

MECH 6323 - Robust Control - Midterm Exam

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```
clear
close all
```

Problem 4 - Plane Autopilot System

Controller Definition

Parameters

```
K_a = -1.5e-3;
K_q = -0.32;
a_z = 2;
a_q = 6;
```

State Matrices

```
A_C = [ 0      0
        K_q*a_q 0];
B_C = [ K_a*a_z      0
        K_a*K_q*a_q K_q*a_q];
C_C = [ K_q      1];
D_C = [ K_a*K_q      K_q];
```

System Definition

```
sys_C = ss(A_C, B_C, C_C, D_C)
```

sys_C =

A =

	x1	x2
x1	0	0
x2	-1.92	0

B =

	u1	u2
x1	-0.003	0
x2	0.00288	-1.92

C =

	x1	x2
y1	-0.32	1

D =

	u1	u2
y1	0.00048	-0.32

Continuous-time state-space model.

```
tf_C = tf(sys_C)
```

```
tf_C =
```

```
From input 1 to output:  
0.00048 s^2 + 0.00384 s + 0.00576  
-----  
s^2
```

```
From input 2 to output:  
-0.32 s - 1.92  
-----  
s
```

Continuous-time transfer function.

Plant Definition

Parameters

```
V = 886.78;  
zeta = 0.6;  
omega = 113;
```

Uncertain Coefficients

Nominal Values

```
Z_alpha_0 = -1.3046;  
Z_delta_0 = -0.2142;  
M_alpha_0 = 47.7109;  
M_delta_0 = -104.83436;
```

Uncertain Dynamics

```
Z_alpha = @(k, delta) Z_alpha_0 * (1 + k * delta);  
Z_delta = @(k, delta) Z_delta_0 * (1 + k * delta);  
M_alpha = @(k, delta) M_alpha_0 * (1 + k * delta);  
M_delta = @(k, delta) M_delta_0 * (1 + k * delta);
```

System Matrices

```
A_P = @(Z_alpha, Z_delta, M_alpha, M_delta) [  
    Z_alpha 1 Z_delta    0  
    M_alpha 0 M_delta    0  
    0      0 0          1  
    0      0 -omega^2 -2*zeta*omega  
];  
B_P = [  
    0  
    0  
    0  
    omega^2  
];
```

```

C_P = @(Z_alpha, Z_delta) [
    V*Z_alpha    0    V*Z_delta    0
    0            1    0            0
];
D_P = [
    0
    0
];

```

Nominal System

Nominal System Matrices

```

A_P_0 = A_P(Z_alpha_0, Z_delta_0, M_alpha_0, M_delta_0)

```

```

A_P_0 = 4×4
104 ×
    -0.0001    0.0001    -0.0000    0
     0.0048         0    -0.0105    0
         0         0         0    0.0001
         0         0    -1.2769   -0.0136

```

```

% double(vpa(subs(A_P, ...
%     [Z_alpha, Z_delta, M_alpha, M_delta], ...
%     [Z_alpha_0, Z_delta_0, M_alpha_0, M_delta_0]), 4));
B_P_0 = B_P

```

```

B_P_0 = 4×1
         0
         0
         0
    12769

```

```

% double(vpa(subs(B_P, ...
%     [Z_alpha, Z_delta, M_alpha, M_delta], ...
%     [Z_alpha_0, Z_delta_0, M_alpha_0, M_delta_0]), 4));
C_P_0 = C_P(Z_alpha_0, Z_delta_0)

```

```

C_P_0 = 2×4
103 ×
    -1.1569         0    -0.1899    0
         0     0.0010         0    0

```

```

% double(vpa(subs(C_P, ...
%     [Z_alpha, Z_delta, M_alpha, M_delta], ...
%     [Z_alpha_0, Z_delta_0, M_alpha_0, M_delta_0]), 4));
D_P_0 = D_P

```

```

D_P_0 = 2×1
         0
         0

```

```

% double(vpa(subs(D_P, ...
%     [Z_alpha, Z_delta, M_alpha, M_delta], ...
%     [Z_alpha_0, Z_delta_0, M_alpha_0, M_delta_0]), 4));

```

Nominal State-space System

```
sys_P_0 = ss(A_P_0, B_P_0, C_P_0, D_P_0)
```

```
sys_P_0 =
```

```
A =
      x1      x2      x3      x4
x1      -1.305      1      -0.2142      0
x2      47.71      0      -104.8      0
x3      0      0      0      1
x4      0      0      -1.277e+04      -135.6
```

```
B =
      u1
x1      0
x2      0
x3      0
x4      1.277e+04
```

```
C =
      x1      x2      x3      x4
y1      -1157      0      -189.9      0
y2      0      1      0      0
```

