### **6.2 Optimality condition**

To be able to search for a solution and design a test to research if the proposed solution has the which effect on the coverage area, the optimal condition is defined in this section. The optimal condition is as simple as the SPL coverage in the coverage area of the speaker without wind. In other words, the line source array has a frontal horizontal directional angle defined as the  $-6$  dB SPL limit of the main pressure lobe. The line source array main lobe is given in the horizontal degree as an addition of the main lobe from the frontal direction to both side and can both be symmetric and asymmetric, depending on the line source array element. The following Figure 6.1 shows an illustration of the main lobe.

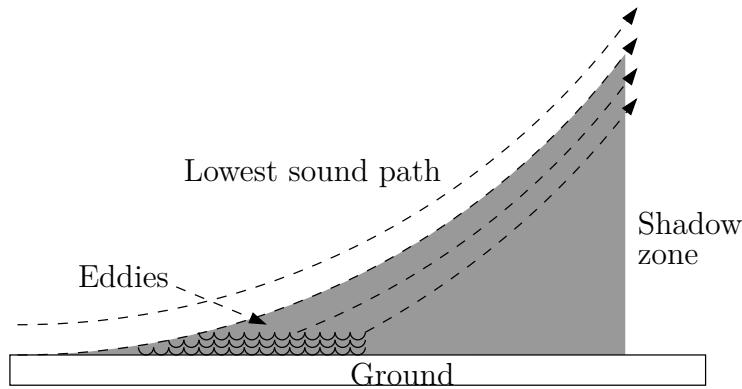


**Figure 6.1:** The figure shows the pressure limit which defined the main lobe of the line source array and the coverage area without wind

As illustrated in Figure 6.1 the coverage area is a parabolic surface which is limited as the  $-6\text{ dB}$  SPL coverage limit of the line source array. This is the coverage area with no wind effect and is the coverage area which is defined as the optimal condition. The solution to the crosswind and the parallel wind, therefore, is a way to be able to adjust the coverage area such that the line source array can eliminate the effect of the wind and cover the area as without wind. To be able to eliminate the wind effect at the audience area, audience area have to be defined. To define the audience area, a questioner is made among the large sound rental company in Denmark which ask for audience area to a concert. The questioner is founded in Appendix L. The goal of the questioner is to find the highest coverage distance from the line source array. The founded maximum distances before delay tower is approximate 60 m, and furthermore, the wind might be stronger than 5 m/s to a concert but wind above 10 m/s to 12 m/s will stops the concert. Therefore the defined coverage area as shown in Figure 6.1 is 60 m from the stage front.

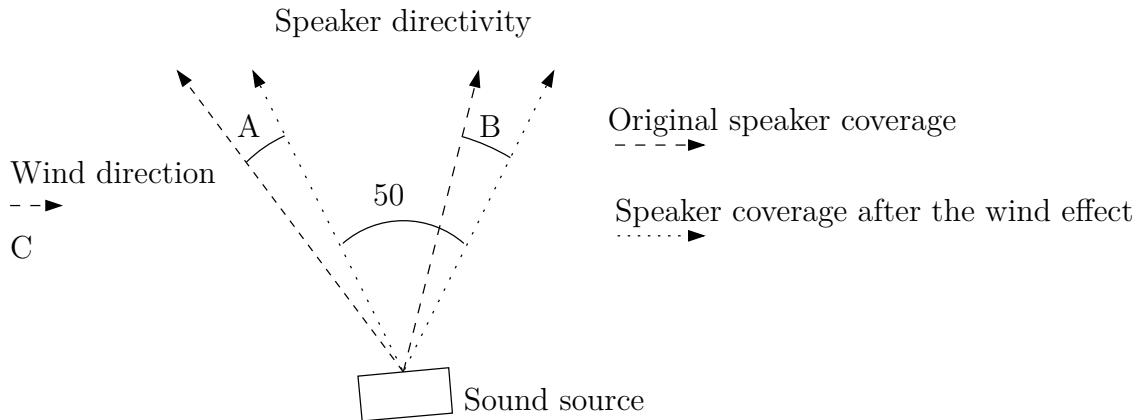
### 6.3 Proposal solution to crosswind

The crosswind problem is shown in section 2.4.1 to highly modified the coverage area. Agents the wind the upwards refraction is shown to attenuate the sound more than  $6\text{ dB}$  SPL A-weighted at a distance of only 25 m and a mean wind strange of 14 m/s. Furthermore, it is founded that the shadow zone SPL depends on the SPL in the sound path, because the wind eddies, eddies the sound into the shadow zone. It is then researched if adding more power into the upwards refraction direction also adds more power into the shadow zone by the wind eddies. The following Figure 6.2 illustrate the eddies theory in upwards refraction.



**Figure 6.2:** The figure shows the sound path above the shadow zone and inside the shadow zone produced by the eddies

The proposed solution is then to steer more power into the direction of upwards refraction and less power into the front and in the direction of downwards refraction to research the eddies theory shown in Figure 6.2. The following Figure 6.3 shows a graphical illustration of the proposed solution to archive a more homogeneous SPL in the coverage area of the line source array with the wind.

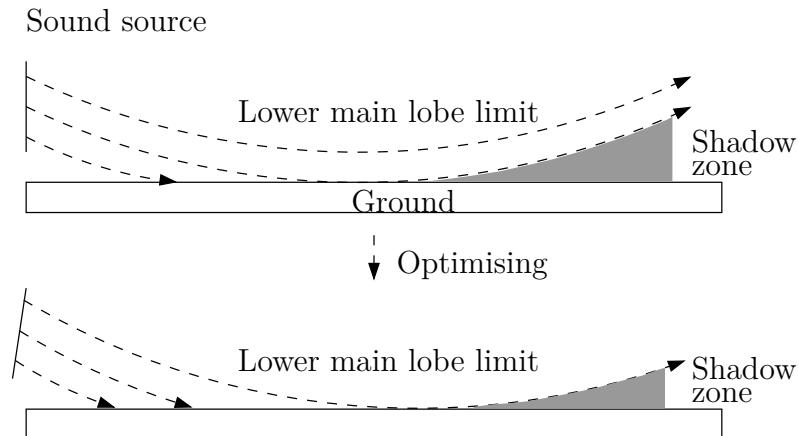


**Figure 6.3:** The figure shows the wanted direction of the sound coverage area after the effect of crosswind. C is the speed of wind in cross direction of the frontal direction of the speaker. A and B is the main lobe angle that needs to be founded. On the figure the angle are equal but that might not be true

The goal is then to search  $A^\circ$  and  $B^\circ$  based on wind speed  $C$  m/s and the optimal coverage area as shown in Figure 6.3 such that the SPL coverage differences is optimized. As founded in section 2.4.1 the refraction is frequency dependent, therefore, finding the optimal  $A^\circ$  and  $B^\circ$  might not be possible for all frequency. Furthermore the refraction in the low frequency is nearly zero for the distance present at the concert.

## 6.4 Proposal solution to parallel wind

The above proposal solution deals with the crosswind problem. When the wind direction change such that the wind comes from the back audiences to the stage, or in other words, is parallel with the frontal direction of the speaker, another theory is research than the eddies theory. The resand to search for another solution is that using the eddies theory in parallel wind require that the power from the line source array is raised. The proposed solution is then to move the shadow zone instead of raising the power in the shadow. To be able to move the shadow zone, the idea is to change the vertical angle of the main lobe, such that the upper speaker either point more downwards or upwards for upwards refraction or downwards refraction respectively. Therefore if the upper speaker points more downwards the energy from the speaker might arrive at the ground where else if the line source element is pointing parallel to the ground, the energy never enters the ground surface. The following Figure 6.4 shows the proposal solution to parallel wind refraction.



**Figure 6.4:** The figure shows the proposal solution to the upwards refraction. The upper part of the figure shows the lower vertical main lobe ray while the array is orthogonal to the ground where the lower part of the figure shows the lower vertical main lobe ray while the line array is angled more downwards

The shadow zone distance is depending on the hight of the line source array from the ground within the limited hight of flying points on the stage. As higher the line source array is flown, as higher the distance is before the shadow zone is present while the vertical angle is optimised to the audience area.

# Chapter 7

## Test of Proposal Solution

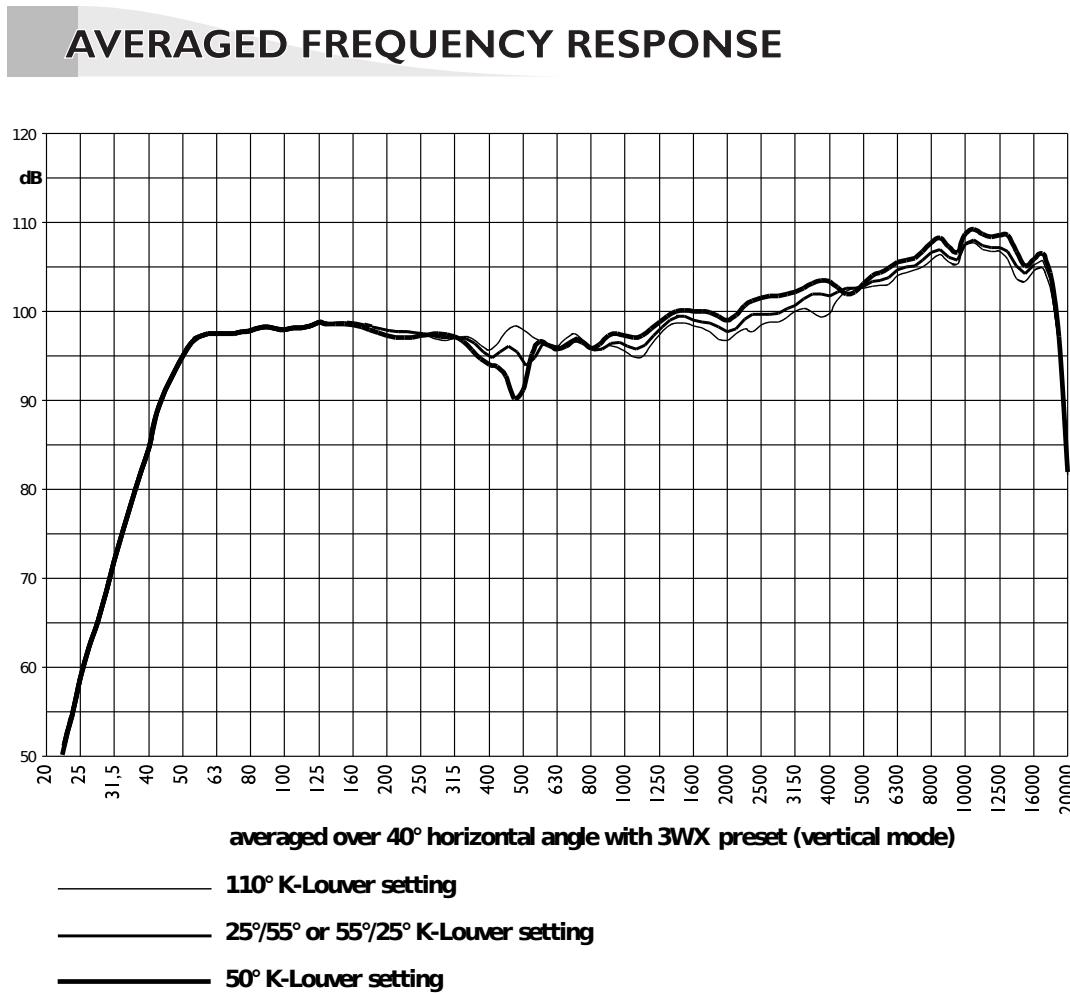
### 7.1 Test of proposal solution

This section aims to design a test setup for testing the proposed solution. The test setup will be based on an L-acoustics KUDO line source array which is described in section 7.2 without any modification. This chapter designs the measuring method and the needed windscreens for wind measurement. To be able to design the measuring, the used line source array is briefly described in section 7.2, then the measuring setup is designed in section 7.3 and in the end, the measuring method is designed in section 7.4.

### 7.2 Description of the used line source array

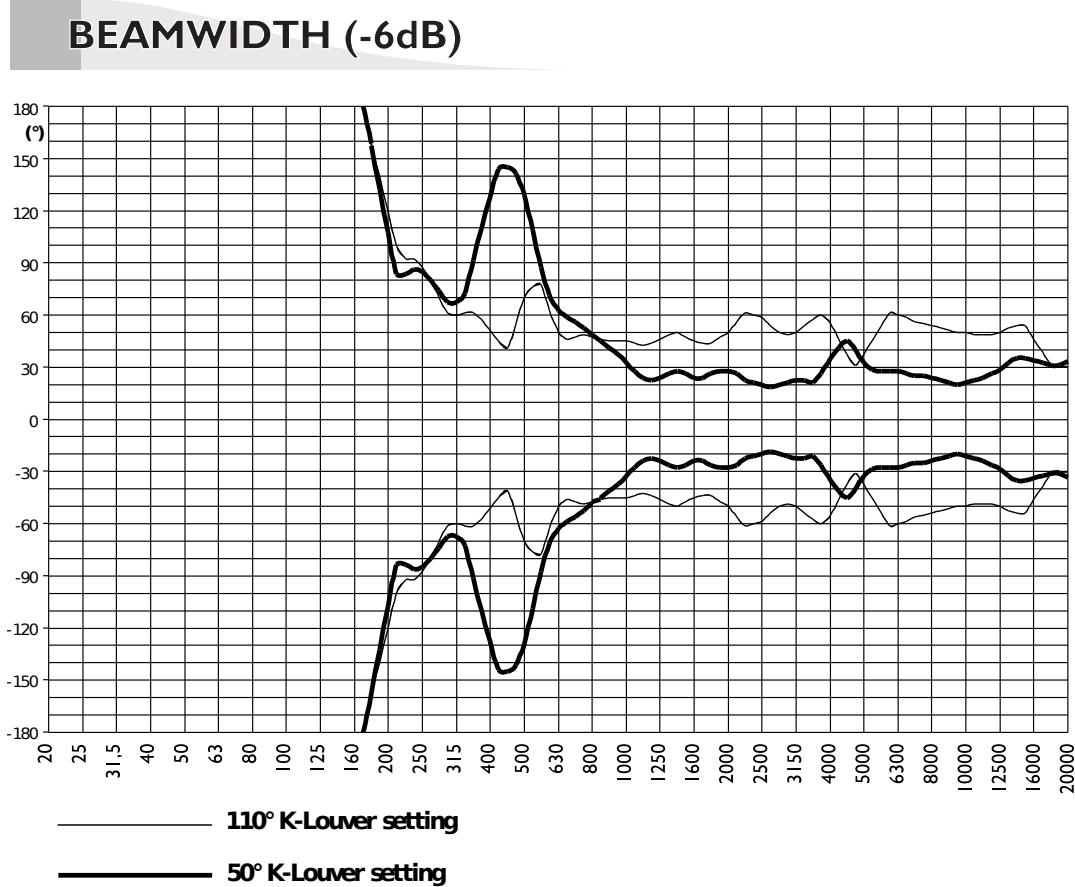
This section aims to explain the functionality for the line source array which is used to test the proposed solution. The description starts with a short introduction to the line source element, then the frequency response of the single element, the horizontal directionality control, and the vertical directionality control is explained.

The line source elements which is used to test the proposed solution is an L-Acoustics KUDO line source array. This line source array is a legacy long throw variable curvature speaker. The speaker is designed as the second option in the K series which today is renewed and renamed to L-acoustics K2. The speaker can be flown as a vertical line with a maximum of 21 elements. The maximum number of an element is due to the safety limit on the flying tools. One single element have a frequency response from 50 Hz to 18 kHz with a maximum deviation of  $\pm 3$  dB SPL and have a maximum SPL of 140 dB SPL at 1 m. The following Figure 7.1 shows the average frequency response over 40° horizontal angle of a single line source element.



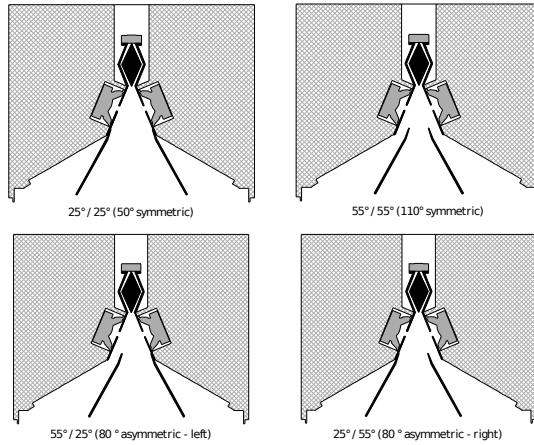
**Figure 7.1:** The graph shows the average frequency response over 40° horizontal angle of a single line source array at 1 W [L-Acoustics, a].

The horizontal coverage angle can be controlled individually on every line source element. The line source element allows both symmetric horizontal coverage and asymmetric coverage. The angle from the frontal direction to the outer main lobe –6 dB SPL is either 25° or 55°. By this two angle for both sides, four coverage angle of the speaker is possible, 110°, 50° and 80° ether to the left or the right. The following the Figure 7.2 shows both the wide and narrow symmetric main lobe option of the L-acoustics KUDO. The asymmetric coverage can be founded in [L-Acoustics, a]



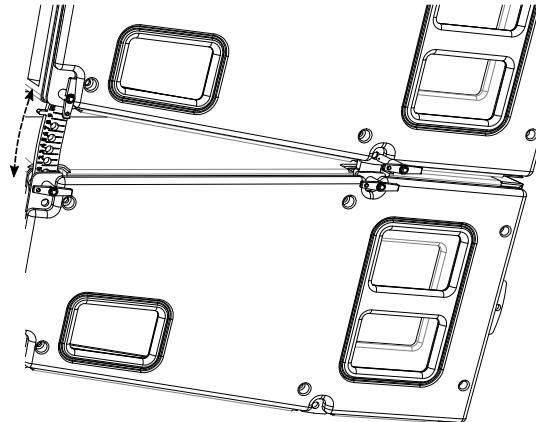
**Figure 7.2:** The graph shows the symmetric coverage area of the L-Acoustics KUDO line source array [L-Acoustics, a].

The mechanical coverage solution in the L-acoustics KUDO as well as other line source array element is not made for wind problems but for neighbouring disruptions and higher SPL in the main lobe of the high frequency. All solution used today is only possible to be changed by hand and is not electrically controlled. The method for changing the horizontal directivity in the L-acoustics KUDO line source element is two plexiglass plate fixed to the front grill. The fixing mechanism can be adjusted sidewise by realising two splits on both plexiglass plates. The plate can then be slid along the grill to change the mouth of the speaker output. The following Figure 7.3 illustrate the principle.



**Figure 7.3:** The figure shows how the horizontal directivity is controlled on a L-Acoustics KUDO line source array element [L-Acoustics, b].

The line source array vertically coverage area can also be controlled from  $0^\circ$  to  $10^\circ$  with  $1^\circ$  step size. To be able to control the vertical main lobe of the line source array, the mechanical solution is the angle between the line source element. This means that the vertical coverage control cannot be controlled on the individual line source element as the horizontal coverage. To be able to control the vertical coverage, the speaker is trapeze designed such that the high frequency horn throat stays together while the angle between the elements is adjusted in the back of the element for every line source element. The following Figure 7.4 shows how the line source element are angled vertically.



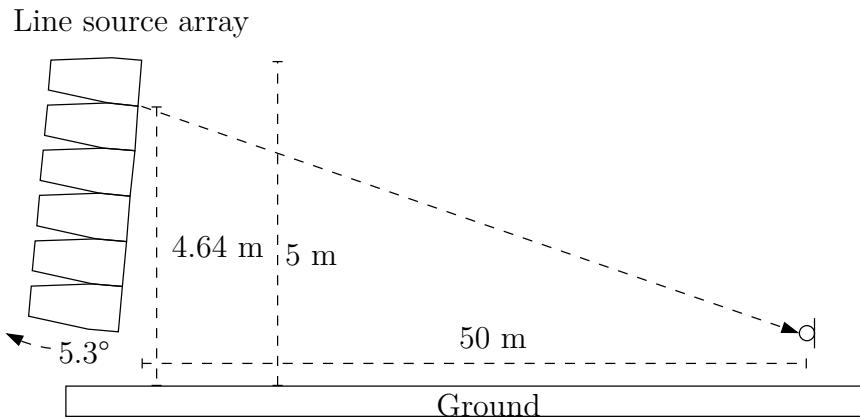
**Figure 7.4:** The figure shows how the vertical directivity is controlled on a L-Acoustics KUDO line source array element [L-Acoustics, c].

To be able to fix the vertical coverage on the L-acoustics KUDO, the upper left rigging pin shall only be placed into the line source element rig when the angle

shown on the metal pease shows the desired vertical coverage between two line source element.

## 7.3 Measuring setup

This section aims to design the speaker setup such that the proposed solution can be tested without mechanical change of the line source array. The test setup, therefore, do not change the speaker directionality adaptive but mechanical by hands before every measurement. The amount of available line source array for the test is limited to six line source element and four belonging low frequency driver. The following Figure 7.5 shows the measuring setup which is used for both measurement.



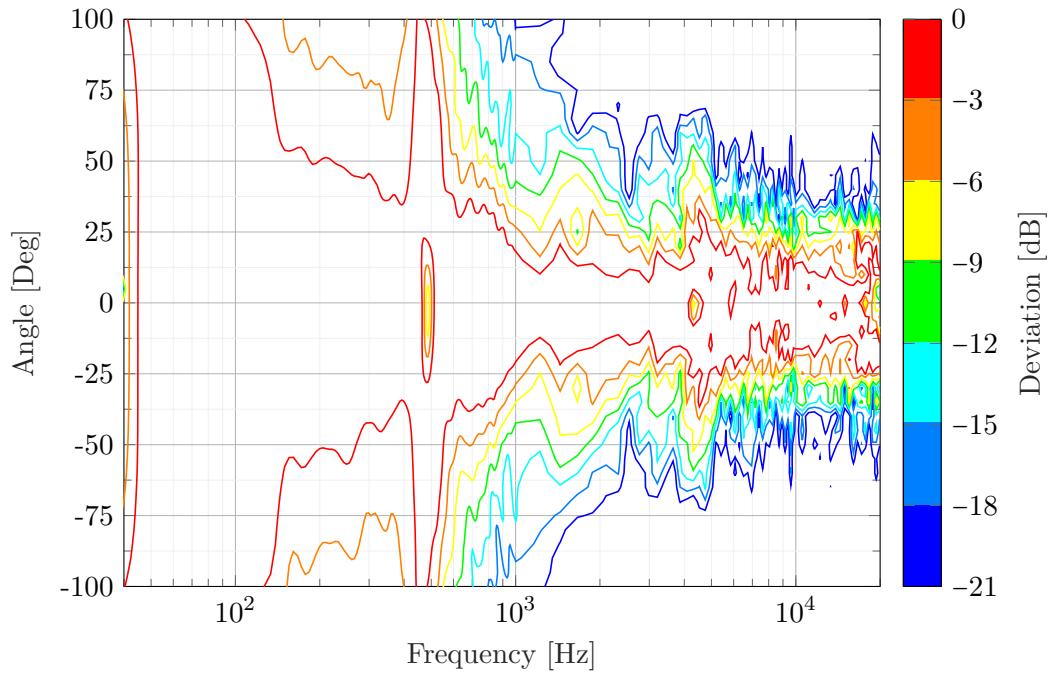
**Figure 7.5:** The figure shows test setup for both measurement

Based on the founded maximum distances from the front of the stage to the delay tower, the line source array is rotated vertically as shown in Figure 7.5, such that the two upper line source element covers the measurement area without wind. The following two section section 7.3.2 and section 7.3.1 describe the line source settings which differs from each other with respect to the rotational procedure.

### 7.3.1 Crosswind line array settings

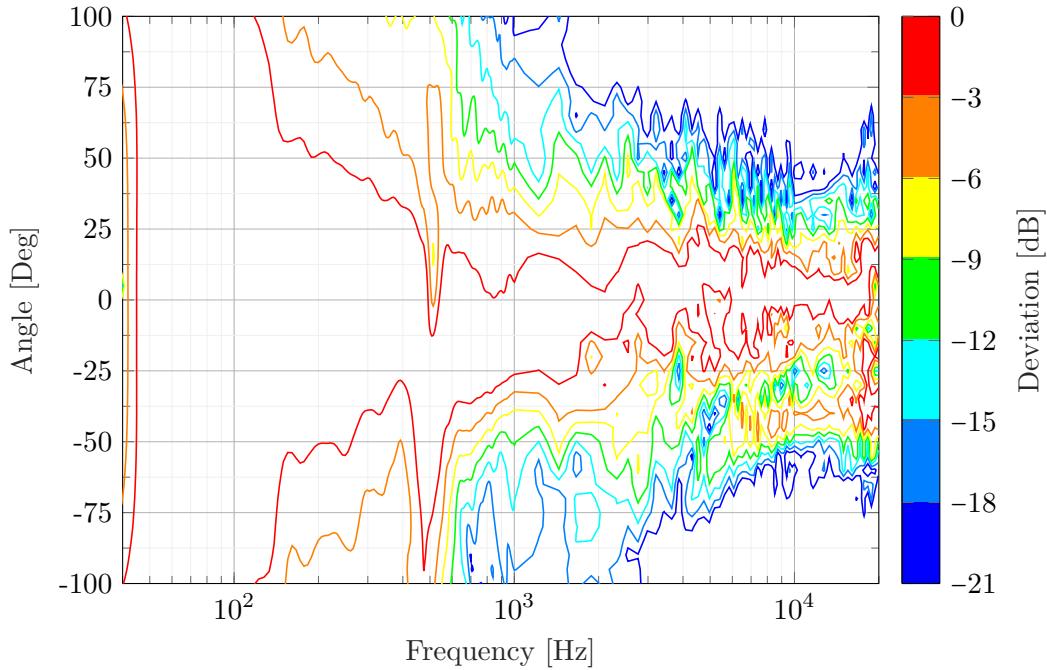
To test the crosswind proposal solution, the idea is to measure the SPL coverage while playing in the frontal direction and then measure the SPL while the line source array is horizontally rotated in the wind direction. To be able to ensure that the horizontal rotation of the line source array keeps the SPL in the downwards refraction direction as much as possible, this section starts designing the directional angle settings of the line source array. It is founded in section 2.4.1 that downwards refraction raises the SPL by downwards reflection but the amplification is much less than the attenuation in upwards refraction and is therefore assumed negligible for directionally chose. Therefore, to decide on the horizontal directionally settings the pressure versus angle

has to be found for the used line source array. The  $-6$  dB SPL directionally is already known from the datasheet, but this detail level is not high enough to decide on any prediction of the attenuation in the downwards refraction direction. Therefore a directionality measurement is made on the used line source array for all possible horizontal directionality settings. The measurement can be founded in Appendix G and the Figure 7.6 shows the resulting directionality of the L-acoustics KUDO with the  $25^\circ / 25^\circ$  settings



**Figure 7.6:** The graph shows a contour plot with 3 dB SPL step of the directionality of the L-acoustics KUDO with  $25^\circ / 25^\circ$  settings. The lower black contour line indicate the dB directionality for the maximum rotation of the speaker

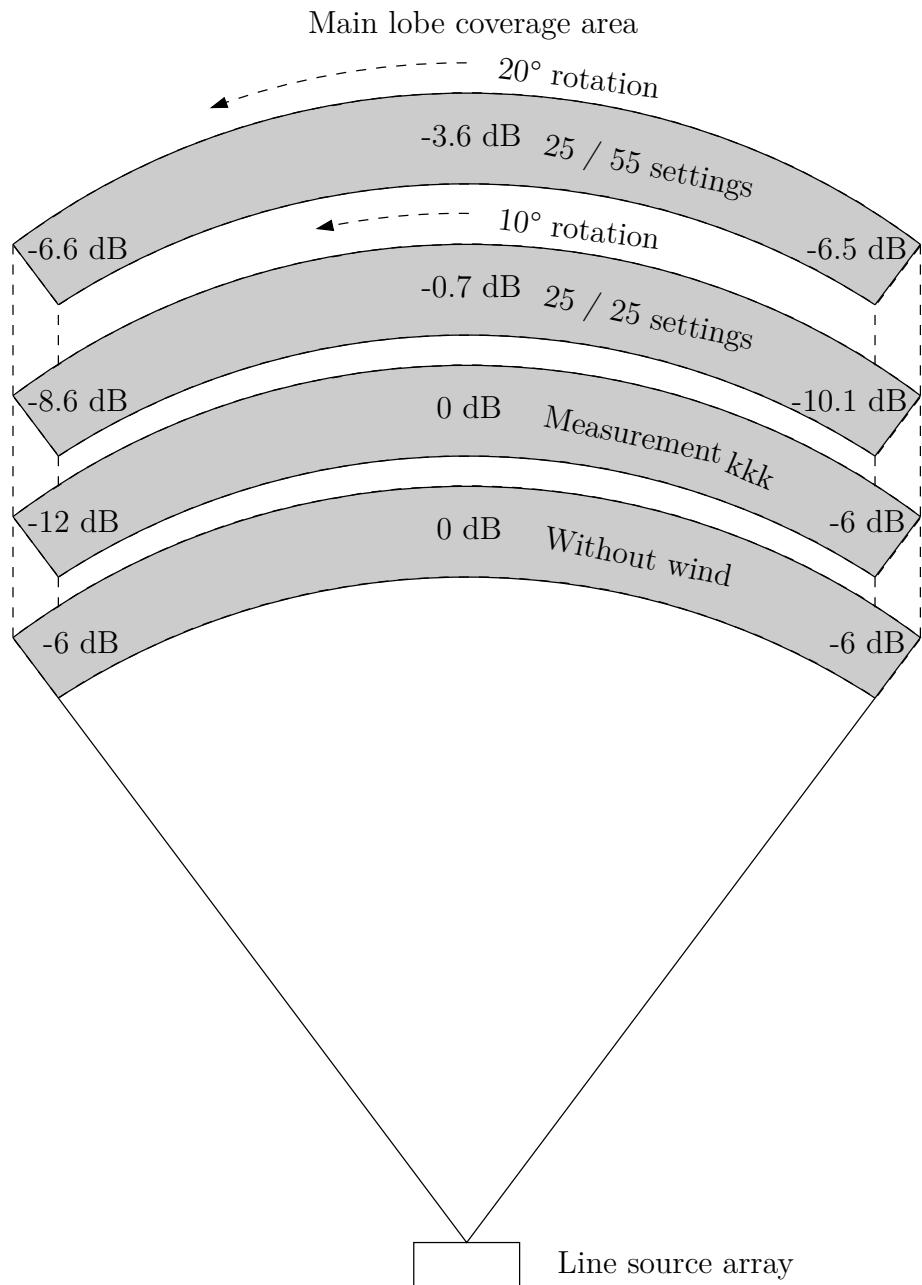
The following Figure 7.7 shows the resulting directionality of the L-acoustics KUDO with the  $25^\circ / 55^\circ$  settings



**Figure 7.7:** The graph shows a contour plot with 3dB SPL step of the directionality of the L-acoustics KUDO with 25° / 55° settings. The lower black contour line indicate the dB directionality for the maximum rotation of the speaker

As seen in Figure 7.6, when the speaker is rotated 25° as the maximum allowed rotation in the proposal solution the SPL in the downwards direction is lowered from approximately –6 dB SPL to approximately –18 dB SPL which is an attenuation of 12 dB SPL. This 12 dB SPL attenuation might attenuate the SPL in the downwards refraction too much. As seen in Figure 7.7, when the speaker is rotated 25° the attenuation SPL in the downwards direction is lowered from approximately –6 dB SPL to approximately –12 dB SPL which is an attenuation of 6 dB SPL. To decide on a mechanical solution an example is calculated based on the measurement above and the measurement in section 2.4.1. The example is based on a rotation of 20°, where the rotational power from a rotation of the L-acoustics KUDO is added to the measurement. The following explains and shows the example.

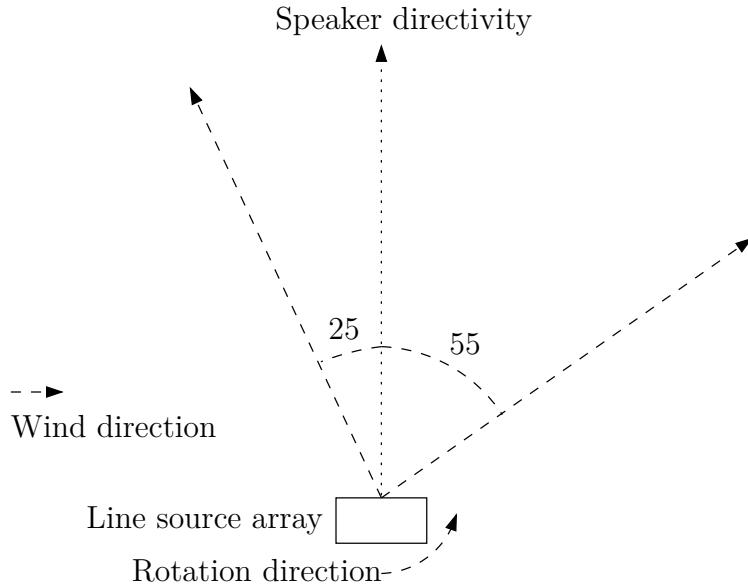
**Example** The example shows four cases from the line array, one case where the data from the datasheet is used, one case where the measurement in section 2.4.1 is used. Then two examples where the differences in SPL is calculated from an rotation of 20° for 25° / 55° settings and a rotation of 10° for 25° / 25° settings and added to the measurement. The following Figure 7.8 shows the example.



**Figure 7.8:** The figure shows the main lobe coverage area without rotation for the to lower and with maximum rotation for the to upper

The centre in the measurement was not measured doing the measurement, so the stated value is a prediction based on [Piercy et al., 1977] which indicate that the energy addition at short distances because of downwards refraction is small compared to the energy loss with upwards refraction.

As seen in Figure 7.8 a rotational of  $20^\circ$  calculate a more homogenous SPL while the line source array is in  $25^\circ / 55^\circ$  settings. The deviation from the frontal direction is approximately 3 dB SPL. In the other case while the rotation is only  $10^\circ$  and the settings is  $25^\circ / 25^\circ$  the SPL is also approximately evenly spread but the deviation to the frontal direction is much higher and is at least  $-7.9$  dB SPL. Based on the calculated example, the chosen directionally settings is  $25^\circ / 25^\circ$  for the measurement. The following Figure 7.9 shows the measurement setup as a top view.



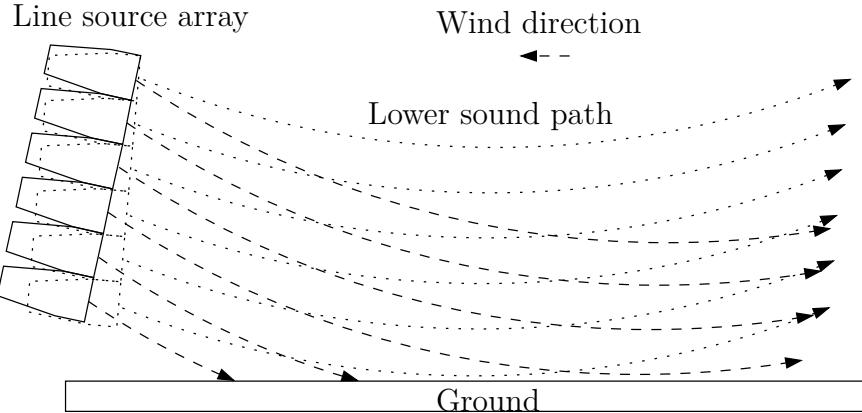
**Figure 7.9:** The figure shows the line source setup for the measurement.

The rotated array is rotated with few degrees for every measurement from  $0^\circ$  until  $25^\circ$ , which mean that the highest possible SPL points in the maximum angle.

The transfer function which shows the lowest SPL deviation between microphone position is the angle of the solution.

### 7.3.2 Parallel wind line array settings

For parallel wind, the idea is to have horizontal symmetric coverage while changing the vertical angle for every measurement. The array is tilted some degree until the optimal angle is measured. The optimal angle is the angle where the shadow zone is pushed as far away as possible concerning the wind speed. The following Figure 7.10 illustrate the line source array from the side.



**Figure 7.10:** The figure shows the line source setup for the measurement. The line source array consist of six KUDO line source element attached with 0° vertical coverage angle

The Figure 7.10 illustrate that the wind makes refraction of sound upwards and therefore the main lobe is curved upwards.

## 7.4 Designing the measurement

This section aims to design a test on the non-modified line source array to test the proposed solution from section 6.1. To be able to test the proposed solution, a measurement system has to be designed. To be sure that the wind noise does not affect the measurement the part of the design takes care about finding the preferable microphone windscreens configuration, based on the available STOF in acoustics lab. The second part measure the frequency dependent attenuation of the chosen windscreens compare to the microphone response without a windscreens. The comparison is done to count for the attenuation of the windscreens such that the measured data reflect the SPL at the point as pleasant as possible. The third part takes care of designing the necessary data logging function. The last part designs the measuring signal playback and record method.

### 7.4.1 Microphone position at crosswind

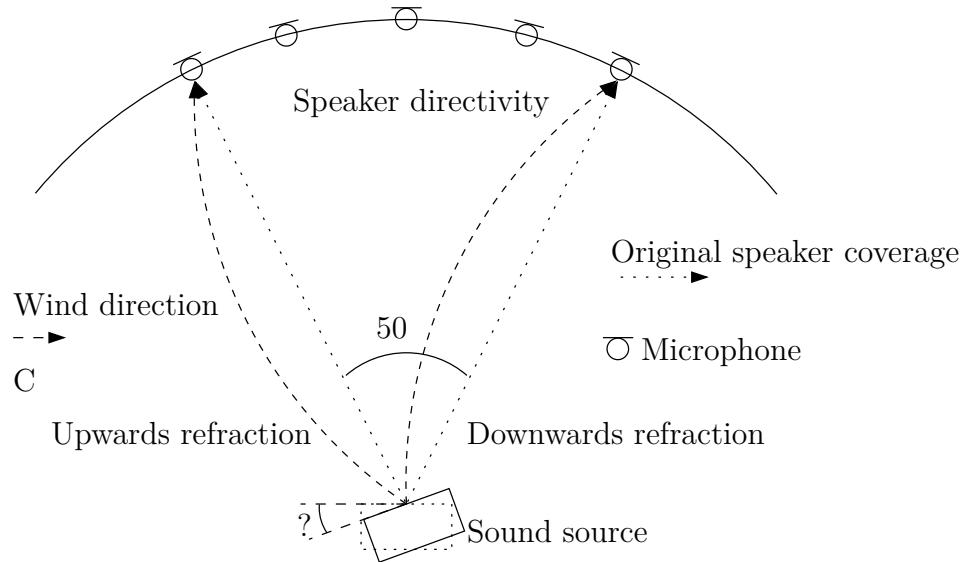
This section aims to design the position of the measuring microphone. The position of the microphone depends on the wind condition, for the crosswind the microphone be placed in the sound field were for the parallel wind, the microphone shall be placed in the shadow zone. The description starts with the former.

The microphone position highly depends on the coverage area of the line source element. Usually, the element which is flown highest cover the as far as possible where the line source element which is closest to the ground cover the frontal audience. Therefore, the distance from the speaker to the microphone has to be found based on the knowledge of coverage distance and the minimum distance before refraction.

The distances from the stage to the back audience depends on the size of the concert. For a small concert, the main stage covers the full area where for large concert delay tower helps the coverage. Delay tower is often used for a concert where the distances from the stage to the audience is above 75 m as Roskilde festival. Roskilde festival situate there delay tower at a distance no longer than 73 m from the main stage Appendix L. The general founded maximum distances from the main stage to the first delay tower was about 73 m for a huge concert, 50 m for a large concert and 30 m for small concert Appendix L. Base on the knowledge of the maximum distances founded in Appendix L and that Roskilde festival is a special case concerning the size and 50 m to 60 m is an often used maximum distance for large concert depending on the hight of the main stage line array. The maximum coverage distances are chosen to be 50 m for the test since the used line array flying tools is not able to fly the line array as high as the asked companies. The flying height of the top line source array element is about from 12 m to 16 m where the flying height of the used test setup is only up to 7 m. Furthermore it was shown in Table 2.1 that refraction occur at a distance of 25 m with 13 m/s.

Another factor which plays a specific role for the microphone distance from the sound source is the hight of the microphone. There are pros and cons for placing the microphone both at the ground or above the ground. The pros of placing the microphone on the ground are that the ground reflection is eliminated, but the cons are that the shadow zone might be closer to the line source array that above the ground, as it can be seen in section 2.4.1. Relating it to the concert situation, the ground reflection in the high frequency is assumed to be low where the ground reflection in the low frequency range is assumed to be higher. Moreover, the hight of the audience ear is not at the ground but in a hight of approximately 1.70 m therefore the most realistic scenario without the audience is at the ear height with an additional ground reflection attenuation mechamisme.

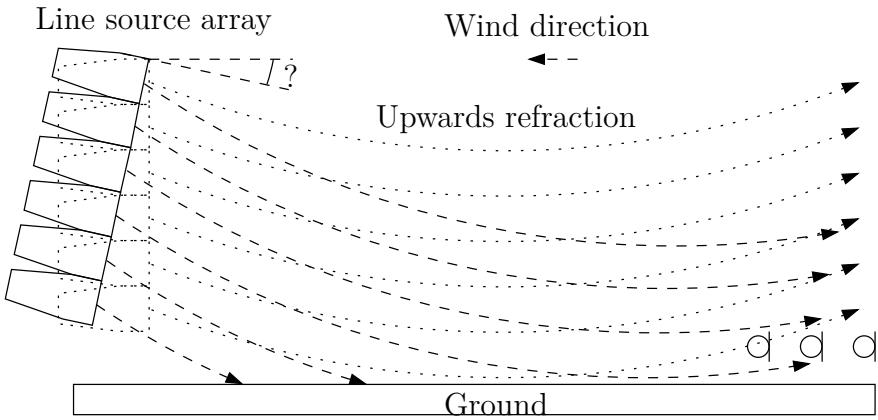
Since the measuring distance is chosen to be 50 m the angel of the speaker is chosen to be the lowest possible angle. This choice is taken because the coverage area at that distance is high at the narrow-angle and is a realistic chose from the company and concert area point of view.?? The following Figure 7.11 shows the microphone position with respect to the speaker position.



