

1. Introduction

$$\begin{aligned}\nabla^2 T(r) &= -\frac{\alpha}{\sqrt{2\pi}r_b^2}e^{-r^2/2r_b^2} \\ \frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial T(r)}{\partial r}\right) &= -\frac{\alpha}{\sqrt{2\pi}r_b^2}e^{-r^2/2r_b^2} \\ \frac{\partial}{\partial r}\left(r\frac{\partial T(r)}{\partial r}\right) &= -\frac{\alpha r}{\sqrt{2\pi}r_b^2}e^{-r^2/2r_b^2}\end{aligned}$$

Integrate both sides and set $a = \alpha/\sqrt{2\pi}$.

$$\begin{aligned}r\frac{\partial T(r)}{\partial r} &= ar_b e^{-r^2/2r_b^2} + C \\ \frac{\partial T(r)}{\partial r} &= \frac{ar_b}{r}e^{-r^2/2r_b^2} + \frac{C}{r}\end{aligned}$$

Integrate again over a region of $0 < r < r_0$:

$$\begin{aligned}T(r')|_r^{r_0} = \Delta T &= \int_r^{r_0} dr' \left(\frac{ar_b}{r'} e^{-r'^2/2r_b^2} + \frac{C}{r'} \right) \\ &= \frac{ar_b}{2} [\text{Ei}(-r_0^2/2r_b^2) - \text{Ei}(-r^2/2r_b^2)] + C \ln(r_0/r)\end{aligned}$$

Or for a uniformly rastered heat load over a circular area radius R

$$\Delta T = \int_r^{r_0} dr \left(\frac{\alpha\Theta(R-r)}{\pi R^2 r} + \frac{C}{r} \right)$$

for $r > R$ this is just $T(r) = C \ln(r/r_0)$. For $r < R$

$$\begin{aligned}T(r) &= \int_r^{r_0} dr \left(\frac{\alpha\Theta(R-r)}{\pi R^2 r} + \frac{C}{r} \right) \\ &= \frac{\alpha}{\pi R^2} \ln(R/r) + C \ln(r_0/r)\end{aligned}$$

Now impose B.C.s $T(r_0) = T_0$.

b

| Source | Value | $\delta P/P(\%)$ |
|----------------------------|---------|------------------|
| Foil Polarization | 0.08005 | 0.57 |
| High Current Extrapolation | — | 0.50 |
| Null Asymmetry (Cu Foil) | 0.00% | 0.22 |
| Beam Bleedthrough | — | 0.18 |
| A_{zz} | 0.75421 | 0.16 |
| Dead Time Correction | 0.148% | 0.15 |
| Other | — | 0.13 |
| Total | | 0.85 |