

COM303: Digital Signal Processing

Lecture 11: z -transform, filter structures and design examples

Overview

- ▶ the z -transform
- ▶ filtering algorithms and filter structures
- ▶ intuitive filter design
- ▶ two more ideal filters

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the *z*-transform

Overview:

- ▶ Constant-Coefficient Difference Equations
- ▶ The z -transform
- ▶ System transfer function
- ▶ Region of convergence and system stability

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The most general LTI systems

- ▶ ideal filters cannot be implemented
- ▶ what is the most general, realizable LTI transformation?
 - linearity: only sums and multiplications
 - time-invariance: only multiplications by constants
 - realizability: only finite number of past and future samples

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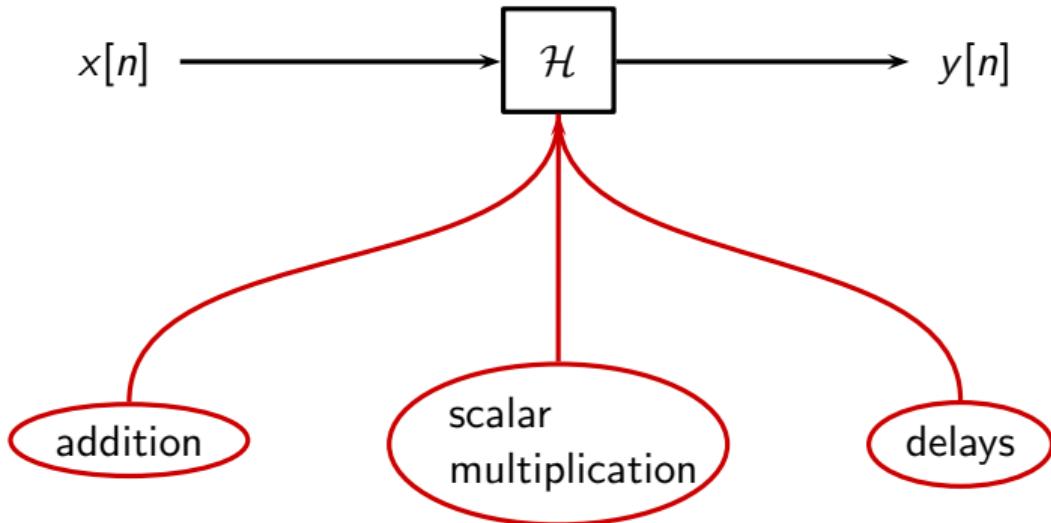
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Linear, time-invariant systems



Constant-Coefficient Difference Equation

$$\sum_{k=0}^N a_k y[n-k] = \sum_{k=0}^M b_k x[n-k]$$

- ▶ uses $M + 1$ input and N output values
- ▶ $a_0 = 1$ (otherwise renormalize)
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Examples:

- ▶ moving average:

$$y[n] = (1/4)x[n] + (1/4)x[n - 1] + (1/4)x[n - 2] + (1/4)x[n - 3]$$

- ▶ leaky integrator:

$$y[n] = \lambda y[n - 1] + (1 - \lambda)x[n]$$

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$$y[n] = \sum_{k=0}^M b_k x[n - k] - \sum_{k=1}^N a_k y[n - k]$$

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- ▶ provides an *algorithm* to compute each output value
- ▶ how do we compute the frequency response? Well, it's the DTFT of...
- ▶ how do we compute the impulse response?

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Apparently unrelated topic: Polynomial Multiplication

$$\begin{aligned}(1 + 3t + 2t^2)(2 + t - t^2 + 4t^3) &= 2 + \quad t - \quad t^2 + 4t^3 \\ &\quad + 6t + 3t^2 - 3t^3 + 12t^4 \\ &\quad + 4t^2 + 2t^3 - 2t^4 \quad + 8t^5 \\ &= 2 + 7t + 6t^2 + 3t^3 + 10t^4 + 8t^5\end{aligned}$$

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Now try this...

$$[\dots \ 1 \ 3 \ 2 \ 0 \ 0 \ \dots] * [\dots \ 2 \ 1 \ -1 \ 4 \ 0 \ \dots] =$$
$$[\dots \ 2 \ 7 \ 6 \ 3 \ 10 \ 8 \ 0 \ \dots]$$

Polynomial multiplication and convolution are the same

$$p(t) = p_0 + p_1 t + \dots + p_P t^P$$

$$q(t) = q_0 + q_1 t + \dots + q_Q t^Q$$

$$r(t) = p(t) \cdot q(t) = \sum_{n=0}^{P+Q} r_n t^n$$

$$r_n = \sum_{k=\max\{0, n-Q\}}^{\min\{n, P\}} p_k q_{n-k}, \quad 0 \leq n \leq P+Q$$

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$$y[n] = \sum_{k=-\infty}^{\infty} x[k]h[n-k]$$

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The z-transform

$$X(z) = \sum_{n=-\infty}^{\infty} x[n]z^{-n}, \quad z \in \mathbb{C}$$

- ▶ associate a power series (i.e. a polynomial) to a sequence
- ▶ for us mostly a *formal operator*...
- ▶ ...but also as the extension of the DTFT to the whole complex plane:

$$X(z)|_{z=e^{j\omega}} = \text{DTFT}\{x[n]\}$$

- ▶ (and now the notation $X(e^{j\omega})$ should make more sense)

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the z -transform is a power *series*

we should (and will) be concerned about its convergence

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Key properties

linearity:

$$\mathcal{Z}\{\alpha x[n] + \beta y[n]\} = \alpha X(z) + \beta Y(z)$$

time shift:

$$\mathcal{Z}\{x[n - N]\} = z^{-N}X(z)$$

convolution:

$$\mathcal{Z}\{h[n] * x[n]\} = H(z)X(z)$$

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Convolution in the z -domain

Consider an LTI system with impulse response $h[n]$

$$y[n] = h[n] * x[n]$$

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Now let's go back to where we started...

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- ▶ causal formulation
- ▶ provides an *algorithm* to compute each output value
- ▶ the frequency response is the DTFT of the impulse response
- ▶ how do we compute the impulse response from the CCDE?

Applying the z -transform to CCDE's

$$\sum_{k=0}^N a_k y[n-k] = \sum_{k=0}^M b_k x[n-k]$$

$$Y(z) \sum_{k=0}^N a_k z^{-k} = X(z) \sum_{k=0}^M b_k z^{-k}$$

$$H(z) = \frac{Y(z)}{X(z)} = \frac{\sum_{k=0}^M b_k z^{-k}}{1 + \sum_{k=1}^N a_k z^{-k}}$$

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Rational Transfer Function

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Leaky Integrator revisited

► CCDE: $y[n] = (1 - \lambda)x[n] + \lambda y[n - 1]$

► impulse response: $h[n] = (1 - \lambda)\lambda^n u[n]$

► transfer function from impulse response

$$H(z) = (1 - \lambda) \sum_{n=0}^{\infty} \lambda^n z^{-n} = \frac{(1 - \lambda)}{1 - \lambda z^{-1}}$$

► transfer function from CCDE:

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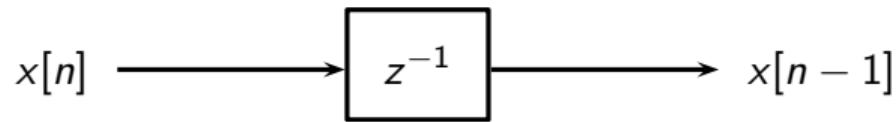
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BTW, remember the delay block?



$$Y(z) = z^{-1} X(z)$$

now the notation should make more sense!

Existence and region of convergence (ROC)

ROC is defined by the absolute convergence of the power series:

$$z \in \text{ROC}\{X(z)\} \iff \sum_{n=-\infty}^{\infty} |x[n]z^{-n}| < \infty$$

How can we determine the ROC?

- ▶ ROC depends on the values of $x[n]$
- ▶ for rational transfer function we can use indirect methods
- ▶ we don't care about convergence in zero and infinity

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Region of convergence (ROC)

observation #1:

for finite-support signals, the z -transform converges everywhere (except in 0 and/or ∞)

$$X(z) = \sum_{n=-M}^N x[n]z^{-n}$$

Region of convergence (ROC)

observation #2:

the region of convergence has circular symmetry: set $z = ae^{j\theta}$:

$$\sum_{n=-\infty}^{\infty} |x[n]z^{-n}| < \infty \iff \sum_{n=-\infty}^{\infty} |x[n]| |a^{-n}| < \infty$$

Region of convergence (ROC)

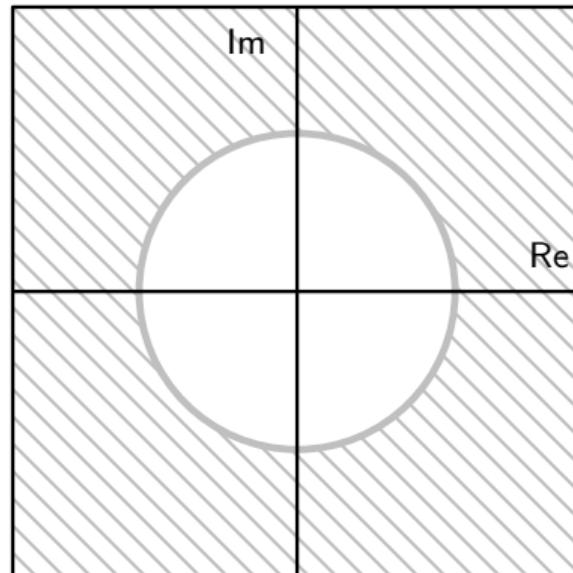
observation #3:

for causal sequences, the ROC extends from a circle to infinity:

assume $z_0 \in \text{ROC}$ and $|z_1| > |z_0|$:

$$\sum_{n=0}^{\infty} |x[n] z_1^{-n}| = \sum_{n=0}^{\infty} \frac{|x[n]|}{|z_1^n|} \leq \sum_{n=0}^{\infty} \frac{|x[n]|}{|z_0^n|} \leq \infty$$

ROC shape for causal sequences



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so where are the convergence problems?

in general, difficult question; but we're only interested in rational transfer functions!

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ROC for causal systems

Consider the transfer function for an LTI system:

$$H(z) = \frac{b_0 + b_1 z^{-1} + \dots + b_M z^{-M}}{1 + a_1 z^{-1} + \dots + a_N z^{-N}}$$

It can always be factored as:

$$H(z) = b_0 \frac{\prod_{n=1}^M (1 - z_n z^{-1})}{\prod_{n=1}^N (1 - p_n z^{-1})}$$

ROC for causal systems

- ▶ z_n 's: zeros of the transfer function
- ▶ p_n 's: poles of the transfer function
- ▶ only trouble spots for ROC are the poles

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ROC extends outwards from a circle touching the largest-magnitude pole

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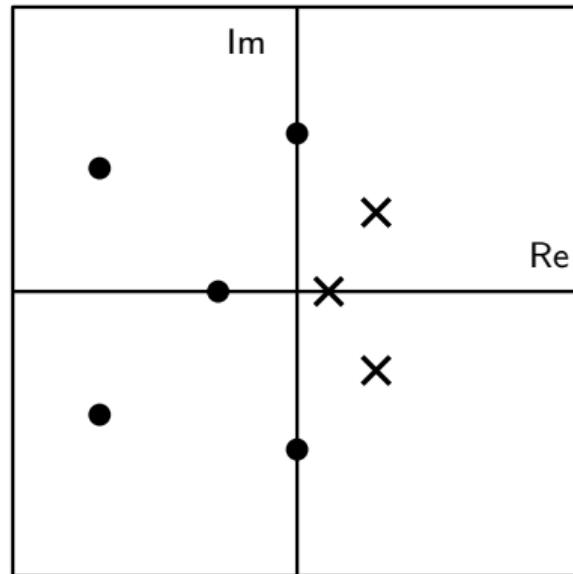
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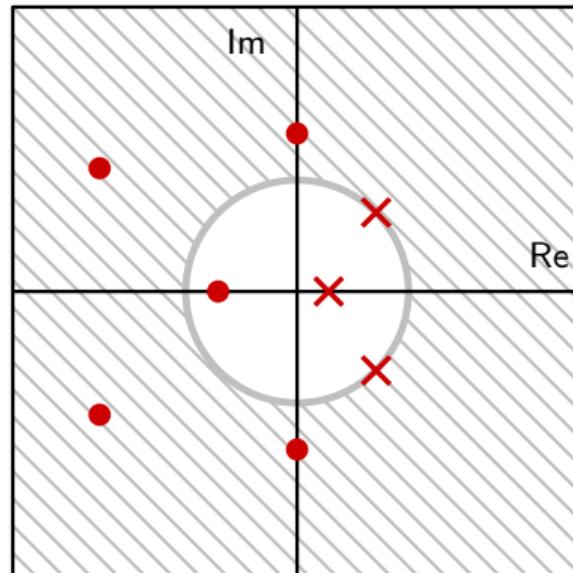
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ROC for causal systems - Proof (sketch)

- ▶ $H(z) = B(z)(1/A(z))$
- ▶ with no loss of generality, assume $B(z) = 1$
- ▶ assume all poles distinct
- ▶ use partial fraction decomposition:

$$H(z) = \prod_{k=0}^{N-1} \frac{1}{(1 - p_k z^{-1})} = \sum_{k=0}^{N-1} \frac{c_k}{(1 - p_k z^{-1})}$$

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ROC for causal systems - Proof (sketch)

Example:

$$\begin{aligned}\frac{1}{1 - 5z^{-1} + 6z^{-2}} &= \frac{1}{(1 - 2z^{-1})(1 - 3z^{-1})} \\ &= \frac{c_0}{1 - 2z^{-1}} + \frac{c_1}{1 - 3z^{-1}}\end{aligned}$$

$$c_0 + c_1 = 1$$

$$2c_0 + 3c_1 = 0$$

$$\frac{1}{1 - 5z^{-1} + 6z^{-2}} = \frac{-2}{1 - 2z^{-1}} + \frac{3}{1 - 3z^{-1}}$$

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$$H(z) = \prod_{k=0}^{N-1} \frac{1}{(1 - p_k z^{-1})} = \sum_{k=0}^{N-1} \frac{c_k}{(1 - p_k z^{-1})}$$

- ▶ remember the leaky integrator...
- ▶ each term corresponds to an exponential sequence:

$$\mathcal{Z}\{p_k^n u[n]\} = \frac{1}{(1 - p_k z^{-1})}$$

- ▶ the ROC for each term is $|z| > |p_k|$
- ▶ intersection of all ROCs is $|z| > |p_{\max}|$

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ROC for causal systems - Proof (sketch)

- ▶ same for multiple poles, just more tedious

$$\mathcal{Z}\{np^n u[n]\} = \frac{pz^{-1}}{(1-pz^{-1})^2}, \quad \text{ROC: } |z| > |p|$$

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- ▶ we could use an inverse z-transform to obtain $h[n]$

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System stability criterion

Consider a filter with impulse response $h[n]$

- ▶ BIBO stability $\iff \sum_{n=-\infty}^{\infty} |h[n]| < \infty$
- ▶ $1 \in \text{ROC} \iff \sum_{n=-\infty}^{\infty} |h[n]| < \infty$ because $H(z)$ converges absolutely in $z = 1$

