

Embedded Wireless Sensor Design for Long Term Structural Health Monitoring

Christopher Bessin², Patrick Blum¹, Matthew P. Iannucci¹, Jordan T. Kirby¹, Zachary McIntosh¹, Elizabeth L. Paul², Michael A. Regan¹, Justin W. Skenyon², Charles J. Wesley¹, and Samuel D. Wiley¹

¹Finite Element Modelling

²Instrumentation Development

May 1, 2014

I have read this paper in its entirety and approve it for submission.

Christopher Bessin

Date

Patrick Blum

Date

Matthew P. Iannucci

Date

Jordan T. Kirby

Date

Zachary McIntosh

Date

Elizabeth L. Paul

Date

Michael A. Regan

Date

Justin W. Skenyon

Date

Charles J. Wesley

Date

Samuel D. Wiley

Date

Contents

1	Introduction	6
1.1	Objectives	6
1.1.1	Phase One	6
1.1.2	Phase Two	6
1.2	Layout	6
2	Finite Element Model (FEM)	7
2.1	Introduction	7
2.1.1	Background of Claiborne Pell Bridge	7
2.1.2	Introduction of FEM	7
2.2	Abaqus FEM Verification	7
2.2.1	L Beam Analysis	7
2.3	Claiborne Pell Bridge Model	7
2.3.1	Modeling Large Suspension Bridges	7
2.3.2	Model Process	7
2.3.3	Limitations of Abaqus FEM	7
3	Instrumentation Package	8
3.1	Introduction	9
3.2	Microprocessor	9
3.2.1	Necessary Specifications	9
3.2.2	Platform Options	9
3.2.3	Final Platform	9
3.3	Sensors	9
3.3.1	Accelerometer	9
3.3.2	Strain Gauge	9
3.3.3	GPS Receiver	9
3.3.4	CORS	9
3.3.5	Analog to Digital Converter	9
3.4	Electronics Design	9
3.4.1	Introduction	9
3.4.2	Circuitry	9
3.4.3	Printed Circuit Board	10
3.5	Software Design	10
3.6	Package Power	10

3.6.1	Power Budget	10
3.6.2	Energy Scavenging Potential	10
3.6.3	Battery Selection	10
4	Data Collection	11
4.1	Phase One Data Collection	11
4.1.1	6g Tri-Axial Accelerometer Data	11
4.2	Phase Two Data Collection	11
4.2.1	6g Tri-Axial Accelerometer Data	11
4.2.2	1.5g Tri-Axial Accelerometer Data	11
4.2.3	Cell Phone Accelerometer	11
4.2.4	Battery Discharge Curve	11
4.2.5	Experimental Observed Efficiency	11
5	Data Analysis	12
5.1	Phase One Data Analysis	12
5.1.1	Comparison of Preliminary Abaqus Model and Preliminary Data . . .	12
5.2	Phase Two Data Analysis	12
5.2.1	Comparison of Developed Abaqus Model with Literature	12
5.2.2	Comparison of Developed Abaqus Model with Developed Abaqus Model	12
6	Future Development	13
6.1	Instrumentation	13
6.1.1	Integration of Strain Gauge	13
6.1.2	Wireless Transmission	16
6.1.3	GPS Time Synchronization	16
6.1.4	Package Assembly	16
6.2	FEM	16
6.2.1	Model Improvements	16
6.2.2	Dynamic Loading	16
7	Conclusion	19
A	Sensor Package Schematics	20

List of Figures

6.1	Omega 3-Element Rosette with pre-soldered leads.	14
6.2	Proposed Package Mounting Location.	15
6.3	Neodymium Mounting Magnet.	17
6.4	Proposed Location for Sensor Package, Wind Turbine and Solar Panels.	18
A.1	Schematic of BeagleBone Black	21
A.2	Schematic of Copernicus II GPS Receiver	22
A.3	Schematic of four ADS1113 ADC units in parallel	23
A.4	Schematic of 5V and 3.3V voltage regulator circuit	24
A.5	Schematic of MMA7361 $\pm 1.5g$ / $\pm 6g$ Tri-Axial Accelerometer	25

List of Tables

Chapter 1

Introduction

1.1 Objectives

1.1.1 Phase One

1.1.2 Phase Two

1.2 Layout

Chapter 2

Finite Element Model (FEM)

