

ME 460/660 Final Exam Solutions

1) $m\ddot{x} + c\dot{x} + kx = 0$

$$\ddot{x} + 2\zeta\omega\dot{x} + \omega^2x = 0$$

$$s^2 X(s) - s x_0 - \dot{x}_0 + 2\zeta\omega(sX(s) - x_0) + \omega^2 X(s) = 0$$

$$+10 \quad X(s) = \frac{s x_0 + \dot{x}_0 + 2\zeta\omega x_0}{s^2 + 2\zeta\omega s + \omega^2}$$

$$X(s) = x_0 \frac{s + \frac{\dot{x}_0}{x_0} + 2\zeta\omega}{s^2 + 2\zeta\omega s + \omega^2}$$

$$x(t) = x_0 \left(e^{-\zeta\omega t} \cos \omega_d t + \frac{\frac{\dot{x}_0}{x_0} + \zeta\omega}{\omega_d} e^{-\zeta\omega t} \sin \omega_d t \right)$$

$$+10 \quad x(t) = e^{-\zeta\omega t} \left(x_0 \cos \omega_d t + \frac{\dot{x}_0 + \zeta\omega x_0}{\omega_d} \sin \omega_d t \right)$$

$$\sqrt{\frac{2500}{(1000^2 - 1)^2 + 2500}} = 5 \times 10^{-3} < 10^{-4}$$

$$\zeta = \frac{c}{2m\omega} \quad \omega = \frac{4000}{1000} = 1.257 \text{ rad/s}$$

$$k = m\omega^2 = 47.4 \text{ N/m}$$

$$c = 2\zeta m\omega = 1.886 \text{ kg/s}$$

$$(\zeta \geq 500.4 \text{ to meet design specifications, } k \leq 18.9 \text{ N/m})$$

2) $m = 30 \text{ kg}$, $T.R. = 10^{-4}$, $\omega_d = 200 \text{ Hz}$
 $\xi = .025$

$$T.R. = \sqrt{\frac{1 + (2\xi r)^2}{(1 - r^2)^2 + (2\xi r)^2}}$$

Assume no damping + tighter design criteria to compensate. $T.R. = 1 \times 10^{-6}$

$$1 \times 10^{-6} = \frac{1}{r^2 - 1}$$

$$r^2 - 1 = 1 \times 10^6$$

$$r \approx 1000 \quad \text{choose } r = 1000$$

See if $\xi = .025$, $r = 1000$ meets original design criteria.

$$T.R. = \sqrt{\frac{1 + (2 \cdot .025 \cdot 1000)^2}{(1000^2 - 1)^2 + (2 \cdot .025 \cdot 1000)^2}}$$

$$= \sqrt{\frac{2501}{(1000^2 - 1)^2 + 2500}} = 5 \times 10^{-5} < 10^{-4}$$

$$r = \frac{\omega_d}{\omega}, \quad \omega = \frac{400\pi}{1000} = 1.257 \text{ rad/s}$$

$$K = m\omega^2 = 47.4 \text{ N/m}$$

$$C = 2\xi\omega m = 1.886 \text{ kg/s}$$

($r \geq 500.4$ to meet design specifications, $K < 189 \text{ N/m}$)

3) The natural frequencies of the individual vibration absorbers must be equal to the driving frequencies.

$$\omega_1 = \frac{1000 \cdot 2\pi}{60} = 104.72 \text{ rad/s}$$

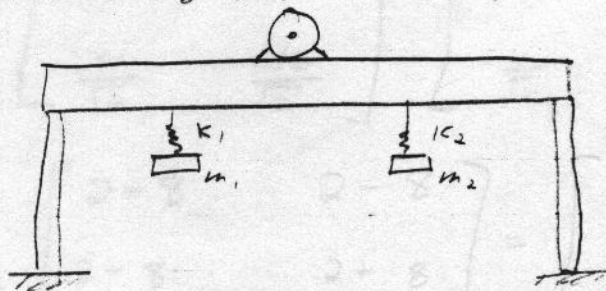
$$\omega_2 = 2\omega_1 = 209.4 \text{ rad/s}$$