```
D =
      u1
y1      0
y2      0
```

Continuous-time state-space model.

Nominal Transfer Function

```
tf_P_0 = tf(sys_P_0)
```

```
tf_P_0 =
```

```
From input to output...
      -2.425e06 s^2 + 2.585e-08 s + 1.664e09
1:  -----
      s^4 + 136.9 s^3 + 1.29e04 s^2 + 1.019e04 s - 6.092e05

      -1.339e06 s - 1.877e06
2:  -----
      s^4 + 136.9 s^3 + 1.29e04 s^2 + 1.019e04 s - 6.092e05
```

Continuous-time transfer function.

Uncertain System Dynamics

Uncertain Matrices

```
A_P = @(k, Delta) A_P( Z_alpha(k, Delta(1)), ...
                       Z_delta(k, Delta(2)), ...
                       M_alpha(k, Delta(3)), ...
                       M_delta(k, Delta(4)));
C_P = @(k, Delta) C_P( Z_alpha(k, Delta(1)), ...
                       Z_delta(k, Delta(2)));
```

Uncertain System

```
sys_P = @(k, Delta) ss(A_P(k, Delta), B_P, C_P(k, Delta), D_P);
```

Feedback System Definition

Open Loop System: $L(s) = C(s)P(s)$

Nominal

```
sys_L_0 = series(sys_C, sys_P_0)
```

sys_L_0 =

A =

	x1	x2	x3	x4	x5	x6
x1	-1.305	1	-0.2142	0	0	0
x2	47.71	0	-104.8	0	0	0
x3	0	0	0	1	0	0
x4	0	0	-1.277e+04	-135.6	-4086	1.277e+04
x5	0	0	0	0	0	0
x6	0	0	0	0	-1.92	0

B =

	u1	u2
x1	0	0
x2	0	0
x3	0	0
x4	6.129	-4086
x5	-0.003	0
x6	0.00288	-1.92

C =

	x1	x2	x3	x4	x5	x6
y1	-1157	0	-189.9	0	0	0
y2	0	1	0	0	0	0

D =

	u1	u2
y1	0	0
y2	0	0

Continuous-time state-space model.

Uncertain

```
sys_L = @(k, Delta) series(sys_C, sys_P(k, Delta));
```

Closed Loop System: $S(s) = \frac{C(s)P(s)}{1 + C(s)P(s)}$

Nominal

```
sys_S_0 = feedback(sys_L_0, eye(size(C_P_0,1)))
```

sys_S_0 =

A =

	x1	x2	x3	x4	x5	x6
x1	-1.305	1	-0.2142	0	0	0
x2	47.71	0	-104.8	0	0	0

x3	0	0	0	1	0	0
x4	7091	4086	-1.16e+04	-135.6	-4086	1.277e+04
x5	-3.471	0	-0.5698	0	0	0
x6	3.332	1.92	0.5471	0	-1.92	0

B =

	u1	u2
x1	0	0
x2	0	0
x3	0	0
x4	6.129	-4086
x5	-0.003	0
x6	0.00288	-1.92

C =

	x1	x2	x3	x4	x5	x6
y1	-1157	0	-189.9	0	0	0
y2	0	1	0	0	0	0

D =

	u1	u2
y1	0	0
y2	0	0

Continuous-time state-space model.

Uncertain

```
sys_S = @(k, Delta) feedback(sys_L(k,Delta), eye(size(C_P_0,1)));
```

(a)

```
eig_S_0 = eig(sys_S_0)
```

```
eig_S_0 = 6x1 complex
-39.2033 +71.5951i
-39.2033 -71.5951i
-49.2597 + 0.0000i
-1.8309 + 0.0000i
-3.7038 + 1.4953i
-3.7038 - 1.4953i
```

Since $\mathcal{R}(\lambda_i) < 0 \ \forall_i$, the closed loop system $S(s)$ is stable.

```
sys_S_stable = isstable(sys_S_0)
```

```
sys_S_stable = logical
1
```

(b)

Random Testing Code

```
i_worst = 1;
k_try = 10;
N_samples = 10000;
Delta_data = 2 * rand([4, N_samples]) - 1;
```

```

for i = 1:N_samples
    % Better Implimentation
    sys_S_test = @(k) sys_S(k, Delta_data(:,i));
    if isstable(sys_S_test(k_try))
        break
    else
        while ~isstable(sys_S_test(k_try))
            k_try = 0.99 * k_try;
            i_worst = i;
        end
    end
    % Alternative (as described in the problem itself)
    % Delta = Delta_data(:,i);
    % sys_S_unstable = true;
    % while sys_S_unstable
    %     sys_S_test = sys_S(k_try, Delta);
    %     if max(real(eig(sys_S_test))) >= 0
    %         k_try = 0.99 * k_try;
    %         i_worst = i;
    %     else
    %         sys_S_unstable = false;
    %     end
    % end
end
end

```

Random Testing Results

