

COM303: Digital Signal Processing

Lecture 19: Quantization

overview

- quantization
- ► A/D and D/A converters
- oversampling



Overview:

- Quantization
- ► Uniform quantization and error analysis
- ► Clipping, saturation, companding

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Quantization

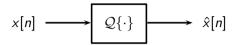
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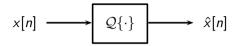
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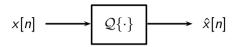
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- storage budget (bits per sample)
- storage scheme (fixed point, floating point)
- properties of the input
 - range
 - probability distribution



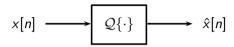
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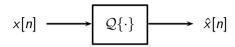
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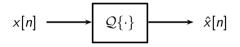
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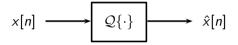
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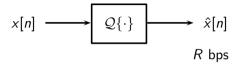
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- each sample is encoded individually (hence scalar)
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- ▶ each sample quantized over 2^R possible values $\Rightarrow 2^R$ intervals.
- each interval associated to a quantization value



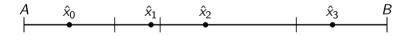
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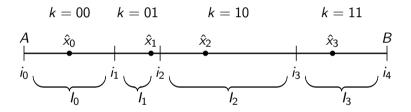


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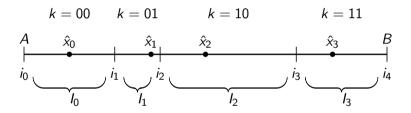


Example for R = 2:



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- ▶ what are the optimal quantization values \hat{x}_k ?

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Optimal Quantization

The optimal quantizer minimizes the energy of the quantization error:

$$e[n] = Q\{x[n]\} - x[n] = \hat{x}[n] - x[n]$$

- ightharpoonup model x[n] as a stochastic process
- ▶ find the optimal i_k and \hat{x}_k that minimize $\sigma_e^2 = \mathbb{E}\left[e^2[n]\right]$
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Quantization MSE

$$\sigma_{e}^{2} = \int_{-\infty}^{\infty} (x - Q\{x\})^{2} f_{x}(x) dx$$
$$= \sum_{k=0}^{2^{R}-1} \int_{i_{k}}^{i_{k+1}} (x - \hat{x}_{k})^{2} f_{x}(x) dx$$

find global minimum wrt $i_k,~\hat{\chi}_k$

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Simple example: optimal one-bit quantizer



3 free parameters: $i_1, \hat{x}_0, \hat{x}_1$

Simple example: optimal one-bit quantizer

$$\sigma_e^2 = \int_A^{i_1} (x - \hat{x}_0)^2 f_x(x) dx + \int_{i_1}^B (x - \hat{x}_1)^2 f_x(x) dx$$

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1:

little calculus reminder

$$\frac{\partial}{\partial t} \int_{\alpha}^{t} f(\tau) d\tau = \frac{\partial}{\partial t} [F(t) - F(\alpha)] = f(t)$$

$$\frac{\partial \sigma_{e}^{2}}{\partial i_{1}} = \frac{\partial}{\partial i_{1}} \left[\int_{A}^{i_{1}} (x - \hat{x}_{0})^{2} f_{x}(x) dx + \int_{i_{1}}^{B} (x - \hat{x}_{1})^{2} f_{x}(x) dx \right]$$

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$$\Rightarrow (\hat{x}_{0} + \hat{x}_{1})$$

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Optimal one-bit quantizer: values

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$$\Rightarrow \hat{x}_{0} = \frac{\int_{A}^{i_{1}} x f_{x}(x) dx}{\int_{A}^{i_{1}} f_{x}(x) dx} \qquad (center of mass)$$

$$\Rightarrow \hat{x}_{1} = \frac{\int_{i_{1}}^{B} x f_{x}(x) dx}{\int_{i_{1}}^{B} f_{x}(x) dx}$$

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For uniformly-distributed input

$$f_{\mathsf{x}}(\mathsf{x}) = \frac{1}{B - A}$$

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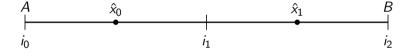
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Optimal one-bit quantizer



