Fourier's Law and the Heat Equation

Chapter Two

Fourier’s Law

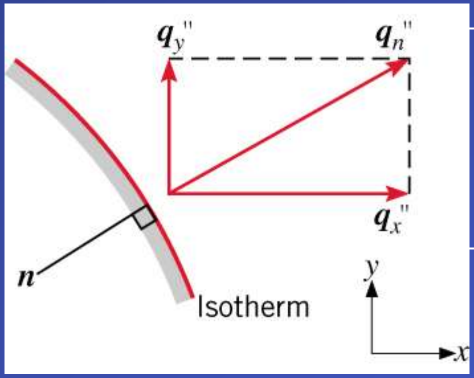
- A rate equation that allows determination of the conduction heat flux from knowledge of the temperature distribution in a medium

- Its most general (vector) form for multidimensional conduction is:

$$\vec{q''} = -k \vec{\nabla} T$$

Implications:

– Heat transfer is in the direction of decreasing temperature (basis for minus sign).



– Fourier’s Law serves to define the thermal conductivity of the medium $\left(k \equiv -\vec{q''} / \vec{\nabla} T \right)$

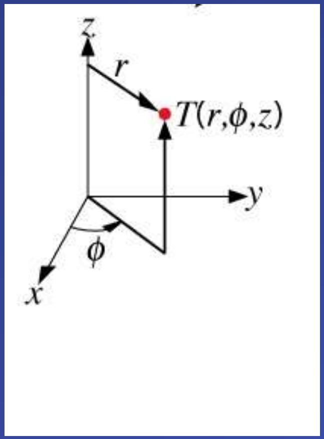
– Direction of heat transfer is perpendicular to lines of constant temperature (isotherms).

– Heat flux vector may be resolved into orthogonal components.

Heat Flux Components

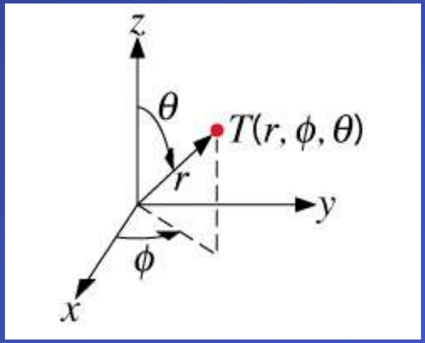
- Cartesian Coordinates: $T\left(x, y, z\right)$

$$\vec{q}'' = \underbrace{-k\frac{\partial T}{\partial x}}_{q''_x}\vec{i} \underbrace{-k\frac{\partial T}{\partial y}}_{q''_y}\vec{j} \underbrace{-k\frac{\partial T}{\partial z}}_{q''_z}\vec{k} \quad (2.3)$$



- Cylindrical Coordinates: $T\left(r, \phi, z\right)$

$$\vec{q}'' = \underbrace{-k\frac{\partial T}{\partial r}}_{q''_r}\vec{i} \underbrace{-k\frac{\partial T}{r\partial \phi}}_{q''_\phi}\vec{j} \underbrace{-k\frac{\partial T}{\partial z}}_{q''_z}\vec{k} \quad (2.18)$$



- Spherical Coordinates: $T\left(r, \phi, \theta\right)$

$$\vec{q}'' = \underbrace{-k\frac{\partial T}{\partial r}}_{q''_r}\vec{i} \underbrace{-k\frac{\partial T}{r\partial \theta}}_{q''_\theta}\vec{j} \underbrace{-k\frac{\partial T}{r\sin\theta\,\partial \phi}}_{q''_\phi}\vec{k} \quad (2.21)$$

- In angular coordinates $(\phi \text{ or } \phi, \theta)$, the temperature gradient is still based on temperature change over a length scale and hence has units of °C/m and not °C/deg.