**Figure 7.11:** The figure shows the measurement setup

#### 7.4.2 Microphone position at parallel wind

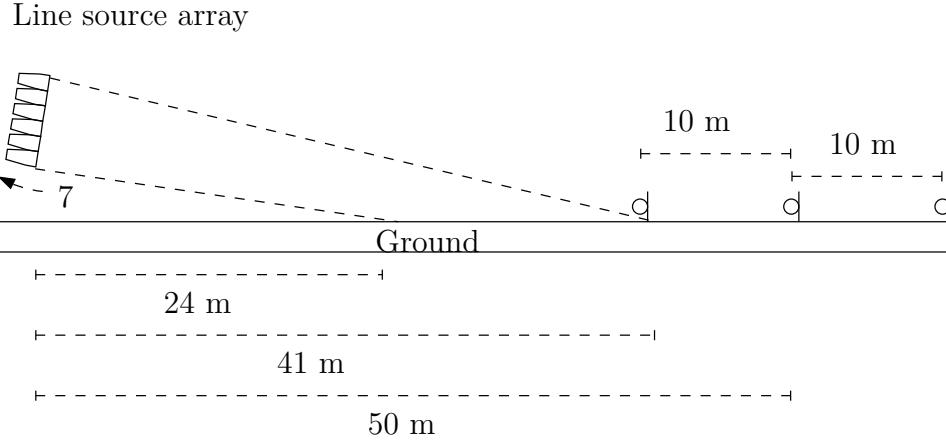
The microphone position of the vertical refraction measurement depends on the shadow zone position, and it is wanted to measure in the shadow zone to explore if it is possible to move the shadow zone backwards by tilting the line array. The following Figure 7.12 illustrate the two measuring cases, which is needed to be measured to conclude on the idea.



**Figure 7.12:** The figure shows the measurement setup

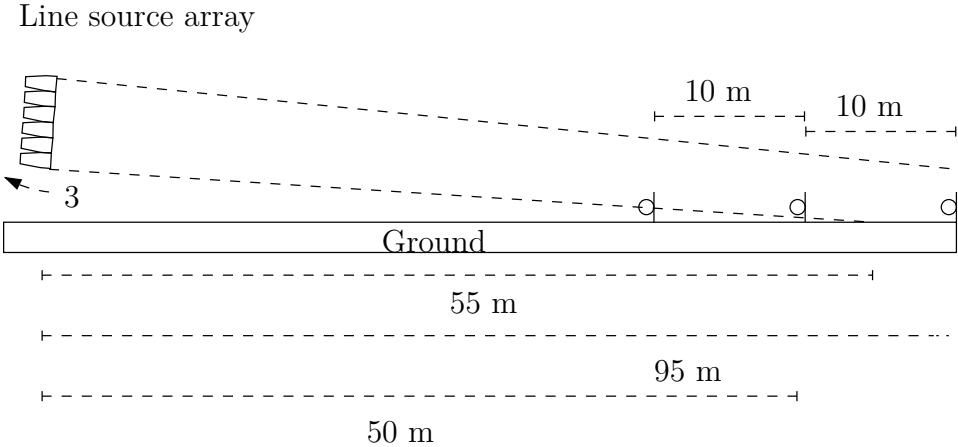
As seen in Figure 7.12 one measurement is where the microphone is within the refracted main lobe of the line source array and one is outside the main lobe of the line source array. To be able to test this scenario, two measuring cases are designed, one

where the main lobe of the line array is angled such that it propagate directly intro the ground in front of all microphone. This measuring case is shown in Figure 7.13.



**Figure 7.13:** The figure shows the measurement setup while the line source array is tilted  $7^\circ$  forward

As seen in Figure 7.13 the main lobe of the line source array is assumed to be near-field which is only hold for high frequencies. At a distances of 40 m this illustration covers frequencies above 6.0 kHz, frequencies below will be wider as the frequency drop section 2.2. But anyway, the highest power of the line source array lays within the center of the main lobe in the frequency of interest due to the directionality charastics of the line source array. In this case the microphone should be without the main lobe while no wind refraction effect the sound, but as the wave is refracted, the microphone is within the main lobe. To make a compainson test case while upwards refraction is present, a test case is designed where the microphone is within the main lobe of the line source array. The following Figure 7.14 illustrate the test case.



**Figure 7.14:** The figure shows the measurement setup while the line source array is tilted  $3^\circ$  forward

In the test case shown in Figure 7.14 more SPL is delivered to the microphone compare to the test case in Figure 7.13. While no wind is present the case in Figure 7.14 delivers the highest SPL to the center microphone and the back microphone, since they are within or at the border of the main lobe. While upwards refraction is present, the proposal solution in section 6.4 suggests that the refraction refract the sound wave such the SPL distribution is vice versa. The upwards refraction refract the sound wave in Figure 7.13 above the microphone and the refraction of the soundwave in Figure 7.14 refract the soundwave to the microphone. In this test case the microphone is situated on the ground such that the microphone is as deep in the shadow zone as possible. In other words, as shown in Figure 6.2, while the microphone is positioned in the same distance from the line source array, while the microphone is on the ground compare to lifted above the ground, the shadow zone is most present at the ground. If more SPL is present in the Figure 7.13 compare to Figure 7.14 the shadow zone distance might be able to be optimised.

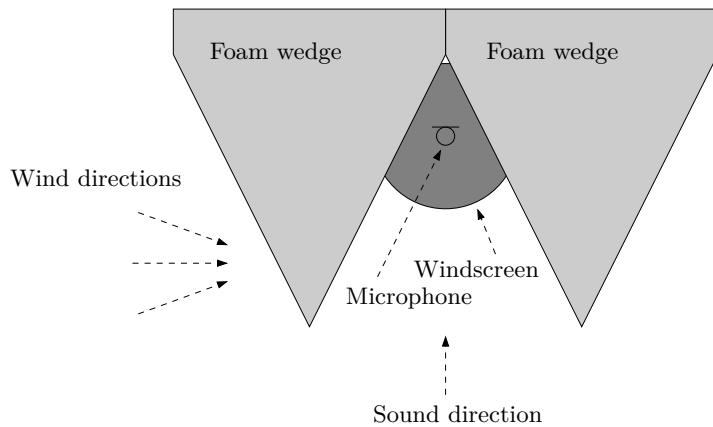
#### 7.4.3 Design of windscreens

The aim of this section is to be able find a windscreens to the measuring microphone such that the wind noise is low compare to the measuring signal. There is one aspect in this windscreens configuration, first the wind noise cannot be filtered electronically between the microphone and the preamp. Therefore the strength of the wind noise shall be as low as the preamp does not overload. Secondly the measurement shall be measurement of the signal and not the wind noise, therefore the signal shall be sufficient higher than the wind noise such that the measurement is trustable and represent the SPL produced by the speaker at the measuring point.

The idea of an additional wind screen is to use the original windscreens to the microphone and then try to stop the wind in just at the microphone with a blocking surface. The surface shall therefore be able to lower the windspeed at the micro-

phone and have as less reflection as possible. The original windscreens are kept on the microphone in the wind stop area to attenuate the wind noise that passes the blockage and attenuate the turbulence produced by the wind stopper.

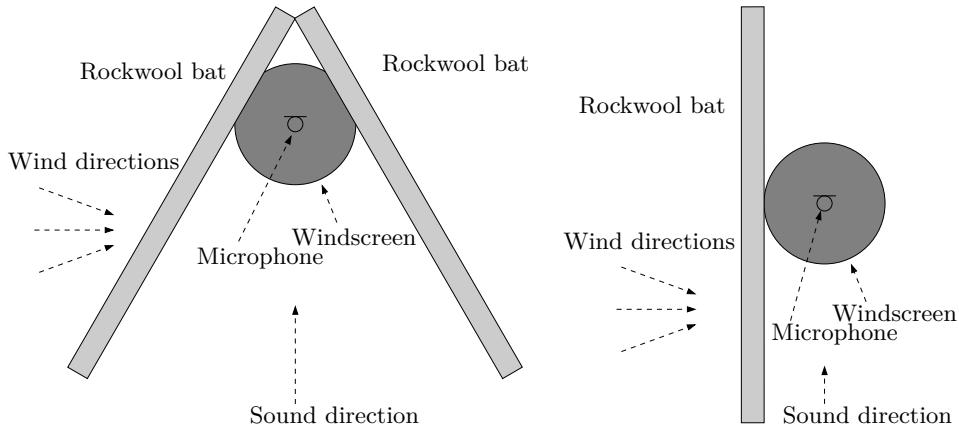
The first two windscreens concept is very identical but just with difference size of material. The idea for the first windscreens is to seal the microphone with foam all around except at the frontal direction. The frontal direction include both  $180^\circ$  angle in the vertical direction and  $90^\circ$  in the horizontal direction. The reason to chose that high degree vertical opening is that no sound from ground reflection is effected and no sound from upwards is stopped by the foam. The reason to have a narrow horizontal opening is to be able to get sound inside the opening but still have a wind stopping effect. The following Figure 7.15 illustrate both windscreens configuration one and windscreens configuration two, just with one size foam wedge.



**Figure 7.15:** The figure shows the foam wedge concept. The concept is covering over two different foam wedges, either two small or two large. The small concept is defined as windscreens configuration one, where the large concept is defined as windscreens configuration two.

The next concept build on the concept in Figure 7.15 just with plan surfaces rockwool plates. The opening is also  $180^\circ$  angle in the vertical direction and  $90^\circ$  in the horizontal direction. The concept is defined as windscreens configuration three. The following Figure 7.16 illustrate the concept.

The next concept build on minimizing the reflection from the additional windscreens by only placing the microphone close against one surface, which cover for the wind noise. The concept is defined as windscreens configuration four. The following Figure 7.17 illustrate the concept.



**Figure 7.16:** The figure shows the rockwool concept. This concept is defined as windscreen configuration three.

**Figure 7.17:** The figure shows the single rockwool concept. This concept is defined as windscreen configuration four.

Before the optimal windscreen configuration is founded, an optimality criteria is defined and a test is designed. The optimal criteria for the windspeed is as low wind noise as possible at the microphone position and low sound reflection. To find the windspeed configuration which meets the criteria best, three tests are made on the windspeed configuration. First the wind speed attenuation of the windspeed configuration is measured to ensure that the windspeed configuration does have an effect on the wind speed. The measurement of the windspeed attenuation can be founded in ???. Secondly the frequency response of the windspeed have to be founded to ensure that the windspeed configuration does not have a large influence on the frequency measurement response of the speaker. To test this criteria, the frequency response of a speaker is measured in the anechoic chamber without any windspeed configuration and without the original windspeed. This measurement is compared with the frequency response of the speaker with the windspeed configuration. The measurement is founded in ???. Finally the wind noise is measured. To measure the wind noise two low speed and low noise fans are generating 2.5 m/s at the microphone position. The wind noise is measured without any windspeed configuration and the original windspeed and compared with the wind noise in the microphone position in the windspeed configuration. To ensure that the background noise is identically on the wind noise measurement with and without the windspeed configuration two microphones are used and recorded simultaneously. Both the time signal and the frequency content is analysed. The measurement is founded in ???. The result for all configuration is as following.

**Configuration one** is the one with the smallest foam wedge and size of the wedge is measured to have the worst wind attenuation. The wind attenuation shows that the wind speed is lowered from 8 m/s to 2 m/s. But the directional turbulence in the wind is more stable in this configuration compare the configuration three and

above. The frequency response of the windscreen configuration is the one that have the lowest effect. At low frequency upto 100 Hz the windscreen does not effect the measurement. Frequency above the frequency response gets off with about 2 dB SPL compare with only the original windscreen. The measured wind noise attenuation is equal zero. In the measurement the wind noise is actualy a bit worse compare to only the original windscreen. The attenuation is both approximatly 10 dB SPL for both with only the original windscreen and the windscreen configuration in the low frequency below 10 Hz, but at some frequency the attenuation is lower than 5 dB SPL for the windscreen configuration. for frequency above 10 Hz the windscreen configuration have no effect.

**Configuration two** is the one with the largest foam wedge and size of the wedge is measured to have one of the best wind attenuation. The wind attenuation shows that the wind speed is lowered from 8 m/s to 1 m/s and have less peek in the wind speed compare to the windscreen with rockwool. The directional turbulence in the wind is more stabile in this configuration compare the configuration three and above but little less stabil compare to configuration one. The frequency response of the windscreen configuration have an amplification in the low frequency range from 80 Hz to 600 Hz of 2 dB SPL. From 1.0 kHz and above the frequency response is very similar compare to only the original windscreen. At low frequency upto 80 Hz the windscreen does not effect the measurement much. The windscreen attenuate the wind noise 10 dB SPL more than only the original windscreen from 30 Hz and downwards to the measured limit at 2 Hz. The frequency range between 30 Hz and 600 Hz have the same attenuation as the original windscreen and the frequency above have further 10 dB SPL more attenuation than the original windscreen.

**Configuration three** is the one with two rockwool bat formed as an arrow and is measured to have wind attenuation between the small wedge and large wedge. The frequency response of the windscreen configuration is the worst. It alternate between  $\pm 6$  dB SPL. At the low frequency range from 80 Hz to 600 Hz the amplification goes from 2 dB SPL at 80 Hz to 6.2 dB SPL at 250 Hz and then back to 0 dB SPL at 700 Hz. At 1.0 kHz the attunuation is at 6 dB SPL and above the frequency response alternate around the frequency response of the original windscreen. The windscreen attenuate the wind noise 10 dB SPL more than only the original windscreen from 30 Hz and downwards to the measured limit at 2 Hz. The frequency range between 30 Hz and 600 Hz have the same attenuation as the original windscreen and the frequency above have further 5 dB SPL to 10 dB SPL more attenuation than the original windscreen. Based on that the frequency response and the wind wind noise attenuation is worse than configuration two, the configuration is excluded from the rest of the test and is not used.

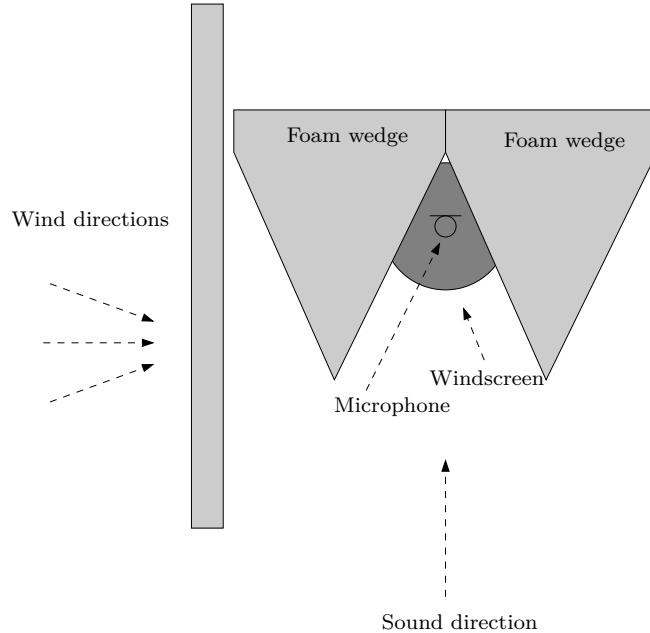
**Configuration four** is the one with only one rockwool bat where the microphone is siturated close to the side of the windscreen and is measured to have one of the best

wind attenuation. The wind attenuation shows that the mean wind speed is lowered from 8 m/s to 1 m/s, but the directional and wind speed turbulence is less stable compare to the configuration the windscreen with foam wedge. The wind speed turbulence circulate from 0 m/s to 2 m/s. The frequency response of the windscreen configuration is does not change more than  $\pm 2$  dB SPL in the low and high frequency range. At frequency from 600 Hz to 300 Hz the windscreen have an attenuation of 4 dB SPL. The noise attenuation is not measured in this configuration, since the mechanical stability is founded to be poor in wind speed above 5 m/s.

#### 7.4.4 Final windscreen solution

Based on the above finding the final windscreen is designed. The design of the final windscreen combines configuration two to and and a updated version of configuration four where the stability problem is solved. This combination is chosen since this two configuration shows the best performance in lowering the wind speed near the microphone and a combination might optimise the wind speed and noise further. Moreover it is chosen that the microphone shall be at the hight of the ear, therefore, an additional ground plan is added to try to stop the ground reflection as much as possible.

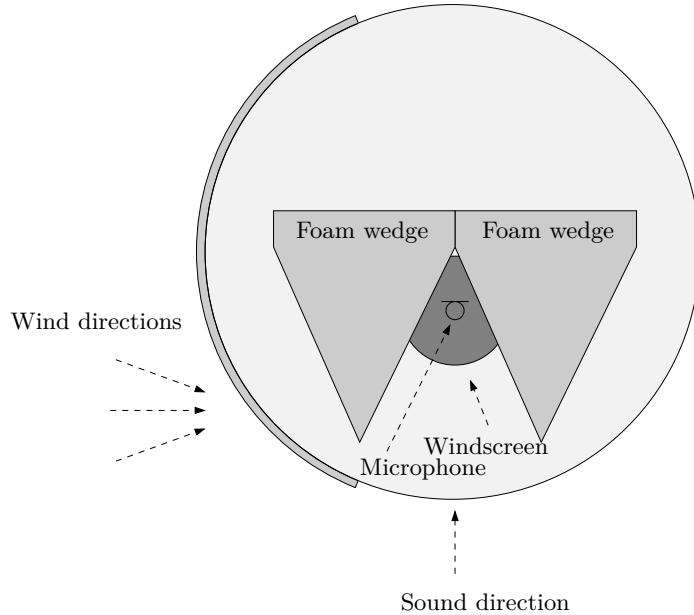
As the first test of the final windscreen solution an preliminary setup is done with the available material in acoustics lab. The preliminary setup is defined as windscreen configuration five. The following Figure 7.18 illustrate the concept.



**Figure 7.18:** The figure shows the single rockwool concept. This concept is defined as windscreen configuration five.

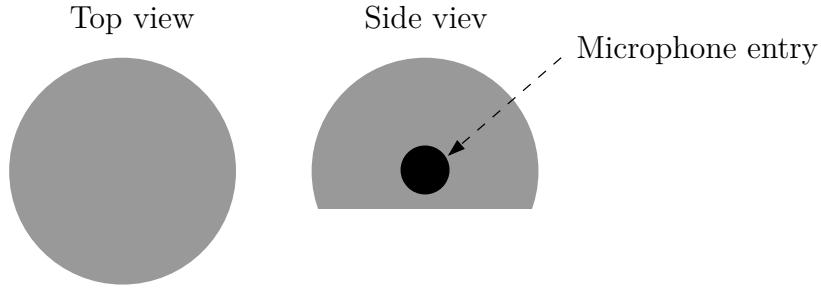
This configuration is measured to have more wind speed attenuation than this combination apart. The wind speed attenuation shows that the mean wind speed is lowered from 8 m/s to 0.8 m/s, but the directional turbulence is less stable compared to the configuration with only foam wedge. The frequency response of the windspeed configuration is as configuration two but with little closer fit to without windspeed in the high frequency.

To deal with the stability problem of the rockwool bat, the rockwool bat is replaced by PVC foam mounted on a circular wood plate as the following Figure 7.19 illustrate



**Figure 7.19:** The figure shows the single rockwool concept

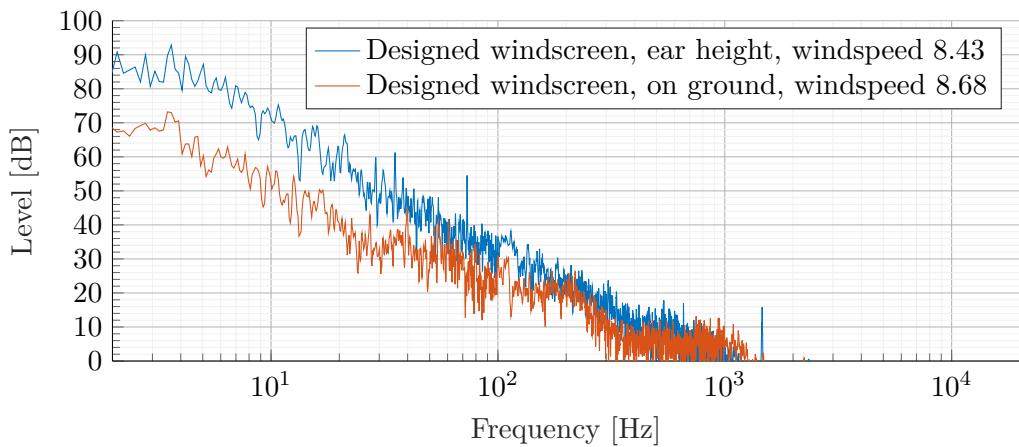
The change in material is made based on the better stability of PVC foam and that the foam wedge is assumed to cancel the reflection from the PVC foam. While adding the wood plate the original windspeed sensor to the microphone then lift the microphone 4.5 cm from the wood plate which might result in sound reflection from the wood plate. To eliminate the reflection from the wood plate the technique from wind turbine measuring setup is used where the windspeed sensor is cut. In the wind turbine microphone setup the cut is done such that half of the microphone is cut down into the wood plate, in this configuration on ... is available, therefore this cut is not suitable. The cut is therefore made 2 mm to 3 mm beneath the microphone such that the microphone is fully covered by the original windspeed sensor. The cut is illustrated in the following Figure 7.20.



**Figure 7.20:** The figure shows the modified original windscreen

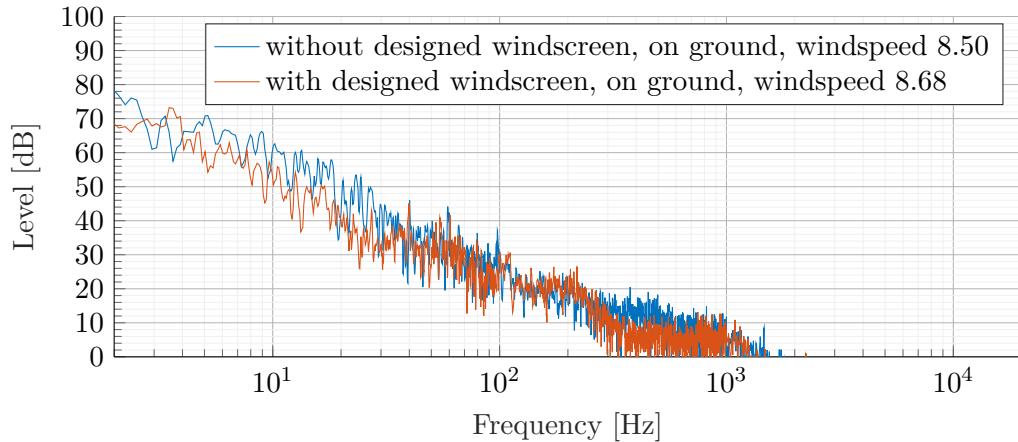
#### 7.4.5 windscreen wind noise attenuation

This section aims to research the wind noise in the windscreen to ensure that the wind noise in real condition does not overload the microphone. The measurement is done both with and without the designed windscreen to decide if the windscreen works in the real scenario with high speed and directionality changing wind. The measurement is furthermore done both in the ear height and on the ground to research is one position have better signal to noise condition in the final measurement. The first preformed measurement is two measurement, one in the ear height and one on the ground. Both measurement is preformed with the designed windscreen. The measurement is done in the same vertical position where the stand is removed and therefore the measurement is not done in parallel. The measurement is done 10 times on each position, such that to measurement with nearly the same wind speed can be compared. The windscreen is placed 90° against the wind, which means that the windscreen is placed in its optimal position where the wind blows directly onto the wide PVC plate. The following Figure 7.21 shows the result.



**Figure 7.21:** The graph shows the frequency content of the measurement with the windscreen in the height of the ear and on the ground

As it is seen in Figure 7.21, the wind noise highly depends on the hight of the windscreen position. By lowering the windscreen from the ear hight done to the ground surface, the wind noise is lowered with approximately 20 dB SPL in the low frequency, which is the frequency area where the wind noise is highest. Furthermore it is research if the designed windscreen have higher wind noise attenuation compare to only the modified original windscreen. The following Figure 7.22 shows the result.

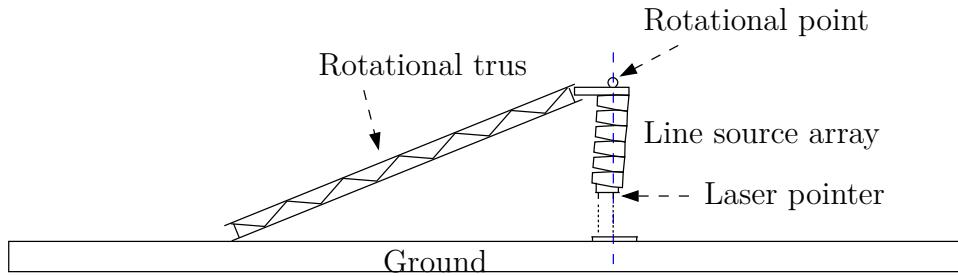


**Figure 7.22:** The graph shows the frequency content of the measurement with and without the windscreen

As seen in Figure 7.22, the windscreens have generally a 5 dB SPL to 10 dB SPL wind noise attenuation. The measurement description is founded in Appendix K. The measurement description also shows noise measurement of the windscreens where the windscreens are rotated both to the left and to the right.

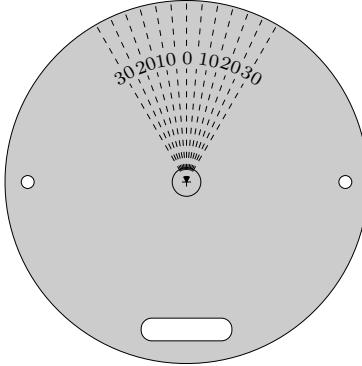
## 7.5 Rotation of the line source array

The aim of this section is to design the turning method for the line source array and ensure that the speaker point in the desired angle. A mechanical solution is chosen for both rotation of the line source array and measuring the rotational angle of the line source array. The mechanical solution to rotate the line source array is a long piece of truss connected to the back of the flying tools of the line source array. By this mechanical solution, a person is able to move the other end of truss and stabilise the angle by placing the end of the truss on the ground. Moreover to ensure that the rotation is done with a specified angle, two laser pointer is attached beneath the line source array. One in the vertical rotation angle and one behind. The one on the rotational axis is then the reference to the back laser pointer. The following ?? illustrate the solution.

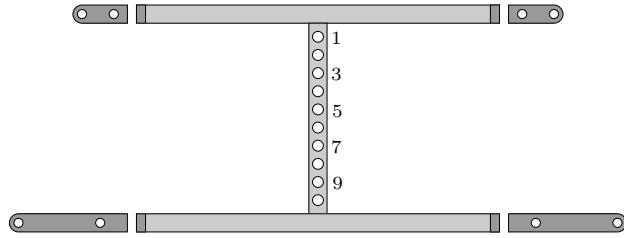


**Figure 7.23:** The figure shows the rotational mechanic where the blue dashed line illustrate the vertical rotational axis.

In Figure 7.23 the reader shall imagine by moving the ground position of the rotational truss towards the reader or away from the reader, the line source array is rotated. The laser pointer holder and plate for measuring the angel is shown in the following two Figure 7.24 and Figure 7.25.



**Figure 7.24:** The figure shows the angle plate.



**Figure 7.25:** The figure shows the laser holder.

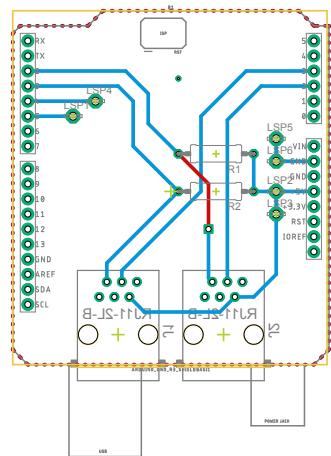
The reference laser pointer is guided into hole 1 in Figure 7.25 which is at the rotational axis while the line source array is tilted  $3^\circ$ . The back laser is guided into hole 10 such that the highest distance between the laser is achieved. The measuring angle plate is then placed on the ground with the reference laser pointing at the  $0^\circ$  angle while the line source points directly forward.

## 7.6 Data logging system

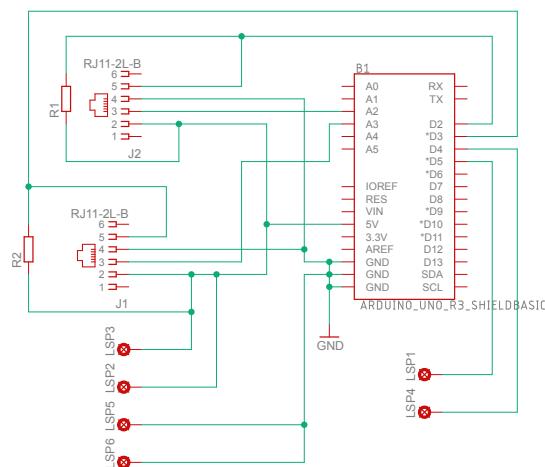
To be able to use the information of the wind speed, temperature and humidity, the data logging of the atmospheric condition have to be synchronised with the measurement.

The humidity and temperature have to be measured.

### 7.6.1 Hardware

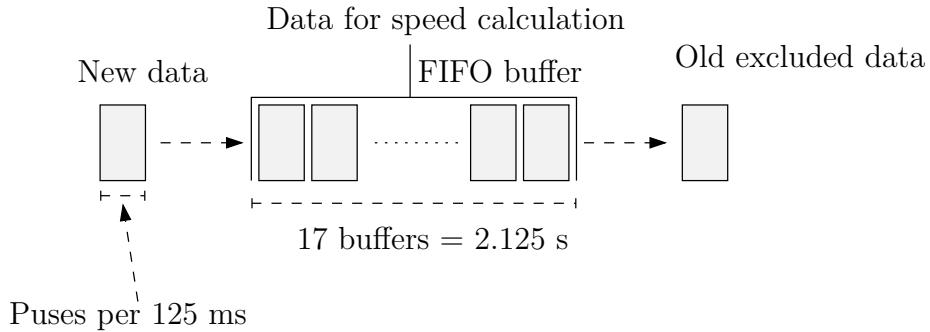


**Figure 7.26:** The figure shows



**Figure 7.27:** The figure shows

### 7.6.2 Firmware



**Figure 7.28:** The figure shows the First In First Out (FIFO) buffer system for wind speed measurement

### 7.6.3 Software

## 7.7 Measuring area

To measure the SPL coverage of the speaker a flat area with mown grass is chosen to be used. The optimal area area without any building or trees might not be possible, therefore blockage or sound refraction surface other than the ground is only allowed to be present in the double of distance compare to the distance from the speaker to the microphone. Based on the refraction effect versus distance founded in section 2.4.1. The distance from the speaker to the microphone array is chosen to be 50 m. The distance is based on the experience of the author described in section 2.1.2 and the founded refraction effect in section 2.4.1. It was founded that the refraction effect should be minimal at a distance of 50 m when the speed of wind is 5 m/s.

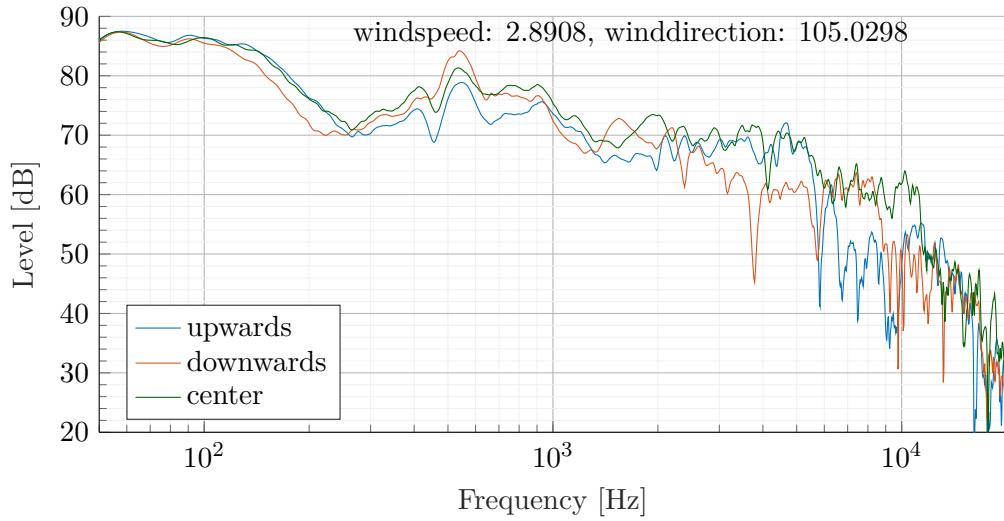
To keep the wind speed realistic for measurement and for concert, but still having wind present, the wind speed doing the measurement is limited in the range for average 5 m/s to 10 m/s. Less average wind speed than 5 m/s is avoided to ensure measureable effect of the wind on sound propagation. The higher limit of the 10 m/s is chosen to ensure that the speaker tower is safe at the hight at 6 m. The limited size of the setup makes the setup wind (følsom) because it is not puttet up as a cube but only as a surface.

# Chapter 8

## Test of measuring design

### 8.1 Test of measuring design

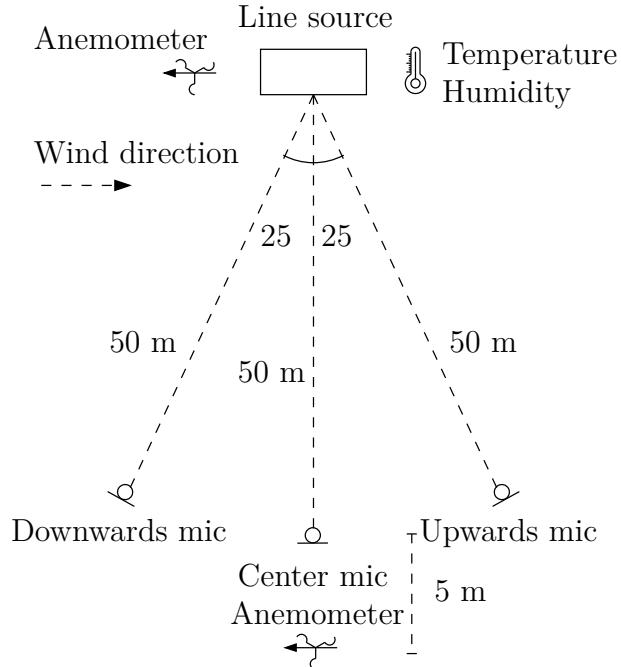
This section aims to test the design measurement in a windy day, to outsource problem and error in the measuring design. The test is done in full scale with all six line source array element and in the designed hight. The test is intended to both test the crosswind measuring design and the parallel wind measuring design, but the wind condition only allowed for crosswind test. After the crosswind measuring design was tested the wind speed dropped to beneath 1 m/s. In the crosswind measuring design, three problems and one code error are observed. The code error is a data save bug, where only the direction of the wind at the speaker tower is saved. The wind direction at the microphone position is not saved doing the test measurement. The code bug is fixed for the final measurement. The following three section 8.1.1, section 8.1.2 and section 8.1.3 explain the observed difficulties or design failure and propose a solution to them. The first difficulty which is discovered is major ground reflections in the measurement. The second problem seems to be frequency response differences of the designed windscreen, where the third error is the angle of the line source array while measuring in the hight of the ear. The explanations is based on the measurement as seen in Figure 8.1 which shows the frequency response on all three microphones at 0° rotation.



**Figure 8.1:** The graph shows the frequency response for all three microphone while the speaker is not rotated

All three microphone measurement in Figure 8.1 is the mean of 10 measurement. The mean is calculated in time domain by aligning the impulse response with help of cross correlation. The wind speed and wind direction is also the mean of the 10 measurement.

To be able to differentiate between the microphone in the explanation, the microphone is named according to the position and the wind direction. In the upwards refraction direction, the microphone is named upwards microphone, in the downwards refraction direction the microphone is named downwards microphone, and the center microphone is named center microphone. The following ?? illustrate the microphone position verses the wind direction.



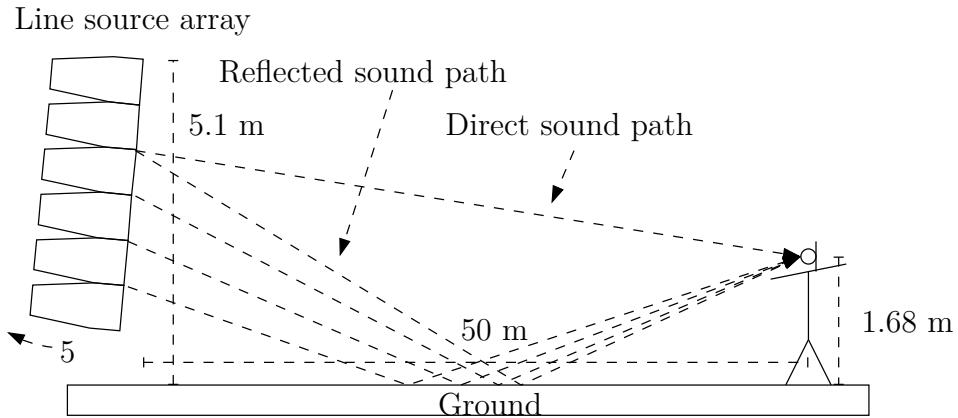
**Figure 8.2:** The figure shows the microphone position versus the position of the line source, while the array is 0° horizontal turned

As seen in Figure 8.2, the position of the anemometer temperature and humidity sensor is also given at its position doing the measurement. To ensure that the measurement is a measure of the transfer function and not the wind noise, a SPL headroom is measured as the first part. The headroom is measured in two ways, one where the wind noise is measured and one where transfer function is measured at high SPL level whereafter the output level to the speaker is lowered by 10 dB SPL and the transfer function is measured again. While the frequency response in the hole frequency range is lowered by 10 dB SPL the headroom is at least 10 dB SPL. The noise floor is founded to be pink noise with 70 dB SPL as its maximum at 2 Hz at all microphone position and with a wind speed of 5 m/s. All measurement is done with sine sweep with constant amplitude and with a headroom of more than 10 dB SPL. The headroom measurement was visually checked by plotting the measuring result in MATLAB®. The headroom measuring check is not saved as a file in this measurement but will be saved and shown in the final measurement.

### 8.1.1 Ground reflections

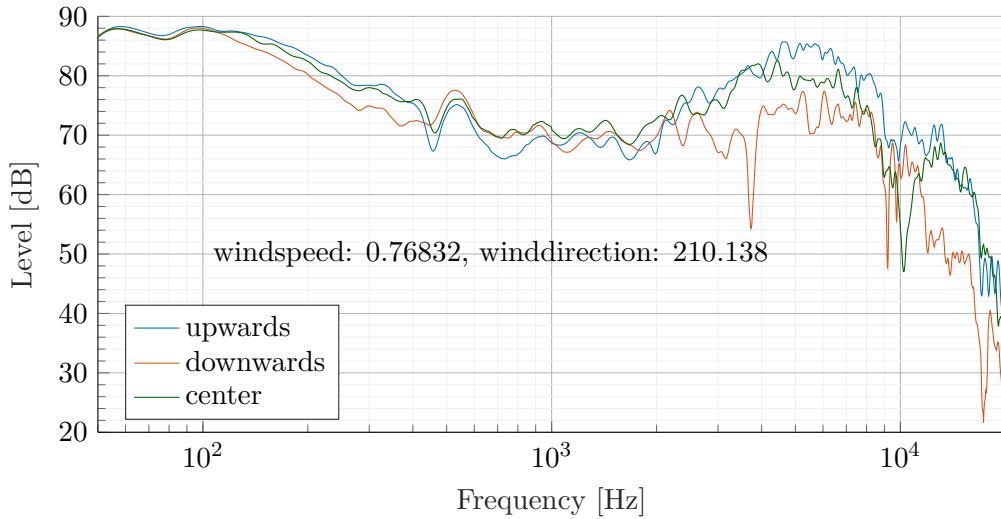
One intended outcome of the windscreens is to block for the ground reflection by the circular wood plate, such that the measuring position can be in the height of the ear as explained in ???. This part of the windscreens fails in fully blocking all ground reflections, and as the frequency grows the effect seems to be worse since higher peaks and depth are present in the measurement compare to the directivity measurement

of the speaker in Figure 7.7. The centre microphone does not have that high peaks and deeps, but the upwards and downwards microphone seems to suffer from ground reflection in the high frequency, which makes the refraction comparison between the microphone position difficult. One thing that might cause the reflection is the position different from  $0^\circ$  vertical of the windscreens in the air to the ground. If the plate is tilted forward, there might be some reflection reaching the microphone. A calculation of the reflection might have helped to justify the ground reflection theory, but since the source is a line source array and not a point source the ground reflection is not as easy to calculate since there might be thousands of sound path from the line source to the microphone. The following Figure 8.3 illustrate the path calculation difficulties and the forward tilting of the windscreens.



**Figure 8.3:** The figure shows an illustration of the measured setup and some soundpath

To be able to make a qualified considering to decide if the peaks and depth are due to ground reflection, the measurement is compared to a measurement where the microphone windscreens is situated on the ground and the frequency characteristics in the measuring direction in Figure 7.7. It have to be noted that the speaker mount, mounted on the windscreens lift the center of the designed windscreens such that the windscreens cannot lay flat on the ground but is tilted forward. The windscreens was tilted forward by  $8^\circ$  doing all measurement on the ground in all microphone position. The following Figure 8.4 shows a frequency response on at all three microphones position of the line source array, where the windscreens is placed on the ground and with a non-rotation line source array.