2.1 Introduction

2.1.1 Background of Claiborne Pell Bridge

2.1.2 Introduction of FEM

2.2 Abaqus FEM Verification

2.2.1 L Beam Analysis

2.3 Claiborne Pell Bridge Model

2.3.1 Modeling Large Suspension Bridges

2.3.2 Model Process

2.3.3 Limitations of Abaqus FEM

Chapter 3

Instrumentation Package

3.1 Introduction

3.2 Microprocessor

3.2.1 Necessary Specifications

3.2.2 Platform Options

3.2.3 Final Platform

3.3 Sensors

3.3.1 Accelerometer

Necessary Specifications

Sensor Options

Sensor Selection

3.3.2 Strain Gauge

Necessary Specifications

Sensor Options

Sensor Selection

3.3.3 GPS Receiver

Necessary Specifications

Sensor Options

Sensor Selection

3.3.4 CORS

3.3.5 Analog to Digital Converter

Necessary Specifications

Platform Options

3.4.3 Printed Circuit Board

3.5 Software Design

3.6 Package Power

3.6.1 Power Budget

3.6.2 Energy Scavenging Potential

Wind Potential

Solar Potential

3.6.3 Battery Selection

Chapter 4

Data Collection

4.1 Phase One Data Collection

4.1.1 6g Tri-Axial Accelerometer Data

4.2 Phase Two Data Collection

4.2.1 6g Tri-Axial Accelerometer Data

4.2.2 1.5g Tri-Axial Accelerometer Data

4.2.3 Cell Phone Accelerometer

4.2.4 Battery Discharge Curve

4.2.5 Experimental Observed Efficiency

Chapter 5

Data Analysis

5.1 Phase One Data Analysis

5.1.1 Comparison of Preliminary Abaqus Model and Preliminary Data

5.2 Phase Two Data Analysis

5.2.1 Comparison of Developed Abaqus Model with Literature

5.2.2 Comparison of Developed Abaqus Model with Developed Abaqus Model

Chapter 6

Future Development

6.1 Instrumentation

6.1.1 Integration of Strain Gauge

Integration of Strain Gauge

Figure 6.1 is one of the 3-element rosette strain gauges with pre-soldered ribbon leads. Purchased from omega engineering with model number SGD-6/120RYT23. These strain gauges were necessary after realizing the difficulty of soldering leads to the original set of strain gauges. The pre-soldered ribbon leads on the second set of strain gauges also proved to be unsuccessful during experimentation. This was because the leads would not stay secured to the attaching clips while tests were being run. Even with the persistent attempts to get the strain gauges connected and working correctly, the data received was still very inaccurate. One possible contributing factor to this may have been the lack of precision when applying the strain gauge to the exact location on the beam. However, one definite factor that contributed to the inaccurate data from the strain gauges was the type of strain gauge that was used. A strain gauge with a different gauge factor and a higher resistance would have been more favorable. The higher the resistance of a strain gauge, the higher the sensitivity. The original sets of strain gauges had a resistance of 120Ω , but to precisely measure strain on a beam the resistance must be much higher, 350Ω or more. The costs for a pack of 6 similar strain gauges with a resistance of 350Ω from omega engineering is one hundred dollars. Another factor that halted the efforts to apply the strain gauge was that they required another ADC output. It is possible to make more outputs, however this also demands that the time synchronization is even more accurate. Nevertheless, higher resistant strain gauges would be better for sensor packages for future developments.

Package Assembly

Package Location Figure 6.2 is an abaqus visualization of the Newport Bridge with the proposed location for the sensor package to be mounted. As shown in the figure, the center of the bridge is the best location for the sensor package. This is because the greatest amplitude of displacement will occur during the first mode of vibration at the middle of the bridge.

