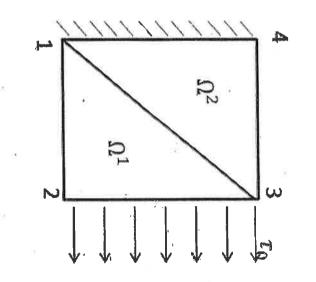
Example:

AMENDED VERSION

is fixed to the wall (left) and pulled by a Compute the displacements if the constant traction $\tau_0 = 1000 \text{N/mm}$. material has $E = 30 \cdot 10^6 N/mm^2$ and Consider a rectangular piece of 120x160 mm and thickness 0.036mm. It

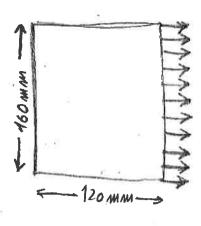


The traction is given in units of strength length, so the Q's must be computed without multiplying by

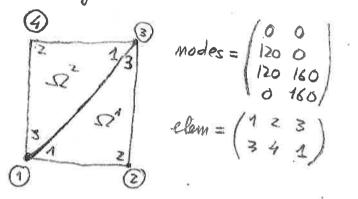
Numerical Factory

Plane Stress 2 Thang. pdf

EXAMPLE



Left edge fixed.



$$modes = \begin{pmatrix} 0 & 0 \\ 120 & 0 \\ 120 & 160 \\ 0 & 160 \end{pmatrix}$$

$$elem = \begin{pmatrix} 1 & 2 & 3 \\ 3 & 4 & 1 \end{pmatrix}$$

Stress problem:

$$G_{11} = G_{22} = \frac{E}{1-\nu^{2}} = \frac{3\times10^{7}}{1-0.25^{2}} = \frac{16}{5}\times10^{7} = 3.2\times10^{7}$$

$$C_{12} = C_{1} = \nu C_{M} = 0.8 \times 10^{7}$$

$$C_{33} = \frac{E}{Z(1+V)} = \frac{3 \times 10^{7}}{Z(1+0.25)} = \frac{3 \times 10^{7}}{Z \cdot 5} = \frac{6}{5} \times 10^{7} = 1.02 \times 10^{7}, \text{ hence}: C = \left(\frac{C_{1} \cdot C_{12}}{C_{23}}\right) = 4.10 \cdot \left(\frac{8}{28} \cdot \frac{21}{33}\right)$$

· Local stiffness matrices:

$$\beta^{1} = (x_{1}^{1} - x_{3}^{1}) = 0.160 = -160, \quad x_{1}^{1} = -(x_{1}^{1} - x_{3}^{1}) = -(120-120) = 0,$$

$$\beta^{1}_{2} = (x_{3}^{1} - x_{4}^{1}) = 160 - 0 = 160, \quad x_{2}^{1} = -(x_{3}^{1} - x_{4}^{1}) = -(120-0) = 120,$$

$$\beta^{1}_{3} = (x_{4}^{1} - x_{2}^{1}) = -(0.120) = 120,$$

Area1: A= 2120+160 = 9600 mm2.

$$B_{4} = \frac{1}{2A_{4}} \begin{pmatrix} \beta_{4}^{1} & 0 & \beta_{2}^{1} & 0 & \beta_{3}^{1} & 0 \\ 0 & \delta_{1}^{1} & 0 & \delta_{2}^{1} & 0 & \delta_{3}^{1} \\ \delta_{1}^{1} & \beta_{1}^{1} & \delta_{2}^{1} & \beta_{2}^{2} & \delta_{3}^{1} & \beta_{3}^{4} \end{pmatrix} = \frac{1}{480} \begin{pmatrix} -4 & 0 & 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & -3 & 0 & 3 \\ 0 & -4 & -3 & 4 & 3 & 0 \end{pmatrix}$$

$$R^{1} = A_{1}th B_{1}^{T} C_{1}B_{1} = 6.10^{3}$$
, $\begin{pmatrix} -4 & 0 & 0 & 0 \\ 0 & 0 & -4 \\ 4 & 0 & -3 \\ 0 & -3 & 4 \\ 0 & 0 & 3 \\ 0 & 3 & 0 \end{pmatrix}$ $\begin{pmatrix} -4 & 0 & 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & -3 & 0 & 3 \\ 0 & -3 & 4 & 3 & 0 \\ 0 & 3 & 0 & 0 & 0 \end{pmatrix}$ herefore:

Therefore:

$$| \beta^{1} | = 6 \times 10^{3} \cdot \begin{vmatrix} 128 & 0 & | & -128 & 24 & | & 0 & -24 \\ 0 & 48 & 36 & -48 & -36 & 0 \\ -128 & 36 & 155 & -60 & -27 & 24 \\ 24 & -48 & -60 & 120 & 36 & -72 \\ \hline 0 & -36 & -27 & 36 & 27 & 0 \\ -24 & 0 & 24 & -72 & 0 & 72 \end{vmatrix} = | K_{i}^{2} | \text{ Since }, \text{ for the given mush}$$

$$| \beta_{i}^{2} = -\beta_{i}^{2}, \text{ and } | \delta_{i}^{2} = -\delta_{i}^{3},$$

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· Global Stiffness Matrix

$$K = \begin{pmatrix} K_{11}^{1} + K_{23}^{2} & K_{12}^{1} & K_{13}^{1} + K_{31}^{2} & K_{32}^{2} \\ * & K_{22}^{1} & K_{23}^{1} & O \\ * & * & K_{33}^{1} + K_{41}^{2} & K_{12}^{2} \\ * & * & * & * \end{pmatrix}$$

Remarks. It = It and now His (e=hz) are the 2x2 blocs in the local stiffness matrices (x)

= 6 × 103.	155	0 120	-128 36	-	4	-60 0	-27 24	36 -72
	-158		155	80	-27	24	0	0
	24 .	-98	-60	120	36	-72	0	0
	t	-60	-27	36	155	0	-128	24
	60	0	24	-72	0	120		-48
	-27		0	0	-128	36	155	-60
	36 -	+2	0	0	24	-48	-60	

· Boundary Conditions

- Essential B.C.: (U1, V1) = (0,0), (U4, V4) = (0,0).

- Natural B.C.

$$Q^{4} = \begin{pmatrix} Q_{1}^{4} \\ Q_{2}^{1} \\ Q_{3}^{1} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^{2} \\ A_{2}^{2} & A_{3}^{2} \end{pmatrix} = \begin{pmatrix} A_{1}^{2} & A_{2}^$$

$$Q = \begin{pmatrix} Q_1 \\ Q_2 = Q_2^4 \\ Q_3 = Q_3^4 + Q_1^2 \\ Q_4 = Q_2^2 \end{pmatrix} = \begin{pmatrix} Q_1 \\ 8 \times 10^9 \\ Q_4 \end{pmatrix}$$

Renark: the traction To Is given in N/mm (units: Force/ length), so we compute the Q's without multiplying by the

thickness

$$Q^2 = \begin{pmatrix} Q_1 \\ Q_2^2 \\ Q_3^2 \end{pmatrix} = \begin{pmatrix} Q_1 \\ Q_2^2 \\ Q_3^2 \end{pmatrix}$$

$$Q_{3} = Q_{3}^{1} + Q_{4}^{1}$$

$$= Q_{31}^{1} + Q_{32}^{1} + Q_{33}^{1} + Q_{33}^{1} + Q_{33}^{1} + Q_{13}^{2} + Q_{13}^{2} = Q_{32}^{1} + Q_{32}^{1} + Q_{13}^{2} = Q_{32}^{1} + Q_{32}^{1} + Q_{13}^{2} = Q_{32}^{1} + Q_{13}^{2} = Q_{32}^{1} + Q_{13}^{2} + Q_{13}^{2} = Q_{32}^{1} + Q_{13}^{2} + Q_{13}^{2} = Q_{13}^{1} + Q_{13}^{2} + Q_{13}^{2} = Q_{13}^{2} + Q_{13}^{2} + Q_{13}^{2} = Q_{13}^{2} + Q_{13}^{2} + Q_{13}^{2} + Q_{13}^{2} + Q_{13}^{2} = Q_{13}^{2} + Q_{13}^{$$