Uniform quantization of uniform input

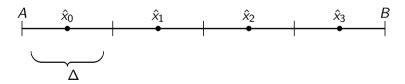
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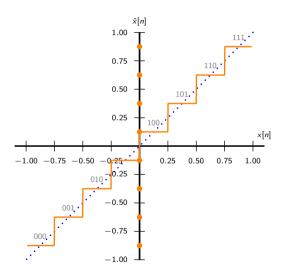
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Uniform 3-Bit quantization function



$$\sigma_{e}^{2} = \int_{A}^{B} f_{x}(x) (Q\{x\} - x)^{2} dx$$
$$= \sum_{k=0}^{2^{R} - 1} \int_{I_{k}} f_{x}(x) (\hat{x}_{k} - x)^{2} dx$$

$$f_{x}(s) = \frac{1}{B - A}$$

$$\Delta = \frac{B - A}{2^{R}}$$

$$I_{k} = [A + k\Delta, A + (k+1)\Delta]$$

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$$= 2^R \int_0^\Delta \frac{(\Delta/2 - x)^2}{B - A} dx$$
$$= \frac{\Delta^2}{12}$$

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Error analysis of the quantization error

fundamental assumptions:

- ▶ signal and quantization error are uncorrelated (ok-ish)
- quantization error process is white (stretch)

quantization noise acts as additive white noise

error energy

$$\sigma_e^2 = \Delta^2/12, \qquad \Delta = (B-A)/2^R$$

- signal energy
- signal to noise ratio

$$SNR = 2^{2R}$$

$$\mathsf{SNR}_{\mathsf{dB}} = 10 \mathsf{log}_{10} \, 2^{2R} pprox 6R \; \mathsf{dB}$$

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- ▶ in dB

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- ▶ in dB

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 $\sigma_{\rm v}^2 = (B - A)^2 / 12$

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The "6dB/bit" rule of thumb

► a compact disk has 16 bits/sample:

$$max SNR = 96dB$$

▶ a DVD has 24 bits/sample:

 $\max SNR = 144dB$

The "6dB/bit" rule of thumb

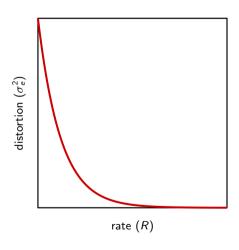
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Rate/Distortion Curve



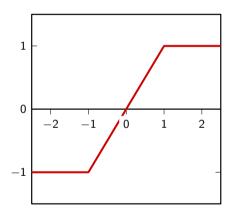
If input is not bounded to [A, B]:

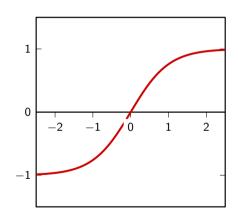
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- smoothly saturate input: this simulates the saturation curves of analog electronics

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Clipping vs saturation





If input is not uniform:

use uniform quantizer and accept increased error.
For instance, if input is Gaussian:

$$\sigma_{\rm e}^2 = \frac{\sqrt{3}\pi}{2} \, \sigma^2 \, \Delta^2$$

- use "companders"
- design optimal quantizer for input distribution, if known (Lloyd-Max algorithm)

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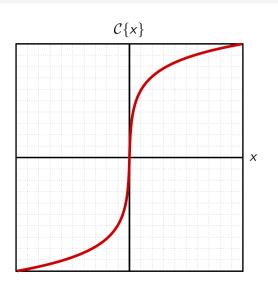
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μ -law compander

$$C\{x[n]\} = \operatorname{sgn}(x[n]) \frac{\ln(1+\mu|x[n]|)}{\ln(1+\mu)}$$



Lloyd-Max Quantizer design

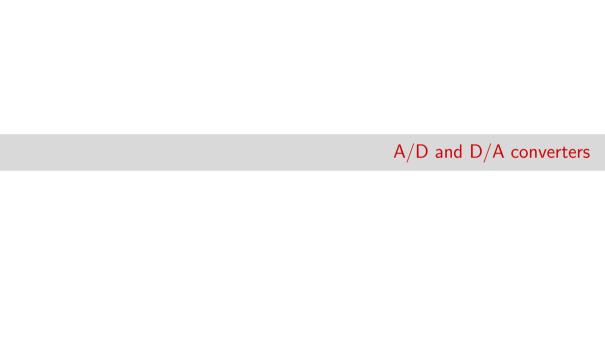
$$\sigma_{\rm e}^2 = \sum_{k=0}^{2^R-1} \int_{i_k}^{i_{k+1}} (x - \hat{x}_k)^2 f_x(x) \, dx$$

