

ME 712 Sp '12 Exam 1

$$1) \begin{bmatrix} \epsilon_x \\ \epsilon_y \\ \gamma_{xy} \end{bmatrix} = \begin{bmatrix} \frac{\partial u}{\partial x} \\ \frac{\partial v}{\partial y} \\ \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \end{bmatrix}$$

$$\begin{bmatrix} \frac{\partial u}{\partial x} \\ \frac{\partial u}{\partial y} \end{bmatrix} = J^{-1} \begin{bmatrix} \frac{\partial u}{\partial \xi} \\ \frac{\partial u}{\partial \eta} \end{bmatrix}, \quad \begin{bmatrix} \frac{\partial v}{\partial x} \\ \frac{\partial v}{\partial y} \end{bmatrix} = J^{-1} \begin{bmatrix} \frac{\partial v}{\partial \xi} \\ \frac{\partial v}{\partial \eta} \end{bmatrix}$$

$$J = \frac{1}{4} \begin{bmatrix} -(1-\xi) & 1-\xi & 1+\xi & -(1+\xi) \\ -(1-\xi) & -(1+\xi) & 1+\xi & 1-\xi \end{bmatrix} \begin{bmatrix} x_1, y_1 \\ x_2, y_2 \\ x_3, y_3 \\ x_4, y_4 \end{bmatrix}$$

$$= \frac{1}{4} \begin{bmatrix} -2 & 2 & 0 & 0 \\ -2 & 0 & 0 & 2 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 2 \\ -1 & 0 \\ 0 & -1 \end{bmatrix}$$

$$= \frac{1}{4} \begin{bmatrix} -2 & 4 \\ -2 & -2 \end{bmatrix}$$

$$\left. \frac{\partial u}{\partial \xi} \right|_0 = \left. \frac{\partial N_2}{\partial \xi} u_3 \right|_0 = 0$$

$$\left. \frac{\partial u}{\partial \xi} \right|_0 = \left. \frac{\partial N_6}{\partial \xi} u_3 \right|_0 = 0$$

$$\left. \frac{\partial v}{\partial \xi} \right|_0 = \left. \frac{\partial N_3}{\partial \xi} u_3 \right|_0 = 0$$

$$\left. \frac{\partial v}{\partial \xi} \right|_0 = \left. \frac{\partial N_7}{\partial \xi} u_3 \right|_0 = 0$$

There is no strain at node 1 if nodes 1, 2 and 4 are fixed.

2) a)  $J$  is the most "skewed" at node 2.  
Evaluating  $J$  for the given coordinates yields

$$J = \begin{bmatrix} -\frac{1}{2} & 1 \\ -\frac{1}{2} & -1 \end{bmatrix}$$

By comparison, at node 4,  $J = \begin{bmatrix} -\frac{1}{2} & \frac{1}{2} \\ -\frac{1}{2} & -\frac{1}{2} \end{bmatrix}$

Idel is an orthogonal transformation. Norms of columns should be similar.

If  $J$  is an orthogonal transformation, then  $J^T = J^{-1}$ . The degree to which  $J \times J^T$  is diagonal can be used as an indicator.

For this case,  $J \times J^T = \begin{bmatrix} 1.25 & -0.75 \\ -0.75 & 1.25 \end{bmatrix}$

If node 2 is moved to  $y=1$ ,

$J \times J^T = \begin{bmatrix} 0.5 & 0 \\ 0 & 0.5 \end{bmatrix}$ . Applying this metric for a wide range of values  $y_2$

$0.75 < y_2 < 1.25$  result in off-diagonal terms under 25% of the diagonal terms.

b) Since this is a constant strain element, only uniformity is possible. Presuming the element passes the (yet to be discussed) patch test, simple "squareness" is all that can be used, so that the ability of strain to vary is consistent. Consistency of  $\det(J)$  throughout the element is simplest metric

across multiple elements in all directions

3)

$$K = \begin{bmatrix} \frac{12EI_x}{a^3} + \frac{12EI_y}{b^3} & \frac{-6EI_x}{a^2} & \frac{6EI_y}{b^2} \\ \frac{-6EI_x}{a^2} & \frac{4EI_x}{a} & 0 \\ \frac{6EI_y}{b^2} & 0 & \frac{4EI_y}{b} \end{bmatrix} \begin{bmatrix} v \\ \theta_1 \\ \theta_2 \end{bmatrix}$$

( $I_z$  is actually correct, but  $I_x$  was given in exam)

4) Using coordinates  $v_1, \theta_1 L, v_2, \theta_2 L$

$$K = \frac{EI_x}{L^3} \begin{bmatrix} 12 & 6 & -12 & 6 \\ 6 & 4 & 6 & 2 \\ -12 & 6 & 12 & -6 \\ 6 & 2 & -6 & 4 \end{bmatrix}$$

We can actually rotate  $90^\circ$  in either direction.  
(but that's renaming a positive  $x$  deflection, adding another problem)

$$\begin{bmatrix} d_1 \\ d_2 \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}}_{T'} \begin{bmatrix} \theta_1 \\ \theta_2 \end{bmatrix}$$

Note that  $K$  must be expanded to include  $u_1, u_2$  before rotation. Then

$$T = \begin{bmatrix} T' & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & T' \end{bmatrix}$$

$$K = \frac{EI}{L^3} \begin{bmatrix} 12 & 0 & -6 & -12 & 0 & -6 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ -6 & 0 & 4 & -6 & 0 & 2 \\ -12 & 0 & -6 & 12 & 0 & 6 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ -6 & 0 & 2 & 6 & 0 & 4 \end{bmatrix}$$

or reduced to only traditional coordinates

$$K = \frac{EI}{L^3} \begin{bmatrix} 12 & -6L & -12 & -6L \\ -6L & 4L^2 & -6L & 2L^2 \\ -12 & -6L & 12 & 6L^2 \\ -6L & 2L^2 & 6L^2 & 4L^2 \end{bmatrix}$$

Terms that differ due to rotation are circled for illustration.