- Heat rate for one-dimensional, radial conduction in a cylinder or sphere:

  – Cylinder

$$q_r = A_r q_r'' = 2\pi r L q_r''$$

or,

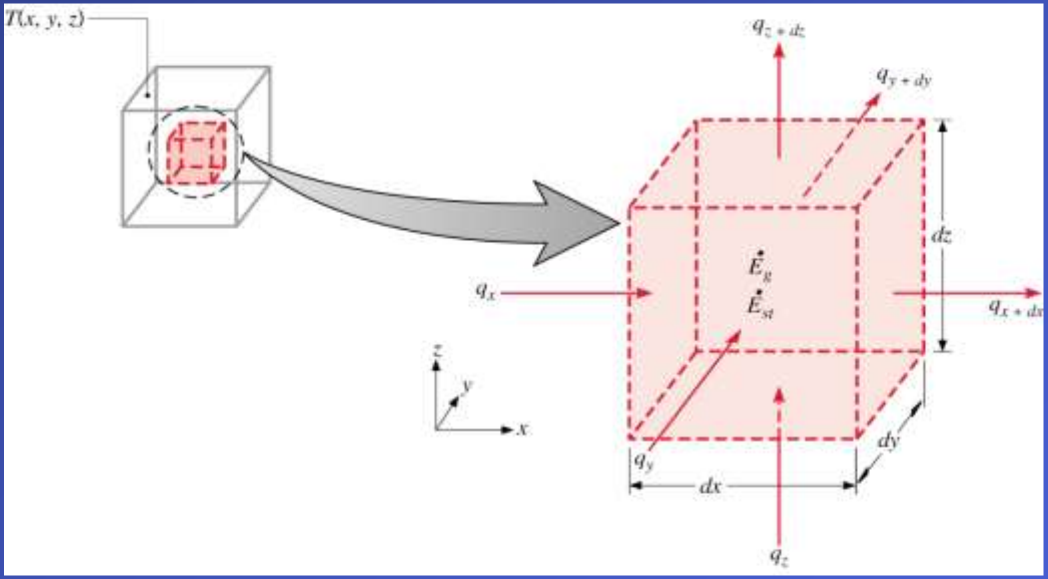
$$q_r' = A_r' q_r'' = 2\pi r q_r''$$

  – Sphere

$$q_r = A_r q_r'' = 4\pi r^2 q_r''$$

The Heat Equation

- A differential equation whose solution provides the temperature distribution in a stationary medium.
- Based on applying conservation of energy to a differential control volume through which energy transfer is exclusively by conduction.
- Cartesian Coordinates:



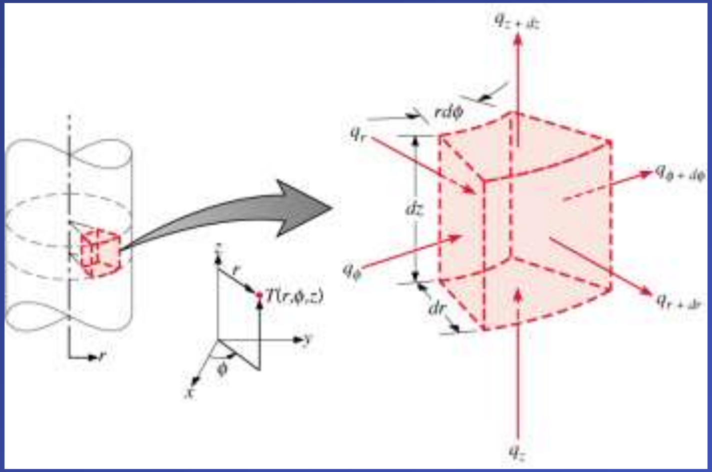
$$\underbrace{\frac{\partial}{\partial x}\left(k\frac{\partial T}{\partial x}\right)+\frac{\partial}{\partial y}\left(k\frac{\partial T}{\partial y}\right)+\frac{\partial}{\partial z}\left(k\frac{\partial T}{\partial z}\right)}_{\text{Net transfer of thermal energy into the control volume (inflow-outflow)}}+\underbrace{\dot{q}}_{\text{Thermal energy generation}}=\underbrace{\rho c_p\frac{\partial T}{\partial t}}_{\text{Change in thermal energy storage}} \qquad (2.13)$$

Net transfer of thermal energy into the control volume (inflow-outflow)

