

PHYS 5306: Classical Dynamics

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(Fall 2020)

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Load relevant packages

```
In [1]: %load_ext autoreload
%autoreload 2
```

```
In [2]: import numpy as np
import scipy.special as special
import matplotlib.pyplot as plt
import matplotlib as mpl
import matplotlib.lines as lines
from mpl_toolkits.mplot3d import Axes3D
%matplotlib inline
%config InlineBackend.figure_format = 'retina'

mpl.rcParams['figure.dpi'] = 100
#mpl.rcParams['figure.figsize'] = [5,3]
mpl.rcParams['text.usetex'] = True
```

0. Useful mathematical identities, special functions, etc.

- Review of vector calculus, calculus of variations, linear algebra, ...
- Trig identities
- Double-angle formulae
- Hyperbolic function identities
- Some standard integrals
- Beta function, Gamma function
- Elliptic functions and elliptic integrals

1. Lagrangian mechanics (1-5)

- Write down the Lagrangian for a simple system in terms of generalized coordinates.
- Distinguish generalized coordinates from Cartesian coordinates.
- Write down Lagrange's equations.
- Define the action in terms of the Lagrangian, and derive Lagrange's equations starting from the action.
- Show that Lagrange's equations are unchanged if one adds a total time derivative $d\phi(q, t)/dt$ to L .
- Include holonomic and non-holonomic constraint forces in the Lagrangian formalism by introducing Lagrange multipliers.
- Define and give examples of a *closed system*, *constant external field*, and *uniform field*.

2. Conservation laws (6-10)

- Show how conservation of energy, momentum, and angular momentum are connected to time translation, space translation, and rotational symmetry.
- Derive the transformation equations for energy, momentum, and angular momentum from one inertial frame K to another K' .
- Write down the general expression for the energy function E .
- Explain what it means for a function to be homogeneous of degree k .
- Write down the expression for the generalized momentum p_i .
- Write down the expression for the center of mass (COM) of a system of particles.
- Write down the virial theorem for a system whose motion takes place in a finite region of space and whose potential energy is a homogeneous function of degree k .

3. Hamiltonian mechanics (40)

- Write down the Hamiltonian $H(p, q, t)$ for a simple system starting from a Lagrangian $L(q, \dot{q}, t)$.
- Write down Hamilton's equations for p_i and q_i .
- Explain the fundamental difference between Hamilton's equations and Lagrange's equations.
- Show the equivalence of Hamilton's equations and Lagrange's equation for simple systems.

4. Central force motion (11, 13-15)

- Write down an integral expression for t in terms of x for 1-d motion in a constant external field $U(x)$.
- Determine the allowed values of the energy and turning points for 1-d motion in a constant external field.
- Transform the problem of two interacting particles into an effective one-body problem by working in the COM frame.
- Show that both energy and angular momentum are conserved for a central potential.
- Write down an expression for the effective potential $U_{\text{eff}}(r)$ in terms of $U(r)$ and ℓ .
- Plot the effective potential for some simple central force potentials.
- From the graph of the effective potential, determine the different types of allowed motion.
- Write down integral expressions for t and ϕ in terms of r for a general central potential.
- Evaluate these two integrals for Kepler's problem for bound orbits, using appropriate trig substitutions.
- Derive the relationship between E , ℓ , a , b , e , and p for an ellipse.
- State the only two central potentials that have closed bound orbits.
- State and derive Kepler's three laws of planetary motion.
- Explain the difference in E and e for elliptical, parabolic, and hyperbolic motion.

5. Collisions and scattering (16-20)

- Draw diagrams relating velocities in the lab and COM frames for the disintegration of a single particle.
- Draw diagrams relating the momenta in the lab and COM frames for an elastic collision of two particles (m_2 initially at rest in the lab frame).
- Explain what information can and cannot be obtained for an elastic collision of two particles, using just conservation of momentum and kinetic energy.
- Derive formulas relating the scattering angles χ , θ_1 , θ_2 in the COM and lab frames.
- Draw diagrams showing how the scattering angle χ is related to the angle of closest approach ϕ_0 .
- Relate the impact parameter ρ and initial velocity v_∞ to the energy E and angular momentum ℓ .
- Derive an integral expression for ϕ_0 and solve it for simple potentials---e.g., $U(r) = \alpha/r$ for Rutherford scattering.
- Write down expressions for $d\sigma$ in terms of $d\rho$, $d\chi$, $d\theta_1$, $d\theta_2$, or $d\Omega$, $d\Omega_1$, $d\Omega_2$.
- Explain how one can obtain an expression for small-angle scattering starting from the integral equation for ϕ_0 .

6. Small oscillations (21-23)

- Explain what stable equilibrium means in terms of the potential energy $U(q)$.
- Calculate the frequency for small oscillations about a position of stable equilibrium.
- Solve the equations of motion for both free and forced oscillation in one dimension, noting the difference between the general solution of the homogeneous equation and a particular integral of the inhomogeneous equation.
- Calculate the normal mode frequencies and normal mode solutions for small oscillations of systems with more than one DOF.

7. Rigid body motion (31-36, 38)

- Draw a diagram showing the body frame and fixed inertial reference frame.
- Show that the angular velocity vector is unchanged under a shift of the origin of the body frame.
- Write down an expression for the components I_{ik} of the inertia tensor as a sum over discrete mass points or as an integral over the volume of the body.
- Indicate how the components of the inertia tensor change if you shift the origin of the body frame.
- Obtain or identify the principal axes of inertia for various rigid bodies.
- Calculate the principal moments of inertia for various rigid bodies.
- Calculate the kinetic energy of a rigid body in terms of its COM motion and rotational kinetic energy.
- Write down an expression for the angular momentum vector \mathbf{M} in terms I_{ik} and Ω_i .
- Write down the equations of motion for a rigid body with respect to an inertial frame.
- Derive Euler's equations for rigid body motion (equations of motion in the body frame).
- Draw a diagram showing the definition of the Euler angles (ϕ, θ, ψ) .
- Calculate the components of $\boldsymbol{\Omega}$ wrt the body frame in terms of the Euler angles and their time derivatives.
- Solve for the reaction forces for rigid bodies in static equilibrium.

8. Non-inertial reference frames (39)

- Draw a diagram relating an inertial and non-inertial reference frame.
- Write down the relationship between velocity vectors in inertial and non-inertial reference frames.
- Distinguish non-inertial reference frames associated with translational and rotational motion.
- Derive the Coriolis, centrifugal, translational acceleration, and rotational acceleration fictitious force terms.
- Explain the physical significance of Foucault's pendulum.

0. Useful mathematical identities, special functions, etc.

1) Review of vector calculus, etc.:

[\(https://link.springer.com/content/pdf/bbm%3A978-3-319-68780-3%2F1.pdf\)](https://link.springer.com/content/pdf/bbm%3A978-3-319-68780-3%2F1.pdf)

2) Trig identities:

$$\cos^2 x + \sin^2 x = 1$$

$$\sin(A \pm B) = \sin A \cos B \pm \cos A \sin B$$

$$\cos(A \pm B) = \cos A \cos B \mp \sin A \sin B$$

$$\tan(A \pm B) = \frac{\tan A \pm \tan B}{1 \mp \tan A \tan B}$$

$$\cos x + \cos y = 2 \cos\left(\frac{x+y}{2}\right) \cos\left(\frac{x-y}{2}\right)$$

$$\sin x + \sin y = 2 \sin\left(\frac{x+y}{2}\right) \cos\left(\frac{x-y}{2}\right)$$

3) Double-angle formulae:

$$\sin 2x = 2 \sin x \cos x$$

$$\cos 2x = \cos^2 x - \sin^2 x = \frac{1 - \tan^2 x}{1 + \tan^2 x}$$

$$\tan 2x = \frac{2 \tan x}{1 - \tan^2 x}$$

$$\cos^2 x = \frac{1 + \cos 2x}{2}, \quad \sin^2 x = \frac{1 - \cos 2x}{2}$$

4) Hyperbolic function identities:

$$\cosh^2 x - \sinh^2 x = 1$$

$$\sinh^{-1} x = \ln\left(x + \sqrt{x^2 + 1}\right)$$

$$\cosh^{-1} x = \ln\left(x + \sqrt{x^2 - 1}\right)$$

$$\tanh^{-1} x = \frac{1}{2} \ln\left(\frac{1+x}{1-x}\right)$$

5) Some standard integrals:

$$\int_a^b u \, dv = uv \Big|_a^b - \int_a^b v \, du$$

$$\int \frac{dx}{1-x^2} = \frac{1}{2} \ln \left| \frac{1+x}{1-x} \right| + \text{const}$$

$$\int \frac{dx}{1+x^2} = \tan^{-1} x + \text{const}$$

$$\int \frac{dx}{\sqrt{1+x^2}} = \sinh^{-1} x + \text{const}$$

$$\int \frac{dx}{\sqrt{1-x^2}} = \sin^{-1} x + \text{const}, \quad |x| \leq 1$$

$$\int \frac{dx}{\sqrt{x^2 - 1}} = \cosh^{-1} x + \text{const}, \quad |x| \geq 1$$

$$\begin{aligned}
 \tan(A \pm B) &= \frac{\sin(A \pm B)}{\cos(A \pm B)} \\
 &= \frac{\sin A \cos B \pm \cos A \sin B}{\cos A \cos B \mp \sin A \sin B} \\
 &= \frac{\tan A \pm \tan B}{1 \mp \tan A \tan B}
 \end{aligned}$$

$$\begin{aligned}
 \cos x + \cos y &= \cos(A+B) + \cos(A-B) \quad \left(\begin{array}{l} x = A+B \\ y = A-B \end{array} \right) \\
 &= \cos A \cos B - \cancel{\sin A \sin B} \\
 &\quad + \cos A \cos B + \cancel{\sin A \sin B} \\
 &= 2 \cos A \cos B \quad A = \frac{1}{2}(x+y) \\
 &= 2 \cos\left(\frac{x+y}{2}\right) \cos\left(\frac{x-y}{2}\right) \quad B = \frac{1}{2}(x-y) \\
 \sin x + \sin y &= \sin(A+B) + \sin(A-B) \\
 &= \sin A \cos B + \cancel{\cos A \sin B} + \sin A \cos B - \cancel{\cos A \sin B} \\
 &= 2 \sin A \cos B = 2 \sin\left(\frac{x+y}{2}\right) \cos\left(\frac{x-y}{2}\right)
 \end{aligned}$$

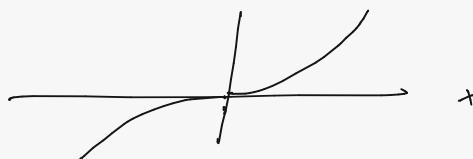
$$\begin{aligned}\cos 2x &= \cos^2 x - \sin^2 x \\ &= \frac{\cos^2 x - \sin^2 x}{\cos^2 x + \sin^2 x} \\ &= \frac{1 - \tan^2 x}{1 + \tan^2 x}\end{aligned}$$

$$\begin{aligned}\cos 2x &= \cos^2 x - \sin^2 x \\ &= 2\cos^2 x - 1 = 1 - 2\sin^2 x\end{aligned}$$

Thus, $\cos^2 x = \frac{1 + \cos 2x}{2}$

$$\sin^2 x = \frac{1 - \cos 2x}{2}$$

$$\cosh x = \frac{e^x + e^{-x}}{2}, \quad \sinh x = \frac{e^x - e^{-x}}{2}$$



$$\begin{aligned}
 (\cosh^2 x - \sinh^2 x) &= \left(\frac{e^x + e^{-x}}{2} \right)^2 - \left(\frac{e^x - e^{-x}}{2} \right)^2 \\
 &= \frac{1}{4} [e^{2x} + e^{-2x} + 2 - (e^{2x} - e^{-2x}) + 2] \\
 &= 1
 \end{aligned}$$

$$\tanh^{-1} x = \frac{1}{2} \ln \left(\frac{1+x}{1-x} \right)$$

Proof: $y = \tanh^{-1} x \iff x = \tanh y$

$$\begin{aligned}
 x &= \tanh y \\
 &= \frac{\sinh y}{\cosh y} \\
 &= \frac{e^y - e^{-y}}{e^y + e^{-y}} \\
 &= \frac{e^{2y} (e^{-2y} - 1)}{e^{2y} (e^{2y} + 1)} \\
 &= \frac{u - 1}{u + 1} \quad \text{where } u = e^{2y}
 \end{aligned}$$

$$x = \frac{u-1}{u+1} \rightarrow xu + x = u - 1 \\ 1+x = u(1-x)$$

$$u = \frac{1+x}{1-x}$$

Thus, $e^{2y} = \frac{1+x}{1-x}$

$$2y = \ln\left(\frac{1+x}{1-x}\right) \rightarrow y = \frac{1}{2} \ln\left(\frac{1+x}{1-x}\right)$$

$$\tanh^{-1} x = \frac{1}{2} \ln\left(\frac{1+x}{1-x}\right)$$

$$\sinh^{-1} x = \ln(x + \sqrt{x^2 + 1})$$

Proof: Let $y = \sinh^{-1} x \iff x = \sinh y$

$$= \frac{1}{2} (e^y - e^{-y}) \\ = \frac{1}{2} e^{-y} (e^{2y} - 1) \\ = \frac{1}{2} \frac{1}{u} (u^2 - 1) \quad \text{where } u = e^y$$

$$x = \frac{1}{2^4} (u^2 - 1)$$

$$2ux = u^2 - 1$$

$$\rightarrow 0 = u^2 - 2xu - 1$$

$$u = \frac{2x \pm \sqrt{4x^2 - 4(-1)}}{2}$$

$$= x \pm \sqrt{x^2 + 1} \quad (\text{take } +\sqrt{\quad} \text{ is odd for } u > 0)$$

$$\text{Thus, } y = \ln u = \ln [x + \sqrt{x^2 + 1}]$$

$$\cosh^{-1} x = \ln [x + \sqrt{x^2 - 1}]$$

Proof: $y = \cosh^{-1} x \iff x = \cosh y$

$$\begin{aligned} &= \frac{1}{2} (e^y + e^{-y}) \\ &= \frac{1}{2} e^y (e^{2y} + 1) \\ &= \frac{1}{2u} (u^2 + 1) \quad \text{where } u = e^y \end{aligned}$$

$$x = \frac{1}{2u} (u^2 + 1)$$

$$2ux = u^2 + 1$$

$$\partial = u^2 - 2ux + 1$$

$$\rightarrow u = \frac{2x \pm \sqrt{4x^2 - 4}}{2}$$

$$= x \pm \sqrt{x^2 - 1} \quad \left(\text{again take } + \sqrt{} \right)$$

Thus, $y = \ln u$

$$= \ln [x \pm \sqrt{x^2 - 1}]$$

Integrals:

$$\int \frac{dx}{1-x^2} = \frac{1}{2} \int \frac{dx}{1-x} + \frac{1}{2} \int \frac{dx}{1+x} = -\frac{1}{2} \ln |1-x| + \frac{1}{2} \ln |1+x| = \frac{1}{2} \ln \left| \frac{1+x}{1-x} \right| + \text{const}$$

$$\frac{1}{1-x^2} = \frac{A}{1-x} + \frac{B}{1+x} = \frac{A(1+x) + B(1-x)}{1-x^2} = \frac{(A+B)x + (A-B)}{1-x^2}$$

$$\rightarrow A+B = 0 \rightarrow A = \frac{1}{2}, B = -\frac{1}{2} \quad \frac{1}{1-x^2} = \frac{1}{2} \left(\frac{1}{1-x} - \frac{1}{1+x} \right)$$

A) Alternatively:

$$\int \frac{dx}{1-x^2} = \int \frac{dy}{\cosh^2 u} \cdot \cosh^2 u = u + \text{const} = \tanh^{-1} x + \text{const}$$

Let: $x = \tanh u$

$$\text{Now: } \cosh^2 u - \sinh^2 u = 1$$

$$1 - \tanh^2 u = \frac{1}{\cosh^2 u}$$

$$\left. \begin{aligned} d(\tanh u) &= d\left(\frac{\sinh u}{\cosh u}\right) \\ &= \left(\frac{\cosh^2 u - \sinh^2 u}{\cosh^2 u}\right) dy \\ &= \frac{dy}{\cosh^2 u} \end{aligned} \right\}$$



$$\int \frac{dx}{1+x^2} = \int \frac{dy}{\cos^2 u} \cdot \cos^2 u = u + \text{const} = \tanh^{-1} x + \text{const}$$

Let: $x = \tan u$

$$\text{Now: } \sin^2 u + \cos^2 u = 1$$

$$\tan^2 u + 1 = \frac{1}{\cos^2 u}$$

$$\left. \begin{aligned} d(\tan u) &= d\left(\frac{\sin u}{\cos u}\right) \\ &= \left(\frac{\cos^2 u + \sin^2 u}{\cos^2 u}\right) dy \\ &= \frac{dy}{\cos^2 u} \end{aligned} \right\}$$

$$\int \frac{dx}{\sqrt{1-x^2}} = \int \frac{\cos u \, dy}{\sqrt{\cos^2 u}} = \int dy = u + \text{const} = \sin^{-1} x + \text{const}$$

but $|x| < 1$

Let: $x = \sin u$

$$dx = \cos u \, du$$

$$1 - \sin^2 u = \cos^2 u$$

$$\int \frac{dx}{\sqrt{1+x^2}} = \int \frac{\cosh u \, dy}{\sqrt{\cosh^2 u}} = \int dy = u + \text{const} = \sinh^{-1} x + \text{const}$$

Let: $x = \sinh u$

$$dx = \cosh u \, du$$

$$1 + \sinh^2 u = \cosh^2 u$$

$$\int \frac{dx}{\sqrt{x^2-1}} = \int \frac{\sinh u \, dy}{\sqrt{\sinh^2 u}} = \int dy = u + \text{const} = \cosh^{-1} x + \text{const}$$

Let: $x = \cosh u > 1$

$$dx = \sinh u \, du$$

$$x^2 - 1 = \cosh^2 u - 1 = \sinh^2 u$$

6) Beta function and Gamma function:

$$B(x, y) \equiv \int_0^1 dt t^{x-1} (1-t)^{y-1} = \frac{\Gamma(x)\Gamma(y)}{\Gamma(x+y)}, \quad \text{where } \operatorname{Re}(x) > 0, \operatorname{Re}(y) > 0$$

$$\Gamma(z) \equiv \int_0^\infty dx x^{z-1} e^{-x}, \quad \text{where } \operatorname{Re}(z) > 0$$

$\Gamma(z)$ is a generalization of the factorial function $n!$:

$$\Gamma(z+1) = z\Gamma(z)$$

Useful value:

$$\Gamma(1/2) = \sqrt{\pi}$$

7) Elliptic functions and integrals:

Consider an ellipse with semi-major axis a , semi-minor axis b , and eccentricity $k \equiv \sqrt{1 - (b/a)^2}$:

$$\left(\frac{x}{a}\right)^2 + \left(\frac{y}{b}\right)^2 = 1$$

As usual let

$$x = r \cos \theta, \quad y = r \sin \theta, \quad r^2 = x^2 + y^2$$

For a given k , define the following three functions

$$\operatorname{cn}(u, k) \equiv x/a, \quad \operatorname{sn}(u, k) \equiv y/b, \quad \operatorname{dn}(u, k) \equiv r/a$$

where the argument u is defined by

$$u \equiv \frac{1}{b} \int_0^\theta r d\theta$$

Then it's easy to show that

$$\operatorname{cn}^2 u + \operatorname{sn}^2 u = 1, \quad \operatorname{dn}^2 u + k^2 \operatorname{sn}^2 u = 1$$

where we have dropped the k dependence above (and henceforth) to simplify the notation.

One can also prove the following differential identities:

$$\frac{d}{du} \operatorname{sn} u = \operatorname{cn} u \operatorname{dn} u, \quad \frac{d}{du} \operatorname{cn} u = -\operatorname{sn} u \operatorname{dn} u, \quad \frac{d}{du} \operatorname{dn} u = -k^2 \operatorname{sn} u \operatorname{cn} u$$

These equations can be integrated, e.g., the first being

$$u = \int \frac{d(\operatorname{sn} u)}{\operatorname{cn} u \operatorname{dn} u} = \int_0^{\operatorname{sn} u} \frac{dt}{\sqrt{1-t^2} \sqrt{1-k^2 t^2}}$$

or, equivalently,

$$\operatorname{sn}^{-1} x = \int_0^x \frac{dt}{\sqrt{1-t^2} \sqrt{1-k^2 t^2}}$$

which is the inverse of the sn function.

This equation is typically written in mathematical handbooks as the *Jacobi elliptic function of the 1st kind* with *amplitude* ϕ and *modulus* k :

$$F(\phi, k) \equiv \int_0^{\sin \phi} \frac{dt}{\sqrt{1-t^2} \sqrt{1-k^2 t^2}}$$

Setting $\sin \phi = 1$ gives the complete elliptic integral of 1st kind:

$$K(k) \equiv F(\pi/2, k) = \int_0^1 \frac{dt}{\sqrt{1-t^2} \sqrt{1-k^2 t^2}}$$

There are also Jacobi elliptic functions and complete elliptic integrals of the 2nd and 3rd kind:

2nd kind:

$$E(\phi, k) \equiv \int_0^{\sin \phi} dt \frac{\sqrt{1-k^2 t^2}}{\sqrt{1-t^2}}, \quad E(k) \equiv \int_0^1 dt \frac{\sqrt{1-k^2 t^2}}{\sqrt{1-t^2}}$$

3rd kind:

$$\pi(n, \phi, k) \equiv \int_0^{\sin \phi} \frac{dt}{(1-n t^2) \sqrt{1-t^2} \sqrt{1-k^2 t^2}}, \quad \pi(n, k) \equiv \int_0^1 \frac{dt}{(1-n t^2) \sqrt{1-t^2} \sqrt{1-k^2 t^2}}$$

The Jacobi elliptic functions and complete elliptic integrals of the 2nd kind arise when computing the arclength along the circumference of an ellipse.

NOTE: The functions $\operatorname{sn}(u, k)$, $\operatorname{cn}(u, k)$ are generalizations of the circular functions $\sin \theta$, $\cos \theta$ to an ellipse with eccentricity k . When $k = 0$, $u \rightarrow \theta$, $\operatorname{sn} \rightarrow \sin$, $\operatorname{cn} \rightarrow \cos$, and $\operatorname{dn} \rightarrow 1$.

The Jacobi elliptic parameter ϕ is related to u via:

$$\sin \phi = \text{sn}(u, k) \quad \text{or} \quad \cos \phi = \text{cn}(u, k)$$

The angle ϕ gives us a different parameterization of the ellipse defined by

$$x = a \cos \phi, \quad y = b \sin \phi$$

Note that ϕ is not the same as the polar coordinate angle θ nor the elliptic parameter u . These three parameters are related by

$$x = r \cos \theta = a \cos \phi = a \text{cn}(u, k), \quad y = r \sin \theta = b \sin \phi = b \text{sn}(u, k)$$

Plot sn(u,k), cn(u,k), and dn(u,k) for different values of k

```
In [3]: # discrete u values
u = np.linspace(0, 10, 10000)

# consider several different values for k
k = np.array([0, 0.25, 0.5, 0.75, 0.9])

# make plots of sn(u,k)
plt.figure()
plt.xlabel('u$', size=20)
plt.ylabel('sn(u$; $k$)', size=20)
for ii in range(len(k)):
    m = k[ii]**2 # scipy uses m=k^2
    sn_u, cn_u, dn_u, ph_u = special.ellipj(u, m)
    plt.plot(u, sn_u)

_=plt.legend(k)

# compare with ordinary sine function
sin_u = np.sin(u)
plt.plot(u, sin_u, color='k', ls='--', lw=3)

#####
# make plots of cn(u,k)
plt.figure()
plt.xlabel('u$', size=20)
plt.ylabel('cn(u$; $k$)', size=20)
for ii in range(len(k)):
    m = k[ii]**2 # scipy uses m=k^2
    sn_u, cn_u, dn_u, ph_u = special.ellipj(u, m)
    plt.plot(u, cn_u)

_=plt.legend(k)

# compare with ordinary cosine function
```

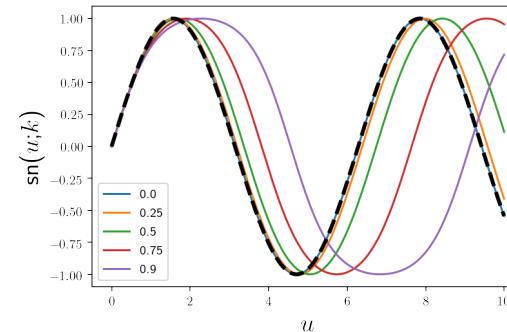
```
cos_u = np.cos(u)
plt.plot(u, cos_u, color='k', ls='--', lw=3)

#####
# make plots of dn(u,k)
plt.figure()
plt.xlabel('u$', size=20)
plt.ylabel('dn(u$; $k$)', size=20)
for ii in range(len(k)):
    m = k[ii]**2 # scipy uses m=k^2
    sn_u, cn_u, dn_u, ph_u = special.ellipj(u, m)
    plt.plot(u, dn_u)

_=plt.legend(k)

# compare with ordinary sine functions
unit = np.ones(len(u))
plt.plot(u, unit, color='k', ls='--', lw=3)
```

Out[3]: [`<matplotlib.lines.Line2D at 0x81a10d208>`]



$$\Gamma(z) \equiv \int_0^\infty dx \quad x^{z-1} \quad e^{-x} \quad \text{Re}(z) > 0$$

$$\begin{aligned}\Gamma\left(\frac{1}{2}\right) &= \int_0^\infty dx \quad x^{-\frac{1}{2}} \quad e^{-x} \\ &= \int_0^\infty 2x du \left(\frac{1}{u}\right) e^{-u^2} \\ &= 2 \int_0^\infty du \quad e^{-u^2}\end{aligned}$$

Let: $u = x^{\frac{1}{2}}$
 $x = u^2 \rightarrow x^{-\frac{1}{2}} = u^{-1}$
 $dx = 2u dy$

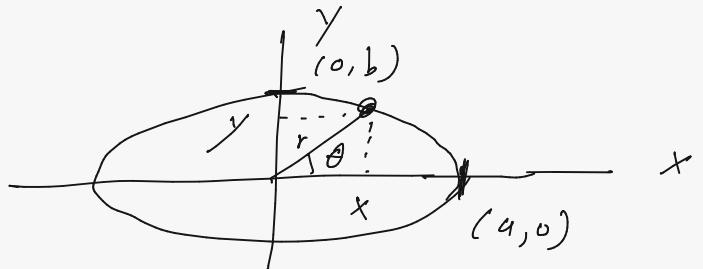
$$\begin{aligned}\text{Thus, } \left(\Gamma\left(\frac{1}{2}\right)\right)^2 &= 4 \int_0^\infty dx \quad e^{-x^2} \int_0^\infty dy \quad e^{-y^2} \\ &= 4 \int_0^\infty \int_0^\infty dx dy \quad e^{-(x^2+y^2)} \\ &= 4 \int_{r=0}^\infty \int_{\phi=0}^{\pi/2} r dr d\phi \quad e^{-r^2} \\ &= 4 \cdot \frac{\pi}{2} \int_0^\infty r dr \quad e^{-r^2} \\ &= 2\pi \int_0^\infty r dr \quad e^{-r^2}\end{aligned}$$

$$\begin{aligned}
 \left(\Gamma\left(\frac{1}{2}\right)\right)^2 &= 2\pi \int_0^\infty r dr e^{-r^2} & u = r^2 \\
 &= \pi \int_0^\infty du e^{-u} & du = 2r dr \\
 &= -\pi e^{-u} \Big|_0^\infty \\
 &= -\pi \left(\frac{1}{\infty} - 1 \right) \\
 &= \pi
 \end{aligned}$$

$$\text{So } \Gamma\left(\frac{1}{2}\right) = \sqrt{\pi}$$



Liaptic Functions / Integrals:



$$\begin{aligned} x &= r \cos \theta \\ y &= r \sin \theta \end{aligned} \quad \left. \begin{array}{l} \text{standard} \\ \text{expressions,} \end{array} \right\}$$

$\Rightarrow \tan \theta = \frac{y}{x}, \quad r^2 = x^2 + y^2$

Ellipse: $\left(\frac{x}{a}\right)^2 + \left(\frac{y}{b}\right)^2 = 1$

Define (for fixed π):

$$cn(u; k) \equiv \frac{x}{a}$$

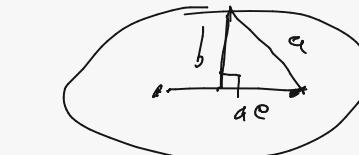
$$sn(u; k) \equiv \frac{y}{b}$$

$$dn(u; k) \equiv \frac{r}{a}$$

where $u \equiv \frac{1}{b} \int_0^\theta r d\theta$

NOTE: For a circle ($a = b = r$) $\rightarrow u = \theta$

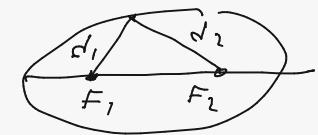
defn:



$$a^2 e^2 + b^2 = a^2$$

$$b^2 = a^2(1 - e^2)$$

$$b = a \sqrt{1 - e^2}$$



$$d_1 + d_2 = 2a$$

$$e^2 = \frac{a^2 - b^2}{a^2} = 1 - \left(\frac{b}{a}\right)^2$$

$$e = \sqrt{1 - \left(\frac{b}{a}\right)^2} = k$$

standard
notation

(called
'modulus')

$$cn(u; 0) = \cos \theta$$

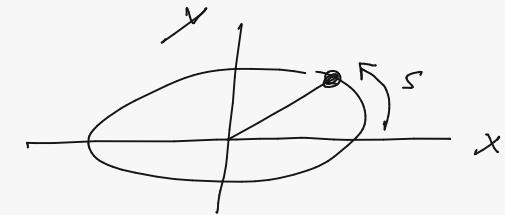
$$sn(u; 0) = \sin \theta$$

$$dn(u; 0) = 1$$

NOTE:

u ≠ arc length s

$$s \equiv \int ds = \int_0^\theta \sqrt{dr^2 + r^2 d\theta^2}$$



no dr term in definition of u

Algebraic

Identity:

$$\left(\frac{x}{a}\right)^2 + \left(\frac{y}{b}\right)^2 = 1 \quad \rightarrow \quad \cos^2 u + \sin^2 u = 1 \quad (\text{since } \cos^2 + \sin^2 = 1)$$

$$H = \sqrt{1 - \left(\frac{b}{a}\right)^2} \quad \Rightarrow \quad \frac{du^2}{u} = \left(\frac{r}{a}\right)^2$$

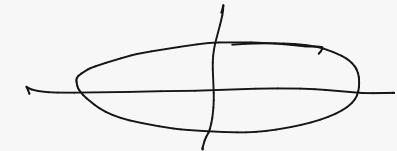
$$= \frac{x^2 + y^2}{a^2}$$

$$\text{So } \sin^2 u + H^2 \sin^2 u = 1$$

Differential identities:

$$\begin{aligned}\frac{d}{du} \sin u &= \frac{d}{du} \left(\frac{y}{r} \right) \\ &= \frac{\cancel{dy}}{r \cancel{du}}\end{aligned}$$

$$du = \frac{rd\theta}{b}$$

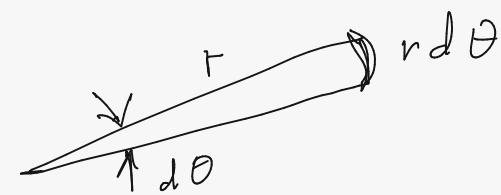


Now: $x = r \cos \theta$, $y = r \sin \theta$

$$\begin{aligned}dx &= dr \cos \theta - r \sin \theta d\theta \\ dy &= dr \sin \theta + r \cos \theta d\theta\end{aligned}$$

$$\begin{aligned}x dy - y dx &= r^2 \cos^2 \theta d\theta + r^2 \sin^2 \theta d\theta \\ &= r^2 d\theta\end{aligned}$$

$$\text{So } rd\theta = \frac{1}{r} (x dy - y dx)$$



$$\rightarrow \frac{d}{du} \sin u = \frac{r \cancel{dy}}{(x \cancel{dy} - y \cancel{dx})}$$

[need to replace terms of \cancel{dy}]

Als:

$$l = \left(\frac{x}{a}\right)^2 + \left(\frac{y}{b}\right)^2$$

$$\rightarrow \partial = \frac{\partial x}{a^2} dx + \frac{\partial y}{b^2} dy$$

$$\frac{x}{a^2} dx = \frac{-y dy}{b^2}$$

so $dx = -\left(\frac{a}{b}\right)^2 \left(\frac{y}{x}\right) dy$

Thus,

$$\frac{d}{dy} \ln u = \frac{r dy}{x dy - y dx} = \frac{r dx}{x dx + y \left(\frac{a}{b}\right)^2 \frac{y}{x} dx}$$

$$= \frac{x r}{x^2 + y^2 \left(\frac{a}{b}\right)^2}$$

$$= \left(\frac{x}{a}\right) \left(\frac{r}{a}\right) \frac{1}{\left(\frac{x}{a}\right)^2 + \left(\frac{y}{b}\right)^2}$$

$$= \ln u - \ln a \quad \left(\text{using } \left(\frac{x}{a}\right)^2 + \left(\frac{y}{b}\right)^2 = 1 \right)$$

From this it follows that:

$$\begin{aligned}\frac{d}{du} \sin u &= \frac{d}{du} \sqrt{1 - \sin^2 u} \\ &= \frac{1}{\cancel{\sqrt{}}} - \cancel{\sqrt{}} \sin u \frac{d}{du} \sin u \\ &= -\frac{\sin u}{\cancel{\sin u}} \cdot \cancel{\sin u} du \\ &= -\sin u \cdot du\end{aligned}$$

$$\begin{aligned}\frac{d}{du} \csc u &= \frac{d}{du} \sqrt{1 - \csc^2 u} \\ &= \frac{1}{\cancel{\sqrt{}}} - \cancel{\sqrt{}} \csc u \frac{d}{du} \csc u \\ &= -\frac{\csc^2 u}{\cancel{\csc u}} \cdot \cancel{\csc u} du \\ &= -\csc^2 u \cdot du\end{aligned}$$

Integral expressions:

$$\frac{d}{du} \sin u = \cos u \quad du$$

$$\rightarrow \int \frac{d(\sin u)}{\cos u \quad du} = \int du$$

$$RHS = u + \text{const}$$

$$LHS = \int \frac{d(\cos u)}{\cos u \quad du}$$

$$= \int \frac{d(\sin u)}{\sqrt{1 - \sin^2 u} \quad \sqrt{1 - H^2 \sin^2 u}}$$

$$= \int \frac{dt}{\sqrt{1 - t^2} \quad \sqrt{1 - H^2 t^2}} \quad (t = \sin u)$$

Now, $\sin^2 u + \cos^2 u = 1$
 $\cos^2 u = 1 - \sin^2 u$

or, equivalently,

$$\int \frac{dt}{\sqrt{1 - t^2} \quad \sqrt{1 - H^2 t^2}} = \sin^{-1} t + \text{const}$$

$$\sin^{-1} t + \text{const} = \int \frac{dt}{\sqrt{1-t^2} \sqrt{1-h^2 t^2}}$$

(analogous to $\int \frac{dt}{\sqrt{1-t^2}} = \sin^{-1} t + \text{const}$)

$$F(\phi, h) = \int_0^{\sin \phi} \frac{dt}{\sqrt{1-t^2} \sqrt{1-h^2 t^2}}$$

/
 amplitude modulus

"Jacobi elliptic function of 1st kind"

$$H(h) \equiv F(\phi=0, h) = \int_0^1 \frac{dt}{\sqrt{1-t^2} \sqrt{1-h^2 t^2}}$$

"Complete elliptic integral of 1st kind"

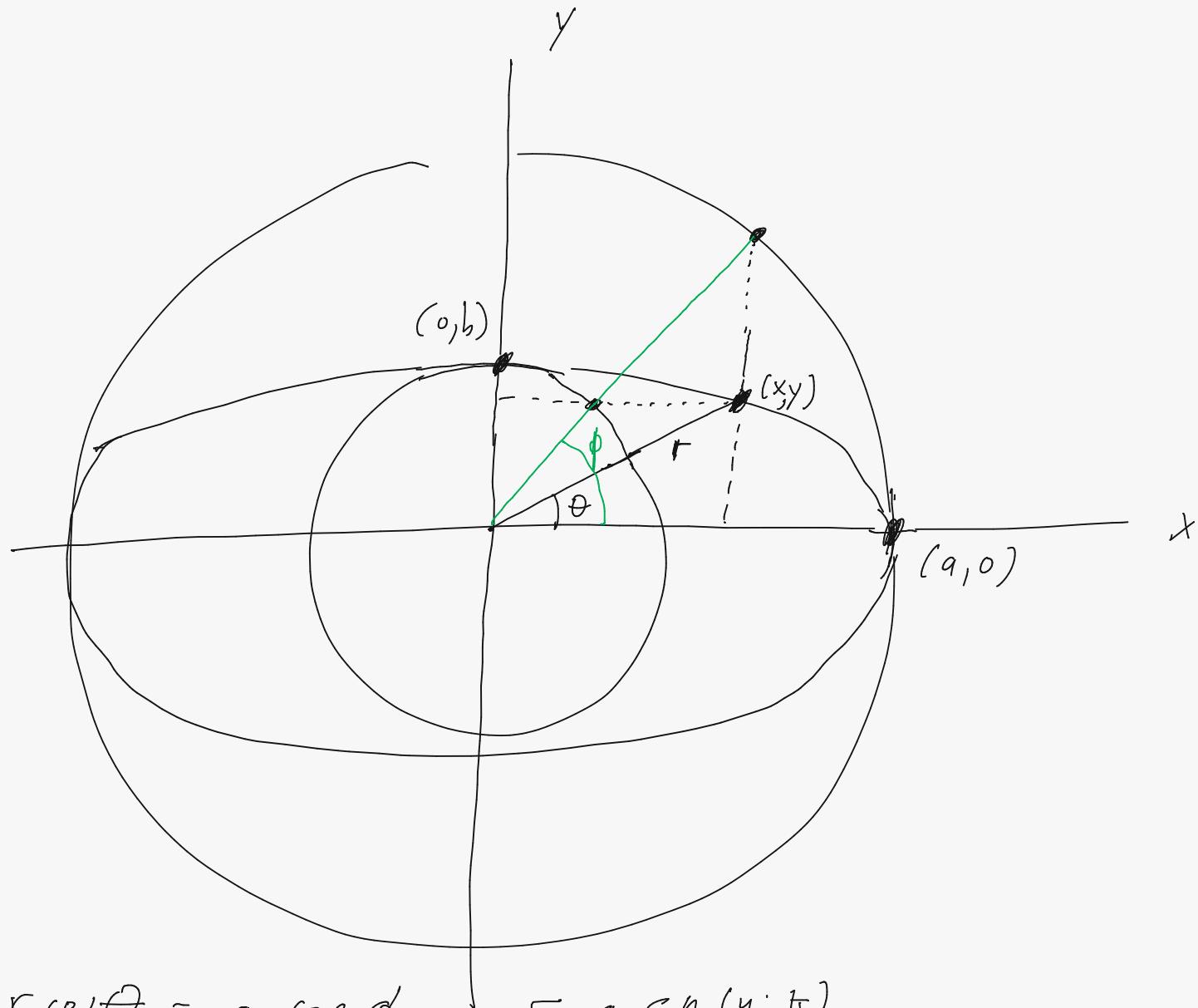
Recall: $u = \sin^{-1} x \iff x = \sin u = \sin \phi$ (or $\cos u = \cos \phi$)

using $\cos u = \sqrt{1-\sin^2 u}$ and

similar expression for $\cos \phi$

Thus, $x = r \cos \theta = a \cos u = a \cos \phi$
 $y = r \sin \theta = b \sin u = b \sin \phi$

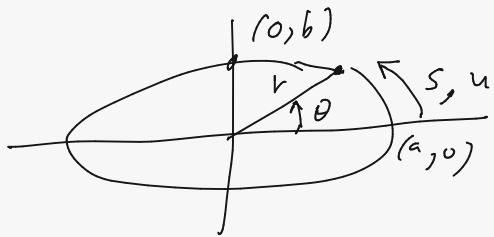
$\theta \neq \phi \neq u$ (except for a circle where $r=a=b$)



$$X = r \cos \theta = a \cos \phi \quad \subseteq a \cos(u; \pi)$$

$$Y = r \sin \theta = b \sin \phi \quad = b \sin(u; \pi)$$

Arc Length Calculations:



$$s = \int ds$$

$$= \int_0^u \left| \frac{ds}{du} \right| du$$

$$\begin{aligned}\frac{ds}{du} &= \sqrt{\left(\frac{dx}{du} \right)^2 + \left(\frac{dy}{du} \right)^2} \quad \text{where } x = a \cos u \\ &= \sqrt{a^2 \left(\frac{d(\cos u)}{du} \right)^2 + b^2 \left(\frac{d(\sin u)}{du} \right)^2} \\ &= du \sqrt{a^2 \sin^2 u + b^2 \cos^2 u} \\ &= du \sqrt{a^2 (1 - \cos^2 u) + b^2 \cos^2 u} \\ &= du \sqrt{a^2 - (a^2 - b^2) \cos^2 u} \\ &= a du \sqrt{1 - \left(\frac{a^2 - b^2}{a^2} \right) \cos^2 u} \\ &= -a \frac{d(\cos u)}{du} \sqrt{\frac{1 - \cos^2 u}{1 - \cos^2 u}}\end{aligned}$$

$\frac{d \sin u}{du} = \cos u \cdot du$
 $\frac{d \cos u}{du} = -\sin u \cdot du$

$a^2 = a^2 e^2 + b^2$
 $e^2 = \frac{a^2 - b^2}{a^2}$

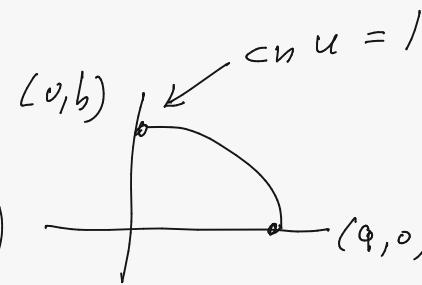
$du = -\frac{d \cos u}{du} \frac{1}{\sin u}$
 $= -\frac{d \cos u}{du} \frac{1}{\sqrt{1 - \cos^2 u}}$

