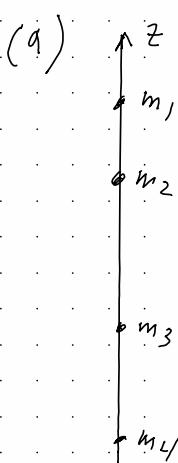


Sec 32, prob 1:



$$I_3 = 0 \text{ since } x_a = y_a = 0$$

for all masses

$$I_1 = \sum_a m_a (r_a^2 - z_a^2) = \sum_a m_a z_a^2$$

$$I_2 = \sum_a m_a (r_a^2 - z_a^2) = \sum_a m_a z_a^2$$

$$\rightarrow I_1 = I_2 = I$$

$$= \sum_a m_a z_a^2$$

(assuming COM at $z=0$)

If COM is not at $z=0$, but at z_{COM} , then:

$$\begin{aligned} I &= \sum_a m_a (z_a - z_{\text{COM}})^2, \quad z_{\text{COM}} = \frac{1}{M} \sum_b m_b z_b \\ &= \sum_a m_a (z_a^2 + z_{\text{COM}}^2 - 2z_{\text{COM}} z_a) \\ &= \sum_a m_a z_a^2 + M z_{\text{COM}}^2 - 2z_{\text{COM}} \underbrace{\sum_a m_a z_a}_{M z_{\text{COM}}} \\ &= \sum_a m_a z_a^2 - M z_{\text{COM}}^2 \end{aligned}$$

This last expression can be written in terms of $d_{ab} \equiv |z_a - z_b|$ as follows:

$$\begin{aligned} I &= \frac{1}{2} \sum_a m_a z_a^2 + \frac{1}{2} \sum_b m_b z_b^2 - \frac{1}{M} \left(\sum_a m_a z_a \right) \left(\sum_b m_b z_b \right) \\ &\approx \frac{1}{2M} \sum_a m_b m_a z_a^2 + \frac{1}{2M} \sum_{a,b} m_a m_b z_a^2 - \frac{1}{M} \sum_a m_a m_b z_a z_b \end{aligned}$$

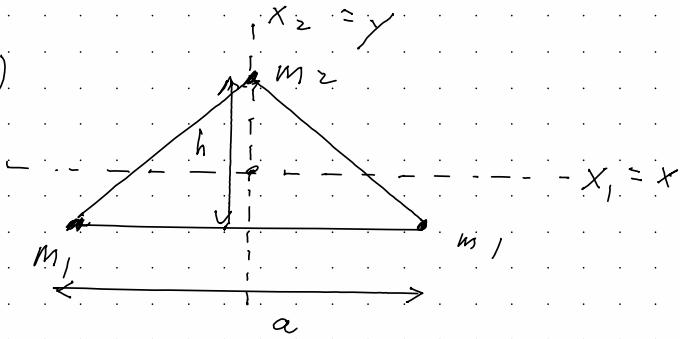
Thus

$$\begin{aligned} I &= \frac{1}{2M} \sum_a \sum_b m_a m_b (z_a^2 + z_b^2 - 2z_a z_b) \\ &= \frac{1}{2M} \sum_a \sum_b m_a m_b (z_a - z_b)^2 \\ &= \frac{1}{2M} \sum_a \sum_b m_a m_b l_{a,b}^2 \end{aligned}$$

NOTE: For just two masses:

$$\begin{aligned} I &= \frac{1}{2M} (m_1 m_2 l^2 + m_2 m_1 l^2) \\ &= \frac{m_1 m_2}{M} l^2 \\ &= m l^2 \quad \text{where } m = \frac{m_1 m_2}{m_1 + m_2} \\ l &= |z_1 - z_2| \end{aligned}$$

(b)



Assume COM at $(x_1, x_2) = (x, y) \approx (0, 0)$

$$\text{Then } 2m_1y_1 + m_2y_2 = 0$$

$$\text{where } y_2 - y_1 = h$$

$$\text{thus, } 2m_1y_1 + m_2(h + y_1) = 0$$

$$(2m_1 + m_2)y_1 + m_2h = 0$$

$$y_1 = \frac{-m_2h}{\mu}, \quad \mu = 2m_1 + m_2 \\ = \text{total mass}$$

$$\begin{aligned} \text{and } y_2 &= y_1 + h \\ &= \frac{-m_2h}{\mu} + h \\ &= \frac{(\mu - m_2)h}{\mu} \\ &= \frac{2m_1h}{\mu} \end{aligned}$$

All masses have $z_a = 0$

$$\text{Thus, } I_3 = \sum_a m_a(r_a^2 - z_a^2) = \sum_a m_a(x_a^2 + y_a^2)$$

$$I_1 = \sum_a m_a(r_a^2 - x_a^2) = \sum_a m_a y_a^2$$

$$I_2 = \sum_a m_a (r_a^2 - x_a^2) = \sum_a m_a x_a^2$$

$$\text{Thus, } I_3 = I_1 + I_2$$

so need to calculate I_1, I_2

$$I_1 = \sum_a m_a y_a^2$$

$$= 2m_1 y_1^2 + m_2 y_2^2$$

$$= 2m_1 \frac{m_2^2 h^2}{m^2} + m_2 \frac{4m_1^2 h^2}{m^2}$$

$$= \frac{2m_1 m_2 h^2}{m^2} (m_2 + 2m_1)$$

$$= \boxed{\frac{2m_1 m_2 h^2}{m}}$$

$$I_2 = \sum_a m_a x_a^2$$

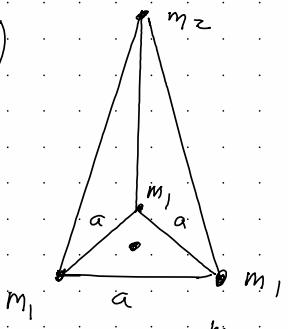
$$= m_1 \left(\frac{a}{z}\right)^2 + m_2 \left(\frac{-a}{z}\right)^2$$

$$= \boxed{\frac{m_1 a^2}{z}}$$

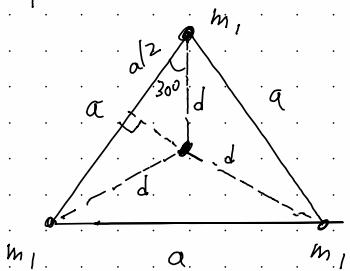
$$I_3 = I_1 + I_2$$

$$= \boxed{\frac{2m_1 m_2 h^2 + \frac{m_1 a^2}{z}}{m}}$$

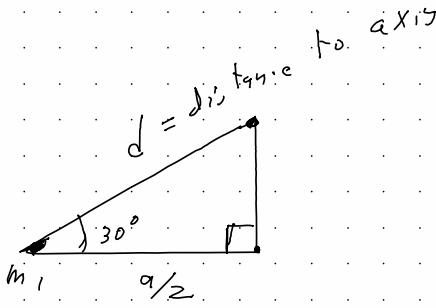
(c)



tetrahedron, height h
base: equilateral \triangle with
side length a



base



$$\cos 30^\circ = \frac{a}{2d} = \frac{\sqrt{3}}{2}$$

$$\rightarrow d = \frac{a}{\sqrt{3}}$$

COM lies on axis of symmetry (Z -axis)

Assume COM has $Z=0$

$$\begin{aligned} \text{Then } O &= m_2 z_2 + 3m_1 z_1, \quad z_2 - z_1 = h \\ &= m_2 (z_1 + h) + 3m_1 z_1 \\ &= (3m_1 + m_2) z_1 + m_2 h \\ \rightarrow z_1 &= \frac{-m_2 h}{3m_1 + m_2} = \frac{-m_2 h}{\mu} \end{aligned}$$

$$\begin{aligned} z_2 &= h + z_1 \\ &= h - \frac{m_2 h}{\mu} \\ &= \frac{3m_1 h}{\mu} \end{aligned}$$

Since a tetrahedron has 3-fold rotational symmetry, the x_1 principal axes can be chosen arbitrarily in the plane \perp to the symmetry axis ($x_3 \hat{=} z$). [x_2 is \perp to x_1, x_3]

$$\text{Thus, } I_1 = I_2 \equiv I$$

$$I_3 = \sum_a m_a (r_a^2 - z_a^2) \\ = \sum_a m_a s_a^2 \quad \text{where } s^2 = r^2 - z^2$$

$$I_1 = \sum_a m_a (r_a^2 - x_a^2) \\ I_2 = \sum_a m_a (r_a^2 - y_a^2) \quad \Rightarrow \text{equal} \quad (I_1 = I_2 \equiv I)$$

$$2I = I_1 + I_2 \\ = \sum_a m_a (2r_a^2 - x_a^2 - y_a^2) \\ = \sum_a m_a (2(s_a^2 + z_a^2) - s_a^2) \\ = \sum_a m_a s_a^2 + 2 \sum_a m_a z_a^2 \\ = I_3 + 2 \sum_a m_a z_a^2$$

$$\text{Thus,}$$

$$I = \frac{1}{2} I_3 + \sum_a m_a z_a^2$$

Now

$$I_3 = \sum_a m_a s_a^2 \\ = 3 m_1 d^2 \\ = \cancel{\frac{1}{2}} m_1 \frac{q^2}{\cancel{2}} = \boxed{m_1 q^2}$$

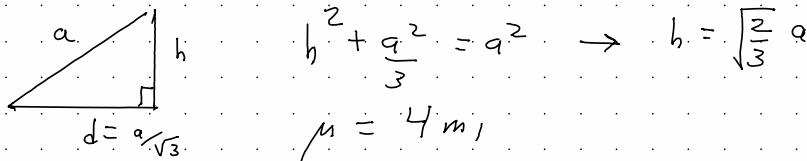
A/so,

$$\begin{aligned}\sum_q m_q z_q^2 &= 3m_1 z_1^2 + m_2 z_2^2 \\&= 3m_1 \left(-\frac{m_2 h}{M}\right)^2 + m_2 \left(\frac{3m_1 h}{M}\right)^2 \\&= \frac{3m_1 m_2 h^2}{M^2} + \frac{9m_1^2 m_2 h^2}{M} \\&= \frac{3m_1 m_2 h^2}{M^2} \underbrace{\left(m_2 + 3m_1\right)}_{M} \\&= \frac{3m_1 m_2 h^2}{M}\end{aligned}$$