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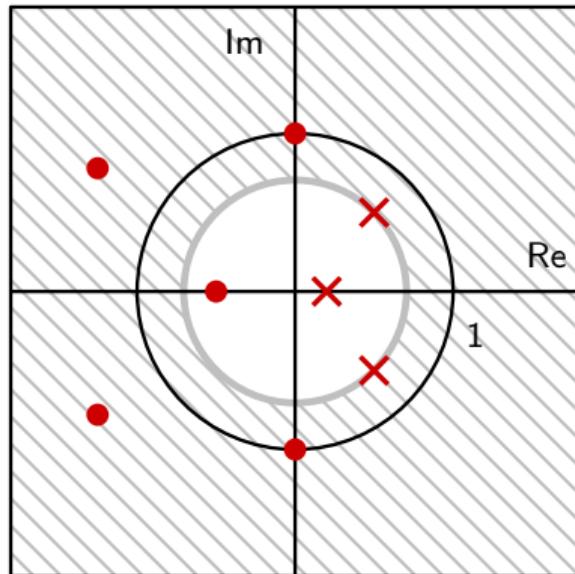
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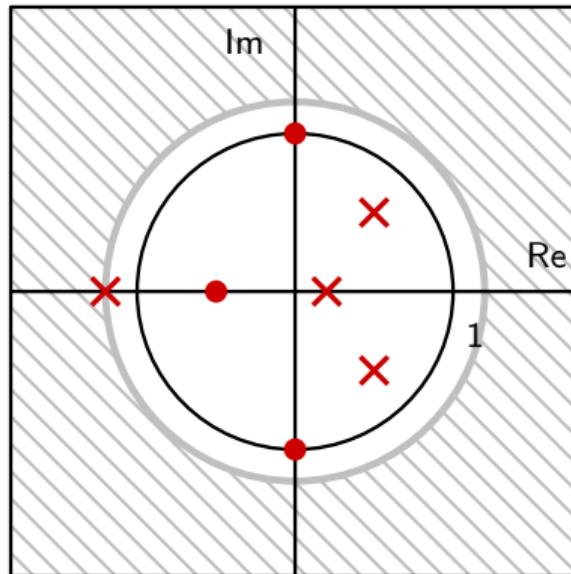
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Stable system



Unstable system



Common confusion...

$$y[n] = 2y[n - 1] + x[n] \quad (\text{unstable!})$$

apply z -transform as a formal operator:

$$H(z) = Y(z)/X(z) = \frac{1}{1 - 2z^{-1}}$$

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Common confusion clarified

ROC depends on $h[n]$, NOT on *formal* value of $H(z)$:

- ▶ $h[n] = 2^n u[n]$
- ▶ to apply the z -transform operator we *assume* to be in the ROC
- ▶ the region of convergence is $|z| > 2$ because

$$\sum_{n=0}^{\infty} a^n z^{-n} = \lim_{N \rightarrow \infty} \frac{1 - (a/z)^N}{1 - (a/z)} = \begin{cases} \frac{1}{1 - az^{-1}} & \text{if } |z| > |a| \\ \infty & \text{otherwise} \end{cases}$$

In other words...

the function $\frac{1}{1 - az^{-1}}$ is defined for all $z \in \mathbb{C} \setminus \{a\}$

BUT

it is the z -transform of $a^n u[n]$ *only* for $|z| > |a|$

Rational Transfer Function

for which values of z does a rational $H(z)$ exist?

- ▶ option 1: compute $h[n]$ explicitly and find ROC for the power series $\sum h[n]z^{-n}$
- ▶ option 2: derive ROC indirectly:
 - ROC is circular symmetric
 - ROC extends outwards for causal sequences
 - ROC cannot include poles

Estimating the frequency response from the pole-zero plot

The “circus tent” method:

- ▶ magnitude of z transform is like a rubber sheet over the complex plane
- ▶ zeros glue the sheet to the ground
- ▶ poles are like ... poles, pushing it up
- ▶ frequency response (in magnitude) is sheet profile around the unit circle

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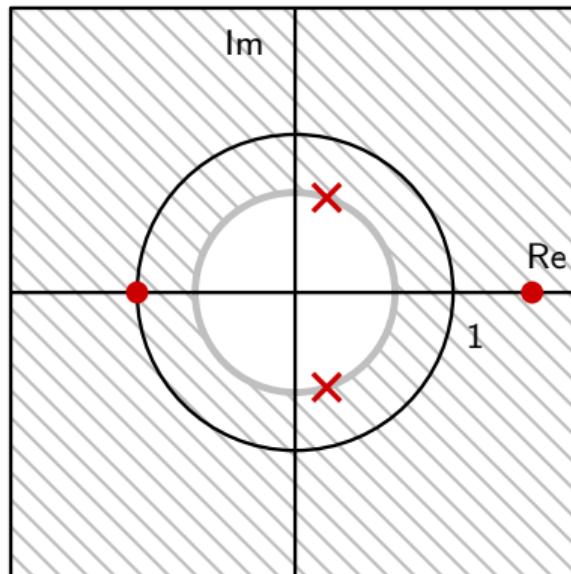
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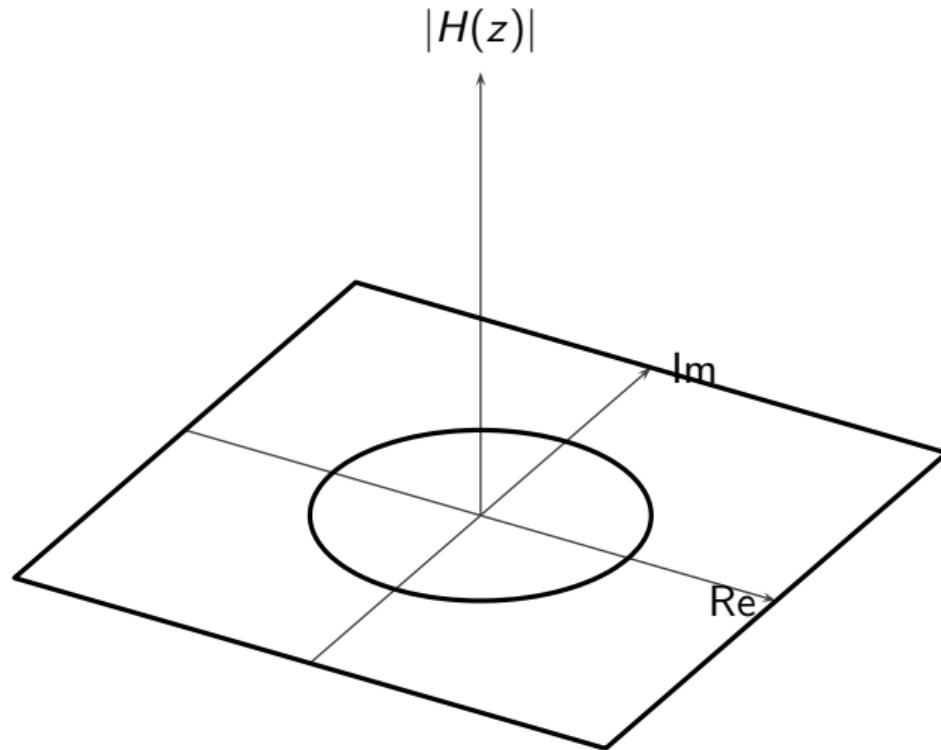
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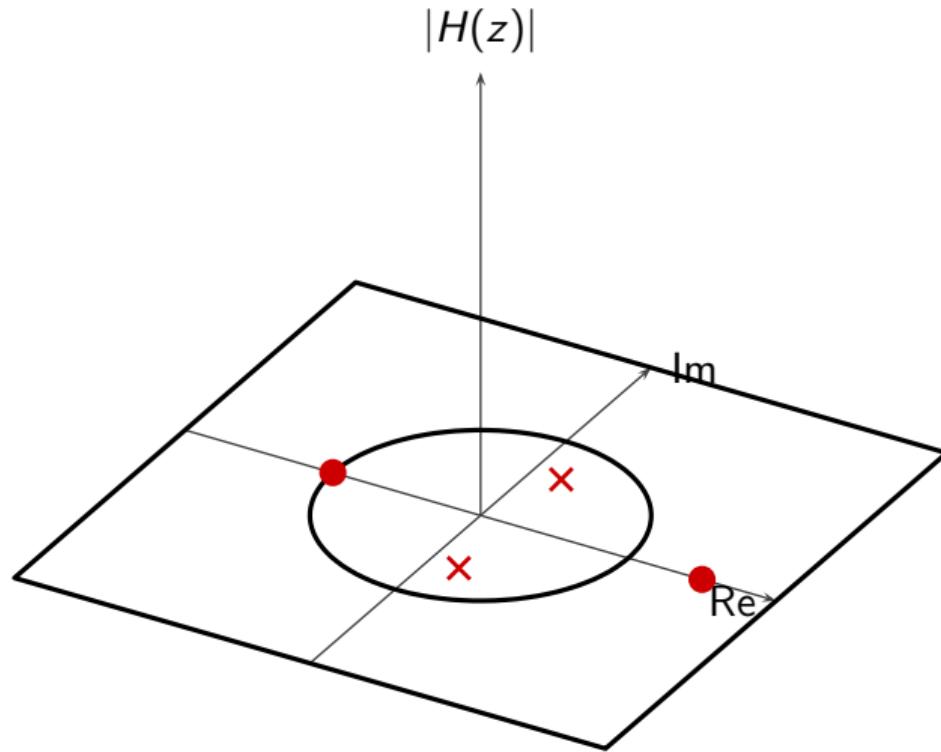
Estimating the frequency response