Let $t \equiv \cosh u$

$$\frac{ds}{du} = -\frac{adt}{du} \sqrt{1-t^2} t^2$$

so

$$s = a \int_0^{\cosh u} \left| \frac{ds}{du} \right| du$$
$$= a \int_0^{\cosh u} \frac{dt \sqrt{1-t^2}}{\sqrt{1-t^2}}$$



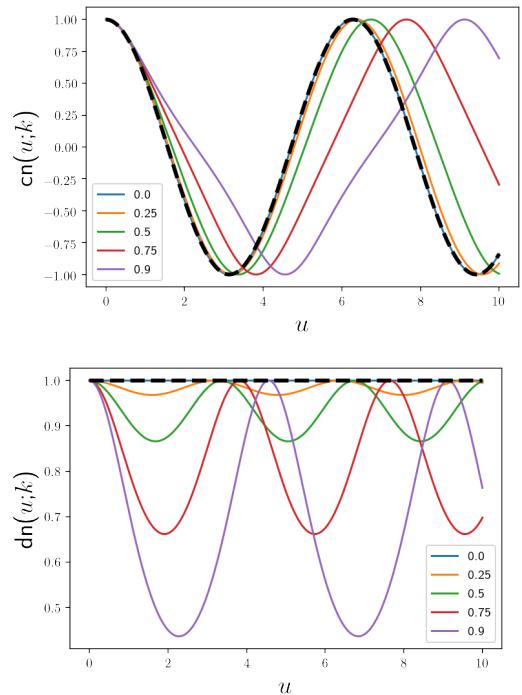
Circumference:

$$C = 4 \cdot \left(\text{arc length from } (a,0) \rightarrow (0,b) \right)$$

$$= 4a \int_0^1 \frac{dt \sqrt{1-t^2}}{\sqrt{1-t^2}}$$

$\equiv E(H)$

complete elliptic integral
of the 2nd kind



Plot an ellipse using the $\text{sn}(u,k)$, $\text{cn}(u,k)$ (or $\sin \phi$, $\cos \phi$) functions

```
In [4]: # semi-major, semi-minor axes
a = 2.
b = 1.

# calculate eccentricity
k = np.sqrt(1-(b/a)**2)
m = k**2 # scipy uses m=k^2
print('k = ', k)
print('m = k^2 = ', m)

# period
P = 4*np.pi*special.ellipk(m)
print('period = ', P)

# circumference
C = 4*a*special.ellipe(m)
print('circumference = ', C)

C_approx = 2*np.pi*np.sqrt((a**2+b**2)/2)
print('approx circumference = ', C_approx)

# calculate elliptic functions
u = np.linspace(0, P, 10000)
sn, cn, dn, ph = special.ellipj(u, m)
x = a*cn
y = b*sn

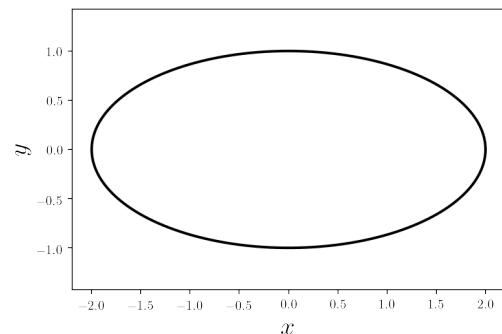
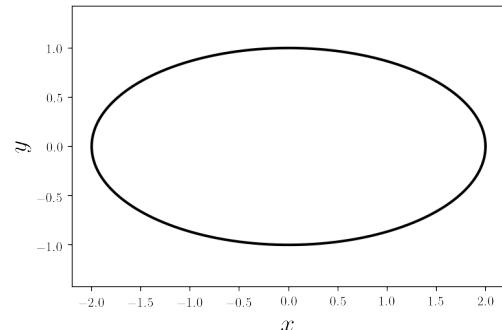
# plot figure
plt.figure()
plt.axis('equal')
plt.plot(x, y, color='k', ls='-', lw=2)
plt.xlabel('$x$', size=20)
plt.ylabel('$y$', size=20)

# alternative parametrization in terms of ordinary sine, cosine and angle phi
phi = np.linspace(0, 2*np.pi, 10000)
x = a*np.cos(phi)
y = b*np.sin(phi)

# plot figure
plt.figure()
plt.axis('equal')
plt.plot(x, y, color='k', ls='-', lw=2)
plt.xlabel('$x$', size=20)
plt.ylabel('$y$', size=20)
```

```
k = 0.8660254037844386
m = k^2 = 0.7499999999999999
period = 8.626062589998572
circumference = 9.688448220547675
approx circumference = 9.934588265796101
```

Out[4]: Text(0, 0.5, '\$y\$')



Compare arc length s, u, phi, theta

```
In [5]: # discrete u values
u = np.linspace(0, 10, 10000)

# consider several different values for k
```

```
k = np.array([0, 0.25, 0.5, 0.75, 0.9])

# corresponding values of a and b
b = np.array([1, 1, 1, 1, 1])
a = b/np.sqrt(1-k**2)

#####
# plot arc length s vs b*u
plt.figure()
plt.xlabel('$b u$', size=20)
plt.ylabel('$s$', size=20)

for ii in range(len(k)):
    m = k[ii]**2 # scipy uses m=k^2
    sn_u, cn_u, dn_u, ph_u = special.ellipj(u, m)
    s_u = a[ii]*special.ellipeinc(ph_u, m)
    plt.plot(b[ii]*u, s_u)

plt.grid('on')
plt.legend(k)

#####
# plot u vs theta
# x = r cos(theta) = a cos(phi) = a cn(u;k)
# y = r sin(theta) = b sin(phi) = b sn(u;k)
plt.figure()
plt.xlabel('theta', size=20)
plt.ylabel('$u$', size=20)

for ii in range(len(k)):
    m = k[ii]**2 # scipy uses m=k^2
    sn_u, cn_u, dn_u, ph_u = special.ellipj(u, m)
    theta_u = np.arctan2(b[ii]*sn_u, a[ii]*cn_u)
    theta_u = np.unwrap(theta_u)
    plt.plot(theta_u, u)

# change tick marks to multiples of pi/2
eps = 0.01
tick_locs = np.arange(0, 3*np.pi+eps, np.pi/2)
tick_labels = ['0', '$\pi$/2', '$\pi$', '3$\pi$/2', '2$\pi$', '5$\pi$/2',
               '3$\pi$']
plt.xticks(tick_locs, tick_labels)
plt.yticks(tick_locs, tick_labels)
plt.grid('on')
plt.xlim(0, 2*np.pi)
plt.ylim(0, 2*np.pi)
plt.legend(k)

#####
# plot u vs phi
```

```

plt.figure()
plt.xlabel('$\phi$', size=20)
plt.ylabel('$u$', size=20)

for ii in range(len(k)):
    m = k[ii]**2 # scipy uses m=k^2
    sn_u, cn_u, dn_u, ph_u = special.ellipj(u, m)
    plt.plot(ph_u, u)

    # change tick marks to multiples of pi/2
    eps = 0.01
    tick_locs = np.arange(0, 3*np.pi+eps, np.pi/2)
    tick_labels = ['0', '$\pi/2$', '$\pi$', '3$\pi/2$', '2$\pi', '5$\pi/2', '3$\pi']
    plt.xticks(tick_locs, tick_labels)
    plt.yticks(tick_locs, tick_labels)
    plt.grid('on')
    plt.xlim(0, 2*np.pi)
    plt.ylim(0, 2*np.pi)
    _=plt.legend(k)

#####
# plot phi vs theta
# x = r cos(theta) = a cos(phi) = a cn(u;k)
# y = r sin(theta) = b sin(phi) = b sn(u;k)
plt.figure()
plt.xlabel('theta', size=20)
plt.ylabel('$\phi$', size=20)

for ii in range(len(k)):
    m = k[ii]**2 # scipy uses m=k^2
    sn_u, cn_u, dn_u, ph_u = special.ellipj(u, m)
    theta_u = np.arctan2(b[ii]*sn_u, a[ii]*cn_u)
    theta_u = np.unwrap(theta_u)
    plt.plot(theta_u, ph_u)

    # alternative
    #phis= np.linspace(0, 2*np.pi, 10000)
    #thetas = np.arctan2(b[ii]*np.sin(phis), a[ii]*np.cos(phis))
    #thetas = np.unwrap(thetas)
    #plt.plot(thetas, phis)

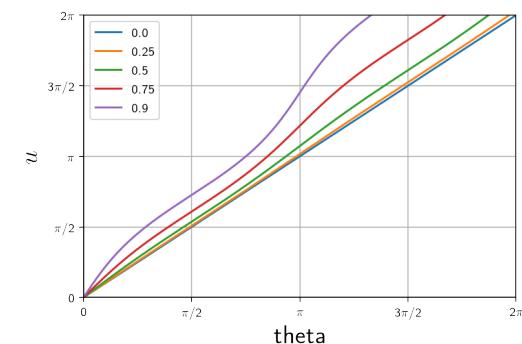
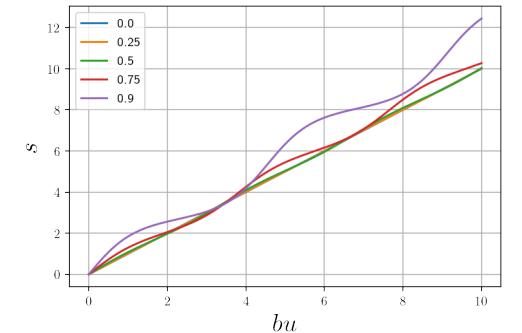
    # change tick marks to multiples of pi/2
    eps = 0.01
    tick_locs = np.arange(0, 3*np.pi+eps, np.pi/2)
    tick_labels = ['0', '$\pi/2$', '$\pi$', '3$\pi/2$', '2$\pi', '5$\pi/2', '3$\pi']
    plt.xticks(tick_locs, tick_labels)
    plt.yticks(tick_locs, tick_labels)
    plt.grid('on')

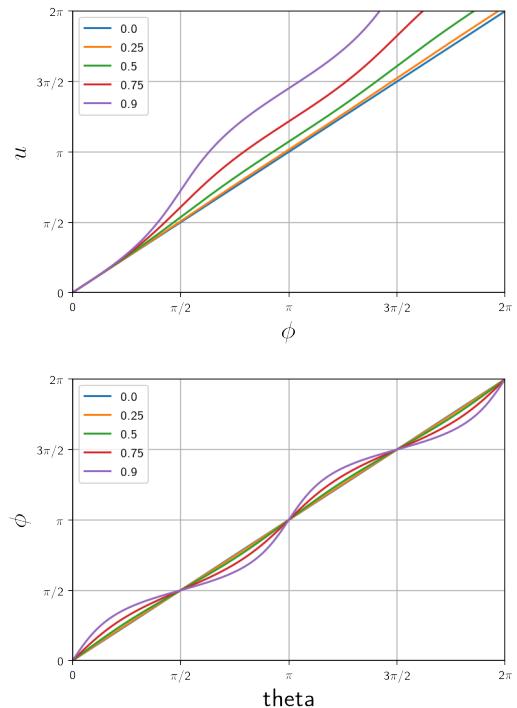
```

```

plt.xlim(0, 2*np.pi)
plt.ylim(0, 2*np.pi)
_=plt.legend(k)

```





Make a figure showing the relationship between ϕ and θ

```
In [6]: # semi-major, semi-minor axes
a = 2.
b = 1.

# define phi array
phis= np.linspace(0, 2*np.pi, 10000)

# calculate corresponding theta values
thetas = np.arctan2(b*np.sin(phis), a*np.cos(phis))
thetas = np.unwrap(thetas)

# ellipse and relevant circles
x_ellipse = a*np.cos(phis)
y_ellipse = b*np.sin(phis)

x_a = a*np.cos(phis)
y_a = a*np.sin(phis)

x_b = b*np.cos(phis)
y_b = b*np.sin(phis)

# particular value of theta and phi
phi0 = np.deg2rad(45)
theta0 = np.arctan2(b*np.sin(phi0), a*np.cos(phi0))
x0 = a*np.cos(phi0)
y0 = b*np.sin(phi0)
r0 = np.sqrt(x0**2 + y0**2)

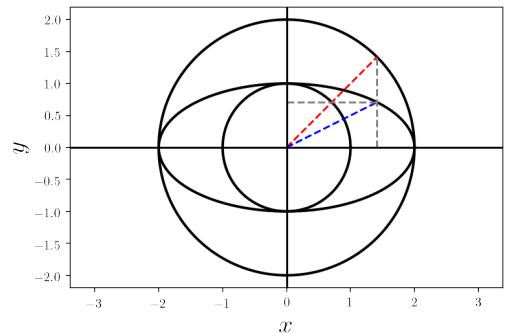
# plot ellipse, circles, and lines showing theta0 and phi0
plt.figure()

plt.plot(x_ellipse, y_ellipse, color='k', ls='-', lw=2)
plt.plot(x_a, y_a, color='k', ls='-', lw=2)
plt.plot(x_b, y_b, color='k', ls='-', lw=2)

plt.plot([0, a*np.cos(phi0)], [0, a*np.sin(phi0)], c='red', ls='--')
plt.plot([0, x0], [0, y0], c='blue', ls='--')
plt.plot([x0, x0], [0, a*np.sin(phi0)], c='grey', ls='--')
plt.plot([0, x0], [y0, y0], c='grey', ls='--')

plt.axhline(0, c='k')
plt.axvline(0, c='k')
plt.axis('equal')
plt.xlabel('$x$', size=20)
plt.ylabel('$y$', size=20)
```

```
Out[6]: Text(0, 0.5, '$y$')
```



Simple pendulum: compare small-angle and exact calculation

```
In [7]: # see L&L prob 11.1, K&S prob 1.7
```

```
# choose maximum angle phi0 (E = mgl(1-cos(phi0)))
phi0 = np.deg2rad(40)
print('phi0 =', np.rad2deg(phi0), ' degrees')

# modulus k
k = np.sin(phi0/2)
m = k**2 # scipy has K(m) where m=k^2

# constants
g = 9.8 # m/s^2
ell = 1 # m

# small angle approximation angular frequency and period
omega0 = np.sqrt(g/ell)
P0 = 2*np.pi/omega0

# actual period
P = (4/omega0)*special.ellipk(m)

# 1st order correction to the period
P1 = P0*(1 + phi0**2/16)

# display periods
print('small angle =', P0, 'sec')
print('1st order =', P1, 'sec')
print('exact period =', P, ' sec')

# discrete times
t = np.linspace(0, 4*P, 10000)

# time evolution for phi
x = omega0*t
sn_x, cn_x, dn_x, ph_x = special.ellipj(x+omega0*t/4, m)
phi = 2*np.arcsin(k*sn_x)

# make plots
plt.figure()
plt.plot(t, np.rad2deg(phi), t, np.rad2deg(phi0)*np.cos(omega0*t))
plt.xlabel('t [s]', size=20)
plt.ylabel('phi [deg]', size=20)
plt.legend(('exact motion', 'small angle approx'))
titlestr = 'phi0 = ' + str(np.rad2deg(phi0)) + ' degrees'
=plt.title(titlestr, size=20)
```

Period calculation: (beyond small-angle approximation)

Lagrangian: $L = T - U$

$$= \frac{1}{2} ml^2 \dot{\phi}^2 + mgl \cos \phi$$

$U = -mgy$

$$= -mgl \cos \phi$$

EOM: $\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\phi}} \right) = \frac{\partial L}{\partial \phi}$

$$ml^2 \ddot{\phi} = -mgl \sin \phi$$

$$\boxed{\ddot{\phi} = -\frac{g}{l} \sin \phi}$$

obtain EOM instead from cons. of energy equation

$$E = T + U = \frac{1}{2} ml^2 \dot{\phi}^2 - mgl \cos \phi$$

If released from rest at $\phi = \phi_0$ ($\equiv \phi(0)$), $\dot{\phi}(0) = 0$
we have

$$E = -mgl \cos \phi_0 = \frac{1}{2} ml^2 \dot{\phi}^2 - mgl \cos \phi$$

$$-mg l (\cos \phi_0 - \cos \phi) = \frac{1}{2} ml^2 \dot{\phi}^2$$

$$\dot{\phi} = -\sqrt{\frac{2g}{\lambda}} \sqrt{\cos \phi - \cos \phi_0}$$

because
 ϕ decreases
from ϕ_0 to 0

$|\phi| \leq \phi_0$ so $\cos \phi - \cos \phi_0 \geq 0$

Thus, $\frac{d\phi}{dt} = -\sqrt{\frac{2g}{\lambda}} \sqrt{\cos \phi - \cos \phi_0}$

$$\int_{t_0}^t dt = -\sqrt{\frac{\lambda}{2g}} \int_{\phi_0}^{\phi} \frac{d\phi}{\sqrt{\cos \phi - \cos \phi_0}}$$

$$\rightarrow t - t_0 = + \sqrt{\frac{\lambda}{2g}} \int_{\phi}^{\phi_0} \frac{d\phi}{\sqrt{\cos \phi - \cos \phi_0}}$$

write: $\cos \phi = \cos\left(\frac{1}{2}\phi\right) = 1 - 2\sin^2\left(\frac{\phi}{2}\right)$

$$\cos \phi_0 = \cos\left(\frac{1}{2}\phi_0\right) = 1 - 2\sin^2\left(\frac{\phi_0}{2}\right)$$

$$\begin{aligned} \rightarrow \cos \phi - \cos \phi_0 &= 2\left(\sin^2\left(\frac{\phi_0}{2}\right) - \sin^2\left(\frac{\phi}{2}\right)\right) \\ &= 2 \sin^2\left(\frac{\phi_0}{2}\right) \left[1 - \frac{\sin^2\left(\frac{\phi}{2}\right)}{\sin^2\left(\frac{\phi_0}{2}\right)} \right] \end{aligned}$$

want to convert
to an elliptic
integral which
involves $\sqrt{1-t^2}$,
 $\sqrt{1-k^2 t^2}$ with $k < 1$

since $|\phi| \leq \phi_0$ we have $\left| \frac{\sin(\frac{\phi}{2})}{\sin(\frac{\phi_0}{2})} \right| \leq 1$.

$\Gamma^{h_{uv}}$

$$t - t_0 = \frac{1}{2\sqrt{\epsilon}} \int_{\phi}^{\phi_0} \frac{d\phi}{\sin(\frac{\phi_0}{2}) \sqrt{1 - \frac{\sin^2(\frac{\phi}{2})}{\sin^2(\frac{\phi_0}{2})}}}$$

Def. h_r:

$$x = \frac{\sin(\frac{\phi}{2})}{\sin(\frac{\phi_0}{2})} \rightarrow \sqrt{\quad} = \sqrt{1-x^2}$$

$$dx = \frac{1}{\sin(\frac{\phi_0}{2})} \frac{1}{2} \cos\left(\frac{\phi}{2}\right) d\phi \rightarrow \frac{d\phi}{\sin(\frac{\phi_0}{2})} = \frac{2 dx}{\cos\left(\frac{\phi}{2}\right)}$$

$$\begin{aligned} \phi = \phi_0 &\rightarrow x = 1 \\ &= \frac{2 dx}{\sqrt{1 - \sin^2\left(\frac{\phi_0}{2}\right)}} \\ &= \frac{2 dx}{\sqrt{1 - \sin^2\left(\frac{\phi_0}{2}\right)} x^2} \\ &= \frac{2 dx}{\sqrt{1 - \frac{x^2}{1+x^2}}} \end{aligned}$$

where $H = \left| \sin\left(\frac{\phi_0}{2}\right) \right|$

T^{ho} ,

$$t - t_0 = \frac{1}{\omega \sqrt{\frac{\sigma}{\kappa}}} \int_{\phi}^{\phi_0} \frac{d\phi}{\sqrt{1 - \kappa^2 x^2} \sqrt{1 - x^2}}$$

where $H = |\sin(\frac{\phi_0}{2})|$
and $x = \frac{\sin(\frac{\phi}{2})}{\sin(\frac{\phi_0}{2})}$

$$= \frac{1}{\omega_0} \left[\int_0^{\phi_0} - \int_0^{\phi} \right] \frac{dx}{\sqrt{1 - \kappa^2 x^2} \sqrt{1 - x^2}} \quad \omega_0 = \sqrt{\frac{\sigma}{\kappa}}$$

$$= \frac{1}{\omega_0} \left[\int_0^1 - \int_0^{\phi} \right] \frac{dx}{\sqrt{1 - \kappa^2 x^2} \sqrt{1 - x^2}}$$

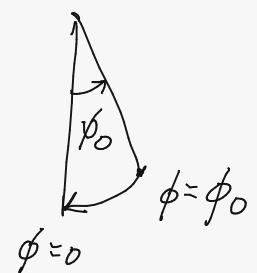
$$= \frac{1}{\omega_0} \left[H(\kappa) - \sin^{-1} \left(\frac{\sin \frac{\phi}{2}}{\sin \frac{\phi_0}{2}} \right) \right]$$

Take $t_0 = 0$:

$$\frac{P_{initial} - P}{P_{initial}} = H \times (\text{time to go from } \phi_0 \text{ to } 0)$$

$$\boxed{P = \frac{4}{\omega_0} H(\kappa)}$$

$\rightarrow H(\kappa) = \left(\frac{P}{4} \right) \omega_0$



$$t = \frac{P}{4} - \frac{\sin^{-1}}{\omega_0} \left(\frac{\sin\left(\frac{\phi}{2}\right)}{\sin\left(\frac{\phi_0}{2}\right)} \right)$$

$$\sin\left(\frac{\phi}{2}\right) = \sin\left(\frac{\phi_0}{2}\right) \sin \left[\left(\frac{P}{4} - t \right) \omega_0 ; \text{H} \right]$$

$$\Rightarrow \boxed{\phi = 2 \sin^{-1} \left[\sin\left(\frac{\phi_0}{2}\right) \sin \left(\omega_0 \left(\frac{P}{4} - t \right); \text{H} \right) \right]}$$

where $P = \frac{4}{\omega_0} \text{H}(k)$

$$\omega_0 = \sqrt{\frac{g}{l}}$$

$$\text{H} \equiv \int \sin\left(\frac{\phi_0}{2}\right) \int$$

Expansion of $H(k)$:

$$H(k) = \int_0^1 \frac{dt}{\sqrt{1-t^2} \sqrt{1-k^2 t^2}}$$

Expansion parameter = k

$$= \int_0^1 \frac{dt}{\sqrt{1-t^2}} \left(1 + \sum k^2 t^2 + \dots \right)$$

$$= \int_0^1 \frac{dt}{\sqrt{1-t^2}} + \sum k^2 \int_0^1 \frac{t^2 dt}{\sqrt{1-t^2}} + \dots$$

$$= \textcircled{A} + \textcircled{B} + \dots$$

$$\textcircled{A} = \int_0^1 \frac{dt}{\sqrt{1-t^2}} = \sin^{-1}(1) = \frac{\pi}{2}$$

$$\textcircled{B} = \frac{1}{2} k^2 \int_0^1 \frac{t^2 dt}{\sqrt{1-t^2}}$$

$$= \frac{1}{2} k^2 \int_0^{\pi/2} \frac{\sin^2 \theta \cos \theta d\theta}{\sqrt{1-\sin^2 \theta}}$$

$$\boxed{\begin{aligned} t &= \sin \theta \\ dt &= \cos \theta d\theta \end{aligned}}$$

$$= \frac{1}{2} k^2 \int_0^{\pi/2} \sin^2 \theta \cos \theta d\theta$$

N. o w:

$$\omega_0 \cdot 2\theta = 1 - 2 \sin^2 \theta \quad \rightarrow \quad \sin^2 \theta = \frac{1 - \omega_0^2 \theta}{2}$$

$$\textcircled{B} = \frac{1}{2} \pi^2 \int_0^{\pi/2} (1 - \omega_0^2 \theta) d\theta$$

$$= \frac{1}{4} \pi^2 \int_0^{\pi/2} (1 - \omega_0^2 \theta) d\theta$$

$$= \frac{1}{4} \pi^2 \left[\theta - \frac{1}{2} \omega_0^2 \theta^2 \right] \Big|_0^{\pi/2}$$

$$= \frac{1}{4} \pi^2 \left[\frac{\pi}{2} - \frac{1}{2} (\cancel{\sin(\pi)} - \cancel{\sin 0}) \right] \quad \cancel{\sim}$$

$$= \frac{1}{8} \pi^2 \pi$$

Thus, $H(\pi) = \frac{\pi}{2} \left(1 + \frac{\pi^2}{4} + \dots \right)$

so $P = \frac{4}{\omega_0} H(\pi) = \frac{2\pi}{\omega_0} \left(1 + \frac{\pi^2}{4} + \dots \right)$

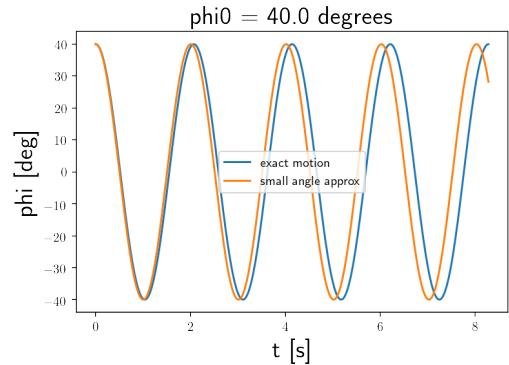
Now: $H = \text{Im} \left(\frac{\phi_0}{z} \right) \approx \frac{\phi_0}{z}$ for $|\phi_0| \ll 1$

thus, $P \approx \frac{2\pi}{\omega_0} \left(1 + \frac{\phi_0^2}{15} \right)$

```

phi0 = 40.0  degrees
small angle  = 2.007089923154493 sec
1st order   = 2.0682293785216155 sec
exact period = 2.069993163286821 sec

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1. Lagrangian mechanics (1-5)

1) Write down the Lagrangian for a simple system in terms of generalized coordinates.

Example:

$$L(x, \dot{x}, t) = \frac{1}{2} m \dot{x}^2 - \frac{1}{2} k x^2$$

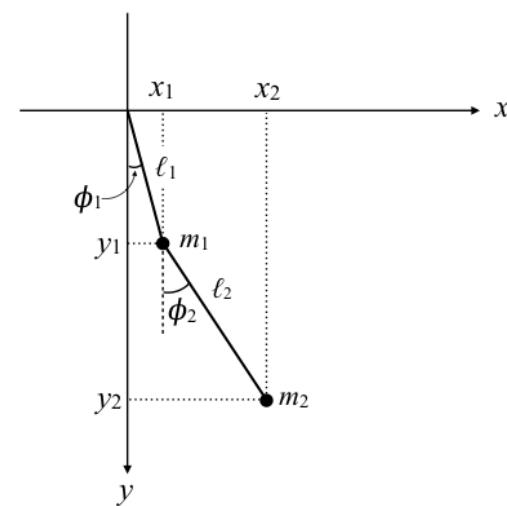
More generally:

$$L(q, \dot{q}, t) = T - U = \frac{1}{2} \sum_{i,k} a_{ik}(q) \dot{q}_i \dot{q}_k - U(q_1, q_2, \dots, q_n, t)$$

for a system of particles in an external field.

2) Distinguish generalized coordinates from Cartesian coordinates.

Example: Double pendulum



Use the two angles ϕ_1, ϕ_2 for the generalized coordinates q_1, q_2 , as opposed to the Cartesian coordinates (x_1, y_1) and (x_2, y_2) , which are subject to constraints imposed by the pendulum rods.

3) Write down Lagrange's equations.

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) = \frac{\partial L}{\partial q_i}, \quad i = 1, 2, \dots, n$$

This is of the form

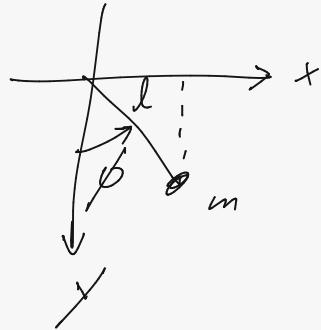
$$\frac{dp_i}{dt} = F_i \quad i = 1, 2, \dots, n$$

where $p_i \equiv \partial L / \partial \dot{q}_i$ and $F_i = -\partial U / \partial q_i$, for the case where the kinetic energy T does not depend explicitly on q .

$$1) \quad L(x, \dot{x}, t) = \frac{1}{2} m \dot{x}^2 - \frac{1}{2} k x^2 \quad (\text{SHO})$$

$$L(\varepsilon, \dot{\varepsilon}, t) = \frac{1}{2} \sum_{i=1}^n (\alpha_i + \beta_i) \dot{\varepsilon}_i^2 - \underbrace{U(\varepsilon_1, \varepsilon_2, \dots, t)}_{\text{external field}}$$

2)



generalized coord: ϕ

Cartesian coords (x, y) — subject to holonomic constraint

$$x^2 + y^2 = l^2$$

solve via: $x = l \sin \phi = x(\phi)$
 $y = l \cos \phi = y(\phi)$

$$3) \quad \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) = \frac{\partial L}{\partial q_i} \iff \ddot{p}_i = -\frac{\partial U}{\partial q_i} \equiv F_i \quad (\text{for } T, \text{ indp of } \varepsilon)$$

$i = 1, 2, \dots, n$ ————— number of DOF

4) Define the action in terms of the Lagrangian, and derive Lagrange's equations starting from the action.

Action:

$$S[q] \equiv \int_{t_1}^{t_2} dt L(q, \dot{q}, t)$$

Lagrange's equations are obtained by setting $\delta S = 0$ for variations δq that vanish at the end points t_1 and t_2 .

The following derivation is for a single degree of freedom. For multiple degrees of freedom, we should vary each $q_i(t)$, $i = 1, 2, \dots, n$ independently.

Derivation:

$$\delta S = \int_{t_1}^{t_2} dt \left[\frac{\partial L}{\partial q} \delta q + \frac{\partial L}{\partial \dot{q}} \delta \dot{q} \right]$$

Integrate the second term by parts using

$$\delta \dot{q} \equiv \delta \left(\frac{dq}{dt} \right) = \frac{d}{dt} \delta q$$

obtaining