A)
$$\frac{\partial \sigma_e^2}{\partial \hat{x}_k} = 0 \Rightarrow \hat{x}_k = \frac{\int_{i_{k-1}}^{i_k} x f_x(x) dx}{\int_{i_{k-1}}^{i_k} f_x(x) dx}$$

B)
$$\frac{\partial \sigma_e^2}{\partial i_k} = 0 \Rightarrow i_k = \frac{\hat{x}_{k-1} + \hat{x}_k}{2}$$

Lloyd-Max Quantizer design

- ightharpoonup start with a guess for the i_k
- ▶ solve A and B iteratively until convergence



Overview:

- ► Analog-to-digital (A/D) conversion
- ▶ Digital-to-analog (D/A) conversion

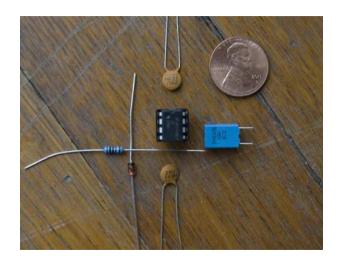
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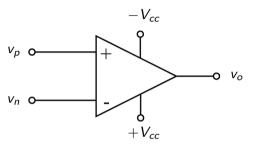
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- quantization discretized amplitude
- ▶ how is it done in practice?

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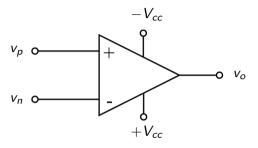


A tiny bit of electronics: the op-amp



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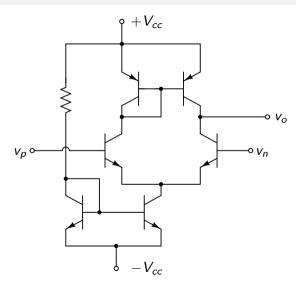
The two key properties

- ▶ infinite input gain $(G \approx \infty)$
- zero input current

The two key properties

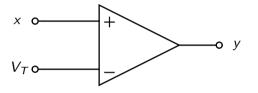
- ▶ infinite input gain $(G \approx \infty)$
- zero input current

Inside the box



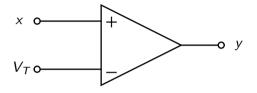
36

The op-amp in open loop: comparator



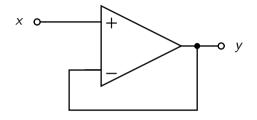
$$y = \begin{cases} +V_{cc} & \text{if } x > V_7 \\ -V_{cc} & \text{if } x < V_7 \end{cases}$$

The op-amp in open loop: comparator



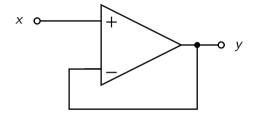
$$y = \begin{cases} +V_{cc} & \text{if } x > V_T \\ -V_{cc} & \text{if } x < V_T \end{cases}$$