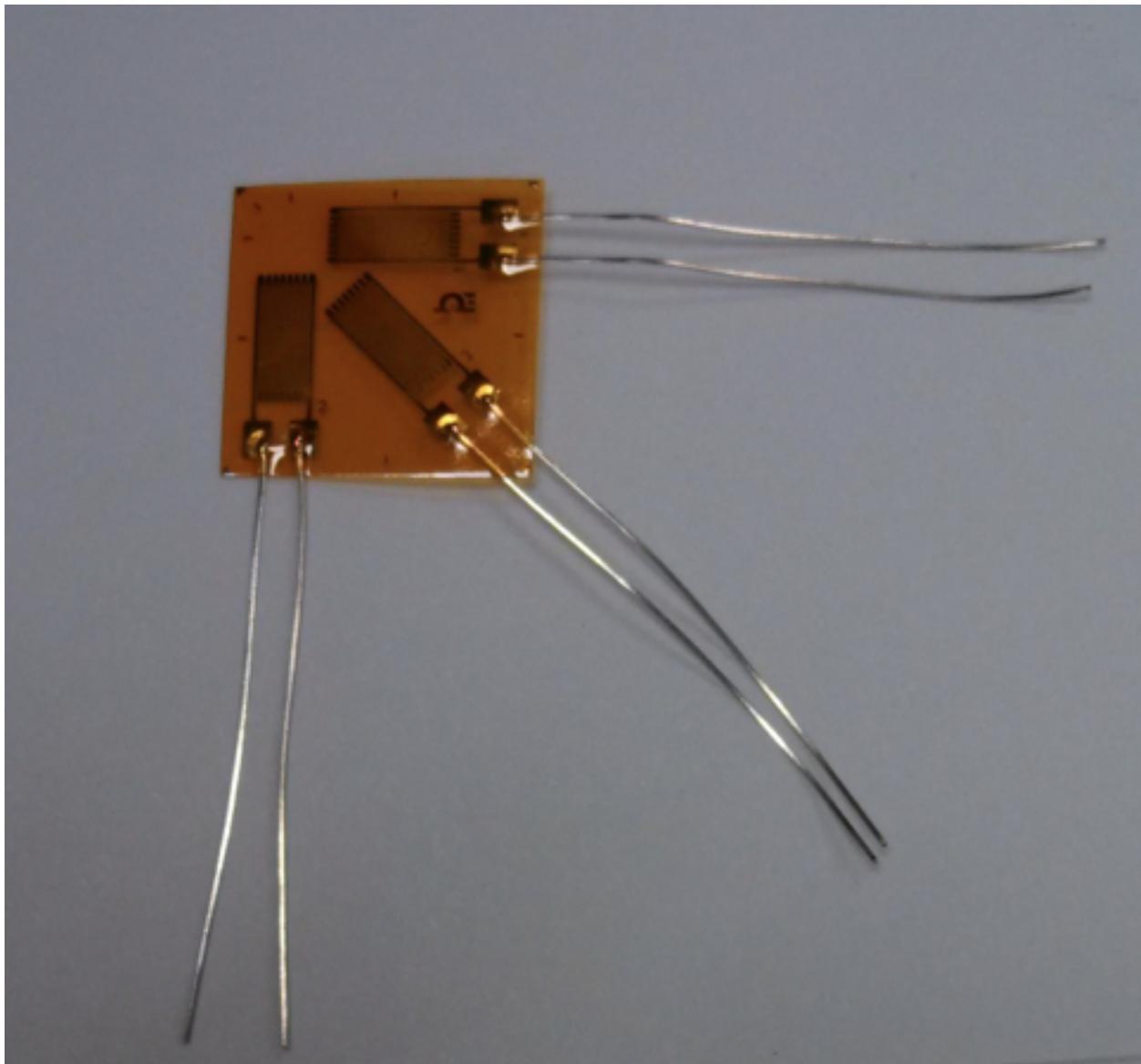


Figure 6.1: Omega 3-Element Rosette with pre-soldered leads.

Mounting the sensor package to the bridge must be done without damaging the structure in any way. The sensor package must also be capable of being moved easily. Most importantly, the package must be secured without any of its own motion, this is so that the sensors can recognize the movement of the bridge and not the package itself. The most economical way of securing the sensor package to the bridge is to use powerful magnets. Neodymium Magnets are strong magnets that work well in all environments and resist demagnetization. One negative aspect of the magnets is that it can be prone to corrosion if not protected with a coating properly. There is also a concern that the magnetic field can disrupt the electronics within the case. However, these issues can be prevented if the correct precautions are taken. The magnets come in many shapes and sizes, shown in Figure 6.2 one can see that the magnets can be bought with pre made holes for screws for mounting to the package.

The magnets in figure 6.2 are model MMR-A-XC from KJMagnetics.com. This magnet is hardly larger than a penny, yet it can easily be screwed into the sensor package and pull a force of 54.14 pounds. With two of these magnets screwed into the sensor package the package would be secured to the bridge. If calculations are run to prove the wind speed on the surface of the package to be too much for this pull force, stronger magnets are available. KJMagnetics.com also has similar magnets but with different pull forces ranging from 26.8 pounds to 260 pounds. These magnets can be used for securing the solar panels and wind turbine as well. Figure 6.4 shows a practicable location for the sensor package along with the solar panels above and the wind turbine hanging just below. The sensor package should be mounted on the outside of one of the major vertical beams at midspan of the bridge. The solar panels and wind turbine must be mounted close within a reasonable distance to keep the cable length to a minimum. The best place to mount the solar panels is on top of the upper horizontal beam on the southern side of the bridge. This will allow for the most amount of sun light and the shortest amount of cable necessary. The best place to mount the wind turbine is on the bottom of the lower horizontal beam on the southern side of the bridge. This location has plenty of wind because it is above the middle of the Narragansett Bay. By mounting the sensor package, solar panels and wind turbine below the deck on the southern side of the bridge the package will be capable of producing its own power and accurately measuring the vibrations of the bridge.