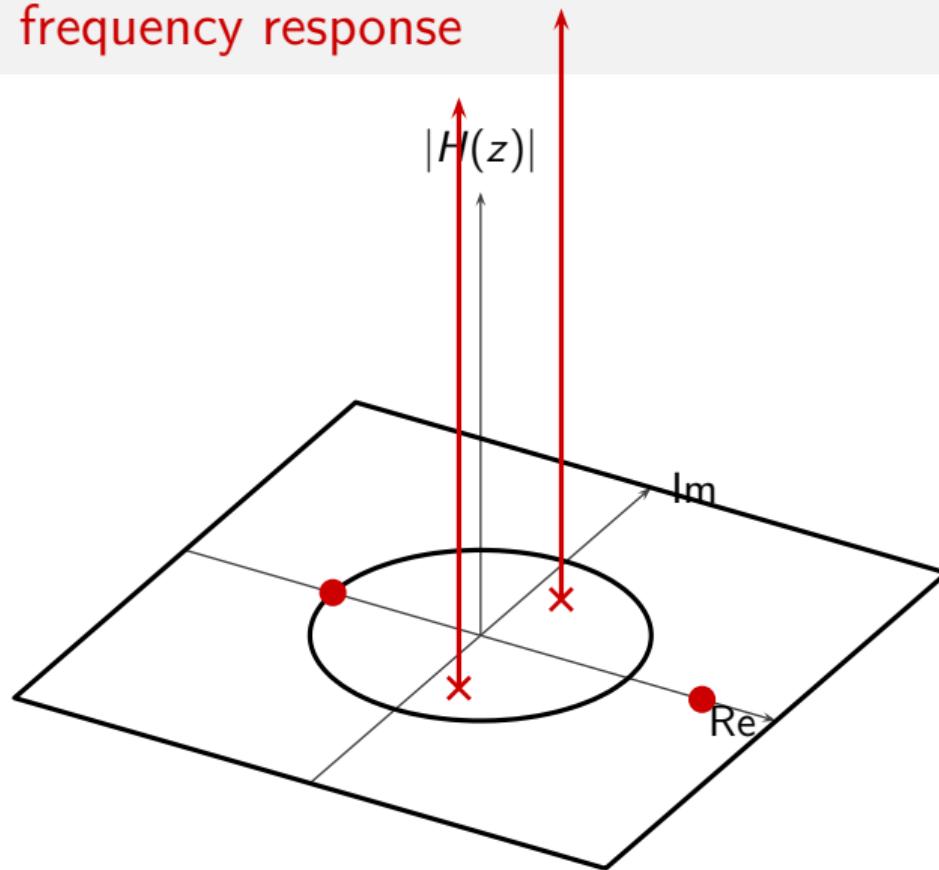
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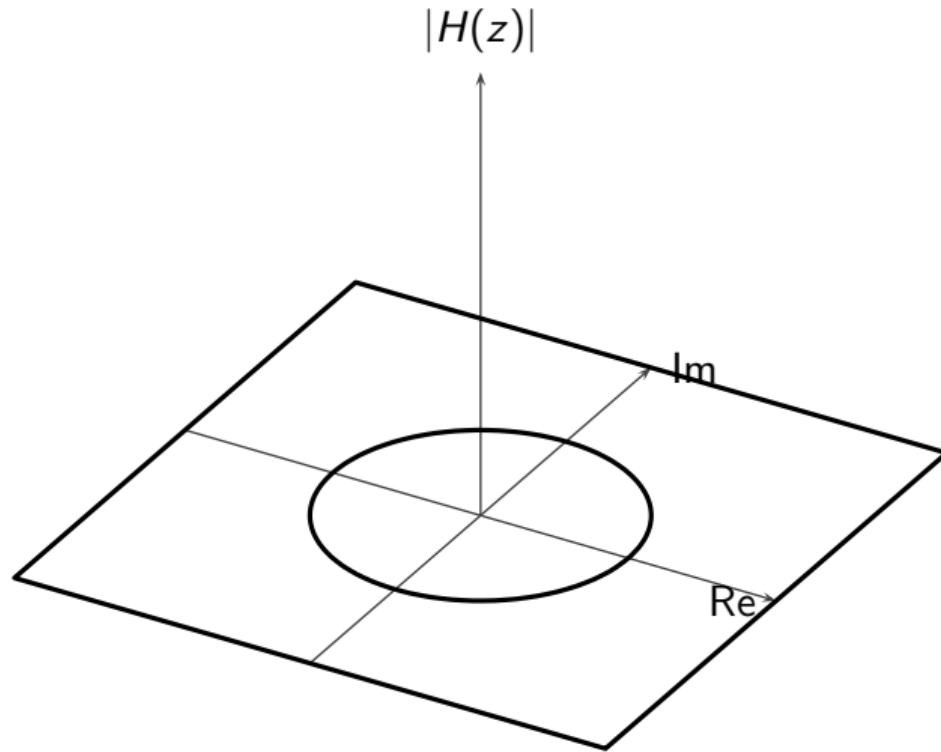
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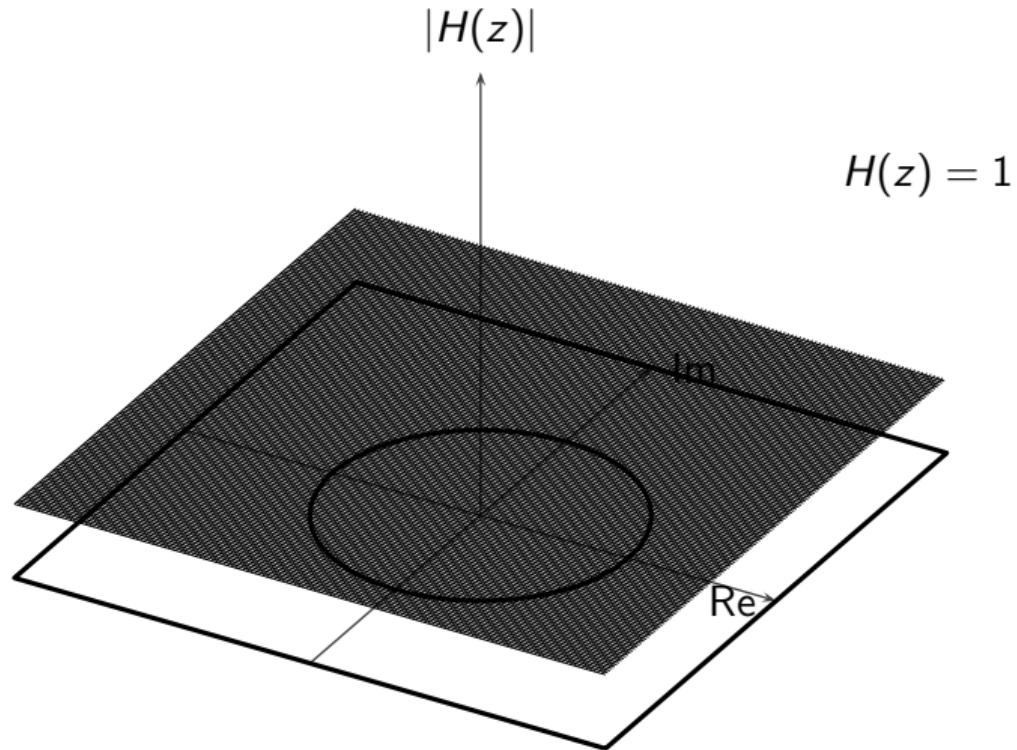
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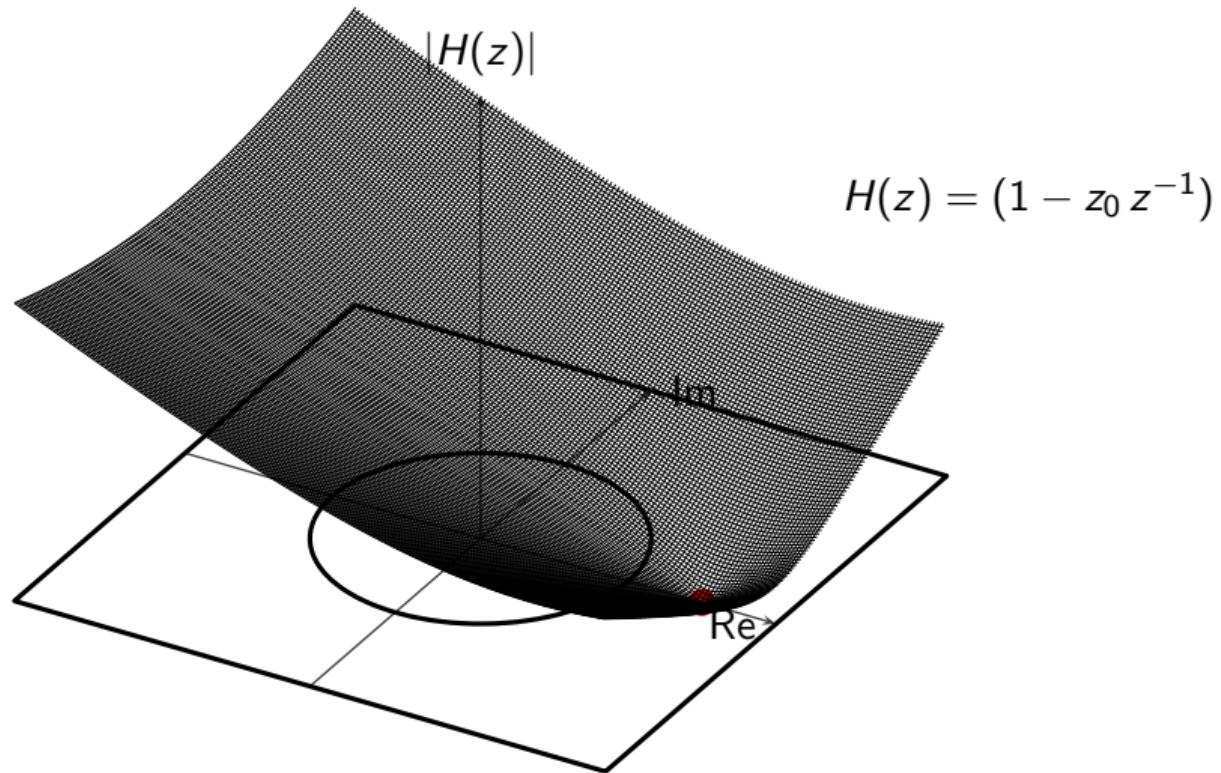
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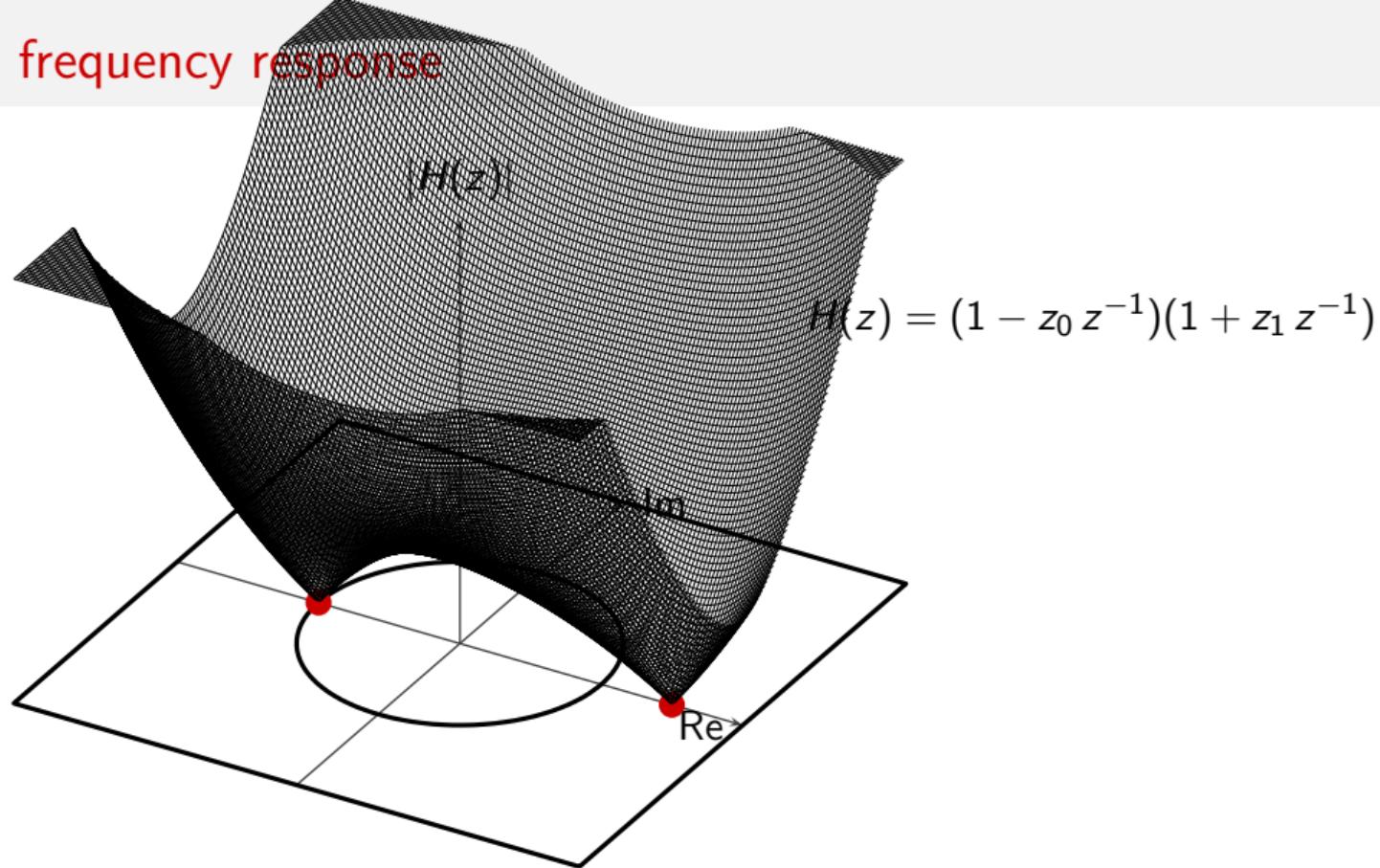
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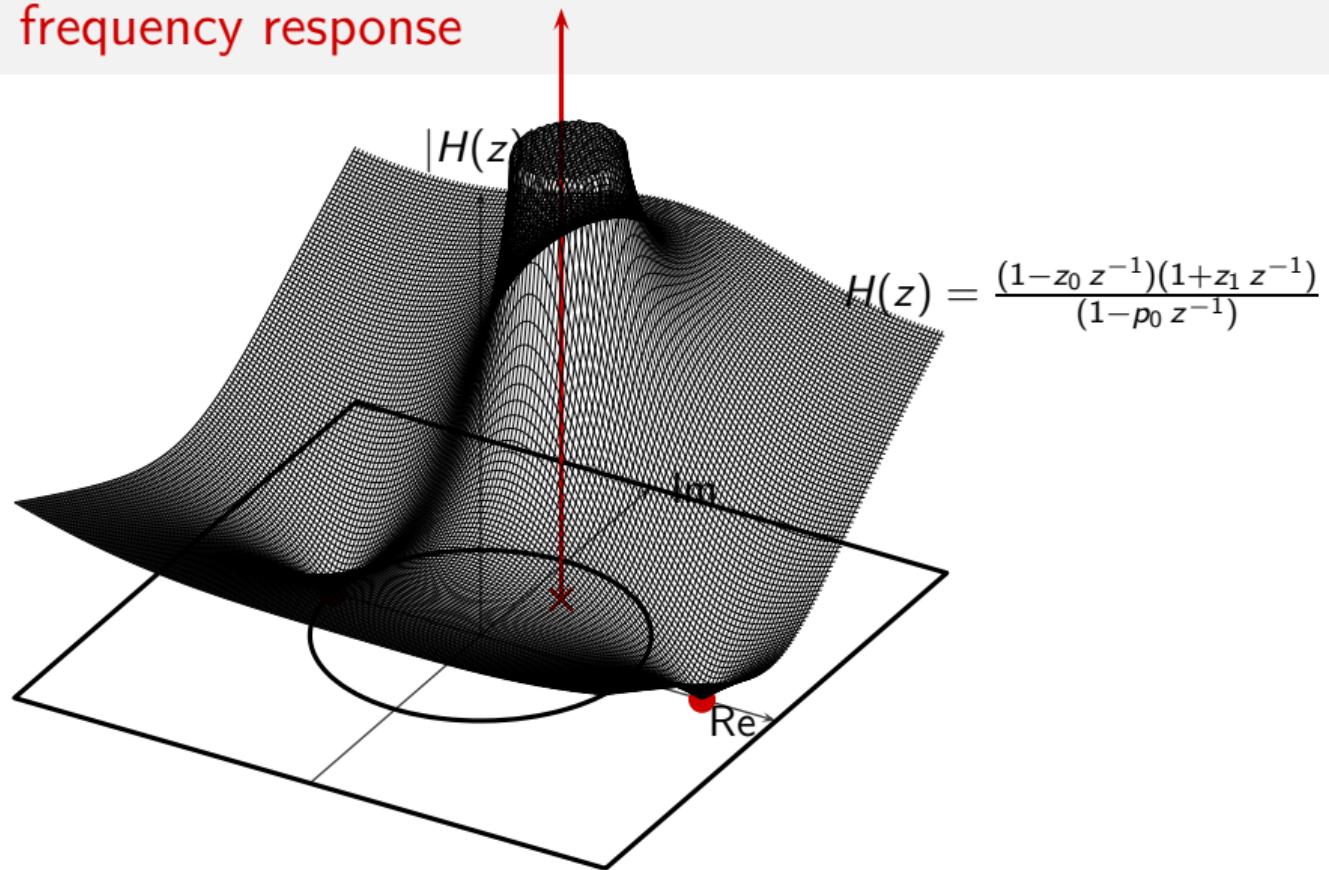
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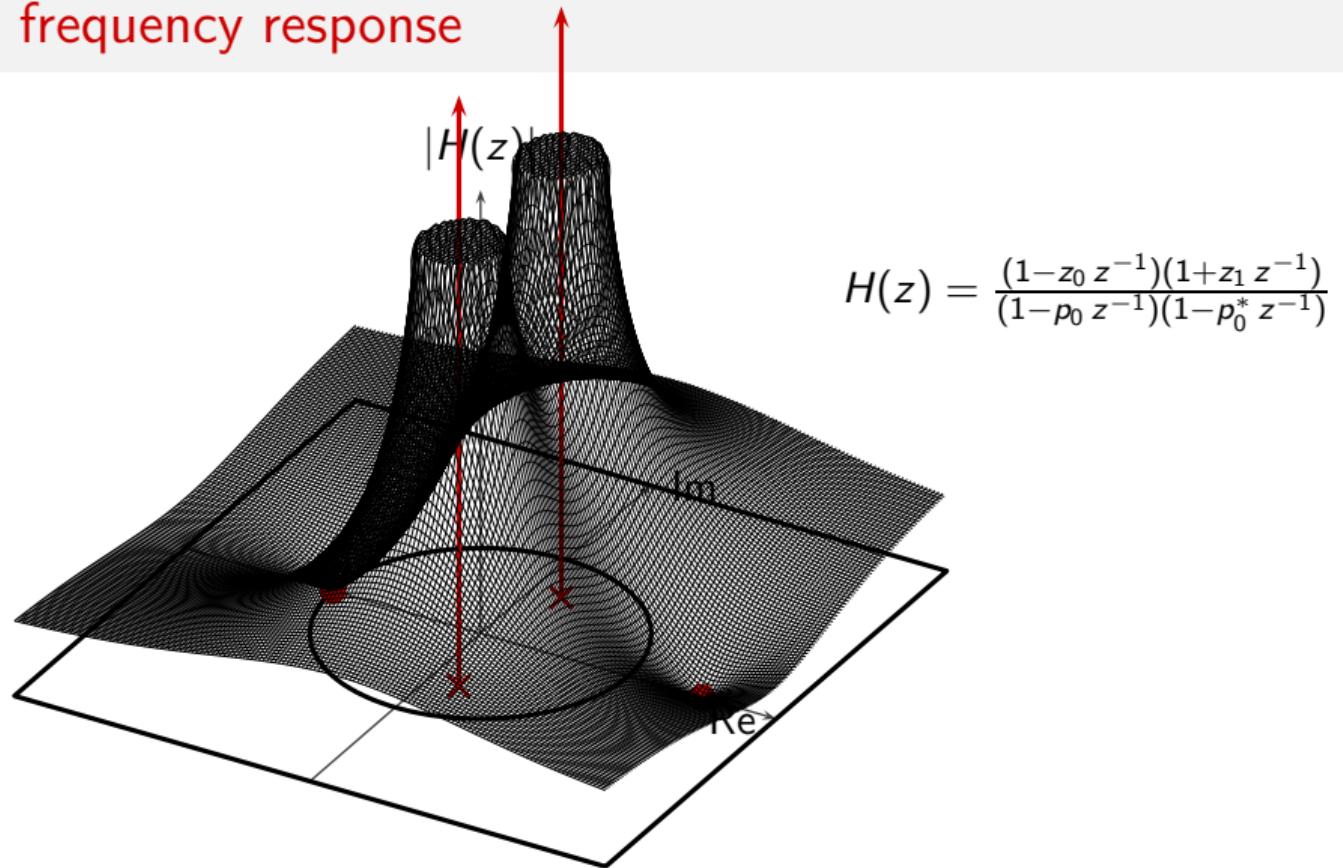
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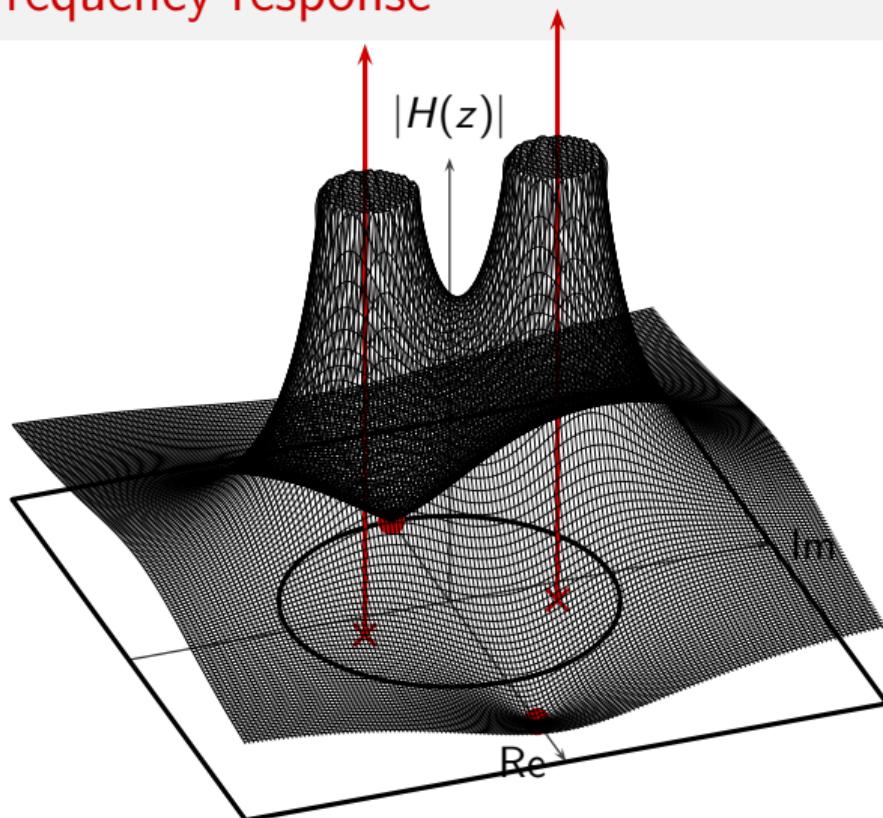