The op-amp in closed loop: buffer

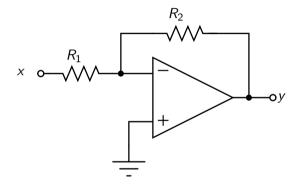


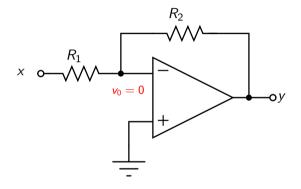
$$y = x$$

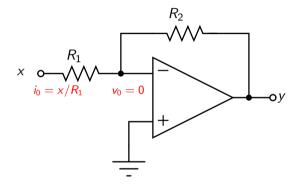
The op-amp in closed loop: buffer

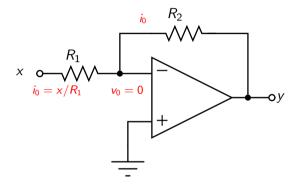


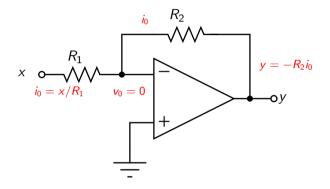
$$y = x$$

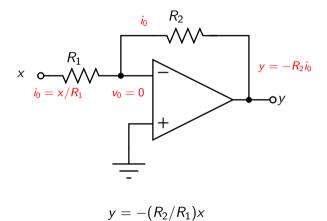




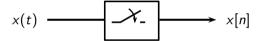




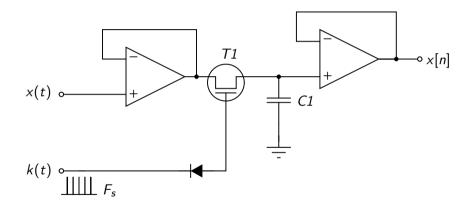




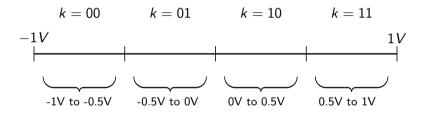
A/D Converter: Sampling

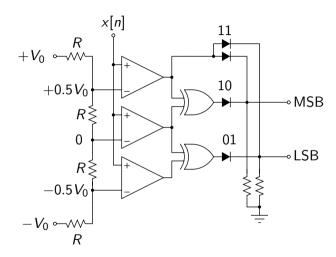


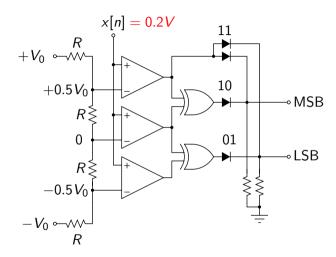
A/D Converter: Sample & Hold

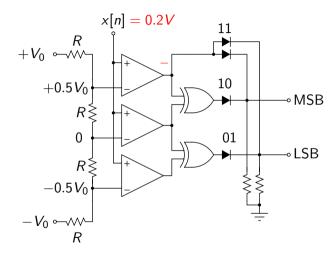


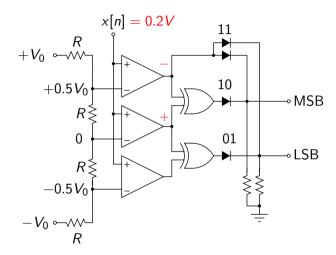
A/D Converter: Quantization

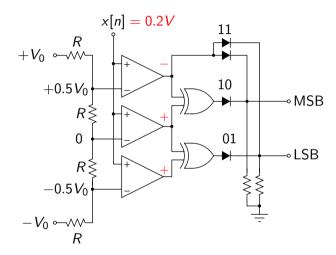


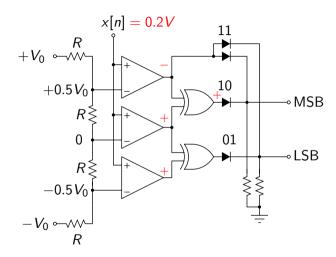


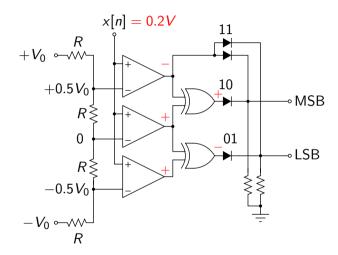


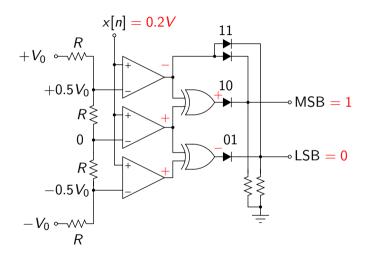




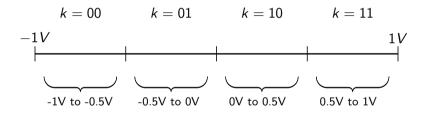








A/D Converter: Quantization

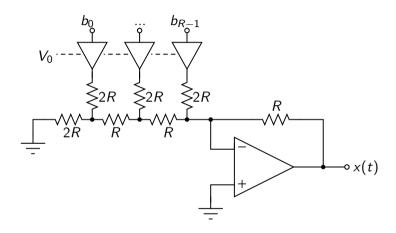


D/A Converter

$$x_B[n] = b_{R-1}b_{R-2}\dots b_1b_0$$

$$\hat{x}[n] = \sum_{k=0}^{R-1} \frac{V_0}{2^k} b_k$$

D/A Converter





Oversampling

- oversampled A/D
 - reduce quantization error

- oversampled D/A
 - use cheaper hardware for interpolation

Oversampling

- oversampled A/D
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Oversampling