```
$$ \delta S = \int_{t_1}^{t_2} dt \left[ \frac{\partial L}{\partial q} \delta q - \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}} \delta q \right) \right]
```

- $\frac{\partial L}{\partial q} \delta q$
- $\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}} \delta q \right)_{t_1}$

The last two terms vanish given the condition that the variations δq vanish at t_1 and t_2 . Since δq is arbitrary, setting $\delta S = 0$ is equivalent to the integrand vanishing:

$$\frac{\partial L}{\partial q} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}} \right) = 0$$

5) Show that Lagrange's equations are unchanged if one adds a total time derivative $df(q, t)/dt$ to L .

Define

$$\bar{L}(q, \dot{q}, t) \equiv L(q, \dot{q}, t) + \frac{df(q, t)}{dt}$$

Then

$$\bar{S}[q] \equiv \int_{t_1}^{t_2} dt \bar{L}(q, \dot{q}, t) = S[q] + f(q, t) \Big|_{t_2} - f(q, t) \Big|_{t_1}$$

From this we see that $\delta \bar{S} = \delta S$, since $\delta q = 0$ at t_1 and t_2 . So the EOMs for L and $\bar{L} \equiv L + df(q, t)/dt$ are the same.

Note: one can obtain the same result by working directly with Lagrange's equations for L and \bar{L} .

$$4) S[\xi] = \int_{t_1}^{t_2} dt L(\xi, \dot{\xi}, t) \quad \leftarrow \text{functional}$$

$\delta S = 0$ (1^{st} order variation)

$$0 = \int_{t_1}^{t_2} dt \left(\frac{\partial L}{\partial \xi} \delta \xi + \frac{\partial L}{\partial \dot{\xi}} \delta \dot{\xi} \right)$$

$$\begin{aligned}\delta \dot{\xi} &= \delta \left(\frac{\partial \xi}{\partial \epsilon} \right) \\ &= \frac{d}{d\epsilon} (\delta \xi)\end{aligned}$$

$$= \int_{t_1}^{t_2} dt \left(\frac{\partial L}{\partial \xi} \delta \xi + \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\xi}} \delta \dot{\xi} \right) - \delta \xi \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\xi}} \right) \right)$$

$$= \left. \frac{\partial L}{\partial \dot{\xi}} \delta \dot{\xi} \right|_{t_1}^{t_2} + \int_{t_1}^{t_2} dt \delta \xi \left(\frac{\partial L}{\partial \xi} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\xi}} \right) \right)$$

For variations fixed at the boundaries ($\delta \xi|_{t_1} = 0, \delta \xi|_{t_2} = 0$) we have

$$0 = \int_{t_1}^{t_2} dt \delta \xi \left(\frac{\partial L}{\partial \xi} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\xi}} \right) \right) \rightarrow \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\xi}} \right) - \frac{\partial L}{\partial \xi} = 0$$

$\forall \delta \xi$

$$5) \text{ Suppose } L \xrightarrow[t_1]{\quad} \bar{L} = L + \frac{d}{dt} f(\underline{z}, t)$$

$$\begin{aligned}\bar{S}[\underline{z}] &= \int_{t_1}^{t_2} dt \bar{L}(\underline{z}, \dot{\underline{z}}, t) \\ &= \int_{t_1}^{t_2} dt \left(L + \frac{d}{dt} f(\underline{z}, t) \right)\end{aligned}$$

$$= S[\underline{z}] + f(\underline{z}, t) \Big|_{t_1}^{t_2}$$

$$\begin{aligned}\delta \bar{S}[\underline{z}] &= \delta S[\underline{z}] + \delta \left[f(z^{(t_2)}, t_2) - f(z^{(t_1)}, t_1) \right] \\ &\in \delta S[\underline{z}]\end{aligned}$$

Since $\underline{z}^{(t_1)}, \underline{z}^{(t_2)}$
are fixed

so Eom are unchanged

c) Holonomic constraints:

$$\varphi_\alpha(q_1, q_2, \dots, q_n; t) = 0, \quad \alpha = 1, 2, \dots, m$$

Define: $\bar{L} = L(q_i, \dot{q}_i, t) + \sum \lambda_\alpha(t) \varphi_\alpha(q_i, t)$

Eoms. $\frac{d}{dt} \left(\frac{\partial \bar{L}}{\partial \dot{q}_i} \right) = \frac{\partial \bar{L}}{\partial q_i} + \sum \lambda_\alpha \frac{\partial \varphi_\alpha}{\partial q_i} \quad (i = 1, 2, \dots, n)$

+ constraint equations $\dot{\varphi}_\alpha = 0 \quad (\alpha = 1, 2, \dots, m)$

are $n+m$ equations for $n+m$ unknowns $q_i(t), \lambda_\alpha(t)$

Non-holonomic constraints:

$$\sum_i c_{\alpha i}(q, t) \dot{q}_i = 0, \quad \alpha = 1, 2, \dots, m$$

L coord differentials, but
can't be integrated

Cannot impose constraints at the level of the Lagrangian,
but instead at the level of Eoms.

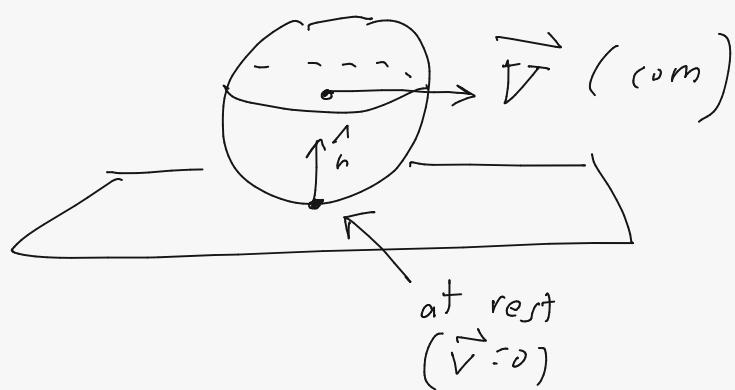
Example:

sphere
rolling
without
slipping
and pivoting
on a
horizontal
surface

Eoms: $\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) = \frac{\partial L}{\partial q_i} + \sum \lambda_\alpha c_{\alpha i} \quad \left. \right\}$

+ constraints: $\sum_i c_{\alpha i} \dot{q}_i = 0$

$n+m$
equations
for $n+m$
unknowns



$$\begin{aligned}\vec{v} &= \vec{V} + \frac{1}{2} \vec{\omega} \times \vec{r} \\ &= \vec{V} - a \frac{1}{2} \vec{\omega} \times \vec{n} \\ \text{so } O &= \vec{V} - a \frac{1}{2} \vec{\omega} \times \vec{n}\end{aligned}$$

$$\downarrow \vec{r} = -a\vec{n}$$

involve
time derivatives,
of \vec{R} and
 $\vec{\phi} = (\phi, \theta, \psi)$
in
Euler angles

7) closed system: no ext. forces (e.g., two bodies interacting gravitationally (central force)). Potential depends only on relative position vectors $\vec{r}_a - \vec{r}_b$

const external field: $\text{Const} \equiv$ no explicit t dependence

$$U = U(\vec{r}_1, \vec{r}_2, \dots, \vec{r}_N), \quad \vec{F}_a = -\frac{\partial U}{\partial \vec{r}_a}$$

uniform external field: $U = - \sum_a \vec{r}_a \cdot \vec{F}_a$ where \vec{F}_a indep. of \vec{r}_a

so $-\frac{\partial U}{\partial \vec{r}_a} = \vec{F}_a$ i.e. e.g., gravity near surface of Earth $U = mgY \rightarrow F_y = -mg$

Thus,

$$E \equiv \sum_i \frac{\partial L}{\partial \dot{q}_i} \dot{q}_i - L = \text{const}$$

This is conservation of energy.

(ii) Space translation symmetry:

$$\mathbf{r}_a \rightarrow \mathbf{r}_a + \delta \mathbf{x}$$

for which

$$L \rightarrow L + \sum_a \frac{\partial L}{\partial \mathbf{r}_a} \cdot \delta \mathbf{x}$$

Then $\delta L = 0$ for all $\delta \mathbf{x}$ implies

$$0 = \sum_a \frac{\partial L}{\partial \mathbf{r}_a} = \sum_a \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\mathbf{r}}_a} \right) = \frac{d}{dt} \left(\sum_a \frac{\partial L}{\partial \dot{\mathbf{r}}_a} \right)$$

where the second equality follows from Lagrange's equations.

Thus,

$$\mathbf{P} \equiv \sum_a \frac{\partial L}{\partial \dot{\mathbf{r}}_a} = \sum_a \mathbf{p}_a = \text{const}$$

This is conservation of total linear momentum.

(iii) Rotational symmetry:

$$\mathbf{r}_a \rightarrow \mathbf{r}_a + \delta \boldsymbol{\phi} \times \mathbf{r}_a, \quad \dot{\mathbf{r}}_a \rightarrow \dot{\mathbf{r}}_a + \delta \boldsymbol{\phi} \times \dot{\mathbf{r}}_a$$

for which

$$L \rightarrow L + \sum_a \left(\frac{\partial L}{\partial \mathbf{r}_a} \cdot (\delta \boldsymbol{\phi} \times \mathbf{r}_a) + \frac{\partial L}{\partial \dot{\mathbf{r}}_a} \cdot (\delta \boldsymbol{\phi} \times \dot{\mathbf{r}}_a) \right) = L + \delta \boldsymbol{\phi} \cdot \sum_a \left(\mathbf{r}_a \times \frac{\partial L}{\partial \mathbf{r}_a} + \dot{\mathbf{r}}_a \times \frac{\partial L}{\partial \dot{\mathbf{r}}_a} \right)$$

Then $\delta L = 0$ for all $\delta \boldsymbol{\phi}$ implies

$$\$ 0 = \sum_a (\delta \boldsymbol{\phi} \cdot \mathbf{r}_a) \frac{\partial L}{\partial \mathbf{r}_a} + \sum_a (\delta \boldsymbol{\phi} \cdot \dot{\mathbf{r}}_a) \frac{\partial L}{\partial \dot{\mathbf{r}}_a}$$

$$+\dot{\mathbf{r}}_a \cdot \mathbf{r}_a \frac{\partial L}{\partial \mathbf{r}_a} + \dot{\mathbf{r}}_a \cdot \mathbf{r}_a \frac{\partial L}{\partial \dot{\mathbf{r}}_a}$$

$$\begin{aligned} & \sum_a \left(\dot{\mathbf{r}}_a \cdot \mathbf{r}_a \frac{\partial L}{\partial \mathbf{r}_a} + \dot{\mathbf{r}}_a \cdot \mathbf{r}_a \frac{\partial L}{\partial \dot{\mathbf{r}}_a} \right) = \sum_a \frac{\partial L}{\partial \mathbf{r}_a} \dot{\mathbf{r}}_a \cdot \mathbf{r}_a + \sum_a \frac{\partial L}{\partial \dot{\mathbf{r}}_a} \dot{\mathbf{r}}_a \cdot \mathbf{r}_a \\ & \frac{\partial L}{\partial \mathbf{r}_a} \dot{\mathbf{r}}_a \cdot \mathbf{r}_a + \frac{\partial L}{\partial \dot{\mathbf{r}}_a} \dot{\mathbf{r}}_a \cdot \mathbf{r}_a = \frac{\partial L}{\partial \mathbf{r}_a} \dot{\mathbf{r}}_a \cdot \mathbf{r}_a + \frac{\partial L}{\partial \dot{\mathbf{r}}_a} \dot{\mathbf{r}}_a \cdot \mathbf{r}_a \end{aligned}$$

where the second equality follows from Lagrange's equations.

Thus,

$$\mathbf{M} \equiv \sum_a \mathbf{r}_a \times \frac{\partial L}{\partial \dot{\mathbf{r}}_a} = \sum_a \mathbf{r}_a \times \mathbf{p}_a = \text{const}$$

This is conservation of total angular momentum.

2) Derive the transformation equations for energy, momentum, and angular momentum from one inertial frame K to another K' .

Consider two inertial frames K and K' , with K' moving with velocity \mathbf{V} wrt K . To simplify the calculations, assume that the origin of the two coordinate systems coincide at the instant under consideration, so that the position vectors \mathbf{r}_a and \mathbf{r}'_a of mass point m_a wrt to the two inertial frames agree.

The velocities \mathbf{v}_a and \mathbf{v}'_a wrt the two frames are related by

$$\mathbf{v}_a = \mathbf{V} + \mathbf{v}'_a$$

Energy:

$$E = \frac{1}{2} \sum_a m_a |\mathbf{v}_a|^2 + U = \frac{1}{2} \sum_a m_a |\mathbf{V} + \mathbf{v}'_a|^2 + U = \frac{1}{2} \sum_a m_a (|\mathbf{V}|^2 + |\mathbf{v}'_a|^2 + 2\mathbf{V} \cdot \mathbf{v}'_a) + U$$

Now

$$\frac{1}{2} \sum_a m_a |\mathbf{V}|^2 = \frac{1}{2} \mu V^2, \quad \frac{1}{2} \sum_a m_a |\mathbf{v}'_a|^2 + U = E', \quad \sum_a m_a \mathbf{V} \cdot \mathbf{v}'_a = \mathbf{V} \cdot \mathbf{P}'$$

where $\mu \equiv \sum_a m_a$ is the total mass, and E' and $\mathbf{P}' \equiv \sum_a m_a \mathbf{v}'_a$ are the energy and the total momentum wrt K' .

Thus

2:

i) Conservation laws
 (a) time translation symmetry: $t \rightarrow t + \delta t$, $\delta = \delta L = \frac{\partial L}{\partial t} \delta t \rightarrow \frac{\partial L}{\partial t} = 0$

$$\begin{aligned} \text{Thus, } \frac{dL}{dt} &= \sum \left(\frac{\partial L}{\partial q_i} \dot{q}_i + \frac{\partial L}{\partial \dot{q}_i} \ddot{q}_i + \cancel{\frac{\partial L}{\partial t}} \right) \\ &= \sum \left[\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) \dot{q}_i + \frac{\partial L}{\partial \dot{q}_i} \ddot{q}_i \right] \\ &= \frac{d}{dt} \left[\sum \frac{\partial L}{\partial \dot{q}_i} \dot{q}_i \right] \end{aligned}$$

so $E = \sum \frac{\partial L}{\partial \dot{q}_i} \dot{q}_i - L$ satisfies $\frac{dE}{dt} = 0$

Note: $E = T + U$ provided $\vec{r}_a = \vec{r}_a(q_1, q_2, \dots, q_n)$ $\vec{r}_i = \vec{r}_i(q_1, q_2, \dots, q_n)$ $\vec{r}_a = \vec{r}_a(\vec{r}_1, \dots, \vec{r}_N)$ $\vec{r}_i = \vec{r}_i(\vec{r}_1, \dots, \vec{r}_N)$ \vec{r}_a no explicit time dependence \vec{r}_i no dependence on \vec{r}_a

$$\begin{aligned} T &= \frac{1}{2} \sum_a m_a |\vec{r}_a|^2 = \frac{1}{2} \sum_a m_a \left\| \sum_i \frac{\partial \vec{r}_a}{\partial q_i} \dot{q}_i \right\|^2 \\ &= \frac{1}{2} \sum_i \sum_a m_a \frac{\partial \vec{r}_a}{\partial q_i} \cdot \frac{\partial \vec{r}_a}{\partial q_i} \dot{q}_i \dot{q}_i \\ &= \frac{1}{2} \sum_{i, k} \alpha_{ik}(q) \dot{q}_i \dot{q}_k \end{aligned}$$

$$\sum_i \frac{\partial T}{\partial \dot{q}_i} \dot{q}_i = \sum_i \left(\sum_k q_{ik} \dot{q}_k \right) \dot{q}_i = 2T$$

Thus, $E = \sum_i \frac{\partial L}{\partial \dot{q}_i} \dot{q}_i - L$

$$= \sum_i \frac{\partial T}{\partial \dot{q}_i} \dot{q}_i - L \quad \left(\text{since } U \text{ does not depend on } \dot{q}_i \right)$$

$$= 2T - L$$

$$= 2T - (T - U)$$

$$= T + U$$

(b) space translation symmetry:

$$0 = \oint L = \sum_a \frac{\partial L}{\partial \dot{r}_a} \cdot \oint \dot{r}_a = \sum_a \frac{\partial L}{\partial \dot{v}_a} \cdot \int \dot{v}_a \quad \text{---}$$

same for all particles

$$= \left(\sum_a \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{v}_a} \right) \right) \cdot \int \dot{v}_a$$

$$= \frac{d}{dt} \left(\sum_a \frac{\partial L}{\partial \dot{v}_a} \right) \cdot \int \dot{v}_a$$

$$= \frac{d}{dt} \left(\sum_a \vec{p}_a \right) \cdot \int \dot{v}_a$$

$$\text{Thus, } \vec{P} = \sum_a \vec{p}_a = \sum_a \frac{\partial L}{\partial \dot{v}_a} = \text{const} \quad \left(\frac{\partial L}{\partial \dot{v}_a} = m \vec{v}_a \right)$$

(so total momentum is conserved)

If $\sum_a \frac{\partial L}{\partial r_a} \cdot \dot{r}_a = 0$ only for \dot{r}_a pointing in a particular \hat{t} direction, then only $\vec{P} \cdot \hat{t} = \text{const}$ (e.g., \dot{r}_x pointing in the x, y directions for a uniform gravitational field in the z -direction)

(c) rotational symmetry ($\dot{\phi}$: rotation about a fixed axis through angle $|\dot{\phi}|$)

$$O = \oint L$$

$$= \sum_a \left(\frac{\partial L}{\partial \dot{r}_a} \cdot \dot{r}_a + \frac{\partial L}{\partial r_a} \cdot \ddot{r}_a \right)$$

$$\begin{aligned} \vec{r}_a &\rightarrow \vec{r}_a + \dot{\phi} \vec{r}_a \times \vec{r}_a \\ \dot{\vec{r}}_a &\rightarrow \dot{\vec{r}}_a + \dot{\phi} \vec{r}_a \times \dot{\vec{r}}_a \end{aligned}$$

$$\begin{aligned} \dot{\vec{r}}_a &= \dot{\phi} \vec{r}_a \times \vec{r}_a \\ \ddot{\vec{r}}_a &= \dot{\phi} \vec{r}_a \times \dot{\vec{r}}_a \end{aligned}$$

$$\text{Thus, } O = \sum_a \left[\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{r}_a} \right) \cdot (\dot{\phi} \vec{r}_a \times \vec{r}_a) + \frac{\partial L}{\partial \vec{r}_a} \cdot (\dot{\phi} \vec{r}_a \times \dot{\vec{r}}_a) \right]$$

" " "

$$\vec{P}_a$$

$$\begin{aligned}
 0 &= \sum_a \left[\frac{d\vec{p}_a}{dt} \cdot (\vec{\delta\phi} \times \vec{r}_a) + \vec{p}_a \cdot (\vec{\delta\phi} \times \dot{\vec{r}}_a) \right] \\
 &= \sum_a \left[\vec{\delta\phi} \cdot \left(\vec{r}_a \times \frac{d\vec{p}_a}{dt} \right) + \vec{\delta\phi} \cdot \left(\dot{\vec{r}}_a \times \vec{p}_a \right) \right] \\
 &= \vec{\delta\phi} \cdot \left(\sum_a \left(\vec{r}_a \times \frac{d\vec{p}_a}{dt} + \dot{\vec{r}}_a \times \vec{p}_a \right) \right) \\
 &= \vec{\delta\phi} \cdot \frac{d}{dt} \left(\sum_a \vec{r}_a \times \vec{p}_a \right)
 \end{aligned}$$

so $\overline{\vec{M}} = \sum_a \vec{r}_a \times \vec{p}_a = \text{const}$

(total angular momentum)

If $\vec{\delta\phi} \cdot \frac{d\vec{M}}{dt} = 0$ only for certain axial directions, if
 then only the component $\vec{M} \cdot \hat{n} = \text{const}$ (e.g.,
 symmetry around the axis of a cylinder)



\exists) H : inertial frame

H' : another inertial frame, moving wrt H with velocity \vec{V}



(assume origins coincide at instant considered
so $\vec{r}_a = \vec{r}'_a$)

H

$$\begin{aligned}\vec{v}_a &= \vec{v}'_a + \vec{V} && \text{subjected}\\ E &= \frac{1}{2} \sum_a m_a |\vec{v}_a|^2 + U(\vec{r}_1, \vec{r}_2, \dots, t) && \text{by } H \rightarrow H' \\ &= \frac{1}{2} \sum_a m_a |\vec{v}'_a + \vec{V}|^2 + U \\ &= \frac{1}{2} \sum_a m_a \left(|\vec{v}'_a|^2 + |\vec{V}|^2 + 2 \vec{v}'_a \cdot \vec{V} \right) + U \\ &= E' + \frac{1}{2} \sum_a m_a |\vec{V}|^2 + \left(\sum_a m_a \vec{v}'_a \right) \cdot \vec{V} + U \\ &= E' + \frac{1}{2} \mu |\vec{V}|^2 + \vec{P}' \cdot \vec{V}\end{aligned}$$

$$\begin{aligned}
 \overrightarrow{P} &= \sum_a m_a \overrightarrow{v}_a \\
 &= \sum_a m_a (\overrightarrow{V} + \overrightarrow{v}_a') \\
 &= \mu \overrightarrow{V} + \overrightarrow{P}'
 \end{aligned}$$

$$\begin{aligned}
 \overrightarrow{M} &= \sum_a m_a \overrightarrow{r}_a \times \overrightarrow{v}_a \\
 &= \sum_a m_a \overrightarrow{r}_a' \times (\overrightarrow{V} + \overrightarrow{v}_a') \\
 &= \left(\sum_a m_a \overrightarrow{r}_a' \right) \times \overrightarrow{V} + \sum_a m_a \overrightarrow{r}_a' \times \overrightarrow{v}_a' \\
 &= \mu \overrightarrow{R} \times \overrightarrow{V} + \overrightarrow{M}' \quad \text{where } \overrightarrow{R} = \text{com position vector}
 \end{aligned}$$

Ther,

$$\begin{aligned}
 E &= E' + \frac{1}{2} \mu V^2 + \overrightarrow{p}' \cdot \overrightarrow{V} \\
 \overrightarrow{p} &= \overrightarrow{p}' + \mu \overrightarrow{V} \\
 \overrightarrow{M} &= \overrightarrow{M}' + \mu \overrightarrow{R} \times \overrightarrow{V}
 \end{aligned}$$

$$E = E' + \frac{1}{2}\mu V^2 + \mathbf{P}' \cdot \mathbf{V}$$

Momentum:

$$\mathbf{P} = \sum_a m_a \mathbf{v}_a = \sum_a m_a (\mathbf{V} + \mathbf{v}'_a) = \mu \mathbf{V} + \mathbf{P}'$$

Angular momentum:

$$\mathbf{M} = \sum_a \mathbf{r}_a \times \mathbf{p}_a = \sum_a m_a \mathbf{r}_a \times \mathbf{v}_a = \sum_a m_a \mathbf{r}_a \times (\mathbf{V} + \mathbf{v}'_a) = \left(\sum_a m_a \mathbf{r}_a \right) \times \mathbf{V} + \sum_a \mathbf{r}'_a \times \mathbf{p}'_a = \mu \mathbf{R} \times$$

where $\mathbf{R} \equiv \sum_a m_a \mathbf{r}_a / \mu$ is the position vector of the COM wrt K .

In summary:

$$E = E' + \frac{1}{2}\mu V^2 + \mathbf{P}' \cdot \mathbf{V}, \quad \mathbf{P} = \mathbf{P}' + \mu \mathbf{V}, \quad \mathbf{M} = \mathbf{M}' + \mu \mathbf{R} \times \mathbf{V}$$

3) Write down the general expression for the energy function E .

$$E \equiv \sum_i \frac{\partial L}{\partial \dot{q}_i} \dot{q}_i - L(q, \dot{q}, t)$$

4) Explain what it means for a function to be homogeneous of degree k .

A function $f(x_1, x_2, \dots, x_n)$ is homogeneous of degree k if

$$f(\alpha x_1, \alpha x_2, \dots, \alpha x_n) = \alpha^k f(x_1, x_2, \dots, x_n)$$

For such a function

$$\sum_i \frac{\partial f}{\partial x_i} x_i = k f(x_1, x_2, \dots, x_n)$$

which can be proved by differentiating both sides of the first equation with respect to α , and then evaluating at $\alpha = 1$.

Example: the kinetic energy

$$T = \frac{1}{2} \sum_{ik} a_{ik}(q) \dot{q}_i \dot{q}_k$$

is homogeneous of degree 2 in the generalized velocities \dot{q}_i , so that

$$\sum_i \frac{\partial T}{\partial \dot{q}_i} \dot{q}_i = 2T$$

5) Write down the expression for the generalized momentum p_i .

$$p_i \equiv \frac{\partial L}{\partial \dot{q}_i}, \quad i = 1, 2, \dots, n$$

6) Write down the expression for the center of mass (COM) of a system of particles.

$$\mathbf{R}_a = \frac{\sum_a m_a \mathbf{r}_a}{\sum_b m_b}$$

7) Write down the virial theorem for a system whose motion takes place in a finite region of space and whose potential energy is a homogeneous function of degree k in the coordinates.

3) Energy function

$$E = \sum_i \frac{\partial L}{\partial \dot{q}_i} \dot{q}_i - L(q, \dot{q}, t) \quad \text{--- function of } q, \dot{q}, t$$

in general

4) $f(x_1, x_2, \dots, x_n)$ is homog of degree κ if

$$f(\alpha x_1, \alpha x_2, \dots, \alpha x_n) = \alpha^\kappa f(x_1, x_2, \dots, x_n)$$

$$\underline{\text{Ex:}} \quad U = mgx \rightarrow \kappa = 1$$

$$U = \frac{1}{2} kx^2 \rightarrow \kappa = 2$$

$$U = -\frac{\alpha}{r} \rightarrow \kappa = -1$$

$$\text{For such a function} \quad \sum_i \frac{\partial f}{\partial x_i} x_i = \kappa f(x_1, x_2, \dots, x_n)$$

$$[\text{e.g., } T = \frac{1}{2} m \dot{x}^2 \text{ is homog of degree 2 in } \dot{x} \text{ so that } \sum_i \frac{\partial T}{\partial \dot{x}_i} \dot{x}_i = 2T]$$

Proof: Differentiate $f(\alpha x_1, \alpha x_2, \dots, \alpha x_n) = \alpha^\kappa f(x_1, x_2, \dots, x_n)$ w.r.t α

$$\text{LHS} = \frac{d}{d\alpha} f(\alpha x_1, \alpha x_2, \dots, \alpha x_n) = \sum_i \frac{\partial f}{\partial x_i} (\alpha x_1, \dots, \alpha x_n) x_i$$

$$\text{RHS} = \frac{d}{d\alpha} [\alpha^\kappa f(x_1, x_2, \dots, x_n)] = \kappa \alpha^{\kappa-1} f(x_1, \dots, x_n)$$

$$\text{Evaluate both sides at } \alpha=1 \rightarrow \kappa f(x_1, \dots, x_n) = \sum_i \frac{\partial f}{\partial x_i} x_i$$

5) Generalized momenta:

$$p_i \equiv \frac{\partial L}{\partial \dot{q}_i} \quad i = 1, 2, \dots, s \quad (\# \text{ of DOF})$$

6) COM of a system of particles

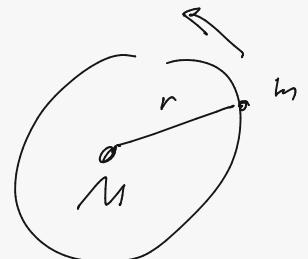
$$\vec{R} = \sum_a m_a \vec{r}_a \neq \sum_b m_b$$

7) Virial Theorem:

Consider circular orbit in Newtonian gravity

$$\frac{mv^2}{r} = \frac{GMm}{r^2} \rightarrow \frac{1}{2}mv^2 = \frac{1}{2} \frac{GMm}{r}$$

$$T = -\frac{1}{2} U \quad (T = -1 \text{ for } U \propto \frac{1}{r})$$



More generally: $2 \langle T \rangle = H \langle U \rangle$ where $\langle \rangle$ means time average

Proof: Assume U is homog of degree H .

Then

$$\sum_a \frac{\partial U}{\partial \vec{r}_a} \cdot \vec{r}_a = H U$$

Average over an orbit (assumed bound) :

$$RHS = \tau \langle U \rangle \quad \text{where} \quad \langle f \rangle \equiv \lim_{\tau \rightarrow \infty} \frac{1}{\tau} \int_0^\tau dt f(t)$$

Now:

$$\begin{aligned} \sum_a \frac{\partial U}{\partial r_a} \cdot \vec{r}_a &= \sum_a -\frac{\partial L}{\partial p_a} \cdot \vec{r}_a \\ &= -\sum_a \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{r}_a} \right) \cdot \vec{r}_a \\ &= -\sum_a \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{r}_a} \cdot \vec{r}_a \right) + \sum_a \frac{\partial L}{\partial \dot{r}_a} \cdot \frac{d \vec{r}_a}{dt} \\ &= -\frac{d}{dt} \left(\sum_a \vec{p}_a \cdot \vec{r}_a \right) + 2T \end{aligned}$$

so

$$\text{LHS} = 2 \langle T \rangle - \left\langle \frac{d}{dt} \left(\sum_a \vec{p}_a \cdot \vec{r}_a \right) \right\rangle$$

$$= 2 \langle T \rangle - \lim_{\tau \rightarrow \infty} \frac{1}{\tau} \left(\sum_a \vec{p}_a \cdot \vec{r}_a \right) \Big|_0^\tau$$

$$\boxed{2 \langle T \rangle = \tau \langle U \rangle}$$

$\boxed{2 \langle T \rangle = \tau \langle U \rangle}$

$= 0$ if bounded motion
 $\sum_a \vec{r}_a, \vec{p}_a$ are finite

Recall that the virial theorem relates the time-averaged KE to the time-averaged potential energy.

For Newtonian gravity, with a mass m in circular orbit of radius r about a fixed mass M :

$$\frac{GMm}{r^2} = \frac{mv^2}{r}$$

which implies

$$U = -\frac{GMm}{r} = -mv^2 = -2T$$

More generally, for a potential that is homogeneous of degree k :

$$k\langle U \rangle = 2\langle T \rangle$$

where angle bracket means time average:

$$\langle f \rangle \equiv \lim_{\tau \rightarrow \infty} \frac{1}{\tau} \int_0^\tau dt f(t)$$

For Newtonian gravity, the potential $U = -GMm/r$ is homogeneous of degree $k = -1$.

Proof:

If U is homogeneous of degree k , then

$$\sum_a \frac{\partial U}{\partial \mathbf{r}_a} \cdot \mathbf{r}_a = kU$$

The LHS of the above equation can be written as

$$\begin{aligned} \$\$ \sum_a \frac{\partial U}{\partial \mathbf{r}_a} \cdot \mathbf{r}_a &= -\sum_a \dot{\mathbf{r}}_a \cdot \nabla U \\ &= -\sum_a \dot{\mathbf{r}}_a \cdot \nabla \left(\frac{1}{2} \mathbf{p}_a^2 - U \right) \end{aligned}$$

- $\sum_a \dot{\mathbf{r}}_a \cdot \nabla \left(\frac{1}{2} \mathbf{p}_a^2 - U \right)$

where the first equality follows from Lagrange's equations and the second equality follows from the product rule.

Thus,

$$\$\$ \mathbf{k} \cdot \mathbf{U} = -\frac{d}{dt} \left(\sum_a \mathbf{p}_a \cdot \mathbf{r}_a \right)$$

- $\sum_a \mathbf{p}_a \cdot \dot{\mathbf{r}}_a$

The last term equals twice the kinetic energy T since $\mathbf{p}_a = m_a \dot{\mathbf{r}}_a$, and the first term vanishes if we take the time average, assuming that the motion is bounded (i.e., finite velocities and finite distances). Thus,

$$k\langle U \rangle = 2\langle T \rangle$$

3. Hamiltonian mechanics (40)

1) Write down the Hamiltonian $H(p, q, t)$ for a simple system starting from a Lagrangian $L(q, \dot{q}, t)$.

General relationship:

$$H(p, q, t) = \sum_i p_i \dot{q}_i - L(q, \dot{q}, t)$$

where on the RHS all of the \dot{q}_i are expressed in terms of q_i , p_i , and t .

1-d example:

$$L(x, \dot{x}, t) = \frac{1}{2} m \dot{x}^2 - U(x)$$

has

$$p \equiv \frac{\partial L}{\partial \dot{x}} = m \dot{x} \quad \Leftrightarrow \quad \dot{x} = \frac{p}{m}$$

leading to

$$H(p, x, t) = \frac{p^2}{2m} + U(x)$$

2) Write down Hamilton's equations for p_i and q_i .

EOMs:

$$\dot{q}_i = \frac{\partial H}{\partial p_i}, \quad \dot{p}_i = -\frac{\partial H}{\partial q_i}, \quad i = 1, 2, \dots, n$$

3. Hamiltonian mechanics

$$1) \quad H(p, q, t) = \left(\sum_i p_i \dot{q}_i - L(q, \dot{q}, t) \right) \Big|_{\dot{q} = \dot{q}(q, p, t)}$$

where $p_i = \frac{\partial L}{\partial \dot{q}_i}$ are the generalized momenta

Example: $L = \frac{1}{2} m \dot{x}^2 - U(x)$

$$p = \frac{\partial L}{\partial \dot{x}} = m \dot{x} \rightarrow \dot{x} = \frac{p}{m}$$

$$H = \left(p \dot{x} - \left(\frac{1}{2} m \dot{x}^2 - U(x) \right) \right) \Big|_{\dot{x} = \frac{p}{m}}$$

$$= \frac{p^2}{2m} - \frac{1}{2} m \left(\frac{p}{m} \right)^2 + U(x)$$

$$= \frac{p^2}{2m} + U(x)$$

2) Hamilton's equations:

$$\dot{q}_i = \frac{\partial H}{\partial p_i}, \quad \dot{p}_i = -\frac{\partial H}{\partial q_i}, \quad i = 1, 2, \dots, s$$

$\underbrace{\hspace{10em}}$
2s 1st order equations.

3) Explain the fundamental difference between Hamilton's equations and Lagrange's equations.

Hamilton's equations are $2n$ first-order differential equations for q_i, p_i , while Lagrange's equationis are n second-order equations for q_i .

4) Show the equivalence of Hamilton's equations and Lagrange's equation for simple systems.

For the above 1-d Lagrangian and Hamiltonian we have:

Lagrange's equation:

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}} \right) = \frac{\partial L}{\partial x} \quad \Rightarrow \quad m\ddot{x} = -\frac{dU}{dx}$$

Hamilton's equations:

$$\dot{x} = \frac{\partial H}{\partial p} = \frac{p}{m}, \quad \dot{p} = -\frac{\partial H}{\partial x} = -\frac{dU}{dx}$$

Solving the first of Hamilton's equations for p , and then substituting this solution into the second equation yields:

$$m\ddot{x} = -\frac{dU}{dx}$$

which is the same as Lagrange's equation.

4. Central force motion (11, 13-15)

1) Write down an integral expression for t in terms of x for 1-d motion in a constant external field $U(x)$.

Conservation of energy:

$$\frac{1}{2}m\dot{x}^2 + U(x) = E$$

where E is a constant. This is a separable differential equation with

$$t = \int \frac{dx}{\sqrt{\frac{2}{m}(E - U(x))}} + \text{const}$$

2) Determine the allowed values of the energy and turning points for 1-d motion in a constant external field.

Allowed values of the energy:

$$E \geq U_{\min}$$

since kinetic energy is positive.

Turning points are solutions to the equation $E - U(x) = 0$.

3) Hamilton's equation: \dot{q}_i is 1st order DE for (q_i, p_i) , $i=1, 2, \dots, r$
 Lagrange's equation: \ddot{x} is 2nd order DE for q_i , $i=1, 2, \dots, r$

4) Consider $L = \frac{1}{2}m\dot{x}^2 - U(x)$, $H = \frac{p^2}{2m} + U(x)$

$$\text{Lagrange's equations: } \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}} \right) = \frac{\partial L}{\partial x}$$

$$\frac{d}{dt} (m\dot{x}) = -\frac{\partial U}{\partial x}$$

$$m\ddot{x} = -\frac{\partial U}{\partial x}$$

Hamilton's equations:

$$\dot{x} = \frac{\partial H}{\partial p} = \frac{p}{m} \Rightarrow p = m\dot{x}$$

$$\dot{p} = -\frac{\partial H}{\partial x} = -\frac{\partial U}{\partial x} \Rightarrow (m\dot{x})' = -\frac{\partial U}{\partial x}$$

$$m\ddot{x} = -\frac{\partial U}{\partial x}$$

same

(4) Central motion

1) $U = U(x)$, 1-d motion

$$L = \frac{1}{2}m\dot{x}^2 - U(x)$$

No explicit t dependence \Rightarrow

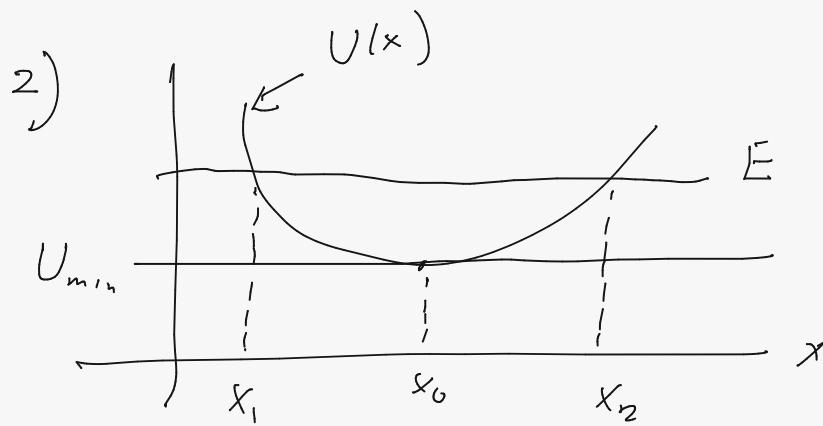
$$E = \frac{\partial L}{\partial \dot{x}} \dot{x} - L = T + U = \text{const}$$

$$E = \frac{1}{2}m\dot{x}^2 + U(x)$$

$$\pm \sqrt{\frac{2}{m}(E - U(x))} = \dot{x} = \frac{dx}{dt}$$

thus, $\pm \int \frac{dx}{\sqrt{\frac{2}{m}(E - U(x))}} = \int dt = t + \text{const}$

(This gives, $t = t(x)$ which can be inverted to get $x = x(t)$)



Need $E \geq U_{\min} = U(x_0)$

since $E - U = T = \frac{1}{2}m\dot{x}^2 \geq 0$

Turning points where $E = U(x)$

In figure to left

$x = x_1, x_2$ are turning points
Since $U(x_1) = U(x_2) = E$

3) Transform the problem of two interacting particles into an effective one-body problem by working in the COM frame.

Lagrangian for two interacting particles:

$$L = T - U = \frac{1}{2}m_1|\dot{\mathbf{r}}_1|^2 + \frac{1}{2}m_2|\dot{\mathbf{r}}_2|^2 - U(\mathbf{r}_1 - \mathbf{r}_2)$$

Total momentum is conserved since L is unchanged by a spatial translation $\mathbf{r}_a \rightarrow \mathbf{r}_a + \delta\mathbf{x}$. Thus, we can work in the COM frame where the COM is the origin of coordinates:

$$m_1\mathbf{r}_1 + m_2\mathbf{r}_2 = 0$$

In terms of the relative separation vector

$$\mathbf{r} \equiv \mathbf{r}_1 - \mathbf{r}_2$$

we have

$$\mathbf{r}_1 = \frac{m_2}{m_1 + m_2}\mathbf{r}, \quad \mathbf{r}_2 = -\frac{m_1}{m_1 + m_2}\mathbf{r}$$

The kinetic energy becomes

$$T = \frac{1}{2}m|\dot{\mathbf{r}}|^2$$

where

$$m \equiv \frac{m_1 m_2}{m_1 + m_2}$$

is the reduced mass. Thus,

$$L = \frac{1}{2}m|\dot{\mathbf{r}}|^2 - U(\mathbf{r})$$

4) Show that both energy and angular momentum are conserved for a central potential.

For a central potential, U depends only on the magnitude of the relative separation vector

$$U = U(|\mathbf{r}_1 - \mathbf{r}_2|) = U(r)$$

Energy

$$E = \frac{\partial L}{\partial \dot{\mathbf{r}}} \cdot \dot{\mathbf{r}} - L = \frac{1}{2}m|\dot{\mathbf{r}}|^2 + U(r)$$

is conserved since the Lagrangian does not depend explicitly on time.

Angular momentum

$$\mathbf{M} = \mathbf{r} \times \mathbf{p} = m\mathbf{r} \times \dot{\mathbf{r}}$$

is conserved since the Lagrangian is unchanged by a rotation

$$\mathbf{r} \rightarrow \mathbf{r} + \delta\phi \times \mathbf{r}, \quad \dot{\mathbf{r}} \rightarrow \dot{\mathbf{r}} + \delta\phi \times \dot{\mathbf{r}}$$

Since \mathbf{M} is conserved, we can choose the orientation of our COM frame such that \mathbf{M} points along the z -axis. Then the motion is in the xy -plane and we can write the Lagrangian in terms of plane-polar coordinates (r, ϕ) and their time derivatives:

$$L = \frac{1}{2}m\left(\dot{r}^2 + r^2\dot{\phi}^2\right) - U(r)$$

Conservation of angular momentum then manifests itself as conservation of

$$p_\phi \equiv \frac{\partial L}{\partial \dot{\phi}}$$

since L does not depend explicitly on ϕ . Taking the derivative, we have

$$p_\phi = mr^2\dot{\phi} \equiv \ell = \text{const}$$

or, equivalently,

$$\dot{\phi} = \frac{\ell}{mr^2}$$

NOTE: Landau and Lifshitz use M instead of ℓ for the magnitude of the angular momentum. I prefer ℓ since M can be confused with the total mass $m_1 + m_2$.

3) Two interacting bodies

$$U = U(\vec{r}_1, \vec{r}_2) = U(\vec{r}_1 - \vec{r}_2) = U(\vec{r}) \text{ where } \vec{r} \equiv \vec{r}_1 - \vec{r}_2$$

$$L = \frac{1}{2} m_1 |\dot{\vec{r}}_1|^2 + \frac{1}{2} m_2 |\dot{\vec{r}}_2|^2 - U(\vec{r}_1 - \vec{r}_2)$$

$\oint L = 0$ for $\vec{r}_a \rightarrow \vec{r}_a + \vec{\delta x} \rightarrow$ total momentum conserved

$$\vec{P} = m_1 \vec{v}_1 + m_2 \vec{v}_2 = \text{const}$$

choose Com frame where $\vec{R} = \frac{m_1 \vec{r}_1 + m_2 \vec{r}_2}{m_1 + m_2} = 0$

This is an inertial frame since $\vec{P}_{\text{com}} = \text{const}$

Given: $m_1 \vec{v}_1 + m_2 \vec{v}_2 = 0$
 $\vec{r}_1 - \vec{r}_2 \equiv \vec{r}$

Find: $(m_1 + m_2) \vec{r}_1 = m_2 \vec{r} \rightarrow \vec{r}_1 = \frac{m_2}{m_1 + m_2} \vec{r}$
 $(m_2 + m_1) \vec{r}_2 = -m_1 \vec{r} \rightarrow \vec{r}_2 = \frac{-m_1}{m_1 + m_2} \vec{r}$

Thus, $|\dot{\vec{r}}_1|^2 = \left(\frac{m_2}{m_1 + m_2} \right)^2 |\dot{\vec{r}}|^2, \quad |\dot{\vec{r}}_2|^2 = \left(\frac{-m_1}{m_1 + m_2} \right)^2 |\dot{\vec{r}}|^2$

$$\begin{aligned}
T &= \frac{1}{2} m_1 |\dot{\vec{r}}_1|^2 + \frac{1}{2} m_2 |\dot{\vec{r}}_2|^2 \\
&= \frac{1}{2} \frac{|\dot{\vec{r}}|^2}{(m_1 + m_2)^2} \left[m_1 m_2^2 \rightarrow m_2 m_1^2 \right] \\
&= \frac{1}{2} \frac{|\dot{\vec{r}}|^2}{(m_1 + m_2)} m_1 m_2 \cancel{(m_1 + m_2)} \\
&= \frac{1}{2} \left(\frac{m_1 m_2}{m_1 + m_2} \right) |\dot{\vec{r}}|^2 \\
&= \frac{1}{2} m |\dot{\vec{r}}|^2 \quad \text{where } m \equiv \frac{m_1 m_2}{m_1 + m_2} \quad (\text{reduced mass})
\end{aligned}$$

Thus,

$$\begin{aligned}
L &= T - U(\vec{r}) \\
&= \frac{1}{2} m |\dot{\vec{r}}|^2 - U(\vec{r})
\end{aligned}$$

so instead of depending on $\vec{r}_1, \vec{r}_2, \dot{\vec{r}}_1, \dot{\vec{r}}_2$, the Lagrangian depends only on $\vec{r}, \dot{\vec{r}}$ where $\vec{r} = \vec{r}_1 - \vec{r}_2$.

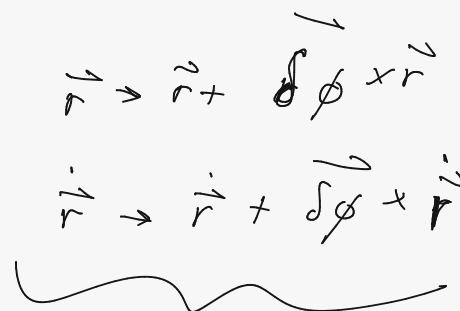
$$4) \text{ Central potential: } U(\vec{r}_1, \vec{r}_2) = U(|\vec{r}_1 - \vec{r}_2|) = U(r)$$

$$L = \frac{1}{2} m |\dot{\vec{r}}|^2 - U(r)$$

$$\delta L = 0 \quad \text{for} \quad t \rightarrow t + \delta t$$



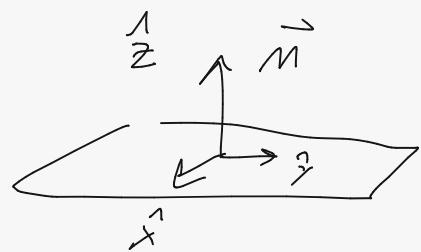
time translation



rotation

Thus, E and $\vec{M} = \vec{r} \times \vec{p} = m \vec{r} \times \vec{v}$ are constant.

Choose coord system so that \vec{M} points along \hat{z}



Then motion takes place in xy -plane

$$\vec{r} = (r, \phi) \quad \text{--- plane polar coords.}$$

$$= x \hat{x} + y \hat{y} \quad \begin{pmatrix} x = r \cos \phi \\ y = r \sin \phi \end{pmatrix}$$

$$\text{with } M_z = \text{const} +$$

$$M_z = p_\phi = \frac{\partial L}{\partial \dot{\phi}} = mr^2 \dot{\phi} \quad \left(L = \frac{1}{2} m (r^2 + r^2 \dot{\phi}^2) - U(r) \right)$$

To show $M_z = p\phi$ ($\vec{M} = \vec{F} \times \vec{p}$) $x = r \cos \phi, y = r \sin \phi$

Proof: $M_z = x \dot{p}_y - y \dot{p}_x$ $\rightarrow x = r \cos \phi - r \sin \phi \dot{\phi}$
 $= r \cos \phi m(r \sin \phi + r \cos \phi \dot{\phi})$ $y = r \sin \phi + r \cos \phi \dot{\phi}$
 $- r \sin \phi m(r \cos \phi - r \sin \phi \dot{\phi})$
 ↙
 cancel
 $= mr^2 \dot{\phi} (\cos^2 \phi + \sin^2 \phi)$
 $= mr^2 \dot{\phi}$



5) Write down an expression for the effective potential $U_{\text{eff}}(r)$ in terms of $U(r)$ and ℓ .

Energy:

$$E = \frac{1}{2}m(\dot{r}^2 + r^2\dot{\phi}^2) + U(r) = \frac{1}{2}m\dot{r}^2 + \frac{\ell^2}{2mr^2} + U(r) = \frac{1}{2}m\dot{r}^2 + U_{\text{eff}}(r)$$

with

$$U_{\text{eff}}(r) = U(r) + \frac{\ell^2}{2mr^2}$$

6) Plot the effective potential for some simple central force potentials.

The code below produces plots for the following potentials:

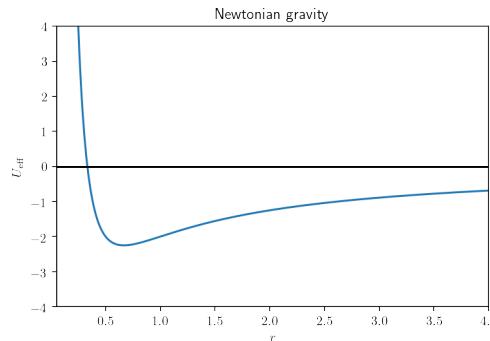
- Newtonian gravity: $U = -\alpha/r$
- 3d harmonic oscillator: $U = \alpha r^2$
- General relativity: $U = -\alpha/r - \beta/r^3$

```
In [8]: # Newtonian gravity (Kepler's problem) effective potential
eps = 1e-4
r = np.linspace(eps, 5, 1000)

U = -3./r
Ueff = U + 1./r**2

plt.figure()
plt.plot(r, Ueff)
plt.axhline(y=0, color='k')
plt.xlim((0.05, 4))
plt.ylim((-4,4))
plt.xlabel('$r$')
plt.ylabel('$U_{\text{eff}}$')
plt.title('Newtonian gravity')
# plt.savefig('newtonian_gravity')
```

Out[8]: Text(0.5, 1.0, 'Newtonian gravity')



5) Effective potential:

$$E = \frac{1}{2} m (\dot{r}^2 + r^2 \dot{\phi}^2) + U(r)$$

$$= \frac{1}{2} m \left(\dot{r}^2 + r^2 \frac{M_z^2}{m^2 r^4} \right) + U(r)$$

$$= \frac{1}{2} m \dot{r}^2 + \left(U(r) + \frac{M_z^2}{2 m r^2} \right)$$

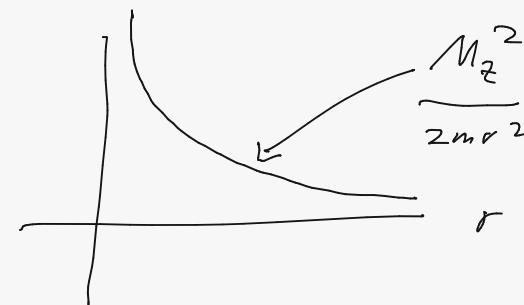
$$= \frac{1}{2} m \dot{r}^2 + U_{\text{eff}}(r)$$

$$\begin{cases} M_z = m r^2 \dot{\phi} \\ \dot{\phi} = \frac{M_z}{m r^2} \end{cases}$$

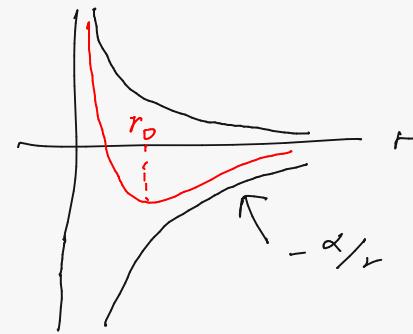
$$U(r) = -\frac{\alpha}{r}, \quad U(r) = \alpha r^2, \quad U(r) = -\frac{\alpha}{r} - \frac{\beta}{r^3}$$

\underbrace{\hspace{10em}}_{\text{Newtonian gravity}} \quad \underbrace{\hspace{10em}}_{\text{Simple oscillator}} \quad \underbrace{\hspace{10em}}_{\text{GR}}

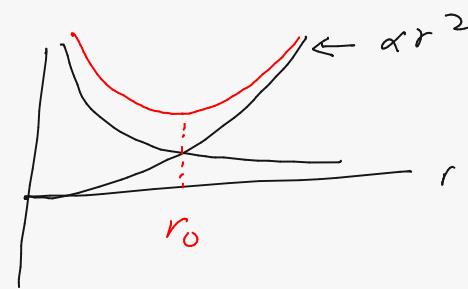
$$U_{\text{eff}}(r) = \frac{M_z^2}{2 m r^2} + U(r)$$



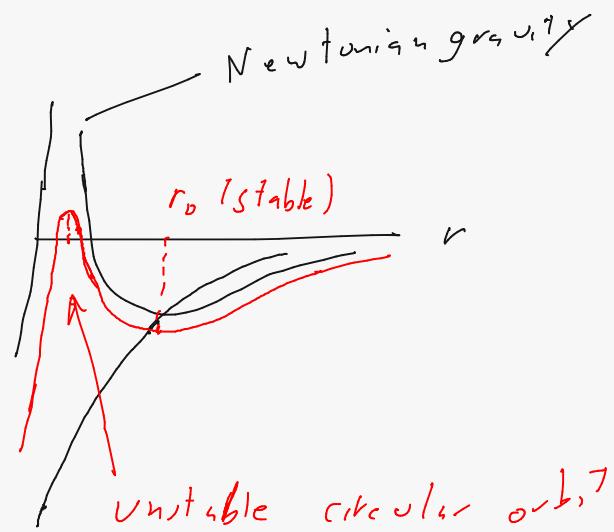
$$U_{\text{eff}}(r) = \frac{M_z^2}{2mv^2} - \frac{\alpha}{r}$$



$$U_{\text{eff}}(r) = \frac{M_z^2}{2mv^2} + \alpha r^2$$



$$U_{\text{eff}}(r) = \frac{M_z^2}{2mv^2} - \frac{\alpha}{r} - \frac{\beta}{r^3}$$

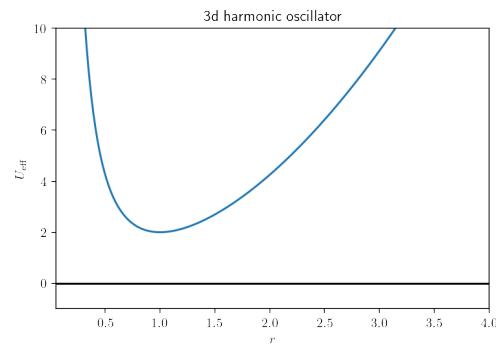