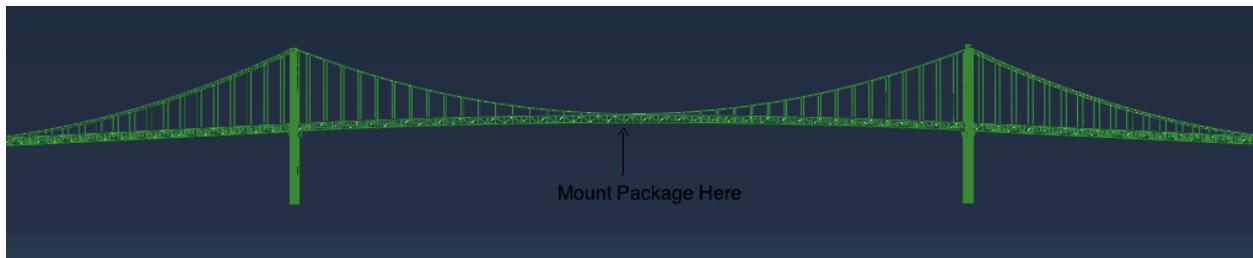


Figure 6.2: Proposed Package Mounting Location.

6.1.2 Wireless Transmission

6.1.3 GPS Time Synchronization

6.1.4 Package Assembly

Fabrication of Circuit Board

Battery Integration

Package Enclosure