```
k_bar = k_try
```

```
k_bar = 1.1639
```

```
Delta_worst = Delta_data(:,i)
```

```

Delta_worst = 4x1
    0.9599
    0.9308
   -0.6538
   -0.5855

```

Since this gets randomized everytime, \bar{k} changes but often gets down below 1 to 0.7-ish, but also stays at 10 sometimes.

Why must $k_{max} \leq \bar{k}$?

Well, many reasons. We know that k_{max} is the largest possible k that maintains stability of the closed-loop system, and therefore all unstabilizing k due to some disturbance would be greater then the lowest-upper bound on k , i.e. $\bar{k} \geq \sup_k S(s)$ stable. Therefore, $k_{max} = \sup_k S(s) \leq \bar{k}$.

(c)

Uncertain System

Bounded Uncertainty

```
delta_1_u = ureal('delta_1', 0);  
delta_2_u = ureal('delta_2', 0);  
delta_3_u = ureal('delta_3', 0);  
delta_4_u = ureal('delta_4', 0);  
  
Delta_u = [  
    delta_1_u  
    delta_2_u  
    delta_3_u  
    delta_4_u  
];
```

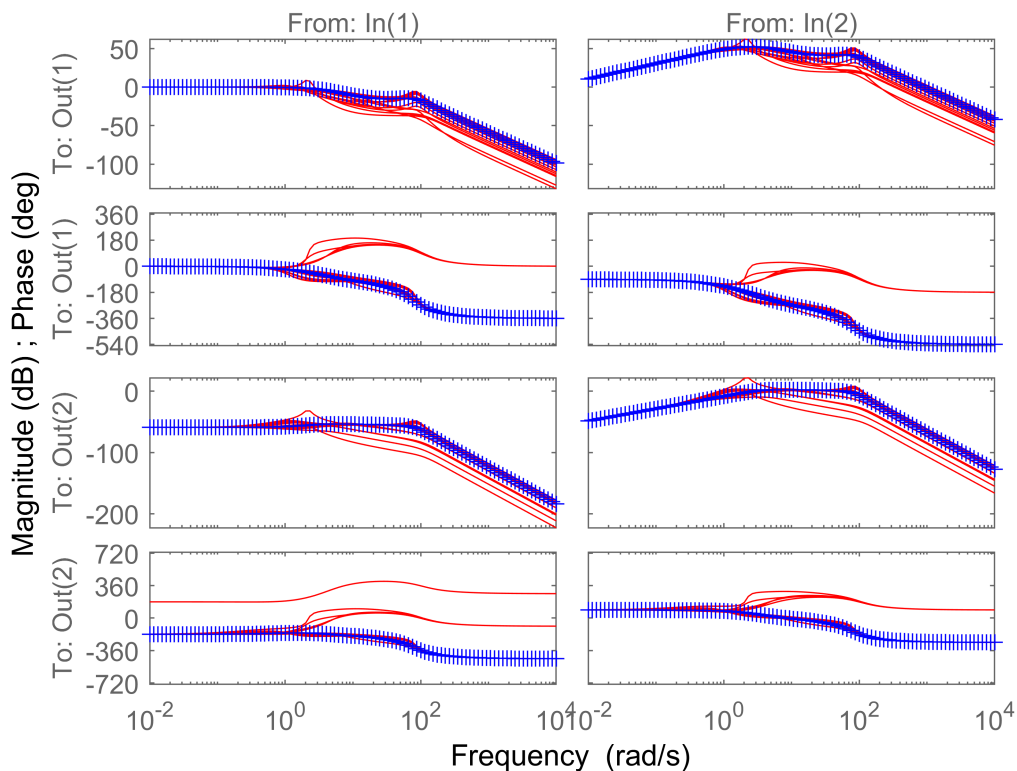
Uncertain SS system

```
sys_S_u = @(k) sys_S(k, Delta_u);
```

Uncertain System Frequency Respons

```
w_min = -2;  
w_max = 4;  
freqs = logspace(w_min,w_max,100);  
sys_S_u_k1 = sys_S_u(1);  
usysfrd = ufrd(sys_S_u_k1, freqs);  
bode(usysfrd, 'r', usysfrd.NominalValue, 'b+')
```

Bode Diagram



robustab

```
opts = robOptions( 'Display','on', ...  
                  'VaryFrequency','on',...  
                  'Sensitivity','on');  
[stabmarg, destabunc, report] = robustab(sys_S_u_k1, opts)
```