Thermal energy generation

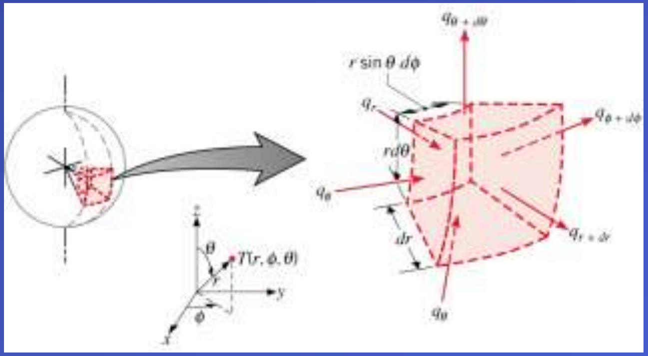
Change in thermal energy storage

- Cylindrical Coordinates:



$$\frac{1}{r}\frac{\partial}{\partial r}\left(kr\frac{\partial T}{\partial r}\right)+\frac{1}{r^2}\frac{\partial}{\partial \phi}\left(k\frac{\partial T}{\partial \phi}\right)+\frac{\partial}{\partial z}\left(k\frac{\partial T}{\partial z}\right)+\dot{q}=\rho c_p\frac{\partial T}{\partial t} \qquad (2.20)$$

- Spherical Coordinates:



$$\frac{1}{r^2}\frac{\partial}{\partial r}\left(kr^2\frac{\partial T}{\partial r}\right)+\frac{1}{r^2\sin^2\theta}\frac{\partial}{\partial \phi}\left(k\frac{\partial T}{\partial \phi}\right)+\frac{1}{r^2\sin\theta}\frac{\partial}{\partial \theta}\left(k\sin\theta\frac{\partial T}{\partial \theta}\right)+\dot{q}=\rho c_p\frac{\partial T}{\partial t} \qquad (2.33)$$

- One-Dimensional Conduction in a Planar Medium with Constant Properties and No Generation

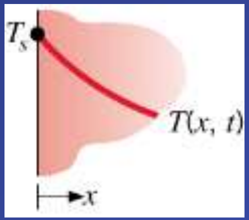
$$\frac{\partial^2 T}{\partial x^2} = \frac{1}{\alpha}\frac{\partial T}{\partial t}$$

$$\alpha \equiv \frac{k}{\rho c_p} \rightarrow$$ thermal diffusivity of the medium

Boundary and Initial Conditions

- For transient conduction, heat equation is first order in time, requiring specification of an initial temperature distribution: $T(x,t)_{t=0} = T(x,0)$
- Since heat equation is second order in space, two boundary conditions must be specified. Some common cases:

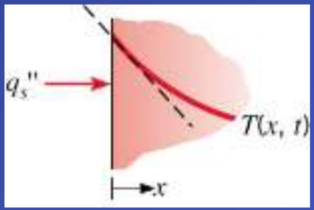
Constant Surface Temperature:



$$T(0,t) = T_s$$

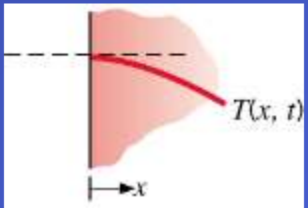
Constant Heat Flux:

Applied Flux



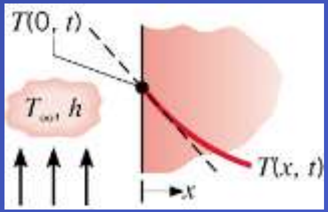
$$-k\frac{\partial T}{\partial x}\Big|_{x=0} = q_s''$$

