

4.17 Bar electret from Prob. 4.11 has $\rho_b = 0$: From divergence theorem

$$\int_V (\nabla \cdot \mathbf{D}) d\tau = \oint_S \mathbf{D} \cdot d\mathbf{a} = Q_{\text{free}} = 0 \implies \nabla \cdot \mathbf{D} = 0 \quad (4.22)$$

So, the field lines for \mathbf{D} are closed loops as shown in Fig. 7.1.

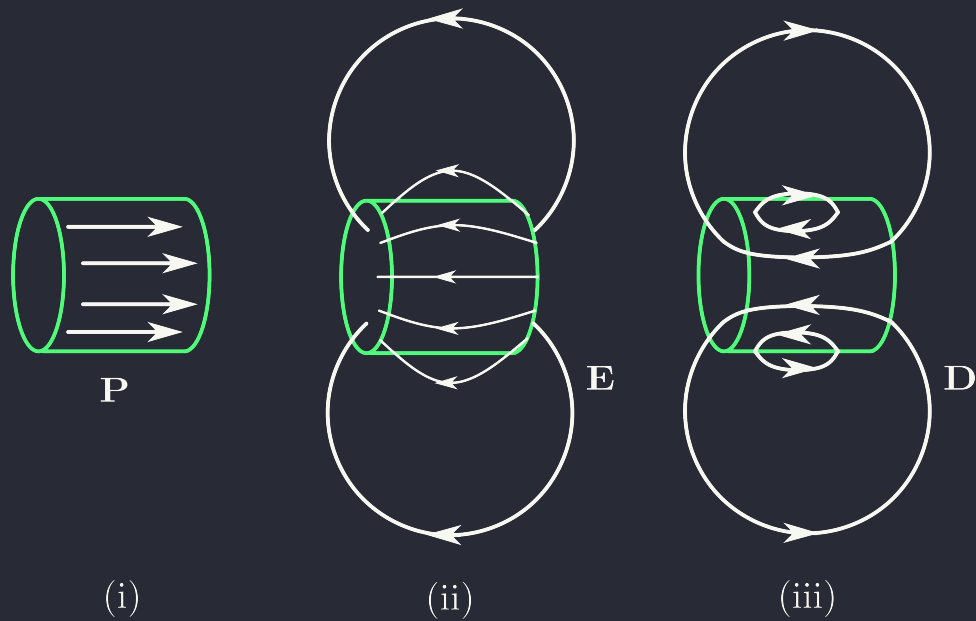


Figure 7.1: Field lines for (i) **P** (ii) **E** (iii) **D**

4.19 For a parallel plate capacitor, the E-field in the air between the plates is two times the E-field of a single plate

(a)

$$\mathbf{E}_{\text{air}} = 2\mathbf{E}_{\text{plate}} = \frac{\sigma}{\epsilon_0} \hat{\mathbf{n}}$$

where $\sigma = \pm Q/A$ is the surface charge density on the plates. The displacement field is

$$\oint \mathbf{D} \cdot d\mathbf{a} = Q_{\text{free}}$$

$$D(A) = \sigma A$$

$$\implies D = \sigma$$

In the linear dielectric medium, \mathbf{D} is proportional to \mathbf{E} by

$$\mathbf{D} = \epsilon \mathbf{E} \quad (4.32)$$

So

$$\implies E = \frac{D}{\epsilon} = \frac{\sigma}{\epsilon}$$

and the potential difference between the plates is the sum of the potential differences in the air and the dielectric

$$\begin{aligned} V &= Ed \\ &= E_{\text{air}}d_{\text{air}} + E_{\text{die}}d_{\text{die}} \\ &= \frac{\sigma}{\epsilon_0} \frac{d}{2} + \frac{\sigma}{\epsilon} \frac{d}{2} \quad \text{using } \sigma = \frac{Q}{A} \\ &= \frac{Qd}{2A\epsilon_0} \left[1 + \frac{\epsilon_0}{\epsilon} \right] \end{aligned}$$

Finally the capacitance of the half filled capacitor (a) is

$$C_a = \frac{Q}{V} = \frac{2A\epsilon_0}{d} \frac{1}{1 + \frac{\epsilon_0}{\epsilon}}$$