```
In [9]: # 3d harmonic oscillator effective potential
eps = 1e-4
r = np.linspace(eps, 5, 1000)

U = r**2
Ueff = U + 1./r**2

plt.figure()
plt.plot(r, Ueff)
plt.axhline(y=0, color='k')
plt.xlim((0.05, 4))
plt.ylim((-1,10))
plt.xlabel('$r$')
plt.ylabel('$U_{\text{eff}}$')
plt.title('3d harmonic oscillator')
#plt.savefig('3d_harmonic_oscillator')
```

Out[9]: Text(0.5, 1.0, '3d harmonic oscillator')

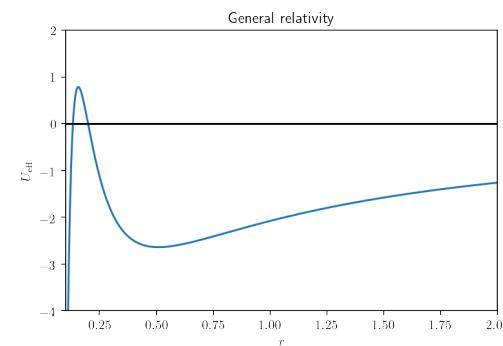


```
In [10]: # GR effective potential
eps = 1e-4
r = np.linspace(eps, 5, 1000)

U1 = -3./r
U2 = -0.08/r**3
Ueff = U1 + U2 + 1./r**2

plt.figure()
plt.plot(r, Ueff)
plt.axhline(y=0, color='k')
plt.xlim((0.1, 2))
plt.ylim((-4,2))
plt.xlabel('$r$')
plt.ylabel('$U_{\text{eff}}$')
plt.title('General relativity')
#plt.savefig('general_relativity')
```

Out[10]: Text(0.5, 1.0, 'General relativity')



7) From the graph of the effective potential, determine the different types of allowed motion.

Different values of the energy E determine the different types of allowed motion.

Example: Newtonian gravity ($U = -\alpha/r$)

- $E < U_{\text{eff,min}}$: not allowed
- $E = U_{\text{eff,min}}$: stable circular orbit
- $U_{\text{eff,min}} < E < 0$: bound (elliptical) orbit
- $E = 0$: (parabolic) scattering orbit
- $E > 0$: (hyperbolic) scattering orbit

For more general potentials, the bound and scattering orbits need not be conic sections.

8) Write down integral expressions for t and ϕ in terms of r for a general central potential.

Start with the energy equation written in the form:

$$E = \frac{1}{2}mr^2 + \frac{\ell^2}{2mr^2} + U(r)$$

This is a separable equation for $r(t)$, which can be solved for t as

$$t = \int \frac{dr}{\sqrt{\frac{2}{m}(E - U(r)) - \frac{\ell^2}{m^2r^2}}} + \text{const}$$

To obtain an integral expression for ϕ in terms of r , use the conservation of angular momentum equation

$$\ell = mr^2\dot{\phi}$$

which implies

$$dt = \frac{mr^2}{\ell} d\phi$$

This leads to separable equation for $r(\phi)$, which can be solved for ϕ as

$$\phi = \int \frac{\ell dr/r^2}{\sqrt{2m(E - U(r)) - \frac{\ell^2}{r^2}}} + \text{const}$$

9) Evaluate these two integrals for Kepler's problem for bound orbits, using appropriate trig substitutions

Kepler's problem: $U(r) = -\alpha/r$ where $\alpha = GMm > 0$ with $M \equiv m_1 + m_2$ denoting the total mass of the system.

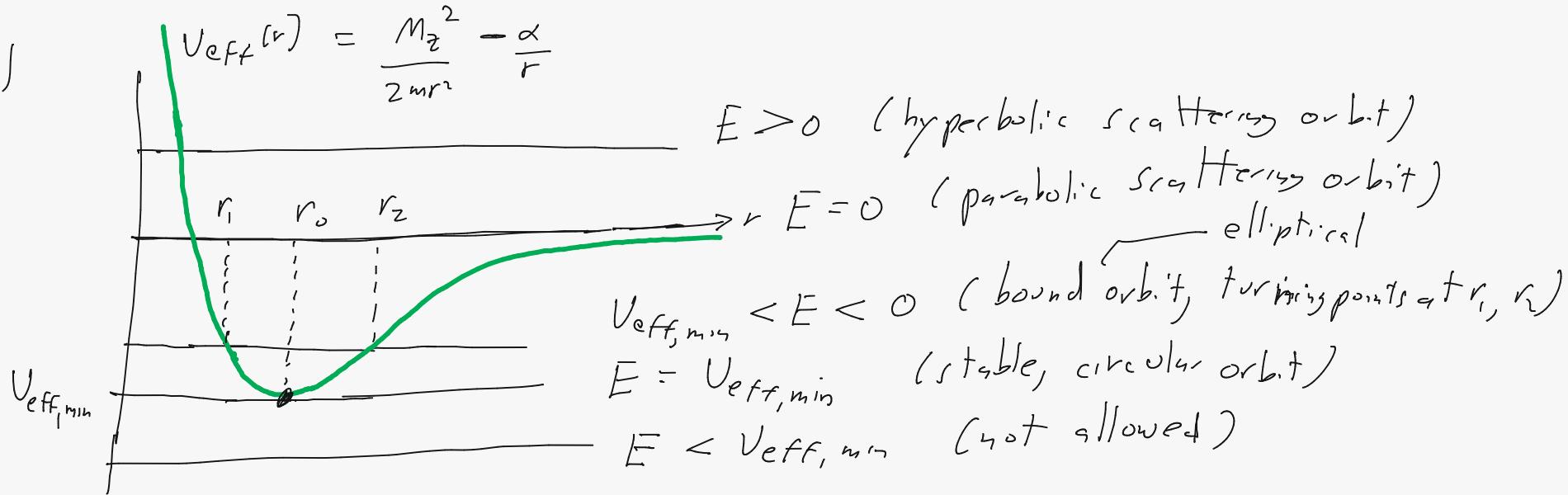
For bound orbits, $U_{\text{eff,min}} \leq E < 0$.

(i) To solve the orbit equation for $r(\phi)$, first make the substitution $u = 1/r$ in the ϕ integral:

$$\phi = \int \frac{-\ell du}{\sqrt{2m(E + GMmu) - \ell^2u^2}} + \text{const}$$

This integral now has the standard form

7)



8) $E = \frac{1}{2} m v^2 + V_{\text{eff}}(r)$, $V_{\text{eff}}(r) = \frac{M_z^2}{2mr^2} + U(r)$

$$\pm \sqrt{\frac{2}{m}(E - V_{\text{eff}}(r))} = \frac{dr}{dt}$$

$$\int dt = \pm \int \frac{dr}{\sqrt{\frac{2}{m}(E - \frac{M_z^2}{2mr^2} - U(r))}}$$

$$\rightarrow t = \pm \int \frac{dr}{\sqrt{\frac{2}{m}(E - U(r)) - \frac{M_z^2}{m^2 r^2}}} + \text{const}$$

Now:

$$\frac{dr}{dt} = \pm \sqrt{\frac{2}{m} (E - U(r)) - \frac{M_z^2}{m^2 r^2}}$$

$$\frac{dr}{dt} = \frac{dr}{d\phi} \frac{d\phi}{dt} \quad , \quad M_z = mr^2\dot{\phi} \rightarrow \frac{d\phi}{dt} = \frac{M_z}{mr^2}$$

Then,

$$\frac{dr}{d\phi} = \frac{\frac{dr}{dt}}{\frac{d\phi}{dt}} = \frac{\pm \sqrt{\frac{2}{m} (E - U(r)) - \frac{M_z^2}{m^2 r^2}}}{\frac{M_z}{mr^2}}$$

$$\rightarrow \int d\phi = \int \frac{\pm M_z dr / mr^2}{\sqrt{\frac{2}{m} (E - U(r)) - \frac{M_z^2}{m^2 r^2}}}$$

$$\phi = \pm \int \frac{M_z dr / r^2}{\sqrt{\frac{2m(E - U(r)) - M_z^2}{m^2 r^2}}} + \text{const}$$

$$9) \text{ Solve } t = t(r), \phi = \phi(r) \text{ for } V(r) = -\alpha/r$$

$$\phi = \int \frac{M_z dr/r^2}{\sqrt{2m(E + \alpha/r) - M_z^2/r^2}} + \text{const}$$

$$\text{Let } u = \frac{1}{r}, \quad du = -\frac{1}{r^2} dr$$

$$\phi = \int \frac{-M_z du}{\sqrt{2m(E + \alpha u) - M_z^2 u^2}} + \text{const}$$

$$\begin{aligned} 2m(E + \alpha u) - M_z^2 u^2 &= -M_z^2 \left(u^2 - \frac{2m\alpha}{M_z^2} u - \frac{2mE}{M_z^2} \right) \\ &= -M_z^2 \left[\left(u - \frac{m\alpha}{M_z^2} \right)^2 - \frac{m^2\alpha^2}{M_z^4} - \frac{2mE}{M_z^2} \right] \end{aligned}$$

$$= -M_z^2 \left[(u - A)^2 - B^2 \right]$$

$$A = \frac{m\alpha}{M_z^2}, \quad B = \sqrt{A^2 + \frac{2mE}{M_z^2}}$$

Thus,

$$\begin{aligned}\phi &= - \int \frac{M_z dy}{\sqrt{-M_z^2 ((u-A)^2 - B^2)}} + \text{const} \\ &= - \int \frac{dy}{\sqrt{B^2 - (u-A)^2}} + \text{const}\end{aligned}$$

Let $u-A = B \sin \theta \rightarrow dy = B \cos \theta d\theta$

$$\begin{aligned}\phi &= - \int \frac{B \cos \theta d\theta}{\sqrt{B^2 - B^2 \sin^2 \theta}} + \text{const} \\ &= - \int d\theta + \text{const} \\ &= - \theta + \text{const} \\ &= - \sin^{-1} \left(\frac{u-A}{B} \right) + \text{const} \\ &= - \sin^{-1} \left(\frac{\frac{1}{r} - A}{B} \right) + \text{const}\end{aligned}$$

$$\phi = -\sin^{-1}\left(\frac{\frac{1}{r} - A}{B}\right) + \text{const}$$

choose const so that $\phi = 0 \Leftrightarrow r = r_{\min}$ (turning point)

Turning points:

$$\frac{1}{r} - A = \pm B$$

$$\frac{1}{r} - A = \pm B$$

$$\frac{\frac{1}{r} - A}{B} = \pm 1 \rightarrow \frac{1}{r} - A = \pm B$$

$$\frac{1}{r_{\min}} = A + B \quad (+\text{sign})$$

$$0 = -\sin^{-1}(1) + \text{const}$$

$$= -\frac{\pi}{2} + \text{const}$$

$$\frac{1}{r_{\max}} = A - B \quad (-\text{sign})$$

$$\rightarrow \text{const} = \frac{\pi}{2}$$

~~$$\phi = -\sin^{-1}\left(\frac{\frac{1}{r} - A}{B}\right) + \frac{\pi}{2}$$~~

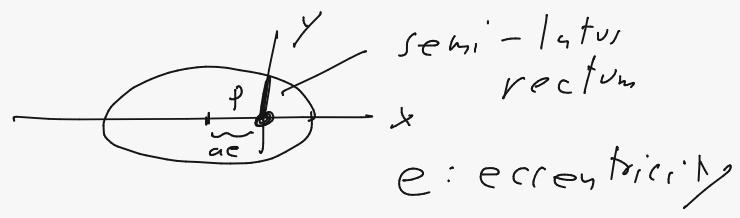
$$-\sin\left(\phi - \frac{\pi}{2}\right) = \frac{\frac{1}{r} - A}{B}$$

$$-\left(\sin\phi \cos\frac{\pi}{2} - \cos\phi \sin\frac{\pi}{2}\right) = \frac{\frac{1}{r} - A}{B} \rightarrow \boxed{\frac{1}{r} = A + B \cos\phi}$$

Now: $\frac{P}{r} = 1 + e \cos \phi$

$$\boxed{\frac{1}{r} = A + B \cos \phi}$$

$$r^2 = x^2 + y^2 \text{ where } \begin{cases} x = r \cos \phi \\ y = r \sin \phi \end{cases}$$



$$\left(\frac{x - x_0}{a}\right)^2 + \left(\frac{y}{b}\right)^2 = 1$$

with $x_0 = -ae$

$$\rightarrow J = Ar + Br \cos \phi$$

$$= A\sqrt{x^2 + y^2} + BX$$

$$(1 - BX)^2 = A^2(x^2 + y^2)$$

$$1 + B^2x^2 - 2BX = A^2x^2 + A^2y^2$$

$$\rightarrow 1 = (A^2 - B^2)x^2 + 2BX + A^2y^2$$

$$= (A^2 - B^2)\left(x^2 + \left(\frac{2B}{A^2 - B^2}\right)x\right) + A^2y^2$$

$$= (A^2 - B^2) \left[\left(x + \frac{B}{A^2 - B^2} \right)^2 - \frac{B^2}{(A^2 - B^2)^2} \right] + A^2y^2$$

$$= (A^2 - B^2) \left(x + \frac{B}{A^2 - B^2} \right)^2 - \frac{B^2}{(A^2 - B^2)} + A^2y^2$$

$$1 + \frac{B^2}{A^2 - B^2} = (A^2 - B^2) \left(x + \frac{B}{A^2 - B^2} \right)^2 + A^2 y^2$$

$$\left(\frac{A^2}{A^2 - B^2} \right) = (A^2 - B^2) \left(x + \frac{B}{A^2 - B^2} \right)^2 + A^2 y^2$$

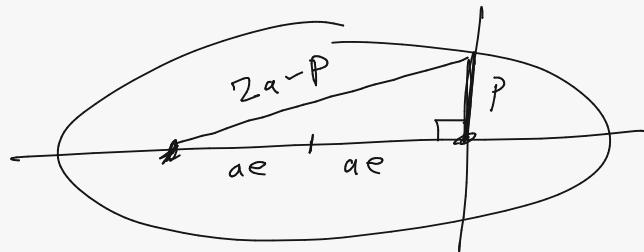
$$\begin{aligned} &= \frac{\left(x + \frac{B}{A^2 - B^2} \right)^2}{\frac{A^2}{(A^2 - B^2)^2}} + \frac{y^2}{\left(\frac{1}{A^2 - B^2} \right)} \\ &= \frac{(x - x_0)^2}{a^2} + \frac{y^2}{b^2} \end{aligned}$$

where $x_0 = -ac = -\frac{B}{A^2 - B^2}$, $A = \frac{m\alpha}{M_z^2}$, $B = \sqrt{A^2 + \frac{2mE}{M_z^2}}$

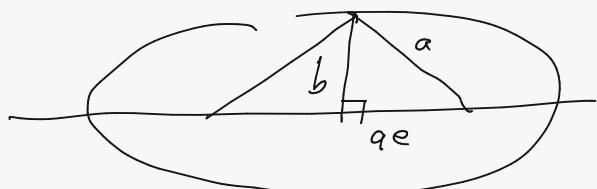
$$a = \frac{A}{A^2 - B^2}, \quad b = \frac{1}{\sqrt{A^2 - B^2}} \rightarrow Ae = B$$

$$\text{so } c = \frac{B}{A} = \frac{\sqrt{A^2 + \frac{2mE}{M_z^2}}}{A} = \sqrt{1 + \frac{\frac{2mE}{M_z^2}}{\frac{m^2\alpha^2}{M_z^4}}} = \sqrt{1 + \frac{2M_z^2 E}{m\alpha^2}} \quad (E < 0)$$

Semi-latus rectum p :



$$\begin{aligned} p^2 + (2ae)^2 &= (2a-p)^2 \\ p^2 + 4a^2e^2 &= 4a^2 + p^2 - 4ap \\ 4a^2e^2 &= 4a^2 - 4ap \\ \boxed{p = a(1-e^2)} \end{aligned}$$



$$(ae)^2 + b^2 = a^2$$

$$\begin{aligned} b^2 &= a^2(1-e^2) \\ \boxed{b = a\sqrt{1-e^2}} \end{aligned}$$

$$a = \frac{A}{A^2 - B^2} = \frac{\frac{1}{2}m\alpha}{M_z^2} \frac{-M_z^2}{-2\mu E} = \frac{\alpha}{-2E} \text{ so } \boxed{E = \frac{-\alpha}{2a}}$$

$$p = a(1-e^2) = -\frac{\alpha}{2E} \left(1 - \left(1 + \frac{M_z^2}{m\alpha^2} \right) \right) = \frac{M_z^2}{m\alpha}$$

Thus, $\boxed{p = \frac{M_z^2}{m\alpha}}$

NOTE: E depends only on α , M_z depends only on p

b) To solve for $t = t(r)$ we use

$$t = \pm \int \frac{dr}{\sqrt{\frac{2}{m}(E - U(r)) - \frac{M_z^2}{m^2 r^2}}} + \text{const}$$

Substitute $U(r) = -\frac{\alpha}{r}$ and $p = \frac{M_z^2}{m\alpha}$ so $E = -\frac{\alpha}{2a}$

$$t = \pm \int \frac{dr}{\sqrt{\frac{2}{m}\left(\frac{-\alpha}{2a} + \frac{\alpha}{r}\right) - \frac{p\alpha}{m r^2}}} + \text{const}$$

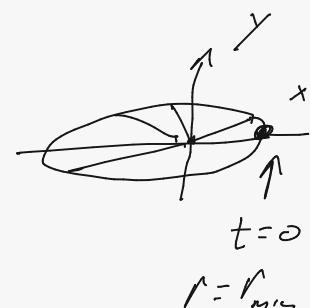
choose
+ sign
so

$t \uparrow$
with
 $\uparrow r$

$$= \pm \int \frac{dr}{\sqrt{\frac{\alpha}{m}\left(\frac{-1}{a} + \frac{2}{r} - \frac{p}{r^2}\right)}} + \text{const}$$

$$= \pm \int \frac{r dr}{\sqrt{\frac{\alpha}{m}} \sqrt{-p + 2r - \frac{r^2}{a}}} + \text{const}$$

Complete the square $\frac{1}{a}(r^2 - 2ra + pa) = \frac{1}{a}[(r-a)^2 - a^2 + pa]$



$$\begin{aligned} \text{Now: } -q^2 + pa &= -q^2 + q(1-e^2)a \\ &= -\cancel{q^2} + \cancel{q^2} - q^2 e^2 \\ &= -q^2 e^2 \end{aligned}$$

Thus,

$$t = \int \frac{r dr}{\sqrt{\frac{\alpha}{m}} \sqrt{-\frac{1}{a} ((r-a)^2 - a^2 e^2)}} + \text{const}$$

$$\underbrace{\sqrt{\frac{\alpha}{ma}} \sqrt{a^2 e^2 - (r-a)^2}}_{\sim} = \sqrt{\frac{\alpha}{ma}} ae \sqrt{1 - \cos^2 \xi} = \sqrt{\frac{\alpha}{ma}} ae \sin \xi$$

$$\text{let: } r-a = -ae \cos \xi \rightarrow r = a(1-e \cos \xi)$$

$$dr = +ae \sin \xi d\xi$$

$$\text{note: } r = a(1-e) \equiv r_{min} \text{ at } \xi = 0$$

$$r dr = a(1-e \cos \xi) ae \sin \xi d\xi$$

$$\rightarrow t = \int \frac{a(1-e \cos \xi) ae \sin \xi d\xi}{\sqrt{\frac{\alpha}{ma}} ae \sin \xi} + \text{const}$$

$$t = \sqrt{\frac{mg^3}{\alpha}} \int (1 - e \cos \xi) d\xi + \text{const}$$

$$= \sqrt{\frac{mg^3}{\alpha}} (\xi - e \sin \xi) + \text{const}$$

choose

$$t = 0 \text{ at } \xi = 0 \iff \text{const} = 0$$

Γ_{hoi}

$$t = \sqrt{\frac{mg^3}{\alpha}} (\xi - e \sin \xi)$$

$$r = a(1 - e \cos \xi)$$

or

$$\boxed{\sqrt{\frac{\alpha}{mg^3}} t = \xi - e \sin \xi}$$

$$r = a(1 - e \cos \xi)$$

so

$$\boxed{wt = \xi - e \sin \xi}$$

$$\boxed{r = a(1 - e \cos \xi)}$$

} parametric representation
 $\xi \in [0, 2\pi]$

$$\frac{H_{\text{cp}}(\omega') \cdot 3^{v+1})_{\text{av}}}{\mu = m_1 + m_2} \quad |$$

$$\omega^2 a^3 = G \mu$$

$$\alpha = G m_1 m_2$$

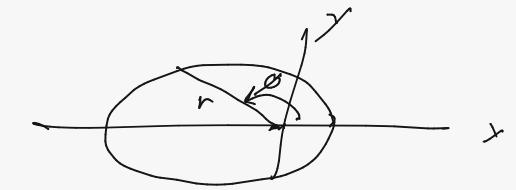
$$= G \mu m$$

$$\rightarrow \omega^2 a^3 = \frac{\alpha}{m}$$

$$\omega = \sqrt{\frac{\alpha}{m g^3}}$$

wrt x, y :

$$x = r \cos \phi, \quad y = r \sin \phi$$



$$\frac{p}{r} = 1 + e \cos \phi,$$

$$p = a(1-e^2)$$

Recall:

$$\begin{aligned} a(1-e^2) &= r + e r \cos \phi \\ &= r + e x \\ &= a(1-e \cos \xi) + e x \\ &= a - ae \cos \xi + e x \end{aligned}$$

Thus,

$$\begin{aligned} x &= a \cos \xi - ae \\ &= a(\cos \xi - e) \\ &= a \cos \xi - ae \end{aligned}$$

$$\begin{aligned} y &= \sqrt{r^2 - x^2} = \sqrt{a^2(1+e^2 \cos^2 \xi - 2ae \cos \xi)} \\ &\quad - a^2(1 \cos^2 \xi + e^2 - 2e \cos \xi) \\ &\equiv a \sqrt{(1-e^2) - (1-e^2) \cos^2 \xi} \\ &\equiv a \sqrt{1-e^2} \sqrt{1-\cos^2 \xi} = b \sin \xi \quad (b = a\sqrt{1-e^2}) \end{aligned}$$

$T^{h\nu},$

$$X = -ae + a \cos \xi$$

$$Y = b \sin \xi$$



$$I \equiv \int \frac{dx}{\sqrt{a + bx + cx^2}}$$

which can either be looked up in a handbook of integrals or solved by completing the square of the expression inside the square root. What type of substitution you make depends on the sign of E .

Completing the square:

$$2mE + 2GMm^2 u - \ell^2 u^2 = -\ell^2 \left[\left(u - \frac{GMm^2}{\ell^2} \right)^2 - \frac{G^2 M^2 m^4}{\ell^4} - \frac{2mE}{\ell^2} \right] = \ell^2 [B^2 - (u - A)^2]$$

where

$$A \equiv \frac{GMm^2}{\ell^2}, \quad B \equiv \sqrt{A^2 + \frac{2mE}{\ell^2}}$$

Thus,

$$\phi = \int \frac{-du}{\sqrt{B^2 - (u - A)^2}} + \text{const}$$

This suggests the trig substitution

$$u - A = B \sin \theta$$

for which the integral becomes

$$\phi = -\theta + \text{const} = -\sin^{-1} \left[\frac{u - A}{B} \right] + \text{const} = -\sin^{-1} \left[\frac{1/r - A}{B} \right] + \text{const}$$

It is convenient to choose the constant such that $\phi = 0$ where $r = r_{\min}$ for the orbit. Then

$$\text{const} = \sin^{-1} \left[\frac{1/r_{\min} - A}{B} \right]$$

But since r_{\min} is a turning point of the motion, it follows that

$$\frac{1}{r_{\min}} - A = B \Rightarrow \text{const} = \sin^{-1}(1) = \pi/2$$

Thus, making this substitution for the constant, and solving for $1/r$, we obtain

$$\frac{1}{r} = A + B \cos \phi$$

This has the form of an ellipse

$$\boxed{\frac{p}{r} = 1 + e \cos \phi}$$

where p is the semi-latus rectum of the ellipse and e is the eccentricity (discussed in detail below). Solving for p and e :

$$p = \frac{\ell^2}{GMm^2}, \quad e = \sqrt{1 + \frac{2E\ell^2}{G^2M^2m^3}}$$

Using the fact that the semi-major axis a and semi-latus rectum p for an ellipse are related by

$$p = a(1 - e^2)$$

it follows from the above expressions that

$$a = -\frac{GMm}{2E} \quad \text{or, equivalently, } E = -\frac{GMm}{2a}$$

(ii) To solve for the time dependence of the orbit, we rewrite the time integral as

$$t = \sqrt{\frac{m}{2|E|}} \int \frac{r dr}{\sqrt{-r^2 + \frac{GMm}{|E|}r - \frac{\ell^2}{2m|E|}}} + \text{const}$$

where we have simplified the square-root in the denominator by pulling out a factor of $\sqrt{\frac{2|E|}{m}} \frac{1}{r}$.

We then use the expressions

$$E = -\frac{GMm}{2a}, \quad p = \frac{\ell^2}{GMm^2}$$

to further simplify the integral:

$$t = \sqrt{\frac{a}{GM}} \int \frac{r dr}{\sqrt{-r^2 + 2ar - pa}} + \text{const}$$

Completing the square in the square root is now easy:

$$-r^2 + 2ar - pa = -[(r - a)^2 - a^2 + pa] = -[(r - a)^2 - a^2 e^2]$$

where we used $p = a(1 - e^2)$ to get the last equality. This suggests the trig substitution

$$r - a = -ae \cos \xi$$

where we have chosen to use a cosine function so that $\xi = 0$ corresponds to $r_{\min} = a(1 - e)$. Making this substitution into the integral yields

$$t = \sqrt{\frac{a}{GM}} \int d\xi a(1 - e \cos \xi) + \text{const} = \sqrt{\frac{a^3}{GM}}(\xi - e \sin \xi)$$

where we have set the constant to zero so that $t = 0$ corresponds to $\xi = 0$.

Thus, we have the parametric representation

$$\boxed{r = a(1 - e \cos \xi), \quad t = \sqrt{\frac{a^3}{GM}}(\xi - e \sin \xi)}$$

We can also find an expression for x and y in terms of ξ :

We start with

$$x = r \cos \phi$$

Using

$$\frac{p}{r} = 1 + e \cos \phi$$

it follows that

$$p = r + ex \quad \text{or} \quad x = \frac{1}{e}(p - r)$$

Substituting for $r = a(1 - e \cos \xi)$ then gives

$$\boxed{x = a(\cos \xi - e)}$$

To find

$$y = r \sin \phi$$

we write it instead as

$$y = \sqrt{r^2 - x^2}$$

Substituting for r and x in terms of ξ gives:

$$\boxed{y = a\sqrt{1 - e^2} \sin \xi}$$

A complete orbit is traversed when ξ goes from 0 to 2π .

Parametric representation of the time-evolution of an elliptical orbit

```
In [11]: # parameters for ellipse
a = 1
e = 0.5
G = 1
M = 1

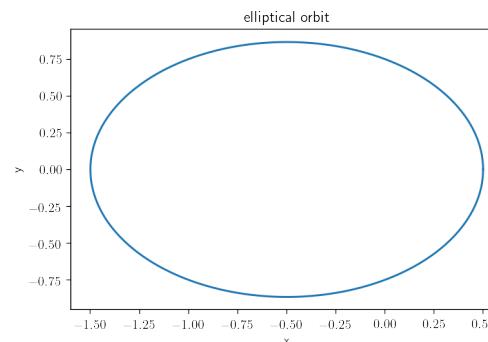
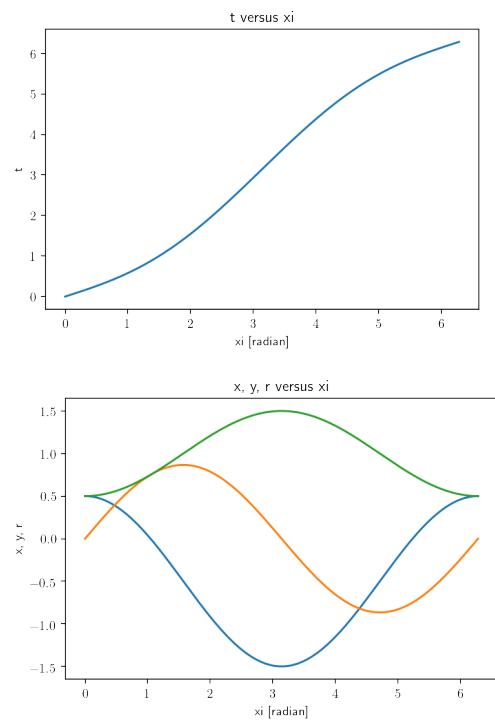
xi = np.linspace(0, 2*np.pi, 10000)
t = np.sqrt(a**3/(G*M)) * (xi - e*np.sin(xi))
r = a*(1-e*np.cos(xi))
x = a*(np.cos(xi)-e)
y = a*np.sqrt(1-e**2)*np.sin(xi)

plt.figure()
plt.plot(xi, t)
plt.xlabel('xi [radian]')
plt.ylabel('t')
plt.title('t versus xi')

plt.figure()
plt.plot(xi, x, xi, y, xi, r)
plt.xlabel('xi [radian]')
plt.ylabel('x, y, r')
plt.title('x, y, r versus xi')