Thus,

$$\begin{aligned}I &= \frac{1}{2} I_3 + \sum_q m_q z_q^2 \\&= \boxed{\frac{1}{2} m_1 q^2 + \frac{3m_1 m_2 h^2}{M}}\end{aligned}$$

Regular tetrahedron: $m_1 = m_2$



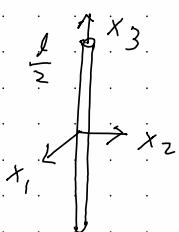
$$b^2 + \frac{a^2}{3} = a^2 \rightarrow b = \sqrt{\frac{2}{3}} a$$

$$M = 4m_1$$

$$\left. \begin{aligned}I_3 &= m_1 a^2 \\I &= \frac{1}{2} m_1 a^2 + \frac{B m_1 m_1}{4m_1} \left(\frac{2}{3}\right) a^2 \\&= m_1 a^2 (= I_1 = I_2)\end{aligned} \right\} \begin{array}{l} \text{so } I_1 = I_2 \\ = I_3 = m_1 a^2 \end{array}$$

Sec 32, Prob 2

(a) Thin rod of length ℓ :



$$I_3 = [0]$$

$$\text{and } I_1 = I_2 \equiv I$$

$$I = \int \rho dV (r^2 - x^2)$$

$$= \int \rho dV z^2$$

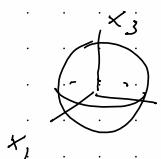
$$= \int dz \left(\frac{\mu}{\ell}\right) z^2$$

$$= \frac{\mu}{\ell} \cdot \frac{z^3}{3} \Big|_{-l/2}^{l/2}$$

$$= \frac{\mu}{\ell} \cdot \frac{2}{3} \frac{l^3}{8}$$

$$= \boxed{\frac{1}{12} \mu l^2}$$

(b) Sphere of radius R :



$$I_1 = I_2 = I_3 \equiv I$$

$$I = \frac{1}{3}(I_1 + I_2 + I_3)$$

$$= \frac{1}{3} \left[\int \rho dV (r^2 - x^2) + \int \rho dV (r^2 - y^2) + \int \rho dV (r^2 - z^2) \right]$$

$$= \frac{1}{3} \int \rho dV [3r^2 - x^2 - y^2 - z^2]$$

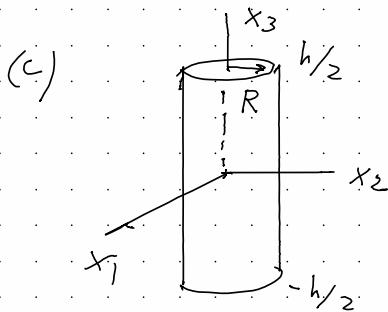
$$= \frac{2}{3} \int \rho dV r^2$$

$$\begin{aligned}
 I &= \frac{2}{3} \int \rho dV \cdot r^2 \\
 &= \frac{2}{3} \frac{M}{4\pi R^3} \int_0^R r^4 dr \underbrace{\int_0^\pi \sin^2 \theta d\theta \int_0^{2\pi} d\phi}_{4\pi} \\
 &= \frac{M}{2\pi R^3} \cdot 4\pi \int_0^R r^4 dr
 \end{aligned}$$

$$\rho = \frac{M}{\frac{4}{3}\pi R^3}$$

$$= \frac{2M}{R^3} \cdot \frac{R^5}{5}$$

$$= \boxed{\frac{2}{5} \mu R^2}$$



$$\rho = \frac{M}{\pi R^2 \cdot h}$$

$$dV = dr \cdot s \cdot d\phi \cdot dz$$

where $s^2 = x^2 + y^2$

$$I_1 = I_2 = L$$

$$2L = I_1 + I_2$$

$$= \int \rho dV (r^2 - x^2) + \int \rho dV (r^2 - y^2)$$

$$= \int \rho dV (2r^2 - s^2)$$

$$= \int \rho dV s^2 + 2 \int \rho dV z^2$$

$$= \int \rho dV s^2 + 2 \int \rho dV z^2$$

$$\rightarrow I = \frac{1}{2} I_3 + \int \rho dV \cdot z^2$$

$$\begin{aligned}
 I_3 &= \int \rho dV z^2 \\
 &= \frac{M}{\pi R^2 h} \int_0^R s^3 ds \int_0^{2\pi} d\phi \int_{-h/2}^{h/2} dz \\
 &= \frac{M}{\pi R^2 h} \cdot \frac{R^4}{4} \cdot 2\pi \cdot h \\
 &= \boxed{\frac{1}{2} M R^2}
 \end{aligned}$$

$$\begin{aligned}
 I &= \frac{1}{2} I_3 + \int \rho dV z^2 \\
 \int \rho dV z^2 &= \frac{M}{\pi R^2 h} \int_0^R s^3 ds \int_0^{2\pi} d\phi \int_{-h/2}^{h/2} z^2 dz \\
 &= \frac{M}{\pi R^2 h} \cdot \frac{R^4}{4} \cdot 2\pi \cdot \left[\frac{z^3}{3} \right]_{-h/2}^{h/2} \\
 &= \frac{M}{h} \cdot \frac{2}{3} \cdot \frac{h^3}{8} \\
 &= \frac{1}{12} M h^2
 \end{aligned}$$

Thus,

$$\begin{aligned}
 I &= \frac{1}{2} \left(\frac{1}{2} M R^2 \right) + \frac{1}{12} M h^2 \\
 &= \frac{1}{4} M R^2 + \frac{1}{12} M h^2 \\
 &= \boxed{\frac{1}{4} M (R^2 + \frac{1}{3} h^2)}
 \end{aligned}$$

Note: special limit by considering

(i) Thin rod ($R \rightarrow 0$)

$$I_3 = 0$$

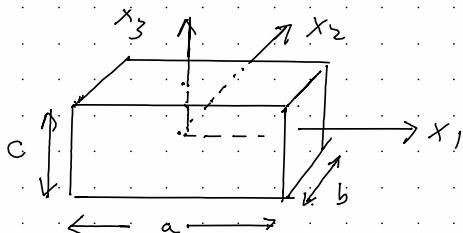
$$I_1 = I_2 = \frac{1}{12} M h^2$$

(ii) Thin disk ($h \rightarrow 0$)

$$I_3 = \frac{1}{2} M R^2$$

$$I_1 = I_2 = \frac{1}{4} M R^2$$

(d)



$$\rho = \frac{M}{abc}$$

$$dV = dx dy dz$$

$$I_1 = \int \rho dV (r^2 - x^2)$$

$$= \int \rho dV (y^2 + z^2)$$

$$= \frac{M}{abc} \int_{-a/2}^{a/2} dx \int_{-b/2}^{b/2} dy \int_{-c/2}^{c/2} dz (y^2 + z^2)$$

$$= \frac{M}{abc} \times \int_{-b/2}^{b/2} dy \left(y^2 z + \frac{z^3}{3} \right) \Big|_{-c/2}^{c/2}$$

$$= \frac{M}{bc} \int_{-b/2}^{b/2} dy \left(cy^2 + \frac{z^2}{3} \cdot \frac{c^3}{8} \right)$$

$$= \frac{M}{bc} \left[\frac{cy^3}{3} \Big|_{-b/2}^{b/2} + \frac{1}{12} c^3 z \Big|_{-b/2}^{b/2} \right]$$

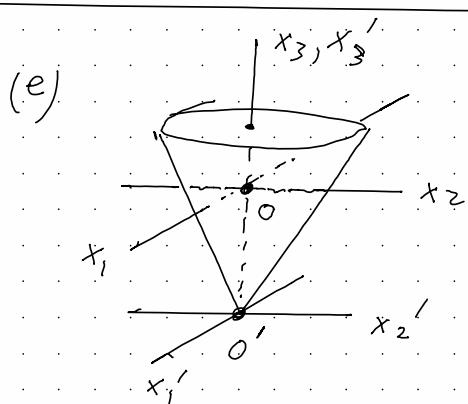
$$I_1 = \frac{M}{bc} \left[c \cdot \frac{b^3}{3} + \frac{1}{12} b c^3 \right]$$

$$= \frac{M}{12bc} [cb^3 + bc^3]$$

$$= \frac{M}{12} (b^2 + c^2)$$

$$I_2 = \frac{M}{12} (c^2 + a^2)$$

$$I_3 = \frac{M}{12} (a^2 + b^2)$$



First calculate

$$I_{ij}' \text{ (wrt } x_1', x_2', x_3' \text{)}.$$

Then calculate I_{ij} via

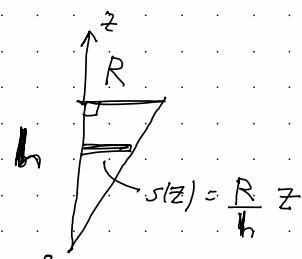
$$I_{ij} = I_{ij}' - M(a^2 \delta_{ij} - a_i a_j)$$

where $\vec{a} = (0, 0, -d)$

d : height of COM above O'

