
```

clc; clear; close all;
E      = 30e6;
G      = 12e6;

cost = @(l,h,t,b) 2.21*l*h^2 + 0.048*(b*t*(14+l));
buckling_load = @(b,t) (4.013*sqrt((E*G*b^2*t^6)/36)/196)*...
    (1-(t/28)*sqrt(E/(4*G)));
M = @(l,b,t) 6000*(14 + 0.5*l);
R = @(l,h,t) 0.5*sqrt(l^2 + (h + t)^2);
J = @(l,h,t) sqrt(2)*h*l*((l^2)/12) + ((h + t)^2)/4);
shear_stress = @(l,h,t,b) sqrt((6000/(sqrt(2)*h*l))^2 + ...
    (6000/sqrt(2)*h)*(M(l,b,t)/J(l,h,t)) + ...
    ((M(l,b,t)*R(l,h,t))/J(l,h,t))^2);
bending_stress = @(l,h,t,b) 84*6000/(b*t^2);
end_deflection = @(l,h,t,b) (10976*6000)/(E*b*t^3);

% Inequality Constraints

h1 = @(l,h,t,b,s1) b-2 + s1^2;
h2 = @(l,h,t,b,s2) 0.125-h + s2^2;
h3 = @(l,h,t,b,s3) h-2 + s3^2;
h4 = @(l,h,t,b,s4) h-b + s4^2;
h5 = @(l,h,t,b,s5) 0.1-t + s5^2;
h6 = @(l,h,t,b,s6) t-10 + s6^2;
h7 = @(l,h,t,b,s7) 0.1-l + s7^2;
h8 = @(l,h,t,b,s8) l-10 + s8^2;
h9 = @(l,h,t,b,s9) 6000-buckling_load(b,t) + s9^2;
h10 = @(l,h,t,b,s10) shear_stress(l,h,t,b)-13600 + s10^2;
h11 = @(l,h,t,b,s11) bending_stress(l,h,t,b)-30000 + s11^2;
h12 = @(l,h,t,b,s12) end_deflection(l,h,t,b)-0.25 + s12^2;

L = @(l,h,t,b,...
    p1,p2,p3,p4,p5,p6,p7,p8,p9,p10,p11,p12,...
    s1,s2,s3,s4,s5,s6,s7,s8,s9,s10,s11,s12)...
    cost(l,h,t,b)...
    + p1 * h1 (l,h,t,b,s1) ...
    + p2 * h2 (l,h,t,b,s2) ...
    + p3 * h3 (l,h,t,b,s3) ...
    + p4 * h4 (l,h,t,b,s4) ...
    + p5 * h5 (l,h,t,b,s5) ...
    + p6 * h6 (l,h,t,b,s6) ...
    + p7 * h7 (l,h,t,b,s7) ...
    + p8 * h8 (l,h,t,b,s8) ...
    + p9 * h9 (l,h,t,b,s9) ...
    + p10 * h10(l,h,t,b,s10)...
    + p11 * h11(l,h,t,b,s11)...
    + p12 * h12(l,h,t,b,s12);

syms l h t b
syms p1 p2 p3 p4 p5 p6 p7 p8 p9 p10 p11 p12
syms s1 s2 s3 s4 s5 s6 s7 s8 s9 s10 s11 s12

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state_array = [l h t b...
               p1 p2 p3 p4 p5 p6 p7 p8 p9 p10 p11 p12...
               s1 s2 s3 s4 s5 s6 s7 s8 s9 s10 s11 s12];

J = gradient(L,state_array);

for k = 1:length(J)
    fprintf("dL_d" + string(state_array(k)) + ...
           " = " + string(J(k)) + ";\n");
end

int_guess = ones(1,28);
int_guess(1:4) = [5 1 5 1.2];

state_out = fsolve(@derivatives_question_5,int_guess);

fprintf("\nl = %0.2f inches\n",state_out(1));
fprintf("h = %0.2f inches\n",state_out(2));
fprintf("t = %0.2f inches\n",state_out(3));
fprintf("b = %0.2f inches\n",state_out(4));
fprintf("cost = $%0.2f\n",cost(state_out(1),state_out(2),...
                             state_out(3),state_out(4)));

l = state_out(1);
h = state_out(2);
t = state_out(3);
b = state_out(4);

fprintf("\nbuckling load = %0.2f psi\n",buckling_load(b,t));
fprintf("shear stress = %0.2f psi\n",shear_stress(l,h,t,b));
fprintf("bending stress = %0.2f psi\n",bending_stress(l,h,t,b));
fprintf("end deflection = %0.2f inches\n",end_deflection(l,h,t,b));

dL_dl = p8 - p7 + (6*b*t)/125 + (221*h^2)/100 - (p10*(36000000/
(h^2*l^3) - (437328071996551125*2^(1/2))/(68719476736*l*((h +
t)^2/4 + l^2/12)) + (1166208191990803*2^(1/2)*(3000*l + 84000))/
(3298534883328*((h + t)^2/4 + l^2/12)^2) - (3000*l + 84000)^2/
(4*h^2*l*((h + t)^2/4 + l^2/12)^2) + (1166208191990803*2^(1/2)*(3000*l
+ 84000))/(549755813888*l^2*((h + t)^2/4 + l^2/12)) + ((3000*l +