**Figure 8.4:** The graph shows the measuring result along all three microphone, while the microphone is in the windscreen and the windscreen is on the ground. The graph is a mean of three measurement for the upwards and downwards microphone and one measurement for the center position. The mean calculation is done in time domain where the all impulse responses is allined with cross-correlation

The frequency depth seen at 3.7 kHz in the downwards direction is due to the directionality characteristics of the line source array and can also be seen in Figure 7.7. The same applies to 9.2 kHz and 10 kHz

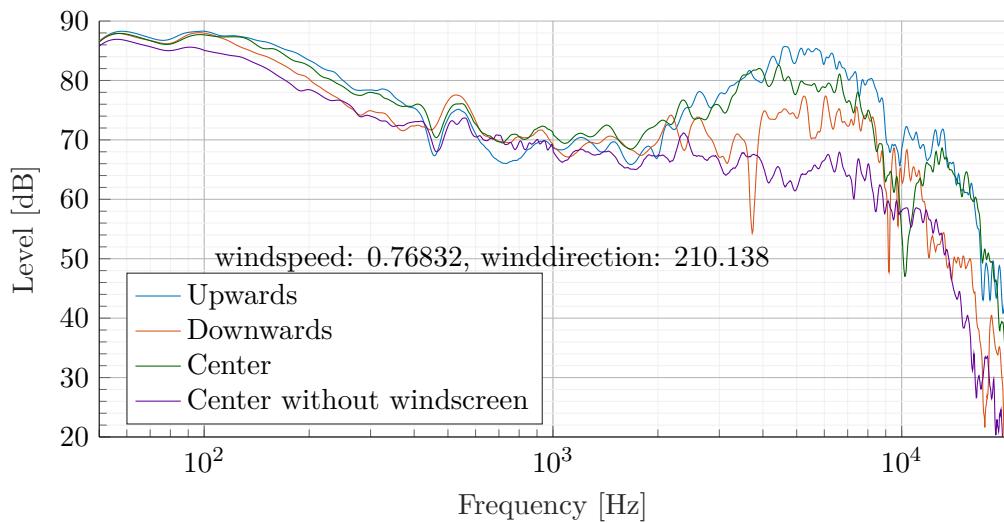
Comparing the measurement where the windscreen is lifted 168 cm from the ground in Figure 8.1 and the measurement in Figure 8.4, it is seen that the first ground reflection comes around 250 Hz depending on the microphone. This ground reflection is dB wise even for all microphone position and might, therefore, be due to sound wave travels through the windscreen bottom plate. The following arriving ground reflection depends highly on the microphone position and then might be due to the vertical angle of the designed windscreen. For the upwards refraction microphone, there seems to be highly reflections in the frequency area from 5.5 kHz to 9.5 kHz where comb filtering is present. Comparing the line source frequency characteristics, it also shows depth in that frequency range, but as high depth as present in the measurement. The measurement has more than 15 dB SPL attenuation where the line source frequency characteristics only have 6 dB SPL attenuation.

Another common response on all microphone while the windscreen lays on the ground is depth around 10 kHz. This depth might be due to the lift of the microphone while it is within the modified original windscreen or that the windscreen is tilted forward and does not lay flat on the ground.

Based on the finding in the measurement, ground reflection occur in the measurement.

### 8.1.2 Frequency differences

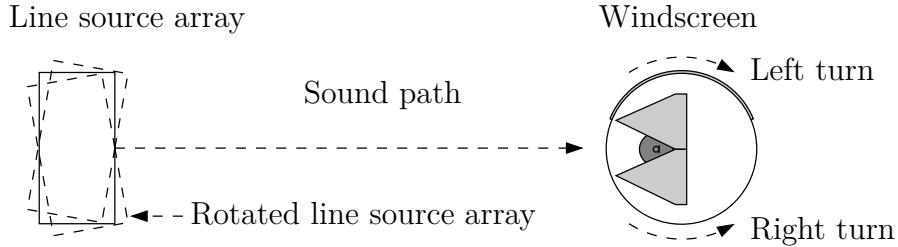
Doing the measurement a frequency differences between 2.0 kHz and 10 kHz is observed and will be researched in this section. The frequency differences is observed while the microphone is laying on the ground whit and without the windscreens. Furthermore the wind doing the measurement is less than 1 m/s and therefore refraction is not present at a distance of 50 m. A comparison measurement is done, where the windscreens are removed from the centre microphone since the wind stopped at the end of the measurement. The following Figure 8.5 shows the measurement result for all three microphones with windscreens and one measurement where the windscreens are removed from the centre microphone. The original modified windscreens covering the microphone is also removed.



**Figure 8.5:** The graph shows the measuring result along all three microphone, where one of the measurement for the center microphone is done with designed windscreen setup and one measurement is done without the design windscreen setup but with the modified original windscreen. While the microphone is in the designed windscreen, the designed windscreen is on the ground. While the microphone is outside the design windscreen, the microphone lays on a wood plate with same size as the designed windscreen. The graph is a mean of three measurement for the upwards and downwards microphone and one measurement for the center position for both center measurement. The mean calculation is done in time domain where the all impulse responses is aligned with cross-correlation

It is seen in Figure 8.5 that the depth at 10 kHz is gone for the center microphone without any windscreens, but either a 20 dB SPL attenuation of the center microphone or a 20 dB SPL amplification while the microphone is within the designed windscreens. The amplification or attenuation is not a problem in itself, the arising problem is that the amplification is not even along the microphone position. The measurement is done with less than 1 m/s of wind speed, and therefore refraction can be excluded as a factor of differences. This means that differences on the windscreens setup might in-

fluences on the frequency response. Three mechanical differences are observed on the windscreens setup doing the measurement. The first is the vertical angle of the windscreen, which was different along all designed windscreens doing the measurement because the ground was uneven. The ground unevenness was measured afterwards to be up to  $8^\circ$ . Secondly, the rotational angle of the designed windscreens was also different along with all designed windscreens. The rotational angle is defined to be  $0^\circ$  to the line source array while the line source array points directly into the centre of the windscreens opening as shown in Figure 8.6.



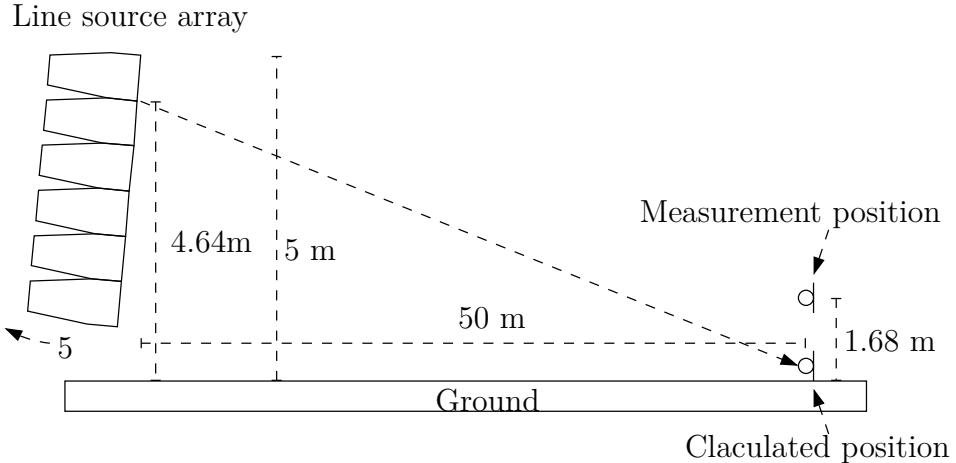
**Figure 8.6:** The figure shows an illustration the windscreen vertical  $0^\circ$  angle

As illustrated in Figure 8.6 no matter the orientation of the speaker, the opening shall point directly to the speaker. In the measurement the opening was not pointing directly to the speaker as shown in Figure 8.6. The vertical angle was adjusted with depends on the wind, which means that the windscreens at downwards direction was turned left, where the windscreens at upwards direction was turned right.

The last differences were the placement of the foam on the plate. In the downwards direction the foam was placed more inwards to the center of the plate while the foam on the other two designed windscreens was placed as shown in Figure 8.6

### 8.1.3 Speaker angle

The angle of the line source array was calculated based on the ground and not from the height of the microphone height. The following Figure 8.7 shows the microphone positions.

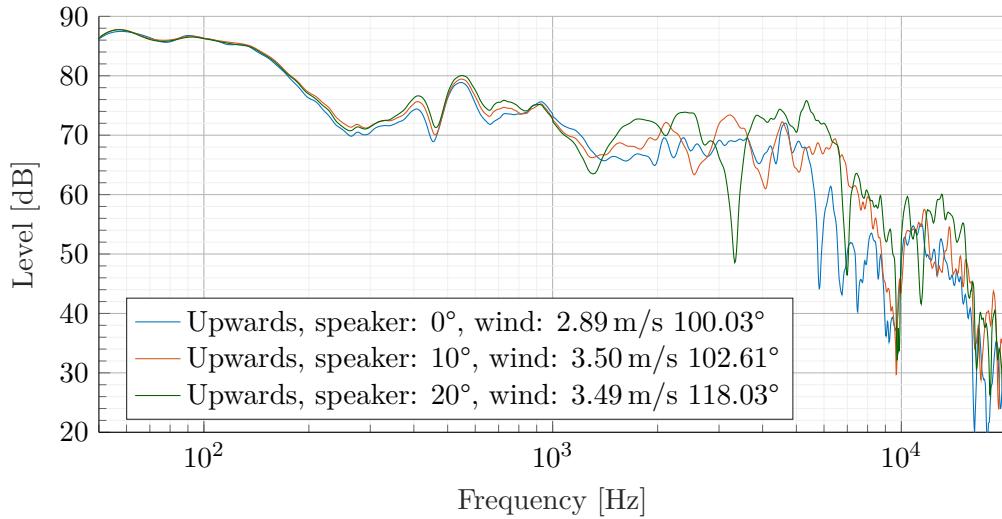


**Figure 8.7:** The figure shows the microphone position doing the calculation of the line source array tilting and the measurement

While using the tilt angle doing the measurement, which was  $5^\circ$ , the highest height before the microphone exit above the nearfield of the line source array coverage main lobe is calculated to be 62 cm. Therefore, since the microphone was placed 1.68 m above the ground the microphone is far above the nearfield main lobe. Comparing the Figure 8.1 and Figure 8.4 it is clearly seen that the microphone was outside the nearfield main lobe of the high frequency. Above 2.0 kHz the SPL is more than 10 dB SPL lower in the ear measuring height compare to the ground position with the same distances to the speaker.

#### 8.1.4 Measuring result

While all error and difficulties are described and disturb the measurement, the measurement indicates that raising the power in the main lobe also raising the power in the shadow zone. Comparing the microphone against each other is difficult since the differences in the boost between the microphone as described in section 8.1.2. Therefore, to extract useful data, the frequency response on the same microphone is compared for  $0^\circ$  of tournament,  $10^\circ$  of tournament and  $20^\circ$  of tournament. The first microphone which is compared is the microphone in the upwards direction. The following Figure 8.8 shows the frequency response for every tournament.



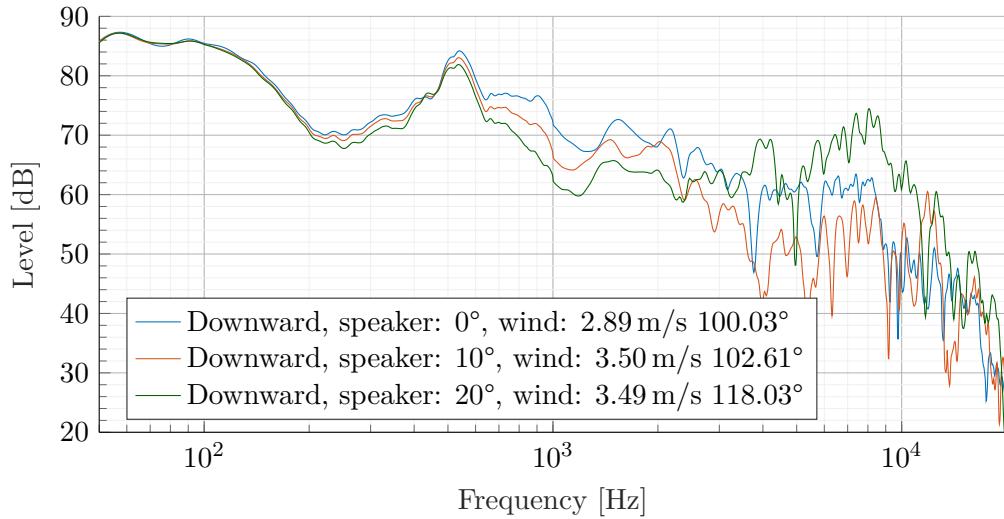
**Figure 8.8:** The graph shows the measuring result for the upwards microphone in three speaker angle, while the microphone is in the windscreens and the windscreens are in the height of the ear. The graph is a mean of 10 measurement in all three angles. The mean calculation is done in time domain where the all impulse responses are aligned with cross-correlation

As seen in Figure 8.8, while the speaker is turned towards the upwards microphone, the SPL is raised. The peaks and depth are not at the same frequency which makes the visual evaluation difficult, but it visually shows that turning the speaker raises the SPL in some frequency area especially above 1.0 kHz. The following Table 8.1 shows the single number SPL both non weighted and A-weighted.

**Table 8.1:** The table shows the measured  $L_{eq,5}$  and  $L_{A_{eq,5}}$  SPL for the upwards microphone

Speaker angle	0°	10°	20°
$L_{eq,5}$	59.65 dB SPL	60.47 dB SPL	61.71 dB SPL
$L_{A_{eq,5}}$	56.91 dB SPL	58.20 dB SPL	60.28 dB SPL

The second microphone which is compared is the microphone in the downwards direction. The following Figure 8.9 shows the frequency response for every tournament.



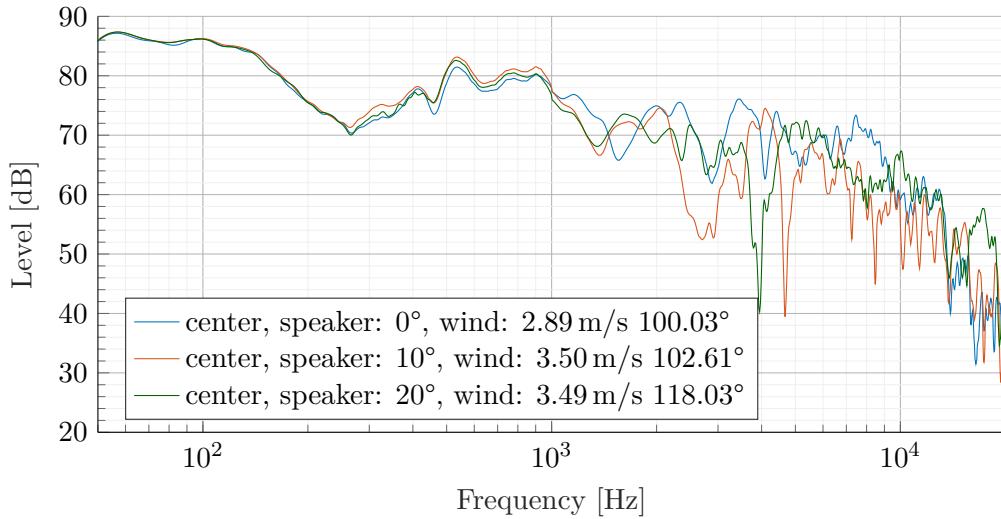
**Figure 8.9:** The graph shows the measuring result for the downwards microphone in three speaker angle, while the microphone is in the windsreen and the windsreen is in the hight of the ear. The graph is a mean of 10 measurement in all three angle. The mean calculation is done in time domain where the all impulse responses is allined with cross-correlation

As seen in Figure 8.9, while the speaker is turned, the SPL is lowered unless the 20° above 2.5 kHz. The raise in power comes from the directionality characteristics of the line source array as seen in Figure 7.7. The peaks and depth is ether not at the same frequency which make the visually justment difficult but it is observed i generally that turning the speaker lower the SPL from 0° to 10° above 650 Hz. The following Table 8.2 shows the single number SPL both non weighted and A-weighted.

**Table 8.2:** The table shows the measured  $L_{eq,5}$  and  $L_{A_{eq,5}}$  SPL for the downwards microphone

Speaker angle	0°	10°	20°
$L_{eq,5}$	59.87 dB SPL	58.47 dB SPL	60.13 dB SPL
$L_{A_{eq,5}}$	57.25 dB SPL	54.60 dB SPL	57.37 dB SPL

The third microphone which is compared is the microphone in the center direction. The following Figure 8.10 shows the frequency response for every tournament.



**Figure 8.10:** The graph shows the measuring result for the center microphone in three speaker angle, while the microphone is in the windspeed screen and the windspeed screen is in the height of the ear. The graph is a mean of 10 measurement in all three angle. The mean calculation is done in time domain where the all impulse responses is aligned with cross-correlation

As seen in Figure 8.10, the frequency response does not either raise or fall markedly while the speaker is turned. The large depth between 2.0 kHz and 5.0 kHz comes from the frequency characteristic of the line source array as seen in Figure 7.7. The following Table 8.3 shows the single number SPL both non weighted and A-weighted.

**Table 8.3:** The table shows the measured  $L_{eq,5}$  and  $L_{A_{eq,5}}$  SPL for the center microphone

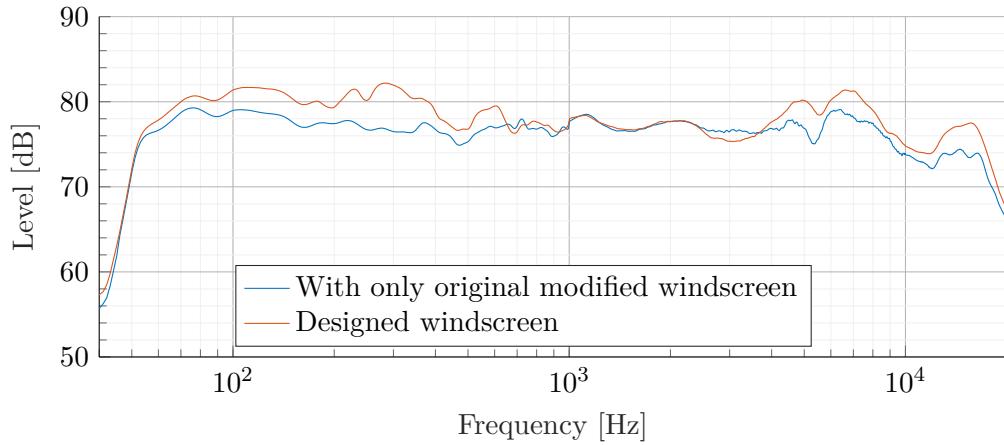
Speaker angle	0°	10°	20°
$L_{eq,5}$	62.73 dB SPL	61.80 dB SPL	61.78 dB SPL
$L_{A_{eq,5}}$	61.65 dB SPL	60.08 dB SPL	60.01 dB SPL

## 8.2 research the problems

To be able to decide the last few detail of the final measurement based on the test and data analysis preformed in section 8.1, the frequency response of the designed windspeed screen is founded in free field condition. Secondly, the wind attenuation of the designed windspeed screen is measured in similar condition to the final measurement and finally the windspeed screen height have to be decided. In section 8.2.1 the frequency response of the windspeed screen is founded where the windspeed screen is rotated and tilted. In section 7.4.5 the wind noise attenuation is measured with different configuration

### 8.2.1 windscreen frequency response

This section aims to research the frequency response of the designed windscreens. It is observed in section 8.1.2 that the measurement with the original windscreens have a boost between 1.0 kHz and 10 kHz compare to one measurement without the designed windscreens. Therefore it has to be founded if the windscreens by itself makes high SPL boost in that frequency range or if the differences is an effect of other sources. To ensure that the windscreens does not have such boost in the measured positions, the windscreens are measured in the anechoic chamber both with tilting and with rotation to research the effect of differences of the windscreens. The measurement is founded in Appendix J. It is observed in the measurement that the windscreens does not have a boost as observed in the measurement in section 8.1.2. The windscreens does have a very small boost of 2 dB SPL beneath 1.0 kHz and above 4.0 kHz but not in the same level as the measurement in section 8.1.2. Furthermore small forward tilting up to 9° only have an attenuation effect above 10 kHz due to plate reflection. A rotation of 30° either to the left or to the right does attenuate in the frequency range of 1.0 kHz to 4.0 kHz. The frequency response of the windscreens is also measured while removing the foam wedge but in this configuration many and high reflection occur and is not an option. Generally the designed windscreens only change the frequency response up to 2 dB SPL while the designed windscreens points with 0° to the line source array and is non tilted. The following measurement Figure 8.11 shows the different while the microphone only is equipped with the original modified windscreens and with the designed windscreens



**Figure 8.11:** The graph shows frequency response of the speaker measured without windscreens and with the designed windscreens with no rotation and no tilting

### 8.3 Update to the final measurement

In the final measurement, the designed windscreen is used as it is designed. It is founded that the windscreen does not have any boost in the high frequency and small differences in position makes no difference. It is founded that high tilting and high rotation does have an effect of the frequency response and shall be avoided to the final measurement. It is furthermore decided that the ground reflection shall be minimised as much as possible, such that it might be possible to compare between microphone. In the end the differences between the speaker characteristics with asymmetric makes it difficult to compare the side microphone since the high degree shows a boost in the higher frequency, as seen in Figure 7.7. Therefore the following points describe the update to the final measurement.

#### Update

The windscreen is positioned at the ground surface height and not in the ear height.

#### Argumentation

This requirement is made according to the founded ground reflection in section 8.1.1 and that the ground reflection shall be minimised such that the microphone might be able to be compared among each other. Secondly it is founded that the wind noise is up to 20 dB SPL lower near the ground section 7.4.5. finally it is assumed in ?? that the reflection is low while the area is full of audience which support that the ground reflection have to be minimised in the measuring point.

#### Update

The windscreen shall lay flat on the ground without tilting higher than 6° and point 0° to the line source array

#### Argumentation

This requirement is made according to the founded frequency response change in section 8.2.1 while the windscreen is tilted and rotated.

#### Update

The angle of the speaker shall be 3.5° downwards

#### Argumentation

This requirement is made according to the founded ground reflection in section 8.1.1, such that it is the lower speaker which have the direct sound path, and therefore ground reflection is minimised

**Update**

The speaker shall have symmetric directionality characteristic with beamwidth of 50°

**Argumentation**

This requirement is made according to the founded in the measuring result section 8.1.4, where the differences in directionality characteristics makes it difficult to compare since the characteristic have a SPL boost in the 55° directionality with an angle of 40°

## **Part III**

# **Measurement**



# Chapter 9

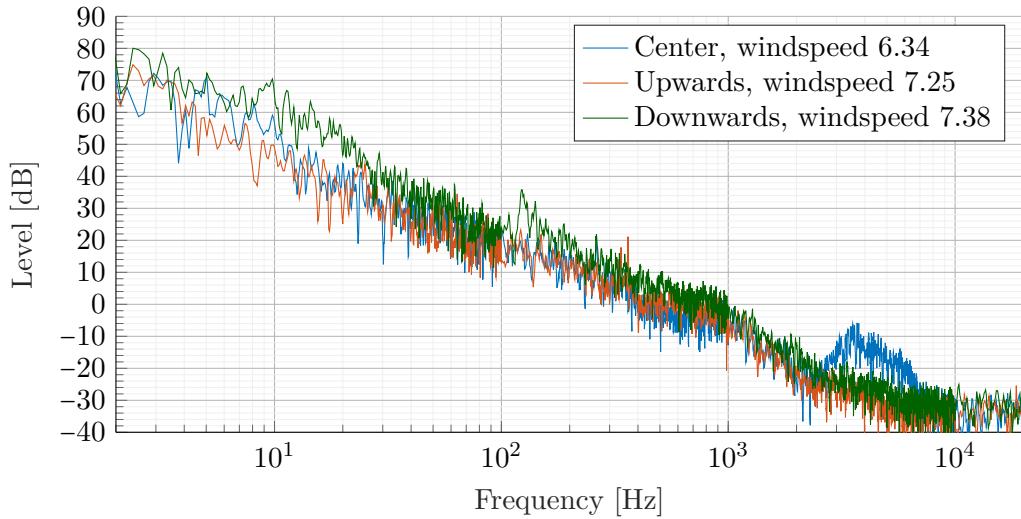
# Measurement

## 9.1 The measurement

The aim of this section is to show the measuring result from the final measurement, then try to find a relation between the wind direction, the wind speed and the angle of the line source array. The first section 9.2 deals with the wind noise in the measurement. The second section 9.3 covers the measurement done in crosswind. The third section 9.4 covers the measurement done in parallel wind. The third section ?? analyses the relation between the wind direction, the wind speed and the angle of the line source array.

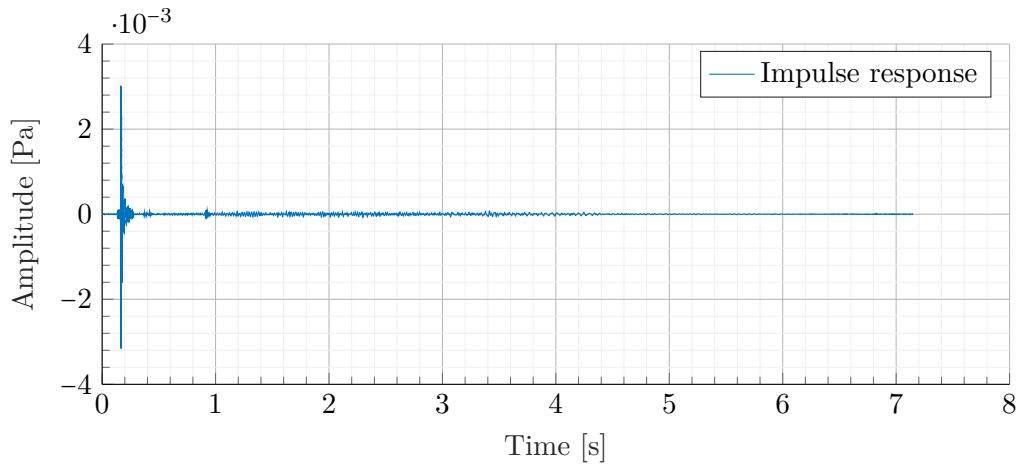
## 9.2 Wind noise doing measurement

Doing the measurement, wind noise is present at the microphone. To ensure that the signal to wind noise level is high, a wind noise measurement is preformed as the first step. The following Figure 9.1 shows the wind noise at all three microphone position with a wind speed of ... .



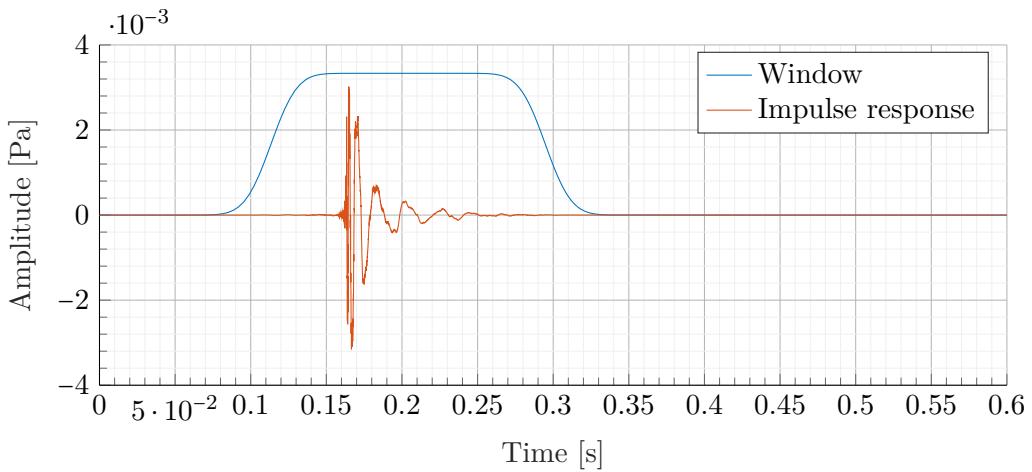
**Figure 9.1:** The graph shows the wind noise in all three measurement microphone at the exact position which is used for the crosswind measurement

The measurement Figure 9.1 shows that the wind noise is pink and therefore most present in the low frequency. To exclude the low frequency wind noise from the measurement, all impulse responses are filtered by a second order high pass filter at 40 Hz. The reason to filter the impulse response at 40 Hz is that the line source array by itself cannot go lower in frequency. The cut off is due to an internal filter in the Digital Signal Processor (DSP) settings of the speaker controller which cannot be turned off. Moreover, due to the way that the impulse response is calculated, wind noise is present along the impulse response. The impulse response is calculated according to ..., where the output signal is convoluted with the measured signal. Then if the noise signal component is present at another time than the signal, the wind noise in the impulse response is present as delayed signal. The following Figure 9.2 shows one impulse response measured during the measurement.



**Figure 9.2:** The graph shows one impulse response measurement of the upwards microphone where the line source array is non rotated

As seen in Figure 9.2, the noise is present along the impulse response time line. This wind noise is not interesting for the analysis and is therefore windowed by a custom made window.

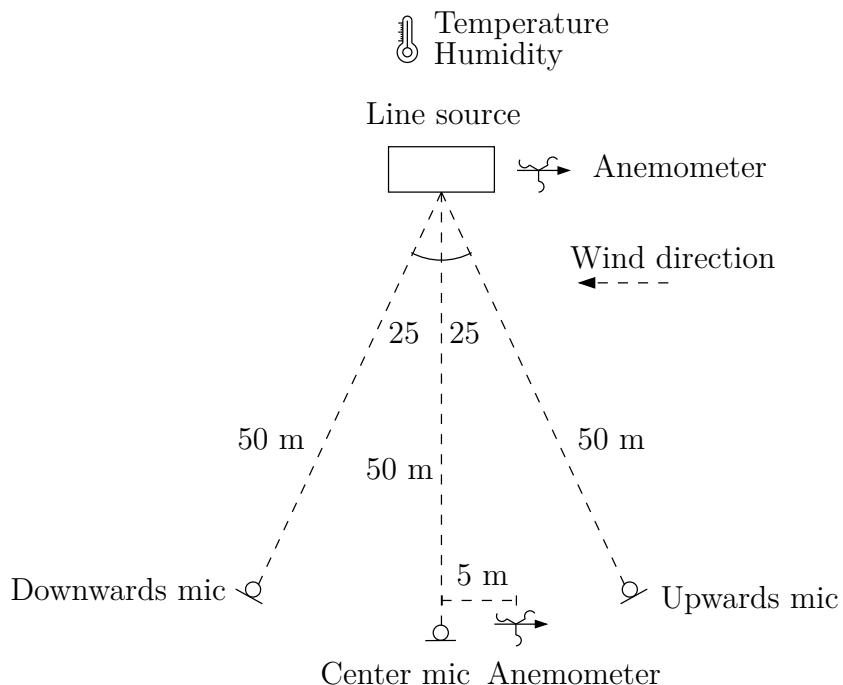


**Figure 9.3:** The graph shows one impulse response measurement of the upwards microphone where the line source array is non rotated

The window function in Figure 9.3 is amplitude wise scaled, such that both the impulse response and the window is visible. The window which is used in the calculation is non-scaled which means that the highest passing area have unity gain of 1 and not  $3.3 \cdot 10^{-3}$ . It is seen that the window passes the impulse response without change, while the noise is filtered.

### 9.3 Crosswind measurement

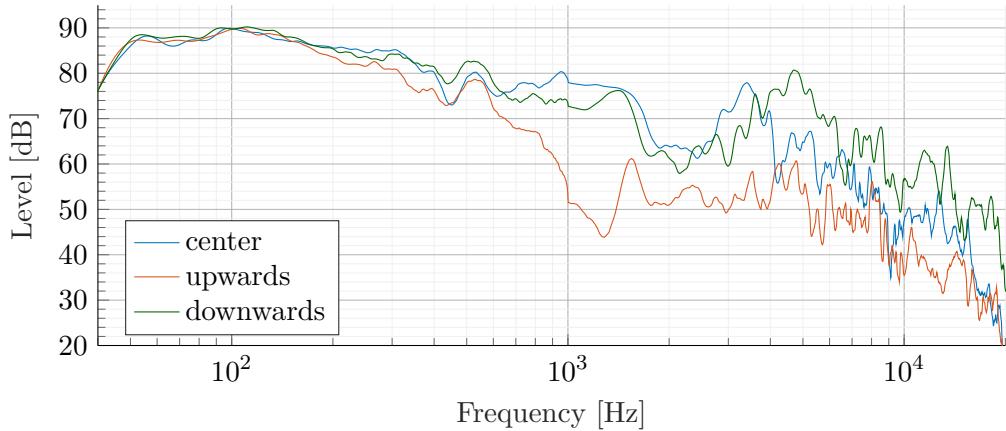
This section is presenting the final measurement which is done according to the crosswind measurement design description in chapter 7 including the update described in chapter 8. The measurement description is founded in ???. The measurement setup is nearly identical to the measurement in chapter 8 unless that the wind direction was turned  $180^\circ$ , the anemometer at the microphone position is placed 5 m to the right of the center microphone instead of 5 m to the back of the center microphone and the anemometer at the line source array is moved to the right side. The measurement setup is illustrated in Figure 9.4.



**Figure 9.4:** The figure shows the microphone position versus the position of the line source, while the array is  $0^\circ$  horizontal turned

while comparing the upwards refraction direction to the downwards direction, it is interesting to analyse at which frequency the refraction starts at the measured distance of 50 m and a wind speed between 5 m/s and 12 m/s. The refraction knowledge is used to generate a high pass filter such that it is only the part where refraction occurs which is compared during the data analysis. The frequency below the refraction is not interesting while comparing if turning the speaker makes more even SPL in the upwards direction compared to the downwards direction. While excluding this part in the one number SPL calculation the refraction part is more visible. To analyse where the refraction occurs, the frequency content is calculated for 3 measurements with high wind speed and compared. At the point where the upwards refraction,

downwards refraction and center microphone gets different is defined as the starting point of refraction at 50 m with the corresponding wind speed in this analysis. The following 3 ??, ?? and ?? shows the frequency response of all three microphone at three different measurement. All measurement is with 0° rotation of the speaker and is chosen since that have the most clear refraction separation and lowest refraction start point compare to the other measurement.

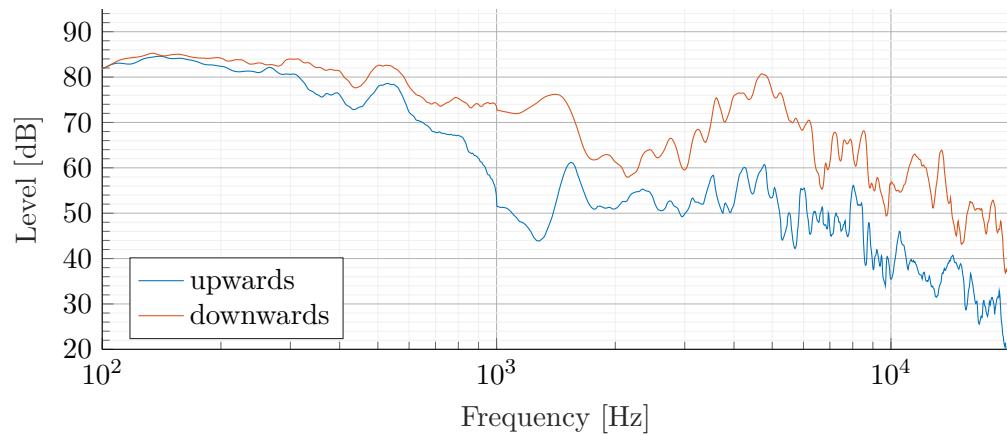


**Figure 9.5:** The graph shows

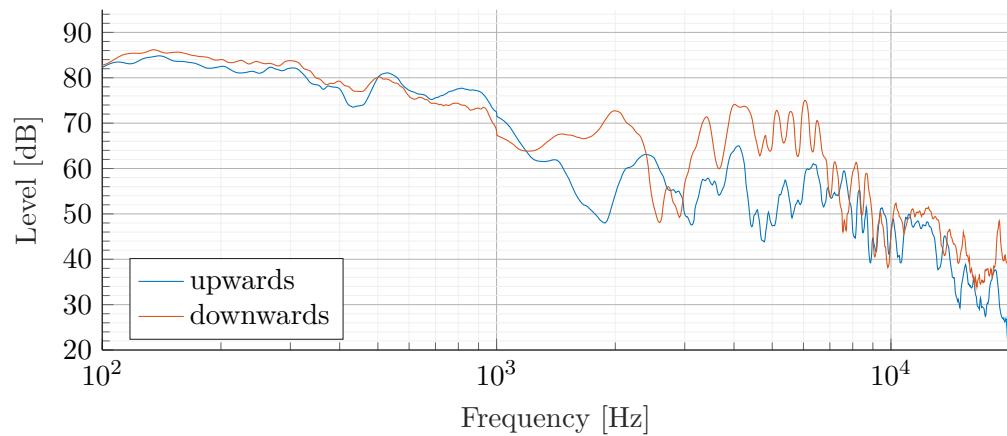
8.00 m/s

As seen in ... the refraction starts at 150 Hz, therefore all beneath 150 Hz have not interest for the further analysis.

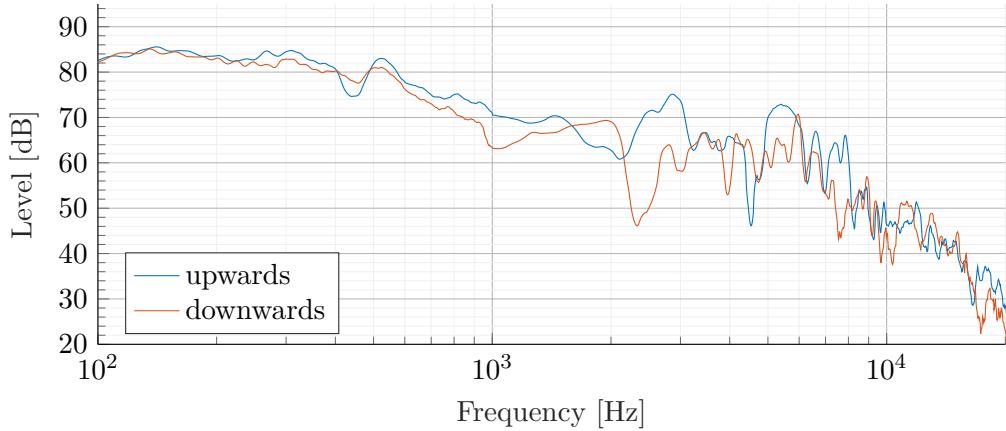
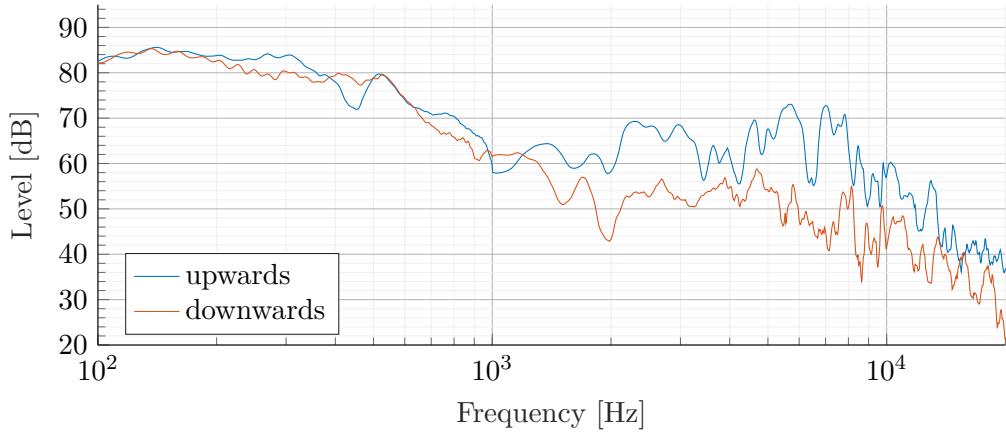
The line source array in the test setup shown in Figure 9.4 is measured in four different angle where every angle above 0° is a rotation towards the upwards microphone. The resolution is with step of 10° with start as 0°, which is the angle shown in Figure 9.4 and up to 30°. The measurement is done at least 10 times for every angle and based on the amount of data, one graph for every angle will be shown where the rest of the result is shown in  $L_{eq,5}$  octave separation above 150 Hz. The graph only includes the upwards measurement and the downwards measurement, the center microphone measurement is given in the  $L_{eq,5}$  and in ?? to keep the plot visually manageable. The chosen graphs are measurements with high and identically with an average of approximately 8 m/s



**Figure 9.6:** The graph shows



**Figure 9.7:** The graph shows

**Figure 9.8:** The graph shows**Figure 9.9:** The graph shows

In the analysis the measurement is split into groups depending on the wind speed with a step of 1 m/s. Furthermore all measurement in the analysis is within  $\pm 25^\circ$  from crosswind to the speaker. Crosswind to the speaker is defined as  $90^\circ$  and therefore  $65^\circ$  to  $115^\circ$  is the acceptable divience, all measurement deviate from this range is excluded. Moreover measurement with wind speed beneath 5 m/s is also excluded. From thoes limitation, the following Table 9.1 shows the amount of measurement for each wind speed step.

**Table 9.1:** The table shows the number of measurement which is between  $65^\circ$  to  $115^\circ$  in the given m/s interval

Speaker angle	$0^\circ$	$10^\circ$	$20^\circ$	$30^\circ$	Total
[5 m/s, 6 m/s[	0	2	4	4	10
[6 m/s, 7 m/s[	2	6	5	5	18
[7 m/s, 8 m/s[	5	3	4	4	16
[8 m/s, 9 m/s[	6	1	2	1	10
[9 m/s, 10 m/s[	1	2	4	0	7
Total	14	14	19	14	61

It is seen in Table 9.1 that 62 measurement is available and the most fall within 6 m/s to 8 m/s.