Volume of cone:

$$\begin{aligned} V &= \int dV \\ &= \int_0^h dz \int_0^{2\pi} d\phi \int_0^{\frac{R}{h}z} s ds \\ &= \pi R^2 \int_0^h z^2 dz \Big|_0^{R^2/h} \end{aligned}$$



$$V = \pi \int_0^h dz \frac{R^2 z^2}{h^2}$$

$$= \frac{\pi R^2}{h^2} \frac{z^3}{3} \Big|_0^h$$

$$= \frac{\pi R^2}{h^2} \frac{h^3}{3}$$

$$= \boxed{\frac{1}{3} \pi R^2 h}$$

Then, $\rho = \frac{M}{V} = \boxed{\frac{M}{\frac{1}{3} \pi R^2 h}}$ (mass density)

$$\begin{aligned} I_3' &= \int \rho dV (r^2 - z^2) \\ &= \int \rho dV r^2 \\ &= \rho \int_0^h dz \int_0^{2\pi} d\phi \int_0^{R^2/h} r^3 dr \\ &= \frac{\rho}{4} \cdot 2\pi \int_0^h dz \int_0^{R^2/h} s^4 ds \Big|_0^{\frac{R^2}{h}} \\ &= \frac{\rho \pi}{2} \int_0^h dz \left(\frac{R^4}{h^4} \right) z^4 \end{aligned}$$

$$= \frac{\rho \pi R^4}{2 h^4} \frac{h^5}{5}$$

$$= \boxed{\frac{\rho \pi R^4 h}{10}}$$

Thus,

$$I_3' = \frac{M}{\frac{1}{3}\pi R^2 h} \cdot \frac{\pi}{10} R^4 h$$

$$= \boxed{\frac{3}{10} M R^2}$$

similar to the cylinder, we have

$$I_1' = I_2' \equiv I'$$

$$I' = \frac{1}{2} I_3' + \int \rho dV z^2$$

Now:

$$\int \rho dV z^2 = \rho \int dz z^2 \int d\phi \int s ds$$

$$= \frac{1}{2} \pi \rho \int_0^h dz z^2 \left. \frac{s^2}{2} \right|_{0}^{Rz/h}$$