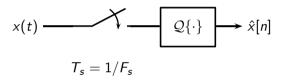
- ▶ oversampled A/D
 - reduce quantization error

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Oversampling

- oversampled A/D
 - reduce quantization error

- oversampled D/A
 - use cheaper hardware for interpolation



$$\hat{x}[n] = x[n] + e[n]$$

Key assumptions:

e[n] i.i.d. process, independent of x[n]

$$P_e(e^{j\omega}) = \frac{\Delta^2}{12}$$
 over $[-\pi, \pi]$ (no aliasing)

Key observation:

$$X(e^{j\omega}) = F_s X\left(\frac{\omega}{2\pi}F_s\right)$$

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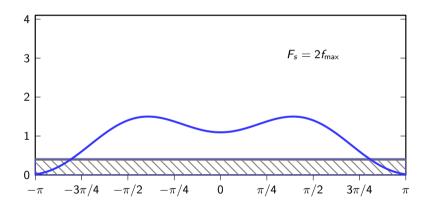
Key assumptions:

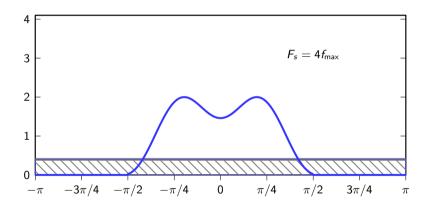
e[n] i.i.d. process, independent of x[n]

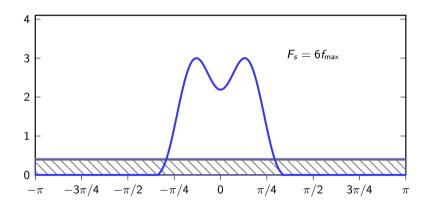
$$P_{\rm e}({
m e}^{j\omega})=rac{\Delta^2}{12}$$
 over $[-\pi,\pi]$ (no aliasing)

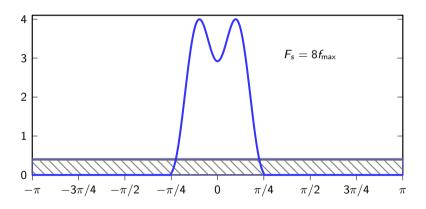
Key observation:

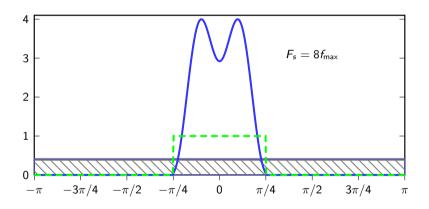
$$X(e^{j\omega}) = F_s X\left(\frac{\omega}{2\pi}F_s\right)$$