Insulated Surface



$$\frac{\partial T}{\partial x}\Big|_{x=0} = 0$$

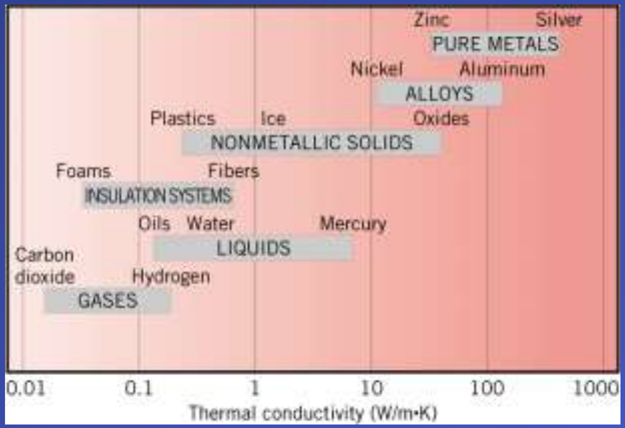
Convection



$$-k\frac{\partial T}{\partial x}\Big|_{x=0} = h\left[T_\infty - T(0,t)\right]$$

Thermophysical Properties

Thermal Conductivity: A measure of a material's ability to transfer thermal energy by conduction.



Thermal Diffusivity: A measure of a material's ability to respond to changes in its thermal environment.

Property Tables:

Solids: Tables A.1 – A.3

Gases: Table A.4

Liquids: Tables A.5 – A.7

Methodology of a Conduction Analysis

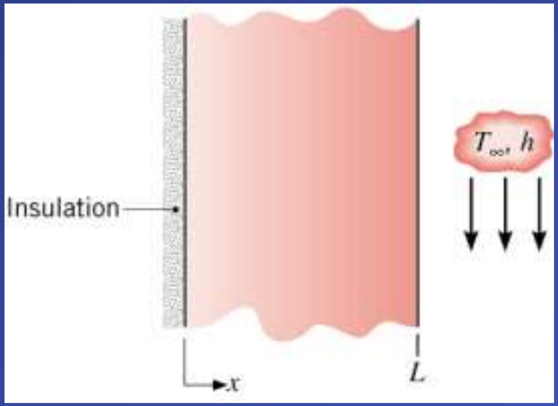
- Solve appropriate form of heat equation to obtain the temperature distribution.

- Knowing the temperature distribution, apply Fourier's Law to obtain the heat flux at any time, location and direction of interest.

- Applications:

  Chapter 3: One-Dimensional, Steady-State Conduction
  Chapter 4: Two-Dimensional, Steady-State Conduction
  Chapter 5: Transient Conduction

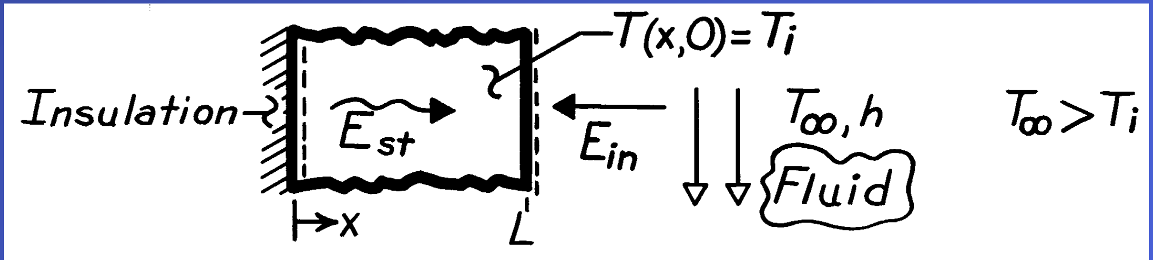
Problem 2.46 Thermal response of a plane wall to convection heat transfer.



KNOWN: Plane wall, initially at a uniform temperature, is suddenly exposed to convective heating.

FIND: (a) Differential equation and initial and boundary conditions which may be used to find the temperature distribution, T(x,t); (b) Sketch T(x,t) for the following conditions: initial ($t \leq 0$), steady-state ($t \to \infty$), and two intermediate times; (c) Sketch heat fluxes as a function of time at the two surfaces; (d) Expression for total energy transferred to wall per unit volume (J/m^3).

SCHEMATIC:



ASSUMPTIONS: (1) One-dimensional conduction, (2) Constant properties, (3) No internal heat generation.

