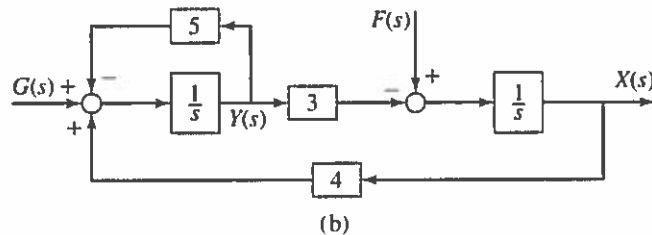


System Dynamics Exam 2

Fall 2015

The FE reference book, calculator, and 1 formula sheet may be used during this exam. Exam books provided. 10 points each.

- Find $\frac{Y(s)}{G(s)}$ for the system shown below.

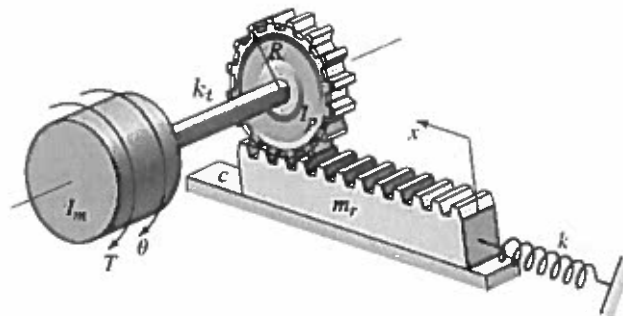


- Write the state space equation matrices A , B , C , and D for the following systems:

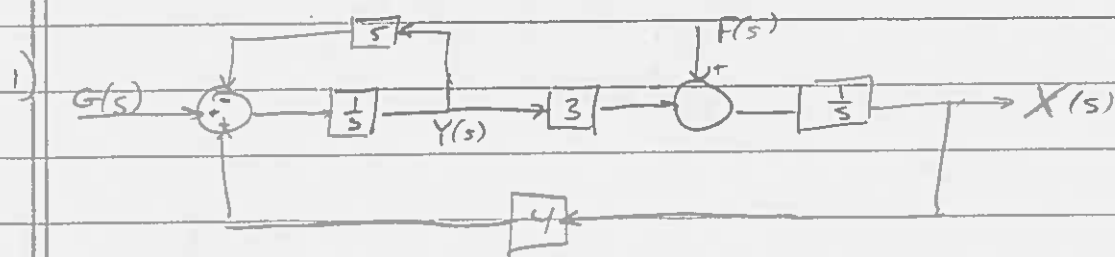
(a) $y(t)$ and $\dot{y}(t)$ are the outputs:

$$\frac{Y(s)}{F(s)} = \frac{6}{3s^3 + 63s^2 + 10}$$

- Note the torsional flexibility of the shaft k_t and derive the differential equation, or equations, of motion for the system below in terms of the unique degrees of freedom. Note the viscous friction c between the surfaces.



ME3210 System Dynamics, Fall 2015 Test 2 Solution



Find $\frac{Y(s)}{G(s)}$.

Note that $F(s)$ is not relevant

First sum block:

$$\underbrace{\left(G(s) + 4X(s) - 5Y(s) \right)}_{\text{blocks}} \frac{1}{s} = Y(s) \quad (1)$$

Second sum block:

$$-3 \frac{Y(s)}{s} = X(s) \quad (2)$$

Substitute (2) into (1)

$$G(s) - \left(\frac{12}{s} + 5 \right) Y(s) = s Y(s)$$

$$G(s) = \left(s + 5 + \frac{12}{s} \right) Y(s)$$

$$s G(s) = (s^2 + 5s + 12) Y(s)$$

$$\boxed{\frac{Y(s)}{G(s)} = \frac{s}{s^2 + 5s + 12}}$$

2)