**Table 9.2:** The table shows the measurement in octave band and within the interval [5 m/s, 6 m/s[ with the given line source array angle

freq	1k			2k			4k			8k			16k		
Mic	U	C	D	U	C	D	U	C	D	U	C	D	U	C	D
$10^\circ$															
m1	54	53	48	47	51	48	46	51	49	39	46	46	29	38	40
m13	47	43	48	41	44	43	48	58	50	43	54	47	35	42	40
avg	51	48	48	44	47	45	47	54	50	41	50	46	32	40	40
Dif	-2.50			1.41			3.10			5.28			7.93		
$20^\circ$															
m4	57	53	49	57	51	49	50	54	52	43	50	51	33	39	39
m8	49	51	46	44	39	40	47	44	48	45	41	46	35	32	34
m15	45	45	47	43	41	42	52	44	41	49	46	38	36	37	32
m17	56	53	48	49	48	45	47	45	48	46	42	45	34	37	36
avg	52	51	48	48	45	44	49	47	47	45	45	45	35	36	35
Dif	-4.06			-4.39			-1.89			-0.29			0.39		
$30^\circ$															
m3	43	46	39	37	34	30	42	40	35	41	35	32	35	26	26
m14	52	46	39	45	39	36	49	49	42	45	44	38	36	34	31
m15	49	48	41	43	36	32	49	41	37	48	36	32	40	26	25
m17	45	44	44	43	37	38	50	46	45	48	39	37	39	30	31
avg	47	46	41	42	37	34	48	44	40	46	39	35	38	29	28
Dif	-6.62			-7.95			-7.98			-10.93			-9.50		

**Table 9.3:** The table shows the measurement in octave band and within the interval [6 m/s, 7 m/s[ with the given line source array angle

freq	1k			2k			4k			8k			16k		
Mic	U	C	D	U	C	D	U	C	D	U	C	D	U	C	D
0°															
m14	46	45	55	35	45	54	46	50	55	41	46	51	29	44	44
m17	42	52	52	33	45	49	42	47	52	38	46	49	28	37	39
avg	44	49	54	34	45	52	44	48	54	39	46	50	28	41	42
Dif	9.62			17.67			9.76			10.75			13.40		
10°															
m5	47	45	44	38	43	37	45	48	47	44	46	44	34	38	38
m6	49	53	51	40	57	57	46	60	59	44	59	58	36	47	46
m8	49	54	53	41	47	53	44	51	54	45	44	48	36	40	43
m9	48	53	50	47	45	42	45	47	46	42	50	44	33	44	36
m11	50	51	48	36	53	41	41	57	49	42	49	47	40	42	44
m12	56	52	51	51	53	51	49	59	56	44	54	52	37	41	41
avg	50	51	49	42	50	47	45	53	52	43	50	49	36	42	41
Dif	-0.39			4.82			6.77			5.38			5.44		
20°															
m2	59	51	50	46	46	44	49	48	51	45	41	43	38	34	35
m6	49	49	48	42	40	42	41	47	46	40	45	41	31	35	31
m9	46	45	47	40	42	41	47	45	47	44	38	44	42	29	31
m19	47	46	47	45	38	44	54	44	42	53	40	40	40	32	34
m20	50	43	45	49	39	39	54	52	43	52	49	43	46	40	36
avg	48	47	48	44	41	42	49	47	46	47	43	42	39	34	33
Dif	-0.84			-2.32			-3.13			-4.67			-5.68		
30°															
m4	51	51	40	48	40	30	47	42	39	46	38	37	34	34	31
m6	41	40	41	43	36	37	48	48	39	51	41	33	43	34	26
m8	49	47	47	44	37	39	52	41	45	47	42	39	42	35	32
m13	49	46	40	47	38	35	54	43	38	52	40	31	42	30	25
m19	41	47	38	48	35	37	57	39	40	54	36	34	43	30	30
avg	46	46	41	46	37	36	52	43	40	50	39	35	41	32	29
Dif	-4.98			-10.22			-11.60			-14.99			-12.14		

**Table 9.4:** The table shows the measurement in octave band and within the interval [7 m/s, 8 m/s[ with the given line source array angle

freq	1k			2k			4k			8k			16k		
Mic	U	C	D	U	C	D	U	C	D	U	C	D	U	C	D
0°															
m10	46	52	53	37	46	45	44	49	50	40	46	52	32	43	45
m15	46	53	51	32	52	44	39	60	49	37	57	50	30	44	40
m18	50	44	52	42	39	45	43	43	50	38	41	48	27	36	42
m20	40	40	51	35	41	48	40	48	51	39	47	49	32	40	42
m22	33	38	52	37	46	42	42	49	56	41	49	59	32	38	45
avg	43	46	52	37	45	45	42	50	51	39	48	52	31	40	43
Dif	8.74			8.19			9.24			12.66			12.39		
10°															
m2	39	52	47	35	49	44	39	58	55	38	49	52	31	44	43
m3	47	48	50	40	52	46	47	54	54	45	49	48	34	39	40
m15	51	52	49	40	49	49	42	49	54	41	53	52	33	46	38
avg	46	51	48	39	50	46	43	54	54	41	51	50	32	43	40
Dif	2.56			7.39			11.68			8.90			7.83		
20°															
m3	51	51	46	48	46	38	56	47	41	47	39	40	34	33	33
m5	46	53	49	38	44	46	46	48	49	46	47	44	34	37	34
m10	48	50	44	40	40	36	43	44	42	41	42	42	34	32	34
m14	46	48	45	40	42	41	48	46	41	44	46	35	34	41	29
avg	48	51	46	41	43	40	48	46	43	44	43	40	34	36	32
Dif	-1.96			-1.16			-4.91			-4.16			-1.52		
30°															
m9	44	44	42	47	39	36	51	46	39	53	41	36	42	31	31
m11	56	42	40	53	39	33	46	46	40	43	40	34	35	33	30
m12	47	51	48	47	41	34	51	45	42	51	39	37	41	30	34
m18	44	46	44	50	41	37	57	48	38	65	41	35	52	35	29
avg	48	46	43	49	40	37	51	46	40	53	40	36	42	32	31
Dif	-4.63			-12.21			-11.61			-17.48			-11.25		

**Table 9.5:** The table shows the measurement in octave band and within the interval [8 m/s, 9 m/s[ with the given line source array angle

freq	1k			2k			4k			8k			16k		
Mic	U	C	D	U	C	D	U	C	D	U	C	D	U	C	D
$0^\circ$															
m9	42	47	51	39	40	45	46	46	48	40	45	45	35	35	42
m11	45	51	53	42	51	47	43	55	52	37	60	47	28	49	42
m12	48	57	52	42	55	52	47	52	50	43	51	54	28	42	49
m13	42	49	54	35	44	56	38	47	56	38	46	51	27	43	43
m16	40	56	52	36	52	49	40	55	60	36	45	53	28	36	46
m19	41	50	50	31	51	44	40	55	52	38	51	55	27	46	45
avg	43	52	52	38	49	49	42	52	55	39	50	52	29	42	44
Dif	8.93			11.23			10.74			12.53			15.42		
$10^\circ$															
m10	48	47	44	41	45	42	49	57	46	45	56	45	32	43	42
Dif	-3.77			1.11			-2.85			0.15			9.30		
$20^\circ$															
m11	43	46	45	42	40	36	52	47	43	49	47	37	40	35	30
m16	50	52	47	50	50	47	53	49	48	50	43	46	36	37	34
avg	47	49	46	46	45	42	53	48	46	50	45	41	38	36	32
Dif	-0.18			-4.58			-6.80			-7.77			-5.76		
$30^\circ$															
m7	46	49	41	52	41	39	58	48	43	54	45	38	40	39	28
Dif	-5.07			-13.06			-15.90			-15.60			-11.15		

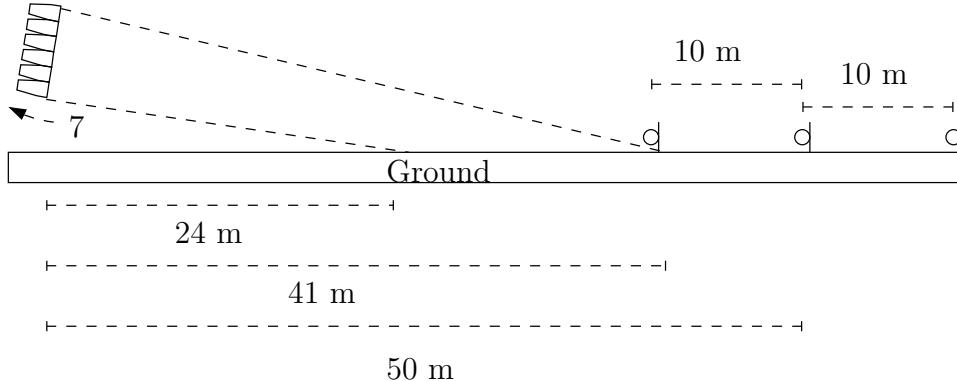
**Table 9.6:** The table shows the measurement in octave band and within the interval [9 m/s, 10 m/s[ with the given line source array angle

freq	1k			2k			4k			8k			16k		
Mic	U	C	D	U	C	D	U	C	D	U	C	D	U	C	D
0°															
m21	46	44	43	43	48	39	55	60	50	47	56	53	37	44	46
Dif	-2.57			-4.00			-5.10			5.98			8.46		
10°															
m4	37	47	47	40	44	45	40	45	48	34	43	47	30	33	42
m7	48	47	47	43	46	43	46	49	53	44	43	48	35	34	38
avg	42	47	47	41	45	44	43	47	50	39	43	48	33	34	40
Dif	4.94			3.10			7.69			8.55			7.64		
20°															
m1	46	50	42	43	44	42	47	44	48	46	43	41	37	38	33
m7	49	46	49	45	40	43	51	48	44	48	46	42	40	38	37
m12	48	50	48	46	42	52	52	51	49	48	46	44	36	36	35
m13	49	45	49	45	42	48	49	47	51	50	44	45	40	35	34
avg	48	48	47	45	42	46	50	47	48	48	45	43	38	37	35
Dif	-0.79			1.44			-1.93			-5.15			-3.73		

## 9.4 parallel wind measurement

This section is presenting the final measurement which is done according to the parallel wind measurement design description in chapter 7 including the update described in chapter 8. The measurement description is founded in ??.

Line source array

**Figure 9.10:** The figure shows the microphone position

The measurement setup is ... The measurement setup is illustrated in ??.

The line source array in the test setup shown in ?? is measured in three different tilt angle, one tilted 5° upwards, one with 0° tilting and one with 5° downwards tilting. The measurement is done at least 10 times for every angle and based on the amount of data, one graph for every angle will be shown where the rest of the result is shown in  $L_{eq,5}$  octave separation above 150 Hz. The chosen graphs are measurement with high and identically with an average of approximately 8 m/s.

To be able to compare the result from each microphone, while the microphone is placed with different distance to the speaker the distance dependency of the microphones is removed. It is decided to norm the distance to 50 m which is the center microphone. Calculating the distance dependency loss is not as simple for a line source array as for a point source, since the SPL loss at doubling of distance depends on the wavelength, distance and height of the line source array section 2.2. Furthermore it also depends on the viscosity of the air section 2.3.1. To be able to remove this factor from the measurement, the frequency range for near field have to be founded. The graph in ?? shows the limiting distance where near field changes to far field for the used line source array. As seen ... All data measured under 5.799 99 kHz is propagating in far field at 40 m and above. This means that all data beneath 5.799 99 kHz is far-field calculation while normalising the frequency response. For the normalising from 40 m to 50 m all frequency above 7.2 kHz is propagating in near-field. Normalising from 60 m to 50 m all frequency above 8.7 kHz is propagating in near-field and frequency beneath 7.2 kHz radiate within far-field. The calculating rate is then as follows ??

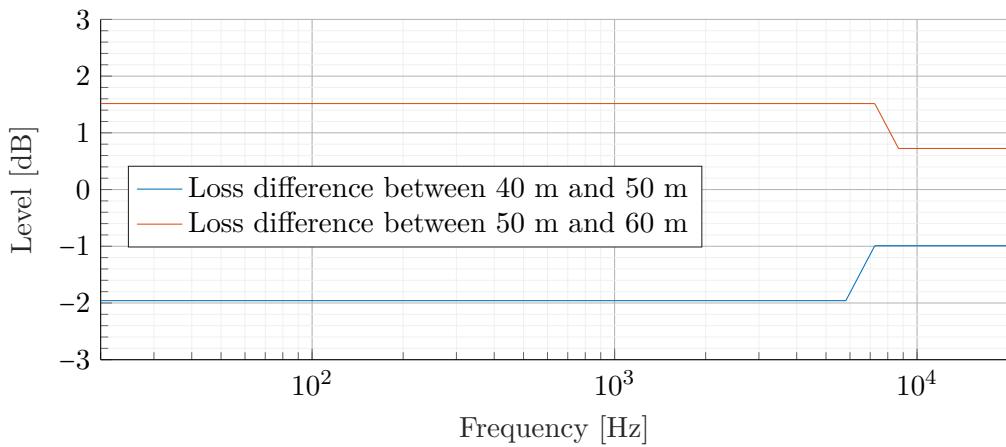
	far-field	near-field
40 - 50	0 hz - 5800 hz	7200 hz - 20000 hz
60 - 40	0 hz - 7200 hz	8700 hz - 20000 hz

To calculate the far-field loss the following Equation 9.1 is used

$$L_2 = L_1 - \left| 20 \log_{10} \left( \frac{r_1}{r_2} \right) \right| \quad (9.1)$$

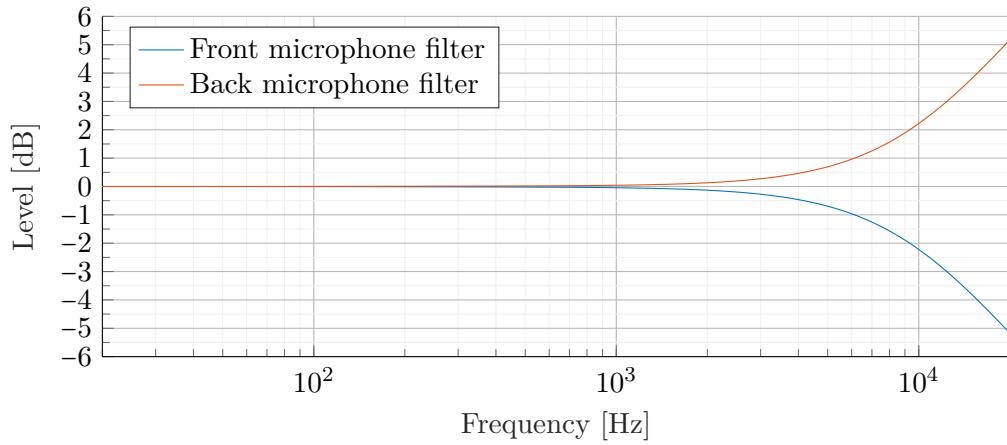
To calculate the near-field loss the following Equation 9.2 is used

$$L_2 = L_1 - \left| 10 \log_{10} \left( \frac{r_1}{r_2} \right) \right| \quad (9.2)$$



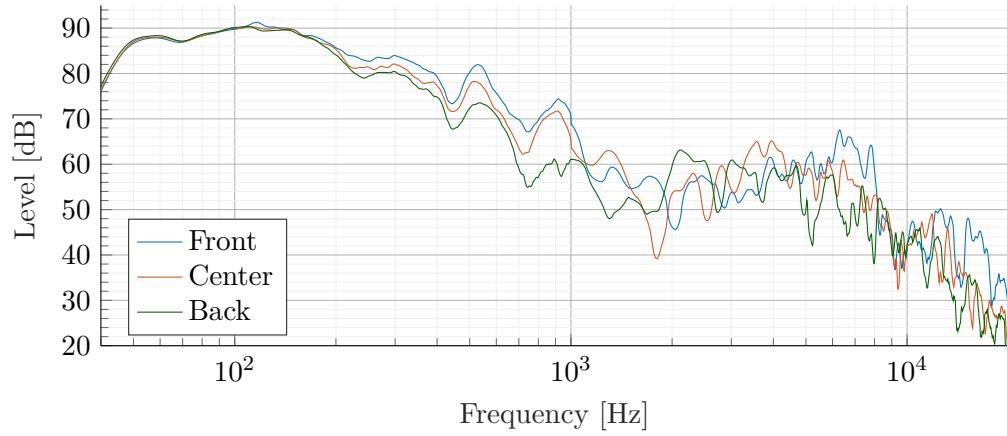
**Figure 9.11:** The graph shows

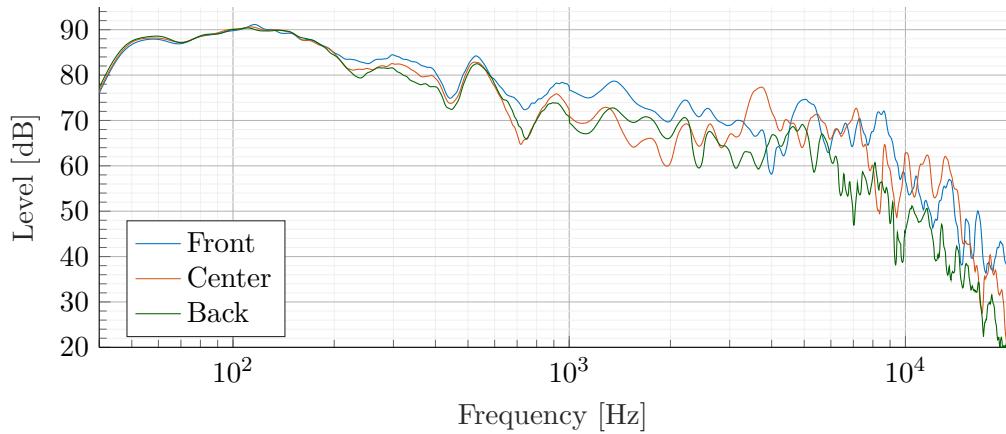
Absorption depending on humidity and temperature, to calculate the loss at 10 m of distances, the formula in standard [] is used with the measured data for every measurement. The atmospherical pressure is not measured doing the measurement, and therefore the reference 101.325 kPa is used as pressure. All 30 measurement is done with short time differences and therefore the temperature and humidity only change with fraction. One filter example is given in Figure 9.12 with 12 °C and 48 % humidity. The example temparature and humidity is from one of the measurement.

**Figure 9.12:** The graph shows

The frequency response in Figure 9.12 is used for compensate the viscosity in the air.

Both the filter in Figure 9.11 and Figure 9.12 is applied to the signal in frequency domain, while afterwards the result is transferred back to time domain for signal analysis.

**Figure 9.13:** The graph shows



**Figure 9.14:** The graph shows

**Table 9.7:** The table shows the number of measurement which is between  $-25^\circ$  to  $25^\circ$  in the given m/s interval

Speaker angle	$3^\circ$	$7^\circ$	Total
$[5 \text{ m/s}, 7 \text{ m/s}[$	3	5	8

**Table 9.8:** The table shows the measurement in octave band and within the interval [5 m/s, 7 m/s[ with the given line source array angle

freq	125		250		500		1k		2k		4k		8k		16k	
deg	3°	7°	3°	7°	3°	7°	3°	7°	3°	7°	3°	7°	3°	7°	3°	7°
F																
m 1-3	59	59	57	57	56	56	50	52	46	48	47	47	51	46	41	38
m 5-4	60	59	58	56	57	54	53	50	51	47	50	48	51	51	44	42
m 6-6	59	59	56	56	53	55	47	55	37	54	53	54	47	54	35	44
m n-6	ND	59	ND	57	ND	57	ND	57	ND	61	ND	66	ND	61	ND	52
m n-10	ND	59	ND	57	ND	57	ND	54	ND	53	ND	56	ND	56	ND	42
avg	59	59	57	57	55	56	50	53	45	52	47	54	50	54	40	44
Dif	-0.6		-0.47		-0.55		3.31		7.57		7.59		4.25		3.39	
C																
m 1-3	59	59	56	56	54	54	50	51	46	54	51	60	46	51	38	37
m 5-4	60	58	57	55	53	53	52	51	49	51	52	55	49	48	37	37
m 6-6	59	59	55	55	50	54	45	50	37	49	45	56	41	53	31	45
m n-6	ND	58	ND	56	ND	55	ND	53	ND	55	ND	56	ND	53	ND	39
m n-10	ND	58	ND	56	ND	54	ND	50	ND	46	ND	50	ND	49	ND	44
avg	59	58	56	55	53	54	49	51	44	51	49	56	45	51	35	40
Dif	-0.64		-0.43		1.44		2.16		6.65		6.19		5.56		5.04	
B																
m1-3	59	59	56	56	54	54	53	51	51	51	48	56	48	47	36	35
m5-4	60	58	56	54	53	48	50	50	47	44	47	48	46	46	35	39
m6-6	58	58	54	54	47	53	37	50	40	50	41	50	37	45	28	34
m6	ND	58	ND	55	ND	53	ND	46	ND	39	ND	43	ND	45	ND	35
m10	ND	58	ND	56	ND	53	ND	46	ND	44	ND	55	ND	53	ND	42
avg	59	58	55	55	52	52	47	49	46	45	45	50	44	47	33	37
Dif	-0.79		-0.57		0.82		1.90		-0.66		4.66		3.73		3.76	



# **Part IV**

# **Results**



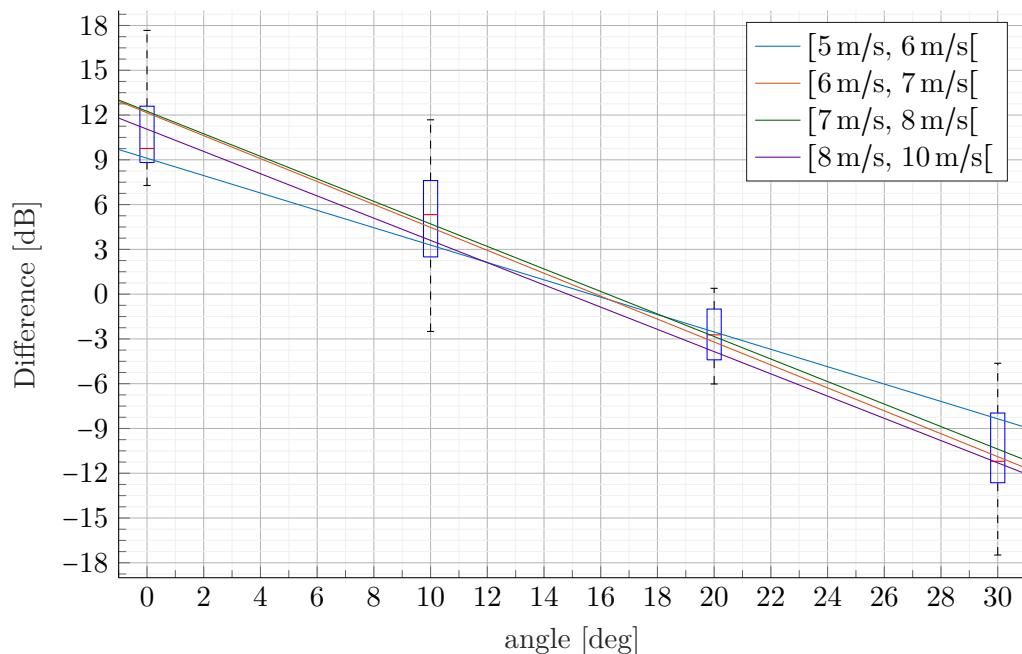
# Chapter 10

## Results

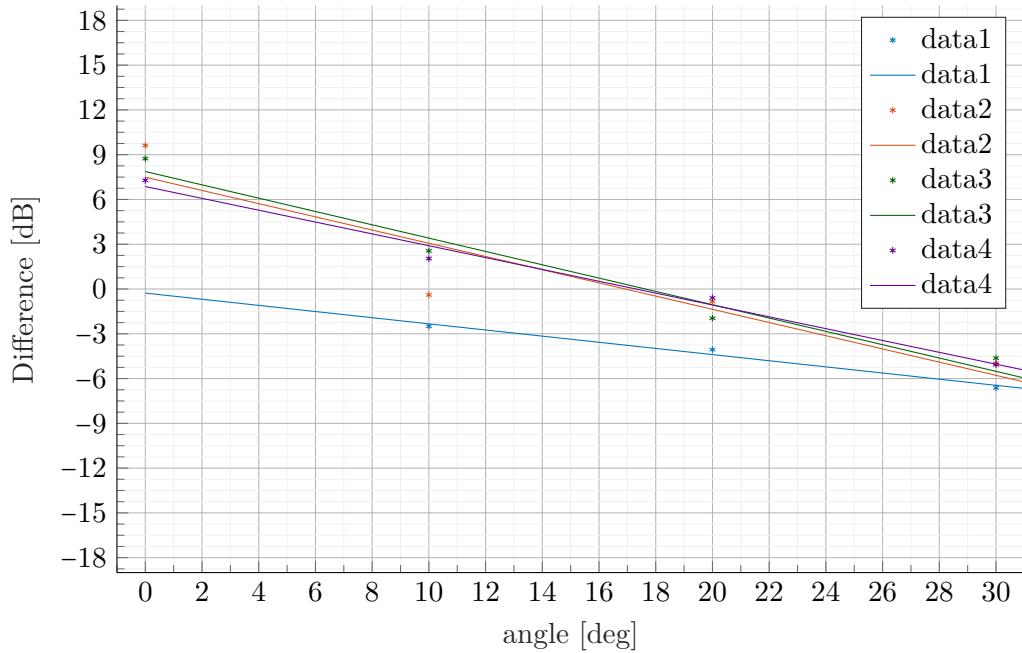
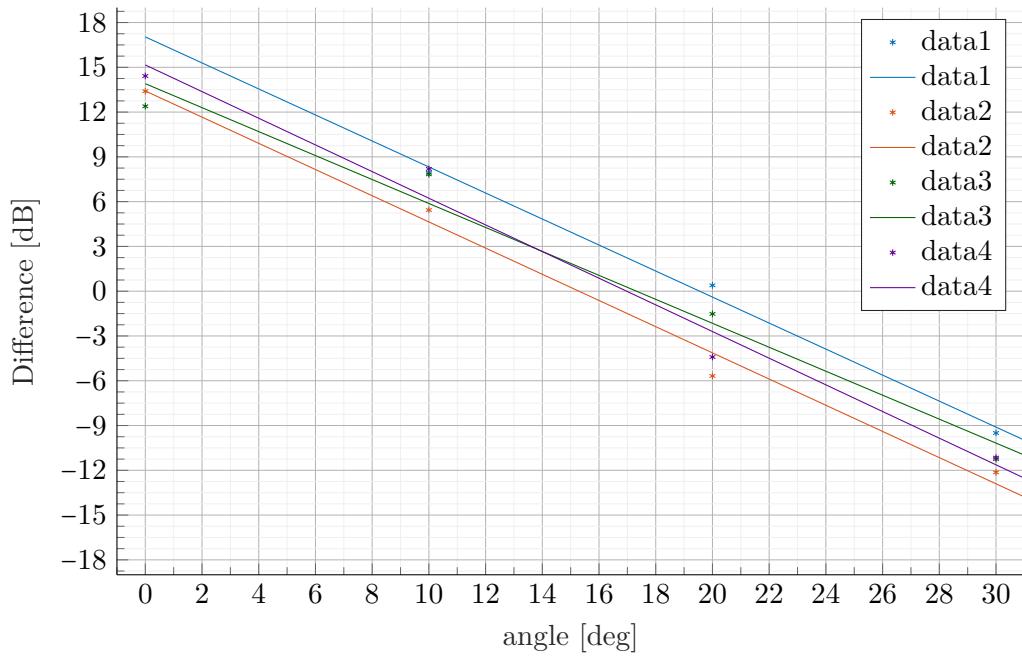
### 10.1 Result

This section aims to analyse the data obtained in the final measurement shown in chapter 9

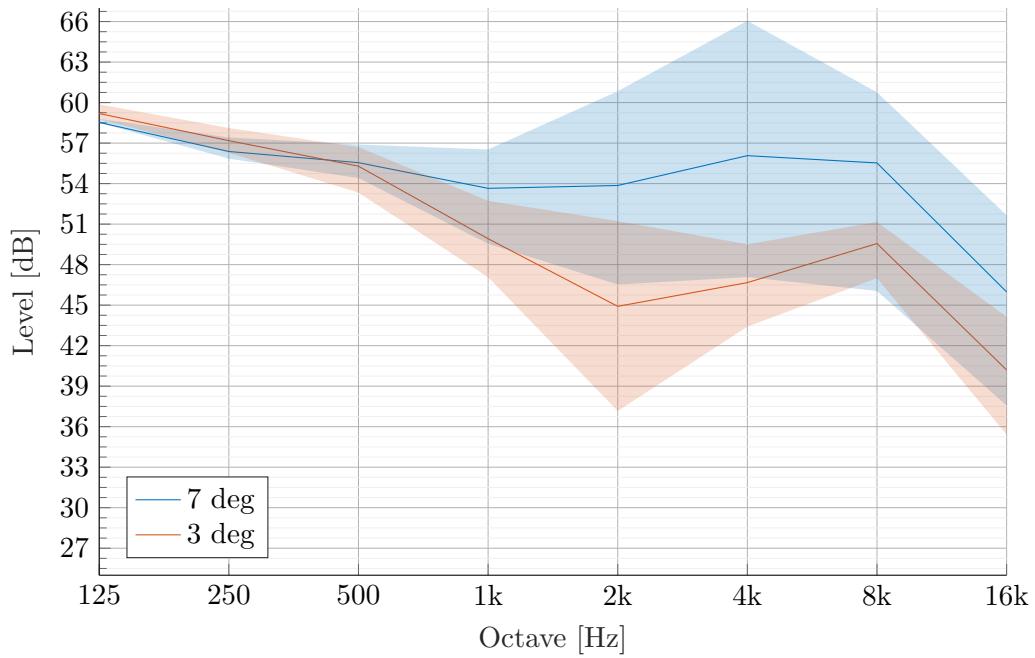
### 10.2 Crosswind data analysis



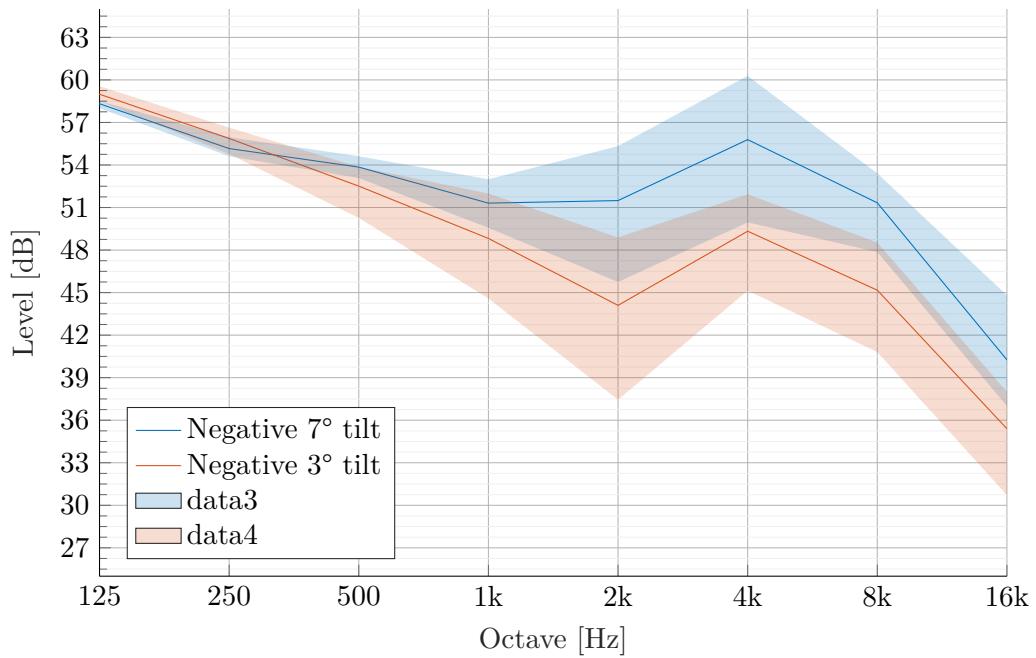
**Figure 10.1:** The graph shows

**Figure 10.2:** The graph shows**Figure 10.3:** The graph shows

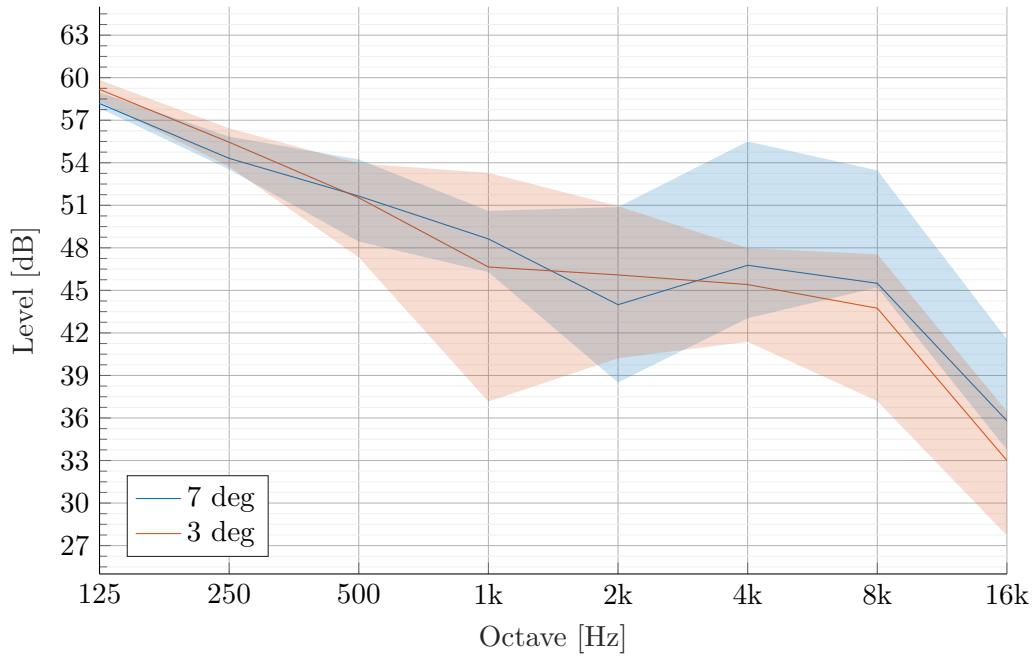
### 10.3 Parallel wind data analysis



**Figure 10.4:** The graph shows



**Figure 10.5:** The graph shows



**Figure 10.6:** The graph shows

## **Chapter 11**

# **Discussion and conclusion**

### **11.1 Conclusion**



# **Part V**

# **Appendix**



# Appendix A

## cross wind effect on line source array

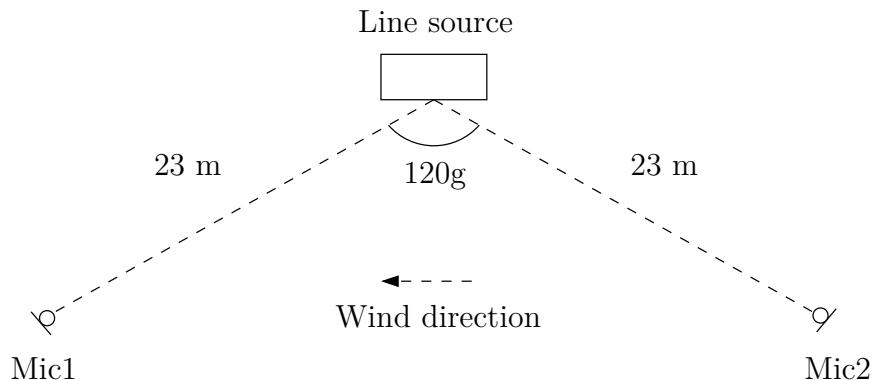
A measurement was made to measure the transfer function differences in two point in cross wind. The used speaker have a horizontal dispersion pattern of 100°.

### Materials and setup

To measure the transfer function in a cross wind situation, the following materials are used:

**Table A.1:** Equipment list

Description	Model	Serial-no	AAU-no
PC	Macbook	W89242W966H	-
Audio interface	RME Fireface UCX	23811948	108230
Microphone	GRAS 26CC	78189	75583
Preamp	GRAS 40 AZ	100268	75551
Microphone	GRAS 26CC	78186	75582
Preamp	GRAS 40 AZ	100267	75550
dB technologies	DVA T4	-	-
Wind measurement tools	Drahtlose Wetterstation	-	2157-45
flying tools	-	-	-



**Figure A.1:** The figure shows the microphone position versus the position of the line source



(a) The picture shows the speaker setup

(b) The figure shows the wind direction

**Figure A.2:** The figures shows the measurement set up for Appendix A and ??

## Test procedure

1. the microphone i calibrated.
2. The wind direction is measured.
3. The materials are set up as in Figure A.1 where the speaker is placed in cross wind direction, such that the frontal wave direction is orthogonal the the wind. The microphone and speaker is connected to the audio interface.
4. The speaker and microphone is placed 1.1 m above the ground
5. the wind direction goes from microphone 2 to microphone 1.
6. 10 sine sweep is performed with a length of 5 s each.
7. The impulse response is calculated and filtered with a 4th order highpass filter at 300 Hz to exclude wind noise.
8. The correlation is calculated for each impulse response to the first impulse response for time alignment [Gunness, 2001] of both microphone channel.

9. The mean impulse response is calculated for the 10 measurement of both microphone.
10. The transfer function is calculated with a 40 sample moving mean filter.
11. The measurement is repeated three times.
12. The measurement is repeated with an angle of  $74^\circ$  and a distance of 25 m for both microphone.

## Measurement area

To be able to measure in a windy area, the football stadium at Fredrick Alfred Nobels Vej 7, 9220 Aalborg is used. The following Figure A.3 shows a picture of the area and the approximate position of the speaker and microphone.

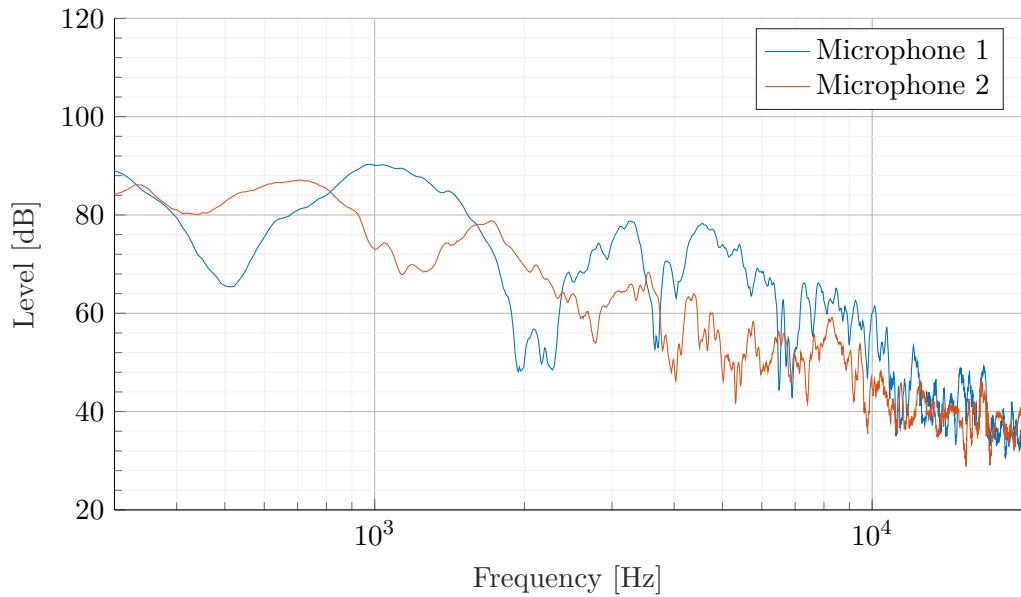


**Figure A.3:** The picture illustrate the area, where the wind flow is measured

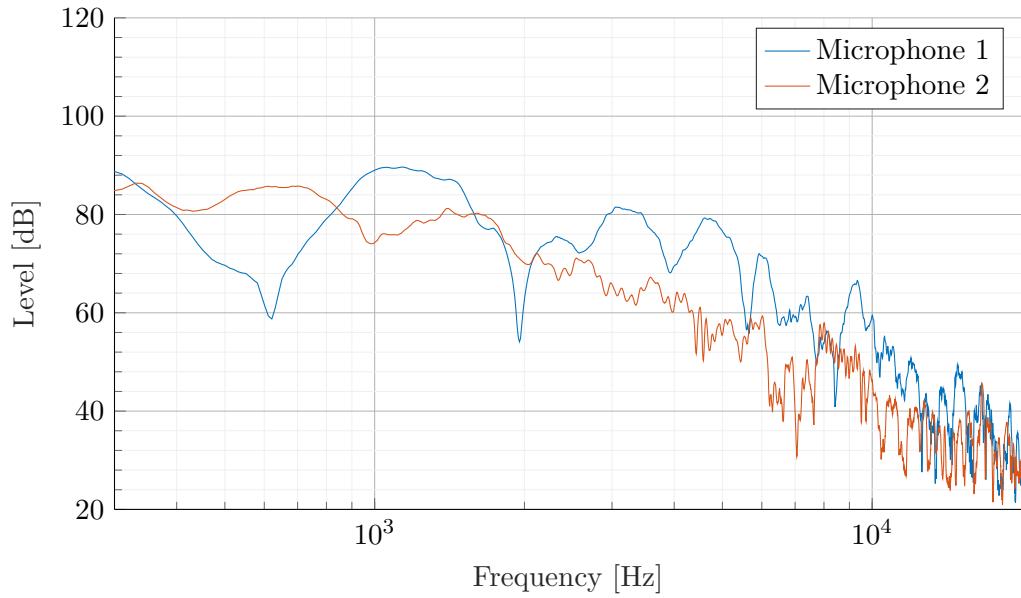
## Results

The wind speed was 14 m/s for each measurement and the temperature was  $5^\circ$ . The humidity was not measured.