Power Management

Package Location

6.2 FEM

6.2.1 Model Improvements

6.2.2 Dynamic Loading

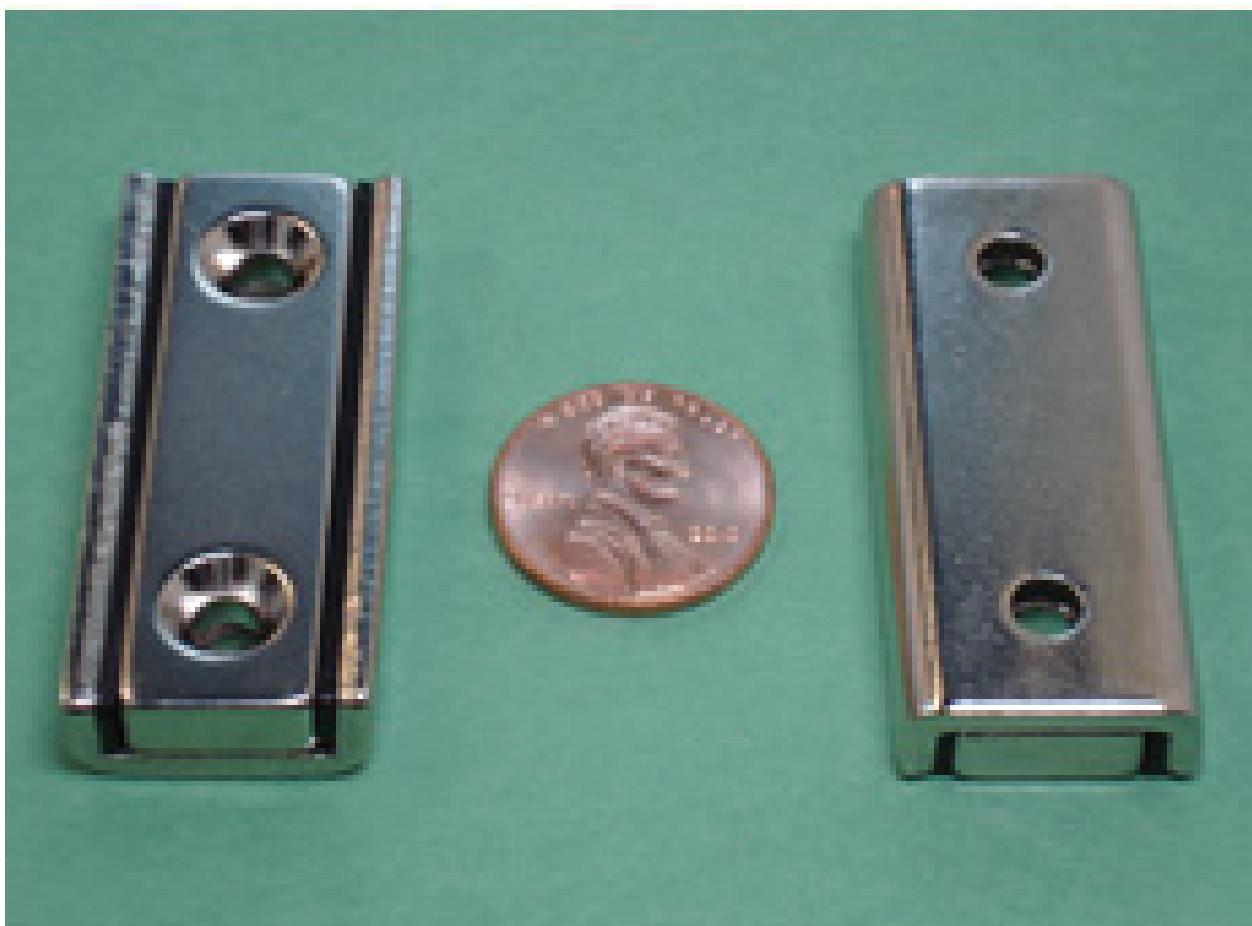
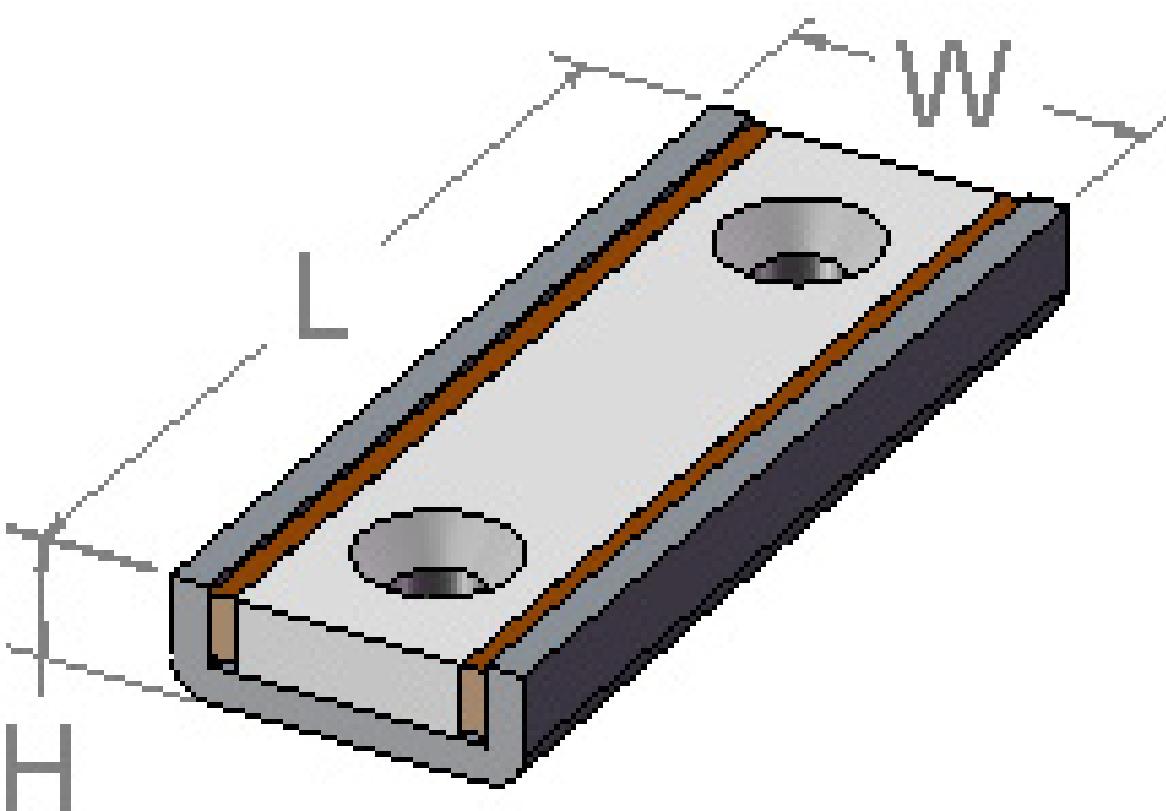




Figure 6.4: Proposed Location for Sensor Package, Wind Turbine and Solar Panels.