plt.figure()
plt.plot(x,y)
plt.xlabel('x')
plt.ylabel('y')
plt.title('elliptical orbit')
```

Out[11]: Text(0.5, 1.0, 'elliptical orbit')



10) Derive the relationship between E , ℓ , a , b , e , and p for an ellipse.

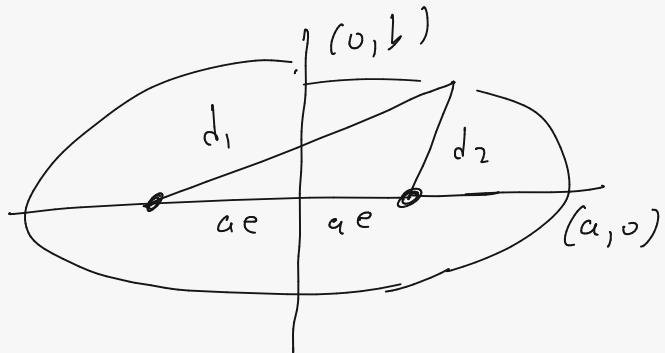
Central force motion is described by two parameters, e.g.,

- E and ℓ (the energy and angular momentum of the motion)
- a and b (the semi-major and semi-minor axes of the ellipse)
- a and e (the semi-major axis and eccentricity of the ellipse)
- a and p (the semi-major axis and semi-latus rectum of the ellipse)
- r_{\min} and r_{\max} (the minimum and maximum radii, perihelion and aphelion for motion around the Sun)
- or other combinations of the above

It is useful to be able to derive expressions relating the different parameterizations.

Ellipse:

10) $E \parallel p/c$:



(a, b, P, e)

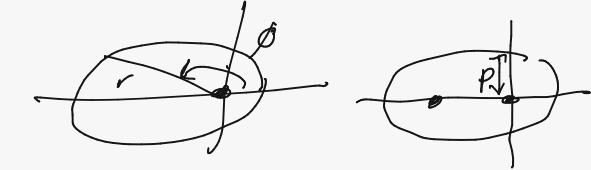
$$d_1 + d_2 = 2a$$

Already showed: $P = a(1-e^2)$

$$b = a\sqrt{1-e^2} \rightarrow e = \sqrt{1 - \left(\frac{b}{a}\right)^2}$$

$$\frac{P}{r} = 1 + e \cos \phi$$

for origin & focal point



$$E = \frac{1}{2}mr^2 + \left(\frac{M^2}{2mr^2} - \frac{\alpha}{r} \right)$$

$$r_{min} = r(\phi=0) = a(1-e)$$

$$r_{max} = r(\phi=\pi) = a(1+e)$$

thus,

$$E = \frac{M^2}{2m a^2(1-e)^2} - \frac{\alpha}{a(1-e)}$$

$$E = \frac{M^2}{2m a^2(1+e)^2} - \frac{\alpha}{a(1+e)}$$

turning points (so $r \neq 0$)

$$r_{min}, r_{max}$$

two equations

solve for E :

$$\frac{E}{(1+e)^2} - \frac{E}{(1-e)^2} = -\frac{\alpha}{a} \left(\frac{1}{(1-e)(1+e)^2} - \frac{1}{(1+e)(1-e)^2} \right)$$

$$\text{Thes} \quad E \left(\frac{(1-e)^2 - (1+e)^2}{(1-e)^2 (1+e)^2} \right) = -\frac{\alpha}{a} \frac{1}{(1-e^2)^2} \left((K_e) - (K_{-e}) \right)$$

$$E (K_{+e}^2 - 2e - K_{-e}^2 - 2e) = -\frac{\alpha}{a} (-2e)$$

$$-4E \neq = 2 \frac{\alpha e}{a}$$

$$\boxed{E = -\frac{\alpha}{2a}}$$

ii) Solve for M :

$$\overline{O} = \frac{M^2}{2ma^2} \left(\frac{1}{(1-e)^2} - \frac{1}{(1+e)^2} \right) - \frac{\alpha}{a} \left(\frac{1}{1-e} - \frac{1}{1+e} \right)$$

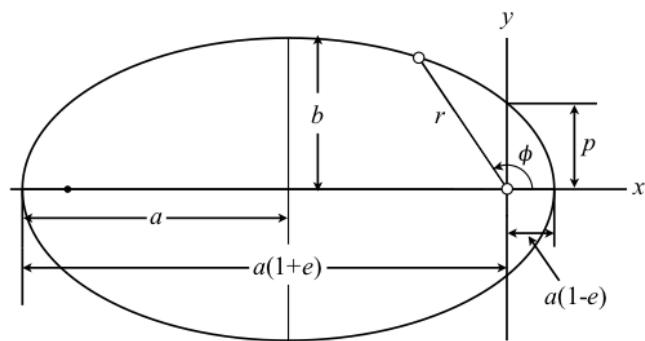
$$= \frac{M^2}{2ma^2} \left(\frac{(1+e)^2 - (1-e)^2}{(1-e^2)^2} \right) - \frac{\alpha}{a} \frac{(K_e - K_{-e})}{(1-e^2)}$$

$$= \frac{M^2}{2ma^2} \frac{4e}{(1-e^2)^2} - \frac{2\alpha e}{a(1-e^2)}$$

multiply by $\frac{a(1-e^2)}{2e}$:

$$\overline{O} = \frac{M^2}{\underbrace{m\alpha(1-e^2)}_P} - \alpha \rightarrow$$

$$\boxed{M = \sqrt{\alpha m P}}$$



Using that fact that

$$d_1 + d_2 = 2a$$

where d_1 and d_2 are the distances from the two focal points to a point on the ellipse, one can show that

$$p = a(1 - e^2)$$

$$b = a\sqrt{1 - e^2}$$

$$e = \frac{\sqrt{a^2 - b^2}}{a}$$

We also have

$$r_{\min} = a(1 - e), \quad r_{\max} = a(1 + e)$$

We also showed earlier that

$$E = -\frac{GMm}{2a}, \quad \ell = \sqrt{GMm^2 p}$$

so that E only depends on a and ℓ only depends on p .

These last two results can also be derived from the conservation of energy equation:

$$E = \frac{1}{2}mr^2 + \frac{\ell^2}{2mr^2} - \frac{GMm}{r}$$

evaluated at $r_{\min} = a(1 - e)$ and $r_{\max} = a(1 + e)$, where $\dot{r} = 0$. One then has two equations which can be solved for E and ℓ in terms of a and e (or a and $p = a(1 - e^2)$), which leads back to the boxed equations.

11) State the only two central potentials that have closed bound orbits.

- $U = -a/r$ (Newtonian gravity)
- $U = ar^2$ (3d harmonic oscillator)

Other potentials can have bound orbits, but they won't be closed. For example, precessing ellipses in general relativity (perihelion precession of Mercury).

12) State and derive Kepler's three laws of planetary motion.

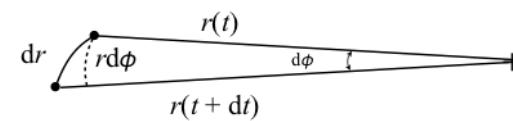
Kepler's laws:

- I. Planets go around the Sun in elliptical orbits with the Sun at one focus
- II. A line connecting a planet to the Sun sweeps out equal areas in equal times
- III. $P^2/a^3 = \text{const}$ for all planets, where P is the orbital period of a planet and a is the semi-major axis of its elliptical orbit around the Sun

NOTE: Kepler's laws need to be adjusted slightly given the finite mass of the Sun. Since the Sun has finite mass, the focal point of the elliptical orbit is actually at the COM of the planet and the Sun. Also, the constant in Kepler's 3rd law is not related to the mass of the Sun but to the total mass of the Earth-planet system.

Proof:

- I. We already proved this law by integrating the orbit equation to find r as a function of ϕ .
- II. Equal areas in equal times means that dA/dt should be constant. From the following figure



we see that the differential area swept out in time interval dt is approximately a triangle, so

11) $U = -\frac{\alpha}{r}$, $U = \frac{1}{2} k r^2$ have bound, closed orbit,

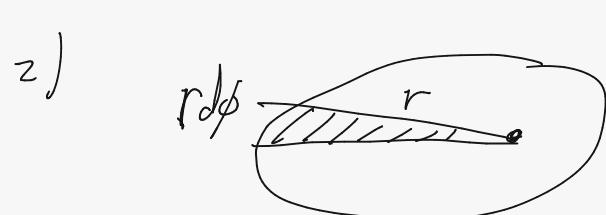
12) 1) Planets move on elliptical orbits around the Sun with the Sun at one focal point

2) A line connecting a planet to the Sun sweeps out equal areas in equal times

3) $\frac{P^2}{a^3} = \text{const}$ for all planets where $P = \text{period}$
of orbit and $a = \text{semi-major axis}$

Proof:

- 1) Integrate $\phi = \phi(r) \rightarrow \frac{P}{r} = 1 + e \cos \phi$



$$dA = \frac{1}{2} r d\phi r$$

$$\frac{dA}{dt} = \frac{1}{2} r^2 \dot{\phi}$$

$$= \frac{1}{2} \frac{M}{m}$$

$$= \text{const}$$

$$M = mr^2 \dot{\phi}$$

$$3) \frac{dA}{dt} = \sum \frac{M}{m}$$

$$\int dA = \int \sum \frac{M}{m} dt$$

$$\cancel{M_{ab}} = \frac{1}{2} \frac{M}{m} P$$

$$= \frac{1}{2} \frac{M}{m} \frac{\cancel{dt}}{\omega}$$

$$\rightarrow \omega = \frac{M}{m a^2 \sqrt{1-e^2}}$$

$$= \frac{\sqrt{G \mu m^2 a (1-e^2)}}{m a^2 \sqrt{1-e^2}}$$

$$= \frac{\sqrt{G \mu}}{a^{3/2}}$$

$$\boxed{\omega^2 a^3 = G \mu}$$

$$M = \sqrt{\alpha m p}$$

$$= \sqrt{G \mu m^2 p}$$

$$= \sqrt{G \mu m^2 a (1-e^2)}$$

$$\omega^2 a^3 = G \mu$$

$$\frac{G \mu m}{a^2} = m \omega^2 a$$

$$\boxed{G \mu = \omega^2 a^3}$$

$$\omega = \sqrt{\frac{G \mu}{a^3}}$$

$$dA = \frac{1}{2} \text{base} \cdot \text{height} = \frac{1}{2} r^2 d\phi$$

Dividing both sides by dt and using $\ell = mr^2 \dot{\phi}$, it follows that

$$\frac{dA}{dt} = \frac{1}{2} r^2 \dot{\phi} = \frac{\ell}{2m} = \text{const}$$

Note that Kepler's 2nd law is a consequence of conservation of angular momentum, and is therefore valid for any central potential.

III. For Kepler's 3rd law, we need to calculate the period of a planet's orbit around the Sun. This can be obtained by integrating Kepler's 2nd law for one complete elliptical orbit:

$$P = \int dt = \int \frac{2m}{\ell} dA = \frac{2m}{\ell} \pi ab$$

where we used $A = \pi ab$ for the area of an ellipse.

Then substituting for

$$b = a\sqrt{1 - e^2}, \quad \ell = \sqrt{GMm^2p}, \quad p = a(1 - e^2)$$

we get

$$P = \frac{2m}{\sqrt{GMm^2p}} \pi a^2 \sqrt{1 - e^2} = 2\pi \sqrt{\frac{a^3}{GM}}$$

so

$$\frac{P^2}{a^3} = \frac{4\pi^2}{GM}$$

which is the desired result. In terms of the angular frequency $\omega = 2\pi/P$, we have

$$\boxed{\omega^2 a^3 = GM}$$

13) Explain the difference in E and e for elliptical, parabolic, and hyperbolic motion.

- Elliptical orbits: $U_{\text{eff,min}} \leq E < 0, 0 \leq e < 1$
- Parabolic (scattering) motion: $E = 0, e = 1$
- Hyperbolic (scattering) motion: $E > 0, e > 1$

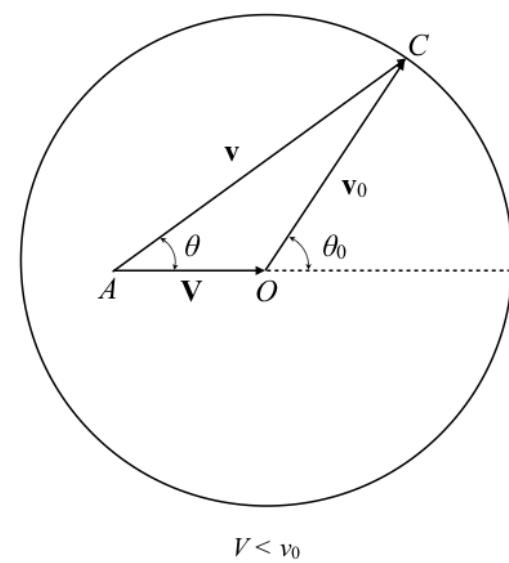
5. Collisions and scattering (16-20)

1) Draw diagrams relating velocities in the lab and COM frames for the disintegration of a single particle.

Notation:

- \mathbf{v}_0 is the velocity of one of the particles produced by the disintegration as seen in the COM frame
- \mathbf{v} is its velocity with respect to the lab frame
- \mathbf{V} is the velocity of the COM of the system (i.e., the velocity of the particle in the lab frame before disintegration)
- θ_0 is the angle that \mathbf{v}_0 makes wrt \mathbf{V} as seen in the COM frame
- θ is the angle that \mathbf{v} makes wrt \mathbf{V} as seen in the lab frame

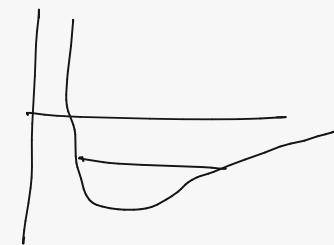
Case $V < v_0$:



$$V < v_0$$

Case $V > v_0$:

13) Elliptical : $E < 0$, $0 \leq e < 1$

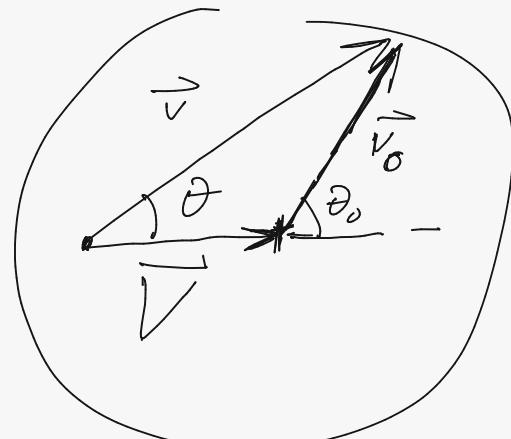


Parabolic : $E = 0$, $e = 1$

Hyperbolic : $E > 0$, $e > 1$

5.) Collision :

i)



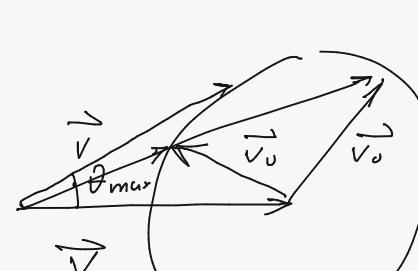
$$|\vec{V}| < |\vec{v}_0|$$

\vec{v} : wrt lab frame

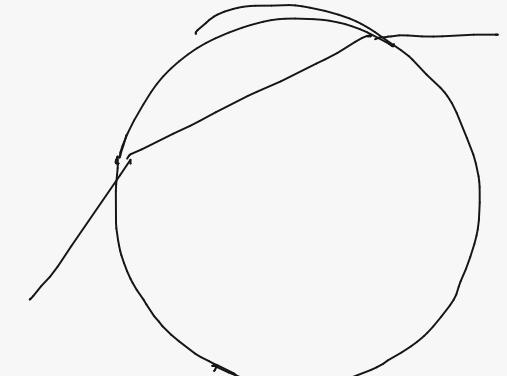
\vec{v}_0 : wrt com frame

\vec{V} : velocity of COM

$$\vec{v} = \vec{V} + \vec{v}_0$$

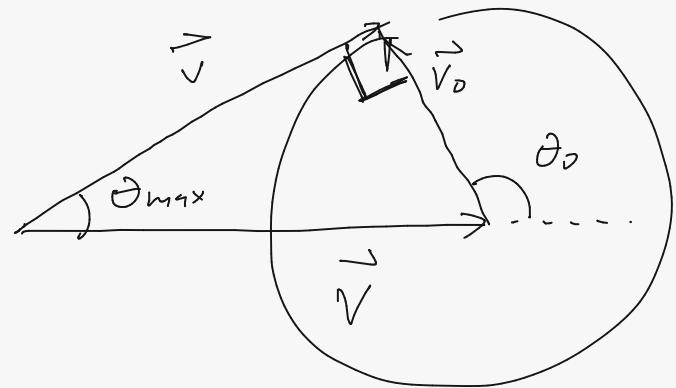


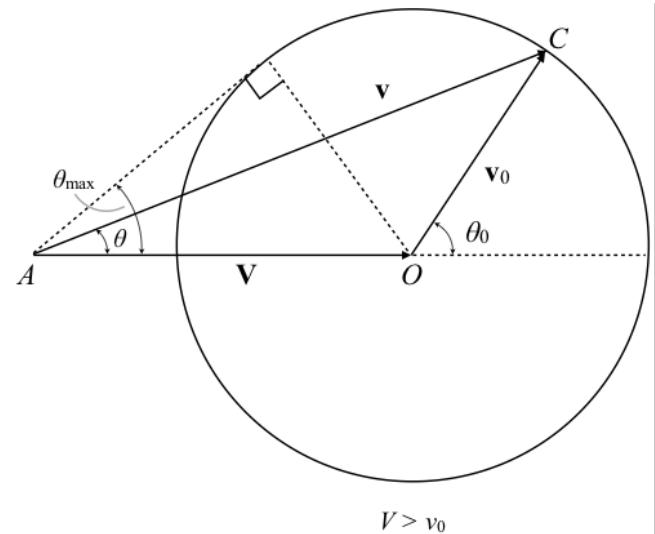
$$|\vec{V}| > |\vec{v}_0|$$



Emitted particle comes out in forward direction only

$$\sin \theta_{max} = \frac{V_0}{V}$$



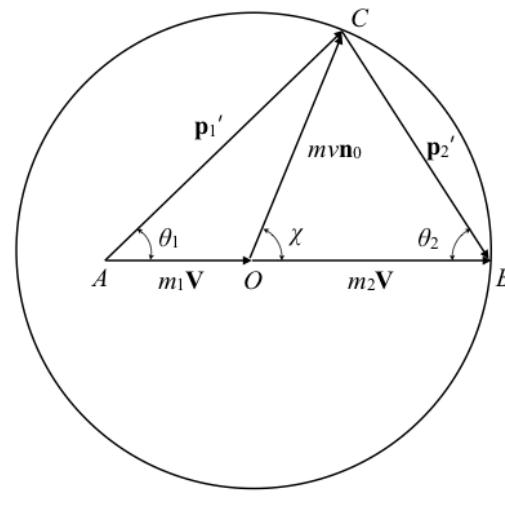


For the case $V > v_0$, the particles produced by the disintegration are emitted only in the forward direction as seen in the lab frame, $\theta < \pi/2$. The maximum angle θ_{\max} is

$$\sin \theta_{\max} = \frac{v_0}{V}$$

- θ_2 is the angle that particle 2 makes wrt \mathbf{V} as seen in the lab frame

Case $m_1 < m_2, v_2 = 0$:



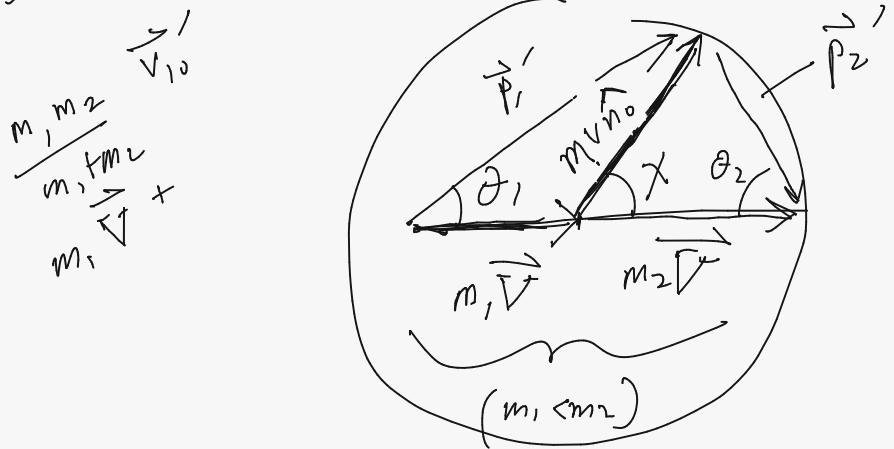
Case $m_1 > m_2, v_2 = 0$:

2) Draw diagrams relating the momenta in the lab and COM frames for an elastic collision of two particles (m_2 initially at rest in the lab frame).

Notation:

- $\mathbf{p}'_1, \mathbf{p}'_2$ are the momenta of the two particles as seen in the lab frame after the collision
- \mathbf{n}_0 is the direction of particle 1 as seen in the COM frame after the collision (subscript '0' denotes quantities wrt COM frame)
- $v = |\mathbf{v}|$ is the magnitude of the relative velocity vector $\mathbf{v} \equiv \mathbf{v}_1 - \mathbf{v}_2$ before the collision (note: $\mathbf{v} = \mathbf{v}_0 \equiv \mathbf{v}_{10} - \mathbf{v}_{20}$)
- m is the reduced mass of the system, $m \equiv m_1 m_2 / (m_1 + m_2)$
- \mathbf{V} is the velocity of the COM of the system $\mathbf{V} \equiv (m_1 \mathbf{v}_1 + m_2 \mathbf{v}_2) / (m_1 + m_2) = m_1 \mathbf{v}_1 / (m_1 + m_2)$ since $\mathbf{v}_2 = 0$
- χ is the angle that particle 1 makes wrt \mathbf{V} as seen in the COM frame
- θ_1 is the angle that particle 1 makes wrt \mathbf{V} as seen in the lab frame

2)



$$\vec{P} = (m_1 + m_2) \vec{V}$$

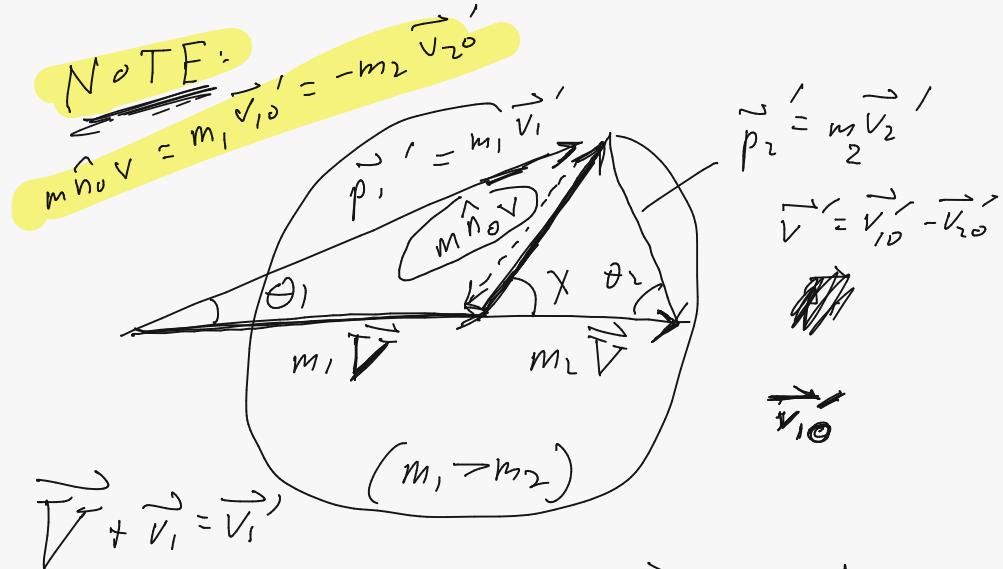
= total momentum before collision

$$\vec{V} = \frac{m_1 \vec{v}_1 + m_2 \vec{v}_2}{m_1 + m_2} = \frac{m_1 \vec{V}_1}{m_1 + m_2} = \frac{\frac{m_1 \vec{V}}{m_1 + m_2}}{m_1 + m_2} = \frac{m_1 \vec{V}_0}{m_1 + m_2}$$

$$m \vec{V}_{N_D} = \cancel{m \vec{V}}$$

$$T = \sum m_i |\vec{V}_{10}|^2 + \sum m_i |\vec{V}_{20}|^2 = \frac{1}{2} m |\vec{V}_0|^2 = \frac{1}{2} m |\vec{V}|^2$$

$$T' = \sum m_i |\vec{V}'_{10}|^2 + \sum m_i |\vec{V}'_{20}|^2 = \frac{1}{2} m |\vec{V}'_0|^2 = \frac{1}{2} m |\vec{V}'|^2$$



$$\vec{V} = \vec{V}_1 - \vec{V}_2$$

$$\vec{V}_0 = \vec{V}_{10} - \vec{V}_{20}$$

Relative
velocity
vector

wrt COM

$\vec{V}_2 = 0$ (wrt lab frame)

$$|\vec{V}'| = |\vec{V}|$$

only direction changes
consequence of
cons. of PE

$$\vec{r} = \vec{r}_1 - \vec{r}_2 \quad \rightarrow \quad m_1 \vec{r}_1 + m_2 \vec{r}_2 = 0$$

$$m_1 \vec{r}_1 = -m_2 (\vec{r}_1 - \vec{r})$$

$$(m_1 + m_2) \vec{r}_1 = m_2 \vec{r}$$

$$\vec{r}_1 = \left(\frac{m_2}{m_1 + m_2} \right) \vec{r}$$

$$\vec{r}_2 = -\left(\frac{m_1}{m_1 + m_2} \right) \vec{r}$$

$$\vec{r}_2 = \vec{r}_1 - \vec{r}$$

$$m_1 \vec{v}_{10}' = -m_2 \vec{v}_{20}'$$

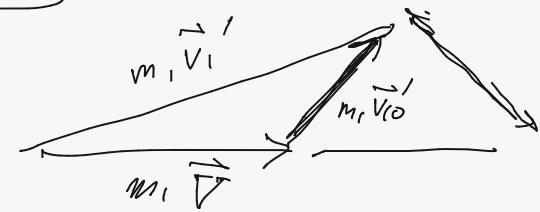
The diagram shows a vector \vec{v}_{10}' originating from a point. It is decomposed into two vectors: $m_2 \vec{v}_{20}'$ pointing downwards and to the left, and $m_2 \vec{v}_n'$ pointing downwards and to the right. The sum of these two vectors is labeled $m_2 \vec{v}_-$.

$$\vec{v}_{10}' = \left(\frac{m_2}{m_1 + m_2} \right) \vec{v}'$$

$$\vec{v}_{10}' = \left(\frac{m_2}{m_1 + m_2} \right) \vec{v}'$$

$$\vec{v}_{20}' = -\left(\frac{m_1}{m_1 + m_2} \right) \vec{v}'$$

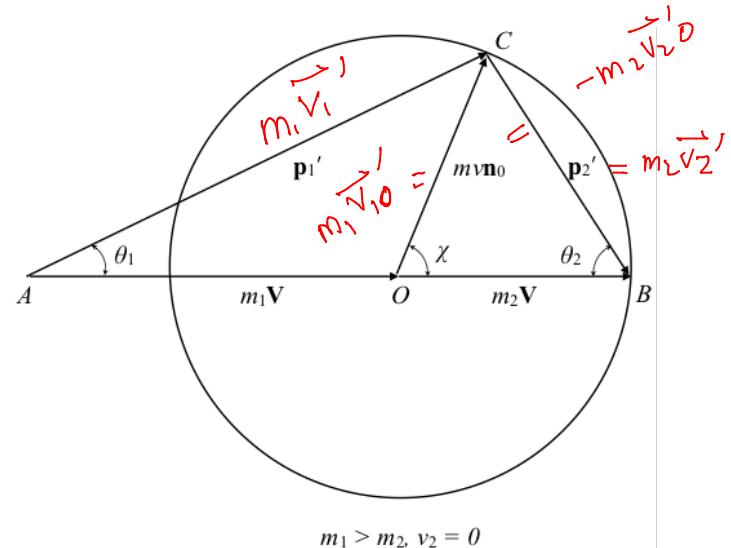
$$\vec{v}_{20}' = \left(\frac{m_1}{m_1 + m_2} \right) \vec{v}'$$



$$\underline{\underline{m_1 \hat{n}_0 V}} = \underline{\underline{m \vec{v}'}}$$

$$= \underline{\underline{\frac{m_1 m_2}{m_1 + m_2} \vec{v}'}}$$

$$= \underline{\underline{m_1 \vec{v}_{10}'}}$$



Conservation of momentum (wrt lab frame):

$$(m_1 + m_2)\mathbf{V} = \mathbf{p}'_1 + \mathbf{p}'_2$$

In the COM frame, the total momentum is zero, since the momenta of the two particles are equal and opposite. After the collision:

$$\mathbf{p}'_{10} = m\mathbf{v}\mathbf{n}_0 = -\mathbf{p}'_{20}$$

Elastic collision: The magnitude v of the relative velocity vector \mathbf{v} is the same before and after the collision, $v = v'$.

For the case where m_2 is initially at rest (i.e., $v_2 = 0$) we have $\mathbf{v} = \mathbf{v}_1$. Thus,

$$m_2 V = m_2 \frac{m_1 v_1}{m_1 + m_2} = m v_1 = m v$$

so B lies on the boundary of the circle.

For the case $m_1 > m_2$, we can only have forward scattering of the particles in the lab frame, $\theta_1, \theta_2 < \pi/2$.

3) Explain what information can and cannot be obtained for an elastic collision of two particles, using just conservation of momentum and kinetic energy.

An elastic collision of two particles is mostly simply analyzed in the COM frame. In this frame, the momenta of the two particles both before and after the collision are equal in magnitude and opposite in direction. Conservation of kinetic energy implies that the magnitude of the relative velocity vector \mathbf{v} is unchanged by the collision since

$$T = \frac{1}{2}m_1|\mathbf{v}_{10}|^2 + \frac{1}{2}m_2|\mathbf{v}_{20}|^2 = \frac{1}{2}m|\mathbf{v}_0|^2$$

where

$$m \equiv \frac{m_1 m_2}{m_1 + m_2}, \quad \mathbf{v}_0 \equiv \mathbf{v}_{10} - \mathbf{v}_{20} = \mathbf{v}_1 - \mathbf{v}_2 \equiv \mathbf{v}$$

Hence an elastic collision can only change the direction of the relative velocity vector. This direction *cannot* be determined. It is denoted by \mathbf{n}_0 in the above figures.

(3) Cons. of $H\bar{E}$ and momentum for an elastic collision gives, 3 equations for 4 unknowns, $v_1', v_2', \theta_1, \theta_2$
 Collision is a plane

Cons. of momentum \rightarrow COM frame

$$\begin{aligned} T &= \frac{1}{2} m_1 |\vec{v}_{10}|^2 + \frac{1}{2} m_2 |\vec{v}_{20}|^2 \\ &= \frac{1}{2} m |\vec{v}_0|^2 \quad \text{where } m = \frac{m_1 m_2}{m_1 + m_2} \quad \text{and } \vec{v}_0 = \vec{v}_{10} - \vec{v}_{20} \end{aligned}$$

Cons. of $H\bar{E}$

$$\begin{array}{ccc} \frac{1}{2} m |\vec{v}_0|^2 & = & \frac{1}{2} m |\vec{v}'_0|^2 \\ || & & || \\ |\vec{v}|^2 & & |\vec{v}'|^2 \end{array}$$

so relative velocity
 vectors before and
 after the collision have
 the same lengths
 but point \vec{r} is different
 direction.

\vec{r} can't be
 determined.

4) Derive formulas relating the scattering angles χ , θ_1 , θ_2 in the COM and lab frames.

From either of the last two figures, one sees that

$$\chi + 2\theta_2 = \pi \quad (\text{from isosceles triangle } OBC)$$

so

$$\boxed{\theta_2 = \frac{1}{2}(\pi - \chi)}$$

Also

$$\tan \theta_1 = \frac{mv \sin \chi}{m_1 V + mv \cos \chi}$$

Using

$$m \equiv \frac{m_1 m_2}{m_1 + m_2}, \quad v = v_1, \quad V = \frac{m_1 v_1}{m_1 + m_2}$$

where the last two results hold since $v_2 = 0$, it follows that

$$\boxed{\tan \theta_1 = \frac{m_2 \sin \chi}{m_1 + m_2 \cos \chi}}$$

For differential cross-section calculations (see below), it is more convenient to invert these equations for χ in terms of θ_1 and θ_2 :

$$\cos \chi = -\left(\frac{m_1}{m_2}\right) \sin^2 \theta_1 \pm \cos \theta_1 \sqrt{1 - \left(\frac{m_1}{m_2}\right)^2 \sin^2 \theta_1}$$

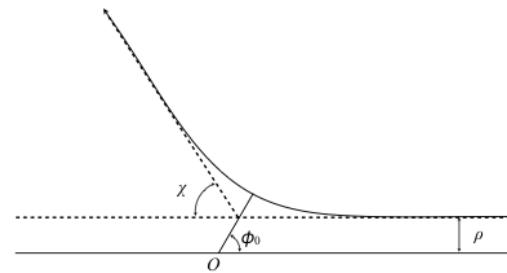
and

$$\chi = \pi - 2\theta_2$$

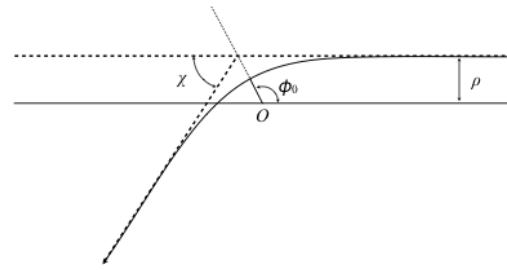
In the above equation for $\cos \chi$ in terms of θ_1 , we should take the + sign for $m_1 < m_2$ in order that $\chi = 0$ corresponds to $\theta_1 = 0$. For $m_1 > m_2$, both signs are necessary, indicating that there are two possible values of χ for a single value of θ_1 .

5) Draw diagrams showing how the scattering angle χ is related to the angle of closest approach ϕ_0 .

Repulsive scattering:



Attractive scattering:



For repulsive scattering

$$\chi + 2\phi_0 = \pi$$

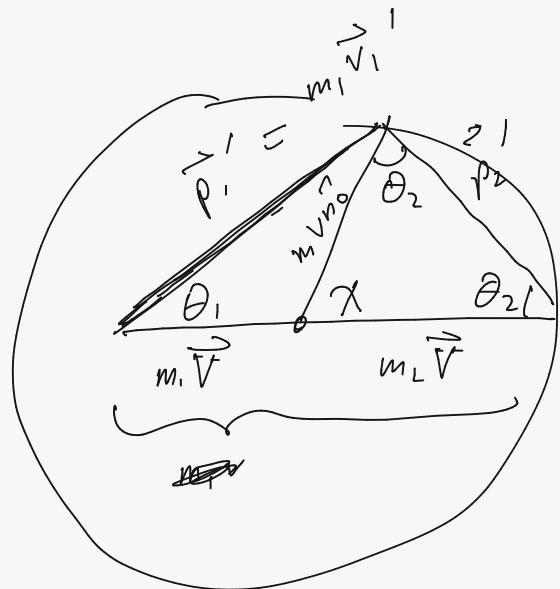
For attractive scattering

$$\phi_0 + (\phi_0 - \chi) = \pi \Rightarrow 2\phi_0 - \chi = \pi$$

Both of these relations can be captured by

$$\chi = |\pi - 2\phi_0|$$

4)



$$\vec{V} = \frac{m_1 \vec{v}_1}{m_1 + m_2} \quad (\vec{v}_2 = 0)$$

$$m_1 \vec{V} = \frac{m_1 m_1}{m_1 + m_2} \vec{v}_1$$

$$= \frac{m_1^2}{m_1 + m_2} \vec{v}$$

$$2\theta_2 + \chi = \pi$$

$$\chi = \pi - 2\theta_2$$

$$\theta_2 = \frac{\pi - \chi}{2}$$

$$\tan \theta_1 = \frac{m_1 \sin \chi}{m_1 V + m_2 \cos \chi}$$

$$= \frac{\frac{m_1 m_2}{m_1 + m_2} V \sin \chi}{\frac{m_1^2}{m_1 + m_2} V + \frac{m_1 m_2}{m_1 + m_2} V \cos \chi}$$

$$= \frac{m_2 \sin \chi}{m_1 + m_2 \cos \chi}$$

$$\boxed{\tan \theta_1 = \frac{m_2 \sin \chi}{m_1 + m_2 \cos \chi}}$$

Invert 1st equation to find $\cos \chi$ in terms of θ_1, θ_2 :

$$\chi = \pi - 2\theta_2 \rightarrow \boxed{\begin{aligned} \cos \chi &= \cos(\pi - 2\theta_2) \\ &= \cos \pi \cos 2\theta_2 + \cancel{\sin \pi} \sin 2\theta_2 \\ &= -\cos 2\theta_2 \end{aligned}}$$

$$\tan \theta_1 = \frac{m_2 \sin \chi}{m_1 + m_2 \cos \chi} = \frac{m_2 \sqrt{1 - \cos^2 \chi}}{m_1 + m_2 \cos \chi}$$

$$\tan^2 \theta_1 (m_1 + m_2 \cos \chi)^2 = m_2^2 (1 - \cos^2 \chi)$$

$$\tan^2 \theta_1 (m_1^2 + m_2^2 \cos^2 \chi + 2m_1 m_2 \cos \chi) = m_2^2 - m_2^2 \cos^2 \chi$$

$$m_2^2 \cos^2 \chi (\tan^2 \theta_1 + 1) + 2m_1 m_2 \tan^2 \theta_1 \cos \chi + (m_1^2 \tan^2 \theta_1 - m_2^2) = 0$$

$$\rightarrow \cos \chi = \frac{-2m_1 m_2 \tan^2 \theta_1 \pm \sqrt{4m_1^2 m_2^2 \tan^4 \theta_1 - 4m_2^2 (\tan^2 \theta_1 + 1)}}{2m_2^2 (\tan^2 \theta_1 + 1)}$$

$$\begin{aligned} \sqrt{\bullet} \rightarrow \bullet &= 4m_1^2 m_2^2 \tan^4 \theta_1 - 4m_2^2 (m_1^2 + m_2^2 \tan^4 \theta_1 + m_1^2 \tan^2 \theta_1 - m_2^2 - m_2^2 \tan^2 \theta_1) \\ &= -4m_1^2 m_2^2 \tan^2 \theta_1 + 4m_1^4 + 4m_2^4 \tan^2 \theta_1 = 4m_2^2 ((m_1^2 - m_2^2) \tan^2 \theta_1 + m_2^2) \end{aligned}$$

$$\begin{aligned}
 0 &= 4m_2^2 \left(m_2^2 (1 + \tan^2 \theta_1) - m_1^2 \tan^2 \theta_1 \right) \\
 &= 4m_2^2 \left(m_2^2 \sec^2 \theta_1 - m_1^2 \cancel{\tan^2 \theta_1} \right) \\
 &= \frac{4m_2^4}{\cos^2 \theta_1} \left(1 - \frac{m_1^2 \sin^2 \theta_1}{m_2^2} \right)
 \end{aligned}$$

$$\begin{cases} \sin^2 \theta_1 + \cos^2 \theta_1 = 1 \\ \tan^2 \theta_1 + 1 = \sec^2 \theta_1 \end{cases}$$

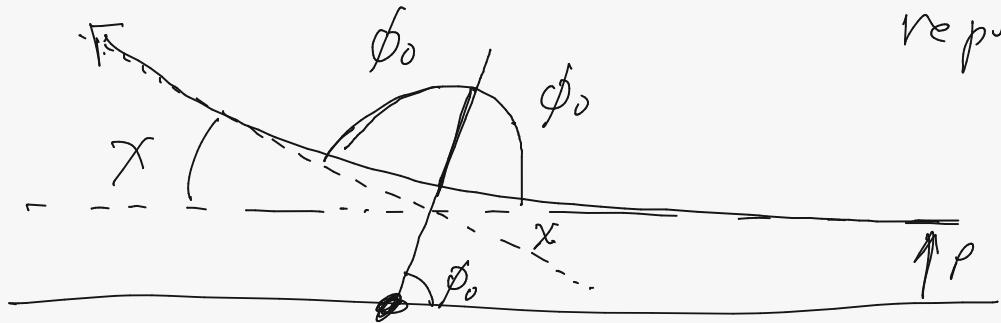
$$\begin{aligned}
 \boxed{\cos \theta_1 \chi} &= -2m_1 m_2 \tan \theta_1 \pm \frac{2m_2^2}{\cos \theta_1} \sqrt{1 - \frac{m_1^2}{m_2^2} \sin^2 \theta_1} \\
 &\quad \boxed{2m_2^2 \sec^2 \theta_1} \\
 &= -\left(\frac{m_1}{m_2}\right) \sin \theta_1 \pm \cos \theta_1 \sqrt{1 - \left(\frac{m_1}{m_2}\right)^2 \sin^2 \theta_1}
 \end{aligned}$$

For $m_1 < m_2$, only one soln. Take + sign so that

$$\chi \approx 0 \leftrightarrow \theta_1 \approx 0$$

$$\left(\cos \theta = -\left(\frac{m_1}{m_2}\right) \theta + \sqrt{1 - \left(\frac{m_1}{m_2}\right)^2 \theta^2} = 1 \right)$$

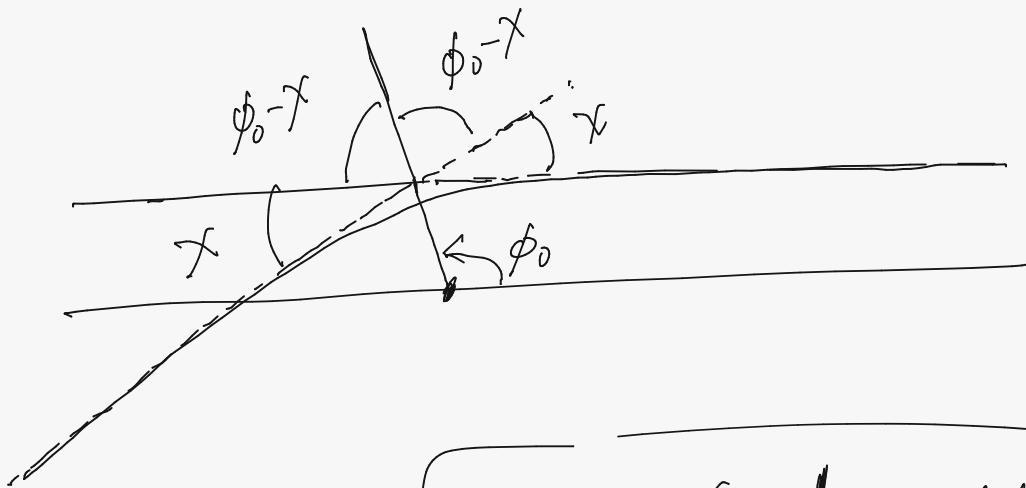
5)



repulsive scattering

$$2\phi_0 + \chi = \pi$$

$$\chi = \pi - 2\phi_0$$



$$2(\phi_0 - \chi) + \chi = \pi$$

$$2\phi_0 - \chi = \pi$$

$$\chi = 2\phi_0 - \pi$$

so $\chi = |\pi - 2\phi_0|$

6) Relate the impact parameter ρ and initial velocity v_∞ to the energy E and angular momentum ℓ .

Relation:

$$E = \frac{1}{2}mv_\infty^2, \quad \ell = m\rho v_\infty$$

where m is the reduced mass of the system $m \equiv m_1m_2/(m_1 + m_2)$.

7) Derive an integral expression for ϕ_0 and solve it for simple potentials---e.g., $U(r) = \alpha/r$ for Rutherford scattering.

Start with the central force differential equation for ϕ :

$$d\phi = \frac{\ell dr/r^2}{\sqrt{2m(E - U(r)) - \frac{\ell^2}{r^2}}}$$

Integrate the LHS from 0 to ϕ_0 and the RHS from r_{\min} to ∞ :

$$\phi_0 = \int_{r_{\min}}^{\infty} \frac{\ell dr/r^2}{\sqrt{2m(E - U(r)) - \frac{\ell^2}{r^2}}}$$

If we substitute for E and ℓ using

$$E = \frac{1}{2}mv_\infty^2, \quad \ell = m\rho v_\infty$$

we obtain

$$\phi_0 = \int_{r_{\min}}^{\infty} \frac{\rho dr/r^2}{\sqrt{1 - \frac{2U(r)}{mv_\infty^2} - \frac{\rho^2}{r^2}}}$$

Rutherford scattering:

Take $U(r) = \alpha/r$. Note that $\alpha > 0$ corresponds to repulsive scattering and $\alpha < 0$ to attractive scattering.

Similar to what we did when solving for the orbit for Kepler's problem, make the substitution $u = \rho/r$. Then $du = -\rho dr/r^2$ and

$$\phi_0 = \int_0^{\rho/r_{\min}} \frac{du}{\sqrt{1 - \frac{2\alpha}{\rho mv_\infty^2}u - u^2}}$$

Again we can complete the square for the quadratic in the square root leading to a trig substitution of the form

$$u + A = B \sin \theta, \quad A \equiv \frac{\alpha}{\rho mv_\infty^2}, \quad B \equiv \sqrt{1 + A^2}$$

which allows us to evaluate the integral:

$$\phi_0 = \cos^{-1} \frac{\alpha/\rho mv_\infty^2}{\sqrt{1 + \left(\frac{\alpha}{\rho mv_\infty^2}\right)^2}}$$

For calculating the differential cross section (see below), it is useful to find an explicit relationship between the impact parameter ρ and scattering angle χ . Using the above expression for ϕ_0 , we get

$$\rho = \frac{|\alpha|}{mv_\infty^2} \tan \phi_0$$

Then using

$$\phi_0 = \frac{\pi}{2} \mp \frac{\chi}{2}$$

we have

$$\rho = \frac{|\alpha|}{mv_\infty^2} \cot\left(\frac{\chi}{2}\right)$$

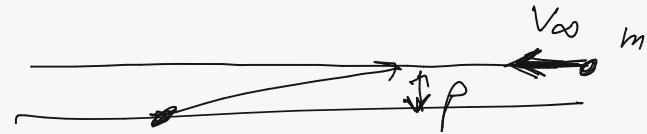
8) Write down expressions for $d\sigma$ in terms of $d\rho$, $d\chi$, $d\theta_1$, $d\theta_2$, or $d\Omega$, $d\Omega_1$, $d\Omega_2$.

Differential cross section:

$$d\sigma = 2\pi\rho d\rho \quad (\text{differential area of annular region})$$

$$6.) \quad E, M \quad v.s. \quad \rho, V_\infty$$

$$E = \frac{1}{2} m V_\infty^2, \quad M = m \rho V_\infty$$



$$|m \vec{r} \times \vec{v}| = m \rho V_\infty$$

7)



$$M = m r^2 \dot{\phi} = \frac{\partial L}{\partial \dot{\phi}}$$

$$E = \frac{1}{2} m (\dot{r}^2 + r^2 \dot{\phi}^2) + U(r)$$

$$\dot{\phi} = \frac{M}{mr^2}$$

$$= \frac{1}{2} m \dot{r}^2 + \frac{M^2}{2mr^2} + U(r)$$

$$\dot{\phi}^2 = \frac{M^2}{m^2 r^4}$$

$$\pm \sqrt{\frac{2}{m} \left(E - U(r) - \frac{M^2}{2mr^2} \right)} = \frac{dr}{dt} = \frac{dr}{d\phi} \dot{\phi} = \frac{M}{mr^2} \frac{dr}{d\phi}$$

$$\rightarrow \int d\phi = \pm \int \frac{dr/r^2}{\left(\frac{m}{M}\right) \sqrt{\frac{2}{m} (E - U(r)) - \frac{M^2}{m^2 r^2}}} + \text{const} = \pm \int \frac{Md\phi}{\sqrt{\frac{2m(E-U(r))}{M^2} - \frac{M^2}{r^2}}} + \text{const}$$

$$\int_0^{\phi_0} d\phi = \oint_{\text{closed loop}} \frac{M dr/r^2}{\sqrt{2m(E-U(r)) - \frac{M^2}{r^2}}}$$

closed loop

$$\phi_0 = \int_{r_{min}}^{\infty} \frac{M dr/r^2}{\sqrt{2m(E-U(r)) - \frac{M^2}{r^2}}}$$

$\phi = 0 \text{ at } r = r_{min}$

Substitute $E = \frac{1}{2} m v_\infty^2$, $M = m p v_\infty$

$$\phi_0 = \int_{r_{min}}^{\infty} \frac{m p v_\infty dr/r^2}{\sqrt{m^2 v_\infty^2 - 2m U(r)} = \frac{m^2 p^2 v_\infty^2}{r^2}}$$

$$= \int_{r_{min}}^{\infty} \frac{m p v_\infty dr/r^2}{\cancel{m v_\infty} \sqrt{1 - \left(\frac{\cancel{m} U(r)}{\frac{1}{2} m v_\infty^2} \right)} = \frac{p^2}{r^2}}$$

$$= \int_{r_{min}}^{\infty} \frac{p dr/r^2}{\sqrt{1 - \frac{p^2}{r^2} - \frac{2U(r)}{m v_\infty^2}}}$$

Tate: $U(r) = \frac{\alpha}{r}$

$\alpha > 0$	\rightarrow	repulsive
$\alpha < 0$	\rightarrow	attractive

Let $u = \frac{1}{r}$, $du = -\frac{1}{r^2} dr$

$$\begin{aligned}
 \phi_v &= \int_0^{\frac{1}{r_{min}}} \frac{-\rho dy}{\sqrt{1 - \rho^2 y^2 - \frac{2\alpha u}{m v_\infty^2}}} \\
 &= \int_0^{\frac{1}{r_{min}}} \frac{\rho dy}{\sqrt{-\rho^2 y^2 - \frac{2\alpha u}{m v_\infty^2} + 1}} \\
 &= \int_0^{\frac{1}{r_{min}}} \frac{\rho dy}{\sqrt{-\rho^2 \left(u^2 + \frac{2\alpha u}{m \rho^2 v_\infty^2} - \frac{1}{\rho^2}\right)}} \\
 &= \int_0^{\frac{1}{r_{min}}} \frac{dy}{\sqrt{-\left[\left(u + \frac{\alpha}{m \rho^2 v_\infty^2}\right)^2 - \frac{1}{\rho^2} - \frac{\alpha^2}{m^2 \rho^4 v_\infty^4}\right]}}
 \end{aligned}$$

$$\phi_0 = \int_0^{\frac{1}{r_{min}}} \frac{dy}{\sqrt{B^2 - (u-A)^2}}$$

where: $A = -\frac{\alpha}{mp^2 v_\infty^2} < 0$

$$B^2 \equiv \frac{1}{p^2} + A^2$$

$$\text{Let } u - A = B \sin \theta$$

$$\rightarrow \sqrt{B^2 - (u-A)^2} = B \cos \theta$$

$$\frac{B^2 - (\frac{u-A}{r_{min}})^2 = 0 \Rightarrow \frac{1}{r_{min}} - A = B}{\sin^2 \theta + \cos^2 \theta = 1}$$

$$du = B \cos \theta \ d\theta$$

$$\phi_0 = \int_{u=0}^{u=\frac{1}{r_{min}}} \frac{B \cos \theta \ d\theta}{B \cos \theta} = \sin^{-1} \left(\frac{u-A}{B} \right) \Big|_0^{\frac{1}{r_{min}}}$$

$$= \sin^{-1} \left(\underbrace{\frac{\frac{1}{r_{min}} - A}{B}}_1 \right) - \sin^{-1} \left(\frac{-A}{B} \right)$$

$$= \frac{\pi}{2} - \sin^{-1} \left(\frac{\frac{\alpha}{mp^2 v_\infty^2}}{\sqrt{\frac{1}{p^2} + \frac{\alpha^2}{m^2 p^4 v_\infty^4}}} \right)$$

$$\sin(\equiv) = \frac{\pi}{2} - \phi_0$$

$$(\equiv) = \sin\left(\frac{\pi}{2} - \phi_0\right) = \sin\frac{\pi}{2} \cos\phi_0 - \cos\frac{\pi}{2} \sin\phi_0 \\ = \cos\phi_0$$

$$\Gamma_{h\nu_1} \frac{\frac{\alpha}{m\rho^2 v_\infty^2}}{\sqrt{\frac{1}{\rho^2} + \frac{\alpha^2}{m^2 \rho^4 v_\infty^4}}} = (\omega)\phi_0$$

$$\rightarrow \boxed{(\omega)\phi_0 = \frac{\frac{\alpha}{m\rho v_\infty^2}}{\sqrt{1 + \left(\frac{\alpha}{m\rho v_\infty^2}\right)^2}}}$$

W_{out}: $\rho = \rho(x)$

——— recall : $x = \pi - 2\phi_0$ (repulsive)
 $x = 2\phi_0 - \pi$ (attractive)

$\rightarrow \phi_0 = \frac{\pi - x}{2}$

$$\cos^2 \phi_0 \left(1 + \left(\frac{\alpha}{\rho m v_\infty^2} \right)^2 \right) = \left(\frac{\alpha}{\rho m v_\infty^2} \right)^2$$

$$\cos^2 \phi_0 = \left(\frac{\alpha}{\rho m v_\infty^2} \right)^2 \left(1 - \cos^2 \phi_0 \right)$$

$\sin^2 \phi_0$

$$\boxed{\rho = \frac{|\alpha|}{m v_\infty^2} \tan \phi_0}$$

$$\tan \phi_0 = \tan \left(\frac{\pi}{2} - \frac{x}{2} \right) = \frac{\sin \left(\frac{\pi}{2} \right) \cos \left(\frac{x}{2} \right) - \cos \left(\frac{\pi}{2} \right) \sin \left(\frac{x}{2} \right)}{\cos \left(\frac{\pi}{2} \right) \cos \left(\frac{x}{2} \right) + \sin \left(\frac{\pi}{2} \right) \sin \left(\frac{x}{2} \right)}$$

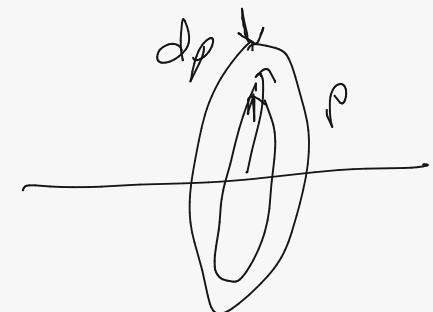
$$= \cot \left(\frac{x}{2} \right)$$

$$S_0 \quad \rho = \frac{|\alpha|}{m v_\infty^2} \cot\left(\frac{x}{2}\right)$$

8.) $d\sigma$ in terms of $d\rho, dx, d\theta_1, d\theta_2, d\Omega_2, d\Omega_1, d\Omega$
 $\underbrace{d\Omega_2, d\Omega_1, d\Omega}_{\text{solid angle}}$

$$d\sigma = 2\pi \int d\rho$$

$$d\sigma = 2\pi \rho(x) \left| \frac{d\rho}{dx} \right| dx$$

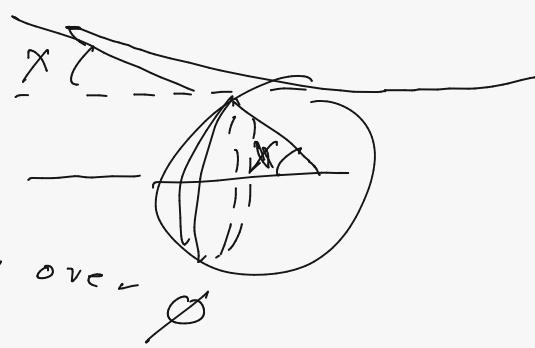


$$d\sigma_1 = 2\pi \left| \frac{d\rho}{d\theta_1} \right| d\theta_1, \quad \text{using } x = x(\theta_1)$$

$$d\sigma_2 = 2\pi \rho(\theta_1) \left| \frac{d\rho}{d\theta_2} \right| d\theta_2$$

$$d\Omega = 2\pi \sin x dx$$

integrating over



$$\frac{d\sigma}{d\Omega} = \frac{\rho(x)}{\sin x} \left| \frac{d\rho}{dx} \right| = \rho(x) \left| \frac{d\rho}{d(\cos x)} \right|$$

$$\text{Similarly, } \frac{d\sigma}{d\Omega_1} = \rho(\theta_1) \left| \frac{d\rho}{d(\cos\theta_1)} \right|$$

$$\frac{d\sigma}{d\Omega_2} = \rho(\theta_2) \left| \frac{d\rho}{d(\cos\theta_2)} \right|$$