$$= \pi \rho \frac{R^2}{h^2} \int_0^h dz z^4$$

$$= \frac{\pi}{5} \rho \frac{R^2}{h^2} \frac{h^5}{5}$$

$$= \frac{\pi}{5} \rho R^2 h^3$$

$$= \frac{\pi}{5} \left(\frac{M}{\frac{1}{3} \pi R^2 h} \right) R^2 h^3$$

$$= \frac{3}{5} M h^2$$

So

$$I' = \frac{1}{2} \left(\frac{3}{10} \mu R^2 \right) + \frac{3}{5} \mu h^2$$
$$= \boxed{\frac{3}{5} \mu \left(\frac{R^2}{4} + h^2 \right)} = I_1' = I_2'$$

~~~~~  
Need to find location of COM:

$$J = \frac{1}{M} \int \rho dV z$$
$$= \frac{1}{\mu} \rho \int_0^h \int_0^{2\pi} \int_0^{Rz/h} s ds d\phi dz$$
$$= \frac{1}{\mu} \rho \cdot 2\pi \int_0^h z dz \frac{1}{2} \left( \frac{R}{h} \right)^2 z^2$$
$$= \frac{\pi \rho}{\mu} \frac{R^2}{h^2} \frac{z^4}{4} \Big|_0^h$$
$$= \frac{\pi \rho}{4\mu} R^2 h^2$$
$$= \frac{\pi}{4\mu} \frac{\mu}{\frac{1}{4}\pi R^2 h} R^2 h^2$$
$$= \boxed{\frac{3}{4} h}$$

Thus,

$$I_{ij} = I_{ij}' - \mu (a^2 \delta_{ij} - a_i a_j)$$

where  $\vec{a} = (0, 0, -\frac{3}{4}h) \rightarrow a^2 = \frac{9}{16}h^2$

$$\begin{aligned} \rightarrow I_1 &= I_1' - \mu a^2 \\ &= \frac{3}{5} \mu \left( \frac{R^2}{4} + h^2 \right) - \mu \frac{9}{16} h^2 \\ &= \frac{3}{20} \mu R^2 + \mu h^2 \left( \underbrace{\frac{3}{5} - \frac{9}{16}}_{\frac{48 - 45}{80}} \right) \\ &= \frac{3}{80} \end{aligned}$$

$$= \boxed{\frac{3}{20} \mu \left( R^2 + \frac{h^2}{4} \right)}$$

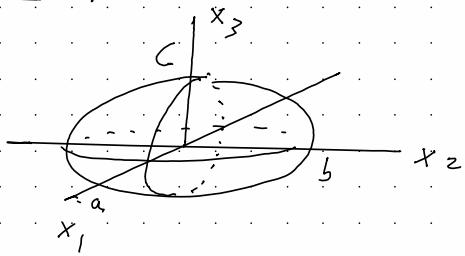
Also,  $I_2 = I_1$

Finally,  $I_3 = I_3' - \mu (a^2 - a^2) \rightarrow 0$

$$= I_3'$$

$$= \boxed{\frac{3}{10} \mu R^2}$$

(f) Ellipsoid with semi-axes  $a, b, c$



$$(a, b, c) \leftrightarrow (x_1, x_2, x_3)$$

Define rescaled coordinates:

$$(u, v, w) = \left( \frac{x_1}{a}, \frac{x_2}{b}, \frac{x_3}{c} \right)$$

so flat boundary of ellipsoid

$$1 = \left( \frac{x_1}{a} \right)^2 + \left( \frac{x_2}{b} \right)^2 + \left( \frac{x_3}{c} \right)^2 = u^2 + v^2 + w^2$$

unit 2-sphere.

Volume:

$$\begin{aligned} V &= \int dx_1 \int dx_2 \int dx_3 \\ &= abc \int_{-2\pi}^{2\pi} du \int_{-\pi}^{\pi} dv \int_0^1 dw \\ &= abc \int_0^{\pi} d\phi \int_0^{\pi} \sin\theta d\theta \int_0^1 r^2 dr \\ &= abc [2\pi \cdot 2 \cdot \frac{r^3}{3}]_0^1 \\ &= \boxed{\frac{4}{3}\pi abc} \end{aligned}$$

$$\rightarrow \rho = \frac{\mu}{\frac{4}{3}\pi abc}$$

$$\begin{aligned}
 I_3 &= \int \rho dV (r^2 - z^2) \\
 &= \int \rho dV (x^2 + y^2) \\
 &= \frac{M}{\frac{4}{3}\pi abc} \iiint dx dy dz (x^2 + y^2) \\
 &= \frac{M}{\frac{4}{3}\pi abc} \iiint du dv dw (a^2 u^2 + b^2 v^2) \\
 &= \frac{M}{\frac{4}{3}\pi r^2} \int r^2 dr \int_{\sin^{-1}\theta}^{\pi} d\theta \int_0^{2\pi} d\phi (a^2 r^2 \sin^2\theta \cos^2\phi \\
 &\quad + b^2 r^2 \sin^2\theta \sin^2\phi) \\
 \text{Now: } \int_{0}^{\pi} \sin^2\theta d\theta \sin^2\theta &= \int_0^{\pi} d(\cos\theta) (1 - \cos^2\theta) \\
 &= \int_{-1}^1 dx (1 - x^2) \\
 &= \left[ x - \frac{x^3}{3} \right] \Big|_1^1 \\
 &= 2 \cdot \frac{2}{3} = \boxed{\frac{4}{3}}
 \end{aligned}$$

$$\int_0^1 r^4 dr = \frac{r^5}{5} \Big|_0^1 = \boxed{\frac{1}{5}}$$

$$\int_0^{2\pi} d\phi \left\{ \begin{matrix} \sin^2 \phi \\ \cos^2 \phi \end{matrix} \right\} = 2\pi \cdot \frac{1}{2} = [2\pi]$$

Thus,

$$I_3 = \frac{M}{\frac{4}{3}\pi} \left( a^2 \frac{4}{3} \cdot \frac{1}{5} \cdot \pi + b^2 \frac{4}{3} \cdot \frac{1}{5} \cdot \pi \right)$$

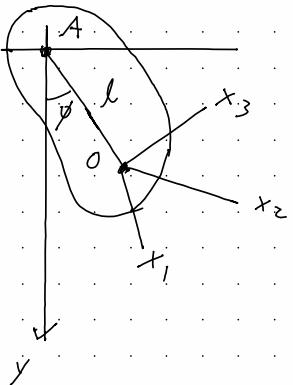
$$= \boxed{\frac{M}{5} (a^2 + b^2)}$$

cyclically permuting  $a, b, c \rightarrow$

$$\boxed{I_1 = \frac{M}{5} (b^2 + c^2)}$$

$$I_2 = \frac{M}{5} (c^2 + a^2)$$

Sec 32, Prob 3:



com at  $\vec{O}$   
rotation axis at A, out of page  
 $\vec{\omega} = \dot{\phi} \hat{n}$

$$U = \mu g l (1 - \cos \phi)$$

$$\approx \frac{1}{2} \mu g l \phi^2 \quad \text{for } \phi \ll 1$$

$$L = T - U$$

$$T = \frac{1}{2} \mu V^2 + \frac{1}{2} (I_1 \Omega_1^2 + I_2 \Omega_2^2 + I_3 \Omega_3^2)$$

$$\vec{\omega} = \dot{\phi} \hat{n} \rightarrow \Omega_1 = \dot{\phi} \hat{n} \cdot \hat{x}_1 = \dot{\phi} \cos \alpha$$

$$\Omega_2 = \dot{\phi} \hat{n} \cdot \hat{x}_2 = \dot{\phi} \cos \beta$$

$$\Omega_3 = \dot{\phi} \hat{n} \cdot \hat{x}_3 = \dot{\phi} \cos \gamma$$

$$V = \lambda \phi$$

Thru,

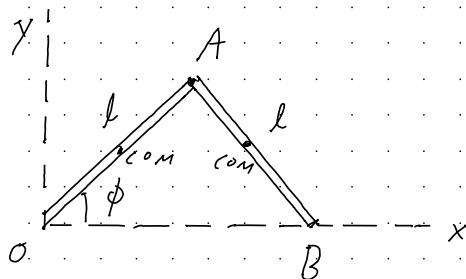
$$T = \frac{1}{2} \mu l^2 \dot{\phi}^2 + \frac{1}{2} \dot{\phi}^2 (I_1 \cos^2 \alpha + I_2 \cos^2 \beta + I_3 \cos^2 \gamma)$$

so

$$L = \frac{1}{2} \dot{\phi}^2 / \mu l^2 + I_1 \cos^2 \alpha + I_2 \cos^2 \beta + I_3 \cos^2 \gamma - \frac{1}{2} \mu g l \dot{\phi}^2$$

$$\rightarrow w = \sqrt{\frac{\mu g l}{\mu l^2 + I_1 \cos^2 \alpha + I_2 \cos^2 \beta + I_3 \cos^2 \gamma}}$$

Sec 32, P, b 4



two uniform rods

$$I_{\text{com}} = \frac{1}{12} M l^2$$

$$I_{\text{end}} = \frac{1}{3} M l^2$$

$$T = T_1 + T_2$$

$$T_1 = \frac{1}{2} M \left(\frac{l}{2}\right)^2 \dot{\phi}^2 + \frac{1}{2} I_{\text{com}} \dot{\phi}^2$$

$$= \frac{1}{8} M l^2 \dot{\phi}^2 + \frac{1}{24} M l^2 \dot{\phi}^2$$

$$= \left(\frac{1}{8} + \frac{1}{24}\right) M l^2 \dot{\phi}^2$$

$$= \frac{1}{6} M l^2 \dot{\phi}^2$$

$$T_2 = \frac{1}{2} M V^2 + \frac{1}{2} I_{\text{com}} \dot{\phi}^2$$

$$\text{Now: } V^2 = \dot{x}^2 + \dot{y}^2$$

$$x = \frac{3}{2} l \cos \phi, \quad y = \frac{1}{2} \sin \phi$$

$$\dot{x} = -\frac{3}{2} l \sin \phi \dot{\phi}, \quad \dot{y} = \frac{1}{2} \cos \phi \dot{\phi}$$

$$\rightarrow V^2 = \frac{9}{4} l^2 \sin^2 \phi \dot{\phi}^2 + \frac{l^2}{4} \cos^2 \phi \dot{\phi}^2$$

$$= 2 l^2 \sin^2 \phi \dot{\phi}^2 + \frac{l^2}{4} \dot{\phi}^2$$

$$= 2 l^2 \dot{\phi}^2 \left( \sin^2 \phi + \frac{1}{8} \right)$$

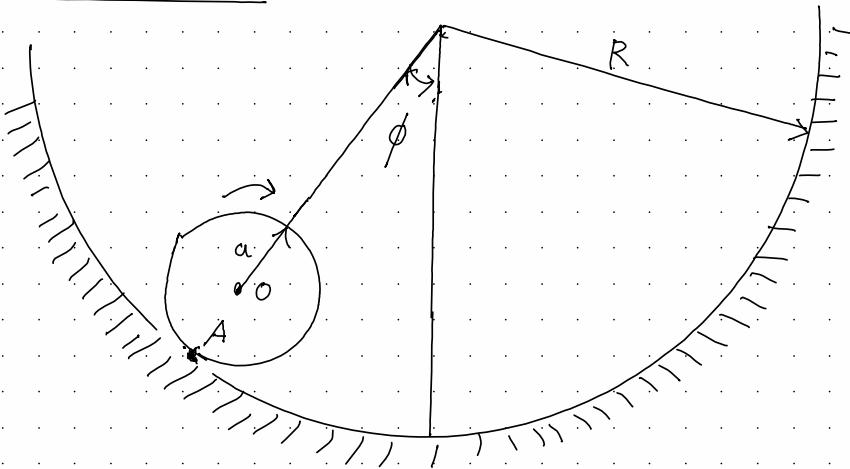
S.D

$$\begin{aligned}T_2 &= \frac{1}{\rho} M^2 l^2 \dot{\phi}^2 \left( \sin^2 \phi + \frac{1}{8} \right) + \frac{1}{24} M^2 l^2 \dot{\phi}^2 \\&= M^2 \dot{\phi}^2 \left( \sin^2 \phi + \frac{1}{8} + \frac{1}{24} \right) \\&= M^2 \dot{\phi}^2 \left( \sin^2 \phi + \frac{1}{6} \right)\end{aligned}$$

Thus,