Chapter 7

Conclusion

Appendix A

Sensor Package Schematics

BeagleBone Black Block

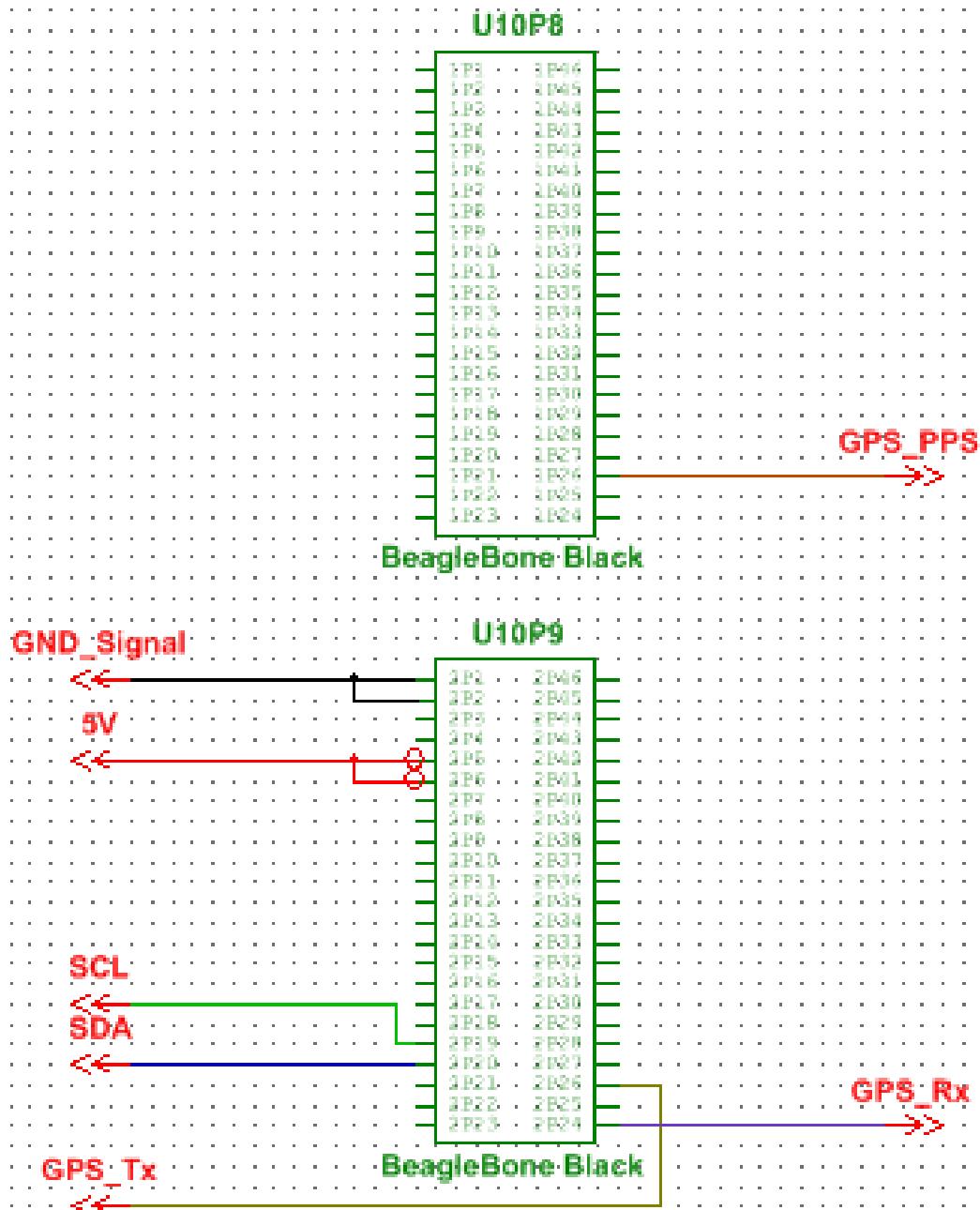


Figure A.1: Schematic of BeagleBone Black

Copernicus II GPS Block

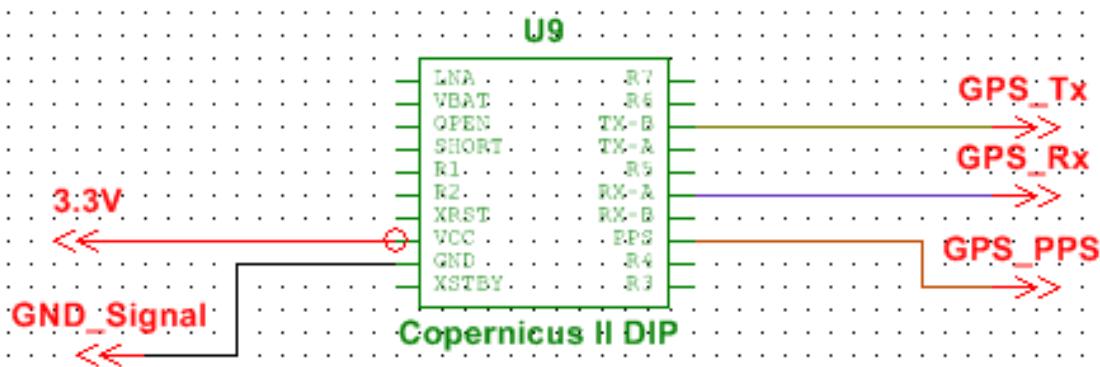