Choose $N = .05$ for each absorber so that the total added mass is 10%.

$$m_1 = m_2 = 3.75 \text{ kg}$$

$$k_1 = m_1 \omega_1^2 = 41100 \text{ N/m}$$

$$k_2 = m_2 \omega_2^2 = 4m_1 \omega_1^2 = 164500 \text{ N/m}$$



They must be attached at points on the structure, not to each other.

Yes

In startup, shut-down, and switching speeds, some of the modes of the table/isolator system will be excited for short periods of time.

$$4) \quad \Lambda = \begin{bmatrix} 4 & 0 \\ 0 & 16 \end{bmatrix}$$

The mode shapes are not constrained, so we may choose them.

$$P = \begin{bmatrix} \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} \end{bmatrix}$$

Because $M = I$, $P^T \tilde{K} P = P^T K P = \Lambda$, $K = P \tilde{K} P^T$
 $(P^T)^{-1} K P^{-1}$

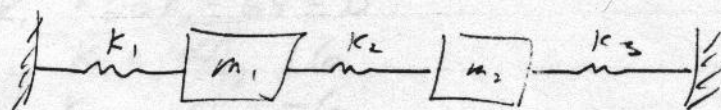
$$K = \begin{bmatrix} \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \end{bmatrix} \begin{bmatrix} 4 & 0 \\ 0 & 16 \end{bmatrix} \begin{bmatrix} \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} \end{bmatrix}$$

$$= \begin{bmatrix} \frac{4}{\sqrt{2}} & \frac{16}{\sqrt{2}} \\ \frac{4}{\sqrt{2}} & \frac{-16}{\sqrt{2}} \end{bmatrix} \begin{bmatrix} \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} \end{bmatrix}$$

$$= \begin{bmatrix} 2+8 & 2-8 \\ 2-8 & 2+8 \end{bmatrix} = \begin{bmatrix} 10 & -6 \\ -6 & 10 \end{bmatrix}$$

The stiffness matrix is $\begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 + k_3 \end{bmatrix}$

where



Thus, $k_2 = 6$, $k_1 = k_3 = 4$

$$\det \begin{bmatrix} k_1 + k_2 - \lambda & -k_2 \\ -k_2 & k_2 + k_3 - \lambda \end{bmatrix} = 0$$

IF $k_1 = k_3$

$$(k_1 + k_2 - \lambda)^2 - k_2^2 = 0$$

$$(k_1 + k_2)^2 - 2\lambda(k_1 + k_2) + \lambda^2 - k_2^2 = 0$$

$$\lambda^2 - 2(k_1 + k_2)\lambda + k_1^2 + 2k_1k_2 = 0$$

$$\lambda = 4, 16$$

$$(\lambda - 4)(\lambda - 16) = 0$$

$$\lambda^2 - 20\lambda + 64 = 0$$

① $k_1 + k_2 = 10$, ② $k_1^2 + 2k_1k_2 = 64$
 $k_2 = 10 - k_1$

① 10 ②

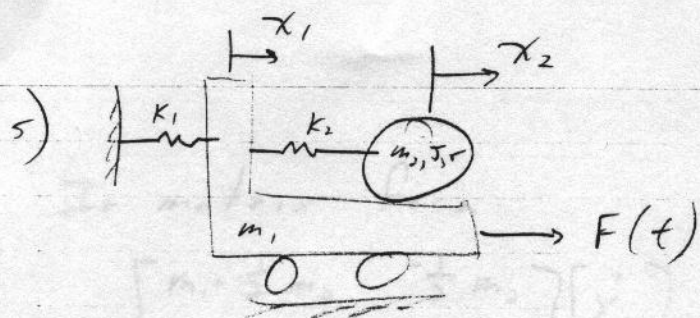
$$k_1^2 + 2k_1(10 - k_1) = 64$$

$$k_1^2 + 20k_1 - 2k_1^2 = 64$$

$$-k_1^2 + 20k_1 - 64 = 0$$

$$\begin{cases} k_1 = 4, 16 \\ k_2 = 6, -6 \end{cases}$$

$$\underline{k_1 = 4 \text{ N/m}, k_2 = 6 \text{ N/m}, k_3 = k_1 = 4 \text{ N/m}}$$