$$\begin{aligned}T &= T_1 + T_2 \\&= \frac{1}{6} M^2 \dot{\phi}^2 + M^2 \dot{\phi}^2 \left( \sin^2 \phi + \frac{1}{6} \right) \\&= M^2 \dot{\phi}^2 \left( \frac{1}{3} + \sin^2 \phi \right) \\&= \frac{1}{3} M^2 \dot{\phi}^2 (1 + 3 \sin^2 \phi)\end{aligned}$$

Sec 32, Prob 6:



Homogeneous cylinder of radius  $a$ , mass  $m$ :

$$I_3 = \frac{1}{2}ma^2 \quad (\text{about com})$$

$$\vec{V} = -(R-a)\dot{\phi} \hat{i} \quad (\text{velocity of com})$$

Instantaneous axis of rotation at  $A$

$$\omega = \vec{V} + \vec{\Omega} + (-a\vec{n}), \quad \vec{\Omega} \text{ into page}$$

$$\text{so } V = \Omega a$$

$$\text{Thus, } \Omega a = (R-a) |\dot{\phi}|$$

$$\Omega = \left(\frac{R-a}{a}\right) |\dot{\phi}|$$

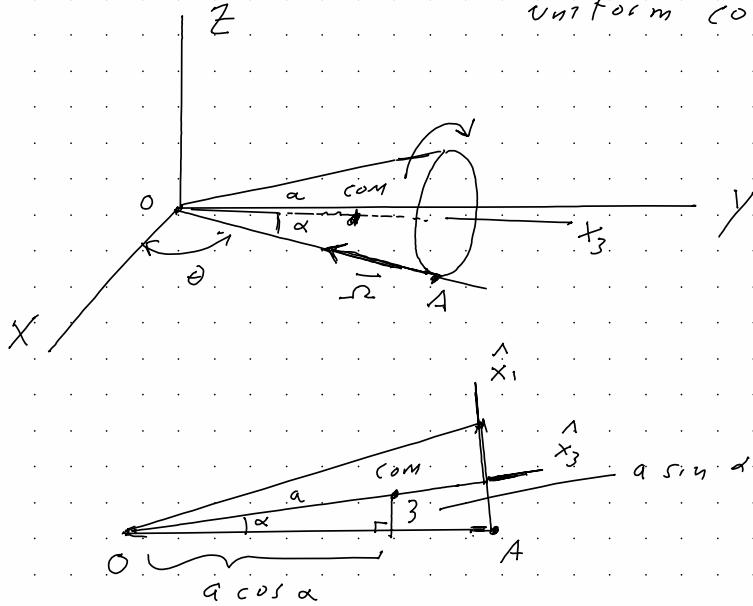
$$T = \frac{1}{2}mV^2 + \frac{1}{2}I_3 \Omega^2$$

$$= \frac{1}{2}m\left(\frac{R-a}{a}\right)^2 |\dot{\phi}|^2 + \frac{1}{2}m a^2 \left(\frac{R-a}{a}\right)^2 |\dot{\phi}|^2$$

$$= m(R-a)^2 |\dot{\phi}|^2 \left(\frac{1}{2} + \frac{1}{4}\right) = \boxed{\left[\frac{3}{4}m(R-a)^2 |\dot{\phi}|^2\right]}$$

Sec 32, Prob 7.

radius  $R$ , height  $h$   
uniform cone



$V$  = velocity of COM

$$= a \cos \alpha \dot{\theta}$$

$OA$ : instantaneous axis of rotation

$$\omega = \vec{V} - a \sin \alpha \vec{\Omega} x_3^1 \quad (1^1 = \hat{z})$$

$$\omega = V - a \sin \alpha \vec{\Omega}$$

$$\text{thus, } a \sin \alpha \vec{\Omega} = \vec{V} = a \cos \alpha \dot{\theta}$$

$$\boxed{\vec{\Omega} = \cot \alpha \dot{\theta}}$$

$\vec{\Omega}$ : directed from A to O

$$\Omega_3 = -\Omega \cos \alpha = -\frac{\cos^2 \alpha}{\sin \alpha} \dot{\theta}$$

$$\Omega_1 = \Omega \sin \alpha = \cos \alpha \dot{\theta}$$

$$\text{Thus, } T = \frac{1}{2} \mu V^2 + \frac{1}{2} (I_1 \omega_1^2 + I_2 \omega_2^2 + I_3 \omega_3^2) \quad (I_2 = I_1)$$

$$= \frac{1}{2} \mu a^2 \cos^2 \alpha \dot{\theta}^2 + \frac{1}{2} (I_1 \cos^2 \alpha \dot{\theta}^2 + I_3 \frac{\cos^4 \alpha}{\sin^2 \alpha} \dot{\theta}^2)$$

$$\text{Now: } I_1 = I_2 = \frac{3}{20} \mu / R^2 + \frac{1}{4} b^2$$

$$I_3 = \frac{3}{10} \mu R^2$$

$$\text{Also: } a = \frac{3}{4} b$$

$$\tan \alpha = \frac{R}{h} \rightarrow R = h \tan \alpha$$

Thus,

$$T = \frac{1}{2} \mu \left( \frac{9}{16} \right) h^2 \cos^2 \alpha \dot{\theta}^2 + \frac{1}{2} \left[ \frac{3}{20} \mu \left( h^2 \tan^2 \alpha + \frac{1}{4} h^2 \right) \cos^2 \alpha \dot{\theta}^2 + \frac{3}{10} \mu h^2 \tan^2 \alpha \frac{\cos^4 \alpha}{\sin^2 \alpha} \dot{\theta}^2 \right] (1 - \cos^2 \alpha)$$

$$= \mu h^2 \dot{\theta}^2 \left[ \frac{9}{32} \cos^2 \alpha + \frac{3}{40} \overbrace{\sin^2 \alpha}^{\cos^2 \alpha} + \frac{3}{160} \cos^2 \alpha + \frac{3}{20} \cos^2 \alpha \right]$$

$$= \mu h^2 \dot{\theta}^2 \left[ \frac{3}{40} + \cos^2 \alpha \left( \frac{9}{32} - \frac{3}{40} + \frac{3}{160} + \frac{3}{20} \right) \right]$$

$$\text{Now: } \frac{9}{32} - \frac{3}{40} + \frac{3}{160} + \frac{3}{20}$$

$$= \frac{1}{160} [45 - 12 + 3 + 24]$$

$$= \frac{60}{160}$$

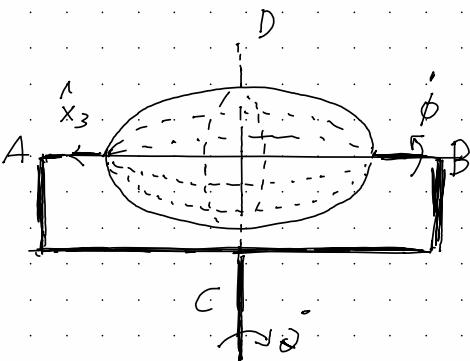
$$= \frac{15}{40}$$

Thus,

$$T = \mu b^2 \theta^2 \left[ \frac{3}{40} + \frac{15}{40} \cos^2 \alpha \right]$$

$$= \boxed{\frac{3}{40} \mu b^2 \theta^2 \left[ 1 + 5 \cos^2 \alpha \right]}$$

Sec 32, Prob 9.



homogeneous ellipsoid  
with principal  
moments of  
inertia  $I_1, I_2, I_3$

$$\vec{\Omega} = \dot{\phi} + \vec{\theta}$$

Now:  $\dot{\phi} = \dot{\phi} \hat{x}_3$

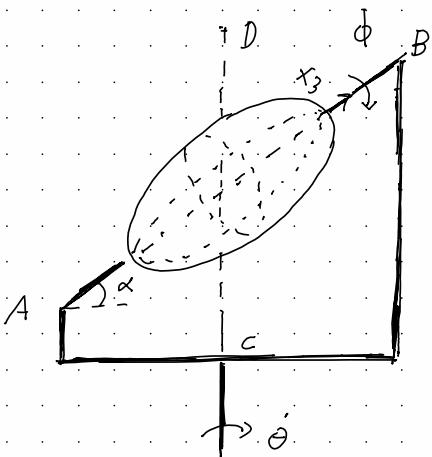
$$\vec{\theta} = \dot{\theta} [\cos \phi \hat{x}_1 + \sin \phi \hat{x}_2]$$

$$\text{so } \vec{\Omega} = \dot{\theta} \cos \phi \hat{x}_1 + \dot{\theta} \sin \phi \hat{x}_2 + \dot{\phi} \hat{x}_3$$

$$T = \frac{1}{2} (I_1 \omega_1^2 + I_2 \omega_2^2 + I_3 \omega_3^2)$$

$$= \frac{1}{2} [(I_1 \cos^2 \phi + I_2 \sin^2 \phi) \dot{\theta}^2 + I_3 \dot{\phi}^2]$$

Sec 32, Prob 10.



Using formula 11, p. 301  
with  $I_1 = I_2$   
(circular cross section)

$$\vec{\Omega} = \vec{\phi} + \vec{\theta}$$

$$\vec{\phi} = \phi \hat{x}_3$$

$$\vec{\theta} = \dot{\theta} \left[ \cos\left(\frac{\pi}{2}-\alpha\right) \hat{x}_3 + \sin\left(\frac{\pi}{2}-\alpha\right) (\cos\phi \hat{x}_1 + \sin\phi \hat{x}_2) \right]$$

$$\text{Now! } \cos\left(\frac{\pi}{2}-\alpha\right) = \cos\left(\frac{\pi}{2}\right) \cos\alpha + \sin\left(\frac{\pi}{2}\right) \sin\alpha \\ = \sin\alpha$$

$$\sin\left(\frac{\pi}{2}-\alpha\right) = \sin\left(\frac{\pi}{2}\right) \cos\alpha - \cos\left(\frac{\pi}{2}\right) \sin\alpha \\ = \cos\alpha$$

$$\text{So } \vec{\theta} = \dot{\theta} \left[ \sin\alpha \hat{x}_3 + \cos\alpha \cos\phi \hat{x}_1 + \cos\alpha \sin\phi \hat{x}_2 \right]$$

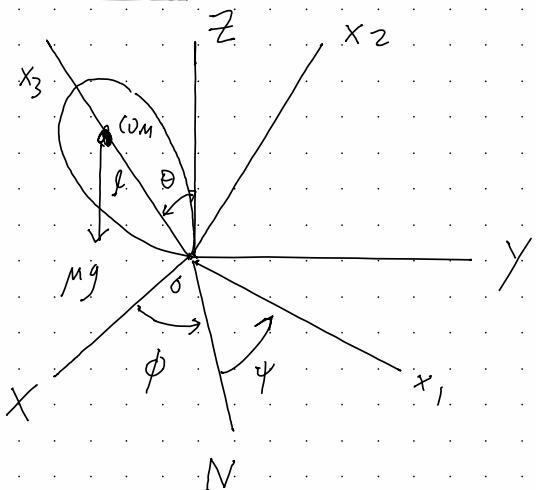
$$\rightarrow \vec{\Omega} = \dot{\theta} \cos\alpha (\cos\phi \hat{x}_1 + \sin\phi \hat{x}_2) + (\phi + \dot{\theta} \sin\alpha) \hat{x}_3$$

$$T = \frac{1}{2} (I_1 \Omega_1^2 + I_2 \Omega_2^2 + I_3 \Omega_3^2)$$

$$= \frac{1}{2} \left[ I_1 \dot{\theta}^2 \cos^2\alpha (\cos^2\phi + \sin^2\phi) + I_3 (\phi + \dot{\theta} \sin\alpha)^2 \right]$$

$$= \frac{1}{2} \left[ I_1 \cos^2\alpha \dot{\theta}^2 + I_3 (\phi + \dot{\theta} \sin\alpha)^2 \right]$$

Sec 35, prob 1:



Symmetrical top:

$I_1 = I_2$ ,  $I_3$  (wrt principal axes passing through COM)

$I'_1 = I_1 + ml^2$  (wrt axes passing through

$I'_2 = I'_1$   $O$ , which is displaced

$I'_3 = I_3$  from the COM by  $l$  in the  
-  $x_3$  direction)

$$L = T - U$$

$$U = mgz = mgl \cos \theta$$

$$T = \frac{1}{2} (I'_1 \Omega_1^2 + I'_2 \Omega_2^2 + I'_3 \Omega_3^2)$$

$$= \frac{1}{2} [I'_1 (\Omega_1^2 + \Omega_2^2) + I'_3 \Omega_3^2]$$

N.o.w: (From (35.1))

$$\Omega_1 = \dot{\phi} \sin \theta \sin \psi + \dot{\theta} \cos \psi$$

$$\Omega_2 = \dot{\phi} \sin \theta \cos \psi - \dot{\theta} \sin \psi$$

$$\Omega_3 = \dot{\phi} \cos \theta + \dot{\psi}$$

so  $\Omega_3^2 = (\dot{\phi} \cos \theta + \dot{\psi})^2$

$$\Omega_1^2 = \dot{\phi}^2 \sin^2 \theta \sin^2 \psi + \dot{\theta}^2 \cos^2 \psi + 2 \dot{\theta} \dot{\psi} \sin \theta \sin \psi \cos \psi$$