Figure A.2: Schematic of Copernicus II GPS Receiver

ADS1113 ADC Block

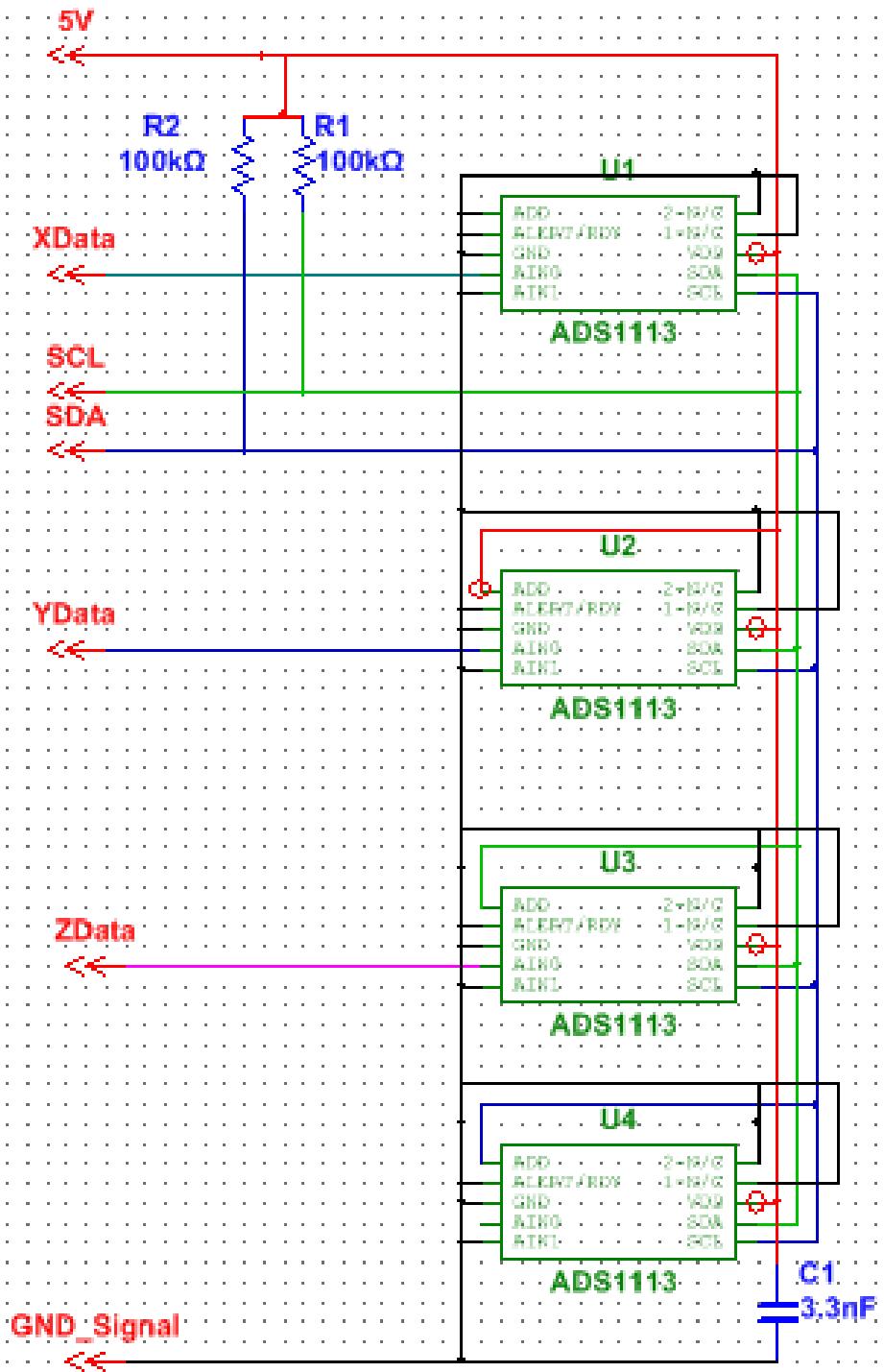


Figure A.3: Schematic of four ADS1113 ADC units in parallel

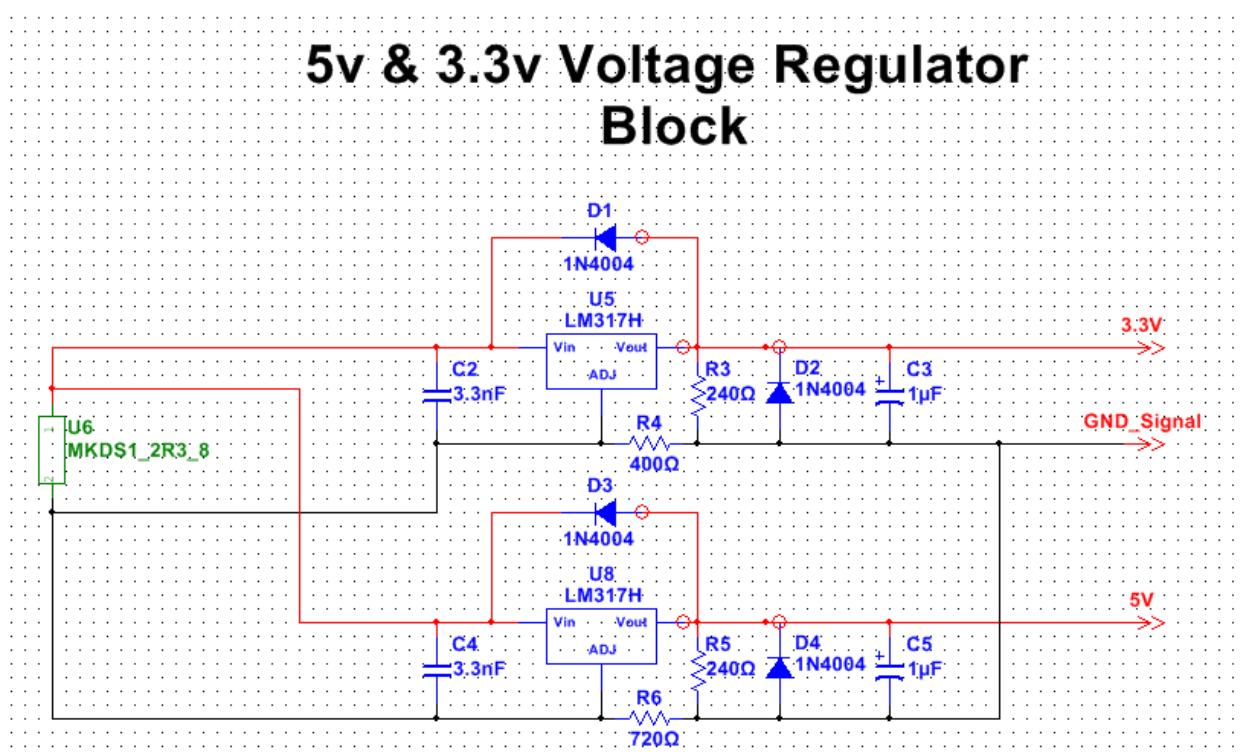