$$3 s^3 Y(s) + 63 s^2 Y(s) + 0.5 + 10 = 6 F(s)$$

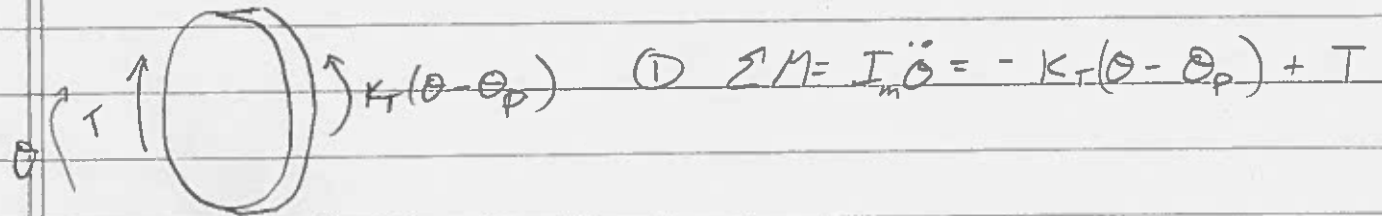
$$\ddot{y} = -\frac{10}{3} y - 21 \dot{y} + 2 F(t)$$

Define the states to be y, \dot{y} and \ddot{y}

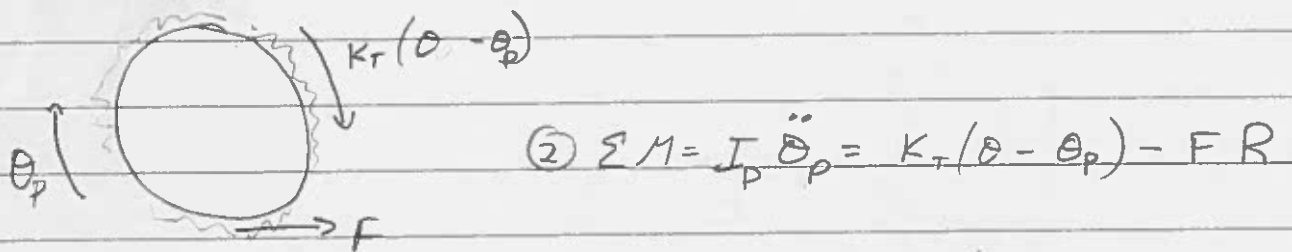
$$\dot{\underline{z}} = \begin{bmatrix} \dot{y} \\ \ddot{y} \\ \dddot{y} \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -\frac{10}{3} & 0 & -21 \end{bmatrix}}_A \underbrace{\begin{bmatrix} y \\ \dot{y} \\ \ddot{y} \end{bmatrix}}_{\underline{z}} + \underbrace{\begin{bmatrix} 0 \\ 0 \\ 2 \end{bmatrix}}_B F(t)$$

$$y = \underbrace{\begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}}_C \underbrace{\begin{bmatrix} \dot{y} \\ \ddot{y} \\ \dddot{y} \end{bmatrix}}_{\underline{z}} + \underbrace{\begin{bmatrix} 0 \\ 0 \end{bmatrix}}_D F(t)$$

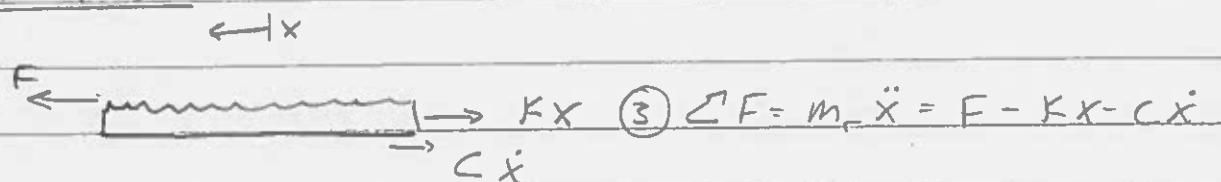
3) FBD Inertia



FBD Pinion:



FBD Rack



From Kinematics $x = R \theta_p$

(3) Becomes (4) $m_r R \ddot{\theta}_p + KR \theta_p + CR \dot{\theta}_p = F$

Substitute (4) into (2)

$$(5) \quad I_p \ddot{\theta}_p + K_T \theta_p - K_T \theta = -m_r R^2 \ddot{\theta}_p - KR^2 \theta_p - CR^2 \dot{\theta}_p$$

⑤ simplifies to

$$\star \quad \underline{(I_p + m_r R^2) \ddot{\theta}_p + c R^2 \ddot{\theta}_p + (K R^2 + K_T) \theta_p - K_T \theta = 0}$$

Equation ① and equation ⑤ are the minimum governing equations

$$\star \quad \underline{I_m \ddot{\theta} + K_T \theta - K_r \theta_p = T}$$