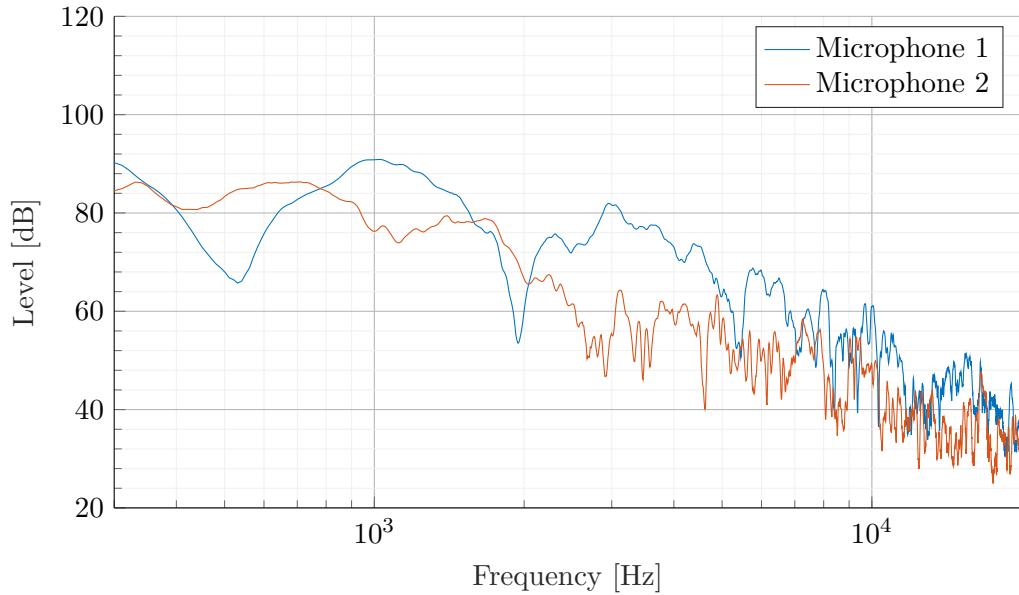
The following measurement shows the result for  $120^\circ$



**Figure A.4:** The graph shows the first transfer function measurement. The  $L_{eq,5}$  Sound Pressure Level (SPL) different between the microphones is 5.49 dB SPL (IR\_6)



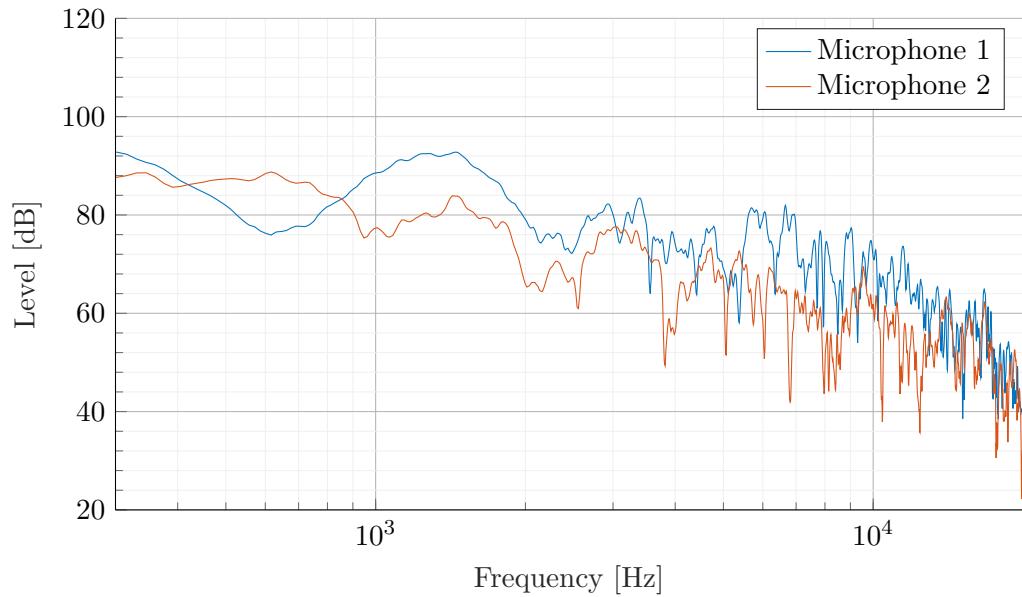
**Figure A.5:** The graph shows the second transfer function measurement. The  $L_{eq,5}$  SPL different between the microphones is 4.40 dB SPL (IR\_7)



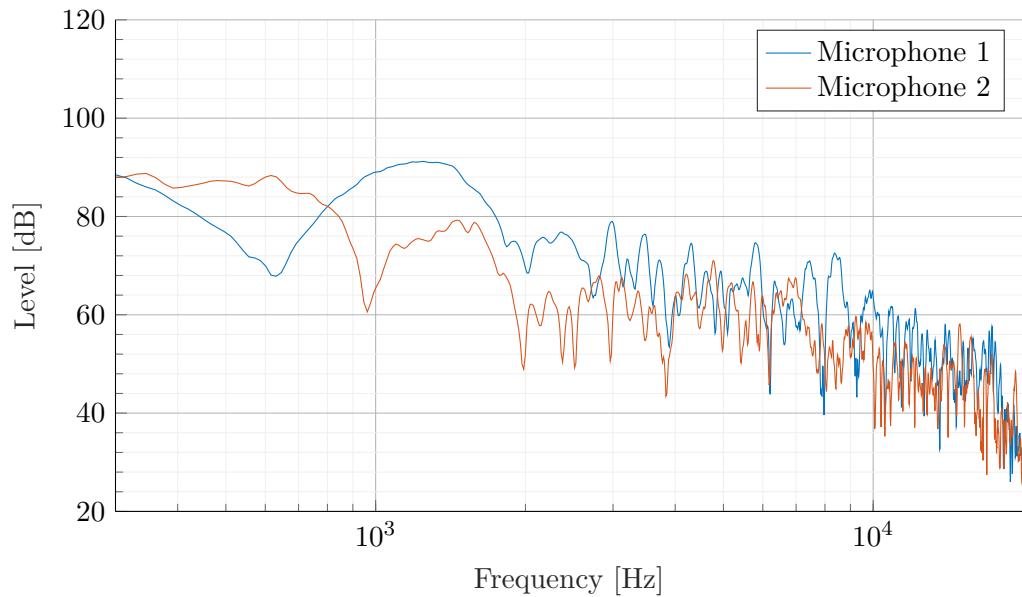
**Figure A.6:** The graph shows the third transfer function measurement. The  $L_{eq,5}$  SPL different between the microphones is 4.23 dB SPL (IR\_8)

On Figure A.4, Figure A.5 and Figure A.6 it is seen that the general pressure is higher for microphone 1. It is also seen that ground reflection effect is much higher on microphone 1 than microphone 2. This support the theory about upwards refraction of sound wave on microphone 2 and downwards refraction on microphone 1

The following measurement shows the result for 74°



**Figure A.7:** The graph shows the first transfer function measurement. The  $L_{eq,5}$  SPL different between the microphones is 4.41 dB SPL (IR\_3)



**Figure A.8:** The graph shows the second transfer function measurement. The  $L_{eq,5}$  SPL different between the microphones is 4.81 dB SPL (IR\_5)

On Figure A.7 and Figure A.8 it is seen that the general pressure is higher for microphone 1. It is also seen that ground reflection effect is much higher on microphone 1 than microphone 2. This support the theory about upwards refraction of sound wave on microphone 2 and downwards refraction on microphone 1

## **Summary**



## Appendix B

# Windscreen concept measurement

A measurement was made to measure the wind attenuation of difference windscreen configuration. All configuration include the GRAS AM0069 windscreen with an additionally wind stopper surface all around the microphone except of the frontal direction. The measurement is done as a preliminary test with low wind speed, to test the concept before a field test with wind speed as in the speaker measurement. The measurement is done to ensure that the measured wind does not overload the preamp of the microphone at the specified wind speed.

### Materials and setup

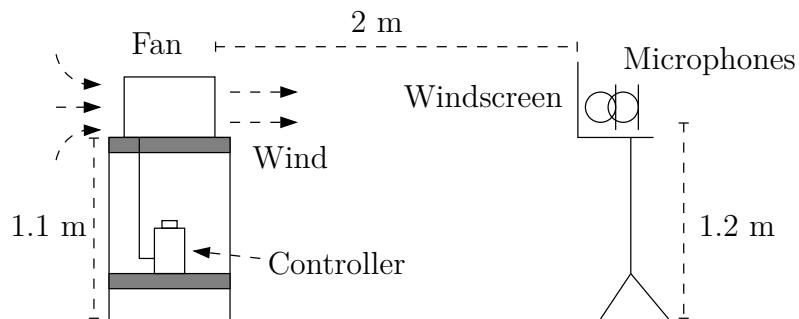
To measure the wind attenuation of the windscreen configuration the following materials are used:

**Table B.1:** Equipment list

Description	Model	Serial-no	AAU-no
PC	Macbook	W89242W966H	-
Audio interface	RME Fireface UCX	23811948	108230
Microphone	GRAS 26CC	78189	75583
Preamp	GRAS 40 AZ	100268	75551
Microphone	GRAS 26CC	78186	75582
Preamp	GRAS 40 AZ	100267	75550

**Table B.2:** Equipment list

Description	Model	Serial-no	AAU-no
Fan	IMPEGA	-	-
Fan	IMPEGA	-	-
Windscreen	GRAS AM0069	-	-
Windscreen	GRAS AM0069	-	-
large foam wedge	-	-	-
Small foam wedge	-	-	-
Rockwool bat	-	-	-



**Figure B.1:** The figure shows the measurement setup for the wind noise measurement in the microphone position and outside the windspeed sensor. The two microphone seems to lay onto each other but it shall show that one is inside the windspeed sensor and one is outside the windspeed sensor



**Figure B.2:** The picture shows the measurement set up

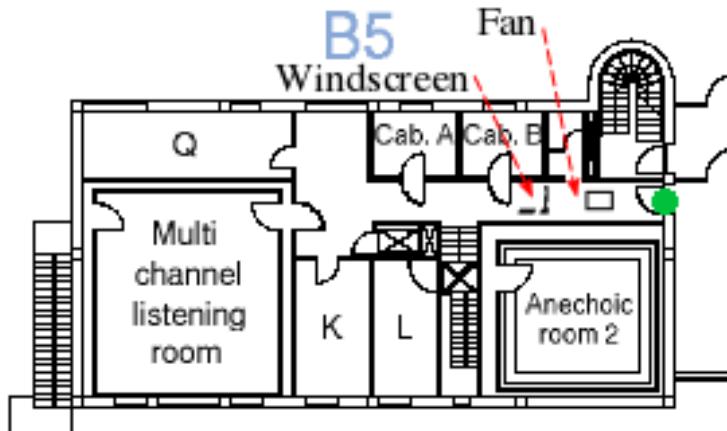
## Test procedure

1. The materials are set up as in Figure B.1 where the two microphone connected to the audio interface.

2. Both microphone is calibrated.
3. Both fan is activated
4. A 7s time signal is measured three times synchronise on both microphone.
5. The frequency content is calculated by **fft** on all six measured time signal.
6. The average of the frequency response for each microphone is calculated
7. The difference between the microphone is calculated to find the attenuation of the windscreens configuration
8. The procedure is done for all windscreens configuration and one where no additionally wind stopper is added around the microphone. This last configuration is defined as reference configuration.
9. A no wind measurement is measured the same way just without the fan activated and only with GRAS AM0069 windscreens in the end.
10. The wind speed is measured.

## Measurement area

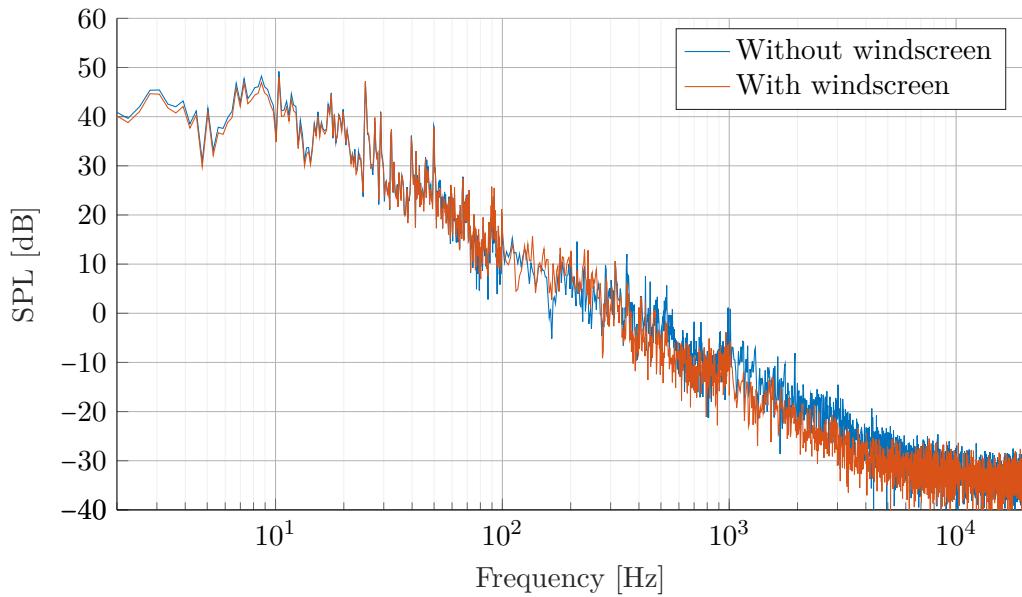
To be able to generate a controlled wind flow, the hall way in Fredrick Bajers vej 7B5, 9200 Aalborg is used. The following Figure B.3 shows a drawing of the area and the position of the fan and windscreens.



**Figure B.3:** The picture illustrate the area, where the wind flow is measured

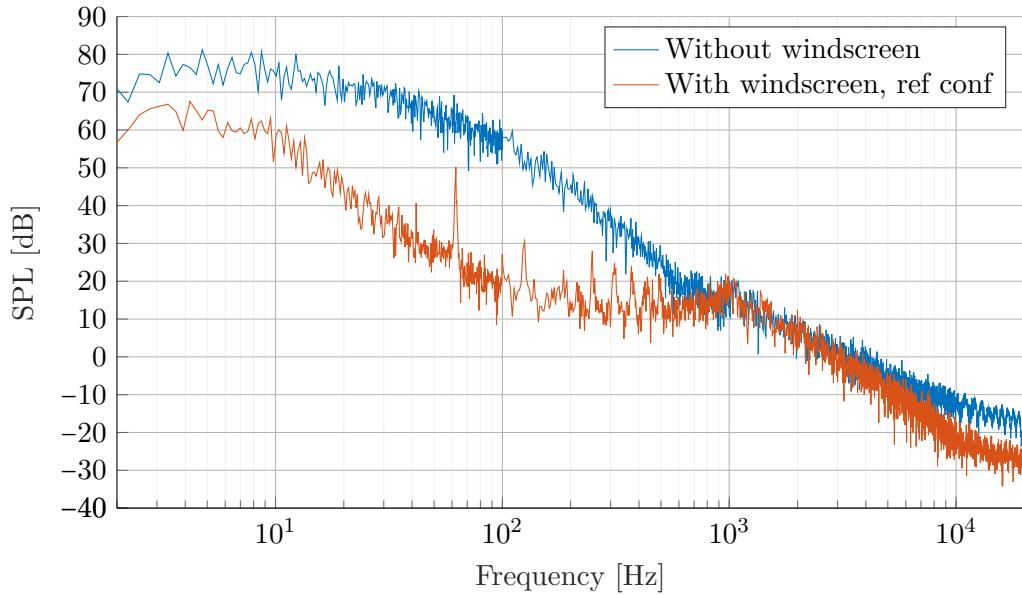
## Results

The following graphs shows the result of the measurement. The wind speed is measured to be 2.5 m/s.



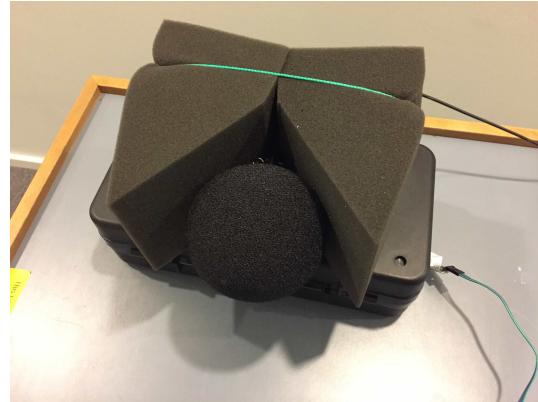
**Figure B.4:** The graph shows the frequency content without the fan activated

The Figure B.4 shows the frequency content in the measuring area without the fan activated for both microphone and the reference windscreen configuration.

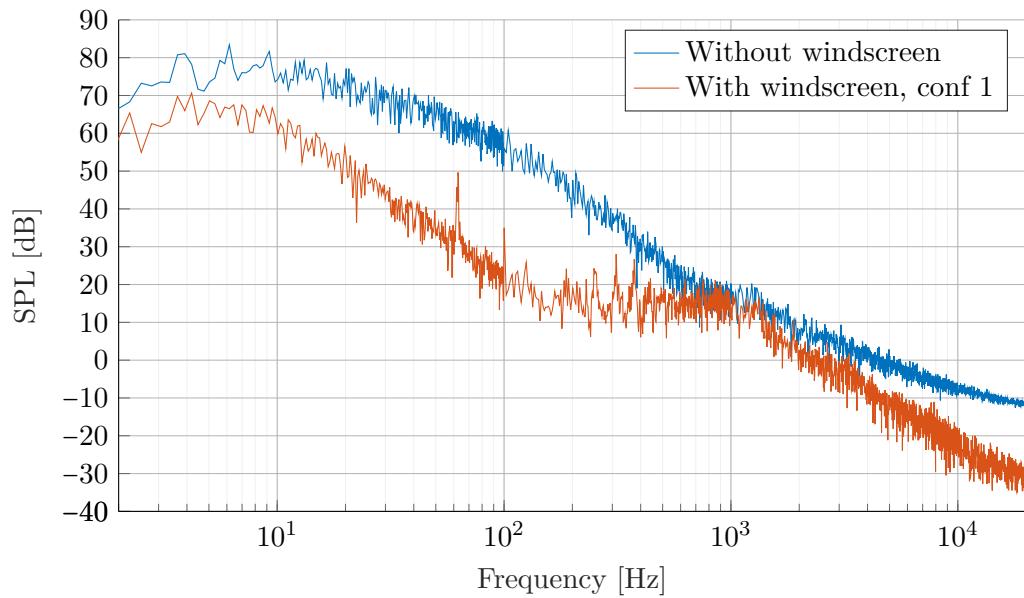


**Figure B.5:** The graph shows the frequency content with the fan activated

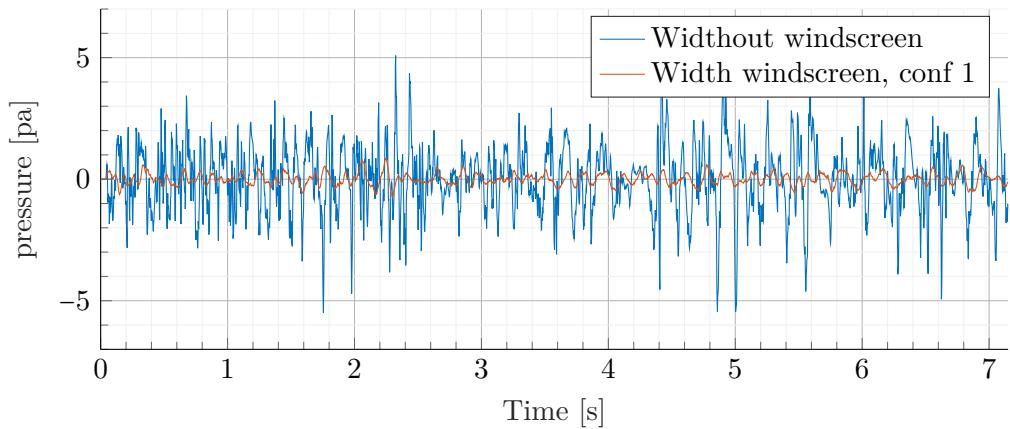
The Figure B.5 shows the frequency content in the measuring area with the fan activated for both microphone and the reference windscreens configuration. It is seen that the highest attenuation is at 900 Hz but the general attenuation is



**Figure B.6:** The picture shows the microphone covered with windscreens and the Small foam wedge windscreens configuration. This configuration is defined as configuration one

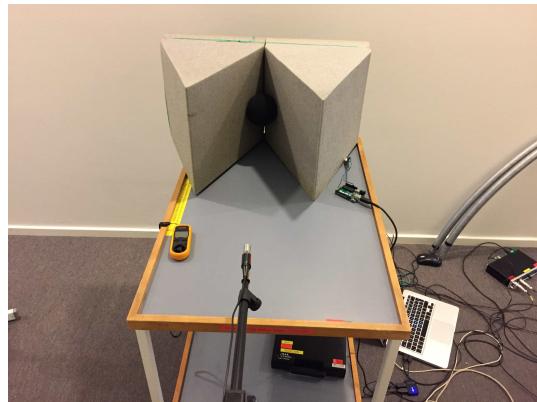


**Figure B.7:** The graph shows the frequency content of the measurement with configuration one

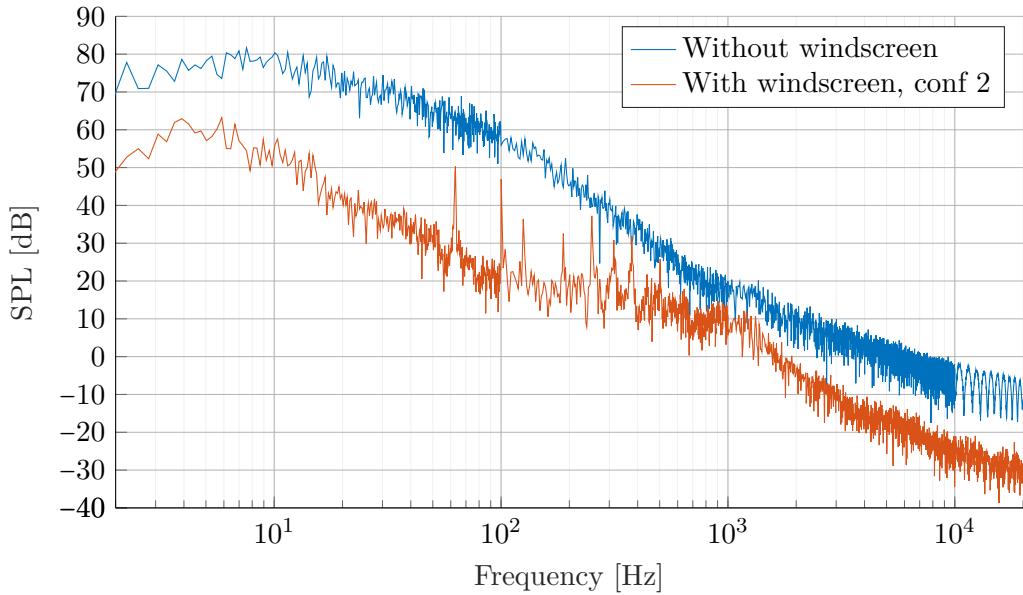


**Figure B.8:** The graph shows one of the time measurement with configuration one

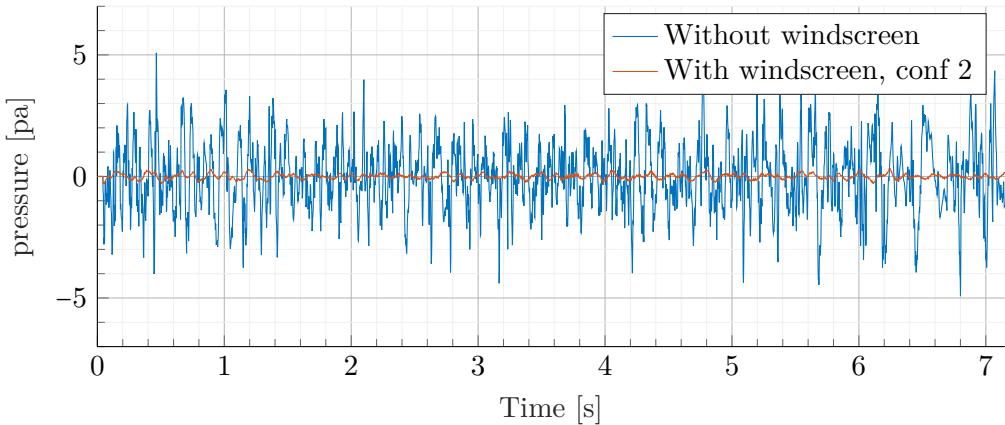
The Figure B.7 and Figure B.8 shows the measurement with configuration one in frequency and time domain respectively. It can be seen that the general windscreen attenuation is not lowered compared to the reference windscreen measurement.



**Figure B.9:** The picture shows the microphone covered with windscreen and the large foam wedge windscreen. This configuration is defined as configuration two.

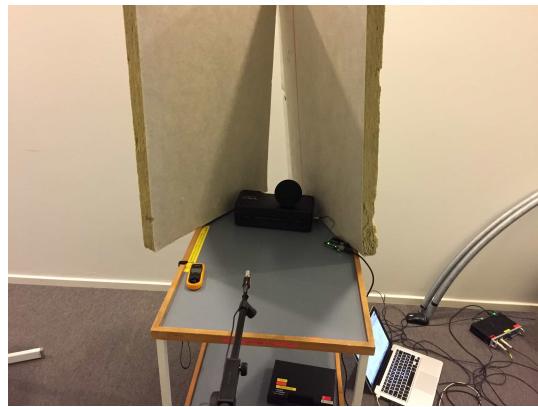


**Figure B.10:** The graph shows the frequency content of the measurement with configuration two

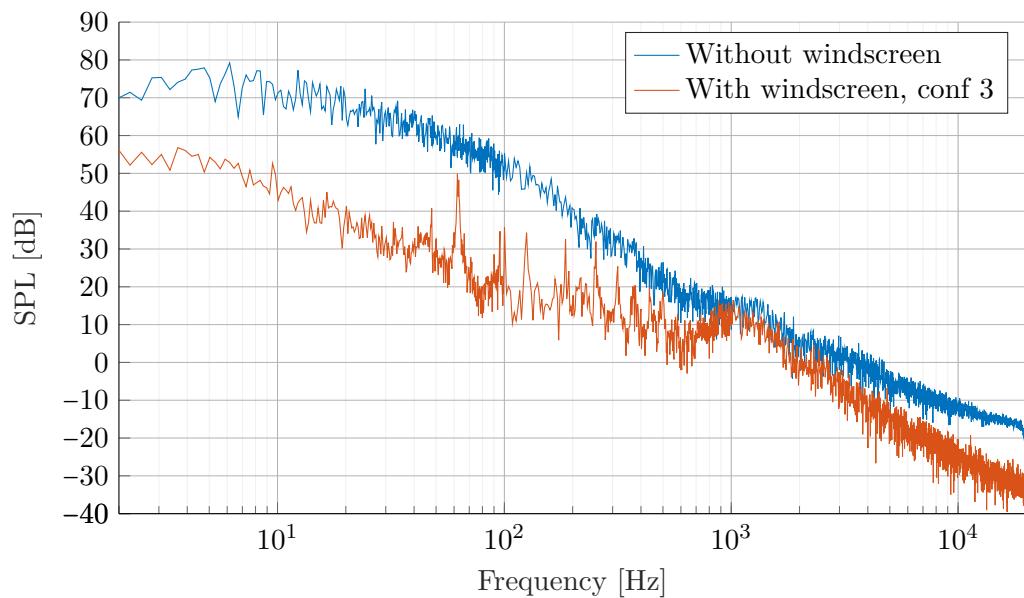


**Figure B.11:** The graph shows one of the time measurement with configuration two

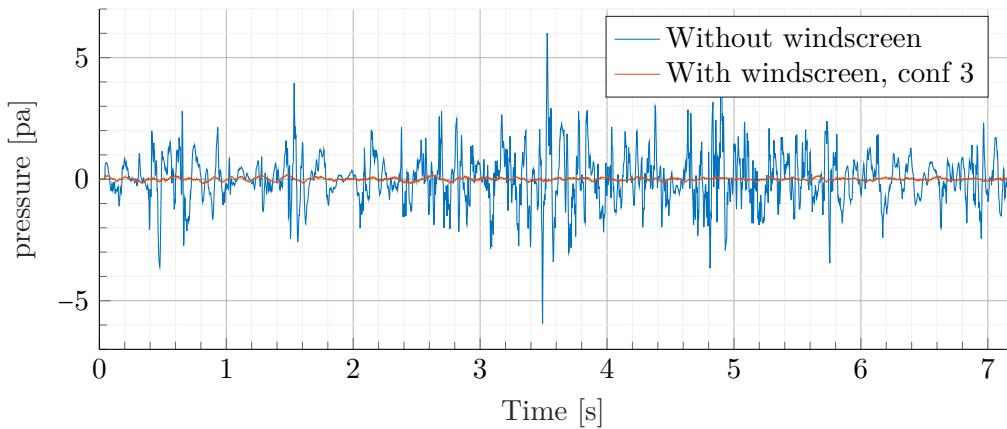
The Figure B.10 and Figure B.11 shows the measurement with configuration two in frequency and time domain respectively. The measurement shows that the windscreens attenuation does have an effect compare to the reference windscreen measurement. The attenuation is nearly greater for all frequency especially in the low and high frequency range.



**Figure B.12:** The picture shows the microphone covered with windscreens and the rockwool wind stopper. This configuration is defined as configuration three.



**Figure B.13:** The graph shows the frequency content of the measurement with configuration three



**Figure B.14:** The graph shows one of the time measurement with configuration three

The Figure B.13 and Figure B.14 shows the measurement with configuration three in frequency and time domain respectively. The measurement shows that the windscreen attenuation does have an effect compare to the reference windscreen measurement but the attenuation is not as good as in configuration two. There is better attenuation in the low frequency compare to the reference windscreen measurement but in the high frequency the attenuation is worse than the reference windscreen measurement, that might be due to reflection on the surface of the rockwool filter.

## Summary

It is shown that the additionally wind stopper hypotheses does attenuate the wind noise at a wind speed of 2.5 m/s



## Appendix C

# Windscreen attenuation measurement

A measurement was made to measure the frequency attenuation of difference windscreen configuration. All configuration include the GRAS AM0069 windscreen with an additionally wind stopper surface all around the microphone except of the frontal direction. The measurement is done in the anechoic chamber. The measurement is done to analyse the effect of the windscreen in the frequency domain to ensure that the chosen windscreen do not add to much reflect to the measurement. The optimal criteria is therefore as low difference as possible.

## Materials and setup

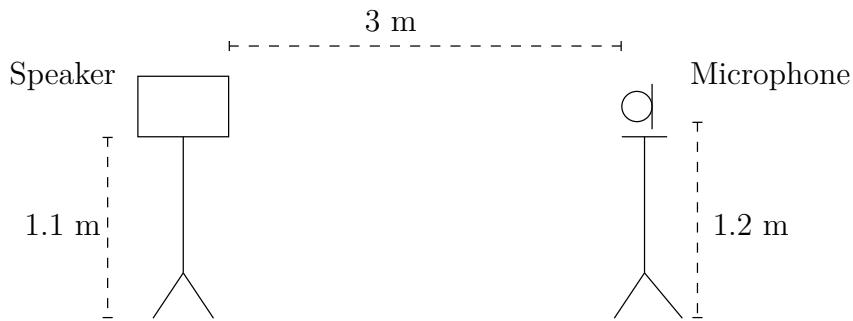
To measure the frequency response of the windscreen configuration the following materials are used:

**Table C.1:** Equipment list

Description	Model	Serial-no	AAU-no
PC	Macbook	W89242W966H	-
Audio interface	RME Fireface UCX	23811948	108230
Microphone	GRAS 26CC	78189	75583
Preamp	GRAS 40 AZ	100268	75551
Windscreen	GRAS AM0069	-	-
large foam wedge	-	-	-
Small foam wedge	-	-	-
Rockwool bat	-	-	-

**Table C.2:** Equipment list

Description	Model	Serial-no	AAU-no
Speaker stand	-	-	-
Speaker stand	-	-	-
Speaker	Dynaudio	03508438	1441-0

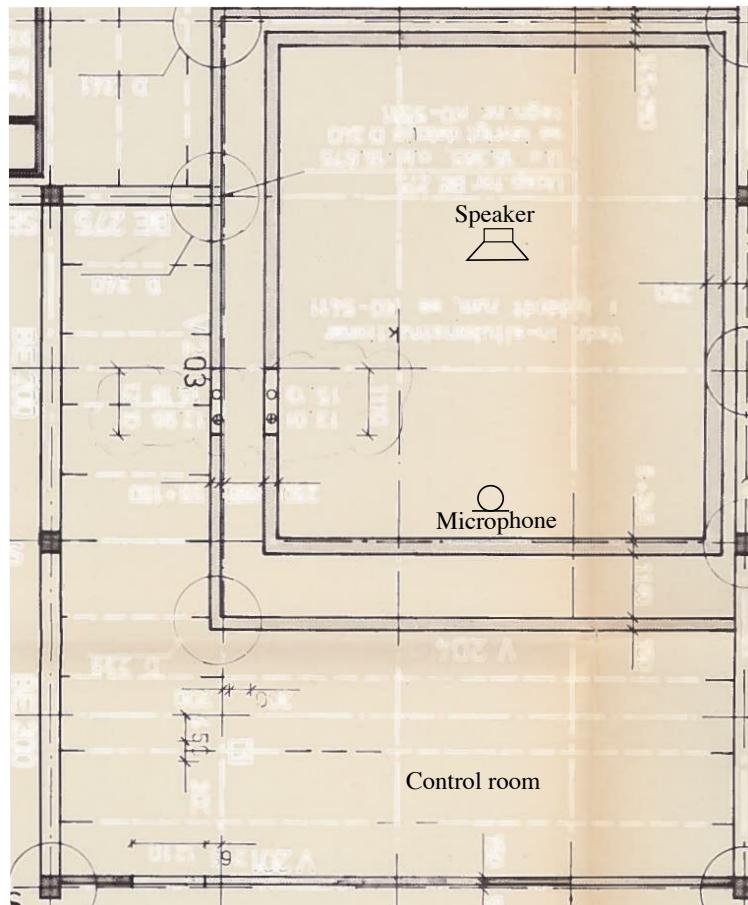
**Figure C.1:** The figure shows the measurement setup in the anechoic chamber

## Test procedure

1. The materials are set up as in Figure C.1 where the microphone is connected to the audio interface.
2. The microphone is calibrated
3. The speaker is placed 3 m from the microphone and pointing in the direction of the microphone.
4. The windscreens configuration is placed such that the microphone have approximately the same position as without the windscreens.
5. The transfer function is measured
6. The procedure is started over until all windscreens are measured.
7. The transfer function is calculated and plotted versus the transfer function without windscreens MATLAB®.
8. The difference between the transfer function with and without windscreens is calculated and plotted in MATLAB®.

## Measurement area

To be able to measure the windscreens frequency response, the anechoic chamber in Fredrick Bajers vej 7B4, 9220 Aalborg is used. The following Figure C.2 shows a drawing of the area and the position of the fan and windscreens.



**Figure C.2:** The picture illustrate the area, where the wind flow is measured

## Results

The following Figure C.3 shows the speaker.



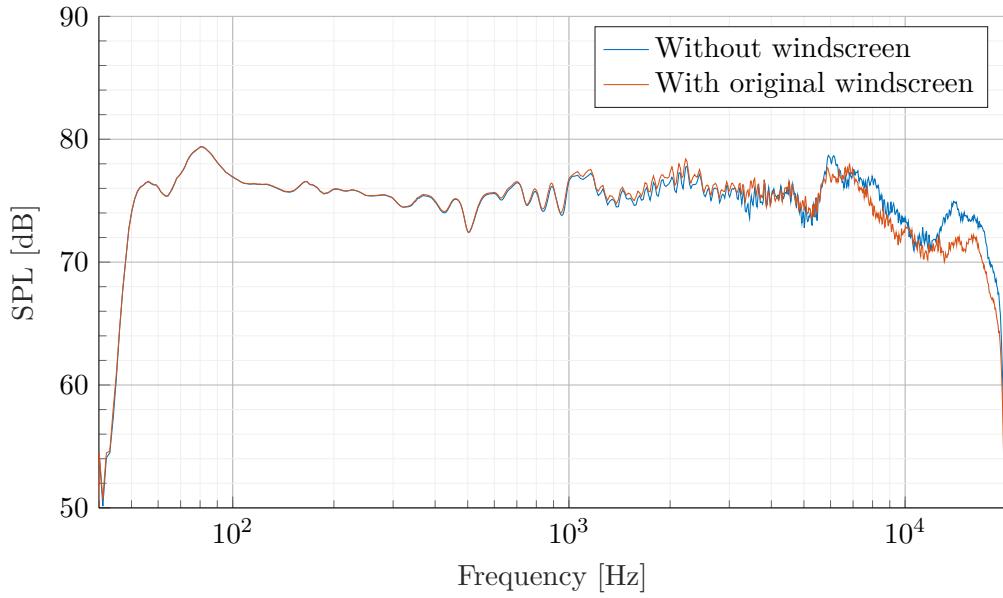
**Figure C.3:** The picture shows the used speaker

The following graphs shows the result of the measurement.



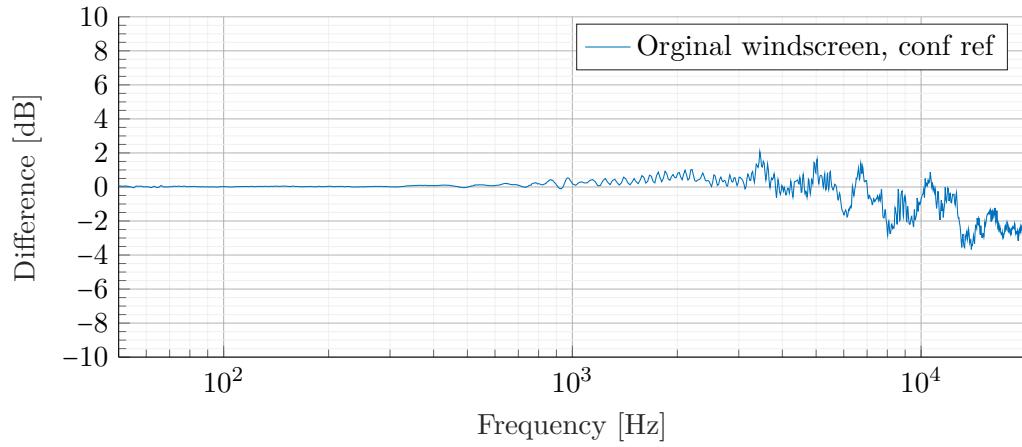
**Figure C.4:** The picture shows the measurement microphone with the original windscreen

The measurement shown in Figure C.5 shows frequency response of the speaker with and without the windscreens. The Figure C.4 shows the microphone position with the windscreens. The position is not changed for the measurement without windscreens.



**Figure C.5:** The graph shows frequency response of the speaker measured without windscreen and with the original windscreen

The measurement shown in Figure C.6 shows the difference SPL between the measurement with and without original windscreen.

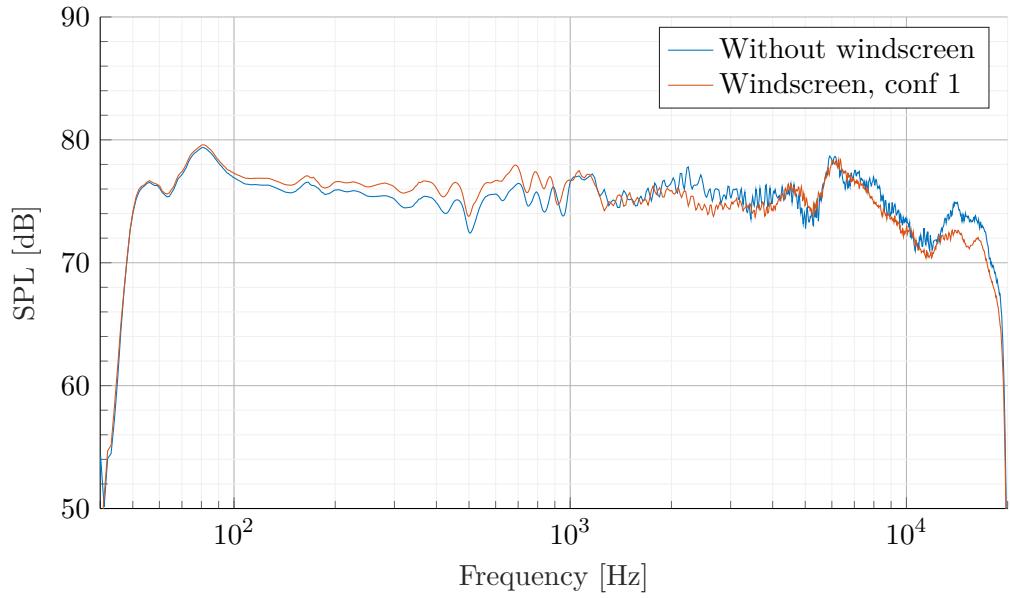


**Figure C.6:** The graph shows frequency response of the windscreen, where the frequency characteristic for the speaker is out calculated.