$$\Omega_2^2 = \dot{\phi}^2 \sin^2 \theta \cos^2 \psi + \dot{\theta}^2 \sin^2 \psi - 2 \dot{\theta} \dot{\psi} \sin \theta \cos \psi \sin \psi$$

$$\rightarrow \Omega_1^2 + \Omega_2^2 = \dot{\phi}^2 \sin^2 \theta + \dot{\theta}^2$$

Thus,

$$L = \frac{1}{2} [ I_1 (\dot{\phi}^2 \sin^2 \theta + \dot{\theta}^2) + I_3 (\dot{\phi} \cos \theta + \dot{\psi})^2 ] - mg l \cos \theta$$

1) No explicit  $t$ -dependence

$$E = T + V = \text{const}$$

2) No explicit  $\phi$ -dependence:

$$p_\phi \equiv \frac{\partial L}{\partial \dot{\phi}} = I_1 \sin^2 \theta \dot{\phi} + I_3 (\dot{\phi} \cos \theta + \dot{\psi}) \cos \theta = \text{const}$$

3) No explicit  $\psi$ -dependence: (see next page)  $= M_2 = \text{const}$

$$p_\psi \equiv \frac{\partial L}{\partial \dot{\psi}} = I_3 (\dot{\phi} \cos \theta + \dot{\psi}) = \text{const} = M_3$$

To show that  $M_Z = M_Z$

$$\begin{aligned}M_Z &= \vec{M} \cdot \hat{\vec{z}} \\&= (M_1 \hat{x}_1 + M_2 \hat{x}_2 + M_3 \hat{x}_3) \cdot \hat{\vec{z}} \\&= M_1 \hat{x}_1 \cdot \hat{\vec{z}} + M_2 \hat{x}_2 \cdot \hat{\vec{z}} + M_3 \hat{x}_3 \cdot \hat{\vec{z}}\end{aligned}$$

Now:  $\hat{x}_3 \cdot \hat{\vec{z}} = \cos \theta$

$$\hat{x}_1 \cdot \hat{\vec{z}} = \sin \theta \sin \psi$$

$$\hat{x}_2 \cdot \hat{\vec{z}} = \sin \theta \cos \psi$$

Thus,

$$\begin{aligned}M_Z &= M_1 \sin \theta \sin \psi + M_2 \sin \theta \cos \psi + M_3 \cos \theta \\&= I_1' \Omega_1 \sin \theta \sin \psi + I_1' \Omega_2 \sin \theta \cos \psi \\&\quad + I_3 \Omega_3 \cos \theta \\&= I_1' (\sin^2 \theta \sin^2 \phi + \cancel{\sin \theta \sin \psi \cos \psi \dot{\theta}}) \\&\quad + I_1' (\sin^2 \theta \cos^2 \phi - \cancel{\sin \theta \cos \psi \sin \psi \dot{\theta}}) \\&\quad + I_3 (\phi \cos \theta + \psi) \cos \theta \\&= I_1' \sin^2 \theta \dot{\phi} + I_3 \cos \theta (\dot{\phi} \cos \theta + \dot{\psi})\end{aligned}$$

We can solve  $M_2, M_3$  for  $\phi, \psi$ :

$$M_2 = I_1' \sin^2 \theta \dot{\phi} + I_3 (\phi \cos \theta + \psi) \cos \theta$$

$$M_3 = I_3 (\dot{\phi} \cos \theta + \dot{\psi})$$

$$\rightarrow M_2 = I_1' \sin^2 \theta \dot{\phi} + M_3 \cos \theta$$

$$\text{so } I_1' \sin^2 \theta \dot{\phi} = M_2 - M_3 \cos \theta$$

$$\boxed{\dot{\phi} = \frac{M_2 - M_3 \cos \theta}{I_1' \sin^2 \theta}}$$

Ans:

$$\frac{M_3}{I_3} = \phi \cos \theta + \psi$$

$$\rightarrow \boxed{\psi = \frac{M_3}{I_3} - \phi \cos \theta}$$

$$= \frac{M_3}{I_3} - \left( \frac{M_2 - M_3 \cos \theta}{I_1' \sin^2 \theta} \right) \cos \theta$$

Ans:

$$\underline{F} = T + \underline{U}$$

$$= \frac{1}{2} [ I_1' (\sin^2 \theta \dot{\phi}^2 + \dot{\theta}^2) + I_3 (\phi \cos \theta + \psi)^2 ] \\ + \mu g l \cos \theta$$

can be rewr. Then as

$$E = \frac{1}{2} I_1' \dot{\theta}^2 + \frac{1}{2} I_1' \sin^2 \theta \dot{\phi}^2 + \frac{1}{2} T_3 \left( \frac{M_3}{I_3} \right)^2 + \mu g l \cos \phi$$

$$= \frac{1}{2} I_1' \dot{\theta}^2 + \frac{1}{2} I_1' \sin^2 \theta \frac{(M_2 - M_3 \cos \theta)^2}{I_1' \sin^4 \theta} + \frac{1}{2} \frac{M_3^2}{I_3} + \mu g l \cos \phi$$

$$= \frac{1}{2} I_1' \dot{\theta}^2 + \frac{1}{2} \frac{M_3^2}{I_3} + \frac{1}{2} \frac{(M_2 - M_3 \cos \theta)^2}{I_1' \sin^2 \theta} + \mu g l \cos \theta$$

Now  $\frac{1}{2} \frac{M_3^2}{I_3} = \text{const}$

Also  $\mu g l \cos \theta = -\mu g l (1 - \cos \theta) + \mu g l$

So

$$E - \frac{1}{2} \frac{M_3^2}{I_3} - \mu g l = \frac{1}{2} I_1' \dot{\theta}^2 + \frac{1}{2} \frac{(M_2 - M_3 \cos \theta)^2}{I_1' \sin^2 \theta} - \mu g l (1 - \cos \theta)$$

$$\rightarrow E' = \frac{1}{2} I_1' \dot{\theta}^2 + U_{\text{eff}}(\theta)$$

where 
$$U_{\text{eff}}(\theta) = \frac{1}{2} \frac{(M_2 - M_3 \cos \theta)^2}{I_1' \sin^2 \theta} - \mu g l (1 - \cos \theta)$$

EOM:

$$E' = \frac{1}{2} I_1' \dot{\theta}^2 + U_{\text{eff}}(\theta)$$

$$\dot{\theta}^2 = \frac{2}{I_1'} (E' - U_{\text{eff}}(\theta))$$

$$\frac{d\theta}{dt} = \sqrt{\frac{2}{I_1'} (E' - U_{\text{eff}}(\theta))}$$

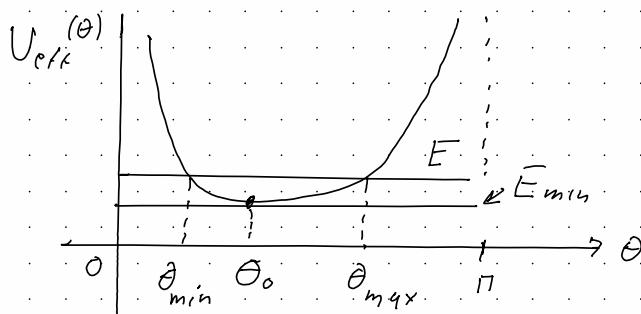
$$\rightarrow \int dt = \int \frac{d\theta}{\sqrt{\frac{2}{I_1'} (E' - U_{\text{eff}}(\theta))}}$$

$$t = \left[ \int \frac{d\theta}{\sqrt{\frac{2}{I_1'} (E' - U_{\text{eff}}(\theta))}} + \text{const} \right]$$

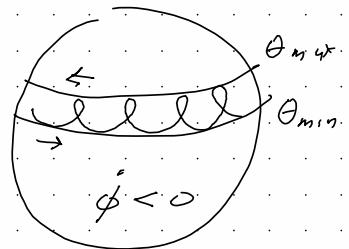
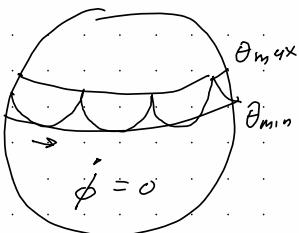
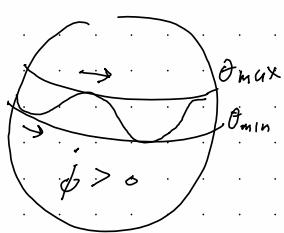
Effective potential:

$$U_{\text{eff}}(\theta) = \frac{1}{2} \frac{(M_z - M_3 \cos \theta)^2}{I_1' \sin^2 \theta} - \mu g l (1 - \cos \theta)$$

For  $M_z \neq M_3$ ,  $U_{\text{eff}}(\theta) \rightarrow \infty$  as  $\theta \rightarrow 0, \pi$



For  $E > E_{\min}$ ,  $\theta$  varies between  $\theta_{\max}$  and  $\theta_{\min}$ . The motion of the  $x_3$ -axis of the top can have the following three forms depending on the sign of  $\dot{\phi}$  when  $\theta = \theta_{\max}$ .



This motion is called nutation.

Sec 3.5, Prob 2

For rotation of a top around a vertical axis, to be stable, we need  $\frac{d^2 U_{\text{eff}}}{d\theta^2} \Big|_{\theta=0} > 0$

Now:

$$U_{\text{eff}}(\theta) = \frac{(M_z - M_3 \omega \theta)^2}{2 I_1 \sin^2 \theta} - \mu g l (1 - \cos \theta)$$

At  $\theta_0$ :

$$M_z = I_1 \sin^2 \theta \dot{\phi} + I_3 (\dot{\phi} \cos \theta + \dot{\psi}) \cos \theta$$

$$M_3 = I_3 (\dot{\phi} \cos \theta + \dot{\psi})$$

In the limit  $\theta \rightarrow 0$

$$M_z \approx I_3 (\dot{\phi} + \dot{\psi}) \quad \text{so they are equal}$$

$$M_3 \approx I_3 (\dot{\phi} + \dot{\psi}) \quad \text{in this limit}$$

Thus,

$$U_{\text{eff}}(\theta) \approx \frac{M_3^2 (1 - \cos \theta)^2}{2 I_1 \sin^2 \theta} - \mu g l (1 - \cos \theta)$$

$$\approx \frac{M_3^2 (\frac{\theta^2}{2})^2}{2 I_1 \sin^2 \theta} - \mu g l \frac{\theta^2}{2}$$

$$= \left( \frac{1}{8} \frac{M_3^2}{I_1} - \frac{1}{2} \mu g l \right) \theta^2$$

Thus

$$U_{\text{eff}}(\theta) \approx \left( \frac{1}{8} \frac{M_3}{I_1} - \frac{1}{2} \mu g l \right) \theta^2$$