$$\begin{aligned} \frac{d\sigma}{d\Omega} &= \rho(x) \left| \frac{d\rho}{d(\cos x)} \right| = \rho \left| \frac{d\rho}{d(\cos\theta_1)} \right| \left| \frac{d(\cos\theta_1)}{d(\cos x)} \right| \\ &= \frac{d\sigma_1}{d\Omega_1} \left| \frac{d(\cos\theta_1)}{d(\cos x)} \right| \end{aligned}$$

$\boxed{\frac{d\sigma_1}{d\Omega_1} = \frac{d\sigma}{d\Omega} \left| \frac{d(\cos x)}{d(\cos\theta_1)} \right|}$

and similarly
for θ_2

$$\text{Using: } (i) \cos \chi = -\cos(2\theta_2)$$

$$(ii) \cos \chi = -\left(\frac{m_1}{m_2}\right) \sin^2 \theta_1 \pm \cos \theta_1 \sqrt{1 - \left(\frac{m_1}{m_2}\right)^2 \sin^2 \theta_1}$$

we have

$$\begin{aligned} d(\cos \chi) &= +2 \sin(2\theta_2) d\theta_2 \\ &= 4 \sin \cancel{\theta_2} \cos \theta_2 d\theta_2 \\ &= -4 \cos \theta_2 d(\cos \theta_2) \end{aligned}$$

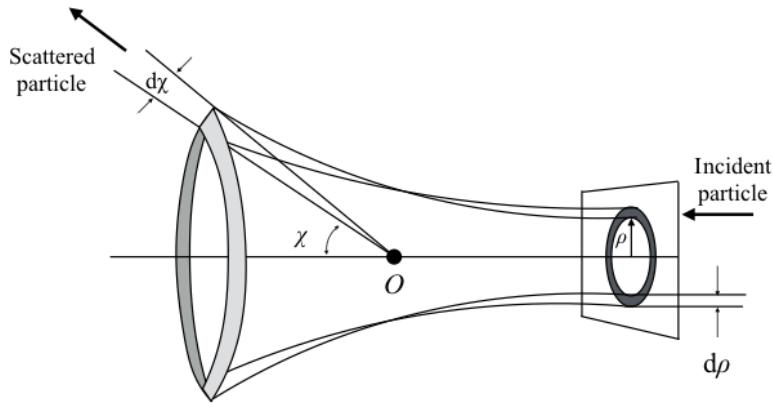
$$SV \boxed{\left| \frac{d(\cos \chi)}{d(\cos \theta_2)} \right| = 4 \cos \theta_2}$$

$$\begin{aligned} \text{And: } d(\cos \chi) &= -2 \left(\frac{m_1}{m_2}\right) \sin \theta_1 \cos \theta_1 d\theta_1 \\ &\quad \pm d(\cos \theta_1) \sqrt{1 - \left(\frac{m_1}{m_2}\right)^2 \sin^2 \theta_1} \cancel{\frac{1}{2}} \cancel{\left(\frac{m_1}{m_2}\right)^2} \cancel{\sin \theta_1 \cos \theta_1} d\theta_1 \\ &= +2 \left(\frac{m_1}{m_2}\right) \cos \theta_1 d(\cos \theta_1) \pm d(\cos \theta_1) \sqrt{1 - \left(\frac{m_1}{m_2}\right)^2 \sin^2 \theta_1} \end{aligned}$$

$$d(\cos\chi) = d(\cos\theta_1) \left[2 \left(\frac{m_1}{m_2} \right) \cos\theta_1 \pm \frac{\left(1 - \left(\frac{m_1}{m_2} \right)^2 \sin^2\theta_1 + \left(\frac{m_1}{m_2} \right)^2 \cos^2\theta_1 \right)}{\sqrt{1 - \left(\frac{m_1}{m_2} \right)^2 \sin^2\theta_1}} \right]$$

$$= d(\cos\theta_1) \left[2 \left(\frac{m_1}{m_2} \right) \cos\theta_1 \pm \frac{1 - \left(\frac{m_1}{m_2} \right)^2 \cos 2\theta_1}{\sqrt{1 - \left(\frac{m_1}{m_2} \right)^2 \sin^2\theta_1}} \right]$$





In the COM frame:

$$d\Omega = 2\pi \sin \chi d\chi = 2\pi d(\cos \chi) \quad (\text{solid angle})$$

$$\frac{d\sigma}{d\Omega} = \frac{\rho}{\sin \chi} \left| \frac{d\rho}{d\chi} \right| = \rho \left| \frac{d\rho}{d(\cos \chi)} \right| \quad (\text{absolute value to keep things positive})$$

In the lab frame (for particle 1):

$$d\Omega_1 = 2\pi \sin \theta_1 d\theta_1 = 2\pi d(\cos \theta_1)$$

$$\frac{d\sigma_1}{d\Omega_1} = \frac{\rho}{\sin \theta_1} \left| \frac{d\rho}{d\theta_1} \right| = \rho \left| \frac{d\rho}{d(\cos \theta_1)} \right| = \frac{d\sigma}{d\Omega} \left| \frac{d(\cos \chi)}{d(\cos \theta_1)} \right|$$

which implies

$$d\sigma_1 = \frac{d\sigma}{d\Omega} \left| \frac{d(\cos \chi)}{d(\cos \theta_1)} \right| d\Omega_1 \quad \text{where} \quad d\Omega_1 = 2\pi \sin \theta_1 d\theta_1$$

The same applies for $d\theta_2, d\Omega_2$.

Thus we need to be able to calculate quantities like $d(\cos \chi)/d(\cos \theta_1)$ and $d(\cos \chi)/d(\cos \theta_2)$.

Recall:

$$\cos \chi = -\left(\frac{m_1}{m_2}\right) \sin^2 \theta_1 \pm \cos \theta_1 \sqrt{1 - \left(\frac{m_1}{m_2}\right)^2 \sin^2 \theta_1}$$

and

$$\chi = \pi - 2\theta_2 \Rightarrow \cos \chi = \cos(\pi - 2\theta_2) = -\cos(2\theta_2)$$

for which

$$d(\cos \chi) = d(\cos \theta) \left[2 \left(\frac{m_1}{m_2} \right) \cos \theta_1 \pm \frac{\left(1 + \left(\frac{m_1}{m_2} \right)^2 \cos^2(2\theta_1) \right)}{\sqrt{1 - \left(\frac{m_1}{m_2} \right)^2 \sin^2 \theta_1}} \right]$$

and

$$d(\cos \chi) = -d(\cos(2\theta_2)) = -4 \cos \theta_2 d(\cos \theta_2)$$

9) Explain how one can obtain an expression for small-angle scattering starting from the integral equation for ϕ_0 .

Recall:

$$\phi_0 = \int_{r_{\min}}^{\infty} \frac{\rho dr / r^2}{\sqrt{1 - \frac{2U(r)}{mv_\infty^2} - \frac{\rho^2}{r^2}}}$$

Small-angle scattering corresponds to

$$\epsilon \equiv -\frac{2U(r)}{mv_\infty^2} \ll 1$$

We expect ϕ_0 to deviate slightly from the $U(r) \rightarrow 0$ value of $\phi_0 = \pi/2$.

Expand the factor of $1/\sqrt{1 - \rho^2/r^2 + \epsilon}$ in the integrand:

$$\frac{1}{\sqrt{1 - \rho^2/r^2 + \epsilon}} = \frac{1}{\sqrt{(1 - \rho^2/r^2) \left[1 + \frac{\epsilon}{1 - \rho^2/r^2} \right]}} \approx \frac{1}{\sqrt{1 - \rho^2/r^2}} \left[1 - \frac{1}{2} \frac{\epsilon}{1 - \rho^2/r^2} \right] = \frac{1}{\sqrt{1 - \rho^2/r^2}} -$$

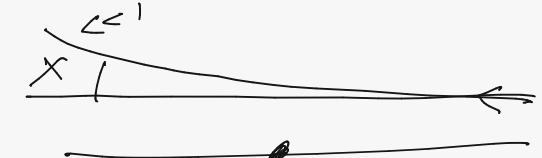
The first term when multiplied by $\rho dr/r^2$ and integrated from r_{\min} to ∞ gives $\pi/2$.

The second term when multiplied by $\rho dr/r^2$ and integrated from r_{\min} to ∞ gives

$$-\frac{1}{2} \int_{r_{\min}}^{\infty} \frac{\epsilon \rho dr / r^2}{(1 - \rho^2/r^2)^{3/2}} \approx \frac{1}{mv_\infty^2} \int_{\rho}^{\infty} \frac{U(r) \rho dr / r^2}{(1 - \rho^2/r^2)^{3/2}}$$

where we have substituted for ϵ and replaced the limit r_{\min} by ρ to get the last approximate equality.

$$9) \quad \phi_0 = \int_{r_{min}}^{\infty} \frac{\rho dr / r^2}{\sqrt{1 - \frac{2U(r)}{mV_\infty^2} - \frac{\rho^2}{r^2}}}$$



Small-angle scattering: $\frac{U(r)}{mV_\infty^2} \ll 1$

$$r_{min} \approx \rho$$

$$\phi_0 = \int_{r_{min} \approx \rho}^{\infty} \frac{\rho dr / r^2}{\sqrt{1 - \frac{\rho^2}{r^2}} \sqrt{1 - \frac{2U(r)}{mV_\infty^2(1 - \frac{\rho^2}{r^2})}}}$$

$$\approx \int_{\rho}^{\infty} \frac{\rho dr / r^2}{\sqrt{1 - \frac{\rho^2}{r^2}}} \left(1 + \frac{1}{2} \frac{2U(r)}{mV_\infty^2(1 - \frac{\rho^2}{r^2})} \right)$$

$$= \int_{\rho}^{\infty} \frac{\rho dr / r^2}{\sqrt{1 - \frac{\rho^2}{r^2}}} + \frac{\rho}{mV_\infty^2} \int_{\rho}^{\infty} \frac{U(r) dr / r^2}{(1 - \frac{\rho^2}{r^2})^{3/2}}$$

Now:

$$\int_{\rho}^{\infty} \frac{\rho dr/r^2}{\sqrt{1 - (\rho/r)^2}} = - \int_1^0 \frac{du}{\sqrt{1-u^2}} = \int_0^1 \frac{du}{\sqrt{1-u^2}}$$

Let $u = \frac{\rho}{r} \rightarrow du = -\frac{\rho}{r^2} dr$

$$= \sin^{-1}(1)$$

$$= \frac{\pi}{2}$$

$$\boxed{\phi_0 = \frac{\pi}{2}}$$

Thus, $\phi_0 \approx \frac{\pi}{2} + \frac{\rho}{mv_\infty^2} \int_{\rho}^{\infty} \frac{U(r) dr/r^2}{(1 - \rho^2/r^2)^{3/2}}$

$$= \frac{\pi}{2} + \left(\frac{1}{mv_\infty^2}\right) \int_{\rho}^{\infty} dr \frac{1}{\rho} \frac{\partial}{\partial \rho} \left[\frac{U(r)}{\sqrt{1 - \rho^2/r^2}} \right]$$
$$= \frac{\pi}{2} + \left(\frac{1}{mv_\infty^2}\right) \frac{1}{\rho} \left[\int_{\rho}^{\infty} dr \frac{U(r)}{\sqrt{1 - \rho^2/r^2}} \right]$$

$\left. -\frac{1}{2} \left(\frac{-2\rho}{r^2}\right) \right]$

Now:

$$\int_{\rho}^{\infty} dr \frac{U(r)}{\sqrt{1 - \rho^2/r^2}}$$

Let: $u = U(r)$, $du = \frac{dr}{\sqrt{1 - \rho^2/r^2}}$ $\rightarrow du = \frac{dU}{dr} dr$

$$V = \int \frac{dr}{\sqrt{1 - \rho^2/r^2}} = \int \frac{r dr}{\sqrt{r^2 - \rho^2}} = \int \frac{dx/2}{\sqrt{x}} = x^{\frac{1}{2}}$$

$$x = r^2 - \rho^2$$

$$dx = 2r dr$$

Since $U(r) \rightarrow 0$ faster than $1/r$

$$\text{In } V, \quad V = \sqrt{r^2 - \rho^2}$$

$$\rightarrow \int_{\rho}^{\infty} dr \frac{U(r)}{\sqrt{1 - \rho^2/r^2}} = U(r) \sqrt{r^2 - \rho^2} \Big|_{\rho}^{\infty} - \int_{\rho}^{\infty} \left(\frac{dU}{dr} \right) \sqrt{r^2 - \rho^2} dr$$

$$\int_0^{\omega} \left[\dot{\phi}_0 \right] \simeq \frac{\pi}{2} - \frac{1}{mv_0^2} \frac{\partial}{\partial p} \left[\int_p^{\omega} dr - \frac{dU}{dr} \sqrt{r^2 - p^2} \right] dr$$

$$= \frac{\pi}{2} + \frac{p}{mv_0^2} \int_p^{\omega} \frac{dr}{r \sqrt{r^2 - p^2}} \frac{dU/dr}{}$$

~~$$\frac{1}{2\sqrt{r}} (-2\rho)$$~~

$$= -\frac{p}{\sqrt{r}}$$

Thus,

$$\phi_0 \approx \frac{\pi}{2} + \frac{1}{mv_\infty^2} \int_{\rho}^{\infty} \frac{U(r)\rho dr/r^2}{(1-\rho^2/r^2)^{3/2}} = \frac{\pi}{2} + \frac{1}{mv_\infty^2} \frac{\partial}{\partial \rho} \left[\int_{\rho}^{\infty} \frac{U(r)dr}{\sqrt{1-\rho^2/r^2}} \right]$$

Now the integral

$$I \equiv \int_{\rho}^{\infty} \frac{U(r)dr}{\sqrt{1-\rho^2/r^2}}$$

can be integrated by parts setting

$$u = U(r), \quad dv = \frac{dr}{\sqrt{1-\rho^2/r^2}} = \frac{r dr}{\sqrt{r^2-\rho^2}}$$

for which

$$du = \frac{dU}{dr} dr, \quad v = \sqrt{r^2 - \rho^2}$$

where the last result was obtained making the substitution $x = r^2 - \rho^2$ to do the integral for v .

Thus,

$$I = U(r) \sqrt{r^2 - \rho^2} \Big|_{\rho}^{\infty} - \int_{\rho}^{\infty} dr \frac{dU}{dr} \sqrt{r^2 - \rho^2} = - \int_{\rho}^{\infty} dr \frac{dU}{dr} \sqrt{r^2 - \rho^2}$$

where the first term vanishes assuming $U(r) \rightarrow 0$ faster than $1/r$ as $r \rightarrow \infty$.

Substituting I back into the expression for ϕ_0 gives

$$\phi_0 \approx \frac{\pi}{2} - \frac{1}{mv_\infty^2} \frac{\partial}{\partial \rho} \left[\int_{\rho}^{\infty} dr \frac{dU}{dr} \sqrt{r^2 - \rho^2} \right] = \frac{\pi}{2} + \frac{\rho}{mv_\infty^2} \int_{\rho}^{\infty} dr \frac{dU}{dr} \frac{1}{\sqrt{r^2 - \rho^2}}$$

which is the desired result.

6. Small oscillations (21-23)

1) Explain what stable equilibrium means in terms of the potential energy $U(q)$.

Stable equilibrium means there exists a local minimum at some q_0 :

$$\frac{dU}{dq} \Big|_{q_0} = 0, \quad \frac{d^2U}{dq^2} \Big|_{q_0} > 0$$

(6.)

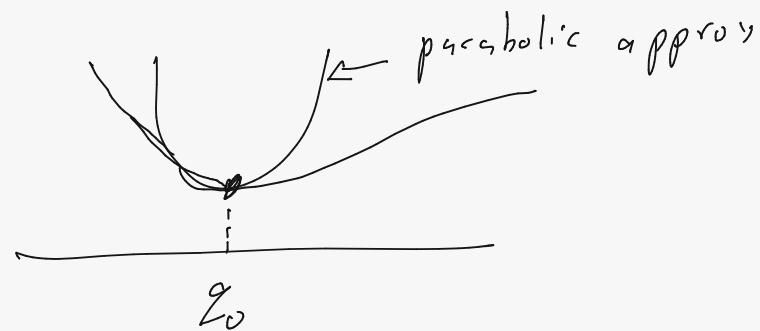
1)

stable equiv at $q = q_0$ means

$$H = d^2$$

$$U'(q_0) = 0$$

$$U''(q_0) \equiv K > 0$$



$$U(q) = U(q_0) + \cancel{U'(q_0)(q - q_0)} + \frac{1}{2} (q - q_0)^2 U''(q_0) + \dots$$

$$= U(q_0) + \frac{1}{2} K (q - q_0)^2$$

$$= \text{const} + \frac{1}{2} K x^2$$

$$x = q - q_0$$

2) Calculate the frequency for small oscillations about a position of stable equilibrium.

Lagrangian:

$$L = \frac{1}{2}a(q)\dot{q}^2 - U(q)$$

Let q_0 be a position of stable equilibrium, and define

$$x \equiv q - q_0$$

which implies $\dot{x} = \dot{q}$.

Then for small deviations around q_0 ,

$$U(q) = U(q_0) + \frac{dU}{dq}\Big|_{q_0}(q - q_0) + \frac{1}{2}\frac{d^2U}{dq^2}\Big|_{q_0}(q - q_0)^2 + \dots \approx U_0 + \frac{1}{2}kx^2$$

where

$$U_0 \equiv U(q_0), \quad k \equiv \frac{d^2U}{dq^2}\Big|_{q_0}$$

So for small deviations around q_0

$$L = \frac{1}{2}m\dot{x}^2 - \frac{1}{2}kx^2$$

where $m \equiv a(q_0)$ and we have dropped the constant U_0 from the Lagrangian.

Lagrange's equation:

$$\frac{d}{dt}\left(\frac{\partial L}{\partial \dot{x}}\right) = \frac{\partial L}{\partial x}$$

gives

$$m\ddot{x} = -kx$$

which has general solution

$$x = c_1 \cos(\omega t) + c_2 \sin(\omega t), \quad \omega \equiv \sqrt{\frac{k}{m}}$$

3) Solve the equations of motion for both free and forced oscillation in one dimension, noting the difference between the general solution of the homogeneous equation and a particular integral of the inhomogeneous equation.

From the previous part we saw that the EOMs for free oscillations is

$$m\ddot{x} = -kx$$

which has general solution

$$x = c_1 \cos(\omega t) + c_2 \sin(\omega t), \quad \omega \equiv \sqrt{\frac{k}{m}}$$

This solution can also be written as

$$x = a \cos(\omega t + \alpha)$$

where

$$a = \sqrt{c_1^2 + c_2^2}, \quad \tan \alpha = -c_2/c_1$$

or as the real part of a complex solution

$$x = \operatorname{re}[A e^{i\omega t}], \quad A = a e^{i\alpha}$$

Forced oscillations:

$$m\ddot{x} = -kx + F(t)$$

or, equivalently,

$$\ddot{x} + \omega^2 x = \frac{F(t)}{m}$$

where $\omega \equiv \sqrt{k/m}$.

This 2nd-order ODE for $x(t)$ can be converted to a 1st-order ODE by defining

$$\xi \equiv \dot{x} + i\omega x$$

for which

$$\dot{\xi} = \ddot{x} + i\omega \dot{x}$$

and

$$2) L = \frac{1}{2} a(q) \dot{q}^2 - U(q)$$

$$U(q) = U(q_0) + \frac{1}{2} \frac{\partial U}{\partial q}(q-q_0)^2 + \dots$$

ignore where $x \equiv q - q_0$

$$= \text{const} + \frac{1}{2} \frac{\partial U}{\partial q} x^2$$

$$a(q) \dot{q}^2 = a(q) \dot{x}^2 \approx a(q_0) \dot{x}^2 \equiv mx^2$$

$$L = \frac{1}{2} m \dot{x}^2 - \frac{1}{2} \frac{\partial U}{\partial q} x^2$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}} \right) = \frac{\partial L}{\partial x} \rightarrow m \ddot{x} = - \frac{\partial U}{\partial q} x$$

$$\ddot{x} = - \frac{\frac{\partial U}{\partial q}}{m} x = - \omega^2 x, \quad \omega \equiv \sqrt{\frac{\frac{\partial U}{\partial q}}{m}}$$

$$x(t) = c_1 \cos \omega t + c_2 \sin \omega t$$

$$= a \cos(\omega t + \alpha)$$

$$= \operatorname{Re} [A e^{i \omega t}]$$

$$A \equiv \begin{matrix} \cos \omega t \\ \sin \omega t \end{matrix}$$

$$= a e^{i \alpha}$$

$$a(\cos \omega t \cos \alpha - \sin \omega t \sin \alpha) = c_1 \cos \omega t + c_2 \sin \omega t$$

$$c_1 = a \cos \alpha, \quad c_2 = -a \sin \alpha$$

$$a^2 = c_1^2 + c_2^2$$

$$\frac{c_1}{c_2} = - \frac{\cos \alpha}{\sin \alpha}$$

$$\tan \alpha = - \frac{c_2}{c_1}$$

3) Free oscillations:

$$\begin{aligned}x(t) &= c_1 \cos \omega t + c_2 \sin \omega t \\&= a \cos(\omega t + \alpha) \\&= \operatorname{Re}[A e^{i\omega t}] \quad , \quad A : \text{complex}\end{aligned}$$

Forced oscillations:

$$L = \frac{1}{2} m \dot{x}^2 - \frac{1}{2} \kappa x^2 + x F(t)$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}} \right) = \frac{\partial L}{\partial x}$$

$$\frac{d}{dt}(m \dot{x}) = -\kappa x + F(t)$$

$$m \ddot{x} = -\kappa x + F(t)$$

$$\ddot{x} = -\frac{\kappa}{m} x + \frac{F(t)}{m}$$

$$\boxed{\ddot{x} + \omega^2 x = \frac{F(t)}{m}}$$

General Solution \Leftarrow particular + homog

Rewrite: $\tilde{z} = \dot{x} + i\omega x \Rightarrow \tilde{z} = \ddot{x} + i\omega \dot{x}$

$$\rightarrow i\omega \tilde{z} = i\omega \dot{x} - \omega^2 x \quad \text{Thus,} \quad \tilde{z} - i\omega \tilde{z} = \ddot{x} + \cancel{i\omega \dot{x}} - \cancel{-i\omega \tilde{z}} + \omega^2 x = \frac{F(t)}{m}$$

$$\zeta - i\omega \xi = \frac{F(t)}{m}$$

1st order equation of the form:

$$y' + P(x)y = Q(x)$$

$$dy + (P(x)y - Q(x)) dx = 0$$

not "exact differential" since "exact" means:

$$A(x,y) dx + B(x,y) dy = dU = \frac{\partial U}{\partial x} dx + \frac{\partial U}{\partial y} dy$$

$$\frac{\partial^2 U}{\partial y \partial x} = \frac{\partial^2 U}{\partial x \partial y} \rightarrow \frac{\partial A}{\partial y} = \frac{\partial B}{\partial x}$$

$$\frac{\partial}{\partial y} [P(x)y - Q(x)] = P(x)$$

$$\frac{\partial}{\partial x} 1 = 0$$

not equal

But can find an integrating factor $\mu(x)$ such that:

$$\mu(x) \left[dy + (P(x)y - Q(x)) dx \right] = dU$$

$$= \frac{\partial U}{\partial x} dx + \frac{\partial U}{\partial y} dy$$

$$\frac{\partial U}{\partial x} = (P(x)y - Q(x)) \mu(x)$$

$$\frac{\partial U}{\partial y} = \mu(x)$$

$$\frac{d\mu}{dx} = \frac{\partial}{\partial y} [\mu(x) (P(x)y - Q(x))] \quad \leftarrow \quad \frac{\partial^2 U}{\partial x \partial y} = \frac{\partial^2 U}{\partial y \partial x}$$

$$\frac{d\mu}{dx} = \mu(x) P(x)$$

$$\frac{d\mu}{\mu} = P(x) dx \quad \rightarrow \quad \ln \mu = \int P(x) dx \equiv I$$

$$\mu(x) = e^{\int^x P(\hat{x}) d\hat{x}} = e^{I(x)}$$

$$\frac{\partial U}{\partial y} = \mu(x) \rightarrow U(x, y) = \mu(x)y + g(x)$$

$$\frac{\partial U}{\partial x} = \mu(x) (P(x)_y - Q(x)) \rightarrow \left(\frac{d\mu}{dx} \right)_y + g'(x) = \mu(x) (P(x)_y - Q(x))$$

~~$\mu(x) P(x)_y + g'(x)$~~ = ~~$\mu(x) P(x)_y - \mu(x) Q(x)$~~

$$g'(x) = -\mu(x) Q(x)$$

$$g'(x) = -e^{\int x} Q(x)$$

$$g(x) = - \int dx Q(x) e^{\int x}$$

Then $U(x, y) = e^{\int x} y - \int dx Q(x) e^{\int x}$

solution $U(x, y) = C = \text{const}$ since then $dU = 0$

$$C = e^{\int x} y - \int dx Q(x) e^{\int x}$$

$$y = e^{-\int P(x) dx} \left[C + \int dx Q(x) e^{\int P(x) dx} \right]$$

↑
general solution of
 $y' + P(x)y = Q(x)$

$$\int P(x) dx$$

check:

$$\begin{aligned}
 y' &= -P(x) e^{-\int P(x) dx} \left[C + \int dx Q(x) e^{\int P(x) dx} \right] \\
 &\quad + e^{-\int P(x) dx} Q(x) e^{\int P(x) dx} \\
 &= -P(x) y + Q(x) \quad \checkmark
 \end{aligned}$$

Compare $y' + P(x)y = Q(x)$ to $\xi - i\omega \xi = F(t)$

$$\xi(t) = e^{i\omega t} \left[\xi_0 + \int_0^t dt \frac{F(\bar{t})}{m} e^{-i\omega \bar{t}} \right]$$

homog. solution complex particular solution

$$\left. \begin{aligned}
 I(t) &= \int_{-i\omega}^t dt \\
 &= -i\omega t
 \end{aligned} \right\}$$

Alternative approach:

$$\ddot{\xi} - i\omega \dot{\xi} = \frac{F(t)}{m}$$

Homog: $\ddot{\xi} - i\omega \dot{\xi} = 0 \rightarrow \dot{\xi} = i\omega \xi$

$$\int \frac{d\xi}{\xi} = \int i\omega dt$$

$$\ln \xi = i\omega t + \text{const}$$

$$\boxed{\xi(t) = \xi_0 e^{i\omega t}}$$

Particular: for $F(t) = F_0 e^{i\omega' t}$

Assume: $\xi_p(t) = A e^{i\omega' t}$

$$A i\omega' e^{i\omega' t} - i\omega A e^{i\omega' t} = \frac{F_0}{m} e^{i\omega' t}$$

$$iA(\omega' - \omega) = \frac{F_0}{m} \rightarrow A = \frac{F_0}{im(\omega' - \omega)}$$

so $\boxed{\xi_p(t) = \frac{F_0}{im(\omega' - \omega)} e^{i\omega' t}}$ (particular solution)

Can add / subtract homog. solution so that $\tilde{x}_p(t=0) = 0$

$$\Rightarrow \tilde{x}_p(t) = \frac{F_0}{im(\omega' - \omega)} \left(e^{i\omega' t} - e^{i\omega t} \right)$$

\uparrow
homog.

In general: $F(t) = \int_{-\infty}^{\infty} dw' e^{i\omega' t} \tilde{F}(\omega') \quad (F \text{ theorem})$

Linear equation \Rightarrow

$$\begin{aligned} \tilde{x}_p(t) &= \int_{-\infty}^{\omega} dw' \frac{\tilde{F}(\omega')}{im(\omega' - \omega)} \left(e^{i\omega' t} - e^{i\omega t} \right) \\ &= e^{i\omega t} \int_{-\infty}^{\omega} dw' \frac{\tilde{F}(\omega')}{im(\omega' - \omega)} \left[e^{i(\omega' - \omega)t} - 1 \right] \end{aligned}$$

Now: $\int_0^t d\bar{t} e^{i(\omega' - \omega)\bar{t}} = \frac{1}{i(\omega' - \omega)} e^{i(\omega' - \omega)t} \Big|_0^t$

$$= \frac{1}{i(\omega' - \omega)} \left[e^{i(\omega' - \omega)t} - 1 \right]$$

$$T^{\hbar \omega_j} \zeta_p(t) = e^{i\omega_j t} \int_{-\infty}^{\infty} d\omega' \frac{\tilde{F}(\omega')}{m} \int_0^t dt' e^{i(\omega' - \omega_j)t}$$

$$= e^{i\omega_j t} \int_0^t dt' \frac{e^{-i\omega_j t'}}{m} \underbrace{\int_{-\infty}^{\infty} d\omega' \tilde{F}(\omega')}_{F(t)} e^{i\omega' t}$$

$$= e^{i\omega_j t} \int_0^t dt' \frac{F(t')}{m} e^{-i\omega_j t'}$$

Result: $\tilde{\zeta}(t) = \dot{x} + i\omega x$

$$T^{\hbar \omega_j} x(t) = \frac{1}{\omega} \operatorname{Im} [\tilde{\zeta}(t)]$$

$$\dot{x}(t) = \operatorname{Re} [\tilde{\zeta}(t)]$$

$$\dot{\xi} - i\omega\xi = \frac{F(t)}{m}$$

This is a linear 1st-order ODE for $\xi(t)$ similar to

$$y'(x) + P(x)y(x) = Q(x)$$

which we can rewrite in differential notation as

$$dy + [P(x)y - Q(x)]dx = 0$$

Although the LHS is not an exact differential, it can be made so by multiplying by an integrating factor $\mu(x)$ for which

$$\mu(x)dy + \mu(x)[P(x)y - Q(x)]dx = dU$$

for some function $U(x, y)$. The integrating factor $\mu(x)$ can be found by solving

$$\frac{d\mu}{dx} = \frac{\partial}{\partial y}(\mu(x)[P(x)y - Q(x)]) = \mu(x)P(x)$$

which is a consequence of

$$\frac{\partial^2 U}{\partial x \partial y} = \frac{\partial^2 U}{\partial y \partial x} \quad \text{with} \quad \frac{\partial U}{\partial x} = \mu(x)[P(x)y - Q(x)], \quad \frac{\partial U}{\partial y} = \mu(x)$$

leading to

$$\mu(x) = e^{I(x)}, \quad I(x) \equiv \int P(x)dx$$

To find U we solve

$$\frac{\partial U}{\partial x} = \mu(x)[P(x)y - Q(x)], \quad \frac{\partial U}{\partial y} = \mu(x),$$

The solution to the 2nd equation is

$$U(x, y) = \mu(x)y + g(x)$$

for some function $g(x)$.

The function $g(x)$ is determined by substituting this solution for U back into the 1st equation:

$$\mu'(x)y + g'(x) = \mu(x)[P(x)y - Q(x)]$$

Substituting our previous solution for $\mu(x)$ leads to

$$g'(x) = -\mu(x)Q(x)$$

which implies

$$g(x) = - \int dx \mu(x)Q(x) = - \int dx e^{I(x)}Q(x)$$

Thus,

$$U(x, y) = e^{I(x)}y - \int dx e^{I(x)}Q(x)$$

The solution to the original 1st-order ODE for y is then given by $U(x, y) = \text{const}$. So

$$y = e^{-I(x)} \left[\int dx e^{I(x)}Q(x) + \text{const} \right], \quad I(x) \equiv \int P(x)dx$$

Returning to the differential equation for $\xi(t)$, we see that $-i\omega$ plays the role of $P(x)$ and $F(t)/m$ plays the role of $Q(x)$.

Thus, the solution for $\xi(t)$ is given by

$$\xi = e^{i\omega t} \left[\int dt e^{-i\omega t} \frac{F(t)}{m} + \text{const} \right]$$

By choosing the limits on the integral to run from 0 to t , the constant becomes $\xi(0) \equiv \xi_0$. Thus,

$$\boxed{\xi = e^{i\omega t} \left[\int_0^t d\bar{t} e^{-i\omega \bar{t}} \frac{F(\bar{t})}{m} + \xi_0 \right]}$$

The first term on the RHS is a particular solution $\xi_p(t)$ to the differential equation for $\xi(t)$; the second term is the general solution to the homogeneous equation and involves the complex integration constant ξ_0 .

To return to $x(t)$, we recall the definition

$$\xi \equiv \dot{x} + i\omega x$$

which implies

$$\boxed{\dot{x} = \text{re}[\xi], \quad x = \text{im}[\xi/\omega]}$$

NOTE: The same solution for $\xi(t)$ can be obtained if we first restrict attention to a sinusoidal force

$$F(t) \equiv F_0 e^{i\omega t}$$

for which a particular solution of the differential equation $\dot{\xi} - i\omega\xi = F(t)/m$ is then

$$\xi_p(t) = \frac{F_0}{im(\omega' - \omega)} (e^{i\omega' t} - e^{i\omega t})$$

Note that we added the last term (proportional to a solution of the homogeneous equation) so that $\xi_p(0) = 0$.

By Fourier's theorem, the most general $F(t)$ is a superposition of sinusoidal forces:

$$F(t) = \int_{-\infty}^{\infty} d\omega' F(\omega') e^{i\omega' t}$$

which means that a particular solution for the most general $F(t)$ is a superposition of particular solutions for sinusoidal forces:

$$\xi_p(t) = \int_{-\infty}^{\infty} d\omega' \frac{F(\omega')}{im(\omega' - \omega)} (e^{i\omega' t} - e^{i\omega t})$$

Factoring out an $e^{i\omega t}$ we find

$$\xi_p(t) = e^{i\omega t} \int_{-\infty}^{\infty} d\omega' \frac{F(\omega')}{im(\omega' - \omega)} [e^{i(\omega' - \omega)t} - 1] = e^{i\omega t} \int_{-\infty}^{\infty} d\omega' \frac{F(\omega')}{m} \int_0^t d\bar{t} e^{i(\omega' - \omega)\bar{t}}$$

Rearranging the order of the integrals then gives

$$\xi_p(t) = e^{i\omega t} \int_0^t d\bar{t} e^{-i\omega \bar{t}} \int_{-\infty}^{\infty} d\omega' \frac{F(\omega')}{m} e^{i\omega' \bar{t}} = e^{i\omega t} \int_0^t d\bar{t} e^{-i\omega \bar{t}} \frac{F(\bar{t})}{m}$$

which is the particular solution we found earlier.

4) Calculate the normal mode frequencies and normal mode solutions for small oscillations of systems with more than one DOF.

The Lagrangian

$$L = \frac{1}{2} \sum_{ik} a_{ik}(q) \dot{q}_i \dot{q}_k - U(q)$$

becomes

$$L = \frac{1}{2} \sum_{i,k} m_{ik} \dot{x}_i \dot{x}_k - \frac{1}{2} \sum_{i,k} k_{ik} x_i x_k$$

for small oscillations around q_{i0} , where

$$x_i \equiv q_i - q_{i0}, \quad m_{ik} \equiv a_{ik}(q_0), \quad k_{ik} \equiv \left. \frac{\partial^2 U}{\partial q_i \partial q_k} \right|_{q_0}$$

Lagrange's equations

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}_i} \right) = \frac{\partial L}{\partial x_i}, \quad i = 1, 2, \dots, n$$

imply

$$\sum_k m_{ik} \ddot{x}_k = - \sum_k k_{ik} x_k, \quad i = 1, 2, \dots, n$$

We guess a sinusoidal solution of the form

$$x_i = A_i e^{i\omega t}, \quad i = 1, 2, \dots, n$$

which converts the above EOMs to

$$\sum_k -\omega^2 m_{ik} A_k e^{i\omega t} = - \sum_k k_{ik} A_k e^{i\omega t}, \quad i = 1, 2, \dots, n$$

or, equivalently,

$$\sum_k (k_{ik} - \omega^2 m_{ik}) A_k = 0, \quad i = 1, 2, \dots, n$$

These equations have a non-trivial solution for the A_i only if the matrix $(k_{ik} - \omega^2 m_{ik})$ is not invertible.

Thus, we must have

$$|k_{ik} - \omega^2 m_{ik}| = 0 \quad (\text{eigenvalue equation})$$

where $| |$ means take the determinant. This is an n th-order polynomial equation for the normal mode frequencies ω_n^2 .

The normal mode oscillations are the corresponding eigenvectors $A_{k\alpha}$, which are solutions to the matrix equation

$$\sum_k (k_{ik} - \omega_n^2 m_{ik}) A_{k\alpha} = 0, \quad i = 1, 2, \dots, n \quad (\text{eigenvector equation})$$

7. Rigid body motion (31-36, 38)

4) small oscillations with more than 1 DOF:

$$L = \frac{1}{2} \sum_{i,H} q_{i,H}(q) \dot{q}_i \cdot \dot{q}_H - U(q)$$

$$U(q) \approx U(q_0) + \frac{1}{2} \sum_{i,H} H_{i,H} (q_i - q_{i,0})(q_H - q_{H,0})$$

where $H_{i,H} = \frac{\partial^2 U}{\partial q_i \cdot \partial q_H} \Big|_{q_0}$

$$\begin{matrix} \Xi x_i & \Xi x_H \end{matrix}$$

$$\rightarrow \boxed{L = \frac{1}{2} \sum_{i,H} m_{i,H} \dot{x}_i \cdot \dot{x}_H - \frac{1}{2} \sum_{i,H} H_{i,H} x_i x_H}$$

where $m_{i,H} = q_{i,H}(q_0)$

Eqn: $\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}_i} \right) = \frac{\partial L}{\partial x_i}$

$$\sum_{i,H} m_{i,H} \ddot{x}_H = - \sum_H H_{i,H} x_H$$

$$\sum_{\text{H}} (m_{i,\text{H}} \ddot{x}_{\text{H}} + k_{i,\text{H}} x_{\text{H}}) = 0$$

in t

Ansatz: $x_{\text{H}} = A_{\text{H}} e^{i\omega t}$

$$\ddot{x}_{\text{H}} = -\omega^2 A_{\text{H}} e^{i\omega t} = -\omega^2 x_{\text{H}}$$

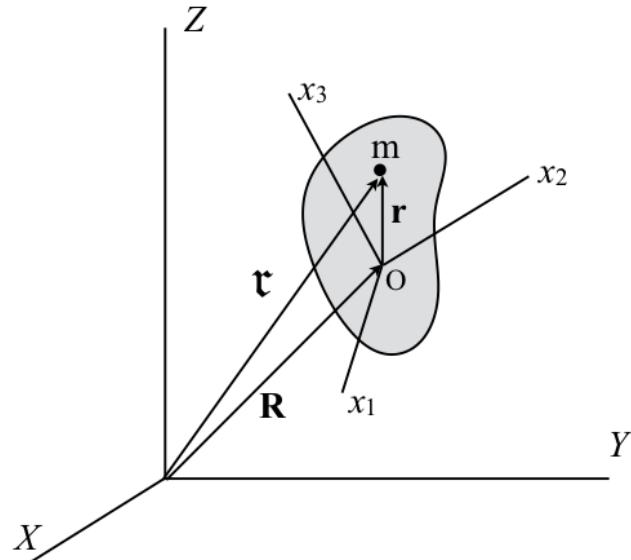
$$\rightarrow \sum_{\text{H}} (-m_{i,\text{H}} \omega^2 + k_{i,\text{H}}) A_{\text{H}} = 0$$

$\underbrace{\text{matrix must have } \det = 0 \text{ in order}}_{\text{to have non-zero } A_{\text{H}}}$

Char. eqn: $\det(k_{i,\text{H}} - m_{i,\text{H}} \omega^2) = 0$

solve for ω then substitute into
to find the corresponding eigenvectors

1) Draw a diagram showing the body frame and fixed inertial reference frame.



Notation:

- (X, Y, Z) : inertial frame
- (x_1, x_2, x_3) : body frame (non-inertial)
- m : point mass m fixed in the body frame
- \mathbf{r}, \mathbf{r}' : position vectors of m wrt to the inertial and body frames
- \mathbf{R} : position vector of the origin O of the body frame (usually taken at the COM of the body)

2) Show that the angular velocity vector is unchanged under a shift of the origin of the body frame.

Consider a shift of origin of the body frame from \mathbf{R} to $\mathbf{R}' \equiv \mathbf{R} + \mathbf{a}$. Let \mathbf{r} and \mathbf{r}' denote the position vectors of a mass point fixed in the rigid body wrt these two origins. Then

$$\mathbf{r} = \mathbf{r}' + \mathbf{a}$$

Wrt to the inertial frame:

$$\mathbf{v} \equiv \frac{d\mathbf{r}}{dt} = \mathbf{V} + \boldsymbol{\Omega} \times \mathbf{r}$$

where $\mathbf{V} \equiv d\mathbf{R}/dt$. Expanding the RHS of the above expression, we have

$$\mathbf{v} = \mathbf{V} + \boldsymbol{\Omega} \times (\mathbf{r}' + \mathbf{a}) = \mathbf{V} + \boldsymbol{\Omega} \times \mathbf{r}' + \boldsymbol{\Omega} \times \mathbf{a} = \mathbf{V}' + \boldsymbol{\Omega}' \times \mathbf{r}'$$

where

$$\mathbf{V}' \equiv \frac{d\mathbf{R}'}{dt} = \mathbf{V} + \boldsymbol{\Omega} \times \mathbf{a}, \quad \boldsymbol{\Omega}' = \boldsymbol{\Omega}$$

This means that the angular velocity vector $\boldsymbol{\Omega}$ is a property of the rigid body as a whole; it is not associated with any particular point in the body.

3) Write down an expression for the components I_{ik} of the inertia tensor as a sum over discrete mass points or as an integral over the volume of the body.

Discrete mass points:

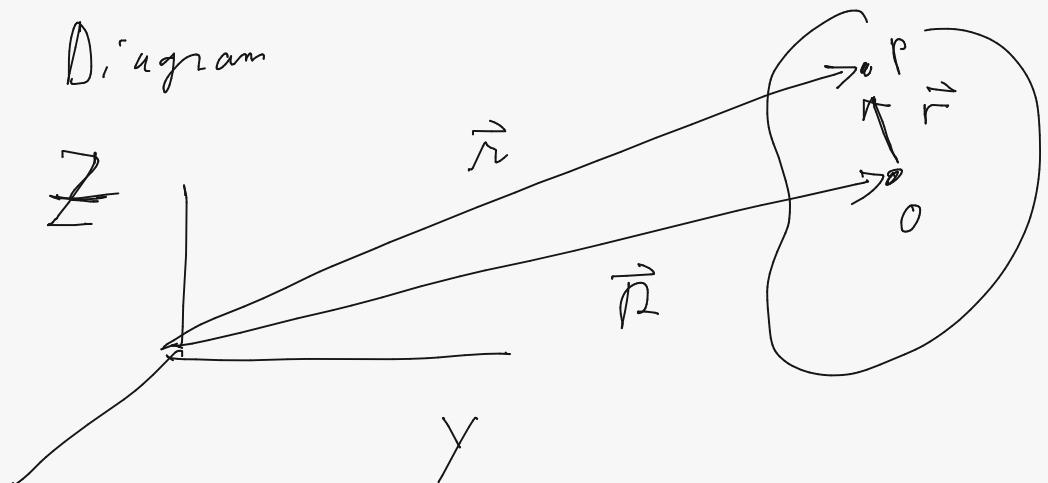
$$I_{ik} = \sum_a m_a (\delta_{ik} |\mathbf{r}_a|^2 - r_{ai} r_{ak})$$

Continuous mass distribution:

$$I_{ik} = \int dV \rho(\mathbf{r}) (\delta_{ik} |\mathbf{r}|^2 - r_i r_k)$$

where we have simply replaced m_a by $\rho(\mathbf{r})dV$ and the summation by an integral.

1) Diagram



ρ : fixed wrt
Rigid body