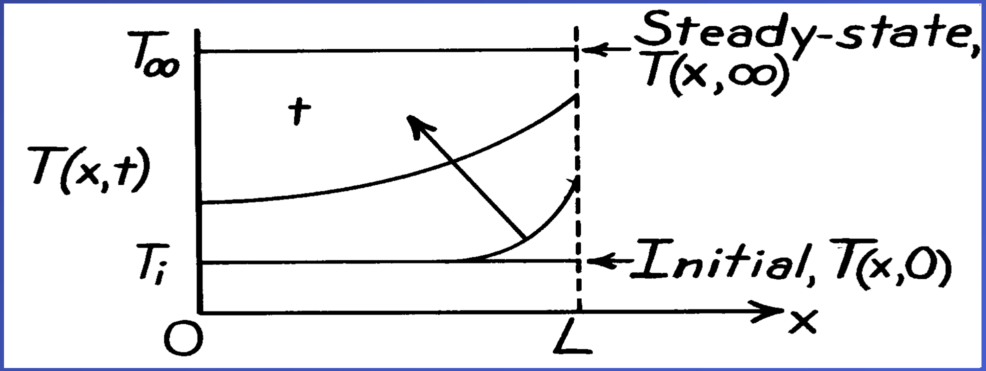
ANALYSIS: (a) For one-dimensional conduction with constant properties, the heat equation has the form,

$$\frac{\partial^2 T}{\partial x^2} = \frac{1}{\alpha}\frac{\partial T}{\partial t}$$

and the conditions are:

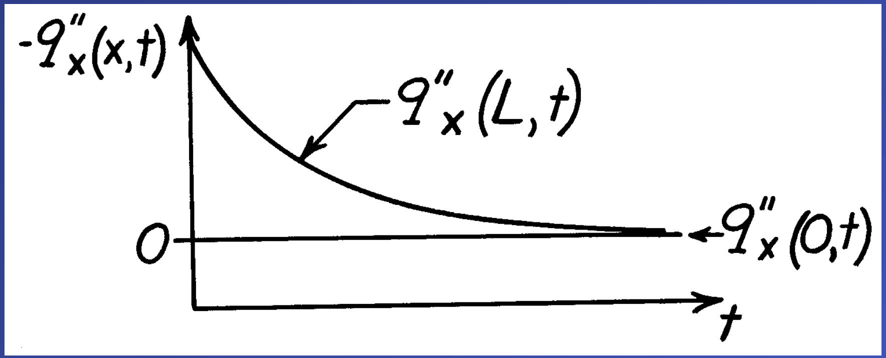
$$\begin{cases} \text{Initial, } t \le 0: & T(x,0) = T_i & \text{uniform temperature} \\ \text{Boundaries: } x=0 & \partial T/\partial x)_0 = 0 & \text{adiabatic surface} \\ \qquad x=L & -k\partial T/\partial x)_L = h\left[T(L,t) - T_\infty\right] & \text{surface convection} \end{cases}$$

(b) The temperature distributions are shown on the sketch.



Note that the gradient at x = 0 is always zero, since this boundary is adiabatic. Note also that the gradient at x = L decreases with time.

c) The heat flux, $q''_x(x,t)$, as a function of time, is shown on the sketch for the surfaces x = 0 and x = L.



d) The total energy transferred to the wall may be expressed as

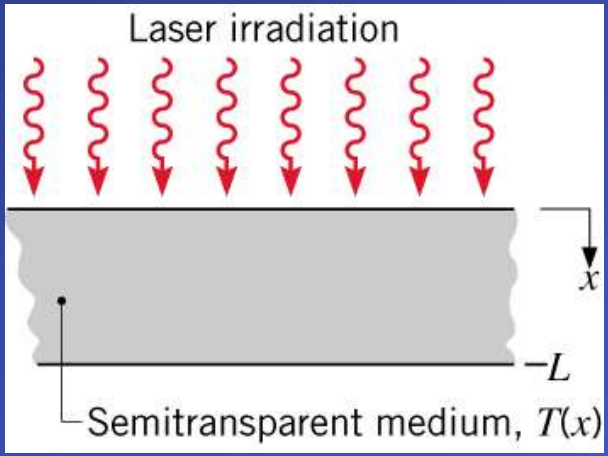
$$E_{in} = \int_0^\infty q''_{conv} A_s dt$$

$$E_{in} = hA_s \int_0^\infty \left(T_\infty - T(L,t)\right) dt$$

Dividing both sides by $A_s L$, the energy transferred per unit volume is

$$\frac{E_{in}}{V} = \frac{h}{L} \int_0^\infty \left[T_\infty - T(L,t)\right] dt \qquad \left[J/m^3\right]$$