Compared to the capacitance of a fully filled capacitor

$$C = \frac{A\epsilon_0}{d} \quad (2.54)$$

So the increase in capacitance is

$$\frac{C_a}{C} = \frac{2}{1 + \frac{\epsilon_0}{\epsilon}}$$

Using the relative permittivity $\epsilon_r = \epsilon/\epsilon_0$, the capacitance of the half filled capacitor (a) increases by a factor of

$$\boxed{\frac{C_a}{C} = \frac{2\epsilon_r}{1 + \epsilon_r}}$$

(i) In air: the E-field increases by the same factor so for a given potential $V = Ed$,

$$\boxed{\mathbf{E}_{\text{air}} = \frac{2\epsilon_r}{1 + \epsilon_r} \frac{V}{d} \hat{\mathbf{n}}}$$

And since $\boxed{\mathbf{P}_{\text{air}} = 0}$ in air, the displacement field $\mathbf{D} = \epsilon_0 \mathbf{E} + \mathbf{P}$ is

$$\boxed{\mathbf{D}_{\text{air}} = \frac{2\epsilon_r}{1 + \epsilon_r} \epsilon_0 \frac{V}{d} \hat{\mathbf{n}}}$$

- (ii) In the dielectric: The E-field in the dielectric is proportional to the E-field in the air (vacuum) by

$$\mathbf{E} = \frac{1}{\epsilon} \mathbf{D} = \frac{1}{\epsilon_r} \mathbf{E}_{\text{vac}} \quad (4.35)$$

so

$$\mathbf{E}_{\text{die}} = \frac{2}{1 + \epsilon_r} \frac{V}{d} \hat{\mathbf{n}}$$

and from (4.35)

$$\begin{aligned} \mathbf{D} &= \epsilon \mathbf{E}, \quad \epsilon = \epsilon_r \epsilon_0 \\ \Rightarrow \mathbf{D}_{\text{die}} &= \frac{2\epsilon_r}{1 + \epsilon_r} \epsilon_0 \frac{V}{d} \hat{\mathbf{n}} = \mathbf{D}_a \end{aligned}$$

Finally, we can find the polarization directly from either (4.21) or

$$\mathbf{P} = \epsilon_0 \chi_e \mathbf{E} = \epsilon_0 (\epsilon_r - 1) \mathbf{E} \quad (4.30)$$

so we might as well use (4.30) and get the polarization in the dielectric as

$$\mathbf{P}_{\text{die}} = \frac{2}{1 + \epsilon_r} \epsilon_0 (\epsilon_r - 1) \frac{V}{d} \hat{\mathbf{n}}$$

- (iii) The free bound surface charge is simply $\sigma_f = D$ so for the top plate

$$\sigma_{f_{\text{top}}} = \frac{2\epsilon_r}{1 + \epsilon_r} \epsilon_0 \frac{V}{d}$$

and $\sigma_{f_{\text{bot}}} = -\sigma_f$ for the bottom plate. And using $\sigma_b = \mathbf{P} \cdot \hat{\mathbf{n}}$ where $\hat{\mathbf{n}}$ points in the negative direction for the top plate, so

$$\sigma_{b_{\text{top}}} = -\frac{2}{1 + \epsilon_r} \epsilon_0 (\epsilon_r - 1) \frac{V}{d} \quad \sigma_{b_{\text{bot}}} = -\sigma_{b_{\text{top}}}$$

- (b) Again, from Gauss's law

$$\begin{aligned} E_{\text{air}} &= \frac{\sigma_{f_{\text{air}}}}{\epsilon_0} \quad \text{and} \quad V = E_{\text{air}} d \\ \Rightarrow \sigma_{f_{\text{air}}} &= \frac{\epsilon_0 V}{d} \end{aligned}$$

for the top plate ($-\sigma_{f_{\text{air}}}$ in the bottom plate) but in the dielectric, using \mathbf{D}

$$\begin{aligned} \oint \mathbf{D} \cdot d\mathbf{a} &= Q_{\text{free}} \\ \Rightarrow D &= \sigma_{f_{\text{die}}} \end{aligned}$$

and from $D = \epsilon E_{\text{die}}$

$$E_{\text{die}} = \frac{\sigma_{f_{\text{die}}}}{\epsilon} = \frac{\sigma_f}{\epsilon_r \epsilon_0}$$