```
Computing bounds... Points completed: 42/42  
Computing peak... Percent completed: 100/100  
System is not robustly stable for the modeled uncertainty.  
-- It can tolerate up to 60.3% of the modeled uncertainty.  
-- There is a destabilizing perturbation amounting to 60.4% of the modeled uncertainty.  
-- This perturbation causes an instability at the frequency 3.44 rad/seconds.  
-- Sensitivity with respect to each uncertain element is:  
    3% for delta_1. Increasing delta_1 by 25% decreases the margin by 0.75%.  
    1% for delta_2. Increasing delta_2 by 25% decreases the margin by 0.25%.  
   16% for delta_3. Increasing delta_3 by 25% decreases the margin by 4%.  
   42% for delta_4. Increasing delta_4 by 25% decreases the margin by 10.5%.  
stabmarg = struct with fields:  
    LowerBound: 0.6035  
    UpperBound: 0.6045  
    CriticalFrequency: 3.4386  
destabunc = struct with fields:  
    delta_1: -0.6045  
    delta_2: -0.6045  
    delta_3: 0.6045  
    delta_4: -0.6045  
report = struct with fields:  
    Model: 1  
    Frequency: [44x1 double]  
    Bounds: [44x2 double]  
    WorstPerturbation: [44x1 struct]  
    Sensitivity: [1x1 struct]
```

From this we have $k_{max} \approx 0.6045$ to result in $k * \Delta = 0.6045 * [-1 \ -1 \ 1 \ -1]^T$.

This value is constant with the numerical results as it is below, but not too small by comparison to what is expected.

Additionally, we know that the critical frequency that this is occurring at is

(d)

```
k_max = 0.6045;  
sys_S_critical = sys_S(k_max, [-1; -1; 1; -1])
```

```
sys_S_critical =
```

```
A =  
      x1      x2      x3      x4      x5      x6  
x1    -0.516      1    -0.08472      0      0      0  
x2     76.55      0    -41.46      0      0      0  
x3      0      0      0      1      0      0  
x4     2804    4086 -1.231e+04   -135.6   -4086  1.277e+04  
x5     -1.373      0    -0.2254      0      0      0  
x6      1.318     1.92     0.2164      0    -1.92      0
```

```

B =
      u1      u2
x1      0      0
x2      0      0
x3      0      0
x4  6.129 -4086
x5 -0.003      0
x6 0.00288 -1.92

```

```

C =
      x1      x2      x3      x4      x5      x6
y1 -457.6      0 -75.12      0      0      0
y2      0      1      0      0      0      0

```

```

D =
      u1 u2
y1      0  0
y2      0  0

```

Continuous-time state-space model.

```
tf_S_critical = tf(sys_S_critical)
```

```
tf_S_critical =
```

From input 1 to output...

```

      -460.4 s^4 - 3684 s^3 + 1.46e05 s^2 + 1.212e06 s + 1.818e06
1:  -----
      s^6 + 136.1 s^5 + 1.23e04 s^4 + 1.619e05 s^3 + 2.989e05 s^2 + 1.896e06 s + 1.818e06

      -254.1 s^3 - 2204 s^2 - 4416 s - 2050
2:  -----
      s^6 + 136.1 s^5 + 1.23e04 s^4 + 1.619e05 s^3 + 2.989e05 s^2 + 1.896e06 s + 1.818e06

```

From input 2 to output...

```

      3.07e05 s^4 + 1.842e06 s^3 - 1.01e08 s^2 - 6.061e08 s
1:  -----
      s^6 + 136.1 s^5 + 1.23e04 s^4 + 1.619e05 s^3 + 2.989e05 s^2 + 1.896e06 s + 1.818e06

      1.694e05 s^3 + 1.13e06 s^2 + 6.835e05 s - 5.387e-11
2:  -----
      s^6 + 136.1 s^5 + 1.23e04 s^4 + 1.619e05 s^3 + 2.989e05 s^2 + 1.896e06 s + 1.818e06

```

Continuous-time transfer function.

```
eig_S_critical = eig(sys_S_critical)
```

```

eig_S_critical = 6x1 complex
-60.4635 +82.3580i
-60.4635 -82.3580i
-14.1488 + 0.0000i
 0.0006 + 3.4385i
 0.0006 - 3.4385i
-1.0412 + 0.0000i

```

As can be seen by the eigenvalues at $\lambda_{4,5} = 0.00 \pm j3.44$, the poles of the system cross the $j\omega$ -axis to become unstable at $k_{max} \approx 0.6045$ with $\omega \approx 3.44$. This confirms the robstab estimates to force the system to become unstable at the maximum perturbation of $\Delta = [-1 \ -1 \ 1 \ -1]^T$.