$$\begin{aligned} \vec{v} &= \frac{d\vec{r}}{dt} = \frac{d\vec{R}}{dt} + \frac{d\phi}{dt} \vec{\omega} \times \vec{r} \\ &= \vec{V} + \vec{\omega} \times \vec{r} \end{aligned}$$

under
completeness

angular velocity

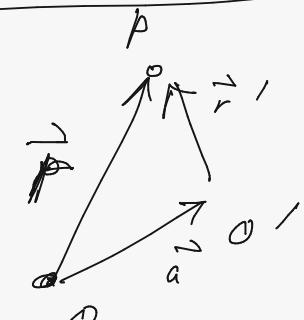
2) Under a shift of origin: $O \rightarrow O'$

$$\vec{r} = \vec{r}' + \vec{a}$$

$$\vec{v} = \vec{V} + \vec{\omega} \times (\vec{r}' + \vec{a})$$

$$= (\vec{V} + \vec{\omega} \times \vec{a}) + \vec{\omega} \times \vec{r}' = \vec{V}' + \vec{\omega}' \times \vec{r}'$$

where $\vec{V}' = \vec{V} + \vec{\omega} \times \vec{a}$



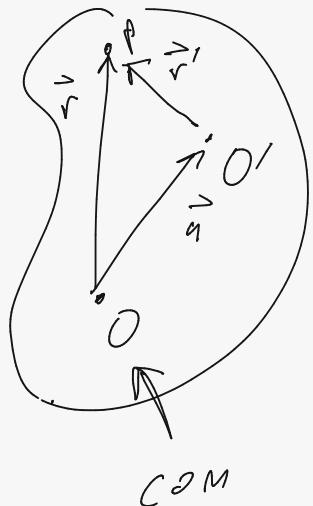
prop. of
rigid body

$$3) \quad I_{ij} = \sum_u m_u (r_u^2 \delta_{ij} - r_{ui} \cdot r_{uj})$$

$$\bar{I}_{ij} = \int \rho dV (r^2 \delta_{ij} - r_i \cdot r_j)$$

$$4) \quad \begin{aligned} \vec{r} &= \vec{r}' + \vec{a} \\ \vec{r}' &= \vec{r} - \vec{a} \end{aligned}$$

$$\bar{I}_{ij}' = \int \rho dV (|\vec{r} - \vec{a}|^2 \delta_{ij} - (r_i - a_i)(r_j - a_j))$$



$$= \int \rho dV ((r^2 + a^2 + 2\vec{r} \cdot \vec{a}) \delta_{ij} - r_i r_j - a_i a_j - r_i a_j - r_j a_i)$$

$$= \int \rho dV (r^2 \delta_{ij} - r_i r_j)$$

$$+ \underbrace{\int \rho dV (a^2 \delta_{ij} - a_i a_j)}_{M} + \delta_{ij} \cdot \vec{a} \cdot \int \rho dV \vec{r}$$

$$- a_j \int \rho dV r_i - a_i \int \rho dV r_j$$

$$= I_{ij} + \mu (a^2 \delta_{ij} - a_i a_j)$$

4) Indicate how the components of the inertia tensor change if you shift the origin of the body frame.

Consider a shift of the origin of the body frame from the COM to \mathbf{a} . Let \mathbf{r} denote the position of mass point m wrt the COM and \mathbf{r}' the position of m wrt the origin at \mathbf{a} . Then

$$\mathbf{r} = \mathbf{r}' + \mathbf{a}$$

for which

$$I'_{ik} = \sum m(\delta_{ik}|\mathbf{r}'|^2 - r'_i r'_k) = \sum m [\delta_{ik}|\mathbf{r} - \mathbf{a}|^2 - (r_i - a_i)(r_k - a_k)] = I_{ik} + \mu (\delta_{ik}|\mathbf{a}|^2 - a_i a_k)$$

where $\mu \equiv \sum m$ is the total mass, and we used $\sum m\mathbf{r} = 0$ (the definition of COM frame) to get the last equality.

Thus

$$I'_{ik} = I_{ik} + \mu (\delta_{ik}|\mathbf{a}|^2 - a_i a_k)$$

The parallel-axis theorem is a special case of the above general result, with the moment of inertia about an axis $\hat{\mathbf{n}}$ defined as $I(\hat{\mathbf{n}}) = \sum_{i,k} I_{ik} n_i n_k$.

5) Obtain or identify the principal axes of inertia for various rigid bodies.

With respect to principal axes x_1, x_2, x_3 passing through the COM of the body, the moment of inertia tensor is diagonal:

$$I_{ik} = I_i \delta_{ik}$$

Principal axes always agree with symmetry axes of the body, if they exist.

If the rigid body lacks such symmetry, one can always diagonalize I_{ik} (which is a real symmetric matrix) by finding the eigenvectors and eigenvalues of the matrix I_{ik} . The eigenvalues are the principal moments of inertia; the eigenvectors are the principal axes.

6) Calculate the principal moments of inertia for various rigid bodies.

One can use the above expressions to calculate the principal moments of inertia for various rigid bodies consisting of either discrete mass points or for continuous mass distributions. This is primarily an exercise in doing multi-dimensional integrals.

Simplifications occur if the rigid body has a uniform mass distribution, since the mass density $\rho(\mathbf{r})$ is then a constant and can be pulled out of the integral.

One needs to use the volume element appropriate for the geometry of the rigid body:

- Cartesian coordinates (x, y, z) for box-type objects: $dV = dx dy dz$
- Spherical coordinates (r, θ, ϕ) for spherical objects or ellipsoids, with the axes appropriately rescaled: $dV = r^2 \sin \theta dr d\theta d\phi$
- Cylindrical coordinate (s, z, ϕ) for cylinders or cones: $dV = s ds dz d\phi$, where $s^2 \equiv x^2 + y^2$

For objects like a cone or cylinder, with degenerate principal axes (x and y) in the plane perpendicular to the main symmetry axis, one can calculate $I \equiv I_1 = I_2$ using the following "trick":

$$I_1 = \int dV \rho[r^2 - x^2], \quad I_2 = \int dV \rho[r^2 - y^2], \quad I_3 = \int dV \rho[r^2 - z^2] = \int dV \rho s^2$$

which implies

$$2I = I_1 + I_2 = \int dV \rho[2r^2 - x^2 - y^2] = \int dV \rho[2(s^2 + z^2) - s^2] = \int dV \rho[s^2 + 2z^2] = I_3 + 2 \int d$$

Thus

$$I \equiv I_1 = I_2 = \frac{1}{2}I_3 + \int dV \rho z^2$$

where the last integral is often easy to do.

Cylinder:

Applying these results to a uniform cylinder of total mass μ , height h , and radius R , we find:

$$I_1 = I_2 = \frac{1}{4}\mu \left(R^2 + \frac{1}{3}h^2 \right), \quad I_3 = \frac{1}{2}\mu R^2$$

It is interesting to take the following limits:

- $h \rightarrow 0$ for a thin disk:

$$I_1 = I_2 = \frac{1}{4}\mu R^2, \quad I_3 = \frac{1}{2}\mu R^2$$

- $R \rightarrow 0$ for a thin rod:

$$I_1 = I_2 = \frac{1}{12}\mu h^2, \quad I_3 = 0$$

5) Principle axes pass thru com of object and reflect symmetry properties.

$I_{ij} = \text{real symmetric} \rightarrow \text{can always diagonalize}$

$$I_{ij} = I_i \delta_{ij}$$

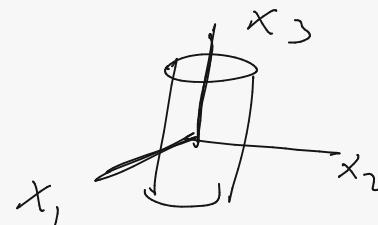
The basis vector in terms of which $I_{ij} = \text{diagonal}$ are the principle axes of the body

6) Volume elements:

$$\begin{aligned} dV &= dx dy dz \\ &= dr r d\theta dz \\ &= dr r d\theta r \sin \theta d\phi \end{aligned}$$

Suppose $I_1 = I_2 \equiv I$ and $I_3 = \text{trivial}$.

~~Then~~ Then

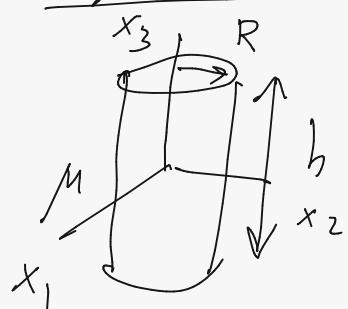


$$\begin{aligned} 2I &= I_1 + I_2 = \int \rho dV (r^2 - x^2 + r^2 - y^2) \quad r^2 = s^2 + z^2 \\ &= \int \rho dV (2r^2 - (x^2 + y^2)) \\ &= \int \rho dV (2s^2 + 2z^2 - s^2) = \int \rho dV (s^2 + 2z^2) \end{aligned}$$

$$I = \frac{1}{2} \underbrace{\int \rho dV s^2}_{I_3} + \underbrace{\int \rho dV z^2}_{\text{center to do}}$$

$$= \frac{1}{2} I_3 + \int \rho dV z^2$$

Cylinder:



$$\text{Volume} = \pi R^2 h$$

$$I_3 = \int \rho dV s^2$$

$$= \frac{M}{\pi R^2 h} \int_0^{2\pi} d\phi \int_0^R dr s^3 \int_{-h/2}^{h/2} dz$$

$$= \frac{M}{\pi R^2 h} \cdot 2\pi \cdot h \cdot \frac{s^4}{4} \Big|_0^R$$

$$= \boxed{\frac{1}{2} M R^2}$$

just like a disk

$$dV = dr s d\phi dt \\ = r dr d\phi dz$$

Theory

$$\begin{aligned} I &= \frac{1}{2} I_3 + \int_{2\pi} \rho dV \cdot z^2 \\ &= \frac{1}{2} I_3 + \frac{m}{\pi R^2 h} \int_0^{2\pi} d\phi \int_0^R s ds \int_{-h/2}^{h/2} z^2 dz \\ &= \frac{m}{\pi R^2 h} \left(2\pi \int_0^R \frac{s^2}{2} \left[\frac{1}{3} z^3 \right]_{-h/2}^{h/2} \right) \end{aligned}$$


$$= \frac{\cancel{2\pi m}}{\cancel{R^2 h}} \cancel{\frac{R^2}{2}} \frac{2}{3} \frac{h^3}{8}$$

$$= \frac{1}{12} m h^2$$

$$= \frac{1}{2} \left(\frac{1}{2} m R^2 \right) + \frac{1}{12} m h^2$$

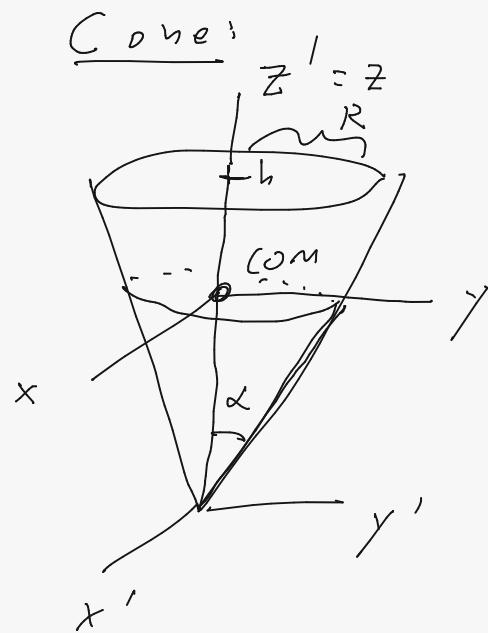
$$\boxed{I = \frac{1}{4} m \left(R^2 + \frac{1}{3} h^2 \right)}$$

$$\begin{aligned} \text{For } h \rightarrow 0 \\ I &= \frac{1}{4} m R^2 \\ &= \frac{1}{2} I_3 \end{aligned}$$

For $R \rightarrow 0$: (thin rod)

$$I_3 = 0$$

$$I = \frac{m}{12} h^2$$



$$s(z) = z \tan \alpha$$

$$\tan \alpha = \frac{s}{z} = \frac{R}{h}$$

Thus,

$$\rho = \frac{M}{\pi R^2 h}$$

$$\rho = \frac{M}{\text{Volume}}$$

$$\begin{aligned} \text{Volume} &= \int dV \\ &= \int d\phi \int dz \int s ds \\ &= \cancel{\pi} \int dz \frac{s^2}{2} \Big|_0^h \\ &= \pi \tan^2 \alpha \int_0^h dz z^2 \\ &= \pi \tan^2 \alpha \frac{z^3}{3} \Big|_0^h \\ &= \frac{\pi}{3} \tan^2 \alpha h^3 \\ &= \frac{\pi}{3} \frac{R^2}{h^2} h^3 \\ &= \frac{1}{3} \pi R^2 \end{aligned}$$

To determine the Com:

$$\begin{aligned} Z_{com} &= \frac{1}{M} \cdot \int \rho dV \cdot z \\ &= \frac{\rho}{M} \int_0^{2\pi} d\phi \int_0^h dz \cdot z \int_0^R s ds \\ &= \frac{3}{\pi R^2 \cdot h} \cdot \cancel{\pi} \int_0^h dz \quad z = \frac{1}{2} z^2 + \frac{1}{4} \alpha \quad \left(\frac{R}{h}\right)^2 \\ &= \frac{3}{\pi R^2 \cdot h} \left(\frac{R}{h}\right)^2 \frac{z^4}{4} \Big|_0^h \\ &= \frac{3}{4 h^3} \cdot h^4 \\ &= \boxed{\frac{3}{4} h} \end{aligned}$$

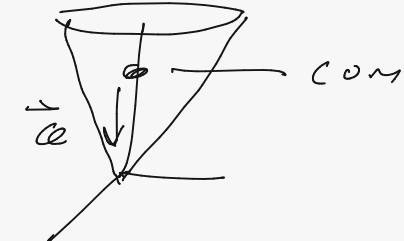
$$\begin{aligned}
 I_z' &:= \int \rho dV (r^2 - z^2) \\
 &= \int_{2\pi} \rho dV s^2 \\
 &= \rho \int d\phi \int_0^h dz \int_0^{z \tan \alpha} dr s^3 \\
 &= \rho 2\pi \int_0^h dz \frac{z^4 \tan^4 \alpha}{4} \\
 &= \rho \frac{\pi}{2} \left(\frac{R}{h}\right)^4 \frac{z^5}{5} \Big|_0^h \\
 &= \rho \frac{\pi}{10} \frac{R^4}{h^4} h^5 \\
 &= \rho \frac{\pi}{10} R^4 h \\
 &= \frac{3M}{\pi R^2 h} \cdot \frac{\pi}{10} R^4 h = \boxed{\frac{3M}{10} R^2}
 \end{aligned}$$

$$\begin{aligned}
I' &= I'_x = F'_y \\
&= \frac{1}{2} I_2' + \int p dV z^2 \\
&= \frac{3}{20} M R^2 + \frac{3M}{\pi R^2 h} \int_0^{2\pi} d\phi \int_0^h dz z^2 \int s ds \\
&= \frac{3}{20} M R^2 + \frac{3M}{\cancel{\pi R^2 h}} \cdot \cancel{2\pi} \int_0^h dz z^2 \frac{1}{2} z^2 \cancel{\frac{1}{2}} \cancel{\frac{h^2}{2}} \cancel{\alpha} \frac{R^2}{h^2} \\
&= \frac{3}{20} M R^2 + \frac{3M}{\cancel{R^2 h}} \frac{R^2}{h^2} \frac{1}{5} h^5 \\
&= \frac{3}{20} M R^2 + \frac{3}{5} M h^2 \\
&= \boxed{\frac{3}{20} M (R^2 + 4h^2)}
\end{aligned}$$

$$I' = \frac{3}{20} \mu (R^2 + 4b^2), \quad I_z' = \frac{3}{10} \mu R^2$$

Recall:

$$I_{ij}' = I_{ij} + \mu (a^2 \delta_{ij} - a_i a_j)$$



$$I_{ij} = I_{ij}' - \mu (a^2 \delta_{ij} - a_i a_j)$$

$$\begin{aligned} I_3 &= I_3' - \mu (a^2 - a \cdot a) \\ &= I_3' \\ &= \boxed{\frac{3}{10} \mu R^2} \end{aligned}$$

$$I = I' - \mu (a^2 - \vec{a}_x \vec{a}_x)$$

$$= \frac{3}{20} \mu (R^2 + 4b^2) - \mu \frac{9}{16} b^2$$

$$= \frac{3}{20} \mu R^2 + \mu b^2 \left(\frac{3}{5} - \frac{9}{16} \right)$$

$$= \boxed{\frac{3}{20} \mu \left(R^2 + \frac{b^2}{4} \right)}$$

$$\begin{aligned} a_x &= a_y = 0 \\ a_z &= -z_{\text{com}} \\ &= -\frac{3}{4} b \end{aligned}$$

$$So \boxed{a = \frac{3}{4} b} = I a_z$$

$$\frac{48 - 45}{80} = \frac{3}{80}$$

Cone:

For a cone, it is simplest to first calculate the components of the inertia tensor wrt (x', y', z') axes with the origin at the tip of the cone and the azimuthal symmetry axis directed along z' . For a uniform right-circular cone of total mass μ , height h , and base radius R , the total volume of the cone is $V = \pi R^2 h / 3$. The COM of mass is located at $x' = 0, y' = 0, z' = 3h/4$.

So we first find:

$$I'_1 = I'_2 = \frac{3}{20}\mu(R^2 + 4h^2), \quad I'_3 = \frac{3}{10}\mu R^2$$

Then use

$$I'_{ik} = I_{ik} + \mu(\delta_{ik}|\mathbf{a}|^2 - a_i a_k)$$

to transform the components of the inertia tensor wrt the primed axes (x', y', z') to the principal axes (x, y, z) passing through the COM. The final result is

$$I_1 = I_2 = \frac{3}{20}\mu\left(R^2 + \frac{1}{4}h^2\right), \quad I_3 = \frac{3}{10}\mu R^2$$

7) Calculate the kinetic energy of a rigid body in terms of its COM motion and rotational kinetic energy.

Kinetic energy of the rigid body viewed as a collection of discrete mass points:

$$T = \frac{1}{2} \sum_a m_a |\mathbf{v}_a|^2$$

where $\mathbf{v}_a \equiv d\mathbf{r}_a/dt$ is the position vector of m_a wrt to the inertial frame.

Since $\mathbf{r}_a = \mathbf{R} + \mathbf{r}_a$, where \mathbf{R} is the position vector of the COM and \mathbf{r}_a is the position vector of m_a wrt to the COM, we have

$$\mathbf{v}_a = \mathbf{V} + \boldsymbol{\Omega} \times \mathbf{r}_a$$

where $\mathbf{V} \equiv d\mathbf{R}/dt$ is the velocity of the COM wrt to the inertial frame and $\boldsymbol{\Omega}$ is the angular velocity of the rigid body. Note that there is no additional velocity term on the RHS since the mass point m_a is fixed wrt the rigid body.

Thus,

$$T = \frac{1}{2} \sum_a m_a |\mathbf{v}_a|^2 = \frac{1}{2} \sum_a m_a |\mathbf{V} + \boldsymbol{\Omega} \times \mathbf{r}_a|^2 = \frac{1}{2} \sum_a m_a [|\mathbf{V}|^2 + 2\mathbf{V} \cdot (\boldsymbol{\Omega} \times \mathbf{r}_a) + (\boldsymbol{\Omega} \times \mathbf{r}_a) \cdot (\boldsymbol{\Omega} \times \mathbf{r}_a)]$$

The three terms on the RHS are:

1st term:

$$\frac{1}{2} \sum_a m_a |\mathbf{V}|^2 = \frac{1}{2} \mu V^2$$

where $\mu \equiv \sum_a m_a$ which is the kinetic energy of the COM wrt the inertial frame.

2nd term:

$$\frac{1}{2} \sum_a m_a 2\mathbf{V} \cdot (\boldsymbol{\Omega} \times \mathbf{r}_a) = \left(\sum_a m_a \mathbf{r}_a \right) \cdot (\mathbf{V} \times \boldsymbol{\Omega}) = 0$$

since $\sum_a m_a \mathbf{r}_a = 0$ by definition of the COM frame.

3rd term:

$$\frac{1}{2} \sum_a m_a (\boldsymbol{\Omega} \times \mathbf{r}_a) \cdot (\boldsymbol{\Omega} \times \mathbf{r}_a)$$

Using vector identities

$$\mathbf{A} \cdot (\mathbf{B} \times \mathbf{C}) = \mathbf{B} \cdot (\mathbf{C} \times \mathbf{A}) = \mathbf{C} \cdot (\mathbf{A} \times \mathbf{B})$$

and

$$\mathbf{A} \times (\mathbf{B} \times \mathbf{C}) = \mathbf{B}(\mathbf{A} \cdot \mathbf{C}) - \mathbf{C}(\mathbf{A} \cdot \mathbf{B})$$

it follows that

$$(\boldsymbol{\Omega} \times \mathbf{r}_a) \cdot (\boldsymbol{\Omega} \times \mathbf{r}_a) = \boldsymbol{\Omega} \cdot [\mathbf{r}_a \times (\boldsymbol{\Omega} \times \mathbf{r}_a)] = \boldsymbol{\Omega} \cdot [\boldsymbol{\Omega} |\mathbf{r}_a|^2 - \mathbf{r}_a (\boldsymbol{\Omega} \cdot \mathbf{r}_a)] = |\boldsymbol{\Omega}|^2 |\mathbf{r}_a|^2 - (\boldsymbol{\Omega} \cdot \mathbf{r}_a)^2 = \sum_{i,k} I_{ik} \Omega_i \Omega_k$$

so

$$3\text{rd term} = \frac{1}{2} \sum_a m_a \sum_{i,k} \Omega_i \Omega_k (\delta_{ik} |\mathbf{r}_a|^2 - r_{ai} r_{ak}) = \frac{1}{2} \sum_{i,k} I_{ik} \Omega_i \Omega_k$$

where

$$I_{ik} = \sum_a m_a (\delta_{ik} |\mathbf{r}_a|^2 - r_{ai} r_{ak})$$

Thus, putting all the pieces together:

7) HE of rotating body

$$T = \frac{1}{2} \sum_a m_a |\vec{v}_a|^2$$

$$= \frac{1}{2} \sum_a m_a |\vec{V} + \vec{\omega} \times \vec{r}_a|^2$$

$$= \frac{1}{2} \sum_a m_a (V^2 + 2\vec{V} \cdot (\vec{\omega} \times \vec{r}_a) + |\vec{\omega} \times \vec{r}_a|^2)$$

$$= \textcircled{a} + \textcircled{b} + \textcircled{c}$$

$$\textcircled{a} = \frac{1}{2} M V^2 \quad (\text{HE of com})$$

$$\textcircled{b} = \underbrace{\left(\sum_a m_a \vec{r}_a \right)}_{\vec{R}_{com} = 0} \cdot (\vec{V} \times \vec{\omega}) = 0 \quad \text{for } O_{com}$$

$$\textcircled{c} = \frac{1}{2} \sum_a m_a (\vec{\omega} \times \vec{r}_a) \cdot (\vec{\omega} \times \vec{r}_a)$$

$$= \frac{1}{2} \sum_a m_a \vec{\omega} \cdot (\vec{r}_a \times (\vec{\omega} \times \vec{r}_a))$$

$$= \frac{1}{2} \sum_a m_a \vec{\omega} \cdot (\vec{\omega} r_a^2 - \vec{r}_a (\vec{r}_a \cdot \vec{\omega}))$$

$$= \frac{1}{2} \sum_a m_a (\delta_{ij} \Omega_i \Omega_j r_a^2 - \Omega_i \Omega_j r_{ai} r_{aj})$$

$$\vec{v}_a = \vec{V} + \vec{r}_a + \vec{r}_a$$

$$\textcircled{c} \quad = \frac{1}{2} \sum_a m_a (r_a^2 \delta_{ij} - r_{ai} r_{aj}) \Omega_i \Omega_j$$

$$= \frac{1}{2} I_{ij} \Omega_i \Omega_j$$

$$\text{thus, } T = \frac{1}{2} M V^2 + \frac{1}{2} I_{ij} \Omega_i \Omega_j$$



$$T = \frac{1}{2}\mu V^2 + \frac{1}{2} \sum_{i,k} I_{ik} \Omega_i \Omega_k$$

The first term is the translational kinetic energy of the rigid body (its COM motion), and the second is its rotational kinetic energy about the COM.

8) Write down an expression for the angular momentum vector \mathbf{M} in terms I_{ik} and Ω_i .

The angular momentum of a rigid body depends on the origin about which it is defined. For rigid body motion it is simplest to define the angular momentum \mathbf{M} of the system wrt to an inertial frame whose origin is instantaneously comoving with the COM of the rigid body.

In that case

$$\mathbf{M} = \sum_a \mathbf{r}_a \times \mathbf{p}_a = \sum_a m_a \mathbf{r}_a \times \mathbf{v}_a$$

where \mathbf{r}_a is the position vector of mass point m_a with respect to the COM and \mathbf{v}_a is its velocity.

Since m_a is fixed in the rigid body

$$\mathbf{v}_a = \boldsymbol{\Omega} \times \mathbf{r}_a$$

Thus,

$$\mathbf{M} = \sum_a m_a \mathbf{r}_a \times (\boldsymbol{\Omega} \times \mathbf{r}_a) = \sum_a m_a (\boldsymbol{\Omega} |\mathbf{r}_a|^2 - \mathbf{r}_a (\boldsymbol{\Omega} \cdot \mathbf{r}_a))$$

where we used

$$\mathbf{A} \times (\mathbf{B} \times \mathbf{C}) = \mathbf{B}(\mathbf{A} \cdot \mathbf{C}) - \mathbf{C}(\mathbf{A} \cdot \mathbf{B})$$

It is more informative to write this last expression in component notation:

$$M_i = \sum_a m_a \left(\Omega_i |\mathbf{r}_a|^2 - r_{ai} \sum_k \Omega_k r_{ak} \right) = \sum_a m_a (\delta_{ik} |\mathbf{r}_a|^2 - r_{ai} r_{ak}) \Omega_k$$

or

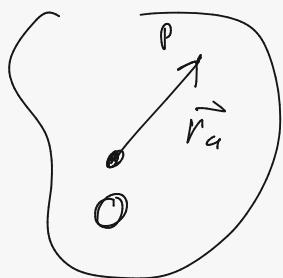
$$M_i = \sum_k I_{ik} \Omega_k$$

where I_{ik} are the components of the moment of inertia tensor.

9) Write down the equations of motion for a rigid body with respect to an inertial frame.

The EOMs for a rigid body wrt an inertial frame are the force and torque equations

8) Angular momentum wrt COM of rigid body



$$\begin{aligned}\vec{M} &= \sum_a m_a \vec{r}_a \times \vec{v}_a \\ &= \sum_a m_a \vec{r}_a \times (\vec{\omega} \times \vec{r}_a) \\ &= \sum_a m_a [\vec{\omega} \cdot \vec{r}_a^2 - \vec{r}_a \cdot (\vec{r}_a \cdot \vec{\omega})]\end{aligned}$$

$$\begin{aligned}M_i &= \sum_a m_a [d_{ij} \cdot \vec{r}_a^2 - \vec{r}_{ai} \cdot \vec{r}_{aj}] \Omega_j \\ &= I_{ij} \cdot \Omega_j\end{aligned}$$

9) EOM for rigid body

$$\frac{d \vec{P}}{dt} = \vec{F} = \sum \vec{f}, \quad \frac{d \vec{M}}{dt} = \vec{F} = \sum \vec{r} \times \vec{f}$$

where $\vec{F} = -\frac{\partial U}{\partial \vec{r}}$ $(\vec{r} = \vec{R} + \vec{r})$

Proof: (method 1)

$$\frac{d \vec{P}}{dt} = \frac{d}{dt} \left(\sum_a \vec{p}_a \right) = \sum_a \frac{d \vec{p}_a}{dt} = \sum_a f_a$$

$$\frac{d\vec{M}}{dt} = \frac{d}{dt} \left(\sum_a \vec{r}_a \times \vec{p}_a^0 \right) = \sum_a \left(\vec{v}_a \times \vec{p}_a^0 + \vec{r}_a \times \frac{d\vec{p}_a}{dt} \right)$$

since $\vec{p}_a = m_a \vec{v}_a$ $\boxed{\vec{f}_a}$

$$= \sum_a \vec{r}_a \times \vec{f}_a \equiv \vec{K}$$

Proof (method 2):

$$\begin{aligned} L &= T - U \\ &= \frac{1}{2} M \vec{V}^2 + \sum_i I_{ij} \Omega_j \cdot \vec{\Omega}_j - U(\vec{R}_1, \vec{R}_2, \dots) \\ dL &= \mu \vec{V} \cdot \vec{dV} + \underbrace{(I_{ij} \Omega_j) \vec{\Omega}_j}_{M_i} - \sum_a \frac{\partial U}{\partial \vec{R}_a} \cdot \vec{dR}_a \\ &= \mu \vec{V} \cdot \vec{dV} + \vec{M} \cdot \vec{dR} - \underbrace{\sum_a \frac{\partial U}{\partial \vec{R}_a} \cdot (\vec{d\phi} \times \vec{v}_a)}_{-\delta \vec{\psi} \cdot \sum_a \vec{r}_a \times \frac{\partial U}{\partial \vec{R}_a}} \end{aligned}$$

Thus,

$$\begin{aligned} \frac{\partial L}{\partial \vec{V}} &= \mu \vec{V} = \vec{P}, \quad \frac{\partial L}{\partial \vec{P}} = \vec{M}, \quad \frac{\partial L}{\partial \vec{R}} = - \sum_a \frac{\partial U}{\partial \vec{R}_a} = \sum_a \vec{f}_a \\ \frac{\partial L}{\partial \vec{\phi}} &= - \sum_a \vec{r}_a \times \frac{\partial U}{\partial \vec{R}_a} = \sum_a \vec{r}_a \times \vec{f}_a \equiv \vec{K} \end{aligned}$$

\int_0

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{P}} \right) = \frac{\partial L}{\partial P}$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{M}} \right) = \frac{\partial L}{\partial M}$$

$$\Rightarrow \begin{cases} \frac{dP}{dt} \\ \frac{dM}{dt} \end{cases} = \begin{cases} \Gamma \\ \dot{H} \end{cases}$$

$$\frac{d\mathbf{P}}{dt} = \sum \mathbf{f} \equiv \mathbf{F}, \quad \frac{d\mathbf{M}}{dt} = \sum \mathbf{r} \times \mathbf{f} \equiv \mathbf{K}$$

where \mathbf{P} is the total momentum of the rigid body wrt the inertial frame and \mathbf{M} is its angular momentum relative to the COM. There are six equations because there are 6 DOFs describing a rigid body: 3 coordinates for the origin of the body frame and the 3 Euler angles specifying the orientation of the body frame with respect to a fixed (space) frame. The time derivatives are wrt an inertial frame, not wrt the non-inertial body frame.

Note that \mathbf{F} and \mathbf{K} are the net *external* force and torque acting on the body, since the *internal* forces and torques cancel out by Newton's 3rd law.

One can prove the force and torque equations two different ways:

1st method:

$$\frac{d\mathbf{P}}{dt} = \frac{d}{dt}(\sum \mathbf{p}) = \sum \dot{\mathbf{p}} = \sum \mathbf{f} \equiv \mathbf{F}$$

For the angular momentum equation we will do the calculation in an inertial reference frame that is instantaneously at rest wrt the COM of the rigid body. Then

$$\frac{d\mathbf{M}}{dt} = \frac{d}{dt}(\sum \mathbf{r} \times \mathbf{p}) = \sum (\dot{\mathbf{r}} \times \mathbf{p} + \mathbf{r} \times \dot{\mathbf{p}}) = \sum \mathbf{r} \times \dot{\mathbf{p}} = \sum \mathbf{r} \times \mathbf{f} \equiv \mathbf{K}$$

where we used the result that $\dot{\mathbf{r}}$ is proportional to \mathbf{p} in the inertial reference frame that we have chosen, so $\dot{\mathbf{r}} \times \mathbf{p} = 0$.

NOTE: This relationship is actually valid in *any* inertial frame since if \mathbf{M} is defined wrt to the COM of the body, it is unchanged by a transformation from one inertial frame to another. (Recall: $\mathbf{M} = \mathbf{M}' + \mu \mathbf{R} \times \mathbf{V}$ for two inertial reference frames K and K' related by velocity \mathbf{V} , where \mathbf{R} is the location of the COM wrt K . For us, $\mathbf{R} = 0$ in K .)

2nd method:

The EOMs can also be obtained from the Lagrangian:

$$L = \frac{1}{2}\mu V^2 + \frac{1}{2} \sum_{i,k} I_{ik} \Omega_i \Omega_k - U$$

viewed as a function of the translational and rotational coordinates \mathbf{R} (COM) and $\boldsymbol{\phi}$ (Euler angles) and their time derivatives \mathbf{V} and $\boldsymbol{\Omega}$.

Proof:

Vary L :

$$\$ \$ \delta L = \mu \mathbf{V} \cdot \delta \mathbf{V} + \sum_{i,k} I_{ik} \Omega_i \delta \Omega_i$$

- $\sum_a \frac{\partial L}{\partial \mathbf{r}_a} \delta \mathbf{r}_a = \sum_a \mathbf{f}_a \delta \mathbf{r}_a$
- $\sum_k I_{ik} \Omega_i \delta \Omega_i = M_i \delta \Omega_i$
- $\frac{\partial L}{\partial \boldsymbol{\phi}} = - \sum_a \mathbf{r}_a \times \mathbf{f}_a$

where we used

$$\mathbf{r}_a = \mathbf{R} + \mathbf{r}_a \Rightarrow \delta \mathbf{r}_a = \delta \mathbf{R} + \delta \boldsymbol{\phi} \times \mathbf{r}_a$$

under a translation of the COM and rotation of the rigid body, respectively.

Thus

$$\frac{\partial L}{\partial \mathbf{V}} = \mu \mathbf{V} = \mathbf{P}, \quad \frac{\partial L}{\partial \mathbf{R}} = - \sum_a \frac{\partial U}{\partial \mathbf{r}_a} = \sum_a \mathbf{f}_a, \quad \frac{\partial L}{\partial \Omega_i} = \sum_k I_{ik} \Omega_k = M_i, \quad \frac{\partial L}{\partial \boldsymbol{\phi}} = - \sum_a \mathbf{r}_a \times \mathbf{f}_a$$

So Lagrange's equations

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \mathbf{V}} \right) = \frac{\partial L}{\partial \mathbf{R}}, \quad \frac{d}{dt} \left(\frac{\partial L}{\partial \Omega_i} \right) = \frac{\partial L}{\partial \boldsymbol{\phi}}$$

are simply

$$\frac{d\mathbf{P}}{dt} = \sum_a \mathbf{f}_a, \quad \frac{d\mathbf{M}}{dt} = \sum_a \mathbf{r}_a \times \mathbf{f}_a$$

10) Derive Euler's equations for rigid body motion (equations of motion in the body frame).

Euler's equations for rigid body motion are the components of the force and torque equations $\mathbf{F} = d\mathbf{P}/dt$ and $\mathbf{K} = d\mathbf{M}/dt$ expressed wrt the principal axes of the body.

We use the general relation:

$$\frac{d\mathbf{A}}{dt} = \frac{d'\mathbf{A}}{dt} + \boldsymbol{\Omega} \times \mathbf{A}$$

where $d\mathbf{A}/dt$ denotes the time derivative of any vector \mathbf{A} wrt the inertial frame and $d'\mathbf{A}/dt$ denotes the time derivative of that same vector wrt to the body frame. Recall that the time derivative of a vector wrt to any reference frame is obtained by simply time differentiating the Cartesian components of that vector wrt to that frame, e.g., $(d'\mathbf{A}/dt)_i \equiv dA_i/dt \equiv \dot{A}_i$.

Force equation:

$$\mathbf{F} = \frac{d\mathbf{P}}{dt} = \frac{d'\mathbf{P}}{dt} + \boldsymbol{\Omega} \times \mathbf{P}$$

10) Euler's equations for rigid body motion:

$\frac{d\vec{p}}{dt} = \vec{F}$ and $\frac{d\vec{m}}{dt} = \vec{H}$ but written w.r.t
principle axes in the rigid body.

Now: $\frac{d\vec{A}}{dt} = \frac{d'\vec{A}}{dt} + \vec{\Omega} \times \vec{A}$

└ w.r.t rotating frame.

Components $\left(\frac{d'\vec{A}}{dt}\right)_i \equiv \frac{dA_i}{dt}$

Thn,

$$\vec{F} = \frac{d\vec{p}}{dt} = \frac{d'\vec{p}}{dt} + \vec{\Omega} \times \vec{p}$$

w.r.t principle axes $(\hat{x}_1, \hat{x}_2, \hat{x}_3)$:

$$F_i = \frac{dp_i}{dt} + \epsilon_{ijk} \Omega_j P_k$$

$$\text{so } F_1 = \frac{dp_1}{dt} + \Omega_2 P_3 - \Omega_3 P_2 \\ = \mu \left(\frac{dv_1}{dt} + \Omega_2 v_3 - \Omega_3 v_2 \right) \quad (\text{and cyclic permutations})$$

$$\vec{H} = \frac{d\vec{n}}{dt} = \frac{d'\vec{n}}{dt} + \vec{\omega} \times \vec{n}$$

$$\begin{aligned}\vec{H}_i &= \frac{d\vec{n}_i}{dt} + \epsilon_{ijk} \omega_j \vec{n}_k \\ &= I_i \frac{d\omega_i}{dt} + \epsilon_{ijk} \omega_j I_k \omega_k\end{aligned}$$

$$\begin{aligned}S_0 \quad \vec{H}_1 &= I_1 \omega_1 + \omega_2 \omega_3 I_3 - \omega_3 I_2 \omega_2 \\ &= I_1 \omega_1 + \omega_2 \omega_3 (I_3 - I_2) \quad (\text{and cyclic permutations})\end{aligned}$$

Wrt principal axes

$$P_i = \mu V_i, \quad i = 1, 2, 3$$

so that

$$\left(\frac{d' \mathbf{P}}{dt} \right)_i \equiv \frac{d P_i}{dt} = \mu \dot{V}_i, \quad (\boldsymbol{\Omega} \times \mathbf{P})_i = \sum_{j,k} \epsilon_{ijk} \Omega_j V_k$$

Thus,

$$\begin{aligned} F_1 &= \mu (\dot{V}_1 + \Omega_2 V_3 - \Omega_3 V_2) \\ F_2 &= \mu (\dot{V}_2 + \Omega_3 V_1 - \Omega_1 V_3) \\ F_3 &= \mu (\dot{V}_3 + \Omega_1 V_2 - \Omega_2 V_1) \end{aligned}$$

Torque equation:

$$\mathbf{K} = \frac{d' \mathbf{M}}{dt} = \frac{d' \mathbf{M}}{dt} + \boldsymbol{\Omega} \times \mathbf{M}$$

Wrt the principal axes

$$M_i = I_i \Omega_i, \quad i = 1, 2, 3$$

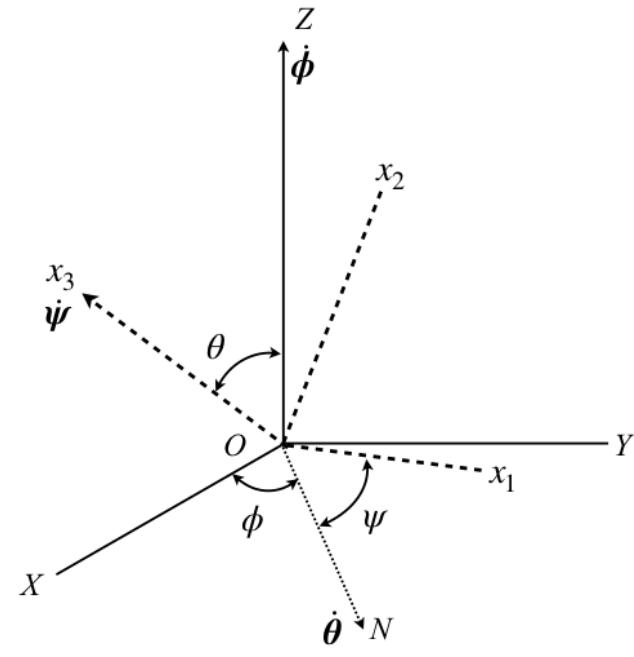
so that

$$\left(\frac{d' \mathbf{M}}{dt} \right)_i \equiv \frac{d M_i}{dt} = I_i \dot{\Omega}_i, \quad (\boldsymbol{\Omega} \times \mathbf{M})_i = \sum_{j,k} \epsilon_{ijk} \Omega_j M_k = \sum_{j,k} \epsilon_{ijk} \Omega_j \Omega_k I_k$$

Thus,

$$\begin{aligned} K_1 &= I_1 \dot{\Omega}_1 + \Omega_2 \Omega_3 (I_3 - I_2) \\ K_2 &= I_2 \dot{\Omega}_2 + \Omega_3 \Omega_1 (I_1 - I_3) \\ K_3 &= I_3 \dot{\Omega}_3 + \Omega_1 \Omega_2 (I_2 - I_1) \end{aligned}$$

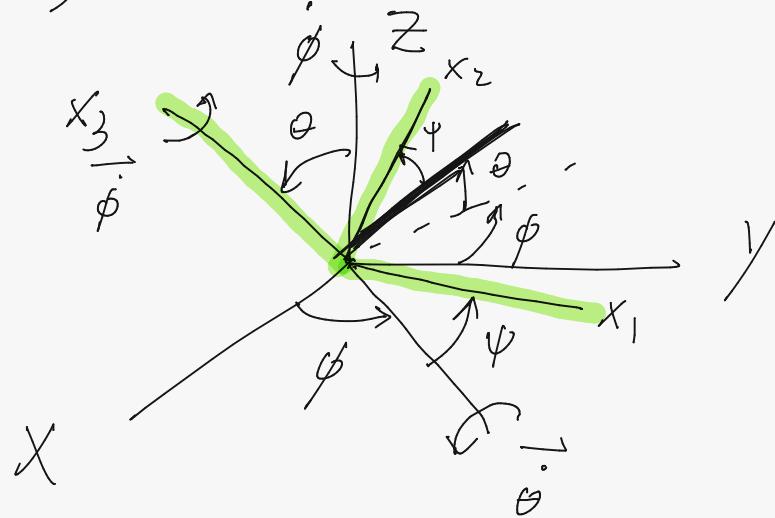
11) Draw a diagram showing the definition of the Euler angles (ϕ, θ, ψ).



First rotate around Z by ϕ , then around the transformed X axis (which is the line of nodes ON) by θ , and then around the transformed Z axis (which is now the x_3 axis) by ψ .

Perform Euler angle rotations of body frame

11) Euler angles,



$$12) \vec{\omega} = \dot{\phi} + \dot{\theta} + \dot{\psi}$$

$$\dot{\phi} = \dot{\phi} \left(\cos \theta \hat{x}_3 + \sin \theta \cos \psi \hat{x}_1 + \sin \theta \sin \psi \hat{x}_2 \right)$$

$$\dot{\theta} = \dot{\theta} \left(\cos \psi \hat{x}_1 - \sin \psi \hat{x}_2 \right)$$

$$\dot{\psi} = \dot{\psi} \hat{x}_3$$

$$\rightarrow \boxed{\vec{\omega} = (\dot{\theta} \cos \psi + \dot{\phi} \sin \theta \sin \psi) \hat{x}_1 + (-\dot{\theta} \sin \psi + \dot{\phi} \sin \theta \cos \psi) \hat{x}_2 + (\dot{\psi} + \dot{\phi} \cos \theta) \hat{x}_3}$$