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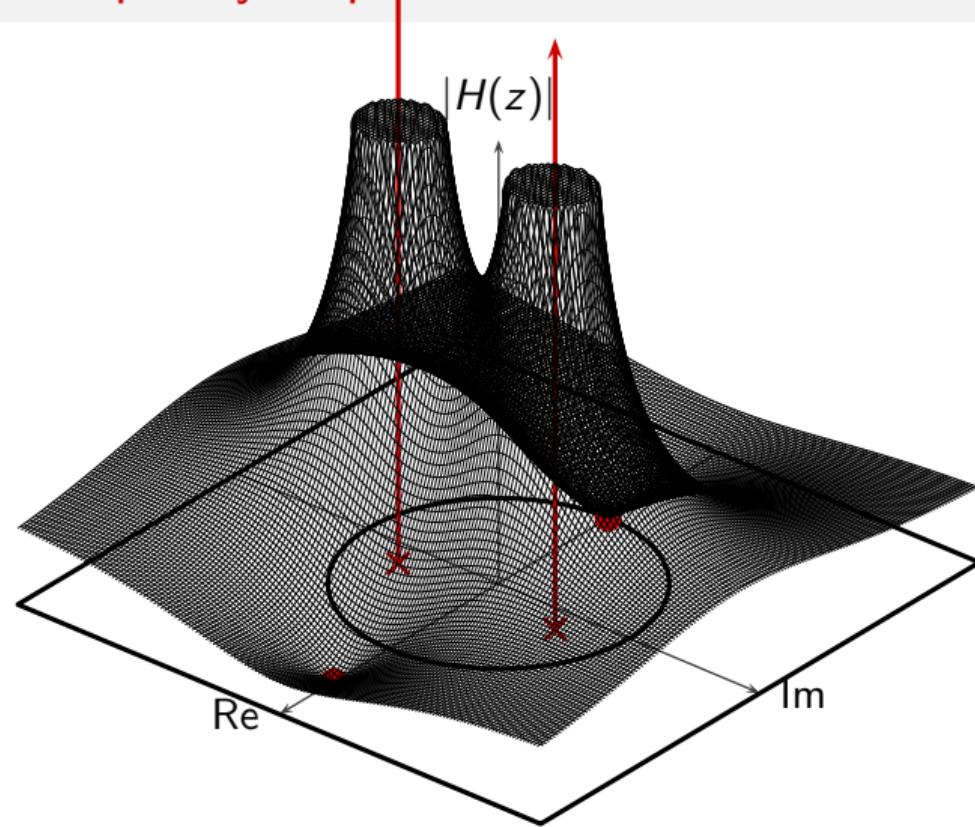
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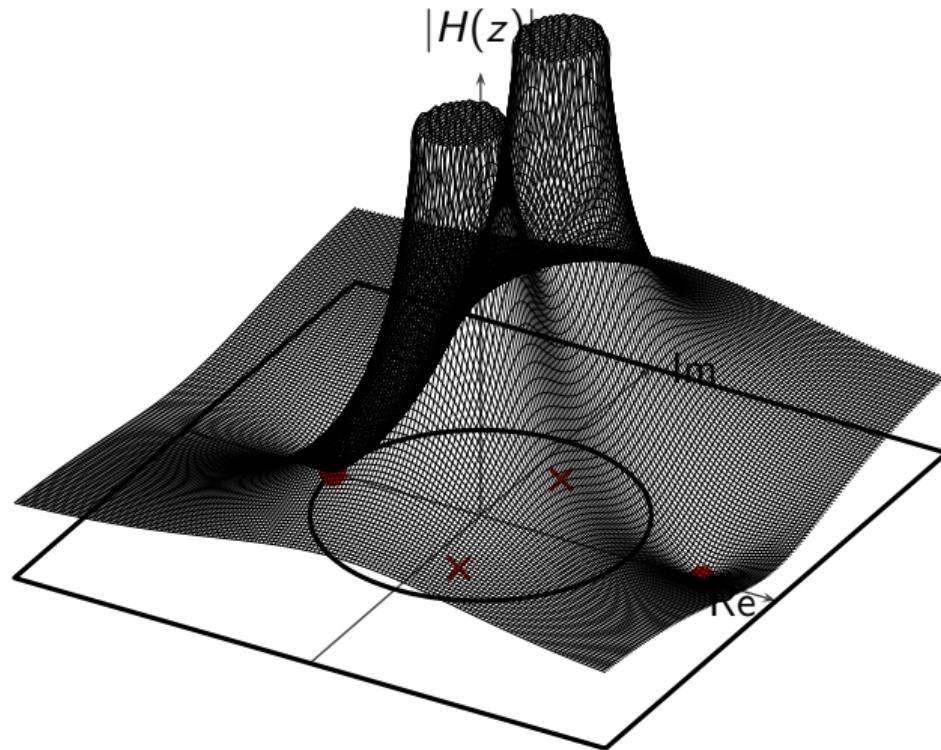
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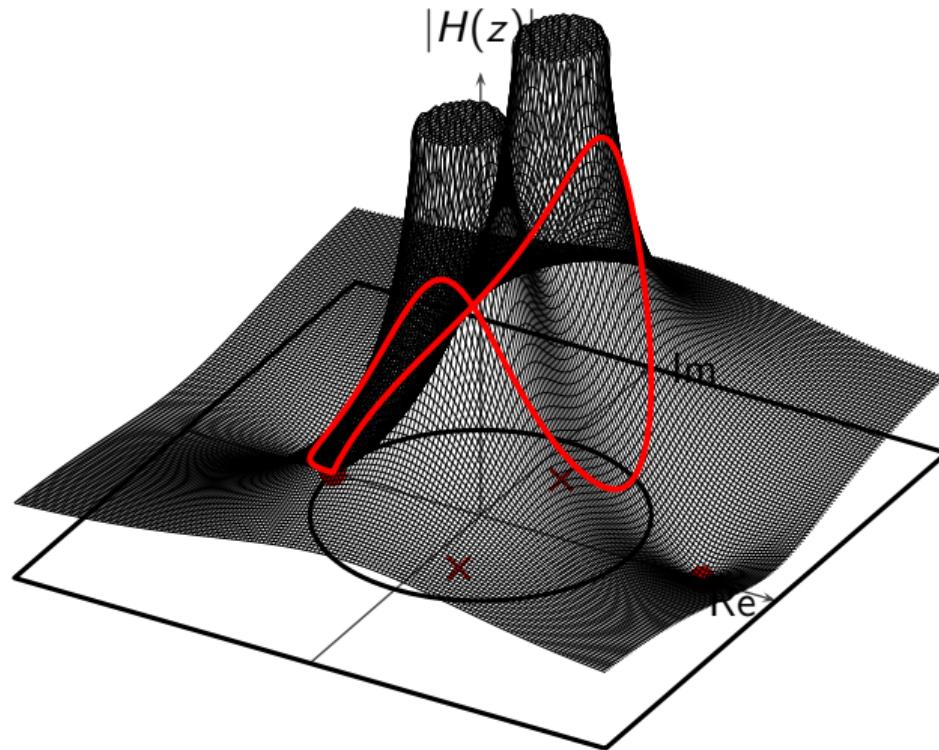
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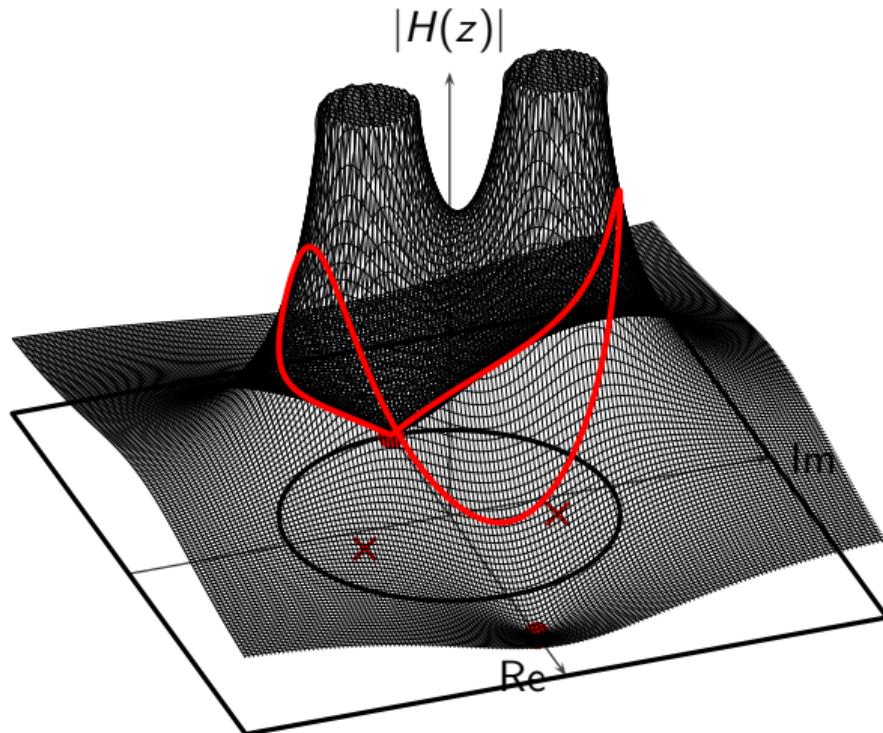
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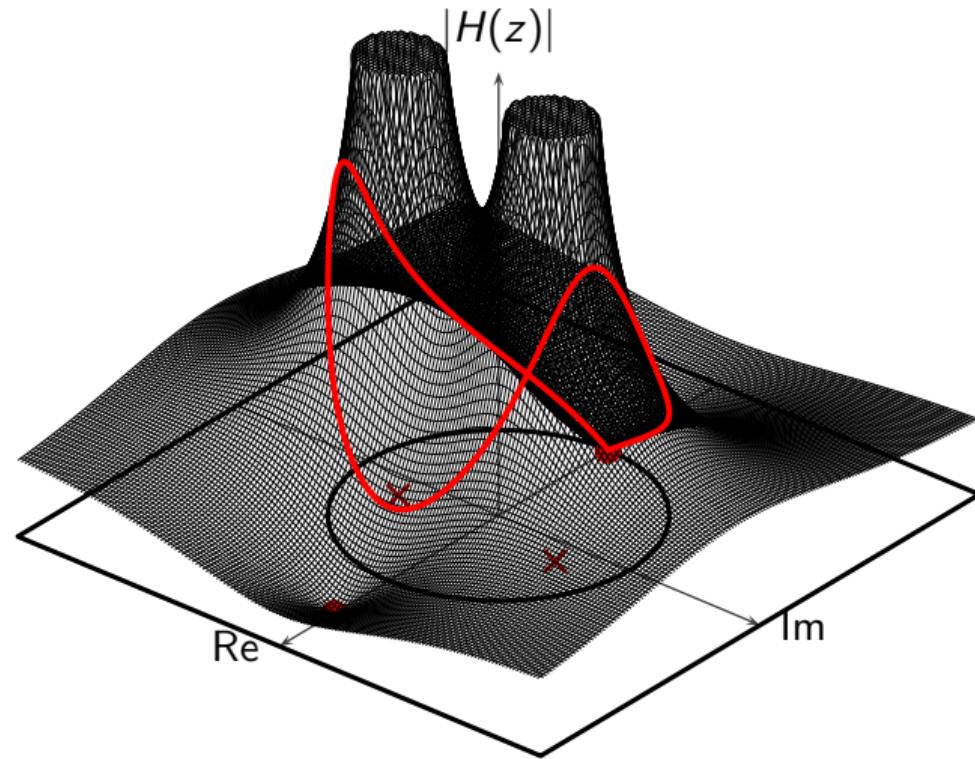
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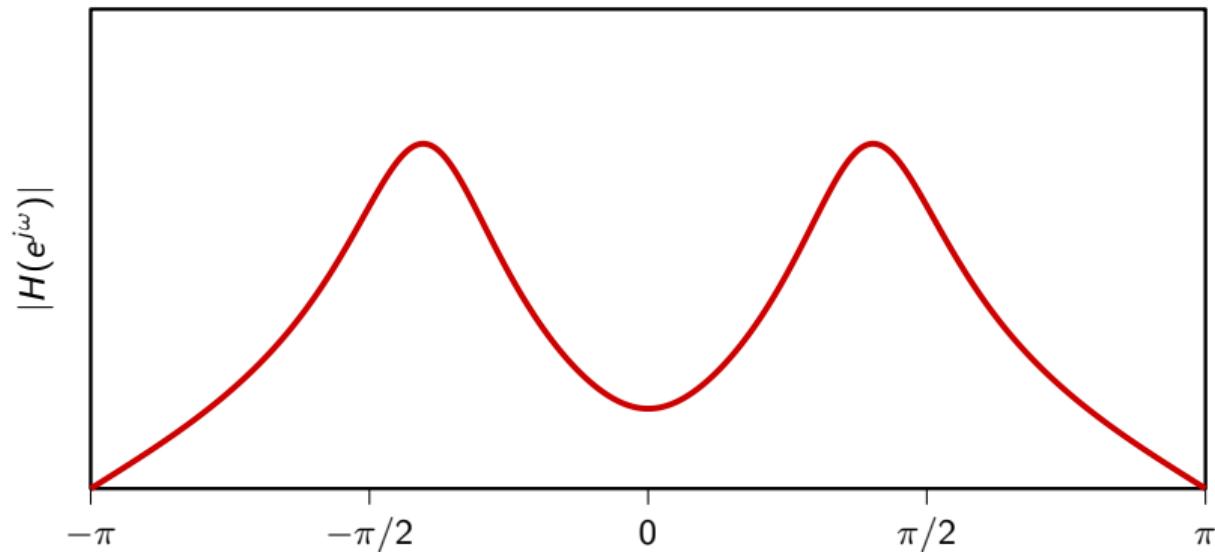
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Estimating the frequency response