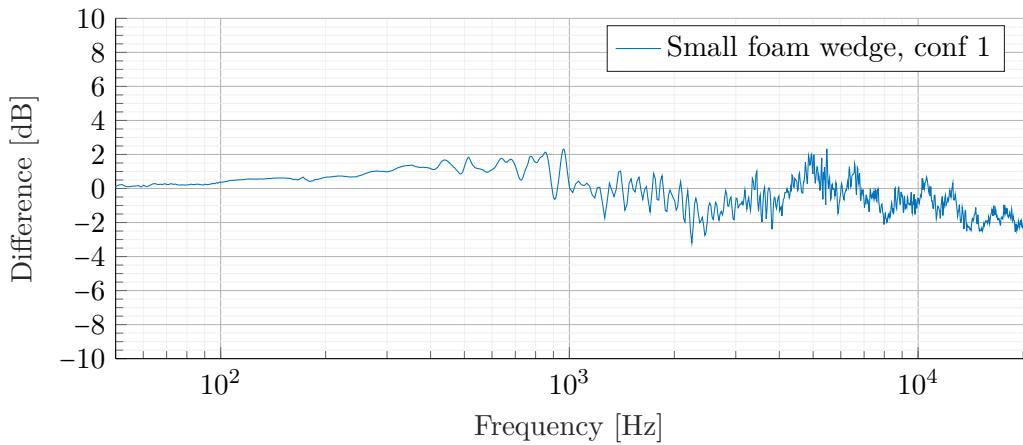


**Figure C.7:** The picture shows the measurement microphone with the large foam wedge configuration two

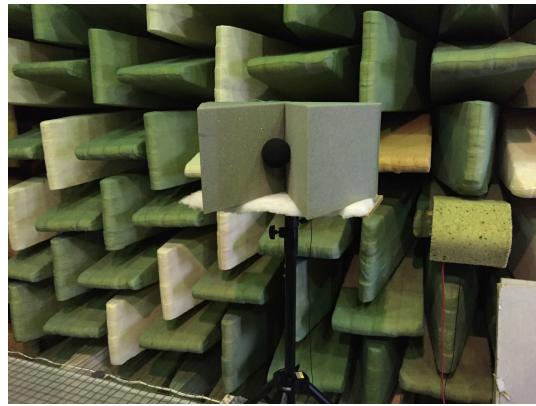
The measurement shown in Figure C.8 shows frequency response of the speaker without the windscreens and with the windscreens configuration one. The Figure C.7 shows the measured set up.



**Figure C.8:** The graph shows frequency response of the speaker measured without windscreens and with windscreens configuration one

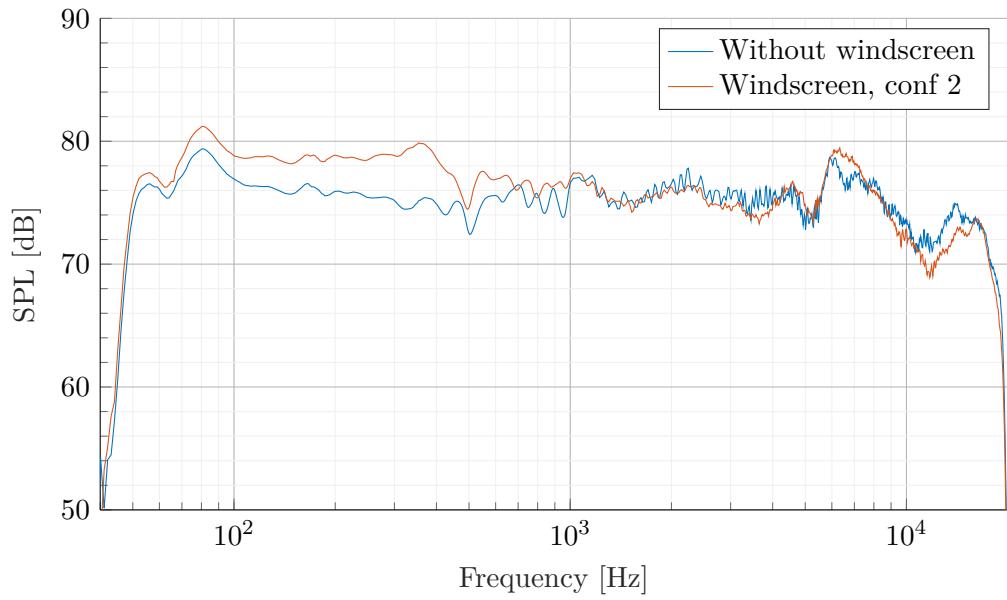


**Figure C.9:** The graph shows frequency response of the windscreen, where the frequency characteristic for the speaker is out calculated.

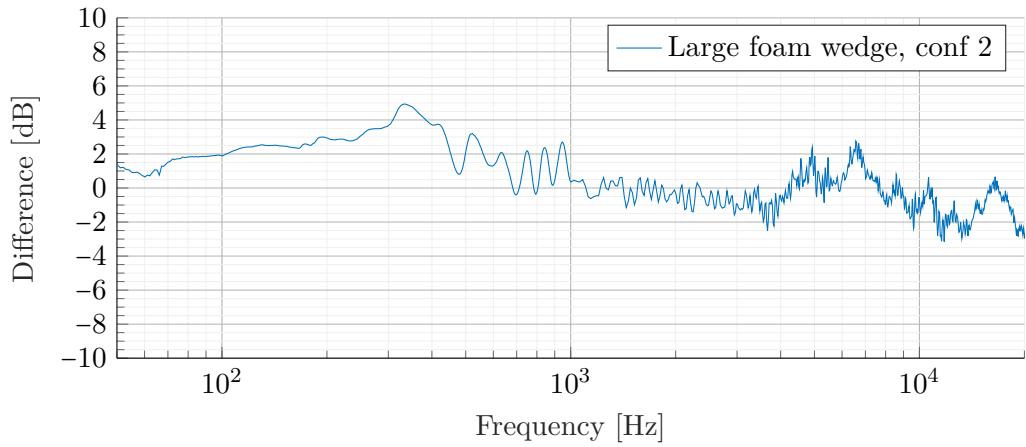


**Figure C.10:** The picture shows the measurement microphone with the large foam wedge configuration two

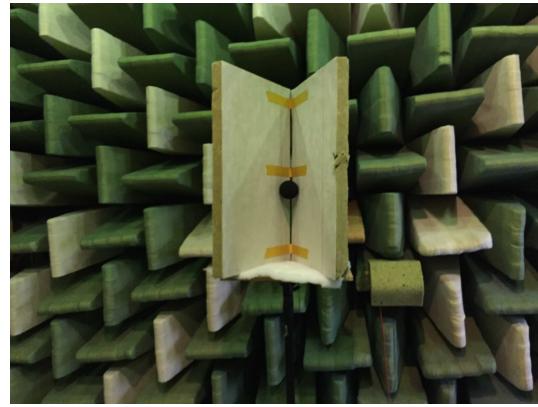
The measurement shown in Figure C.11 shows frequency response of the speaker without the windscreens and with the windscreens configuration two. The Figure C.10 shows the measured set up.



**Figure C.11:** The graph shows frequency response of the speaker measured without windscreen and with windscreen configuration two

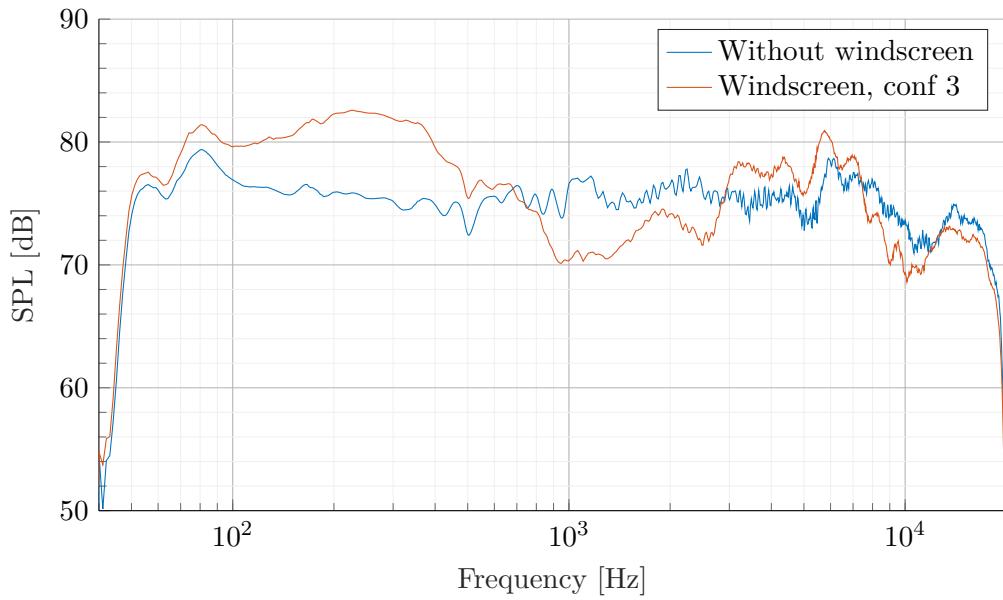


**Figure C.12:** The graph shows frequency response of the windscreen, where the frequency characteristic for the speaker is out calculated.

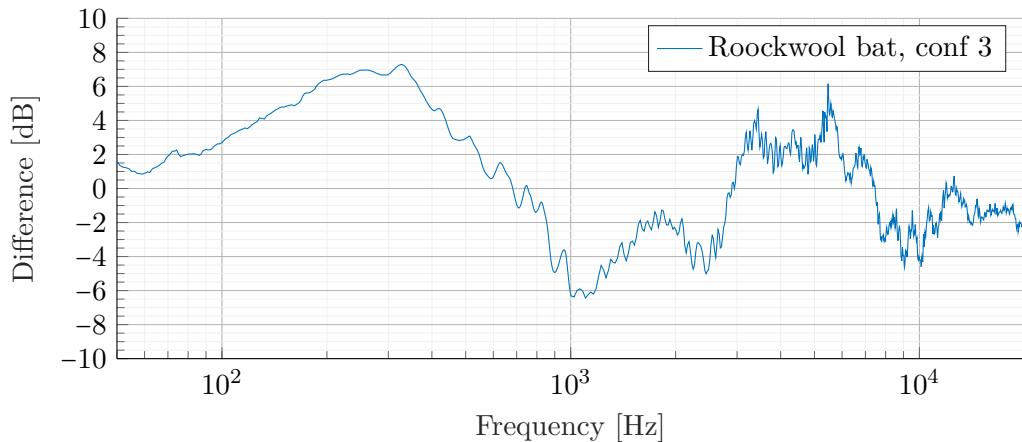


**Figure C.13:** The picture shows the measurement microphone with the rockwool bat configuration three

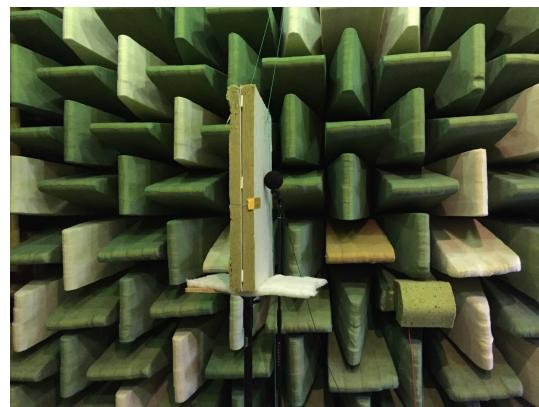
The measurement shown in Figure C.14 shows frequency response of the speaker without the windscreens and with the windscreens configuration three. The Figure C.13 shows the measured set up. In this measurement both the speaker and the microphone is lifted 20 cm



**Figure C.14:** The graph shows frequency response of the speaker measured without windscreens and with windscreens configuration three

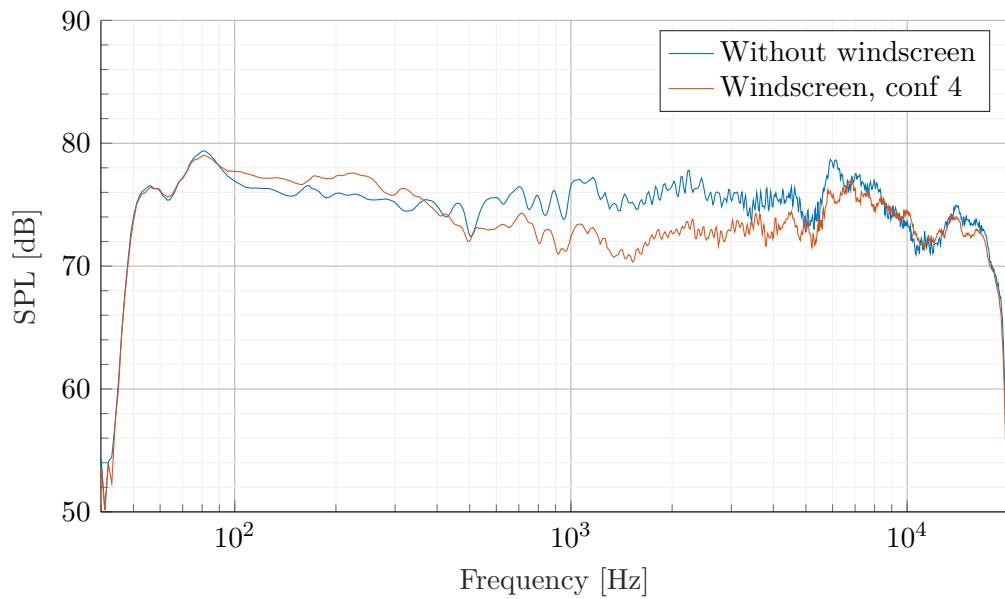


**Figure C.15:** The graph shows frequency response of the windscreens, where the frequency characteristic for the speaker is out calculated.

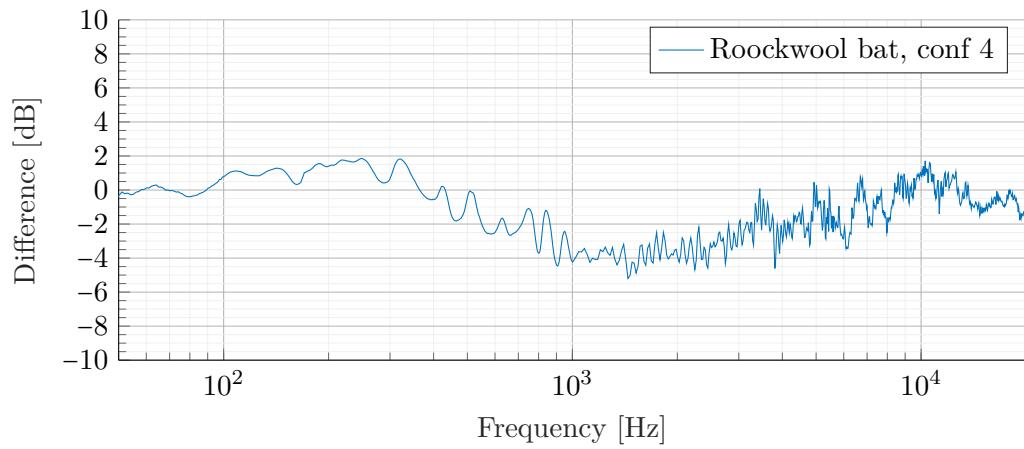


**Figure C.16:** The picture shows the measurement microphone with the rockwool bat configuration four

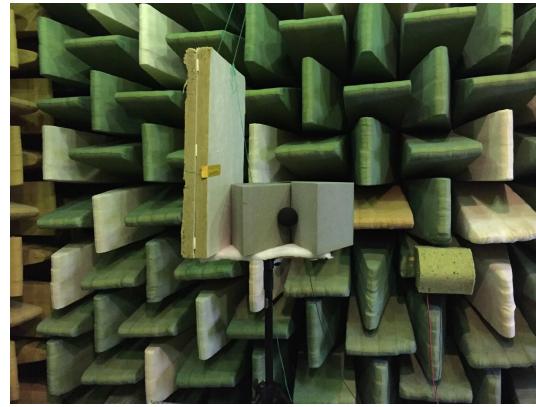
The measurement shown in Figure C.17 shows frequency response of the speaker without the windscreens and with the windscreens configuration four. The Figure C.16 shows the measured set up. In this measurement both the speaker and the microphone is lifted 30 cm



**Figure C.17:** The graph shows frequency response of the speaker measured without windscreen and with windscreen configuration four

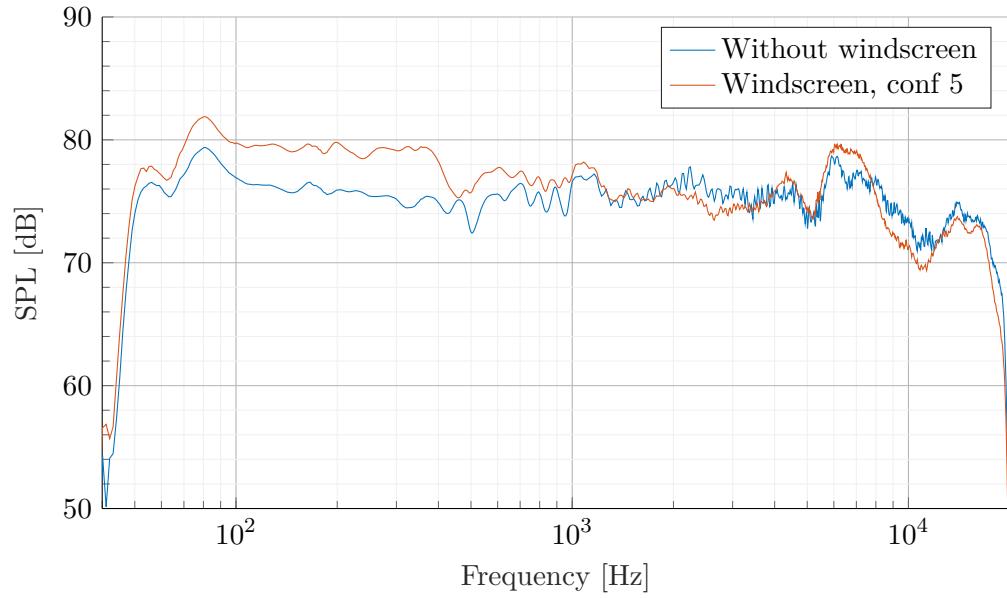


**Figure C.18:** The graph shows frequency response of the windscreen, where the frequency characteristic for the speaker is out calculated.

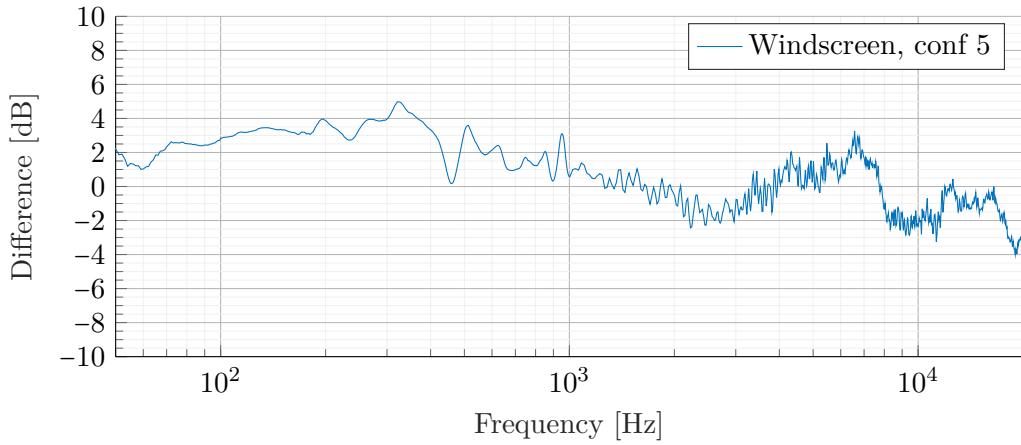


**Figure C.19:** The picture shows the measurement microphone with the rockwool bat configuration four

The measurement shown in Figure C.20 shows frequency response of the speaker without the windscreen and with the windscreen configuration four. The Figure C.19 shows the measured set up.



**Figure C.20:** The graph shows frequency response of the speaker measured without windscreen and with windscreen configuration five



**Figure C.21:** The graph shows frequency response of the windscreen, where the frequency characteristic for the speaker is out calculated.

## Summary

It is seen in the graph that all windscreen configuration change the frequency response of the microphone, even with only the original windscreen. Without taking the reference configuration intro account, the one with the lowest frequency change in the low frequency response is configuration one and four. The one with the lowest frequency change in the middle frequency is configuration one and two. The one with lowest frequency change in the high frequency is configuration four. The mix between configuration two and four shows a low frequency change in the middle and high frequency.



## Appendix D

# Windscreen attenuation measurement

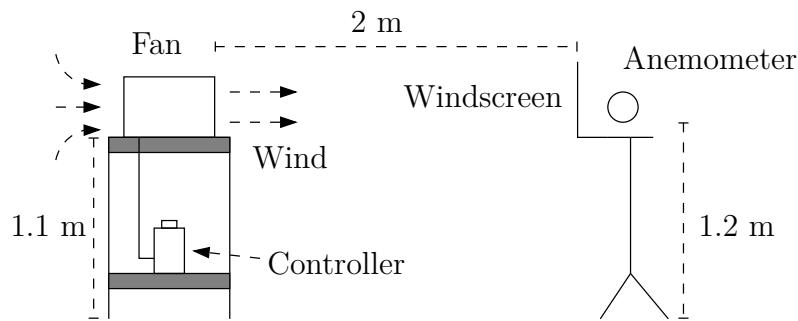
A measurement was made to measure the wind attenuation in the microphone position with the difference windscreen configuration.

### Materials and setup

To measure the wind attenuation of the windscreen configuration the following materials are used:

**Table D.1:** Equipment list

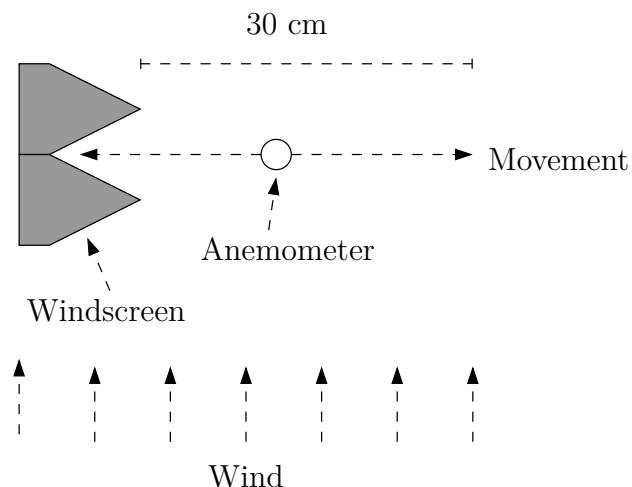
Description	Model	Serial-no	AAU-no
PC	Macbook	W89242W966H	-
large foam wedge	-	-	-
Small foam wedge	-	-	-
Rockwool bat	-	-	-
Fast fan	-	-	-
Fan control	transformator	-	60398
Windspeed tools	FT technologies FT742-D-SM	9002-922	105634



**Figure D.1:** The figure shows the measurement setup for the wind speed measurement in the microphone position

## Test procedure

1. The materials are set up as in Figure D.1.
2. The fan is placed such that it produces crosswind.
3. The fan is activated.
4. The anemometer is activated to record.
5. The anemometer is placed in the wind for approximately 10 s.
6. Then the anemometer is moved into the microphone position for approximately 10 s.
7. Then the anemometer is moved back in the wind for approximately 10 s.
8. Then the anemometer is moved into the microphone position for approximately 10 s again.
9. The wind speed measurement is plotted in MATLAB® with a moving mean filter with 2 sample and as m/s versus s.
10. Next the wind direction measurement is plotted in MATLAB® with a moving mean filter with 2 sample and as ° versus s.
11. The measurement is done for all windscreen configuration the same way.



**Figure D.2:** The figure shows the movement of the anemometer doing the measurement

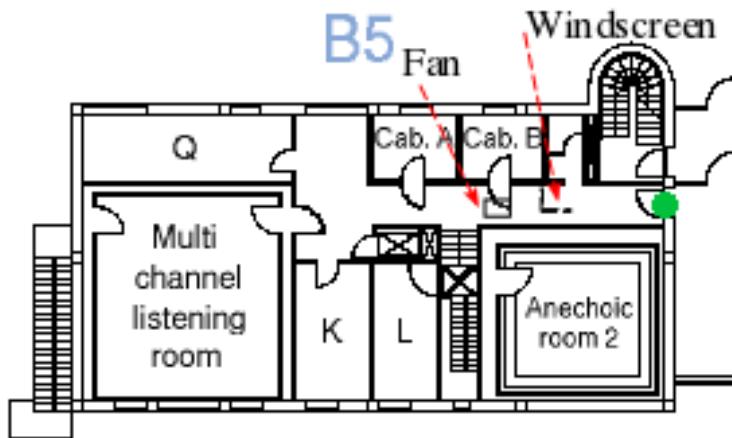
The following Figure D.3 shows the anemometer used for the measurement.



**Figure D.3:** The picture shows anemometer used for the measurement

## Measurement area

To be able to generate a controlled wind flow, the hall way in Fredrick Bajers vej 7B5, 9220 Aalborg is used. The following Figure B.3 shows a drawing of the area and the position of the fan and windscreens.



**Figure D.4:** The picture illustrate the area, where the wind flow is measured

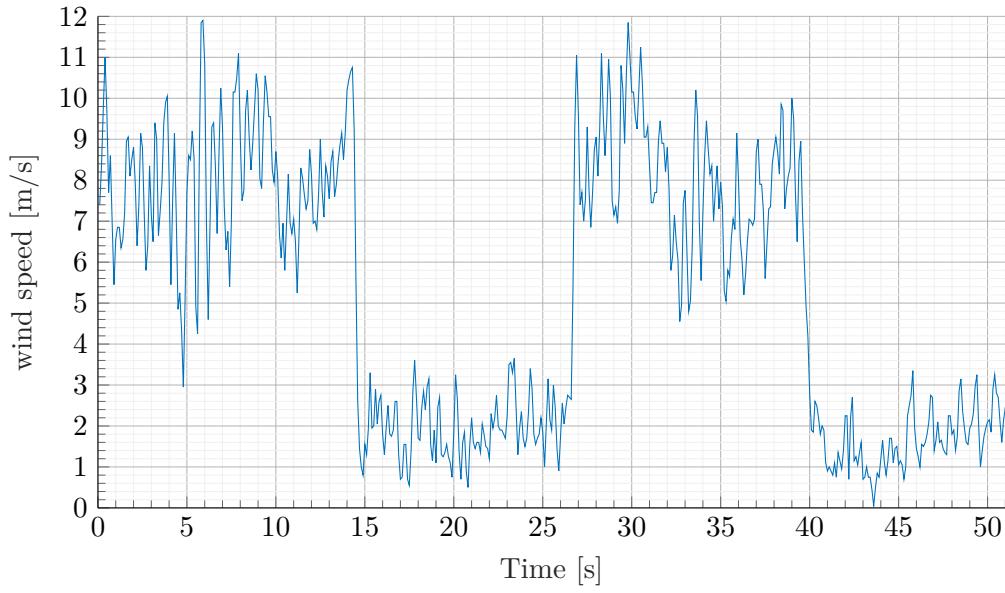
## Results

The following graphs shows the result of the measurement.

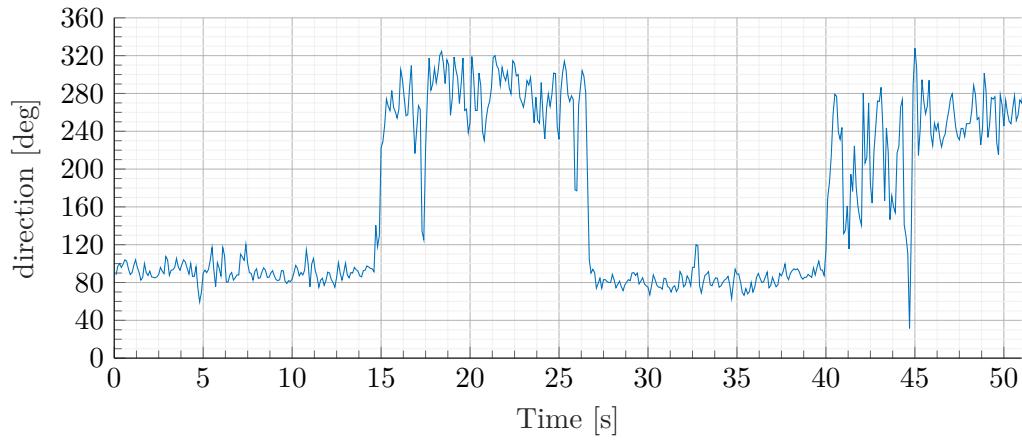
Figure D.5 shows the measurement setup of the foam wedge, where the Figure D.6 shows the result.



**Figure D.5:** The picture shows the measurement setup with the small wedge, configuration one



**Figure D.6:** The graph shows the wind speed versus time for configuration one. The grape have a high speed period and a low speed period, in the high speed period, the anemometer is in the wind approximately 30 cm from the windscreens where in the low speed period, the anemometer is inside the windscreens.

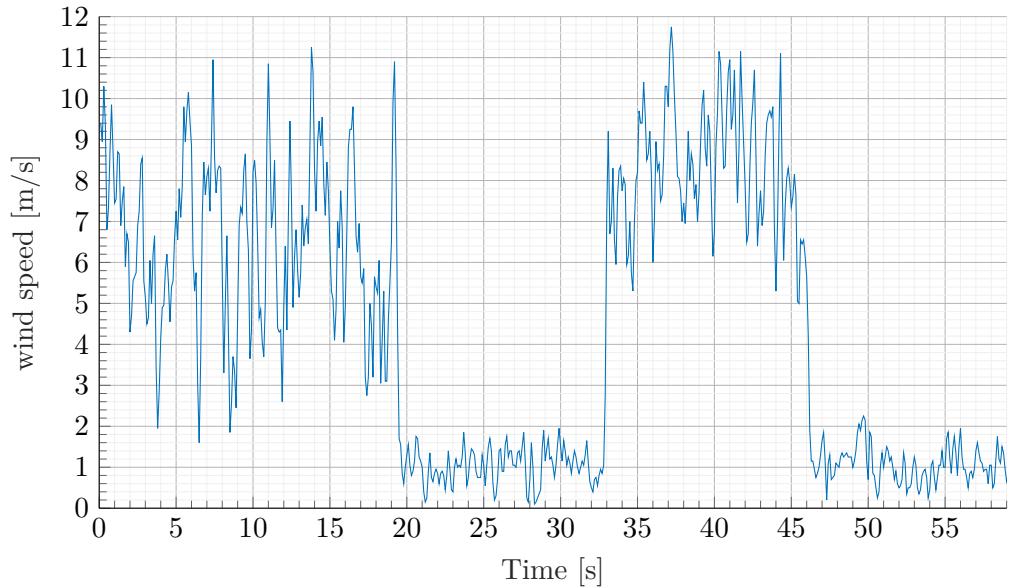


**Figure D.7:** The graph shows the synchronous direction of the wind with respect to the wind speed in Figure D.6

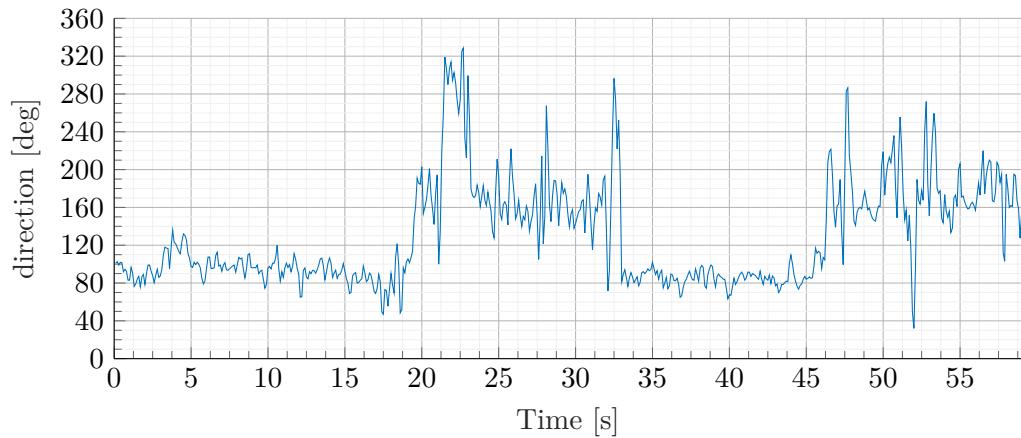
It is seen in Figure D.6 that the wind speed is lowered from approximately 8 m/s to 2 m/s. It is seen in Figure D.7 that the windscreens produce turbulence in the windscreens and the direction of the wind change approximately  $180^\circ$ .



**Figure D.8:** The picture shows the measurement setup for the large wedge, configuration two



**Figure D.9:** The graph shows the wind speed versus time for configuration two. The grape have a high speed period and a low speed period, in the high speed period, the anemometer is in the wind approximately 30 cm from the windscreens where in the low speed period, the anemometer is inside the windscreens.

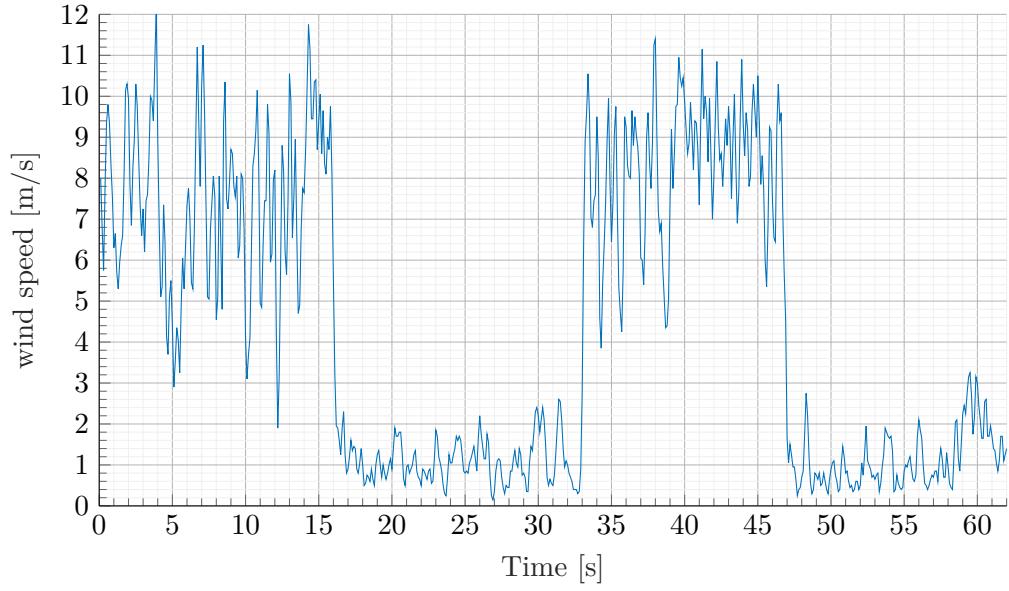


**Figure D.10:** The graph shows the synchronous direction of the wind with respect to the wind speed in Figure D.9

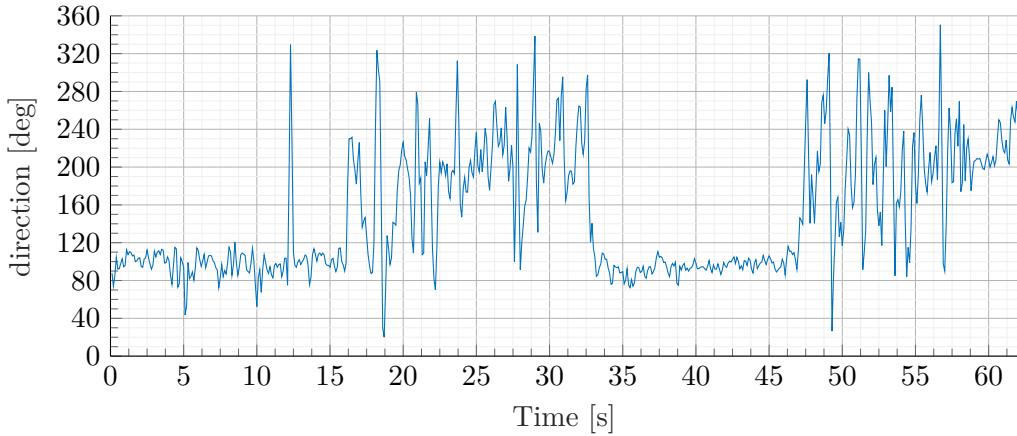
It is seen in Figure D.9 that the wind speed is lowered from approximately 7.5 m/s to 1 m/s. It is seen in Figure D.10 that the windspeed produces turbulence as high as with the small foam wedge in the windspeed and the direction of the wind changes approximately 70°.



**Figure D.11:** The picture shows the measurement setup for the single rockwool bat, configuration four



**Figure D.12:** The graph shows the wind speed versus time for configuration four. The grape have a high speed period and a low speed period, in the high speed period, the anemometer is in the wind approximately 30 cm from the windscreens where in the low speed period, the anemometer is inside the windscreens.



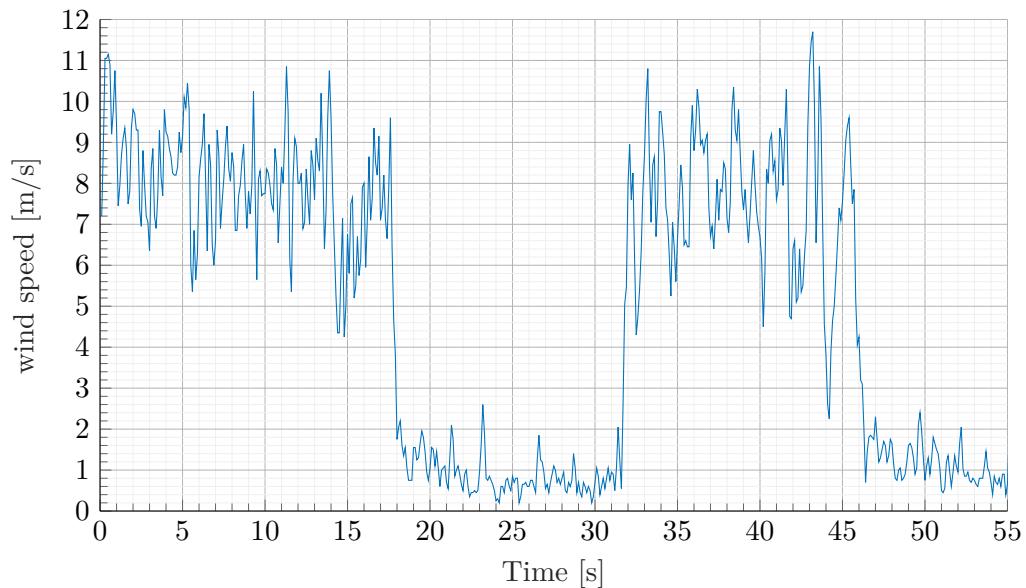
**Figure D.13:** The graph shows the synchronous direction of the wind with respect to the wind speed in Figure D.12

It is seen in Figure D.12 that the wind speed is lowered from approximately 8 m/s to 1 m/s. It is seen in Figure D.13 that the windscreens produce higher tur-

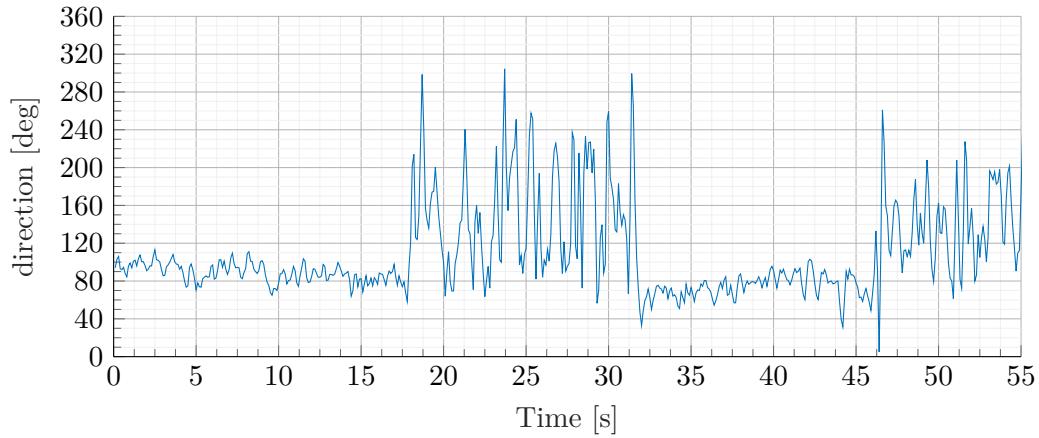
bulence compare to the foam wedge windscreens. The direction of the wind change is approximately  $100^\circ$ .



**Figure D.14:** The picture shows the measurement with the large wedge and single rockwool bat, configuration five.



**Figure D.15:** The graph shows the wind speed versus time for configuration five. The graph have a high speed period and a low speed period, in the high speed period, the anemometer is in the wind approximately 30 cm from the windscreens where in the low speed period, the anemometer is inside the windscreens.



**Figure D.16:** The graph shows the synchronous direction of the wind with respect to the wind speed in Figure D.15

It is seen in Figure D.15 that the wind speed is lowered from approximately 8 m/s to 0.8 m/s. It is seen in Figure D.16 that this windscreens produces the highest turbulence of all windscreens. The direction of the wind change approximately 60°.

## Summary

It is measured that all windscreens configuration lower the wind speed in the microphone position. The lowest attenuation of the wind is of the small foam wedge where the highest wind speed attenuation is attained by configuration five. Generally all windscreens yield turbulence wind direction, but the single rockwool bat configuration four seems to be the worst with respect to directional turbulence.

## Appendix E

# Windscreen attenuation measurement

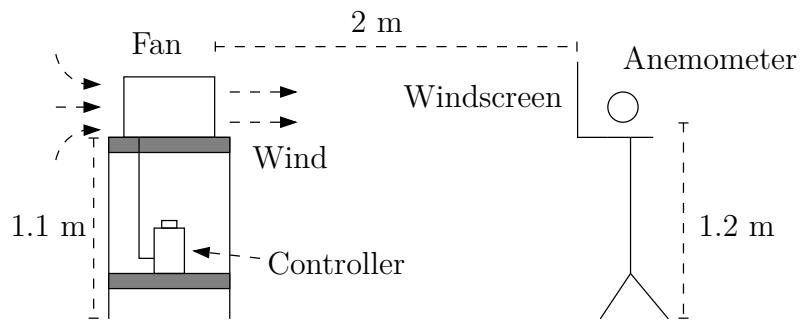
A measurement was made to measure the wind attenuation in the microphone position with the difference windscreen configuration.