```
In [12]: def Rx(a):
    """
    calculate passive rotation matrix around x-axis
    """

    R = np.array([[1, 0, 0],
                 [0, np.cos(a), np.sin(a)],
                 [0, -np.sin(a), np.cos(a)]])

    return R
```

```
In [13]: def Ry(a):
    """
    calculate passive rotation matrix around y-axis
    """

    R = np.array([[np.cos(a), 0, -np.sin(a)],
                 [0, 1, 0],
                 [np.sin(a), 0, np.cos(a)]])

    return R
```

```
In [14]: def Rz(a):
    """
    calculate passive rotation matrix around z-axis
    """

    R = np.array([[np.cos(a), np.sin(a), 0],
                 [-np.sin(a), np.cos(a), 0],
                 [0, 0, 1]])

    return R
```

```
In [15]: def rotate(axis, angle, prevRot):
    """
    actively rotate basis vectors about transformed axis thru angle (in radians)

    prevRot: previous rotation matrix (3x3)
    """

    # passive rotation matrix about axis thru angle
    if axis == 'x':
        rot = Rx(angle)

    if axis == 'y':
        rot = Ry(angle)

    if axis == 'z':
        rot = Rz(angle)
```

```
# convert to active rotation
R = np.linalg.inv(rot)

# conjugate R by previous active rotation to rotate around *transformed* axis
Rprime = np.dot(prevRot, np.dot(R, np.linalg.inv(prevRot)) )

# new combined rotation
newRot = np.dot(Rprime, prevRot)

# rotate basis vectors
ex = np.dot(newRot, np.array([1, 0, 0]))
ey = np.dot(newRot, np.array([0, 1, 0]))
ez = np.dot(newRot, np.array([0, 0, 1]))

return ex, ey, ez, newRot
```

```
In [16]: # interactive rotations

# initial rotation (identity)
prevRot = np.eye(3)

# loop for successive rotations
counter = 1
while l!=0:

    # input axis, angle
    print('\n')
    axis = input('input rotation axis (x,y,z; q to quit): ')
    if axis=='q':
        break
```

```

angle = input('input rotation angle (degrees): ')
# convert string input to float and degrees to radians
angle = float(angle)
angle = np.deg2rad(angle)

# perform rotation
ex, ey, ez, newRot = rotate(axis, angle, prevRot)

# plot
fig = plt.figure()
ax = fig.gca(projection='3d')
ax.set_axis_off()
ax.view_init(elev=20, azim=15)

# space frame
ax.quiver(0, 0, 0, 1, 0, 0, color='k', linestyle='-' )
ax.quiver(0, 0, 0, 0, 1, 0, color='k', linestyle='-' )
ax.quiver(0, 0, 0, 0, 0, 1, color='k', linestyle='-' )

# body frame
ax.quiver(0, 0, 0, ex[0], ex[1], ex[2], color='b', linestyle='--' )
ax.quiver(0, 0, 0, ey[0], ey[1], ey[2], color='g', linestyle='--' )
ax.quiver(0, 0, 0, ez[0], ez[1], ez[2], color='r', linestyle='--' )

# savefig
figtitle = 'euler_' + str(counter)
plt.savefig(figtitle, bbox_inches='tight', dpi=400)

# display figure
plt.show()

# prepare for next rotation
prevRot = newRot
counter = counter + 1

```

input rotation axis (x,y,z; q to quit): q

12) Calculate the components of Ω wrt body frame in terms of the Euler angles and their time derivatives.

From the above diagram, one sees that

$$\Omega = \dot{\phi} + \dot{\theta} + \dot{\psi}$$

where

$$\dot{\phi} = \dot{\phi} [\sin \theta \sin \psi \hat{x}_1 + \sin \theta \cos \psi \hat{x}_2 + \cos \theta \hat{x}_3] , \quad \dot{\theta} = \dot{\theta} [\cos \psi \hat{x}_1 - \sin \psi \hat{x}_2] , \quad \dot{\psi} = \dot{\psi} \hat{x}_3$$

Adding these together we get

$$\Omega = \Omega_1 \hat{x}_1 + \Omega_2 \hat{x}_2 + \Omega_3 \hat{x}_3$$

with

$$\Omega_1 = \dot{\phi} \sin \theta \sin \psi + \dot{\theta} \cos \psi , \quad \Omega_2 = \dot{\phi} \sin \theta \cos \psi - \dot{\theta} \sin \psi , \quad \Omega_3 = \dot{\phi} \cos \theta + \dot{\psi}$$

13) Solve for the reaction forces for rigid bodies in static equilibrium.

In static equilibrium a rigid body has no translational or rotational acceleration:

$$\frac{d\mathbf{P}}{dt} = 0 , \quad \frac{d\mathbf{M}}{dt} = 0$$

Given the EOMs for a rigid body, the above equations are equivalent to

$$\mathbf{F} \equiv \sum \mathbf{f} = 0 , \quad \mathbf{K} \equiv \sum \mathbf{r} \times \mathbf{f} = 0$$

where the reaction forces are included in the summations over \mathbf{f} and $\mathbf{r} \times \mathbf{f}$.

The number of force and torque equations (i.e., the number of different components, which is at most 6) must equal the number of unknown components of the reaction forces that you are trying to solve for.

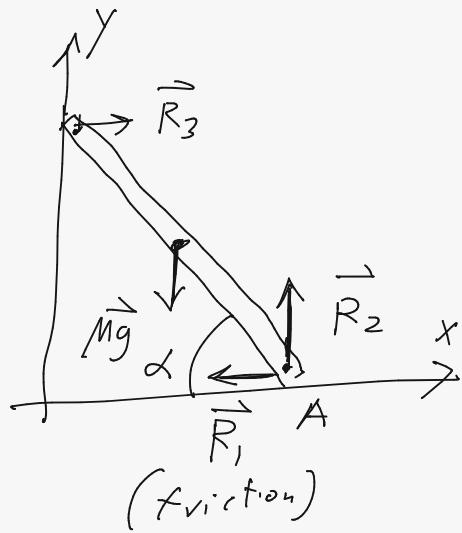
8. Non-inertial reference frames (39)

13) static equilibrium:

$$\frac{d\vec{P}}{dt} = \sum \vec{F} = 0 \quad , \quad \frac{d\vec{M}}{dt} = \sum \vec{r} \times \vec{F} = 0$$

Include reaction forces $\Rightarrow \sum \vec{F} = 0 \text{ and } \sum \vec{r} \times \vec{F} = 0$.

Example:



3 equations for 3 unknowns:

$$(i) \vec{R}_3 + \vec{R}_1 = 0$$

$$R_3 \hat{x} - R_1 \hat{x} = 0 \rightarrow \boxed{R_3 = R_1}$$

$$(ii) -Mg \hat{y} + R_2 \hat{y} = 0 \rightarrow \boxed{R_2 = Mg}$$

(iii) Torque about pt A:

$$-R_3 l \sin \alpha + Mg \frac{l}{2} \cos \alpha = 0$$

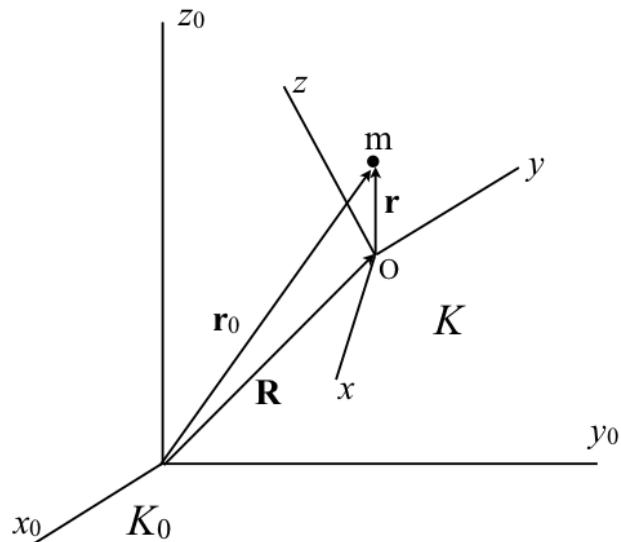
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so

$$\boxed{R_3 \sin \alpha = \frac{1}{2} Mg \cos \alpha} \rightarrow \boxed{R_3 = \frac{1}{2} \frac{Mg}{\tan \alpha}}$$

1) Draw a diagram relating an inertial and non-inertial reference frame.



Notation:

- K_0 : inertial frame
- K : non-inertial frame
- m : point mass m (not necessarily fixed in either frame)
- \mathbf{r}_0, \mathbf{r} : position vectors of m wrt to K_0, K
- \mathbf{R} : position vector of the origin O of the non-inertial reference frame

2) Write down the relationship between velocity vectors in inertial and non-inertial reference frames.

Since

$$\mathbf{r}_0 = \mathbf{R} + \mathbf{r}$$

it follows that

$$\mathbf{v}_0 \equiv \dot{\mathbf{r}}_0 = \mathbf{V} + \mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r}$$

where $\mathbf{V} \equiv \dot{\mathbf{R}}$ and $\boldsymbol{\Omega}$ are the translational and rotational velocity of K wrt K_0 , and \mathbf{v} is the velocity of m wrt K .

3) Distinguish non-inertial reference frames associated with translational and rotational motion.

- A non-inertial reference frame associated with translational motion would need to have a non-zero linear acceleration $\mathbf{W} \equiv \ddot{\mathbf{V}} = \ddot{\mathbf{R}}$.
- A non-inertial reference frame associated with rotational motion only needs to have a non-zero angular velocity $\boldsymbol{\Omega}$. A non-zero angular acceleration $\dot{\boldsymbol{\Omega}}$ is not required.

4) Derive the Coriolis, centrifugal, translational acceleration, and rotational acceleration fictitious force terms.

Newton's 2nd law in the inertial frame is:

$$m\mathbf{a}_0 = \mathbf{F}$$

where $\mathbf{a}_0 \equiv \dot{\mathbf{v}}_0$ is the acceleration of \mathbf{r}_0 in the inertial frame.

To obtain Newton's 2nd law in the non-inertial reference frame, we need to express \mathbf{a}_0 in terms of the acceleration \mathbf{a} wrt the non-inertial frame plus other terms, which give rise to fictitious forces.

Recall that the time derivative of any vector \mathbf{A} wrt the inertial frame K_0 is given by

$$\dot{\mathbf{A}} \equiv \frac{d\mathbf{A}}{dt} \Big|_0 = \frac{d\mathbf{A}}{dt} + \boldsymbol{\Omega} \times \mathbf{A}$$

8.) Non-inertial reference frames.

1)



(non-inertial frame)

$$\vec{r}_0 = \vec{R} + \vec{r}$$

(inertial)

2) velocity vector

$$\vec{v}_0 = \frac{d\vec{r}_0}{dt} \Big|_0 = \frac{d\vec{R}}{dt} \Big|_0 + \frac{d\vec{r}}{dt} \Big|_0$$

$$\overbrace{\vec{V}}^{\text{velocity of origin } O} = \frac{d\vec{R}}{dt} \Big|_0 \quad \text{and} \quad \frac{d\vec{r}}{dt} \Big|_0 = \frac{d\vec{r}}{dt} + \vec{\Omega} \times \vec{r}$$

velocity of origin O
w.r.t inertial frame

w
 \vec{v} : w.r.t non-inertial
frame

$$\text{Thus, } \vec{v}_0 = \vec{V} + \vec{v} + \vec{\Omega} \times \vec{r}$$

- 3) non-inertial frame:
 translational motion: need $\overrightarrow{W} = \frac{d\vec{V}}{dt} \Big|_0 = \frac{d\vec{R}}{dt^2} \Big|_0 \neq 0$
 rotational motion: need $\vec{\Omega} \neq 0$.

4) Newton's 2nd law in a non-inertial ref. frame.

$$\vec{F} = m\vec{a}_0 \quad (\text{w.r.t inertial frame})$$

$$\begin{aligned}
 \vec{a}_0 &= \frac{d\vec{v}_0}{dt} \Big|_0 \\
 &= \frac{d}{dt} \Big|_0 \left(\vec{V} + \vec{v} + \vec{\Omega} \times \vec{r} \right) \\
 &= \frac{d\vec{V}}{dt} \Big|_0 + \frac{d\vec{v}}{dt} \Big|_0 + \frac{d\vec{r}}{dt} \Big|_0 \times \vec{v} + \vec{\Omega} \times \frac{d\vec{r}}{dt} \Big|_0 \\
 &= \overrightarrow{W} + \frac{d\vec{v}}{dt} + \vec{\Omega} \times \vec{v} + \left(\frac{d\vec{\Omega}}{dt} + \vec{\Omega} \times \vec{\Omega} \right) \times \vec{r} + \vec{\Omega} \times \left(\frac{d\vec{r}}{dt} + \vec{\Omega} \times \vec{r} \right) \\
 &= \overrightarrow{a} + \overrightarrow{W} + \vec{\Omega} \times \vec{v} + \dot{\vec{\Omega}} \times \vec{r} + \vec{\Omega} \times \vec{v} + \vec{\Omega} \times (\vec{\Omega} \times \vec{r}) \\
 &= \overrightarrow{a} + \overrightarrow{W} + \vec{\Omega} \times \vec{v} + 2\vec{\Omega} \times \vec{v} + \vec{\Omega} \times (\vec{\Omega} \times \vec{r})
 \end{aligned}$$

\int_0

$$\vec{F} = m \vec{a}_0 \\ = m (\vec{a} + \vec{W} + \vec{\Omega} \times \vec{r} + 2\vec{\Omega} \times \vec{v} + \vec{\Omega} \times (\vec{\Omega} \times \vec{r}))$$

$$\rightarrow m \vec{a} = \vec{F} - m \vec{W} - m \vec{\Omega} \times \vec{r} - 2m \vec{\Omega} \times \vec{v} - m \vec{\Omega} \times (\vec{\Omega} \times \vec{r})$$

linear acceleration angular acceleration Coriolis Centrifugal

Alternative derivations:

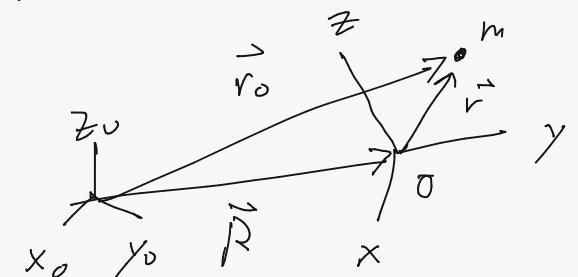
$$L = T - U \quad (\text{in an inertial frame})$$

$$= \frac{1}{2} m \vec{V}_0^2 - U \leftarrow U(r_0) = U(r)$$

$$= \frac{1}{2} m \left| \vec{V} + (\vec{v} + \vec{\Omega} \times \vec{r}) \right|^2 - U$$

$$= \frac{1}{2} m \vec{V}^2 + \frac{1}{2} m \left| \vec{v} + \vec{\Omega} \times \vec{r} \right|^2 + m \vec{V} \cdot (\vec{v} + \vec{\Omega} \times \vec{r}) - U$$

$$= \frac{1}{2} m \vec{V}^2 + \frac{1}{2} m v^2 + \frac{1}{2} m \left| \vec{\Omega} \times \vec{r} \right|^2 + m \vec{v} \cdot (\vec{\Omega} \times \vec{r}) \\ + m \vec{V} \cdot (\vec{v} + \vec{\Omega} \times \vec{r}) - U$$



$\vec{V}_{a/y}$ w.r.t \vec{r} and \vec{v} :

$$\delta L = m \vec{v} \cdot \delta \vec{v} + m (\vec{\Omega} \times \vec{r}) \cdot (\vec{\Omega} \times \delta \vec{r}) + m \delta \vec{v} \cdot (\vec{\Omega} \times \vec{r}) \\ + m \vec{v} \cdot (\vec{\Omega} \times \delta \vec{r}) + m \vec{\nabla} \cdot \delta \vec{v} + m \vec{\nabla} \cdot (\vec{\Omega} \times \delta \vec{r}) \\ - \frac{\partial U}{\partial r} \cdot \delta r$$

$$\rightarrow \frac{\partial L}{\partial \vec{v}} = m \vec{v} + m (\vec{\Omega} \times \vec{r}) + m \vec{\nabla}$$

$$\frac{\partial L}{\partial \vec{r}} = m (\vec{\Omega} \times \vec{r}) \times \vec{\Omega} + m \vec{v} \times \vec{\Omega} + m (\vec{\nabla} \times \vec{r})$$

$$S \circ \frac{d}{dt} \left(\frac{\partial L}{\partial \vec{v}} \right) = \frac{\partial L}{\partial \vec{r}} \quad (m \rho \text{ lies})$$

$$m \vec{a} + m (\vec{\Omega} \times \vec{r}) + m (\vec{\Omega} \times \vec{v}) + m \frac{d \vec{\nabla}}{dt}$$

w.r.t non
inertial
frame

$$= m (\vec{\Omega} \times \vec{r}) \times \vec{\Omega} + m (\vec{v} \times \vec{\Omega}) + m (\vec{\nabla} \times \vec{r})$$

$$\begin{aligned}
 \text{L} \cdot m \vec{a} &= -m \vec{\omega} \times (\vec{\omega} \times \vec{v}) - 2m \vec{\omega} \times \vec{v} - m \left(\frac{d\vec{V}}{dt} + \vec{\omega} \times \vec{V} \right) - m \vec{\omega} \times \vec{r} \\
 &= -m \vec{\omega} \times (\vec{\omega} \times \vec{v}) - 2m \vec{\omega} \times \vec{v} - m \overbrace{\vec{W}}^{\uparrow} - m \vec{\omega} \times \vec{r}
 \end{aligned}$$

accels. of origin O
 wrt inertial frame

where $d\mathbf{A}/dt$ is the time derivative of \mathbf{A} wrt the non-inertial frame K . (The time derivative of a vector wrt to any reference frame is obtained by simply time differentiating the Cartesian components of that vector wrt that frame.)

Applying this formula to each side of the velocity vector

$$\mathbf{v}_0 = \mathbf{V} + \mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r}$$

we have

LHS:

$$\mathbf{a}_0 \equiv \frac{d\mathbf{v}_0}{dt} \Big|_0$$

RHS:

$$\frac{d\mathbf{V}}{dt} \Big|_0 \equiv \dot{\mathbf{V}} \equiv \mathbf{W}, \quad \frac{d\mathbf{v}}{dt} \Big|_0 = \mathbf{a} + \boldsymbol{\Omega} \times \mathbf{v}, \quad \frac{d}{dt} \Big|_0 (\boldsymbol{\Omega} \times \mathbf{r}) = \dot{\boldsymbol{\Omega}} \times \mathbf{r} + \boldsymbol{\Omega} \times (\mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r})$$

Thus,

$$\mathbf{a}_0 = \mathbf{W} + \mathbf{a} + \dot{\boldsymbol{\Omega}} \times \mathbf{r} + 2\boldsymbol{\Omega} \times \mathbf{v} + \boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \mathbf{r})$$

Newton's 2nd law in a non-inertial reference frame:

$$m\mathbf{a} = \mathbf{F} - m\mathbf{W} - m\dot{\boldsymbol{\Omega}} \times \mathbf{r} - 2m\boldsymbol{\Omega} \times \mathbf{v} - m\boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \mathbf{r})$$

The fictitious forces terms on the RHS are associated with translational acceleration, rotational acceleration, Coriolis, and centrifugal forces.

The above equation can also be derived from Lagrange's equations starting with the Lagrangian

$$L = \frac{1}{2}m|\mathbf{v}_0|^2 - U = \frac{1}{2}m(\mathbf{V} + \mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r}) \cdot (\mathbf{V} + \mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r}) - U$$

The variation of L wrt \mathbf{r} and \mathbf{v} is

$$\delta L = m\delta\mathbf{v} \cdot (\mathbf{V} + \mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r}) + m(\boldsymbol{\Omega} \times \delta\mathbf{r}) \cdot (\mathbf{V} + \mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r}) - \frac{\partial U}{\partial \mathbf{r}} \cdot \delta\mathbf{r}$$

which implies

$$\frac{\partial L}{\partial \mathbf{r}} = -\frac{\partial U}{\partial \mathbf{r}} - m\boldsymbol{\Omega} \times (\mathbf{V} + \mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r}), \quad \frac{\partial L}{\partial \mathbf{v}} = m(\mathbf{V} + \mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r})$$

Lagrange's equations:

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \mathbf{v}} \right) = \frac{\partial L}{\partial \mathbf{r}}$$

LHS

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \mathbf{v}} \right) = m \left(\frac{d\mathbf{V}}{dt} + \mathbf{a} + \dot{\boldsymbol{\Omega}} \times \mathbf{r} + \boldsymbol{\Omega} \times \mathbf{v} \right)$$

where we used $\mathbf{v} \equiv d\mathbf{r}/dt$, $\mathbf{a} \equiv d\mathbf{v}/dt$, and $\dot{\boldsymbol{\Omega}} \equiv d\boldsymbol{\Omega}/dt|_0 = d\boldsymbol{\Omega}/dt$ since $\boldsymbol{\Omega} \times \boldsymbol{\Omega} = 0$.

Equating with $\partial L/\partial \mathbf{r}$ gives

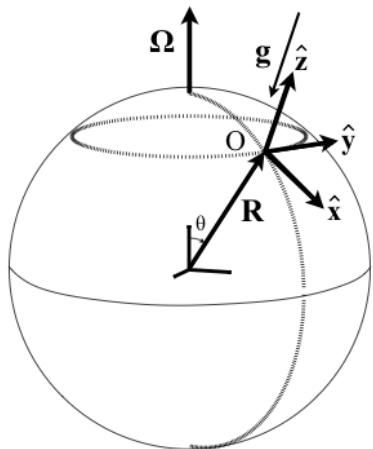
$$m\mathbf{a} = -\frac{\partial U}{\partial \mathbf{r}} - m\mathbf{W} - m\dot{\boldsymbol{\Omega}} \times \mathbf{r} - 2m\boldsymbol{\Omega} \times \mathbf{v} - m\boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \mathbf{r})$$

where we used $\mathbf{W} \equiv \dot{\mathbf{V}} = d\mathbf{V}/dt + \boldsymbol{\Omega} \times \mathbf{V}$.

5) Explain the physical significance of Foucault's pendulum.

The precession of the plane of oscillation of Foucault's pendulum is proof that a lab attached to the surface of the Earth is a non-inertial reference frame.

Reference frame:



Precession of plane of oscillation:



The main contribution to the precession comes from Earth's daily rotational motion. One solves

$$ma = \mathbf{T} + mg - 2m\boldsymbol{\Omega} \times \mathbf{v}$$

for the motion of the pendulum bob in the xy -plane, ignoring any motion in the vertical direction.

Code for producing the precessional motion is given below.

In [17]: # Foucault pendulum analysis

```
# some constants
T_day = 24*3660 #s
D = 1 # m
g = 9.8 # m/s^2
L = 30 # m
lat = 49 # degree (Paris)
theta = 90-lat # degree

# angular frequency of oscillation
# NOTE: reduced by a factor of 200 so that one can easily see precessi
on after a few oscillations
w = np.sqrt(g/L) * (1/200)
T = 2*np.pi/w # period
print('T = ', T, 'sec')
Nt = 10000
t = np.linspace(0, 3*T, Nt)

# angular velocity
Omega = 2*np.pi/T_day
Omega_z = Omega*np.cos(np.deg2rad(theta))

# solution
x = D*( np.cos(Omega_z*t)*np.cos(w*t) + (Omega_z/w)*np.sin(Omega_z*t)*
np.sin(w*t) )
y = D*(-np.sin(Omega_z*t)*np.cos(w*t) + (Omega_z/w)*np.cos(Omega_z*t)*
np.sin(w*t) )

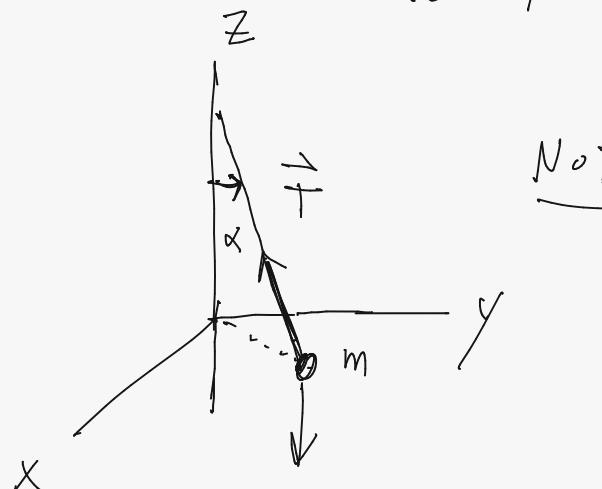
# plot trajectory in x-y plane
plt.figure()
plt.plot(x, y)
plt.axis('equal')
plt.xlim(-1.2, 1.2)
plt.ylim(-1.2, 1.2)
plt.axis('equal')
plt.xlabel('x [m]')
plt.ylabel('y [m]')
plt.title('Foucault pendulum: precession of plane of oscillation')
```

5) Significance of Foucault's pendulum: a bob attached to the surface of the Earth is a non-inertial reference frame.

Using $\vec{\omega} = \omega \hat{z}$, $\vec{W} = 0$ (ignoring yearly orbital motion)

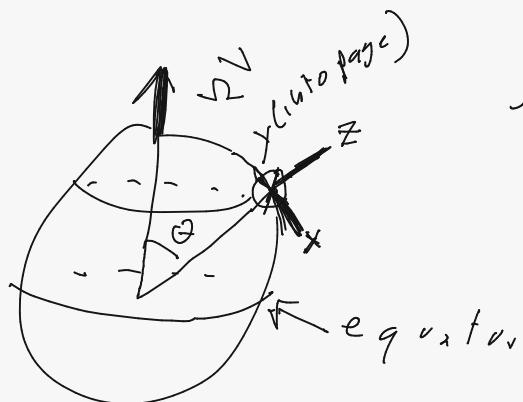
$$\rightarrow m\vec{a} = \vec{F} - 2m\vec{\omega} \times \vec{v} - m\vec{\omega} \times (\vec{\omega} \times \vec{v})$$

$$\approx \vec{T} + m\vec{g} - 2m\vec{\omega} \times \vec{v}$$



NOTE: $\Omega = \frac{2\pi}{1 \text{ day}} = \frac{2\pi}{24 \cdot 60 \cdot 60 \text{ sec.}} \approx \frac{1}{43,200}$

$$\approx \frac{1}{15,000}$$



so $\vec{\omega} \times (\vec{\omega} \times \vec{v}) \ll 1$

can be ignored relative to $\vec{\omega} \times \vec{v}$

$$\vec{\omega} = \Omega_{\text{rot}} \hat{z} - \Omega_{\text{rot}} \theta \hat{x}$$

Ignore motion in z-direction:

$$\vec{v} \approx \dot{x}\hat{x} + \dot{y}\hat{y}$$

$$\vec{a} \approx \ddot{x}\hat{x} + \ddot{y}\hat{y}$$

$$\vec{\Omega} = -\Omega_{\text{rot}}\theta \hat{x} + \Omega_{\text{rot}}\theta \hat{z}$$

$$\vec{T} = T_{\cos\alpha} \hat{z} - \underbrace{T_{\sin\alpha} \cos\phi}_{x/L} \hat{x} - \underbrace{T_{\sin\alpha} \sin\phi}_{y/L} \hat{y}$$

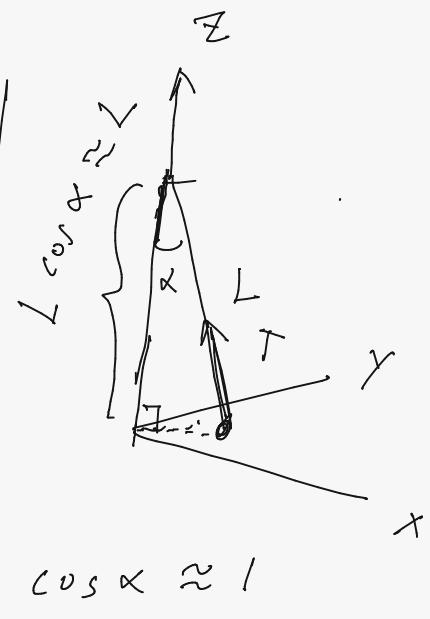
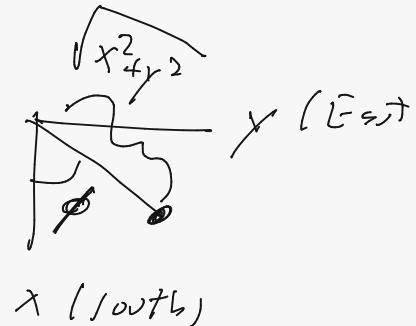
$$\rightarrow \vec{\Omega} \times \vec{v} = -\Omega_{\text{rot}}\theta \hat{y} \hat{z} + \Omega_{\text{rot}}\theta (\dot{x}\hat{y} - \dot{y}\hat{x})$$

$$\vec{mg} = -mg \hat{z} = \Omega \hat{z}$$

$$\text{by, } m\ddot{x} = -T x/L + 2m\Omega_{\text{rot}}\theta \dot{y}$$

$$m\ddot{y} = -T y/L - 2m\Omega_{\text{rot}}\theta \dot{x}$$

$$0 = m\ddot{z} \approx T - mg + \underbrace{2m\Omega_{\text{rot}}\theta \dot{y}}_{\text{ignore relative to other terms}}$$



$$\rightarrow \ddot{x} \approx -\frac{g}{L}x + 2\Omega_z \dot{y}$$

$$\ddot{y} \approx -\frac{g}{L}y - 2\Omega_z \dot{x}$$

Define $\frac{g}{L} = \omega^2$

$$\rightarrow \ddot{x} \approx -\omega^2 x + 2\Omega_z \dot{y}$$

$$\ddot{y} \approx -\omega^2 y - 2\Omega_z \dot{x}$$

Define: $\xi = x + iy \rightarrow \bar{\xi} = \dot{x} + i\dot{y} \rightarrow \ddot{\xi} = \ddot{x} + i\ddot{y}$

$$\ddot{x} + i\ddot{y} \approx -\omega^2(x+iy) + 2\Omega_z \underbrace{(y-i\dot{x})}_{-i(\dot{x}+i\dot{y})}$$

$$\ddot{\xi} \approx -\omega^2 \xi - 2i\Omega_z \bar{\xi}$$

Thus, $\boxed{\ddot{\xi} + 2i\Omega_z \bar{\xi} + \omega^2 \xi = 0}$

$$\text{Ansatz: } \xi = e^{i\lambda t}$$

$$\begin{aligned} \rightarrow 0 &= \ddot{\xi} + 2i\Omega_z \dot{\xi} + \omega^2 \xi \\ &= (-\lambda^2 + 2i\Omega_z(\lambda) + \omega^2) e^{i\lambda t} \\ &= -\lambda^2 - 2\Omega_z \lambda + \omega^2 \\ &= \lambda^2 + 2\Omega_z \lambda - \omega^2 \end{aligned}$$

$$\lambda = \frac{-2\Omega_z \pm \sqrt{4\Omega_z^2 + 4\omega^2}}{2}$$

$$= -\Omega_z \pm \sqrt{\Omega_z^2 + \omega^2}$$

$$\approx -\Omega_z \pm \omega \quad (\text{only } \omega \gg \Omega_z)$$

$$\begin{aligned} \text{Thus, } \xi(t) &= A e^{i\lambda_+ t} + B e^{i\lambda_- t} \\ &= A e^{-i(\Omega_z - \omega)t} + B e^{-i(\Omega_z + \omega)t} \end{aligned}$$



$$\ddot{z}(t) = (A e^{i\omega t} + B e^{-i\omega t}) e^{-i\Omega_2 t}$$

Initial conditions:

$$x(0) = D, \quad y(0) = 0, \quad \dot{x}(0) = 0, \quad \dot{y}(0) = 0$$

$$\rightarrow z(0) = D, \quad \dot{z}(0) = 0$$

$$\text{so } D = A + B$$

$$\begin{aligned} 0 &= A(i\omega - i\Omega_2) + B(-i\omega - i\Omega_2) \\ &= (A - B)\omega - (A + B)\Omega_2 \end{aligned}$$

$$\text{Then, } 0 = (A - B)\omega - D\Omega_2$$

$$\begin{aligned} \rightarrow A - B &= D \left(\frac{\Omega_2}{\omega} \right) \quad \rightarrow \quad A = \frac{1}{2} D \left(1 + \frac{\Omega_2}{\omega} \right) \\ A + B &= D \quad \quad \quad B = D - \frac{1}{2} D \left(1 + \frac{\Omega_2}{\omega} \right) \\ &= \frac{1}{2} D \left(1 - \frac{\Omega_2}{\omega} \right) \end{aligned}$$

$$\bar{z} = x + iy$$

$$x = \operatorname{Re} \bar{z}$$

$$y = \operatorname{Im} \bar{z}$$

$$\begin{aligned}\bar{z}(t) &= \left(\frac{1}{2} D \left(1 + \frac{\Omega_x}{\omega} \right) e^{i\omega t} + \frac{1}{2} D \left(1 - \frac{\Omega_x}{\omega} \right) e^{-i\omega t} \right) e^{-i\Omega_x t} \\ &= \left[\frac{1}{2} D \left(e^{i\omega t} + e^{-i\omega t} \right) + \frac{1}{2} D \frac{\Omega_x}{\omega} \left(e^{i\omega t} - e^{-i\omega t} \right) \right] e^{-i\Omega_x t} \\ &= D \left(\cos \omega t + i \frac{\Omega_x}{\omega} \sin \omega t \right) \left(\cos(\Omega_x t) - i \sin(\Omega_x t) \right)\end{aligned}$$

$$= D \left(\cos \omega t \cos(\Omega_x t) + \frac{\Omega_x}{\omega} \sin \omega t \sin(\Omega_x t) \right)$$

$$+ i D \left(\frac{\Omega_x}{\omega} \sin \omega t \cos(\Omega_x t) - \cos \omega t \sin(\Omega_x t) \right)$$

$$\rightarrow x(t) = D \left(\cos \omega t \cos(\Omega_x t) + \frac{\Omega_x}{\omega} \sin \omega t \sin(\Omega_x t) \right)$$

$$y(t) = D \left(\cos \omega t \sin(\Omega_x t) + \frac{\Omega_x}{\omega} \sin \omega t \cos(\Omega_x t) \right)$$

$$\begin{bmatrix} \vec{x}(t) \\ \vec{y}(t) \end{bmatrix} = \begin{bmatrix} \cos(\Omega_z t) & \sin(\Omega_z t) \\ -\sin(\Omega_z t) & \cos(\Omega_z t) \end{bmatrix} \begin{bmatrix} D \cos(\omega t) \\ D \frac{\Omega_z}{\omega} \sin(\omega t) \end{bmatrix}$$

passive rotation by $\Omega_z t$

In frame rotating with $\Omega_z t \rightarrow$

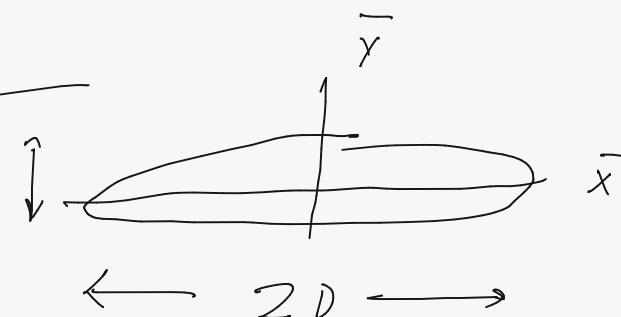
$$\bar{x}(t) = D \cos(\omega t)$$

$$\bar{y}(t) = D \left(\frac{\Omega_z}{\omega} \right) \sin(\omega t)$$

$$s_0 \left(\frac{\bar{x}(t)}{D} \right)^2 + \left(\frac{\bar{y}(t)}{D \frac{\Omega_z}{\omega}} \right)^2 = 1$$

$\underbrace{\hspace{10em}}$
e llipse

$$\left(\frac{\Omega_z}{\omega} \ll 1 \right)$$



```
T = 2198.6568517060523 sec
```

```
Out[17]: Text(0.5, 1.0, 'Foucault pendulum: precession of plane of oscillatio  
n')
```