Figure A.4: Schematic of 5V and 3.3V voltage regulator circuit

MMA7361 1.5/6g Accelerometer Block

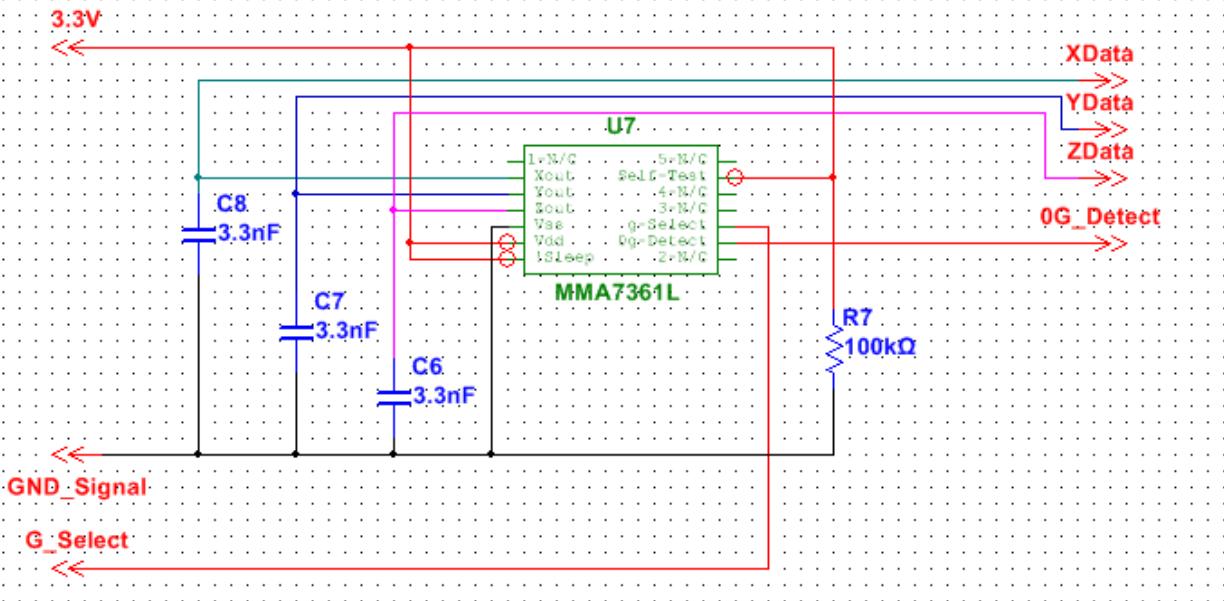


Figure A.5: Schematic of MMA7361 $\pm 1.5g$ / $\pm 6g$ Tri-Axial Accelerometer