### Materials and setup

To measure the wind attenuation of the windscreen configuration the following materials are used:

**Table E.1:** Equipment list

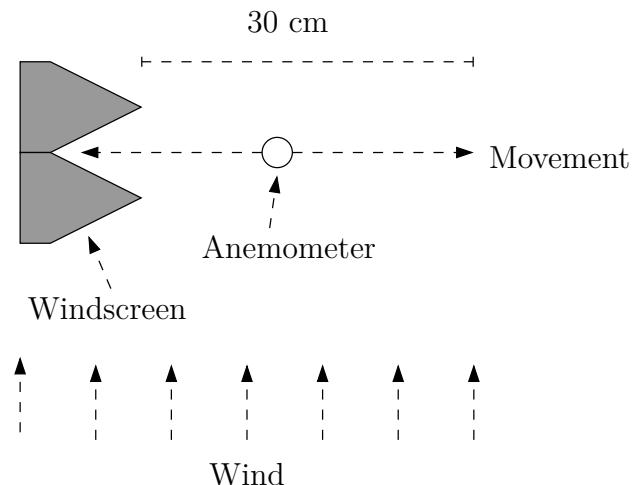
Description	Model	Serial-no	AAU-no
PC	Macbook	W89242W966H	-
Optimised windscreen	-	-	-
Fast fan	-	-	-
Fan control	tranformator	-	60398
Windspeed tools	FT technologies FT742-D-SM	9002-922	105634



**Figure E.1:** The figure shows the measurement setup for the wind speed measurement in the microphone position

## Test procedure

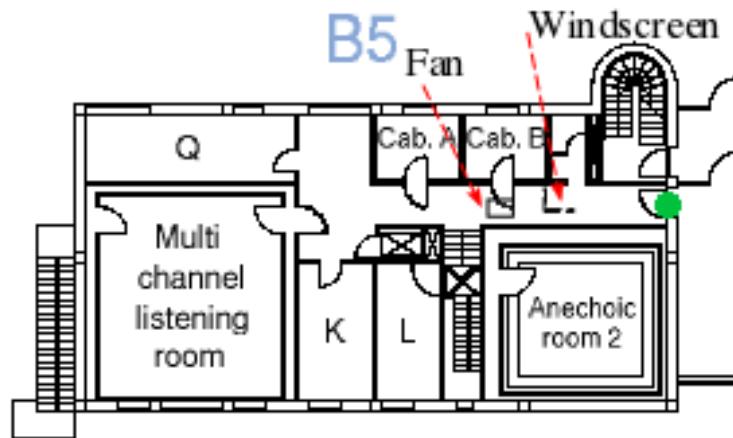
1. The materials are set up as in Figure E.1.
2. The fan is placed such that it produces crosswind.
3. The fan is activated.
4. The anemometer is activated to record.
5. The anemometer is placed in the wind for approximately 10 s.
6. Then the anemometer is moved into the microphone position for approximately 10 s.
7. Then the anemometer is moved back in the wind for approximately 10 s.
8. Then the anemometer is moved into the microphone position for approximately 10 s again.
9. The wind speed measurement is plotted in MATLAB® with a moving mean filter with 2 sample and as m/s versus s.
10. Next the wind direction measurement is plotted in MATLAB® with a moving mean filter with 2 sample and as ° versus s.



**Figure E.2:** The figure shows the movement of the anemometer doing the measurement

## Measurement area

To be able to generate a controlled wind flow, the hall way in Fredrick Bajers vej 7B5, 9220 Aalborg is used. The following ?? shows a drawing of the area and the position of the fan and windscreens.



**Figure E.3:** The picture illustrate the area, where the wind flow is measured

## Results

The following graphs shows the result of the measurement.

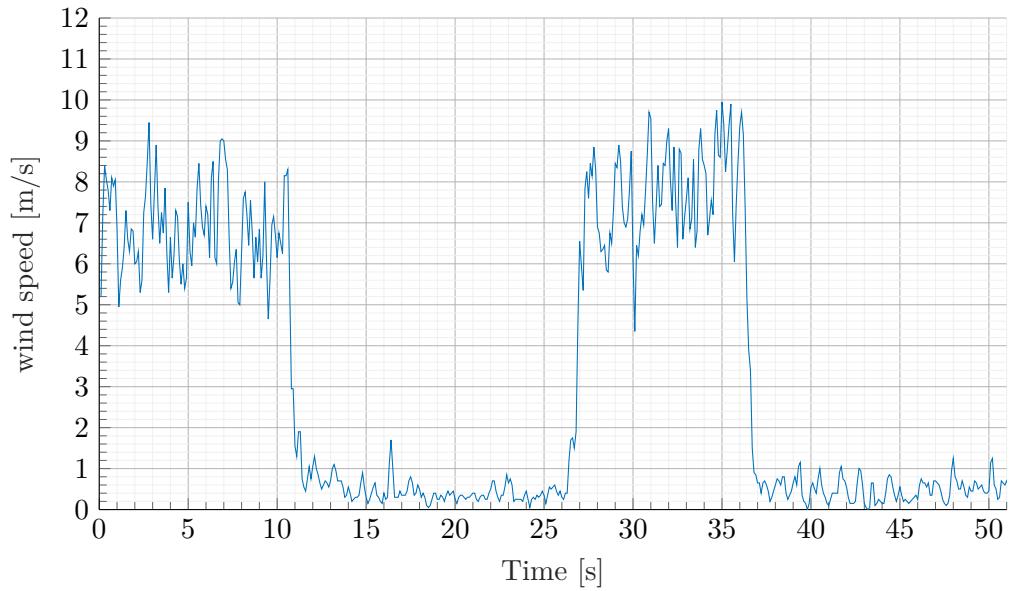
Figure D.5 shows the measurement setup of the foam wedge, where the ?? shows the result.



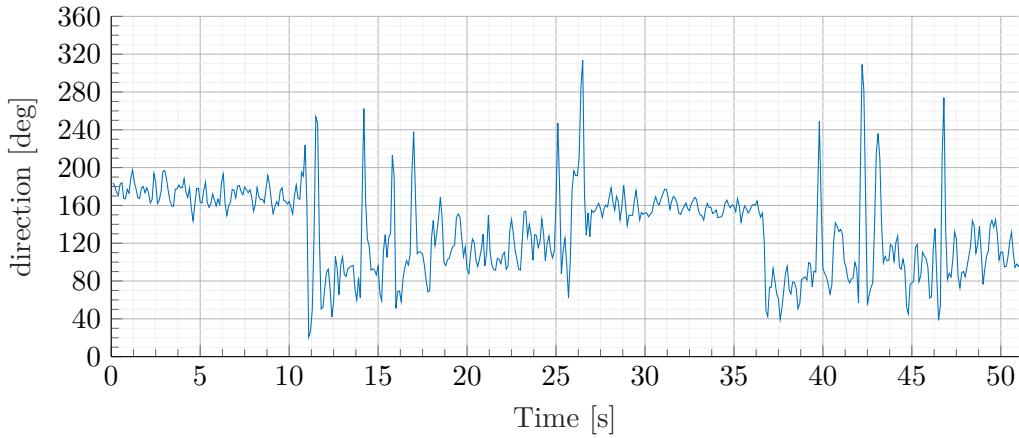
(a) The picture shows the measurement setup for the optimised windscreen configuration five from back

(b) The picture shows the measurement setup for the optimised windscreen configuration five in front

**Figure E.4:** ap:wind:large\_opt\_pic



**Figure E.5:** The graph shows the wind speed versus time for the optimised configuration five. The graph have a high speed period and a low speed period. In the high speed period, the anemometer is in the wind approximately 30 cm from the windscreens where in the low speed period, the anemometer is inside the windscreens.



**Figure E.6:** The graph shows the synchronous direction of the wind with respect to the wind speed in Figure E.5

It is seen in Figure E.5 that the wind speed is lowered from approximately 8 m/s to 0.5 m/s. It is seen in Figure E.6 that the windspeed produces turbulence in the windspeed and the direction of the wind change approximately  $-100^\circ$ . The reason that the angle is negative in this measurement is that the anemometer is turned  $180^\circ$  in the vertical plan for practical reason.

## Summary

It is measured that the optimised windspeed lower the wind turbulence by optimising the aerodynamics with curved surface and small thin edges.



## Appendix F

# Outline ET 250-3D turntable control

In this appendix the control of an Outline ET 250-3D turntable will be described. The turntable can be controlled in three ways. the first which are Transistor–Transistor Logic (TTL) commands through a jack connector. Secondly, it can be controlled by specific Dynamic Link library (DLL) commands through Ethernet. All of those are included in a software pack available from the manufacturer. Thirdly the turntable can be controlled by User Datagram Protocol (UDP) commands through Ethernet. For controlling the turntable by MATLAB, the second Ethernet based control method is the easiest to do because MATLAB supports Ethernet access. The DLL method requires a complicated scripts which might only work on Windows operation systems. UDP can be sent and received by the vast majority of operating systems, which support IPv4 Ethernet connection. The usage of UDP leads to short and simple scripts, where the script opens a UDP channel as a file, and e.g. the script shall only edit the file in the right position to move the turntable. Because of the advantages in implementation, UDP is chosen over the other controlling methods for the turntable.

## Materials and setup

The following materials are used:

**Table F.1:** Equipment list

Description	Model	Serial-no	AAU-no
PC	Macbook	W89242W966H	-
Turntable	Outline ET 250-3D	REIBO012	-
PC - software	MATLAB 2018b	-	-

## The UDP setup of the computer

To establish connection between the turntable and computer, both have to run at the same SUBNET MASK. The turntable comes with a factory setting for Ethernet connection which is as follows:

**Table F.2:** Turntable network address

Internet Protocol (IP)	192.168.1.34
SUBNET MASK	255.255.255.0
DEFAULT GATEWAY	192.168.1.250
BROADCAST IP	192.168.1.255

## Turtable control command

The software is implemented as a function, where the user can retrieve the turntable position, specify a position and stop the turntable. The function name is:

**Code snippet F.1:** The turntable control function | ET250\_3D.m

```
1 function [angle] = ET250_3D(cmd, angle)
```

The function is made as a switch case with input variable "cmd", and an angle input. The following command can be send to the "cmd" of the function:

**Table F.3:** Function commands

cmd = 'udp_start'	Which start a connection on port 7000
cmd = 'set'	Which move the turntable to the specified angle
cmd = 'get'	Which get the position of the turntable
cmd = 'stop'	Which stop the turntable from moving
cmd = 'udp_stop'	Which stop the connection on port 7000

## The MATLAB function

**Code snippet F.2:** The turntable control function | ET250\_3D.m

```
1 function [angle] = ET250_3D(cmd, angle)
2
3
4 switch cmd
5
6   case 'udp_start'
7     echoudp('on', 7000)
8     u = udp('192.168.1.34', 7000);
9     fopen(u)
10
11
```

```

12     case 'set'
13         %request current position
14         fwrite(u,hex2dec(['04';'00';'00';'04']))
15         x = fread(u,7);
16         angle_current = (x(4)*256+x(5))/10;
17
18         %calc shortest way
19         angle_delta = angle-angle_current;
20         if angle_delta > 180
21             angle_delta = angle_delta - 360;
22         end
23         if angle_delta < -180
24             angle_delta = angle_delta + 360;
25         end
26
27         cmd(1) = uint8( 1.5-sign(angle_delta)/2 );
28             %1st byte = direction
29         cmd(2) = uint8( floor(abs(angle_delta*10)/256) );
29             %angle in degree*10
30         cmd(3) = uint8( mod(floor(abs(angle_delta*10)),256) );
30             %angle in degree*10
31         cmd(4) = 0;
32
33         fwrite(u,cmd)
34             %receive
34             ACK
35
36     case 'get'
37         %request current position
38         fwrite(u,hex2dec(['04';'00';'00';'04']))
39         x = fread(u,7);
40         angle = (x(4)*256+x(5))/10;
41
42     case 'stop'
43         fwrite(u,hex2dec(['03';'00';'00';'03'])) %send
43             stop stop
44         x = dec2hex(fread(u,2));
45
46     case 'udp_stop'
47         echoudp('off')
48         fclose(u)
49 end
50
51
52 end

```



## Appendix G

# The directionality of L-acoustics KUDO

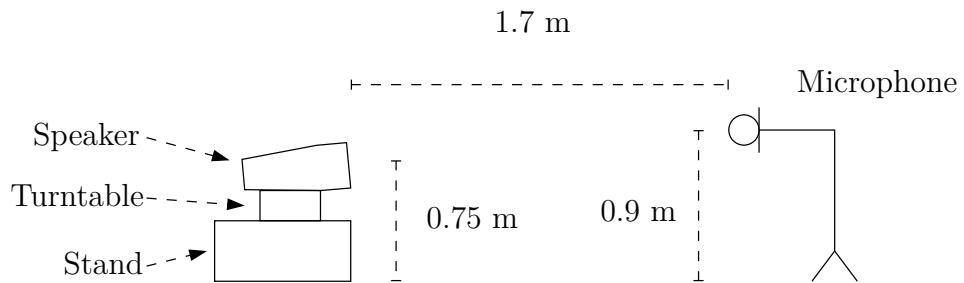
A measurement was made to measure the directionality of a L-acoustics KUDO. The goal of this appendix is to measure the polar response and calculate transfer functions of the line source array element in a free field environment with calibrated measuring equipment. During the measurement of the polar response, impulse responses are measured with a specified degree step size all around the speaker. E.g. if the step is one degree, the loudspeaker will be turned 1 degree for every impulse response measurement, until  $360^\circ$  is achieved.

### Materials and setup

To measure the directionality of the line source element, the following materials are used:

**Table G.1:** Equipment list

Description	Model	Serial-no	AAU-no
PC	Macbook	W89242W966H	-
Audio interface	RME Fireface UCX	23811948	108230
Microphone	GRAS 26CC	78189	75583
Preamp	GRAS 40 AZ	100268	75551
Speaker	L-acoustics KUDO	7733	-
Turntable	Outline ET 250-3D	REIBO012	-
PC - software	MATLAB 2018b	-	-



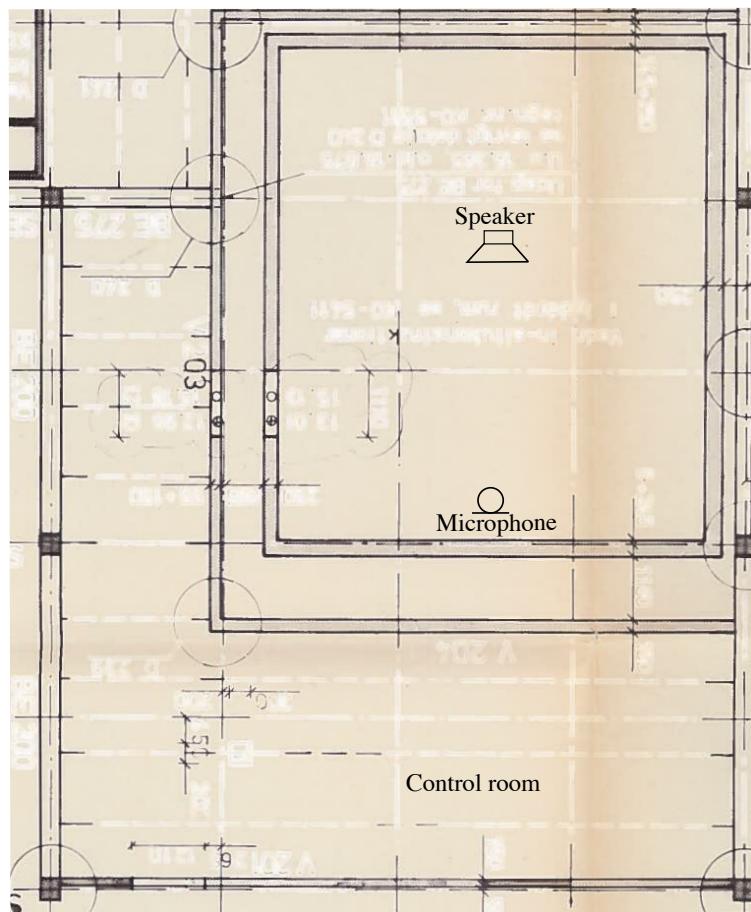
**Figure G.1:** The figure shows the measurement setup in the anechoic chamber

## Test procedure

1. The materials are set up as in Figure G.1 where the microphone is connected to the audio interface.
2. The microphone is calibrated
3. The speaker is placed 1.7 m from the microphone and pointing in the direction of the microphone.
4. The impulse response is measured for every  $5^\circ$
5. The  $-3 \text{ dB SPL}$  step contour is calculated until  $-21 \text{ dB SPL}$  and plotted.

## Measurement area

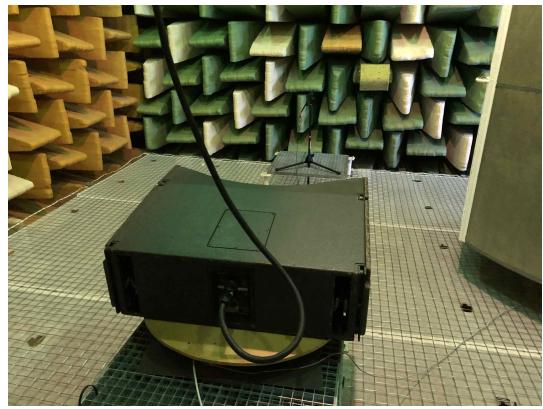
To be able to measure the windscreen frequency response, the anechoic chamber in Fredrick Bajers vej 7B4, 9220 Aalborg is used. The following Figure G.2 shows a drawing of the area and the position of the fan and windscreens.



**Figure G.2:** The picture illustrate the position of the microphone and the speaker

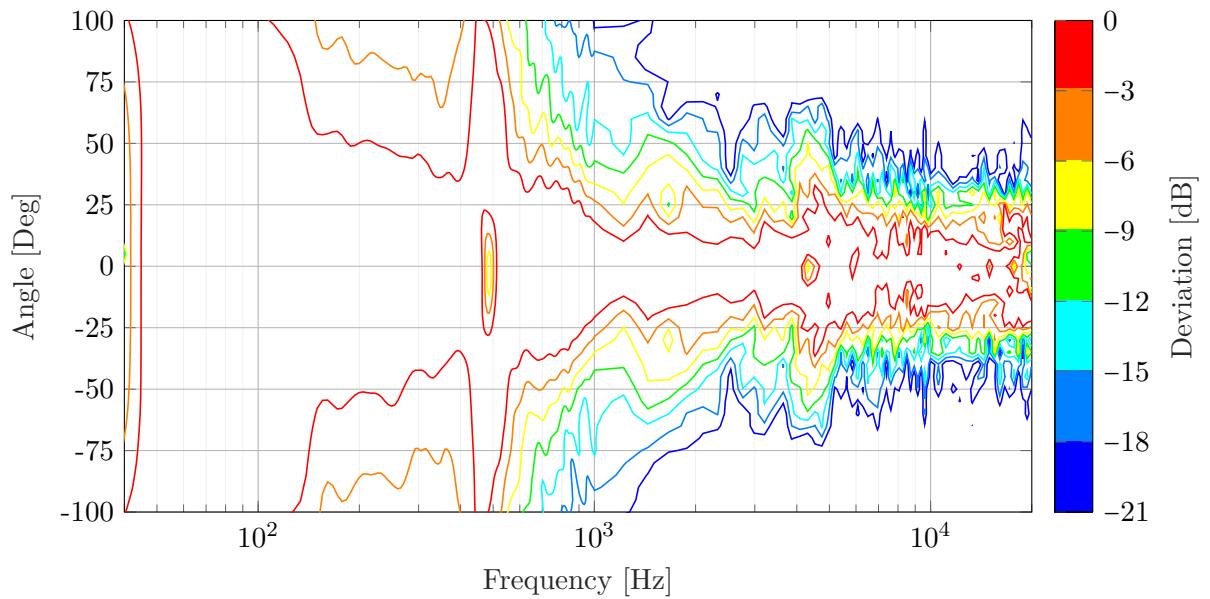
## Results

The following Figure G.3 shows the measurement setup.

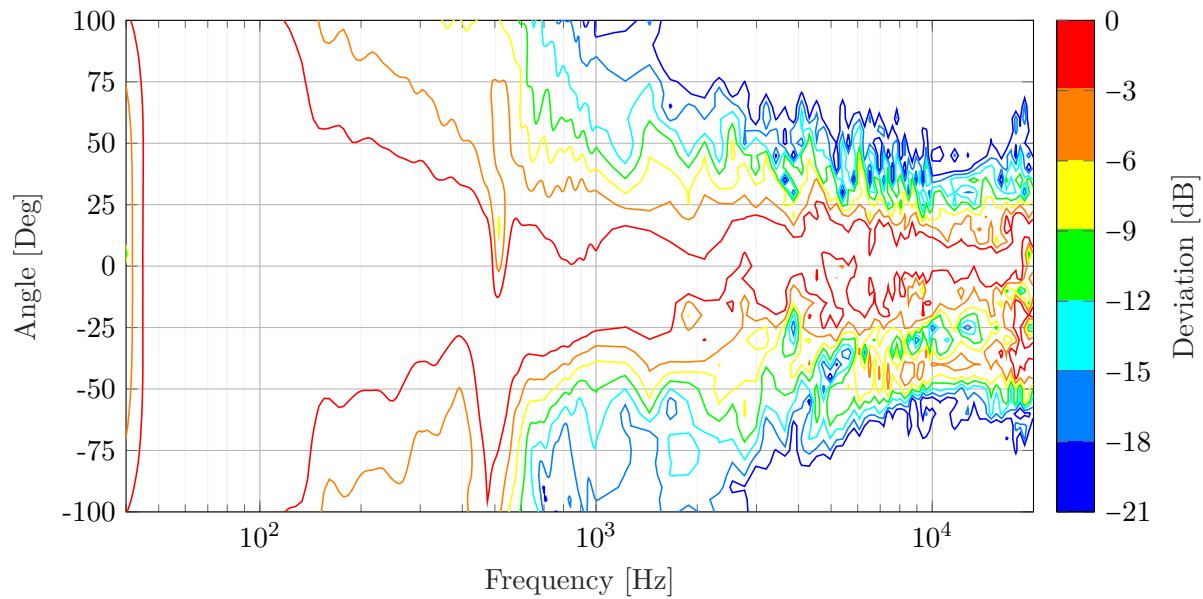


**Figure G.3:** The picture shows the measurement setup

The following graphs shows the result of the measurement.



**Figure G.4:** The graph shows



**Figure G.5:** The graph shows

## Summary



## **Appendix H**

# **cross wind effect on line source array**

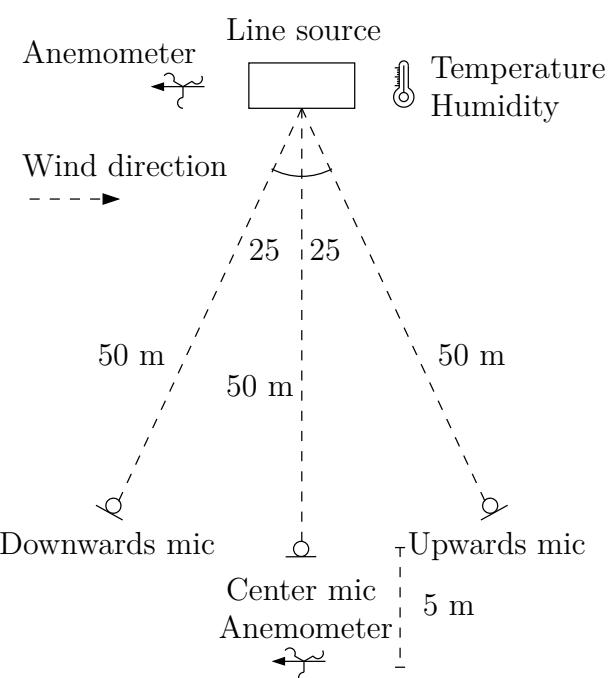
A measurement was made to measure the transfer function differences in three point in crosswind. One microphone situated in downwards direction, one microphone situated in upwards direction and one microphone situated in center, which is between the other two microphone. The used speaker have a horizontal dispersion pattern of 80°, but it is the 50° angle which is used as explained in ??

### **Materials and setup**

To measure the transfer function in a crosswind situation, the following materials are used:

**Table H.1:** Equipment list

Description	Model	Serial-no	AAU-no
PC	Macbook	W89242W966H	-
Audio interface	RME Fireface UCX	23811948	108230
Microphone	GRAS 26CC	78189	75583
Preamp	GRAS 40 AZ	100268	75551
Microphone	GRAS 26CC	78186	75582
Preamp	GRAS 40 AZ	100267	75550
Microphone	GRAS 26CC	??	
Preamp	GRAS 40 AZ		
3 Windscreen	Author design	-	-
Line source element	L-acoustics KUDO		
Line source element	L-acoustics KUDO		
Line source element	L-acoustics KUDO		
Line source element	L-acoustics KUDO		
Line source element	L-acoustics KUDO		
Amplifier	Lab PLM10000Q		
Amplifier	Lab PLM10000Q		
Mixer	Yamaha LS9		
Wind measurement tools	Davis	-	
Angling tools flying tools	Author design	-	
	-	-	-

**Figure H.1:** The figure shows the microphone position versus the position of the line source, while the array is 0° horizontal turned



(a) The picture shows the speaker setup



(b) The figure shows the wind direction

**Figure H.2:** The figures shows the measurement set up for Appendix A and ??

## Test procedure

1. The microphone is calibrated.
2. The wind direction is measured.
3. The materials are set up as in Figure H.1 where the speaker is placed in cross wind direction, such that the frontal wave direction is orthogonal to the wind. The microphone and speaker is connected to the audio interface.
4. The speaker is placed 2.92 m above the ground.
5. The speaker is tilted 5° pointing down against the ground.
6. The microphone is placed 1.68 m above the ground, 50 m from the speaker. One 25° to the left of the speaker, one 25° to the right of the speaker and one in center between the two other microphones.
7. The anemometer at the speakers is situated on the speaker tower in the same side as shown on the setup and a height of 4.64 m
8. The anemometer at the microphone position is lifted 1.68 m above the ground.
9. The wind direction goes from the upwards microphone to the downwards microphone.
10. The humidity and temperature is measured at the speaker position.
11. 10 sine sweep is performed with a length of 5 s each while the wind direction and speed is measured.
12. The impulse response is calculated and filtered with a 4th order highpass filter at 20 Hz.
13. The correlation is calculated for each impulse response to the first impulse response for time alignment [Gunness, 2001] of all microphone channels.
14. The mean impulse response is calculated for the 10 measurement of all three microphone.
15. The transfer function is calculated with a 10 sample moving mean filter.

16. The transfer function is down sampled to fit the plotting program.
17. The transfer function is calculated with a 5 sample moving mean filter.
18. The wind measurement is synchronised to the transfer function in time.
19. The measurement is repeated 6 times with different horizontal speaker angle from  $0^\circ$  to  $30^\circ$  in step of  $5^\circ$

## Measurement area

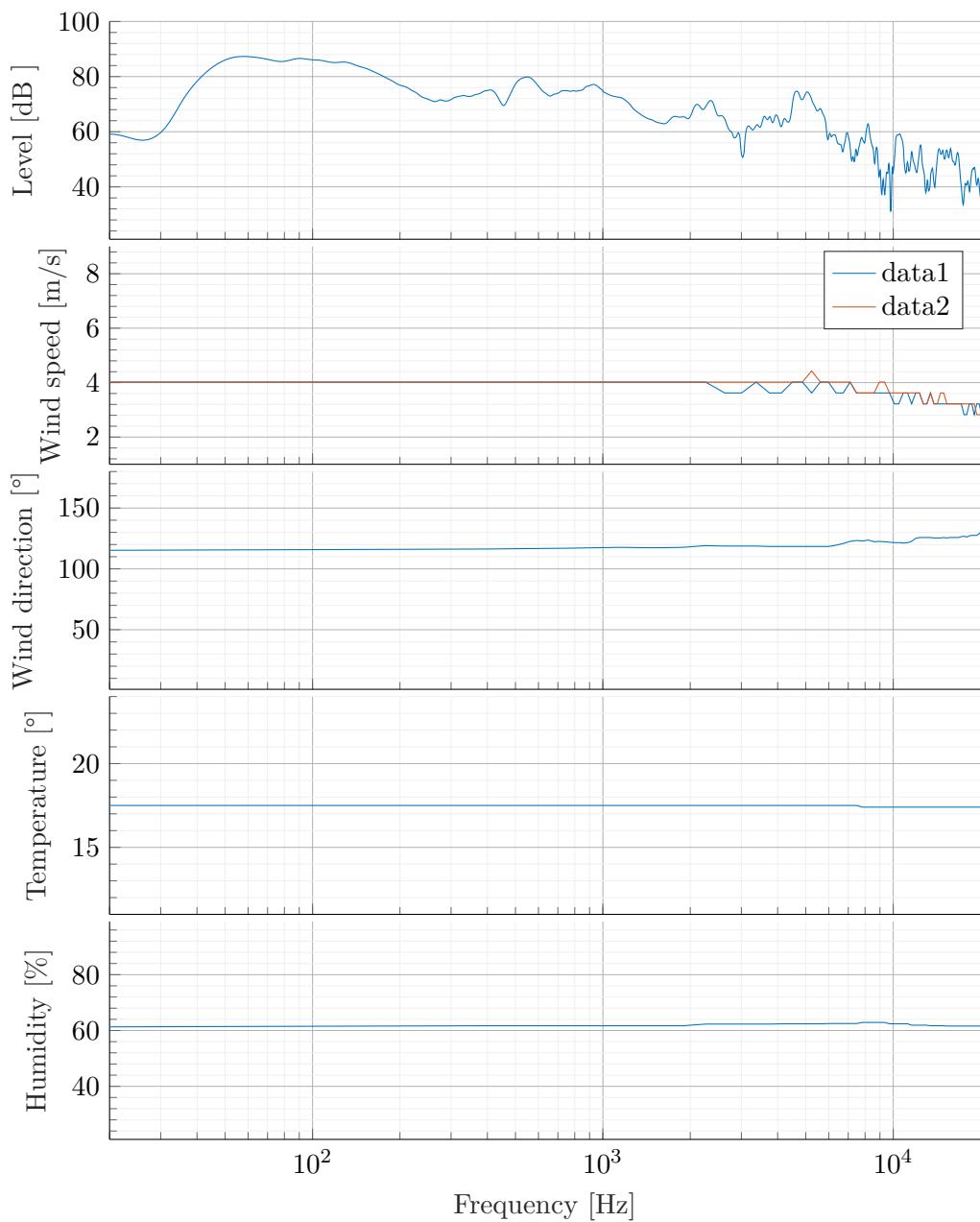
To be able to measure in a windy area, parking lot at Tryvej 13, 9320 Hjallerup is used. The following Figure H.3 shows a picture of the area and the approximate position of the speaker and microphone.



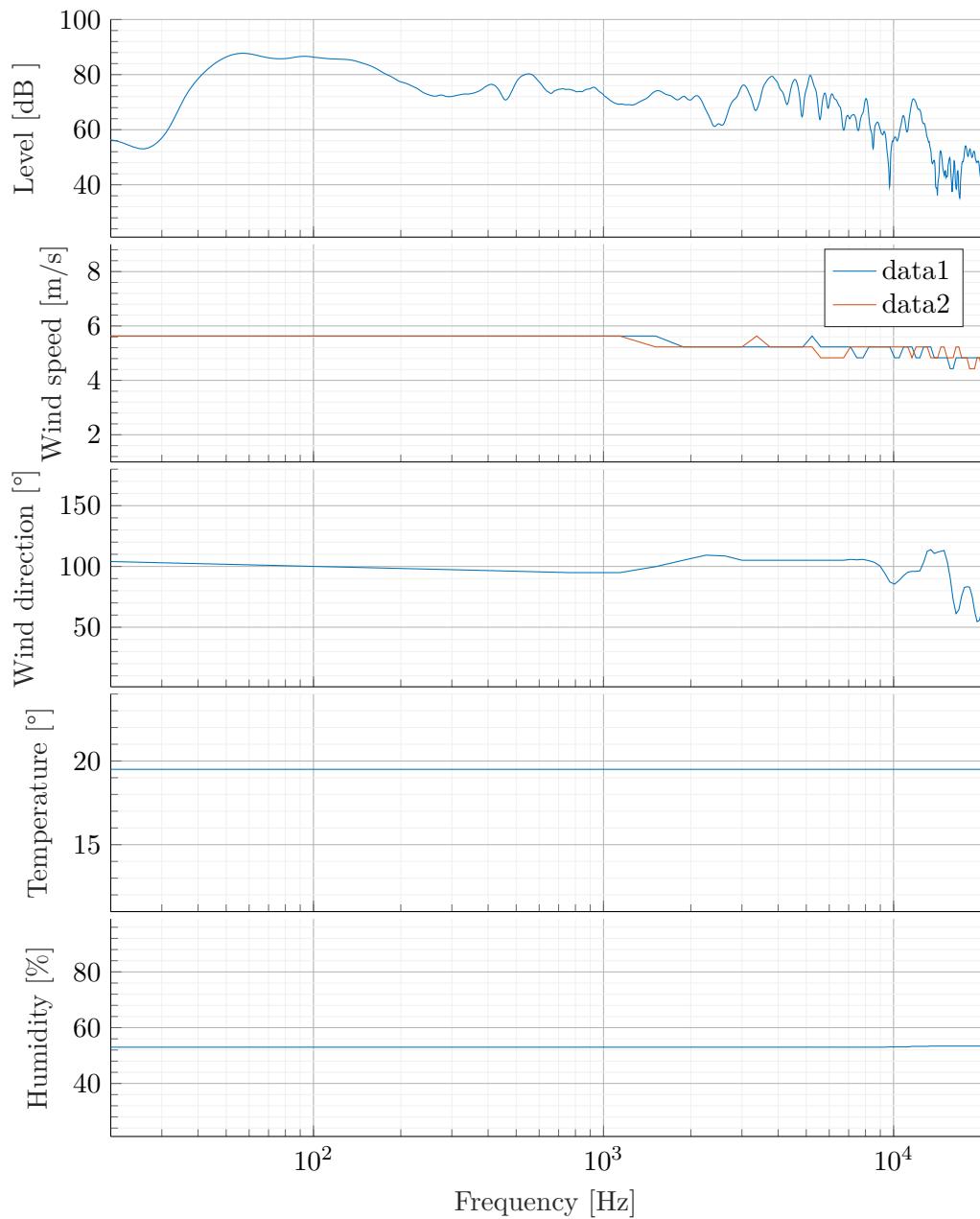
**Figure H.3:** The picture illustrate the area, where the wind flow is measured

## Results

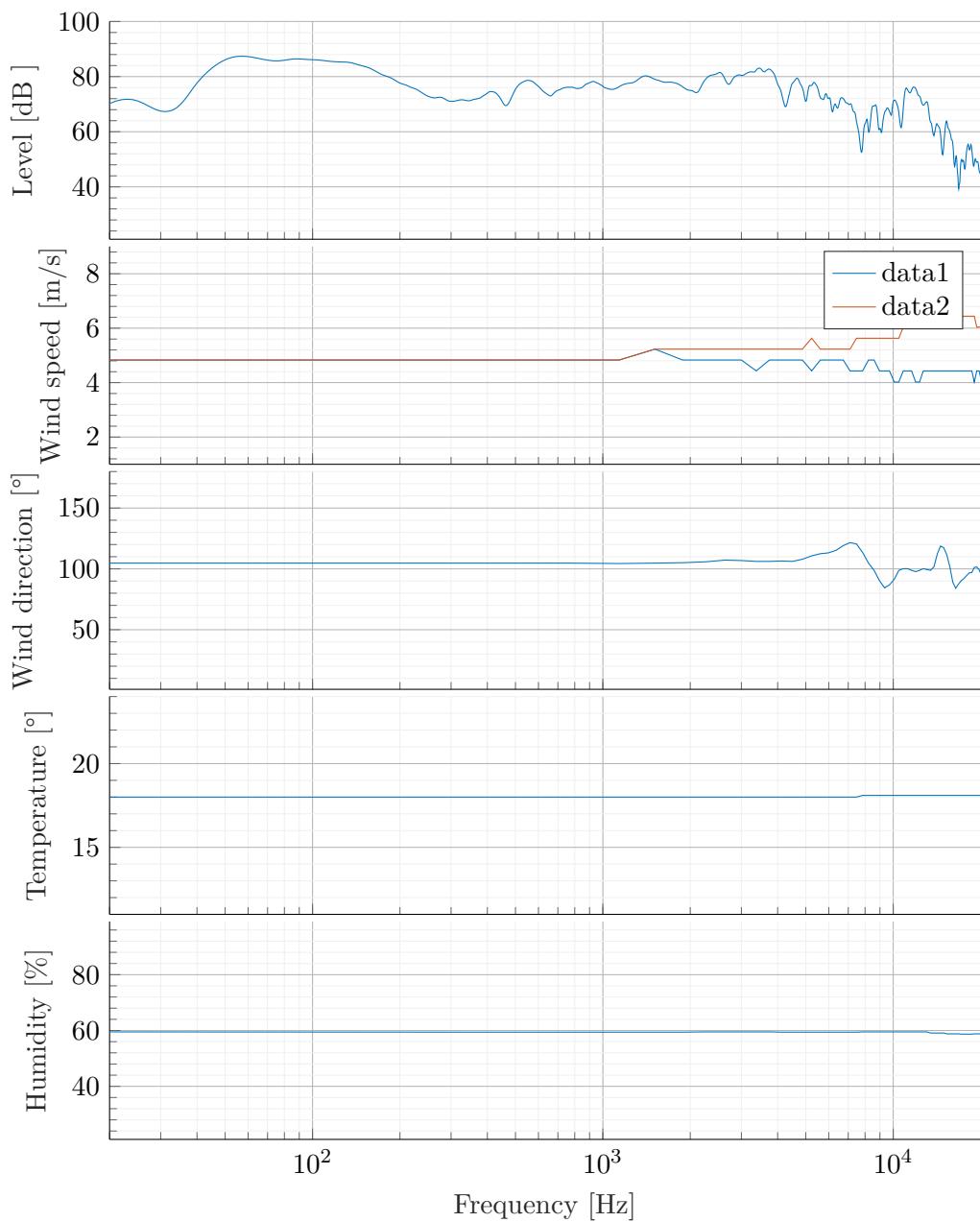
All measuring result is not shown here, the rest can be founded in the attached file. One synchronised measurement is shown for the upwards microphone where the speaker is turned  $0^\circ$ ,  $10^\circ$ ,  $20^\circ$  and  $30^\circ$ . The shown measurement result is for one measurement and is not a mean from 10. This shows the time synchronised result. The average result can be founded in ??.



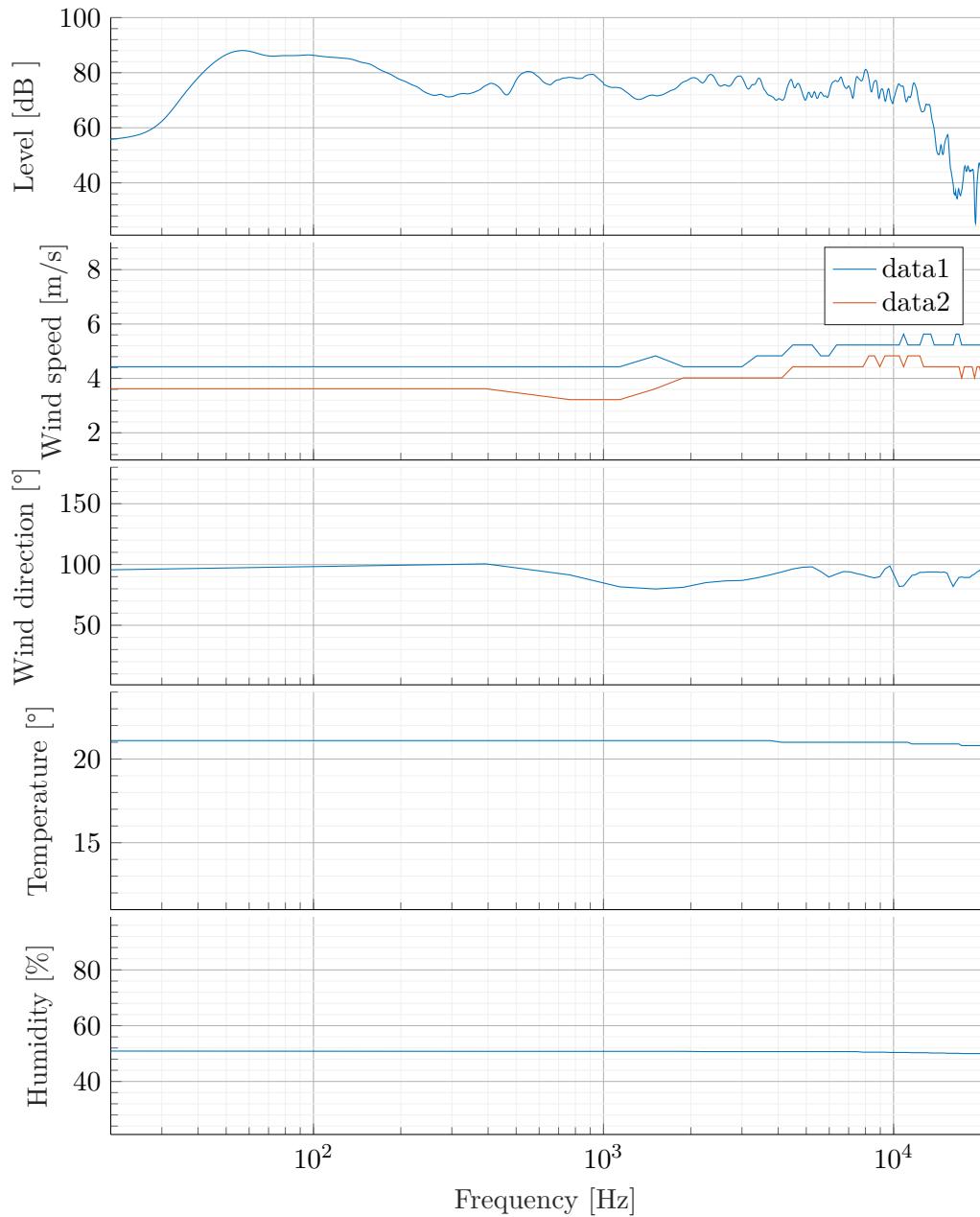
**Figure H.4:** the graph shows



**Figure H.5:** the graph shows



**Figure H.6:** the graph shows



**Figure H.7:** the graph shows

## Summary

## Appendix I

# Line source array angle measuring design

To measure the angle of the speaker, a angle plate with coloured laser indicator is designed.