84000)^2*((h + t)^2 + l^2))/(24*h^2*l*((h + t)^2/4 + l^2/12)^3)
+ ((3000*l + 84000)^2*((h + t)^2 + l^2))/(4*h^2*l^3*((h + t)^2/4
+ l^2/12)^2) - ((18000000*l + 504000000)*((h + t)^2 + l^2))/
(8*h^2*l^2*((h + t)^2/4 + l^2/12)^2))/(2*(18000000/(h^2*l^2) +
(1166208191990803*2^(1/2)*(3000*l + 84000))/(549755813888*l*((h
+ t)^2/4 + l^2/12)) + ((3000*l + 84000)^2*((h + t)^2 + l^2))/
(8*h^2*l^2*((h + t)^2/4 + l^2/12)^2))^(1/2));
dL_dh = p3 - p2 + p4 + (221*h*l)/50 - (p10*(36000000/(h^3*l^2) +
((3000*l + 84000)^2*((h + t)^2 + l^2))/(4*h^3*l^2*((h + t)^2/4
+ l^2/12)^2) - ((3000*l + 84000)^2*(2*h + 2*t))/(8*h^2*l^2*((h
+ t)^2/4 + l^2/12)^2) + (1166208191990803*2^(1/2)*(3000*l +
84000)*(h/2 + t/2))/(549755813888*l*((h + t)^2/4 + l^2/12)^2)

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+ ((3000*1 + 84000)^2*((h + t)^2 + 1^2)*(h/2 + t/2))/
(4*h^2*1^2*((h + t)^2/4 + 1^2/12)^3))/ (2*(18000000/(h^2*1^2) +
(1166208191990803*2^(1/2)*(3000*1 + 84000))/(549755813888*1*((h
+ t)^2/4 + 1^2/12)) + ((3000*1 + 84000)^2*((h + t)^2 + 1^2))/
(8*h^2*1^2*((h + t)^2/4 + 1^2/12)^2))^^(1/2));
dL_dt = p6 - p5 + (6*b*(1 + 14))/125 +
p9*((501625*2^(1/2)*5^(1/2)*10^(1/2)*(b^2*t^6)^^(1/2))/2744
+ (3009750*10^(1/2)*b^2*t^5*((2^(1/2)*5^(1/2)*t)/112 - 1))/
(49*(b^2*t^6)^^(1/2))) - (1008000*p11)/(b*t^3) - (4116*p12)/(625*b*t^4)
- (p10*((1166208191990803*2^(1/2)*(3000*1 + 84000)*(h/2 + t/2))/
(549755813888*1*((h + t)^2/4 + 1^2/12)^2) - ((3000*1 + 84000)^2*(2*h +
2*t))/(8*h^2*1^2*((h + t)^2/4 + 1^2/12)^2) + ((3000*1 + 84000)^2*((h
+ t)^2 + 1^2)*(h/2 + t/2))/(4*h^2*1^2*((h + t)^2/4 + 1^2/12)^3))/
(2*(18000000/(h^2*1^2) + (1166208191990803*2^(1/2)*(3000*1 + 84000))/
(549755813888*1*((h + t)^2/4 + 1^2/12)) + ((3000*1 + 84000)^2*((h +
t)^2 + 1^2))/(8*h^2*1^2*((h + t)^2/4 + 1^2/12)^2))^^(1/2));
dL_db = p1 - p4 + (6*t*(1 + 14))/125 -
(504000*p11)/(b^2*t^2) - (1372*p12)/(625*b^2*t^3) +
(1003250*10^(1/2)*b*p9*t^6*((2^(1/2)*5^(1/2)*t)/112 - 1))/
(49*(b^2*t^6)^^(1/2));
dL_dp1 = b + s1^2 - 2;
dL_dp2 = s2^2 - h + 1/8;
dL_dp3 = h + s3^2 - 2;
dL_dp4 = h - b + s4^2;
dL_dp5 = s5^2 - t + 1/10;
dL_dp6 = t + s6^2 - 10;
dL_dp7 = s7^2 - 1 + 1/10;
dL_dp8 = 1 + s8^2 - 10;
dL_dp9 = s9^2 + (1003250*10^(1/2)*((2^(1/2)*5^(1/2)*t)/112 -
1)*(b^2*t^6)^^(1/2))/49 + 6000;
dL_dp10 = (18000000/(h^2*1^2) + (1166208191990803*2^(1/2)*(3000*1
+ 84000))/(549755813888*1*((h + t)^2/4 + 1^2/12)) + ((3000*1
+ 84000)^2*((h + t)^2 + 1^2))/(8*h^2*1^2*((h + t)^2/4 +
1^2/12)^2))^^(1/2) + s10^2 - 13600;
dL_dp11 = s11^2 + 504000/(b*t^2) - 30000;
dL_dp12 = s12^2 + 1372/(625*b*t^3) - 1/4;
dL_ds1 = 2*p1*s1;
dL_ds2 = 2*p2*s2;
dL_ds3 = 2*p3*s3;
dL_ds4 = 2*p4*s4;
dL_ds5 = 2*p5*s5;
dL_ds6 = 2*p6*s6;
dL_ds7 = 2*p7*s7;
dL_ds8 = 2*p8*s8;
dL_ds9 = 2*p9*s9;
dL_ds10 = 2*p10*s10;
dL_ds11 = 2*p11*s11;
dL_ds12 = 2*p12*s12;

```

Solver stopped prematurely.

fsolve stopped because it exceeded the function evaluation limit,
options.MaxFunctionEvaluations = 2800 (the default value).

l = 6.08 inches
h = 0.94 inches
t = 1.75 inches
b = 1.58 inches
cost = \$14.60

buckling load = 523386.08 psi
shear stress = 9177.91 psi
bending stress = 103878.28 psi
end deflection = 0.26 inches

Published with MATLAB® R2018a