Estimating the frequency response



filtering algorithms and structures

Overview:

- ▶ Algorithms for CCDE's
- ▶ Block diagram
- ▶ Real-time processing

An old friend

```
class Leaky:  
    def __init__(self, lmb):  
        self.lmb=lmb  
        self.y=0  
  
    def compute(self, x):  
        self.y = self.lmb * self.y + (1 - self.lmb) * x  
        return self.y
```

Testing the code

```
>>> from leaky import Leaky  
>>> li = Leaky(0.95)  
>>> for v in [0, 0, 0, 0, 1, 0, 0, 0, 0, 0]:  
>>>     print(li.compute(v), end=' ')  
  
0.0, 0.0, 0.0, 0.0, 0.0500000000000000, 0.0475000000000000,  
0.0451250000000000, 0.0428687500000000, 0.0407253125000000,  
0.038689046875000, 0.0367545945312500  
>>>
```

Key points

- ▶ we need a “memory cell” to store previous output
- ▶ we need to initialize the storage before first use
- ▶ we need 2 multiplications and one addition per output sample

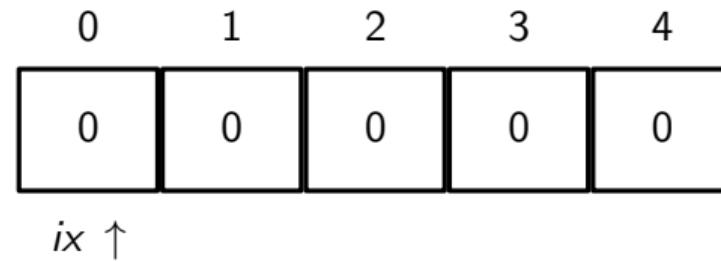
Another old friend

$$y[n] = \frac{1}{M} \sum_{k=0}^{M-1} x[n - k]$$

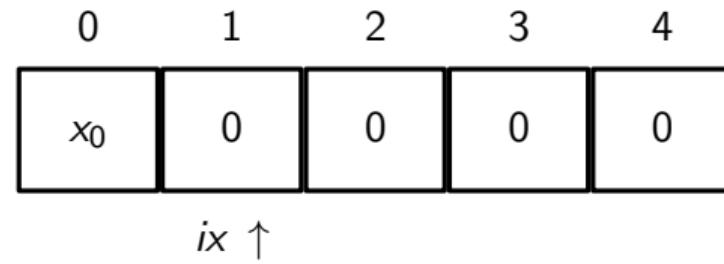
Another old friend

```
class MA:  
    def __init__(self, M):  
        self.M = M  
        self.buf = [0.0] * M  
        self.ix = 0  
  
    def compute(self, x):  
        self.buf[self.ix] = x  
        self.ix = (self.ix + 1) % self.M  
        res = 0.0  
        for v in self.buf:  
            res += v  
        return res / float(self.M)
```

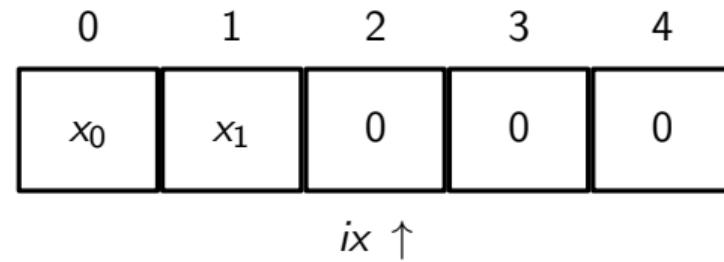
The circular buffer



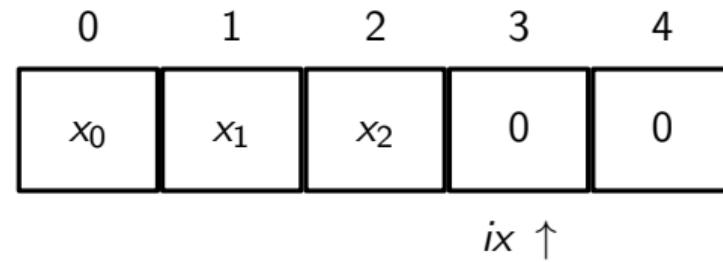
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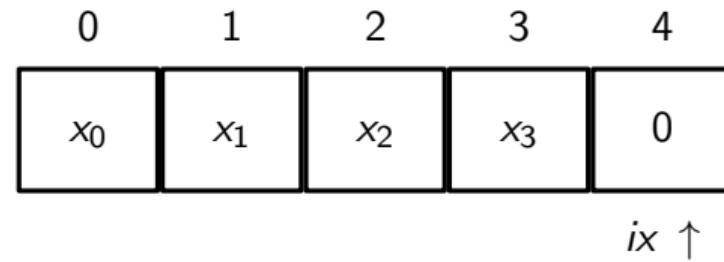
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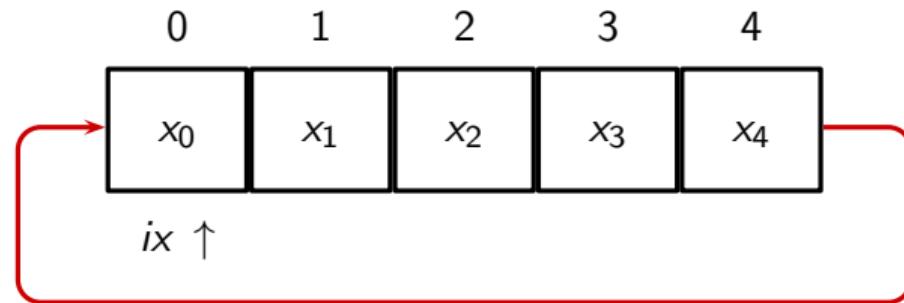
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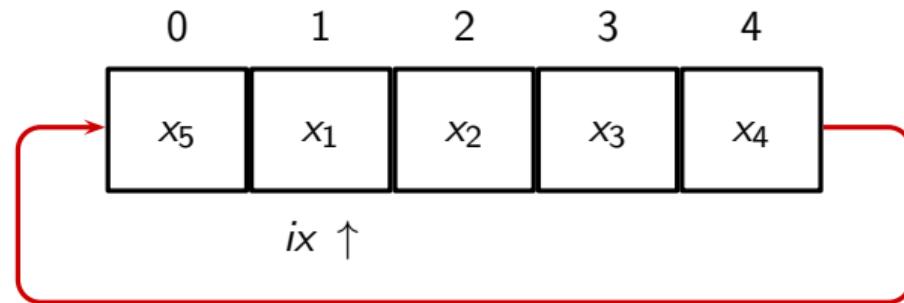
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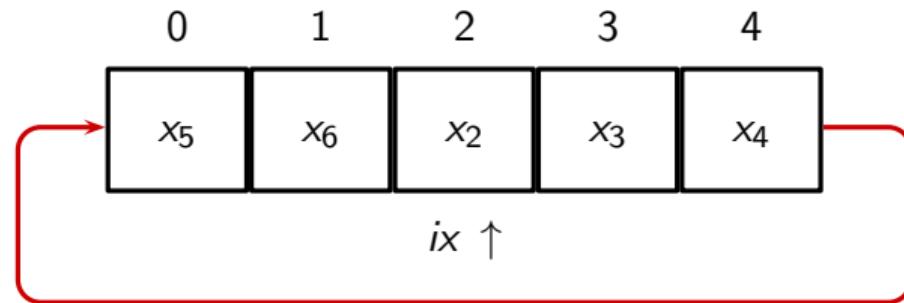
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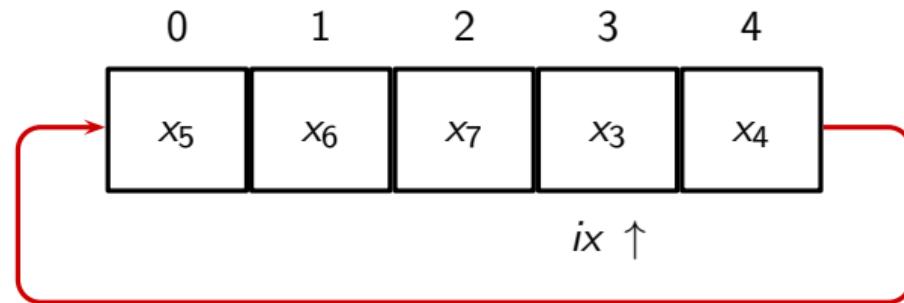
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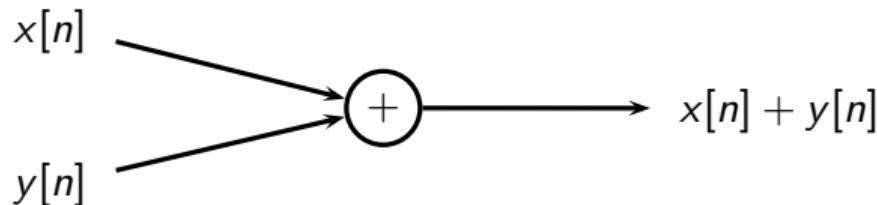
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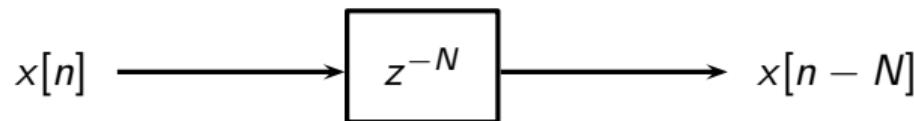
Key points

- ▶ we now need M memory cells to store previous input values
- ▶ we need to initialize the storage before first use
- ▶ we need 1 division and M additions per output sample

We can abstract from the implementation

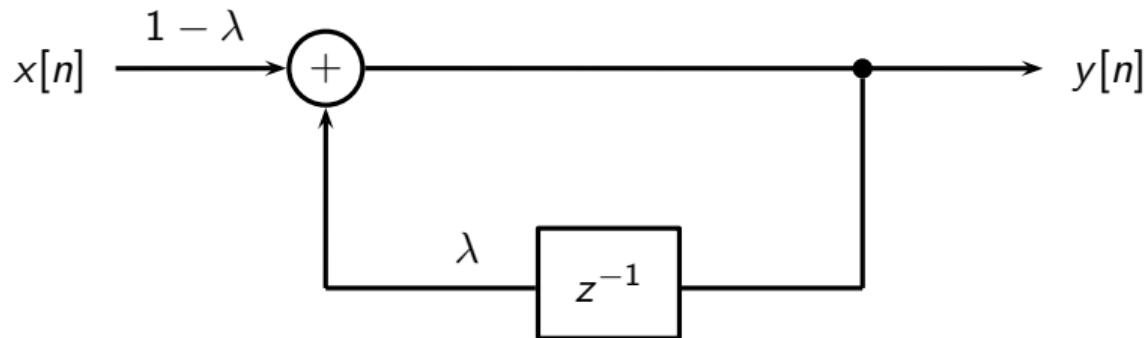


$$x[n] \xrightarrow{\alpha} \alpha x[n]$$



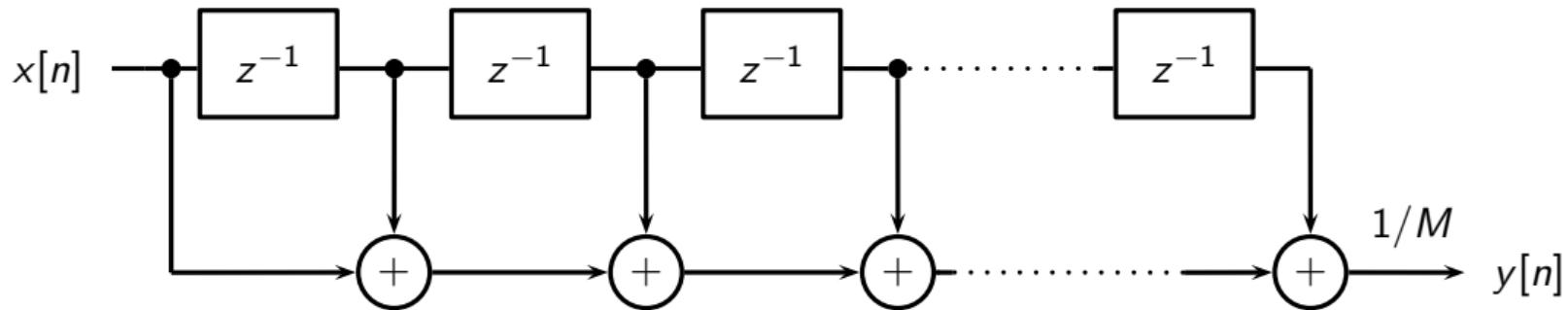
Leaky Integrator

$$y[n] = \lambda y[n - 1] + (1 - \lambda)x[n]$$



Moving Average

$$y[n] = \frac{1}{M} \sum_{k=0}^{M-1} x[n - k]$$



The second-order section

$$y[n] + a_1y[n - 1] + a_2y[n - 2] = b_0x[n] + b_1x[n - 1] + b_2x[n - 2]$$

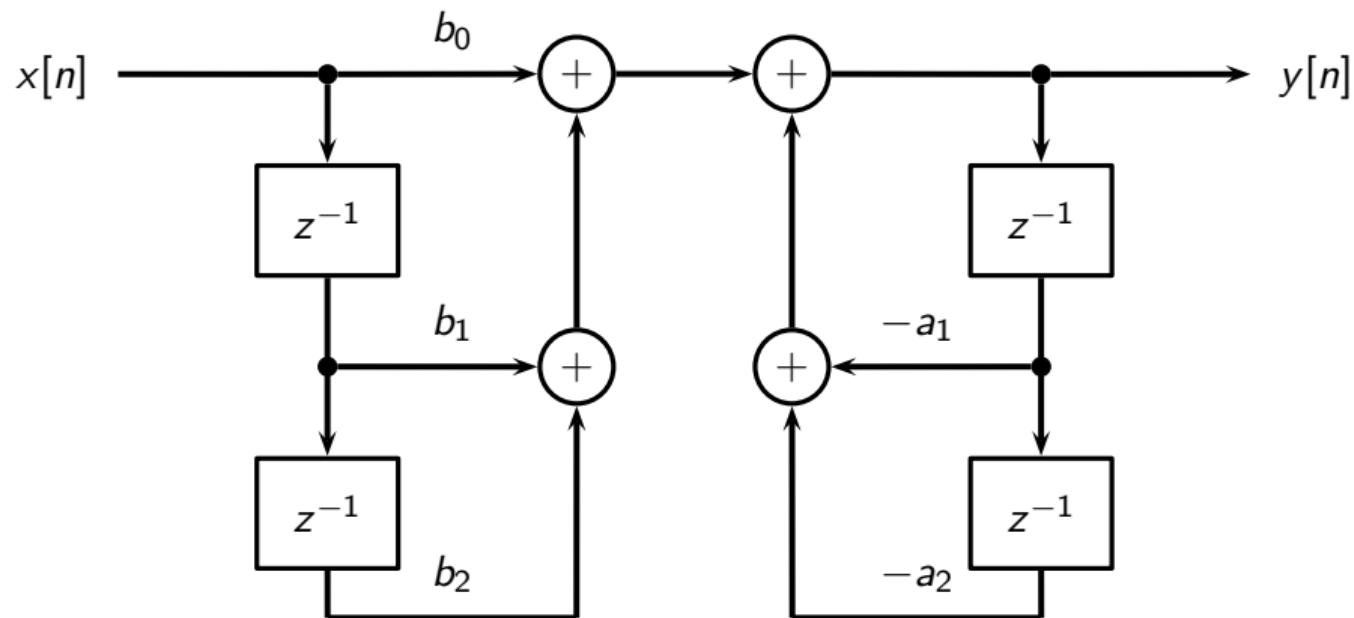
$$H(z) = \frac{b_0 + b_1z^{-1} + b_2z^{-2}}{1 + a_1z^{-1} + a_2z^{-2}} = \frac{B(z)}{A(z)}$$