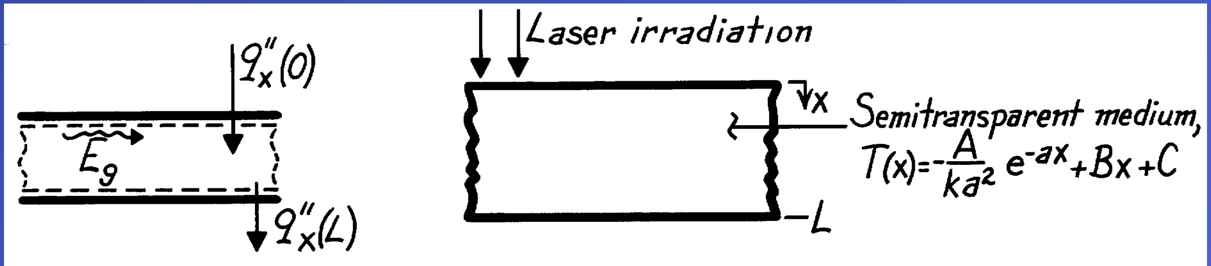
Problem 2.28 Surface heat fluxes, heat generation and total rate of radiation absorption in an irradiated semi-transparent material with a prescribed temperature distribution.



KNOWN: Temperature distribution in a semi-transparent medium subjected to radiative flux

FIND: (a) Expressions for the heat flux at the front and rear surfaces, (b) The heat generation rate $\dot{q}(x)$, and (c) Expression for absorbed radiation per unit surface area.

SCHEMATIC:



ASSUMPTIONS: (1) Steady-state conditions, (2) One-dimensional conduction in medium, (3) Constant properties, (4) All laser irradiation is absorbed and can be characterized by an internal volumetric heat generation term $\dot{q}(x)$.

ANALYSIS: (a) Knowing the temperature distribution, the surface heat fluxes are found using Fourier's law,

$$q''_x = -k\left[\frac{dT}{dx}\right] = -k\left[-\frac{A}{ka^2}(-a)e^{-ax} + B\right]$$

Front Surface, x=0: $q''_x(0) = -k\left[+\frac{A}{ka}\cdot 1 + B\right] = -\left[\frac{A}{a} + kB\right]$ <

Rear Surface, x=L: $q''_x(L) = -k\left[+\frac{A}{ka}e^{-aL} + B\right] = -\left[\frac{A}{a}e^{-aL} + kB\right].$ <

(b) The heat diffusion equation for the medium is

$$\frac{d}{dx}\left(\frac{dT}{dx}\right) + \frac{\dot{q}}{k} = 0 \quad \text{or} \quad \dot{q} = -k\frac{d}{dx}\left(\frac{dT}{dx}\right)$$

$$\dot{q}(x) = -k\frac{d}{dx}\left[+\frac{A}{ka}e^{-ax} + B\right] = Ae^{-ax}.$$

(c) Performing an energy balance on the medium,

$$\dot{E}_{in} - \dot{E}_{out} + \dot{E}_g = 0$$

On a unit area basis

$$\dot{E}''_g = -\dot{E}''_{in} + \dot{E}''_{out} = -q''_x(0) + q''_x(L) = +\frac{A}{a}\left(1 - e^{-aL}\right). \qquad <$$

Alternatively, evaluate $\dot{E}''_g$ by integration over the volume of the medium,

$$\dot{E}''_g = \int_0^L \dot{q}(x)dx = \int_0^L Ae^{-ax}dx = -\frac{A}{a}\left[e^{-ax}\right]_0^L = \frac{A}{a}\left(1 - e^{-aL}\right).$$