## Materials and setup

The following material is used

**Table I.1:** Equipment list

Description	Model	Serial-no	AAU-no
Laser pen	Red	-	-
Laser pen	Green	-	-
Angle plate	-	-	-
Laser pen holder	-	-	-



(a) The picture shows the angle finder plate  
(b) The figure shows the lasers and the laser holder

**Figure I.1:** The figures shows the angle finder martial for the used line source array

### Adjusting the line source horizontal angle

1. The materials are set up as in Figure I.1.
2. The line source array is turned until the laser pointers light is on the drawn line of the angle or with the same distance to the line.

## Appendix J

# Windscreen influence of frequency response

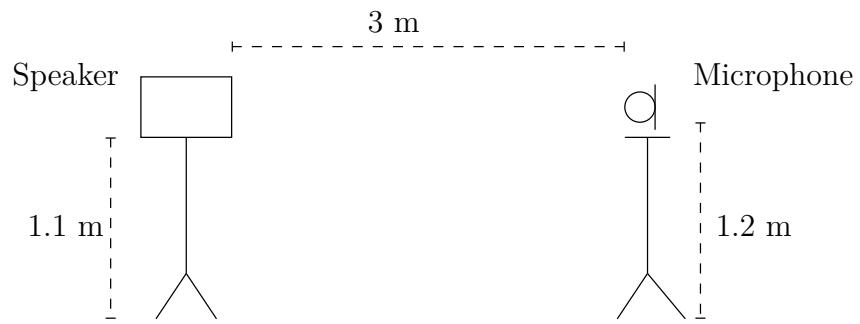
A measurement was made to measure the frequency influence of the designed windscreen. The configuration include the modified GRAS AM0069 windscreen. The measurement is done in the anechoic chamber. The measurement is done to analyse the effect of the windscreen in the frequency domain to find out if the observed frequency boost in ?? is an artefact of the windscreen.

### Materials and setup

To measure the frequency response of the windscreen configuration the following materials are used:

**Table J.1:** Equipment list

Description	Model	Serial-no	AAU-no
PC	Macbook	W89242W966H	-
Audio interface	RME Fireface UCX	23811948	108230
Microphone	GRAS 26CC	78189	75583
Preamp	GRAS 40 AZ	100268	75551
Windscreen	GRAS AM0069	-	-
large foam wedge	-	-	-
Speaker stand	-	-	-
Speaker	Dynaudio	03508438	1441-0

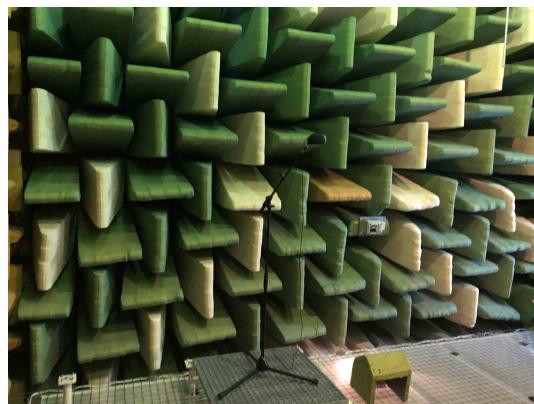


**Figure J.1:** The figure shows the measurement setup in the anechoic chamber

The following Figure J.2 shows the speaker.



**Figure J.2:** The picture shows the used speaker



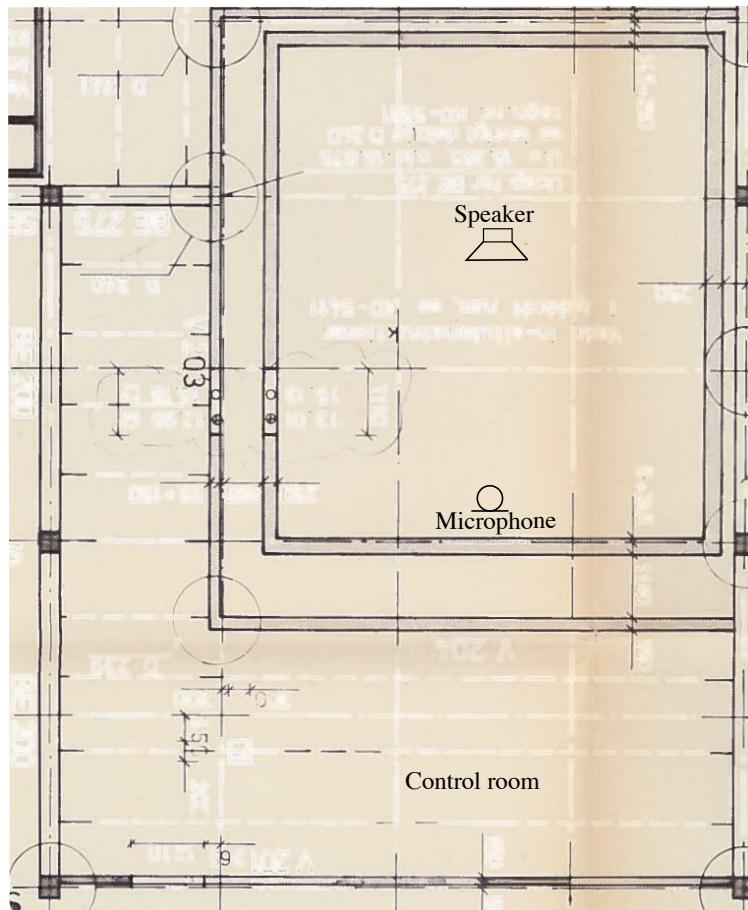
**Figure J.3:** The picture shows the measurement microphone with the original modified windscreens

## Test procedure

1. The materials are set up as in Figure J.1 where the microphone is connected to the audio interface.
2. The microphone is calibrated
3. The speaker is placed 3 m from the microphone and pointing in the direction of the microphone.
4. The transfer function is measured of the speaker without the designed windscreen and with the modified windscreens.
5. The windscreens configuration is placed such that the microphone have approximately the same position as without the designed windscreens, (while the windscreens are tilted the microphone is closer to the speaker).
6. The transfer function is measured
7. The transfer function is calculated and plotted versus the transfer function without designed windscreens but with modified original windscreens MATLAB®.
8. The position of the windscreens is changed both with tilting and rotation while the measuring is repeated.
9. In the end the designed windscreens are measured without foam wedge.

## Measurement area

To be able to measure the windscreens frequency response, the anechoic chamber in Fredrick Bajers vej 7B4, 9220 Aalborg is used. The following Figure J.4 shows a drawing of the area and the position of the fan and windscreens.

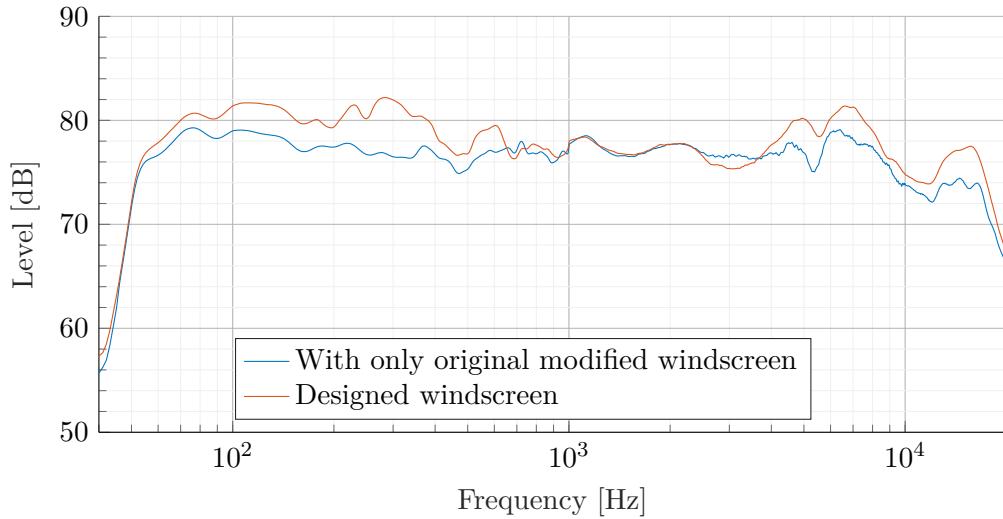


**Figure J.4:** The picture illustrate the area, where the wind flow is measured

## Results

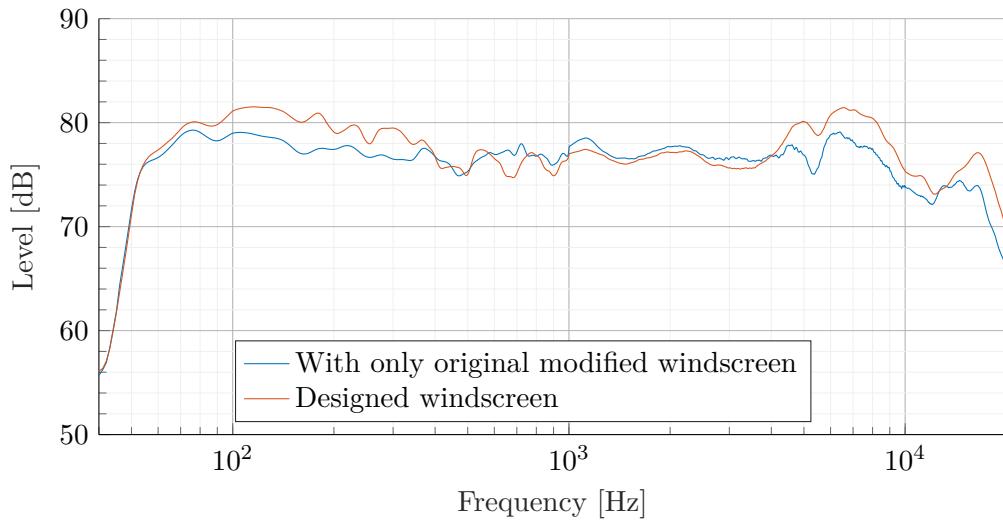
The following graphs shows the result of the measurement.

The first measurement in Figure J.5 shows the transfer function while the foam wedge is at its designed position and without tilting and rotation. Therefore the windscreens point with  $0^\circ$  to the speaker and the windscreens plate have vertical and horizontal of  $0^\circ$



**Figure J.5:** The graph shows frequency response of the speaker measured without windscreen and with the designed windscreen with no rotation and no tilting

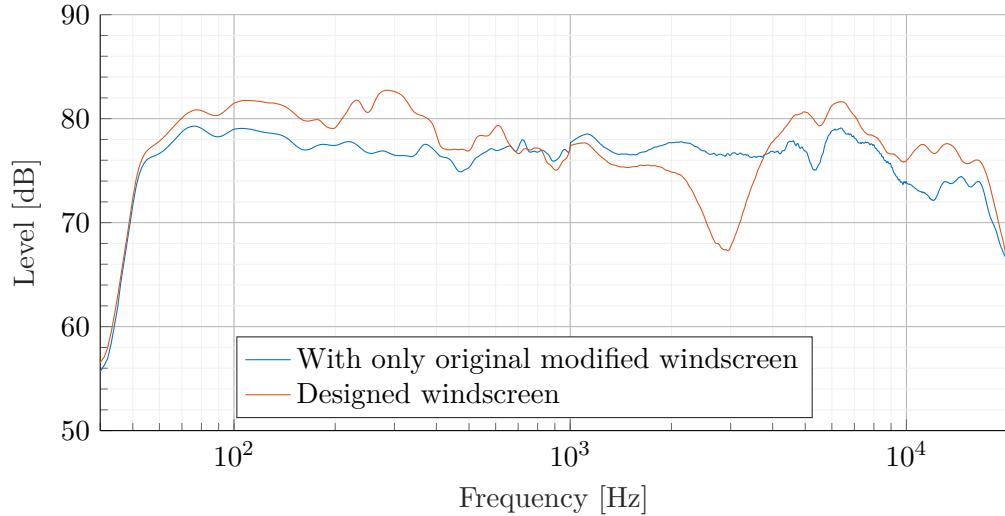
The next measurement in Figure J.6 shows the transfer function while the foam wedge is moved 20 cm back compare to its designed position and without tilting and rotation.



**Figure J.6:** The graph shows frequency response of the speaker measured without windscreen and with the designed windscreen with no rotation and no tilting while the foam wedge is moved 20 cm back

As seen in Figure J.6 the frequency response does not change markedly compare to Figure J.5. It is seen that the general level is 0.5 dB SPL lower as expected since the microphone is moved back.

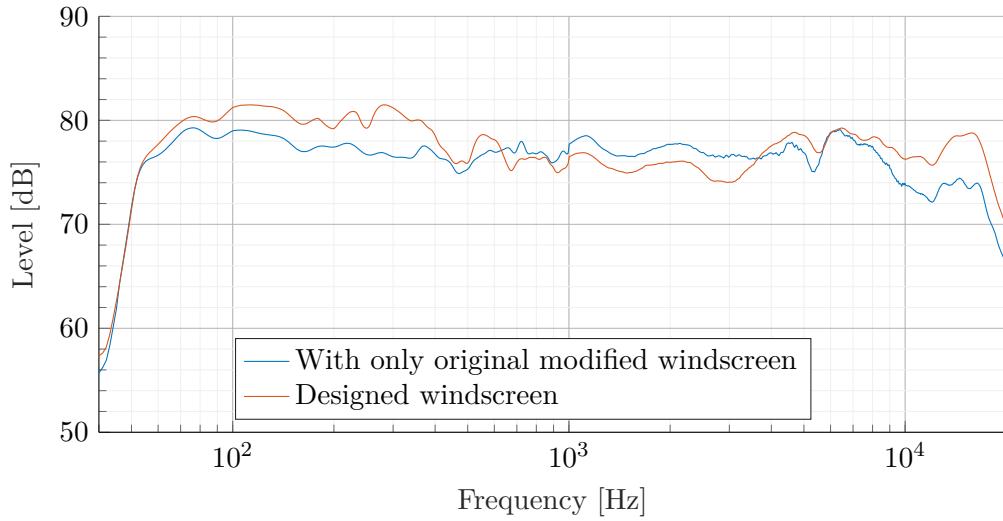
The next measurement in Figure J.7 shows the transfer function while the foam wedge is at its designed position and without tilting and with 30° right rotation. Therefore the white PVC plate covers more the opening to the microphone and the windscreens have vertical and horizontal of 0°



**Figure J.7:** The graph shows frequency response of the speaker measured without windscreen and with the designed windscreen with no tilting and a right rotation of 30°

It is seen in Figure J.7 that 30° right rotation gives a SPL depth between 1.0 kHz and 4.0 kHz otherwise the frequency response is similar to Figure J.5

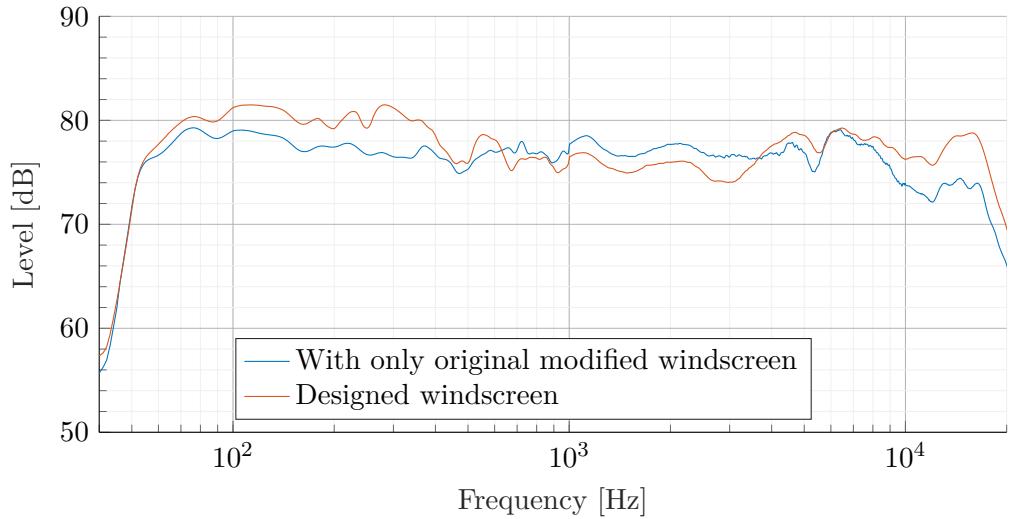
The next measurement in Figure J.8 shows the transfer function while the foam wedge is at its designed position and without tilting and with 30° left rotation. Therefore the foam wedge covers more the opening to the microphone and the windscreens have vertical and horizontal of 0°



**Figure J.8:** The graph shows frequency response of the speaker measured without windscreen and with the designed windscreen with no no tilting and a left rotation of 30°

It is seen in Figure J.8 that 30° left rotation also gives a SPL depth between 1.0 kHz and 4.0 kHz but much less than Figure J.7. Otherwise the frequency response is similar to Figure J.5

The next measurement in Figure J.9 shows the transfer function while the foam wedge is at its designed position and with a tilting of 9° and without rotation. Therefore the windscreens point with 0° to the speaker and the windscreens plate have horizontal of 0°



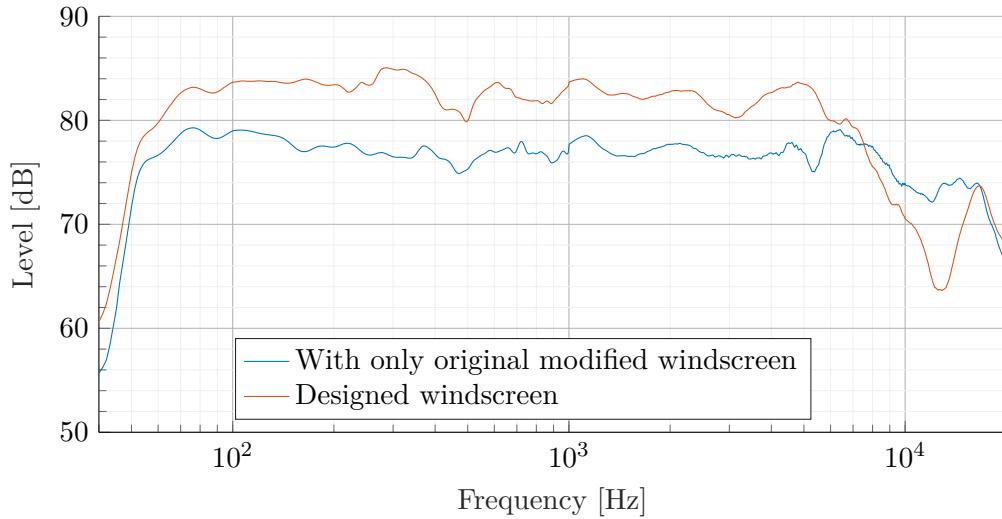
**Figure J.9:** The graph shows frequency response of the speaker measured without windscreen and with the designed windscreen with no rotation and a frontal tilting of 9°

As seen in Figure J.9 the frequency response does not change markedly compare to Figure J.5. It is seen that the general level is 2 dB SPL higher as expected since the microphone is moved closer to the speaker as shown in Figure J.10.



**Figure J.10:** The picture shows the measurement microphone with the tilted designed windscreen

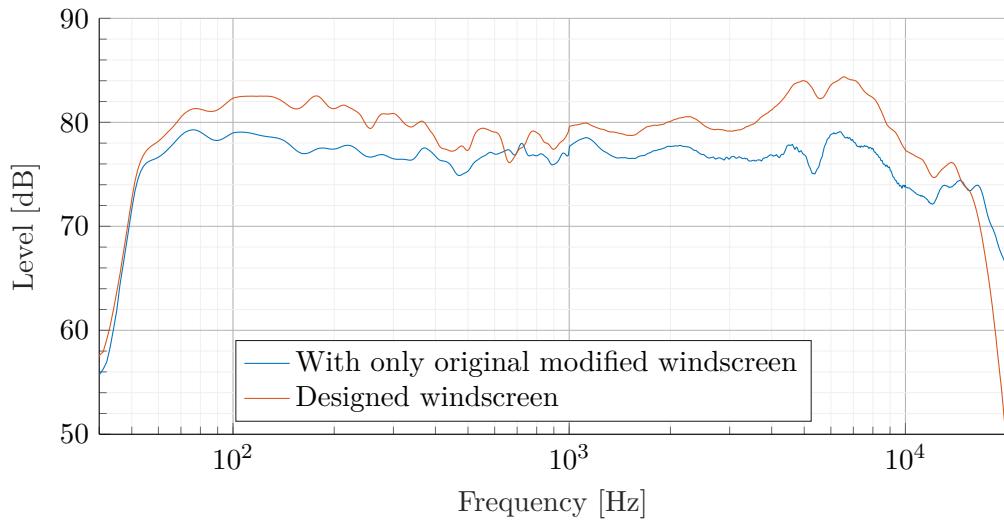
Moreover there is a roll off in the frequency higher than 10 kHz which might result from a plate reflection of the sound since the microphone is lifted by the modified original windscreen. To research the roll off the tilting of the plate is raised to 20°. The result of tilting 20° is shown in Figure J.11



**Figure J.11:** The graph shows frequency response of the speaker measured without windscreens and with the designed windscreens with no rotation and a frontal tilting of  $9^\circ$

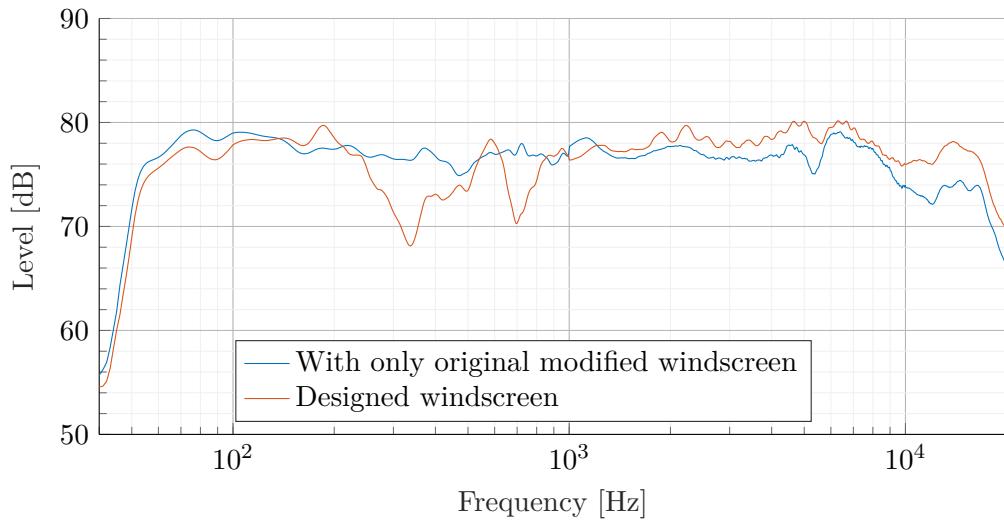
As seen in Figure J.11, the roll off is due to a plate reflection. While tilting  $20^\circ$  the reflection frequency is lowered which means that the sound path differences of the reflected sound path grows.

A tilting of the windscreens while the foam wedge is moved 20 cm is measured as the last measurement while the foam wedge is on the plate. The following Figure J.12 shows the result with a tilt of  $8^\circ$  and no rotation.

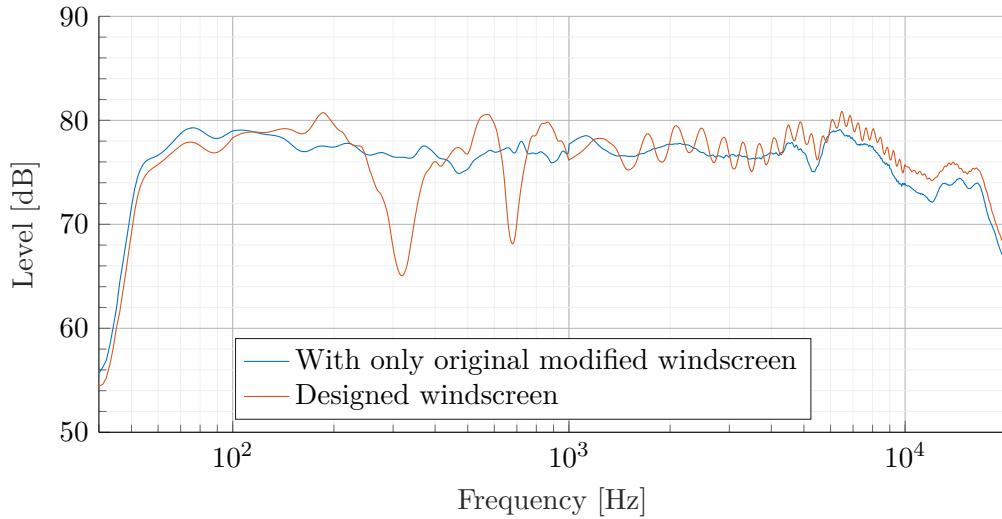


**Figure J.12:** The graph shows frequency response of the speaker measured without windscreen and with the designed windscreen moved 20 cm back with no rotation and a frontal tilting of  $8^\circ$

The last two measurement shows the frequency response while the foam wedge is removed. The first measurement in Figure J.13 shows the frequency response without tilting and rotation. The second measurement in Figure J.14 shows the frequency response without tilting and a rotation of  $30^\circ$  to the right.



**Figure J.13:** The graph shows frequency response of the speaker measured without windscreen and without the designed windscreen without the foam wedge and with no rotation and no tilting



**Figure J.14:** The graph shows frequency response of the speaker measured without windscreen and with the designed windscreen without the foam wedge and with no tilting and a right turn of  $30^\circ$

It is seen in measurement Figure J.13 and Figure J.14 that removing the foam wedge gives depth in 310 Hz and 690 Hz and the frequency response shows generally more reflections than with foam wedge.

## Summary

The designed windscreen gives a small boost in frequency below 1.0 kHz and above 4.0 kHz but the boost is only approximately 2 dB SPL. Moreover tilting of the designed windscreen gives plate reflection in the high frequency, but tilting at  $9^\circ$  only affect frequency above 10 kHz. Rotating the windscreen ether to the left or right gives a depth within 1.0 kHz to 4.0 kHz. While moving the foam wedge backwards the frequency response of the designed windscreen have only negligible differences. Removing the wedge gives high reflection from the designed windscreen.



## Appendix K

# Wind noise in designed windscreen

A measurement was made to measure the wind attenuation of the designed windscreen. All measurement include the modified GRAS AM0069 windscreens. The measurement is done in real scenario outside on a flat area with above 5 m/s wind speed. The measurement is done to ensure that the measured wind does not overload the preamp of the microphone at the measured wind speed.

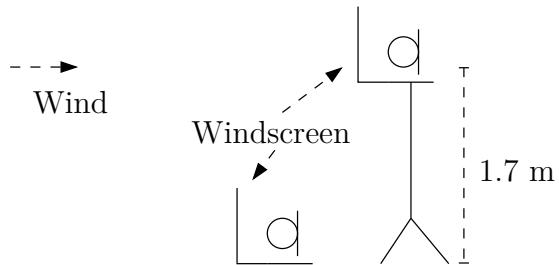
## Materials and setup

To measure the wind attenuation of the windscreen configuration the following materials are used:

**Table K.1:** Equipment list

Description	Model	Serial-no	AAU-no
PC	Macbook	W89242W966H	-
Audio interface	RME Fireface UCX	23811948	108230
Microphone	GRAS 26CC	78189	75583
Preamp	GRAS 40 AZ	100268	75551
Windscreens	GRAS AM0069	-	-
Designed windscreens	-	-	-

**Table K.2:** Equipment list



**Figure K.1:** The figure shows the measurement setup for the wind noise measurement.



**Figure K.2:** The picture shows the measurement set up

## Test procedure

1. The materials are set up as in Figure K.1 where the microphone is connected to the audio interface.
2. The microphone is calibrated.
3. A 7 s time signal is measured.
4. The frequency content is calculated by `fft` after the time signal is windowed by a Hanning window.
5. The procedure is done with and without the windscreens.
6. The procedure is done where the windscreens are rotated 50° and -50°.
7. The result is plotted in MATLAB®.
8. The measurement is done over for every position until similar wind speed is measured with about 8.5 m/s.

## Measurement area

To be able to measure in a windy area, the football stadium at Fredrick Alfred Nobels Vej 7, 9220 Aalborg is used. The following Figure K.3 shows a picture of the area and the approximate position of the speaker and microphone.

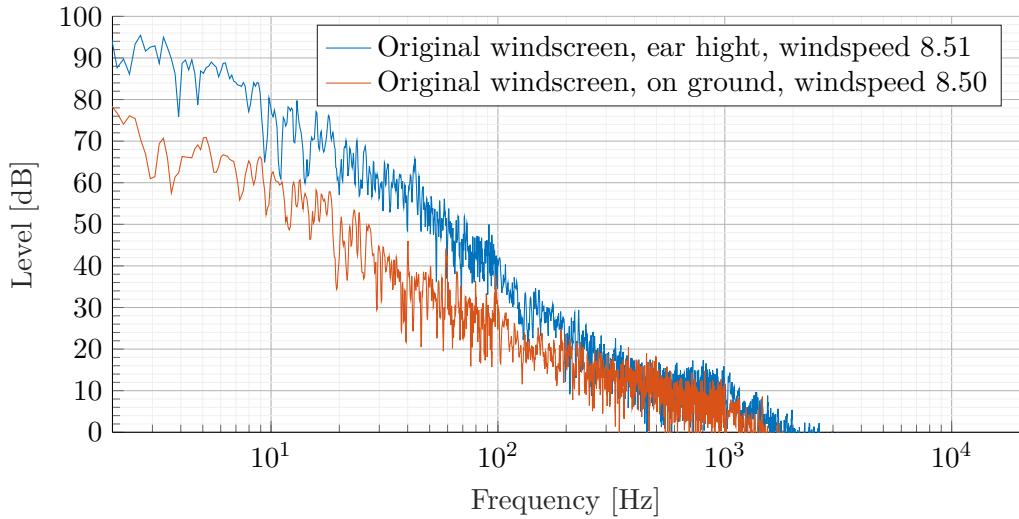


**Figure K.3:** The picture illustrate the area, where the measured is done

## Results

The following graphs shows the result of the measurement.

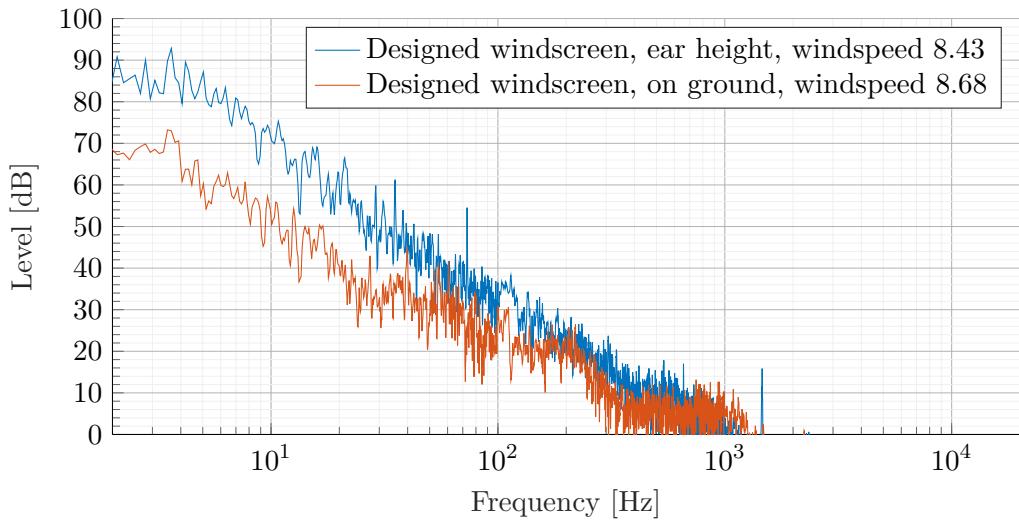
The graph in Figure K.4 shows a measurement where the modified original wind-screen is on the ground and in the hight of 1.7 m.



**Figure K.4:** The graph shows the frequency content of the measurement without the windscreen

As seen in Figure K.4, the wind noise is more than 10 dB SPL lower while the modified original windscreen is moved from the hight of 1.7 m to the ground.

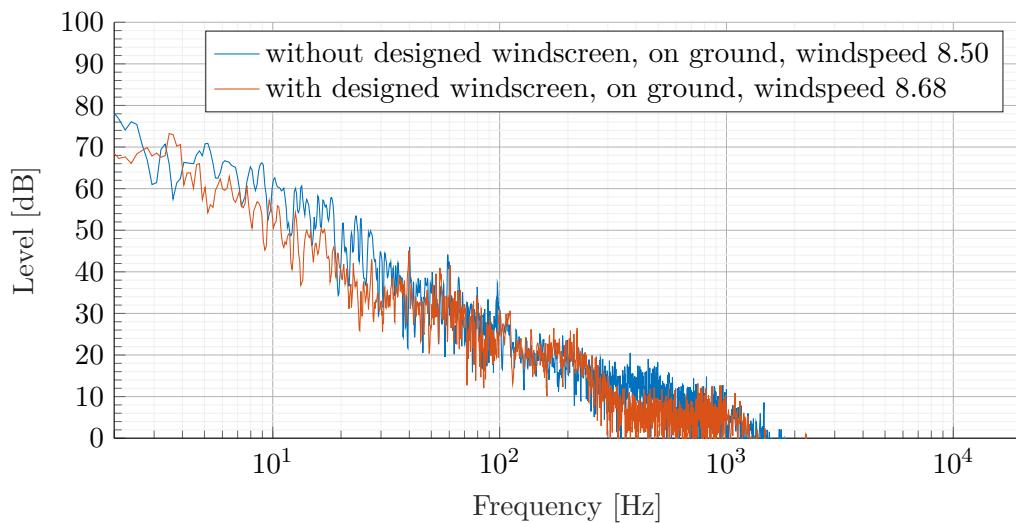
The graph in Figure K.5 shows a measurement where the designed windscreen is on the ground and in the hight of 1.7 m. The windscreen is 90° to the wind in both measurement, which mean that the wind is orthogonal to the middle of the white PVC plate.



**Figure K.5:** The graph shows the frequency content of the measurement without the windscreen

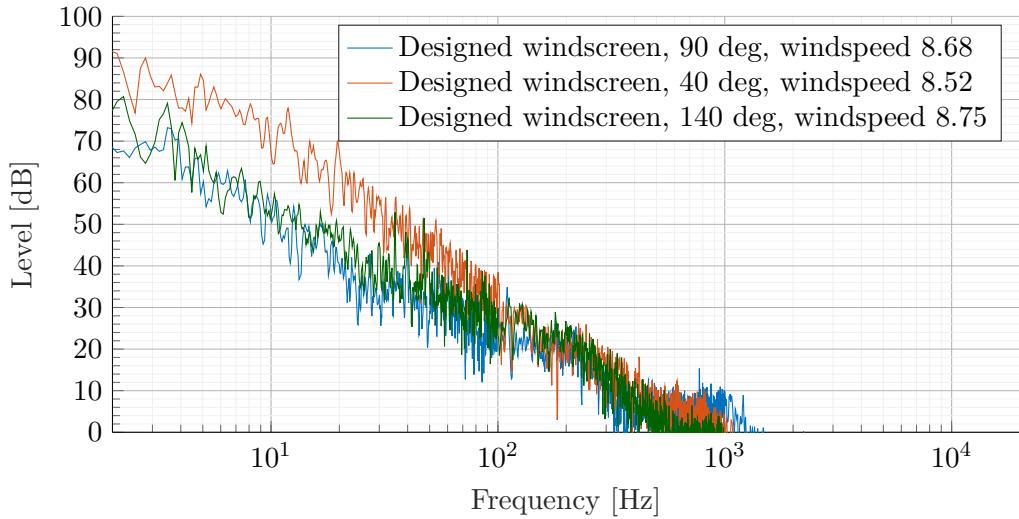
As in Figure K.4 The wind noise is lowered more than 10 dB SPL in Figure K.5. Furthermore, the wind noise is lowered approximately 5 dB SPL to 10 dB SPL from 100 Hz and below while the designed windscreen is used. The highest attenuation is while the the windscreen is lifted above the ground.

Based on the observed ground reflection shown in section 8.1.1 and the high noise differences founded in the above measurement, only the measurement on the ground is shown in the rest of the measurement. The measurement in ear hight is chosen to be irrelevant since the measurement for the final test is done with microphone on the ground. The measurement in the hight of the ear can be founded in the file. The following measurement Figure K.6 shows the measurement with and without the designed windscreen.



**Figure K.6:** The graph shows the frequency content of the measurement without the windscreen

As it is seen in Figure K.6 and explained above, it is clearly seen that the designed windscreen attenuate the wind noise. The next measurement Figure K.7 shows the differences in wind noise while the windscreen is ether rotated 50° to the left and to the right.



**Figure K.7:** The graph shows the frequency content of the measurement without the windscreen

As seen in Figure K.7 the wind noise depend on the angle of the wind to the designed windscreen. While the designed windscreen is rotated  $50^\circ$  to the left, the windscreen does not have any wind noise attenuation compare to the measurement with only the modified windscreen. While the designed windscreen is rotated  $50^\circ$  to the right, the wind noise follows the wind noise while the designed windscreen is non rotated unless around 2 Hz where the noise is 10 dB SPL higher.

## Summary

It is founded that changing the position from the ear hight to the ground is have by it self a wind noise attenuation of more that 10 dB SPL and further the designed windscreen attenuate at less 5 dB SPL more while the designed windscreen is orthogonal to the wind, so non rotated and rotated such that the wind blows to the back of the designed windscreen. While the designed windscreen opening is rotated to the wind, the designed windscreen have no wind noise attenuation.

## Appendix L

### Questionnaire

A questionnaire was made to find the maximum coverage distance for a line array.

Question	Answer	Unit
<i>Company</i>	Profox	
<i>What is the distances between the main stage to the first delay tower at large concert</i>	50	[m]
<i>How many audience attempt to a large concert you produces</i>	15000+	Number
<i>What is the distances between the main stage to the first delay tower at medium concert</i>	30	[m]
<i>How many audience attempt to a medium concert you produces</i>	5000+	Number
<i>Flying hight of top speaker</i>	12 - 16	[m]
<i>Does the wind direction and speed influence on the distance decision</i>	No	
<i>Do you want to know the end result</i>	Yes	

Question	Answer	Unit
<i>Company</i>	Nordic sales	
<i>What is the distances between the main stage to the first delay tower at large concert</i>	75	[m]
<i>How many audience attempt to a large concert you produces</i>	100000+	Number
<i>What is the distances between the main stage to the first delay tower at medium concert</i>	50	[m]
<i>How many audience attempt to a medium concert you produces</i>	30000	Number
<i>Flying hight of top speaker</i>	?	[m]
<i>Does the wind direction and speed influence on the distance decision</i>	Yes	
<i>Do you want to know the end result</i>	No	

Question	Answer	Unit
<i>Company</i>	Moto rental	
<i>What is the distances between the main stage to the first delay tower at large concert</i>	50-60	[m]
<i>How many audience attempt to a large concert you produces</i>	20000+	Number
<i>What is the distances between the main stage to the first delay tower at medium concert</i>	50	[m]
<i>How many audience attempt to a medium concert you produces</i>	5000+	Number
<i>Flying hight of top speaker</i>	12 - 16	[m]
<i>Does the wind direction and speed influence on the distance decision</i>	Yes	
<i>Do you want to know the end result</i>	Yes	

Question	Answer	Unit
<i>Company</i>	Roskilde festival	
<i>What is the distances between the main stage to the first delay tower at large concert</i>	73	[m]
<i>How many audience attempt to a large concert you produces</i>	100000+	Number
<i>What is the distances between the main stage to the first delay tower at medium concert</i>	?	[m]
<i>How many audience attempt to a medium concert you produces</i>	?	Number
<i>Flying hight of top speaker</i>	?	[m]
<i>Does the wind direction and speed influence on the distance decision</i>	No	
<i>Do you want to know the end result</i>	No	
Question	Answer	Unit
<i>Company</i>	AV-center Aalborg	
<i>What is the distances between the main stage to the first delay tower at large concert</i>	60	[m]
<i>How many audience attempt to a large concert you produces</i>	20000+	Number
<i>What is the distances between the main stage to the first delay tower at medium concert</i>	30	[m]
<i>How many audience attempt to a medium concert you produces</i>	5000+	Number
<i>Flying hight of top speaker</i>	14 - 16	[m]
<i>Does the wind direction and speed influence on the distance decision</i>	Yes	
<i>Do you want to know the end result</i>	Yes	
<i>comment: The biggest problem lays in the frequency range from 1.0 kHz to 7.0 kHz where the understanding of the music despisers and the music sound muddy</i>	-	

Question	Answer	Unit
<i>Company</i>	Kinovox	
<i>What is the distances between the main stage to the first delay tower at large concert</i>	60	[m]
<i>How many audience attempt to a large concert you produces</i>	20000+	Number
<i>What is the distances between the main stage to the first delay tower at medium concert</i>	30	[m]
<i>How many audience attempt to a medium concert you produces</i>	10000	Number
<i>Flying hight of top speaker</i>	14 - 16	[m]
<i>Does the wind direction and speed influence on the distance decision</i>	Yes	
<i>Do you want to know the end result</i>	No	
<i>comment: He use to rotate the line array agents the wind if he know that the wind is crosswind and the wind will continue along the concert time. Moreover he would stop the concert if the wind speed is above 10 m/s</i>	-	

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