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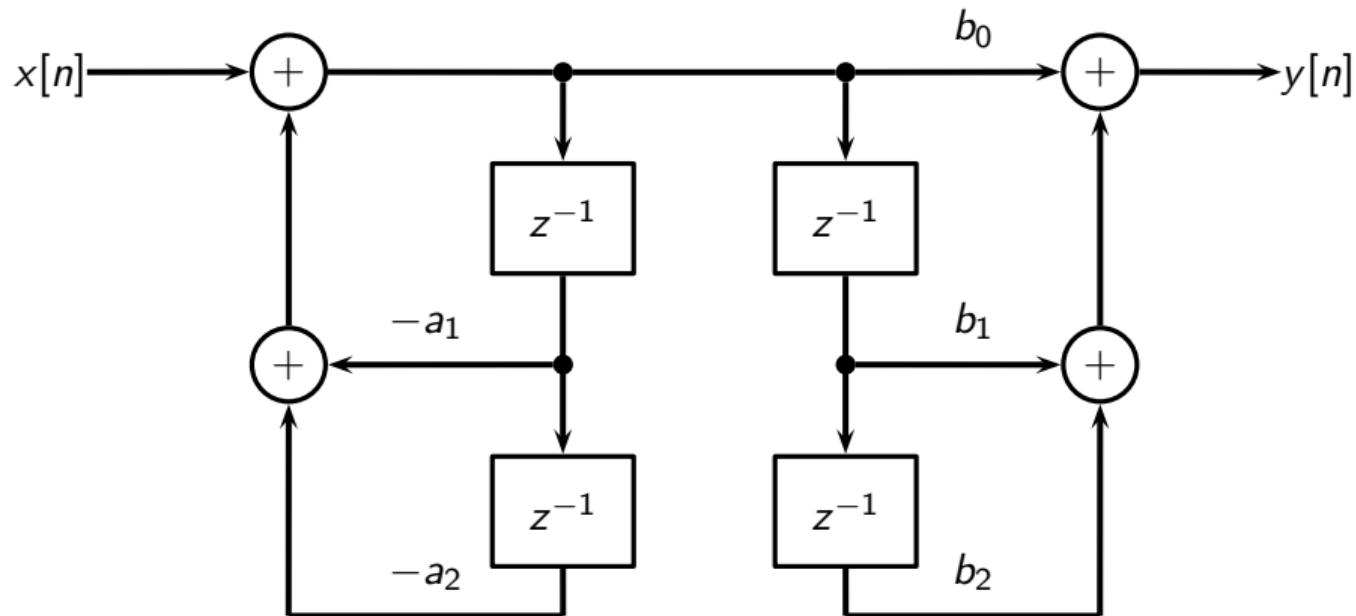
Second-order section, direct form I



$$B(z)$$

$$1/A(z)$$

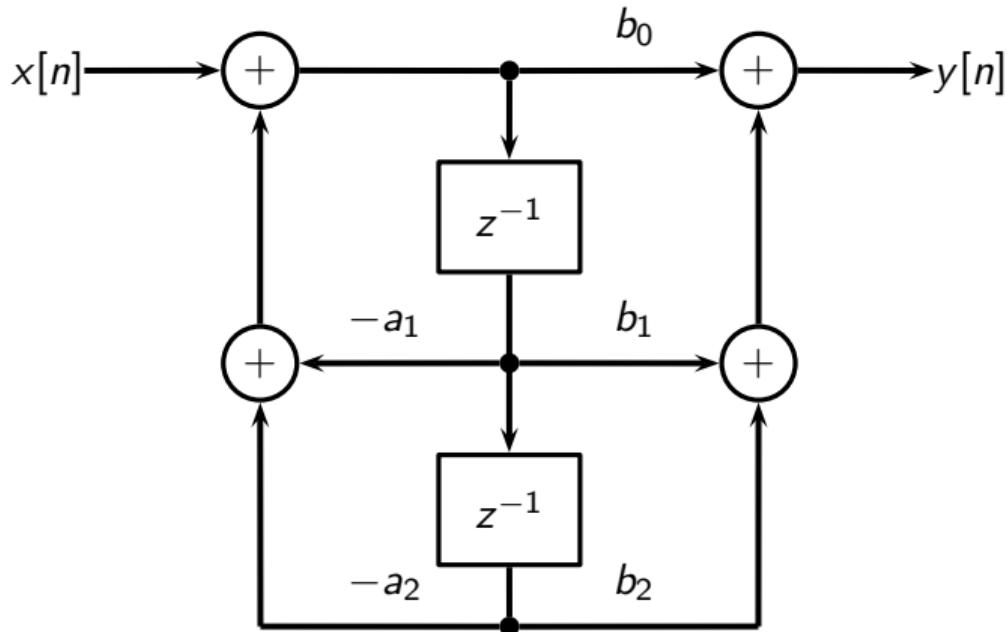
Second-order section, direct form I, inverted order



$$1/A(z)$$

$$B(z)$$

Second-order section, direct form II



intuitive filter design

Overview:

- ▶ General problem
- ▶ “Intuitive” IIR design

Simple, useful filters

- ▶ many signal processing problems can be solved using simple filters
- ▶ we have seen simple lowpass filters already (Moving Average, Leaky Integrator)
- ▶ simple (low order) transfer functions allow for intuitive design and tuning

Simple lowpass

- ▶ let only low frequencies pass
- ▶ used to remove high frequency components (e.g. noise)
- ▶ useful in audio, communication, control systems
- ▶ we know a simple answer: leaky integrator

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Leaky Integrator

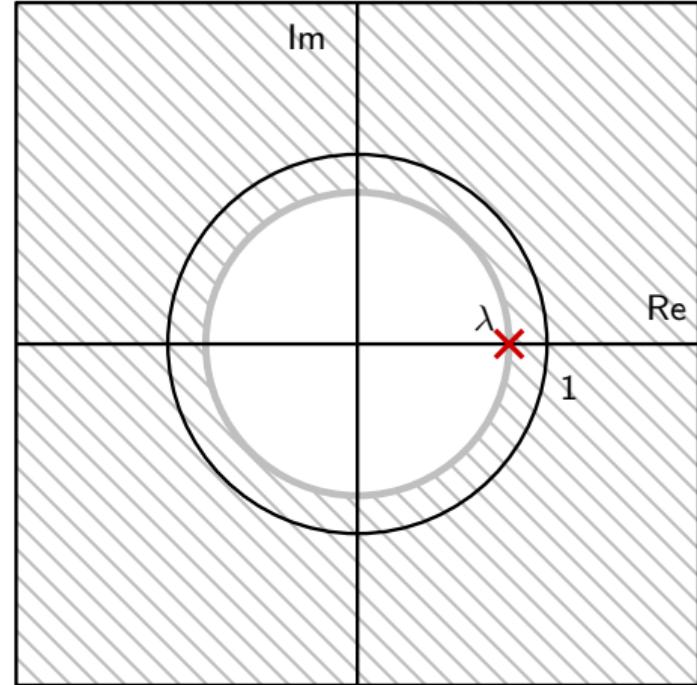
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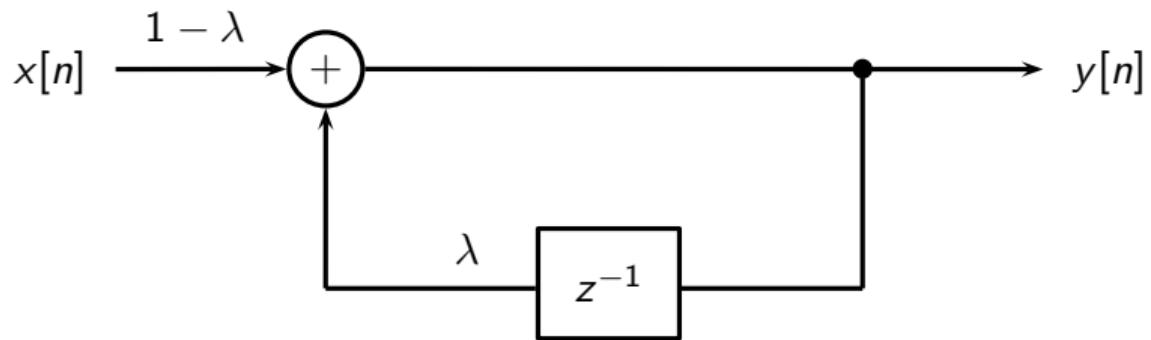
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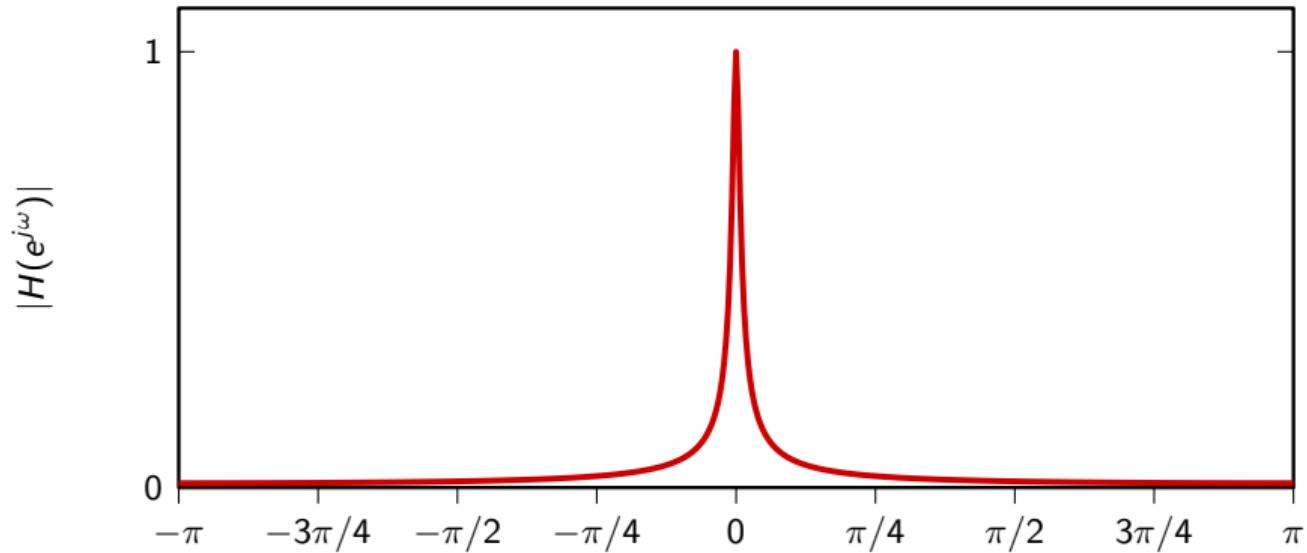
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Leaky Integrator, filter structure



Leaky Integrator, $\lambda = 0.98$



Resonator

- ▶ a resonator is a narrow bandpass filter
- ▶ used to detect the presence of a sinusoid of a given frequency
- ▶ useful in communication systems and telephony (DTMF)
- ▶ idea: shift the passband of the Leaky Integrator!

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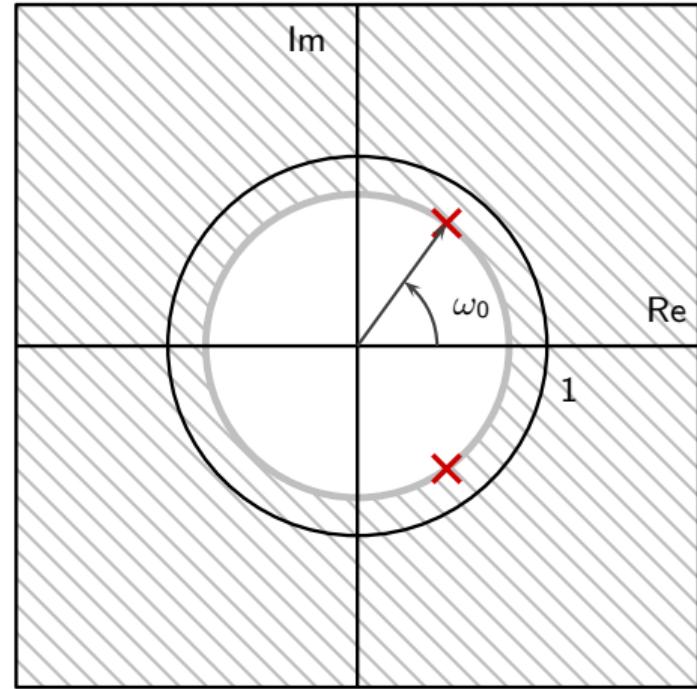
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- ▶ useful in communication systems and telephony (DTMF)
- ▶ idea: shift the passband of the Leaky Integrator!

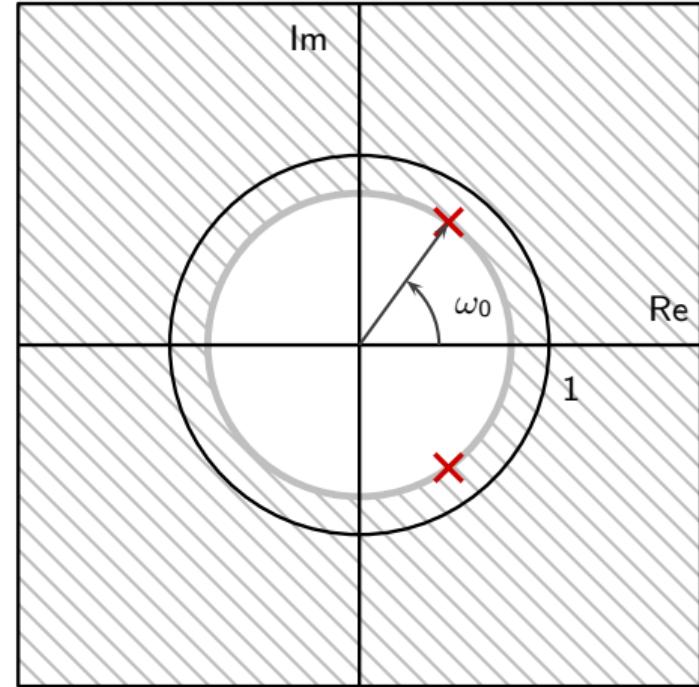
Resonator



Resonator

$$H(z) = \frac{G_0}{(1 - pz^{-1})(1 - p^*z^{-1})}$$

$$p = \lambda e^{j\omega_0}$$

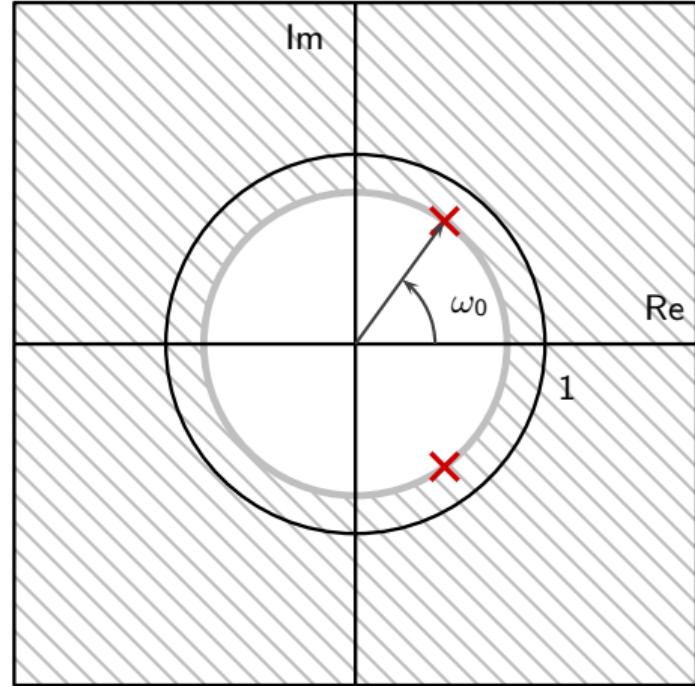


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$$p = \lambda e^{j\omega_0}$$