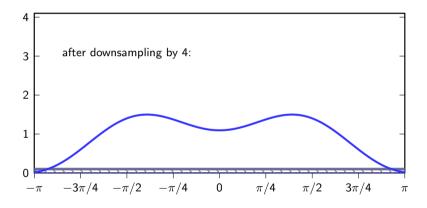


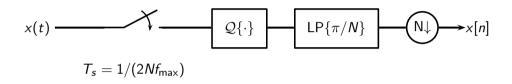




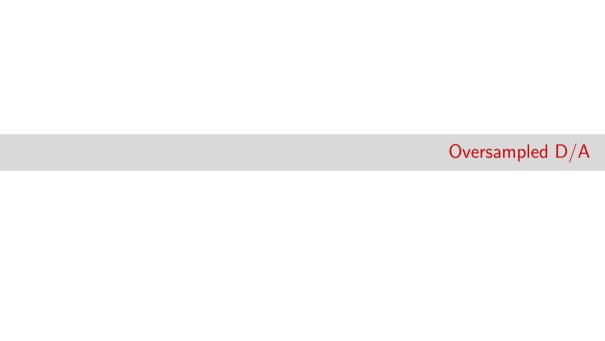




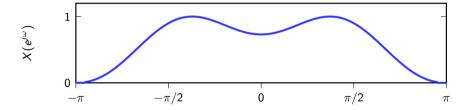


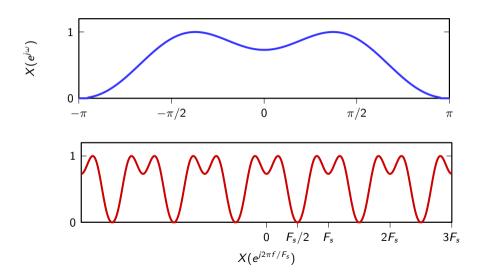


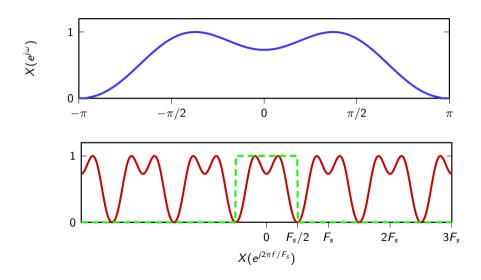
- ► $SNR_O \approx NSNR$
- ▶ 3dB per octave (doubling of F_s)
- but key assumption (independence) breaks down fast...

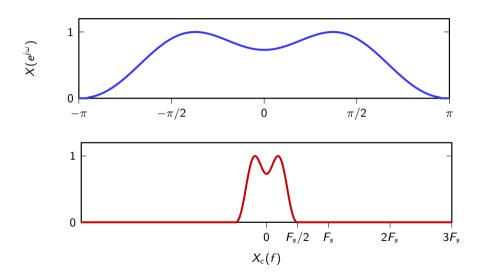


$$X_c(f) = rac{1}{F_s} X(e^{j2\pi f/F_s}) \operatorname{rect}\left(rac{f}{F_s}
ight)$$









In general:

$$X_c(f) = \frac{1}{F_s} X(e^{j2\pi f/F_s}) I\left(\frac{f}{F_s}\right)$$

The cheapest (hence most common) interpolator is the zero-order hold:

$$i_0(t) = \text{rect}(t)$$

$$f_0(f) = \operatorname{sinc}(f)$$

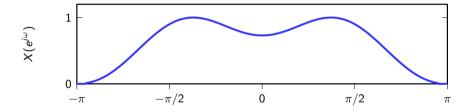
In general:

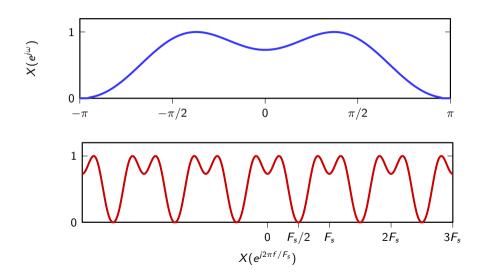
$$X_c(f) = \frac{1}{F_s} X(e^{j2\pi f/F_s}) I\left(\frac{f}{F_s}\right)$$

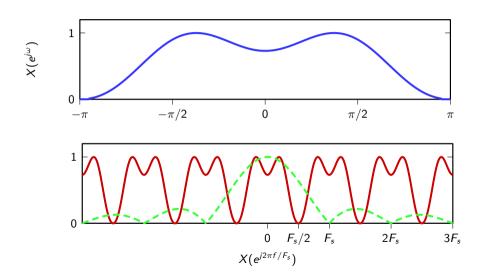
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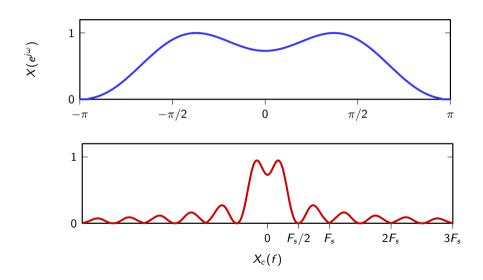
$$i_0(t) = \operatorname{rect}(t)$$