Then using the potential difference $V = E_{\text{die}} d$

$$\Rightarrow \sigma_{f_{\text{die}}} = \epsilon_r \epsilon_0 \frac{V}{d}$$

for the top plate (negative for bottom). From this, we can find the capacitance $C = Q/V$ where

$$\begin{aligned} Q &= \sigma_{f_{\text{air}}} \frac{A}{2} + \sigma_{f_{\text{die}}} \frac{A}{2} \\ &= \frac{\epsilon_0 V A}{2d} + \frac{\epsilon_r \epsilon_0 V A}{2d} \end{aligned}$$

so

$$\implies C = \frac{A\epsilon_0}{2d}(1 + \epsilon_r)$$

From (2.54), the capacitance increases by a factor of

$$\frac{C_b}{C} = \frac{1 + \epsilon_r}{2}$$

(i) The E-field in the air is just the E-field between two plates

$$\mathbf{E}_{\text{air}} = \frac{V}{d} \hat{\mathbf{n}}$$

and $\mathbf{P}_{\text{air}} = 0$ for air thus the displacement field (4.21) $\mathbf{D} = \epsilon_0 \mathbf{E} + 0$, or

$$\mathbf{D}_{\text{air}} = \epsilon_0 \frac{V}{d} \hat{\mathbf{n}}$$

(ii) The E-field in the dielectric using (4.32):

$$\mathbf{E}_{\text{die}} = \frac{1}{\epsilon} \mathbf{D}$$

where $D = \sigma_{f_{\text{die}}}$ so

$$\mathbf{D} = \epsilon_r \epsilon_0 \frac{V}{d} \hat{\mathbf{n}}$$

Then we can use $\epsilon = \epsilon_r \epsilon_0$ so

$$\mathbf{E}_{\text{die}} = \frac{V}{d} \hat{\mathbf{n}} = \mathbf{E}_{\text{air}}$$

Now the polarization is given by (4.30)

$$\mathbf{P}_{\text{die}} = \epsilon_0(\epsilon_r - 1) \frac{V}{d} \hat{\mathbf{n}}$$

Finally, the bound charge is $\sigma_b = \mathbf{P} \cdot \hat{\mathbf{n}}$ so

$$\sigma_{b_{\text{top}}} = -\epsilon_0(\epsilon_r - 1) \frac{V}{d} \quad \sigma_{b_{\text{bot}}} = -\sigma_{b_{\text{top}}}$$

4.37 Between two linear dielectric, show that the E-field lines bend by

$$\frac{\tan \theta_2}{\tan \theta_1} = \frac{\epsilon_2}{\epsilon_1} \quad (4.68)$$

Since $\sigma_f = 0$ so from the boundary conditions

$$D_1^\perp - D_2^\perp = \sigma_b = 0 \implies D_1^\perp = D_2^\perp$$

or from (4.32)

$$D_{y1} = D_{y2} \implies \epsilon_1 E_{y1} = \epsilon_2 E_{y2}$$

Also from the boundary conditions, the parallel components of \mathbf{E} are continuous so

$$E_{x1} = E_{x2} \implies \tan \theta_1 = \frac{E_{y1}}{E_{x1}}, \quad \text{and} \quad \tan \theta_2 = \frac{E_{y2}}{E_{x2}}$$

Thus

$$\begin{aligned} \frac{\tan \theta_2}{\tan \theta_1} &= \frac{E_{y2}/E_{x2}}{E_{y1}/E_{x1}} \\ &= \frac{E_{y2}}{E_{y1}} \quad \text{using} \quad E_{x1} = \frac{\epsilon_2}{\epsilon_1} E_{x2} \\ \frac{\tan \theta_2}{\tan \theta_1} &= \frac{\epsilon_2}{\epsilon_1} \end{aligned}$$

From Snell's Law

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

where a convex lens has $n_2 > n_1$ which makes the angle of refraction smaller than the angle of incidence $\theta_2 < \theta_1$ thus the light ray bends towards the normal or “focuses” the light. For the dielectric interface, its convex lens

$$\epsilon_2 > \epsilon_1 \implies \tan \theta_2 > \tan \theta_1$$

So $\theta_2 > \theta_1$, thus the E-field lines bend away from the normal which will “defocus” the E-field.