$$y[n] = G_0x[n] - a_1y[n-1] - a_2y[n-2]$$



Resonator

$$\begin{aligned} H(z) &= \frac{G_0}{(1 - pz^{-1})(1 - p^*z^{-1})}, \quad p = \lambda e^{j\omega_0} \\ &= \frac{G_0}{1 - 2\Re\{p\} z^{-1} + |p|^2 z^{-2}} \\ &= \frac{G_0}{1 - 2\lambda \cos \omega_0 z^{-1} + |\lambda|^2 z^{-2}} \end{aligned}$$

$$a_1 = 2\lambda \cos \omega_0$$

$$a_2 = -|\lambda|^2$$

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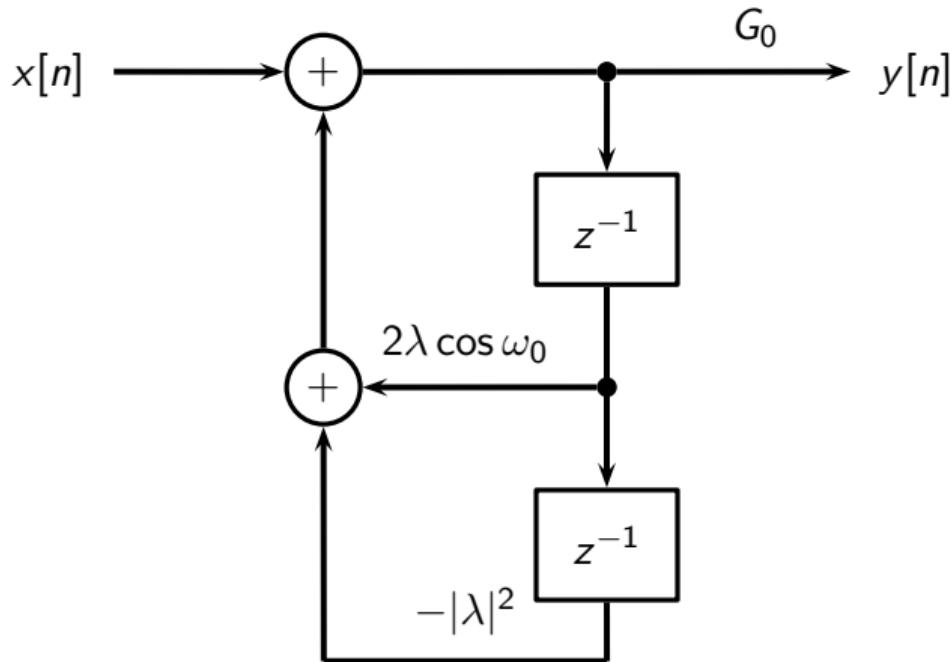
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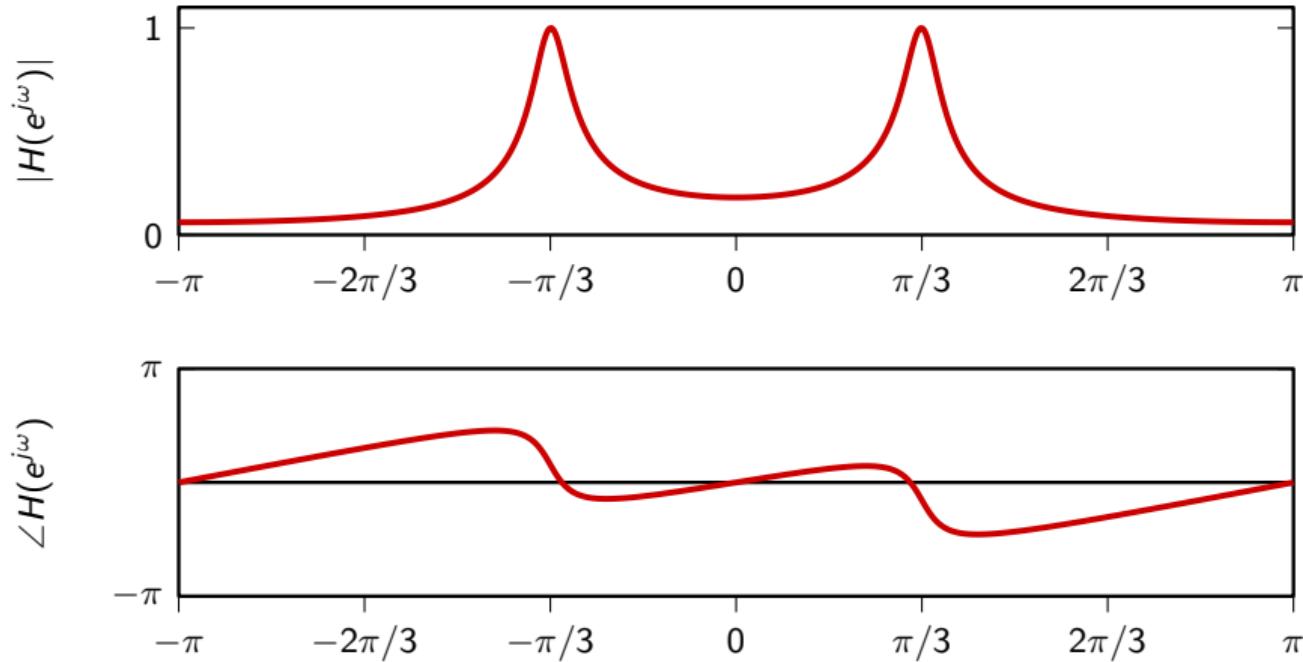
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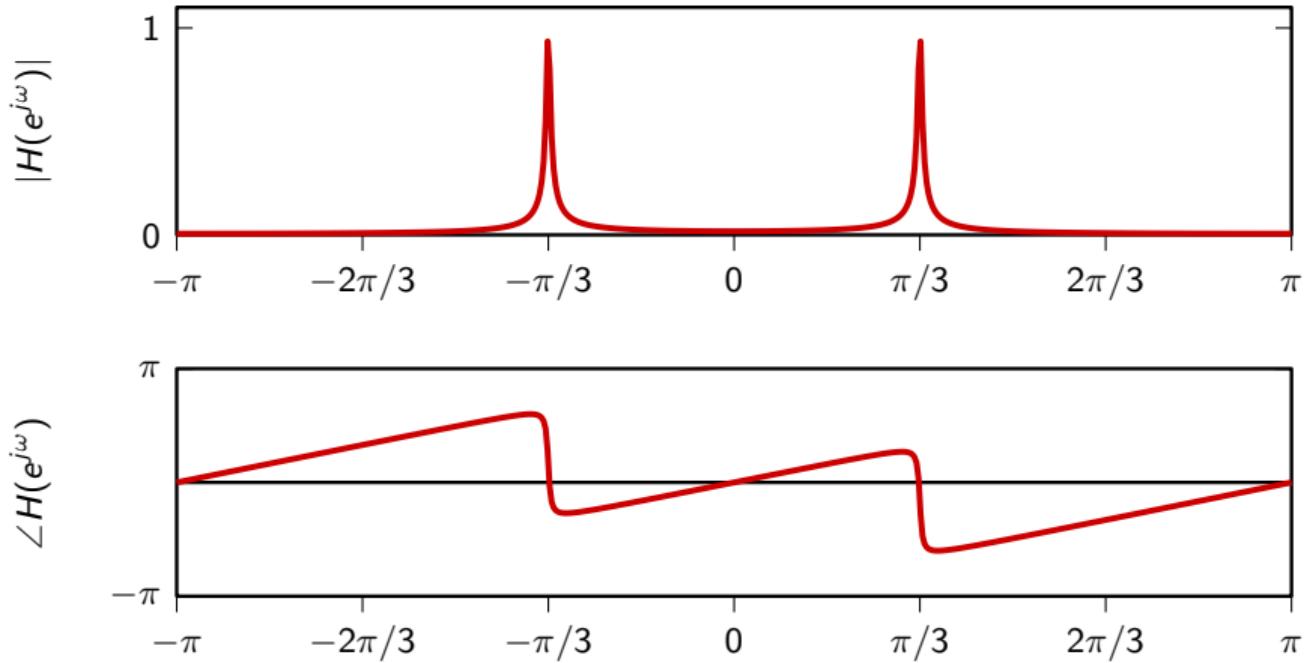
Resonator, filter structure



Resonator, $\lambda = 0.9, \omega_0 = \pi/3$



Resonator, $\lambda = 0.99$, $\omega_0 = \pi/3$



DC removal

- ▶ a DC-balanced signal has zero sum: $\lim_{N \rightarrow \infty} \sum_{n=-N}^N x[n] = 0$
i.e. there is no Direct Current component
- ▶ its DTFT value at zero is zero
- ▶ we want to remove the DC bias from a non zero-centered signal
- ▶ we want to kill the frequency component at $\omega = 0$

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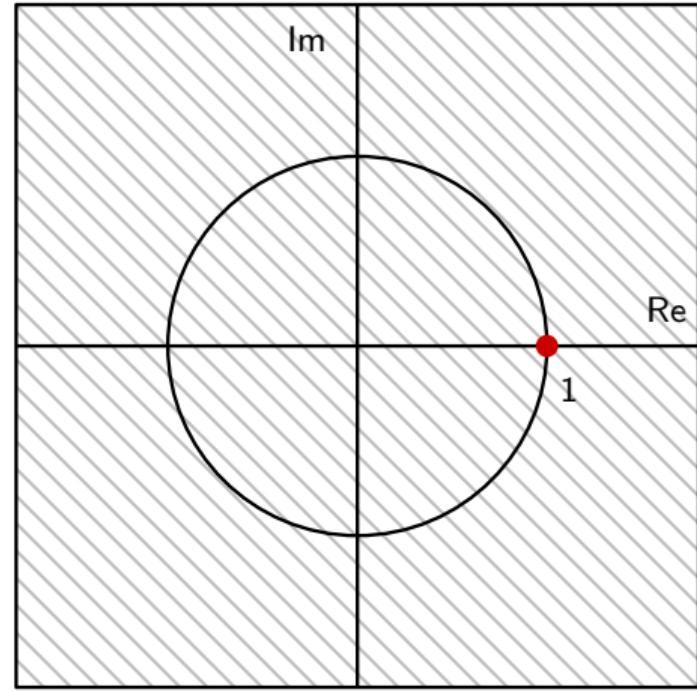
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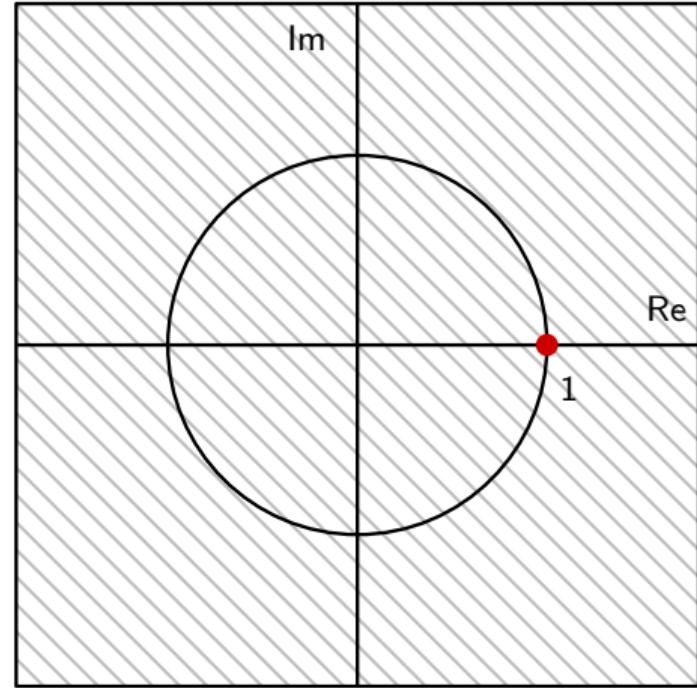
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DC removal



DC removal

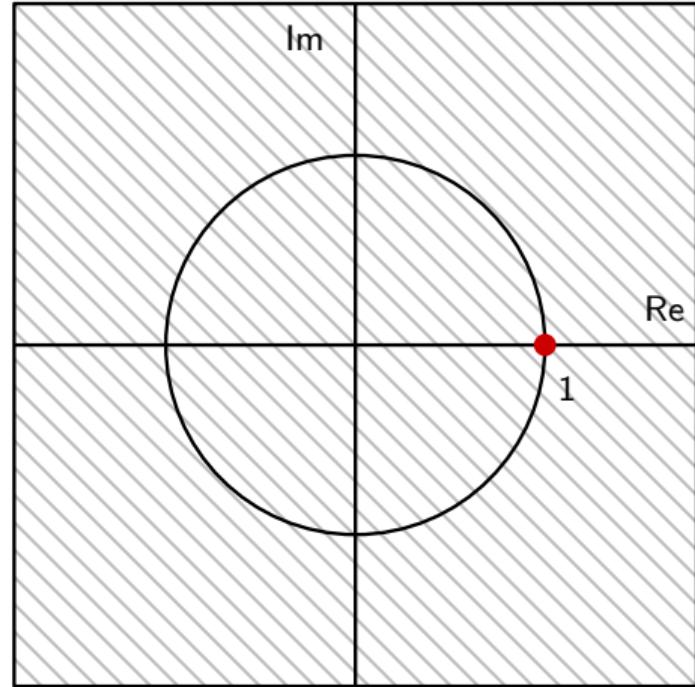
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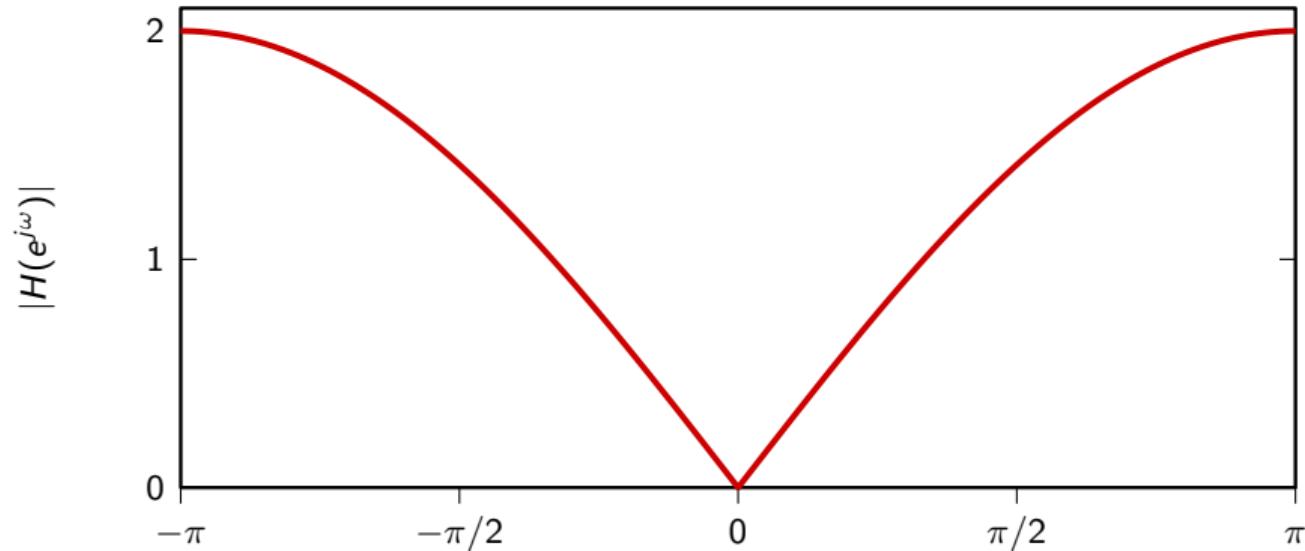
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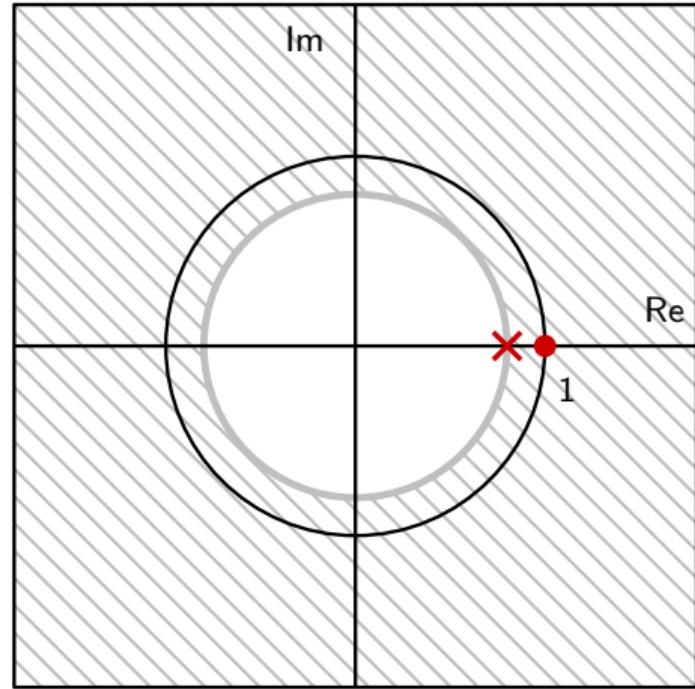
$$y[n] = x[n] - x[n - 1]$$