x_2 is absolute motion of disk



$$U = \frac{1}{2} k_1 x_1^2 + \frac{1}{2} k_2 (x_2 - x_1)^2 \quad + 6$$

$$T = \frac{1}{2} m_1 \dot{x}_1^2 + \frac{1}{2} m_2 \dot{x}_2^2 + \frac{1}{2} J \dot{\theta}^2$$

$$r \dot{\theta} = \dot{x}_2 - \dot{x}_1, \quad J = \frac{1}{2} m_2 r^2$$

$$T = \frac{1}{2} m_1 \dot{x}_1^2 + \frac{1}{2} m_2 \dot{x}_2^2 + \frac{1}{4} m_2 (\dot{x}_2 - \dot{x}_1)^2 \quad + 4$$

Lagrange's Eqs

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}_i} \right) - \frac{\partial T}{\partial q_i} + \frac{\partial U}{\partial q_i} = 0 \quad + 4$$

$$\begin{aligned} \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{x}_1} \right) &= m_1 \ddot{x}_1 - \frac{1}{2} m_2 (\ddot{x}_2 - \ddot{x}_1) \\ &= (m_1 + \frac{1}{2} m_2) \ddot{x}_1 - \frac{1}{2} m_2 \ddot{x}_2 \end{aligned}$$

$$\begin{aligned} \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{x}_2} \right) &= m_2 \ddot{x}_2 + \frac{1}{2} m_2 (\ddot{x}_2 - \ddot{x}_1) \\ &= -\frac{1}{2} m_2 \ddot{x}_1 + \frac{3}{2} m_2 \ddot{x}_2 \end{aligned}$$

$i=1$:

$$(m_1 + \frac{1}{2} m_2) \ddot{x}_1 - \frac{1}{2} m_2 \ddot{x}_2 + k_1 x_1 + k_2 (x_1 - x_2) = F(t)$$

$i=2$:

$$-\frac{1}{2} m_2 \ddot{x}_1 + \frac{3}{2} m_2 \ddot{x}_2 + k_2 (x_2 - x_1) = 0 \quad + 4$$

In matrix form

$$\begin{bmatrix} m_1 + \frac{1}{2} m_2 & -\frac{1}{2} m_2 \\ -\frac{1}{2} m_2 & \frac{3}{2} m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} K_1 + K_2 & -K_2 \\ -K_2 & K_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} F(t) \\ 0 \end{bmatrix}$$

$$s^2 X(s) - s x_0 - v_0 + 2 \gamma \omega (s X(s) - x_0) - \omega^2 X(s) = 0$$

$$X(s) = \frac{s x_0 + v_0 + \gamma \omega x_0}{s^2 - 2 \gamma \omega s + \omega^2}$$

$$X(s) = x_0 \frac{s - \frac{v_0}{x_0} + \gamma \omega}{s^2 - 2 \gamma \omega s + \omega^2}$$

$$x(t) = x_0 \left(e^{-\gamma \omega t} \cos \omega_d t + \frac{\frac{v_0}{x_0} - \gamma \omega}{\omega_d} e^{-\gamma \omega t} \sin \omega_d t \right)$$

$$x(t) = e^{-\gamma \omega t} \left(x_0 \cos \omega_d t + \frac{v_0 - \gamma \omega x_0}{\omega_d} \sin \omega_d t \right)$$