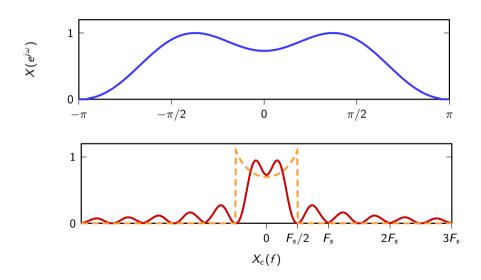
$$I_0(f) = \operatorname{sinc}(f)$$





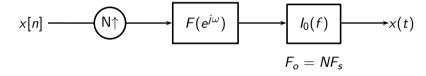






key problems:

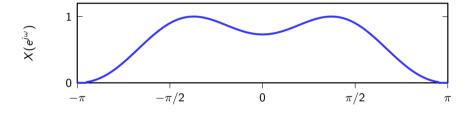
- ▶ we need to undo the in-band distortion in the analog domain
- ▶ we have a significant out-of-band distortion
- ▶ only advantage: minimal D/A rate

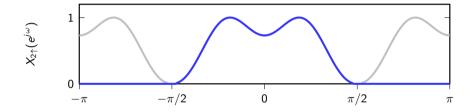


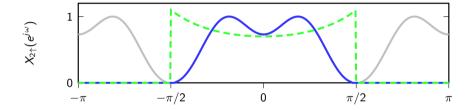
consider a N-upsampled and interpolated version of x[n]:

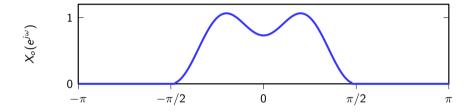
$$X_o(e^{j\omega}) = X_{N\uparrow}(e^{j\omega}) F(e^{j\omega}) = X(e^{j\omega N}) F(e^{j\omega})$$

- $ightharpoonup F(e^{j\omega}) = N \operatorname{rect}(\omega N/(2\pi)) C(e^{j\omega})$
- ▶ rect matches the upsampler
- $ightharpoonup C(e^{j\omega})$ compensates for zoh in-band distortion









interpolate $x_o[n]$ with $F_o = NF_s$:

$$X_{o}(f) = \frac{1}{F_{o}} X_{o}(e^{j2\pi f/F_{o}}) I_{0}\left(\frac{f}{F_{o}}\right)$$

$$= \frac{1}{F_{o}} \left[X(e^{j\omega N}) F(e^{j\omega})\right]_{\omega=2\pi f/F_{o}} I_{0}\left(\frac{f}{F_{o}}\right)$$

$$= \frac{N}{F_{o}} \left[X(e^{j\omega N}) \operatorname{rect}\left(\frac{\omega N}{2\pi}\right) C(e^{j\omega})\right]_{\omega=2\pi f/F_{o}} I_{0}\left(\frac{f}{F_{o}}\right)$$

$$= \frac{1}{F_{s}} X(e^{j2\pi f/F_{s}}) \operatorname{rect}\left(\frac{f}{F_{s}}\right) C(e^{j2\pi f/F_{o}}) I_{0}\left(\frac{f}{F_{o}}\right)$$

$$= X(f) \quad \text{for } |f| < F_{s}/2$$

interpolate $x_o[n]$ with $F_o = NF_s$:

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interpolate $x_o[n]$ with $F_o = NF_s$:

$$\begin{split} X_{o}(f) &= \frac{1}{F_{o}} X_{o}(e^{j2\pi f/F_{o}}) I_{0}\left(\frac{f}{F_{o}}\right) \\ &= \frac{1}{F_{o}} \left[X(e^{j\omega N}) F(e^{j\omega})\right]_{\omega=2\pi f/F_{o}} I_{0}\left(\frac{f}{F_{o}}\right) \\ &= \frac{N}{F_{o}} \left[X(e^{j\omega N}) \operatorname{rect}\left(\frac{\omega N}{2\pi}\right) C(e^{j\omega})\right]_{\omega=2\pi f/F_{o}} I_{0}\left(\frac{f}{F_{o}}\right) \\ &= \frac{1}{F_{s}} X(e^{j2\pi f/F_{s}}) \operatorname{rect}\left(\frac{f}{F_{s}}\right) C(e^{j2\pi f/F_{o}}) I_{0}\left(\frac{f}{F_{o}}\right) \\ &= X(f) \quad \text{for } |f| < F_{s}/2 \end{split}$$

interpolate $x_o[n]$ with $F_o = NF_s$:

$$\begin{split} X_o(f) &= \frac{1}{F_o} \, X_o(e^{j2\pi f/F_o}) \, I_0\left(\frac{f}{F_o}\right) \\ &= \frac{1}{F_o} \, \left[X(e^{j\omega N}) \, F(e^{j\omega}) \right]_{\omega = 2\pi f/F_o} \, I_0\left(\frac{f}{F_o}\right) \\ &= \frac{N}{F_o} \, \left[X(e^{j\omega N}) \, \operatorname{rect}\left(\frac{\omega N}{2\pi}\right) \, C(e^{j\omega}) \right]_{\omega = 2\pi f/F_o} \, I_0\left(\frac{f}{F_o}\right) \\ &= \frac{1}{F_s} \, X(e^{j2\pi f/F_s}) \, \operatorname{rect}\left(\frac{f}{F_s}\right) \, C(e^{j2\pi f/F_o}) \, I_0\left(\frac{f}{F_o}\right) \\ &= X(f) \quad \text{for } |f| < F_s/2 \end{split}$$

interpolate $x_o[n]$ with $F_o = NF_s$:

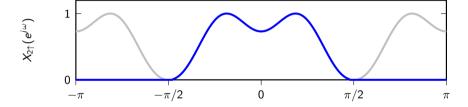
$$X_{o}(f) = \frac{1}{F_{o}} X_{o}(e^{j2\pi f/F_{o}}) I_{0}\left(\frac{f}{F_{o}}\right)$$

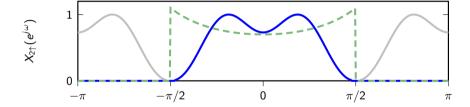
$$= \frac{1}{F_{o}} \left[X(e^{j\omega N}) F(e^{j\omega})\right]_{\omega=2\pi f/F_{o}} I_{0}\left(\frac{f}{F_{o}}\right)$$

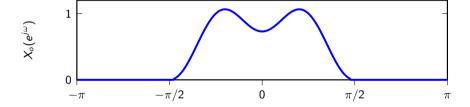
$$= \frac{N}{F_{o}} \left[X(e^{j\omega N}) \operatorname{rect}\left(\frac{\omega N}{2\pi}\right) C(e^{j\omega})\right]_{\omega=2\pi f/F_{o}} I_{0}\left(\frac{f}{F_{o}}\right)$$

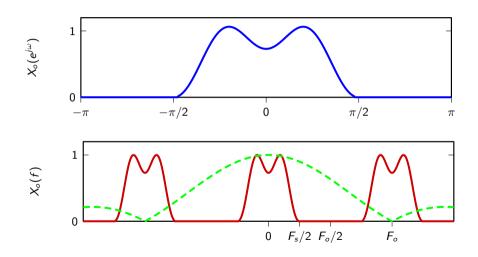
$$= \frac{1}{F_{s}} X(e^{j2\pi f/F_{s}}) \operatorname{rect}\left(\frac{f}{F_{s}}\right) C(e^{j2\pi f/F_{o}}) I_{0}\left(\frac{f}{F_{o}}\right)$$

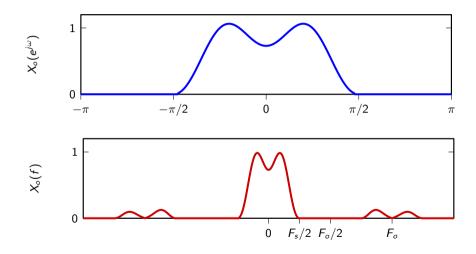
$$= X(f) \quad \text{for } |f| < F_{s}/2$$

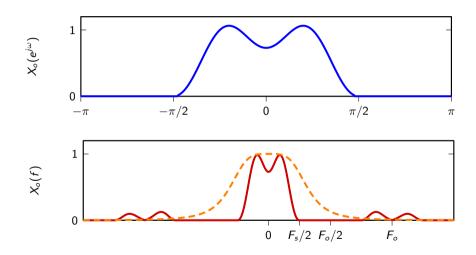












key points:

- ▶ we can pre-compensate the in-band distortion in the digital domain
- ▶ we can interpolate with a cheap ZOH
- ▶ the higher the upsampling, the cheaper the analog lowpass needed to eliminate out-of-band distortion
- ▶ only price: higher D/A rate