DC notch

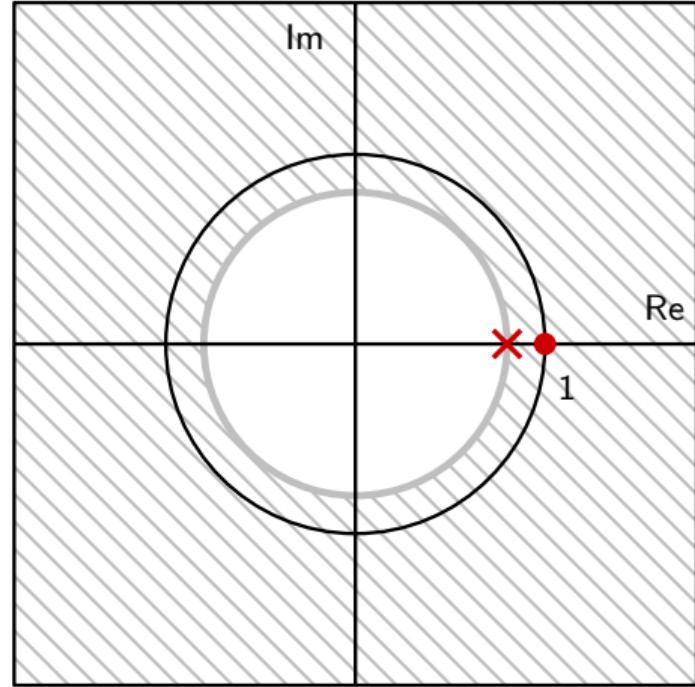


DC removal, improved



DC removal, improved

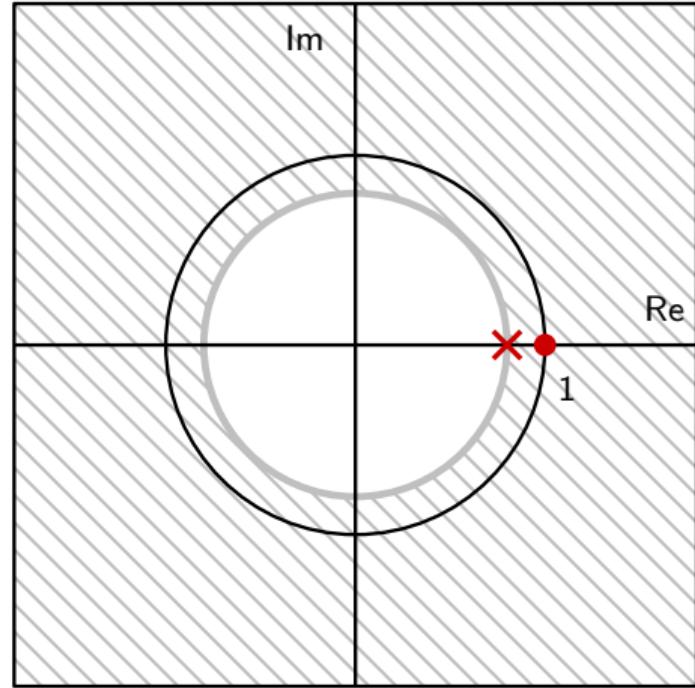
$$H(z) = \frac{1 - z^{-1}}{1 - \lambda z^{-1}}$$



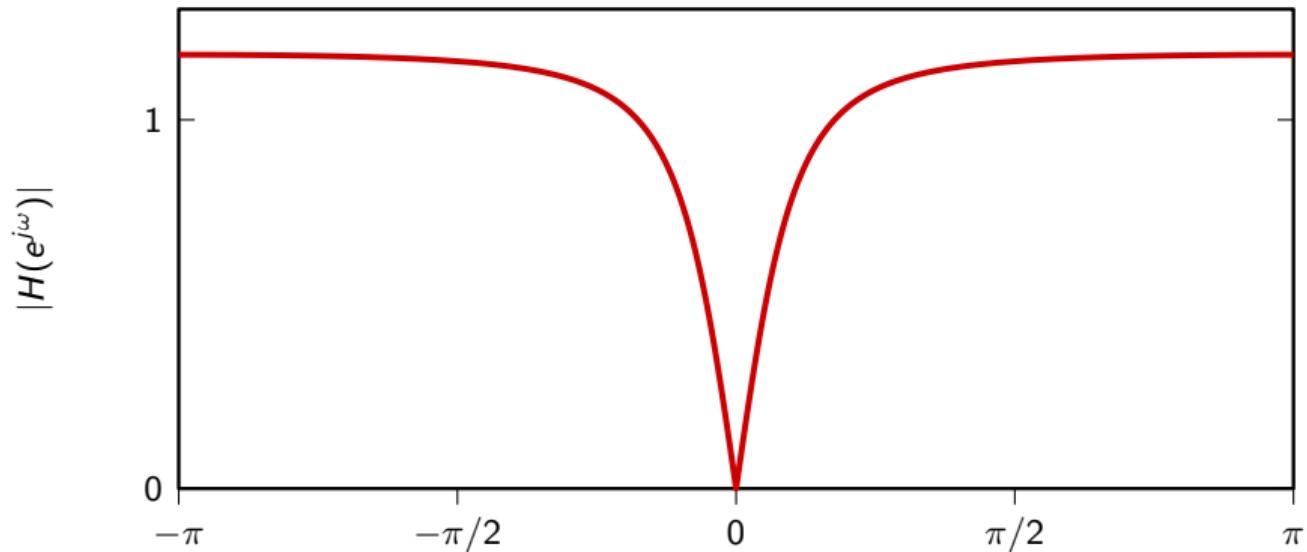
DC removal, improved

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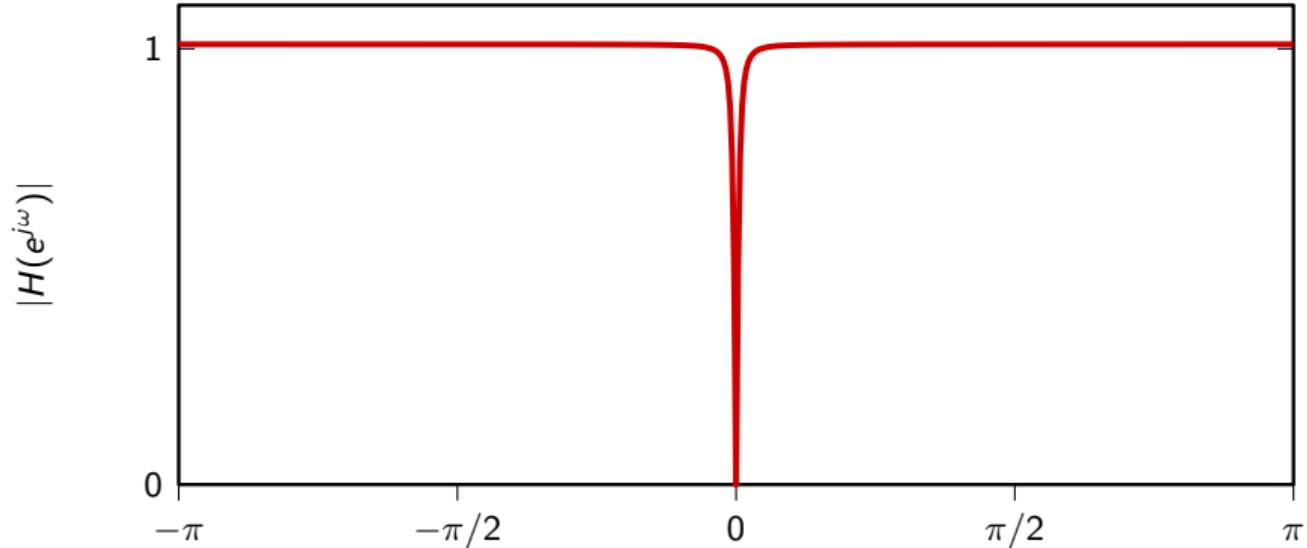
$$y[n] = \lambda y[n-1] + x[n] - x[n-1]$$



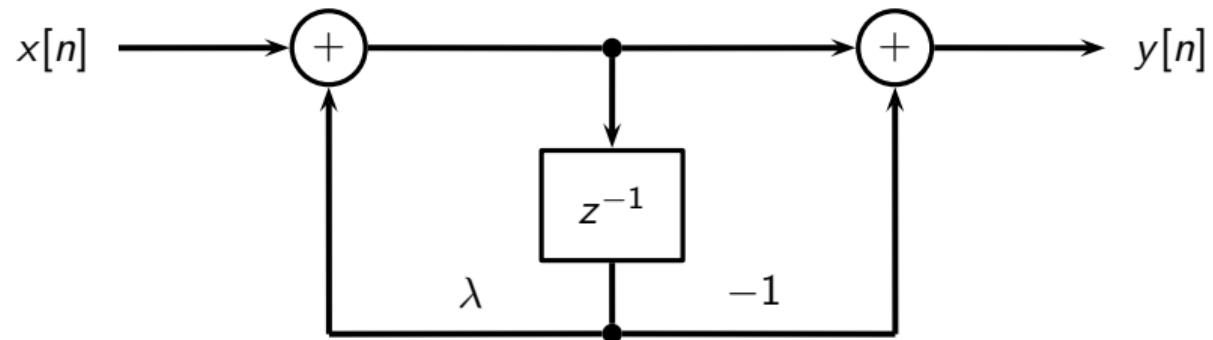
DC notch, $\lambda = 0.7$



DC notch, $\lambda = 0.98$



DC notch, filter structure



Hum removal

- ▶ similar to DC removal but we want to remove a specific nonzero frequency
- ▶ very useful for musicians: amplifiers for electric guitars pick up the hum from the electric mains (50Hz in Europe and 60Hz in North America)
- ▶ we need to tune the hum removal according to country

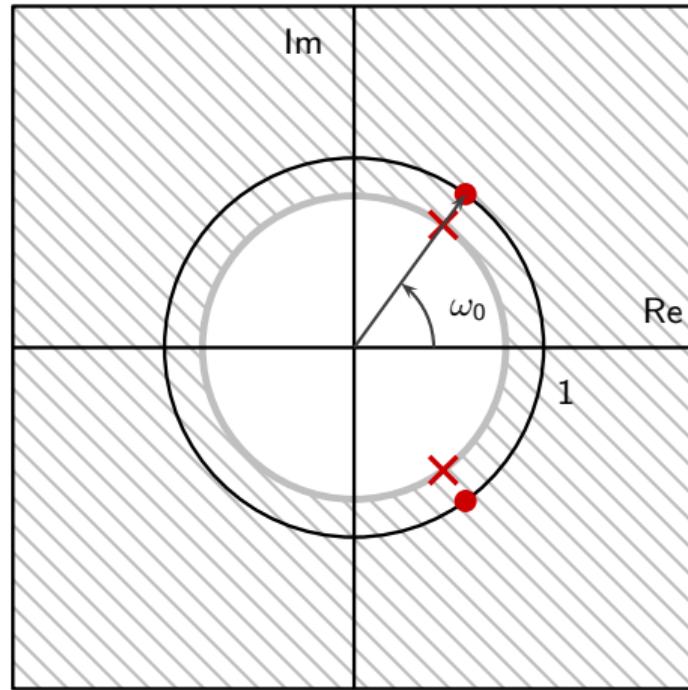
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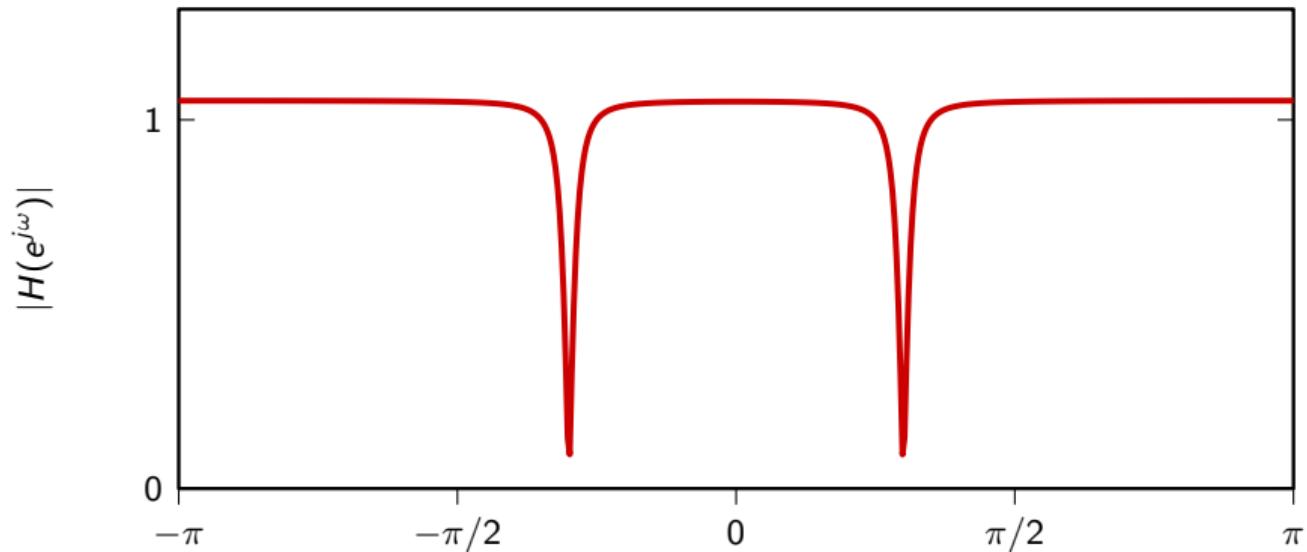
Hum removal



Hum removal

$$H(z) = \frac{(1 - e^{j\omega_0} z^{-1})(1 - e^{-j\omega_0} z^{-1})}{(1 - \lambda e^{j\omega_0} z^{-1})(1 - \lambda e^{-j\omega_0} z^{-1})}$$

Hum removal, $\lambda = 0.95$



Hum removal, filter structure