$$\rightarrow U_{\text{eff}}(0) = 0$$

$$\frac{dU_{\text{eff}}}{d\theta} \Big|_{\theta=0} = 2 \left( \frac{1}{8} \frac{M_3}{I_1} - \frac{1}{2} \mu g l \right) \theta \Big|_{\theta=0} = 0$$

$$\frac{d^2U_{\text{eff}}}{d\theta^2} \Big|_{\theta=0} = 2 \left( \frac{1}{8} \frac{M_3}{I_1} - \frac{1}{2} \mu g l \right)$$

Need  $\frac{d^2U_{\text{eff}}}{d\theta^2} \Big|_{\theta=0} > 0$  for stable rotation!

$$\frac{1}{8} \frac{M_3^2}{I_1} - \frac{1}{2} \mu g l > 0$$

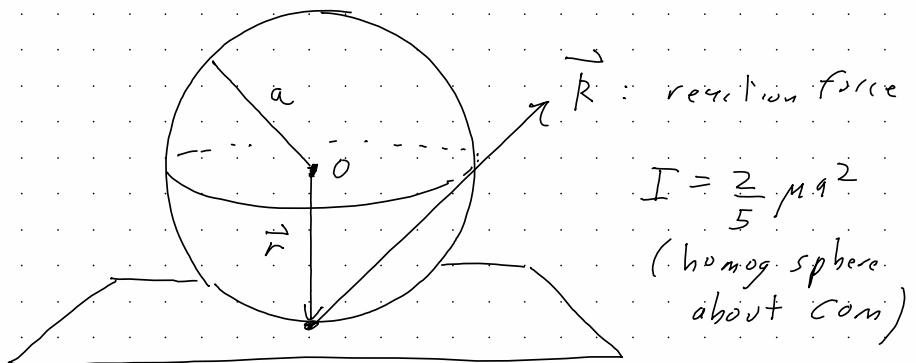
$$\boxed{M_3^2 > 4 \mu g l I_1}$$

Equivalently, since  $M_3 = I_3 \omega_3$

$$\boxed{\omega_3^2 > \frac{4 \mu g l I_1}{I_3^2}}$$

Sec. 38, Prob 1:

Homogeneous sphere (radius  $a$ ) rolling without slipping on a horizontal surface, subject to applied force  $\vec{F}$  and torque  $\vec{\tau}$



$$I = \frac{2}{5} \mu a^2$$

(homog. sphere  
about com)

$$\frac{d\vec{P}}{dt} = \vec{F} + \vec{R} \rightarrow m \frac{d\vec{V}}{dt} = \vec{F} + \vec{R}$$

$$\frac{d\vec{m}}{dt} = \vec{\tau} + \vec{F} \times \vec{R} \rightarrow I \frac{d\vec{\Omega}}{dt} = \vec{\tau} - a \hat{z} \times \vec{R}$$

Rolling without slipping:

$$\begin{aligned} \vec{O} &= \vec{V} + \vec{\Omega} \times \vec{r} \\ &= \vec{V} - a \vec{\Omega} \times \hat{z} \end{aligned}$$

$$\text{So } \vec{V} = a \vec{\Omega} \times \hat{z}$$

Using  $(\vec{A} \times \vec{B})_i = A_2 B_3 - A_3 B_2$ , etc

|                     |
|---------------------|
| $V_x = a \Omega_y$  |
| $V_y = -a \Omega_x$ |
| $V_z = 0$           |

no motion off surface

Combined:

$$\mu \frac{d\vec{V}}{dt} = \vec{F} + \vec{R} \quad (1)$$

$$I \frac{d\vec{\omega}}{dt} = \vec{R} - a \hat{z} \times \vec{R} \quad (2)$$

$$V_x = a \Omega_y, V_y = -a \Omega_x, V_z = 0 \quad (\text{constraint})$$

Take time derivative of constraint equation:

$$\frac{dV_x}{dt} = a \frac{d\Omega_y}{dt}, \quad \frac{dV_y}{dt} = -a \frac{d\Omega_x}{dt}$$

Substitute from (1), (2) into these two equations

$$\frac{1}{\mu} (F_x + R_x) = \frac{a}{I} (K_y - a R_x)$$

$$\frac{1}{\mu} (F_y + R_y) = -\frac{a}{I} (K_x + a R_y)$$

Thus,

$$F_x + R_x = \frac{ma}{I} K_y - \frac{ma^2}{I} R_x$$

$$R_x \left( \frac{I + ma^2}{I} \right) = \frac{ma}{I} K_y - F_x$$

$$R_x \frac{\frac{7}{5} ma^2}{\frac{2}{5} ma^2} = \frac{ma}{\frac{2}{5} ma^2} K_y - F_x$$

$$\rightarrow \boxed{R_x = \frac{5}{7} \frac{K_y}{a} - \frac{2}{7} F_x}$$

Similarly,

$$F_y + R_y = -\frac{\mu a}{I} K_x - \frac{m a^2}{I} R_y$$

$$R_y \left( \frac{I + \mu a^2}{I} \right) = -\frac{\mu a}{I} K_x - F_y$$

$$\frac{R_y \frac{7 \mu a^2}{5}}{\frac{2 \mu a^2}{5}} = -\cancel{\mu a} K_x - F_y$$

$$\rightarrow \boxed{R_y = -\frac{5}{7} \frac{K_x}{a} - \frac{2}{7} F_y}$$

Also,

$$\mu \frac{dV_z}{dt} = F_z + R_z$$

$$\rightarrow \boxed{R_z = -F_z}$$

Using these expression for  $R_x, R_y$  we can write down Eoms for  $V_x, V_y$

$$\boxed{\begin{aligned} \mu \frac{dV_x}{dt} &= F_x + R_x \\ &= F_x + \frac{5}{7} \frac{K_y}{a} - \frac{2}{7} F_x \\ &= \frac{5}{7} \left( F_x + \frac{K_y}{a} \right) \end{aligned}}$$

Similarly

$$\boxed{\frac{M \frac{dV_Y}{dt}}{dt} = F_Y + R_Y}$$
$$= F_Y - \frac{5}{7} \frac{K_X}{a} - \frac{2}{7} F_X$$
$$= \frac{5}{7} \left( F_Y - \frac{K_X}{a} \right)$$

Summary:

$$R_X = \frac{5}{7} \frac{K_X}{a} - \frac{2}{7} F_X$$

$$R_Y = -\frac{5}{7} \frac{K_X}{a} - \frac{2}{7} F_Y$$

$$R_Z = -F_Z$$

$$M \frac{dV_X}{dt} = \frac{5}{7} \left( F_X + \frac{K_Y}{a} \right)$$

$$M \frac{dV_Y}{dt} = \frac{5}{7} \left( F_Y - \frac{K_X}{a} \right)$$

$$V_Z = 0$$

$$\Omega_X = -\frac{V_Y}{a}$$

$$\Omega_Y = \frac{V_X}{a}$$

$$I \frac{d\Omega_Z}{dt} = K_Z$$

Example:

Suppose:  $\overrightarrow{F} = -\mu g \hat{z} + F_0 \hat{x}$   
 $\overrightarrow{R} = 0$

Then:  $F_x = F_0$ ,  $F_y = 0$ ,  $F_z = -\mu g$

Solution from previous page gives:

$$R_x = -\frac{2}{7} F_0$$

$$R_y = 0$$

$$R_z = \mu g \quad (\text{normal force upward})$$

$$m \frac{dV_x}{dt} = \frac{5}{7} F_0 \rightarrow V_x = \frac{5}{7} \frac{F_0}{m} t + V_{x0}$$

$$m \frac{dV_y}{dt} = 0 \rightarrow V_y = \text{const} = V_{y0}$$

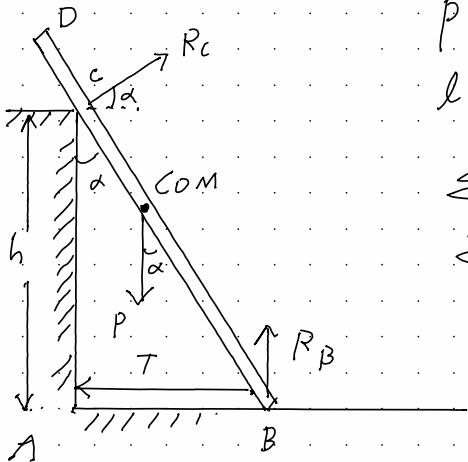
$$V_z = 0$$

$$\Omega_x = -\frac{V_{y0}}{a}$$

$$\Omega_y = \frac{V_x}{a} = \frac{5}{7} \frac{F_0}{ma} t + \frac{V_{x0}}{a}$$

$$I \frac{d\Omega_z}{dt} = 0 \rightarrow \Omega_z = \text{const} = \Omega_{z0}$$

Sec 38, Prob 2



$$P = \text{weight} = \mu g$$

$l$ : length of uniform rod

$$\sum \vec{F} = 0$$

$$\sum \vec{r} \times \vec{F} = 0$$

including reaction Force  
 $T, R_C, R_B$

horizontal direction

$$-T + R_C \cos \alpha = 0 \quad (1)$$

vertical direction

$$R_C \sin \alpha - P + R_B = 0 \quad (2)$$

torques around D:

$$\frac{l}{2} \sin \alpha P - \frac{h}{\cos \alpha} R_C = 0 \quad (3)$$

Thus,

$$\frac{1}{\cos \alpha} R_C = \frac{l}{2} \sin \alpha P$$

$$R_C = \frac{lP}{2h} \sin \alpha \cos \alpha$$

$$T = R_C \cos \alpha$$

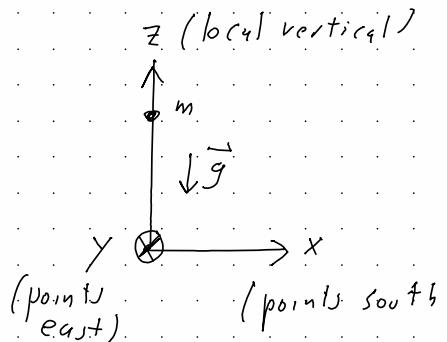
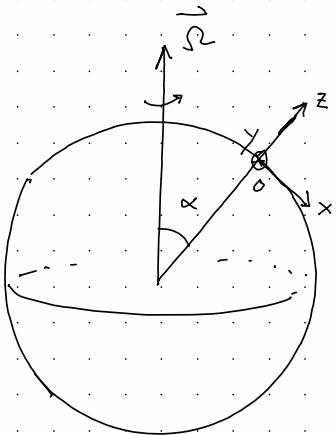
$$R_B = P - R_C \sin \alpha$$



$$\cos \alpha = \frac{d}{l}$$

$$\Rightarrow d = \frac{l}{\cos \alpha}$$

Sec 39, prob 1:



( $\alpha$ : location on Earth relative to North pole)

Newton's 2nd law in rotating frame

$$m\vec{a} = \vec{mg} - m\vec{W} - 2m\vec{\Omega} \times \vec{v} - m\vec{\Omega} \times (\vec{\Omega} \times \vec{r})$$

where  $\vec{W} = \vec{\Omega} \times (\vec{\Omega} \times \vec{R})$   
= acceleration of origin of  
rotating frame

Thus,

$$m\vec{a} = \vec{mg} - m\vec{\Omega} \times (\vec{\Omega} \times (\vec{r} + \vec{R})) - 2m\vec{\Omega} \times \vec{v}$$

$\underbrace{2^{\text{nd}} \text{ order in } \vec{\Omega}}$   
[ignore]

$$\approx \vec{mg} - 2m\vec{\Omega} \times \vec{v}$$

Now:  $\vec{g} = -g\vec{z}$

$$\vec{\Omega} = \Omega \cos \alpha \vec{z} + \Omega \sin \alpha \vec{x}$$

$$(\vec{\omega} \times \vec{v})_x = \cancel{\omega_y v_z} - \omega_z \dot{y} \\ = -\omega_z \dot{y}$$