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Reduced system
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Remark. F=0: no internal forces (for ex. weight, inertial forces,...) are tower into

$$6 \times 10^{3} \times \begin{pmatrix} 155 & -60 & | -27 & 24 \\ -60 & 120 & 36 & -72 \\ \hline -27 & 36 & 155 & 0 \\ 24 & -72 & 0 & 120 \end{pmatrix} \begin{pmatrix} \overline{V_{z}} \\ \overline{V_{3}} \\ \overline{V_{3}} \end{pmatrix} = \frac{1}{\sqrt{2}} \times 8 \times 10^{4} \begin{pmatrix} 1 \\ 0 \\ \hline 3 \end{pmatrix}$$

$$t = 0.036 \text{ mm}$$
 $t = 0.48 \left(\frac{0}{10} \right)$
 $t = 0.48 \left(\frac{0}{10} \right)$

(globel)

Solution:
$$V_2 = 4.0648 \times 10^3 \text{ mm} \ 1.4291 \times 10^4 \text{ mm}$$

$$V_2 = 7.0692 \times 10^4 \text{ mm} \ 1.9637 \times 10^4 \text{ mm}$$

$$V_3 = 3.6406 \times 10^3 \text{ mm} \ 1.0113 \times 10^4 \text{ mm}$$

$$V_3 = -3.8881 \times 10^4 \text{ mm} \ -1.0800 \times 10^4 \text{ mm}$$

So, the displacements (in mm) are:

displacements (in mm) are:

$$V_1 = 0$$
 $V_2 = 4.0648 \times 10^{-3}$
 $V_2 = 7.0692 \times 10^{-4}$
 $V_3 = 3.6406 \times 10^{-3}$
 $V_4 = 0$
 $V_4 = 0$
 $V_4 = 0$
 $V_4 = 0$
 $V_5 = 0$
 $V_6 = 0$
 $V_7 = 0$
 $V_8 = 0$
 $V_$

Stress:

Remark 3. When using linear briangular elements, $\sigma = \begin{pmatrix} \sigma_x \\ \sigma_y \end{pmatrix} \mathcal{E} = \begin{pmatrix} \frac{\partial \sigma}{\partial x} \\ \frac{\partial v}{\partial y} \end{pmatrix}$ (i.e. the Stress and the strains respectively) are constant on each element.

$$\begin{cases} \sigma_{N}^{2} \\ \sigma_{1}^{2} \\ \end{pmatrix} = \frac{4 \times 10^{6}}{480} \begin{pmatrix} 7 & 2 \\ 2 & 8 \\ 3 \end{pmatrix} \begin{pmatrix} -\frac{1}{4} & 0.4 & 0.0 & 0 \\ 0.0 & 0.3 & 0.3 \\ 0.-\frac{1}{4} & 3.4 & 3.0 \end{pmatrix} \begin{pmatrix} u_{1}^{4} = \sqrt{4} & 0.0 \\ v_{2}^{2} = \sqrt{2} = 4.0697 \times 10^{3} \\ v_{3}^{2} = \sqrt{2} = 7.0697 \times 10^{3} \\ v_{1}^{2} = \sqrt{2} = 7.0697 \times 10^{3} \\ v_{2}^{3} = \sqrt{2} = 7.0697 \times 10^{3} \\ v_{3}^{2} = \sqrt{2} = 7.069$$