$$(\vec{\omega} \times \vec{v})_y = \omega_z v_x - \cancel{\omega_x v_z} \\ = \omega_z \dot{x} - \omega_x \dot{z}$$

$$(\vec{\omega} \times \vec{v})_z = \omega_x v_y - \cancel{\omega_y v_x} \\ = \omega_x \dot{y}$$

Thus,

$$\ddot{x} = +2\omega_z \dot{y}$$

$$\ddot{y} = -2(\omega_z \dot{x} - \omega_x \dot{z})$$

$$\ddot{z} = -g + \omega_x \dot{y}$$

Want to solve these equations to 1<sup>st</sup> order in  $\omega$   
The 0<sup>th</sup> order solution is

$$\left. \begin{aligned} x_0(t) &= 0 \\ y_0(t) &= 0 \\ z_0(t) &= h - \frac{1}{2}gt^2 \end{aligned} \right\} \begin{array}{l} \text{drop from} \\ \text{vertical} \\ \text{height } h \end{array}$$

Write  $x(t) = x_0(t) + x_1(t)$ , etc.

Then

$$\ddot{x}_1 = 2\omega_z \dot{y}_1 \approx 0$$

$$\ddot{y}_1 = -2(\omega_z \dot{x}_1 - \omega_x(-gt + z_1)) \approx -2\omega_x g t$$

$$-\cancel{g} + z_1 = -g + \omega_x \dot{y}_1 \approx 0$$

Thus, only need to solve

$$Y_1 = -2\Omega_x g t$$

$$\rightarrow X_1 = -\Omega_x g t^2$$

$$Y_1 = -\frac{1}{3} \Omega_x g t^3$$

Now:  $\Omega_x = -\Omega \sin \alpha$

$$T = \sqrt{\frac{2h}{g}} \quad (0^{th} \text{ order solution to}$$

$$0 = h - \frac{1}{2} g T^2$$

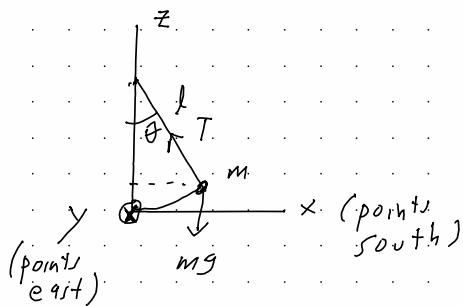
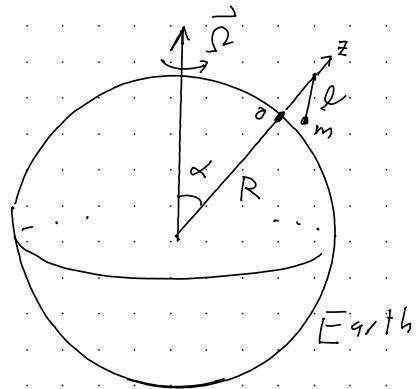
so object hits the ground at

$$Y = Y_1 = +\frac{1}{3} \Omega \sin \alpha \left( \frac{2h}{g} \right)^{3/2}$$

indicates that the object  
hits the ground to the East  
of the dropping location.

Sec 39, Prob 3.

Foucault's pendulum, small oscillations



Newton's 2nd law in rotating frame:

$$m\vec{a} = \vec{T} + \vec{mg} - m\vec{W} - 2m\vec{\Omega} \times \vec{v} - m\vec{\omega} \times (\vec{\omega} \times \vec{r})$$

$$\begin{aligned} \text{Now } \vec{W} &= \text{acceleration of origin O} \\ &= \vec{\omega} \times (\vec{\omega} \times \vec{R}) \end{aligned}$$

Thus,

$$m\vec{a} = \vec{T} + \vec{mg} - m\vec{\omega} \times (\vec{\omega} \times (\vec{r} + \vec{R})) - 2m\vec{\omega} \times \vec{v}$$

$\underbrace{\quad}_{\text{2nd order in } \vec{\omega}}$

[ignore]

$$\approx \vec{T} + \vec{mg} - 2m\vec{\omega} \times \vec{v}$$

$$\begin{aligned} \text{Now: } \vec{T} &= T \cos \theta \hat{z} - T \sin \theta \cos \phi \hat{x} - T \sin \theta \sin \phi \hat{y} \\ &\approx T \hat{z} - T \left( \frac{x}{l} \right) \hat{x} - T \left( \frac{y}{l} \right) \hat{y} \end{aligned}$$

assuming  $\theta \ll 1$  (small oscillations)

$$\vec{g} = -\vec{g} \hat{z}$$

$$\begin{aligned} (\vec{\omega} \times \vec{v})_x &= \Omega_y v_z - \Omega_z v_y \\ &= \Omega_y \hat{z} - \Omega_z \hat{y} \\ &\approx -\Omega_z \hat{y} \end{aligned}$$

$$\begin{aligned} (\vec{\omega} \times \vec{v})_y &= \Omega_z v_x - \Omega_x v_z \\ &= \Omega_z \hat{x} - \Omega_x \hat{z} \\ &\approx \Omega_z \hat{x} \end{aligned}$$

$$\begin{aligned} (\vec{\omega} \times \vec{v})_z &= \Omega_x v_y - \Omega_y v_x \\ &= \Omega_x \hat{y} \end{aligned}$$

$$T^{(h_0, r)} \quad \vec{ma} = \vec{T} + m\vec{g} - 2m\vec{\omega} \times \vec{v}$$

becomes

$$m\ddot{x} = -T\left(\frac{x}{l}\right) + 2m\Omega_z \dot{y}$$

$$m\ddot{y} = -T\left(\frac{y}{l}\right) - 2m\Omega_z \dot{x}$$

$$m\ddot{z} = T - mg - 2m\Omega_x \dot{y}$$

$$\text{Now: } \Omega_x \dot{y} \sim \sqrt{\frac{D}{P}}$$

where  $D = \text{Max displacement in } xy \text{-plane}$   
 $P = \text{period} = 2\pi \sqrt{\frac{l}{g}} \approx \frac{2\pi}{\omega}$

$$\text{Now } \frac{\Omega D}{P} = \frac{\Omega D}{2\pi} w$$

$$<< \frac{l w^2}{2\pi}$$

$$= \frac{k}{2\pi} \frac{g}{k}$$

$$= \frac{g}{2\pi}$$



Since  $\Omega << \omega$

$D << l$  (small oscillations)

$$\text{Thus, } m\Omega_x y \ll mg$$

so we can ignore these terms relative to  $mg$

$$\rightarrow \theta \approx T - mg \rightarrow \boxed{T \approx mg}$$

$$m\ddot{x} \approx -mg \frac{x}{l} + 2m\Omega_z \dot{y}$$

$$\boxed{\ddot{x} \approx -\omega^2 x + 2\Omega_z \dot{y}}$$

$$m\ddot{y} \approx -mg \frac{y}{l} - 2m\Omega_z \dot{x}$$

$$\boxed{\ddot{y} \approx -\omega^2 y - 2\Omega_z \dot{x}}$$

just need  
to solve  
these two  
equation

Standard "trick":

Define  $S = x + iy$  (complex valued)

$$\text{then } \tilde{S} = \dot{x} + i\dot{y}$$

$$\tilde{S} = \ddot{x} + i\ddot{y}$$

$$\begin{aligned}
 \text{so } \ddot{\zeta} &= -\omega^2 \zeta + 2i\Omega_z (\dot{y} - i\dot{x}) \\
 &= -\omega^2 \zeta - 2i\Omega_z (\dot{x} + i\dot{y}) \\
 &= -\omega^2 \zeta - 2i\Omega_z \dot{\zeta}
 \end{aligned}$$

thus,

$$\ddot{\zeta} + 2i\Omega_z \dot{\zeta} + \omega^2 \zeta = 0$$

Trial solution:  $e^{i\lambda t}$

$$\zeta(t) = e^{i\lambda t}$$

$$\begin{aligned}
 \rightarrow -\lambda^2 - 2i\Omega_z \lambda + \omega^2 &= 0 \\
 \lambda^2 + 2i\Omega_z \lambda - \omega^2 &= 0
 \end{aligned}$$

Solve quadratic:

$$\lambda_{\pm} = \frac{-2\Omega_z \pm \sqrt{4\Omega_z^2 + 4\omega^2}}{2}$$

$$\approx -\Omega_z \pm \omega \quad (\text{since } \Omega \ll \omega)$$

General solution:

$$\begin{aligned}
 \zeta(t) &= A e^{-i(\Omega_z - \omega)t} + B e^{-i(\Omega_z + \omega)t} \\
 &= e^{-i\Omega_z t} (A e^{i\omega t} + B e^{-i\omega t}) \\
 &= e^{-i\Omega_z t} \zeta_0(t)
 \end{aligned}$$

where  $\zeta_0(t)$  = general solution of small oscillation problem in an inertial frame.

The factor  $e^{-i\omega t}$  causes the plane of oscillation of the pendulum to precess with angular frequency

$$\Omega_z = \sqrt{2} \cos \alpha$$

angle of location  
on Earth

$$\begin{aligned} (\alpha = 0 &\leftrightarrow \text{NPole}) \\ (\alpha = \pi/2 &\leftrightarrow \text{Equator}) \end{aligned}$$

Precession period:

$$\begin{aligned} P_{\text{precession}} &= \frac{2\pi}{\Omega_z} \\ &= \frac{2\pi}{\sqrt{2} \cos \alpha} \end{aligned}$$

$$\begin{aligned} \Omega &= \text{revolution / 24 hrs} \\ &= \frac{2\pi \text{ rad}}{24 \text{ hrs}} \end{aligned}$$

$$P_{\text{precession}} = \frac{24 \text{ hrs}}{\cos \alpha}$$

$$= \begin{cases} 24 \text{ hrs at N Pole} \\ \infty \text{ at equator (so no precession)} \end{cases}$$